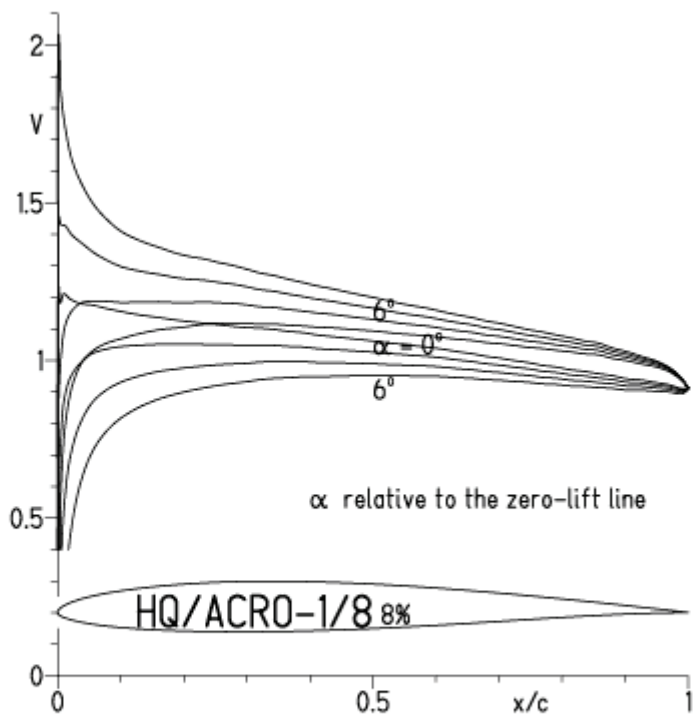


HQ/ACRO-1/8, N=11

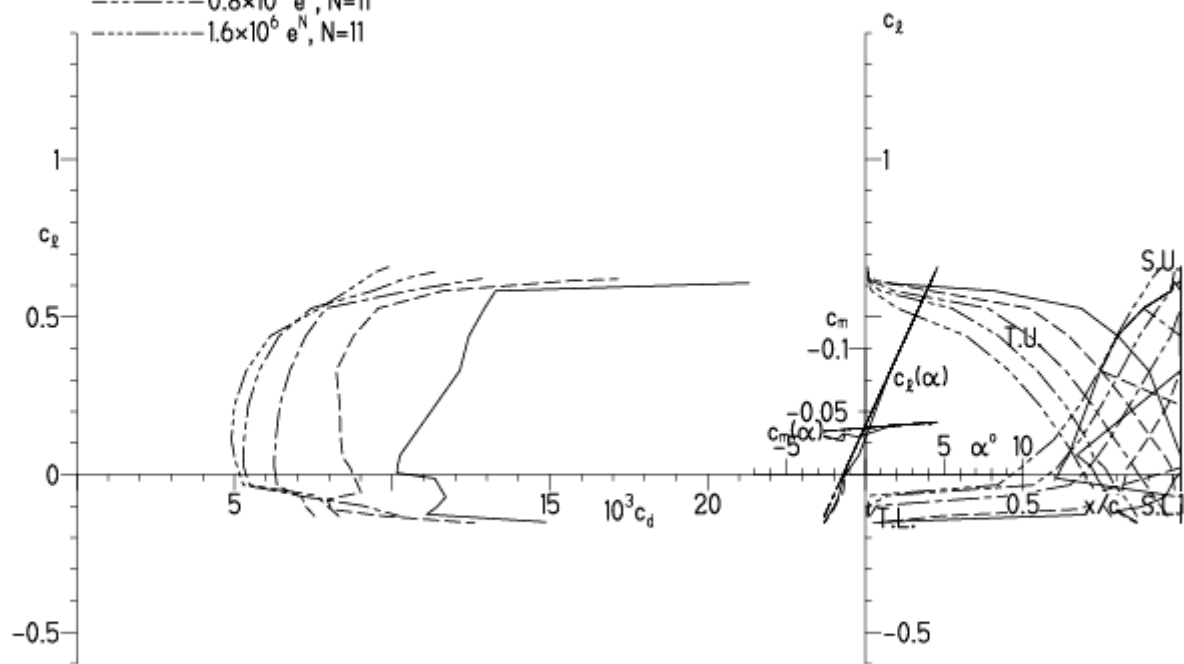
EPPLER 2005 V. 8.5.07 RUN 8.3.12 11:03



EPPLER 2005 V. 8.5.07 RUN 8.3.12 11:03

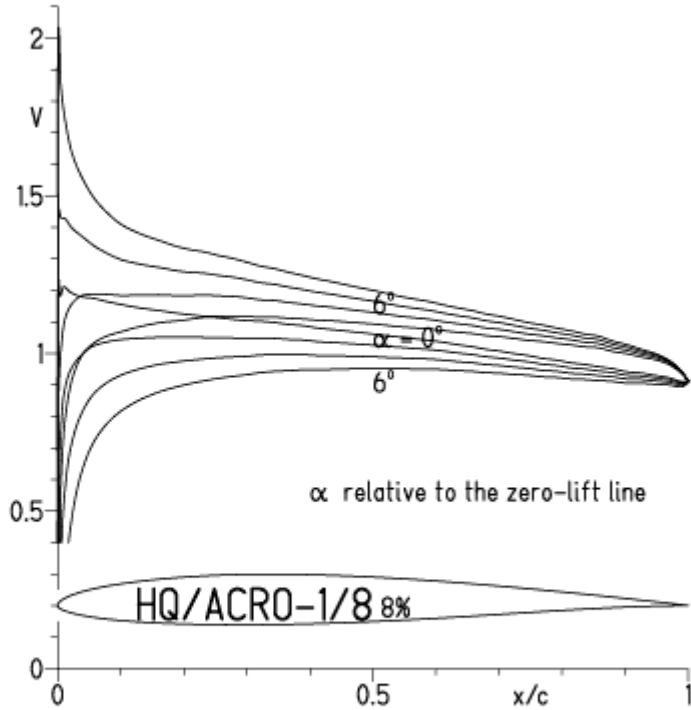
HQ/ACRO-1/8 8%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1/8, N=9

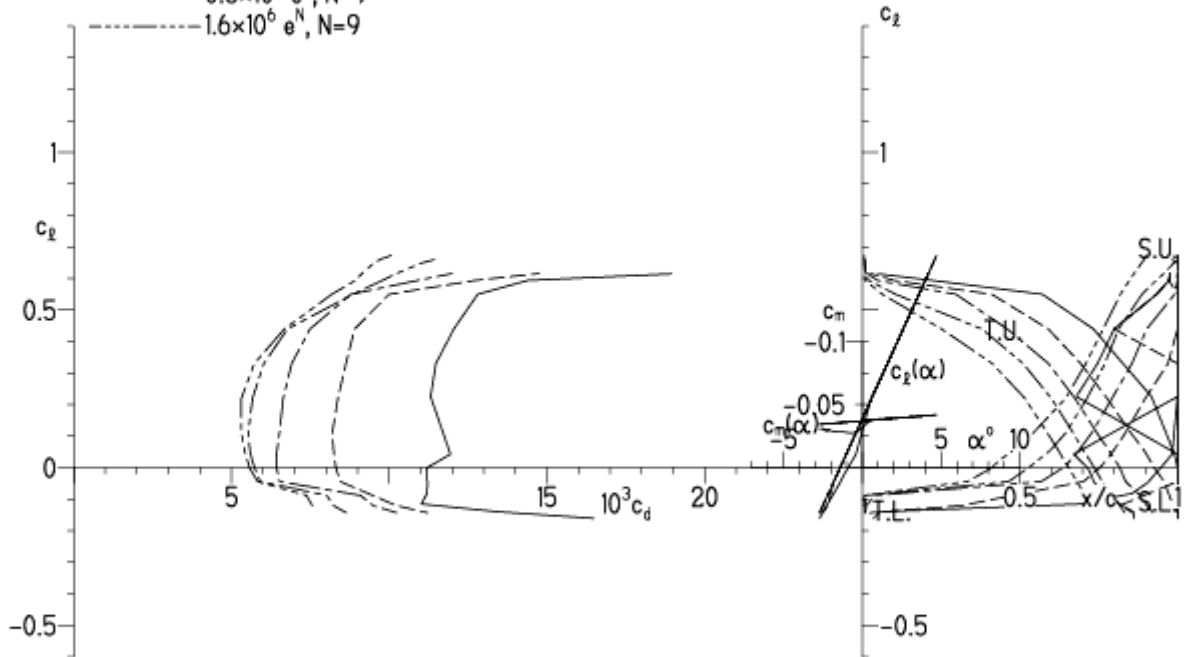
EPPLER 2005 V. 8.5.07 RUN 8.3.12 11:20



EPPLER 2005 V. 8.5.07 RUN 8.3.12 11:20

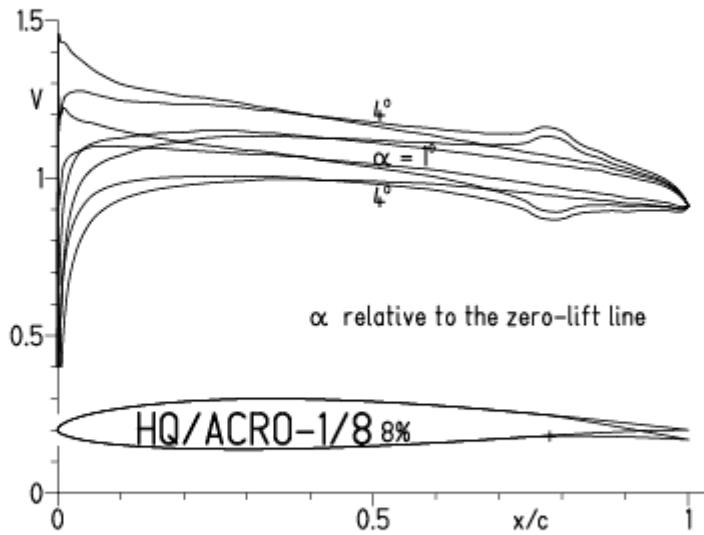
HQ/ACRO-1/8 8%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · · - $0.8 \times 10^6 e^N, N=9$
- · · · - $1.6 \times 10^6 e^N, N=9$



HQ/ACRO-1/8, N=11, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 11:42

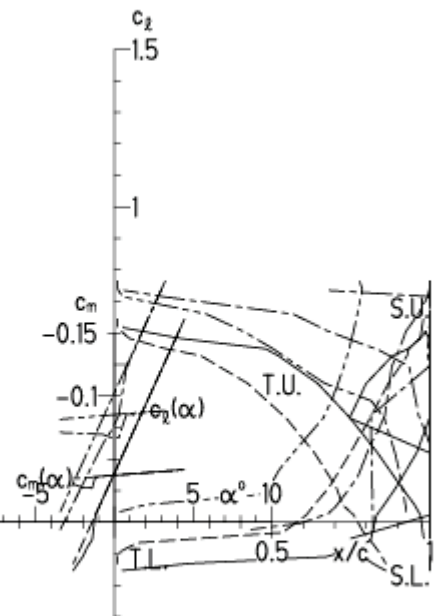
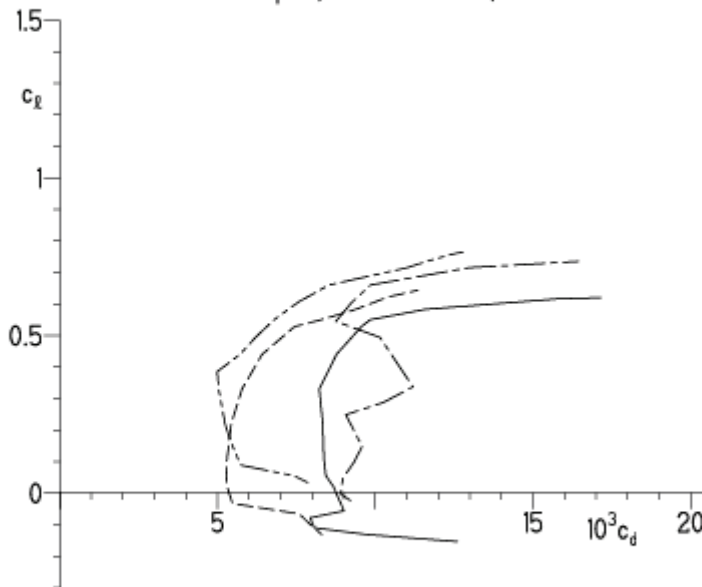


EPPLER 2005 V. 8.5.07 RUN 20.3.12 11:42

HQ/ACRO-1/8 8%

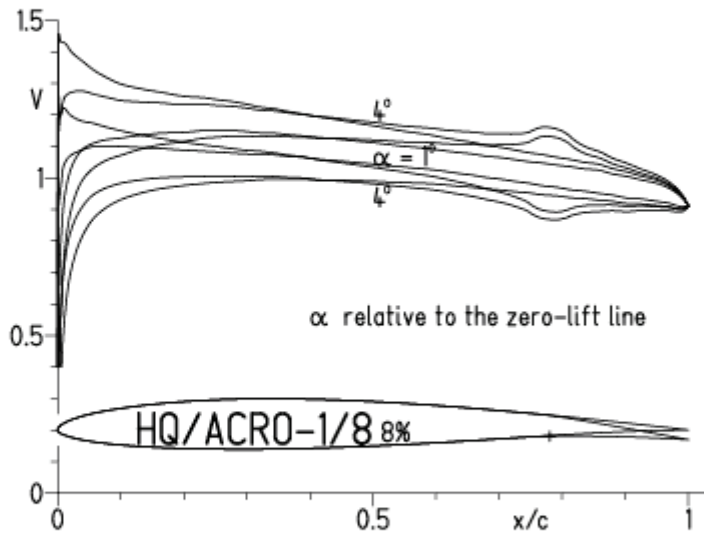
- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.8 \times 10^6 e^N, N=11$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

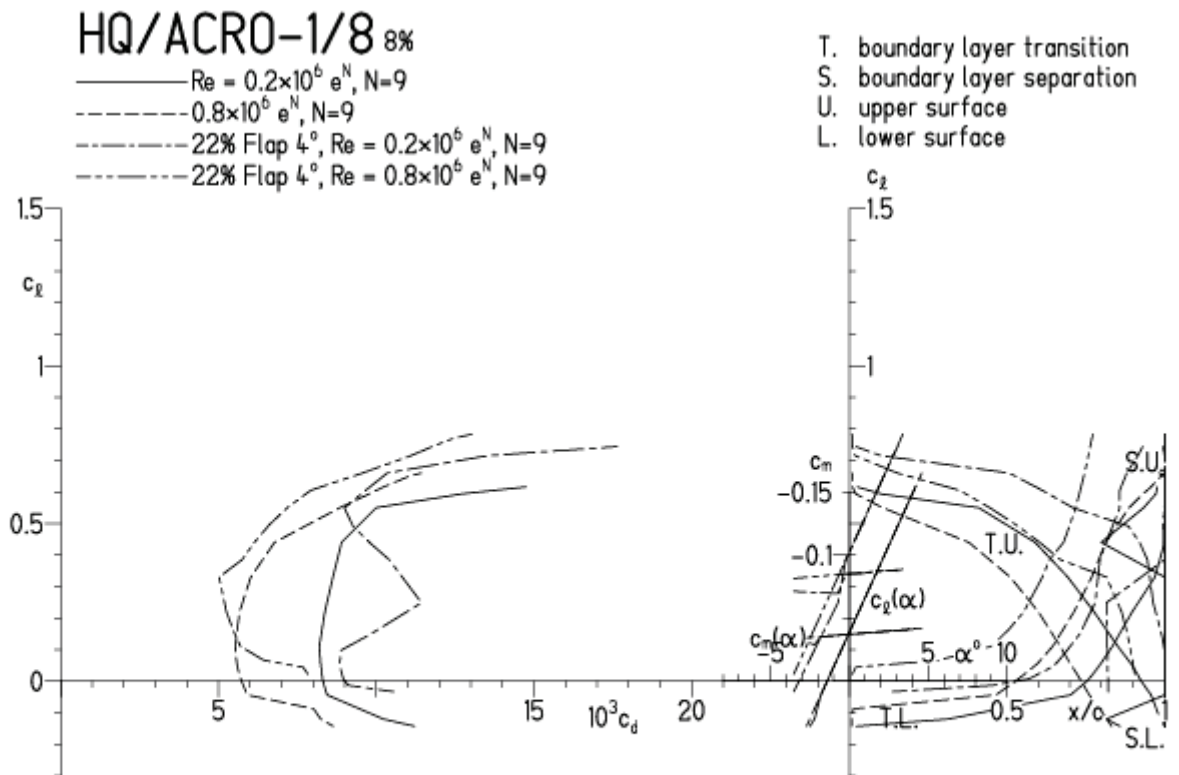


HQ/ACRO-1/8, N=9, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 11:46

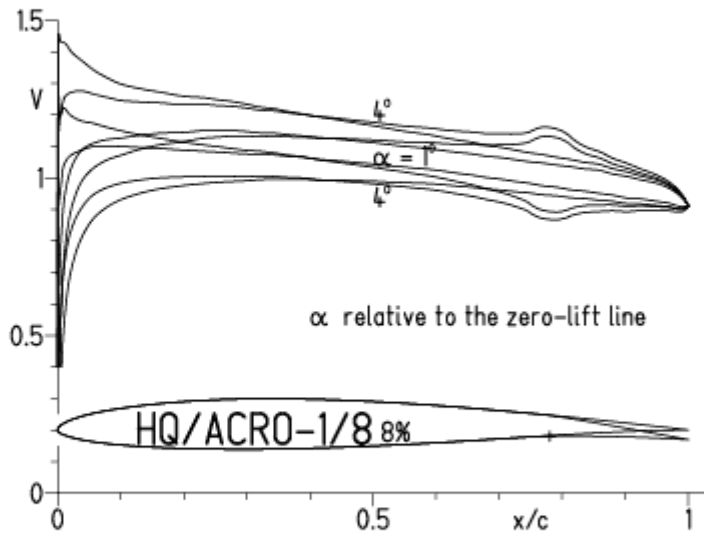


EPPLER 2005 V. 8.5.07 RUN 20.3.12 11:46



HQ/ACRO-1/8, N=9, mit 4° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbolatorposition bei 45 – 55 % der Profiltiefe)

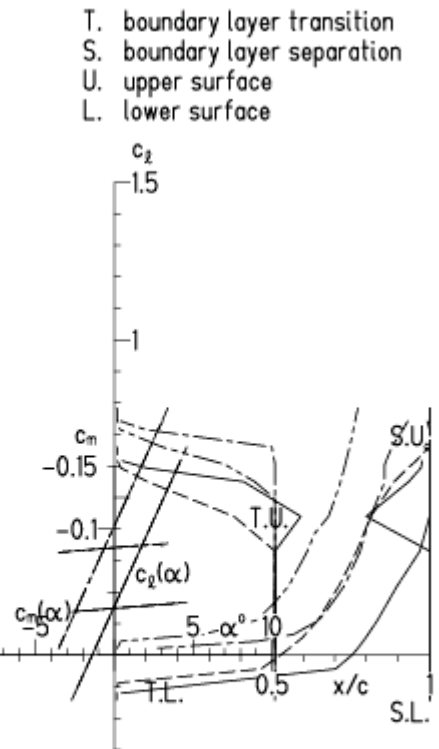
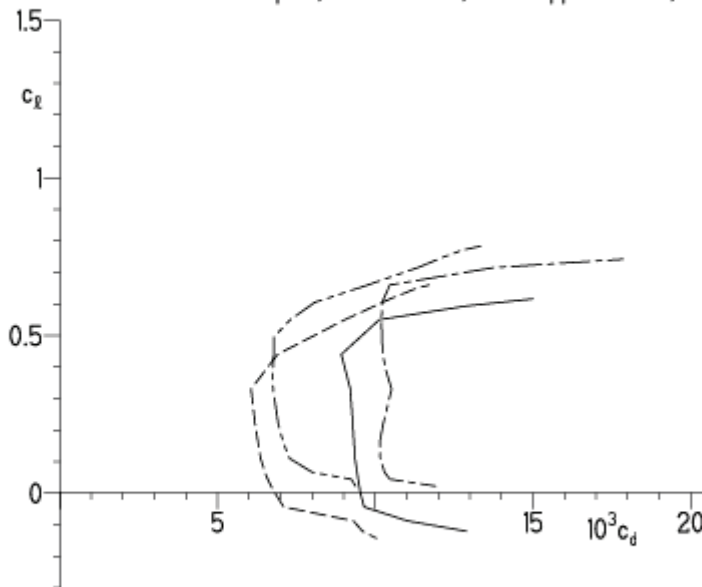
EPPLER 2005 V. 8.5.07 RUN 20.3.12 11:50



EPPLER 2005 V. 8.5.07 RUN 20.3.12 11:50

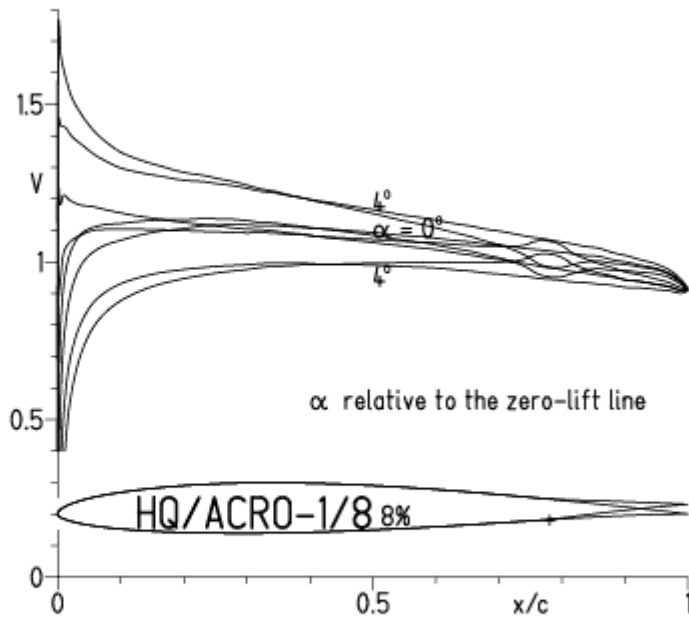
HQ/ACRO-1/8 8%

- $Re = 0.2 \times 10^6$, Turb. upper 51% e^N , N=9
- - - 0.8×10^6 , Turb. upper 51% e^N , N=9
- · - · 22% Flap 4° , $Re = 0.2 \times 10^6$, Turb. upper 51% e^N , N=9
- · - · 22% Flap 4° , $Re = 0.8 \times 10^6$, Turb. upper 51% e^N , N=9



HQ/ACRO-1/8, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 v. 8.5.07 RUN 20.3.12 11:53

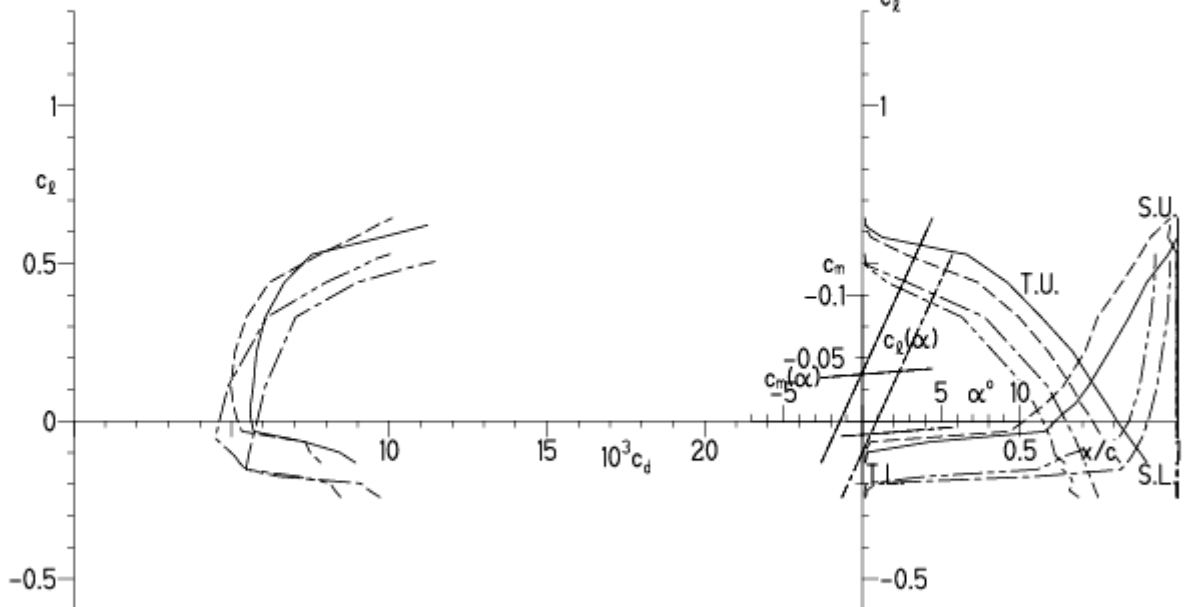


EPPLER 2005 v. 8.5.07 RUN 20.3.12 11:53

HQ/ACRO-1/8 8%

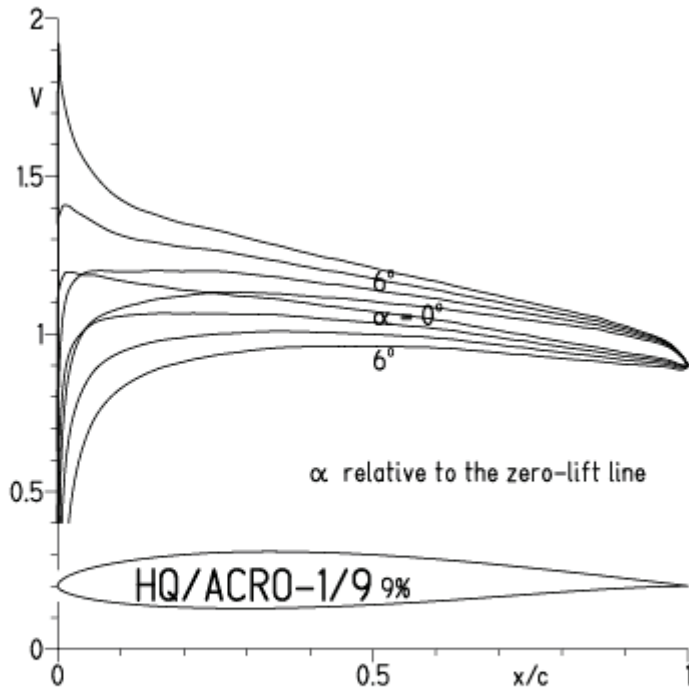
- $Re = 0.6 \times 10^6 e^N, N=11$
- - - $1.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 1.2 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1/9, N=11

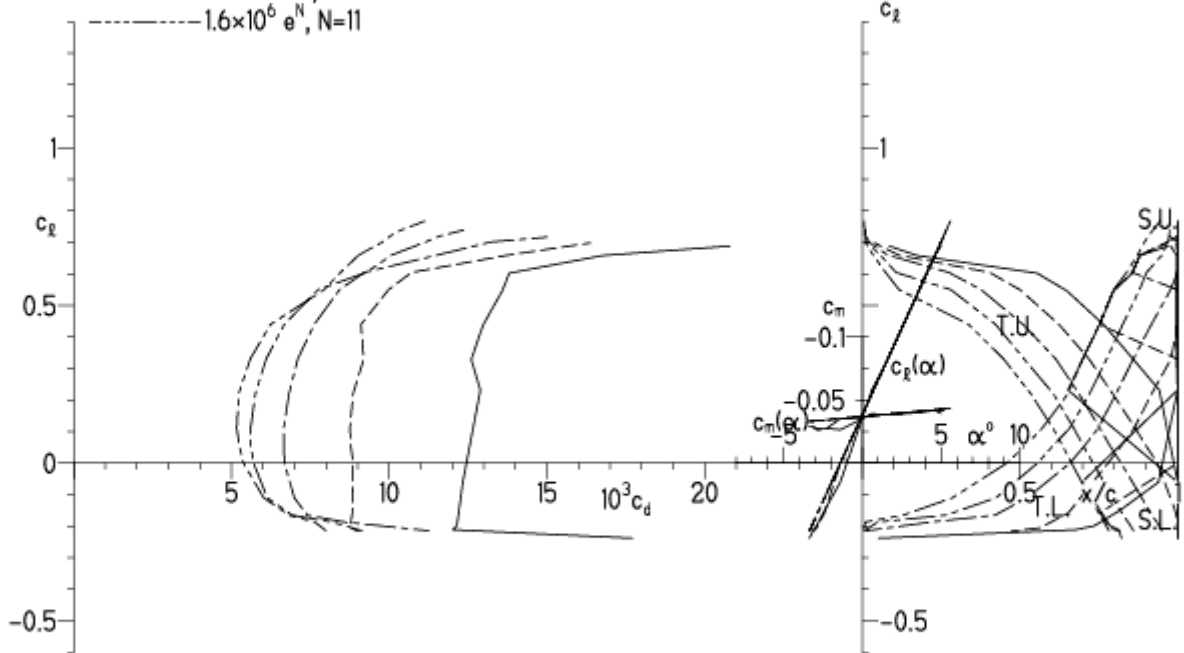
EPPLER 2005 V. 8.5.07 RUN 8.3.12 16:06



EPPLER 2005 V. 8.5.07 RUN 8.3.12 16:06

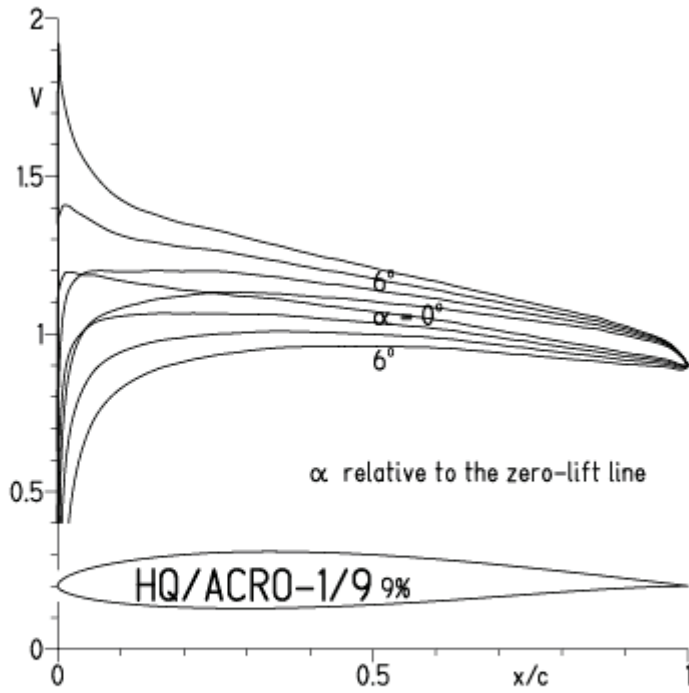
HQ/ACRO-1/9 9%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · · - $0.8 \times 10^6 e^N, N=11$
- · · · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1/9, N=9

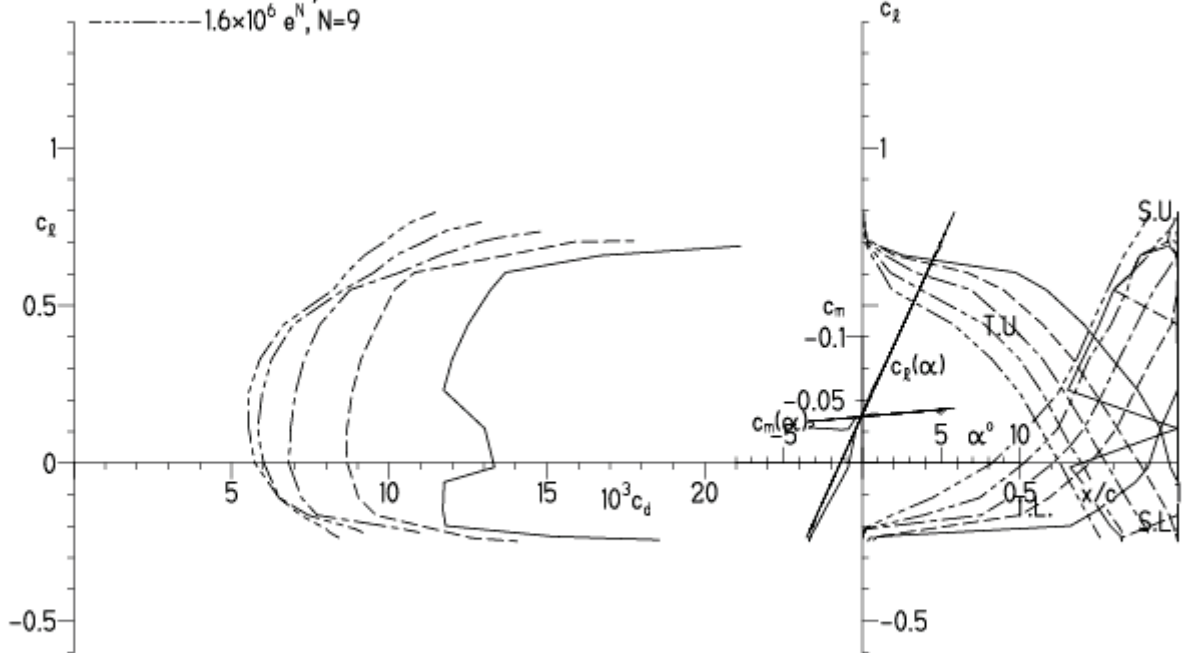
EPPLER 2005 V. 8.5.07 RUN 8.3.12 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.12 16:33

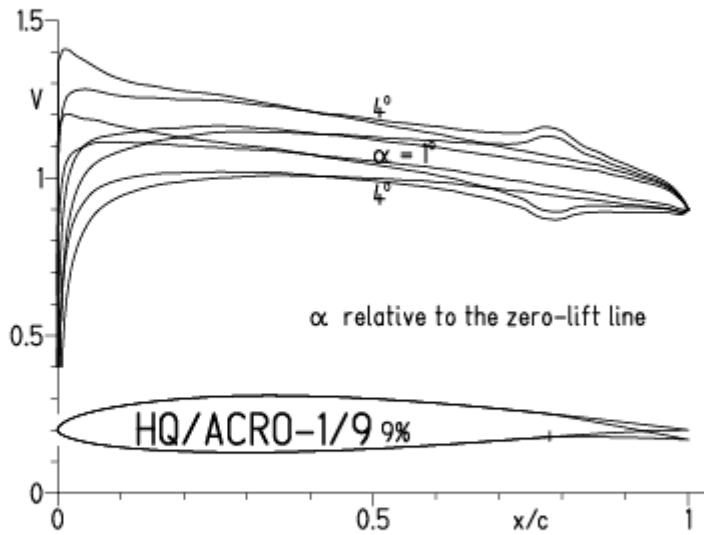
HQ/ACRO-1/9 9%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · · - $0.8 \times 10^6 e^N, N=9$
- · · · - $1.6 \times 10^6 e^N, N=9$



HQ/ACRO-1/9, N=11, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 11:58

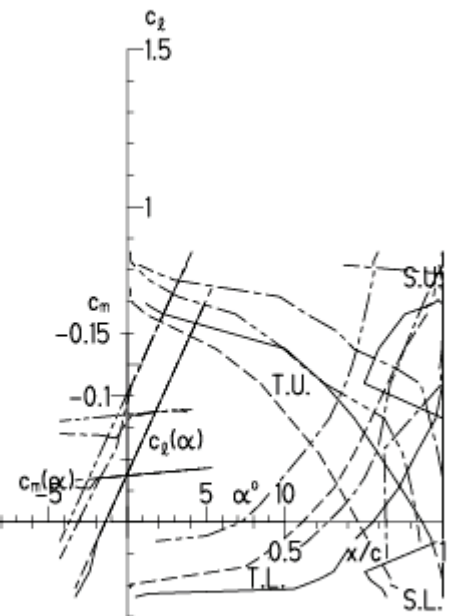
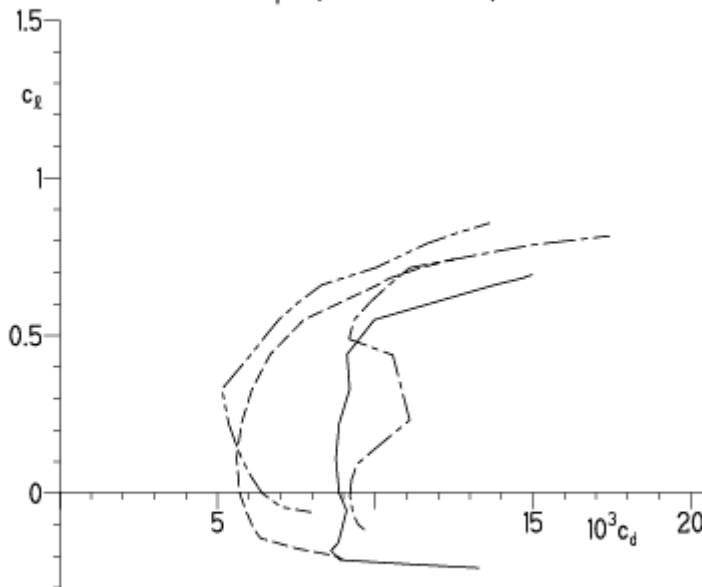


EPPLER 2005 V. 8.5.07 RUN 20.3.12 11:58

HQ/ACRO-1/9 9%

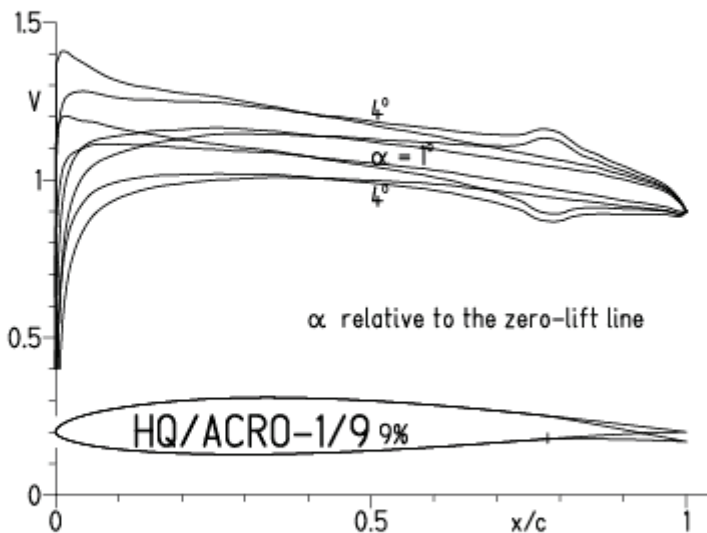
- $Re = 0.2 \times 10^6$ e^N, N=11
- - - 0.8×10^6 e^N, N=11
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6$ e^N, N=11
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6$ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

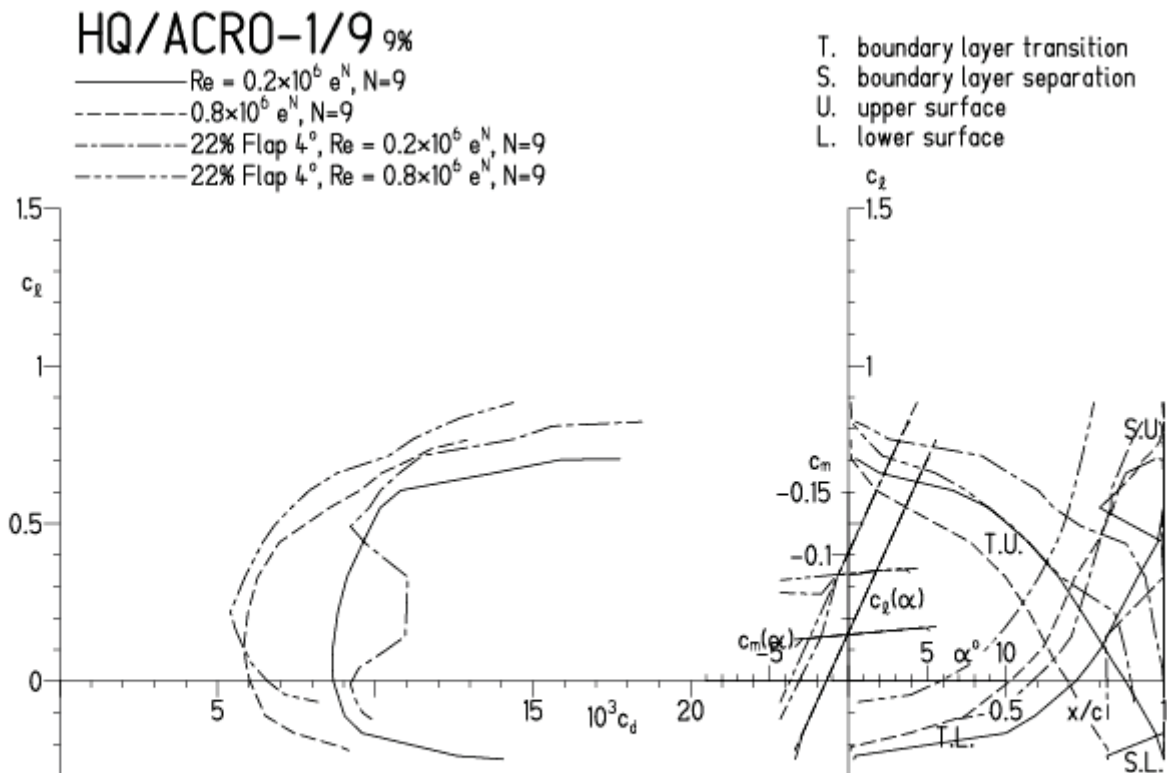


HQ/ACRO-1/9, N=9, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:01

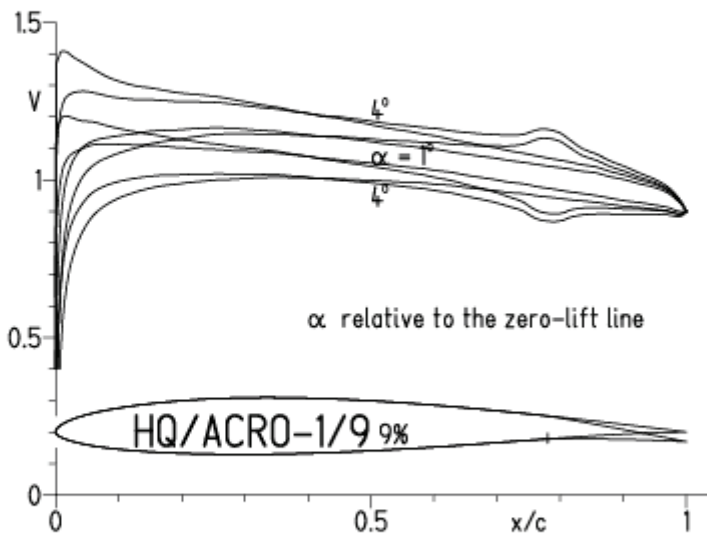


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:01



HQ/ACRO-1/9, N=9, mit 4° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbulatorposition bei 45 – 55 % der Profiltiefe)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:06

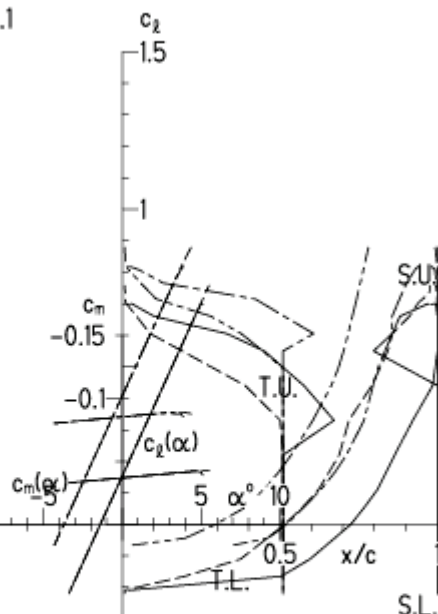
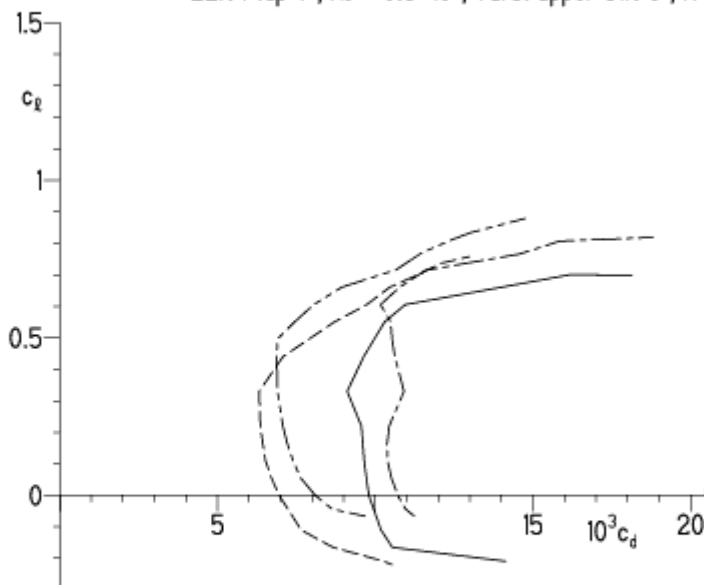


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:06

HQ/ACRO-1/9 9%

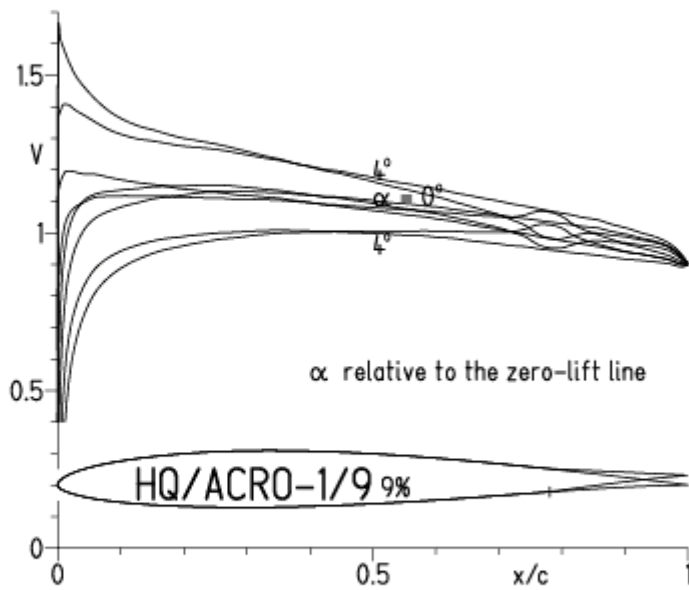
- Re = 0.2×10⁶, Turb. upper 51% e^N, N=9.1
- - - 0.8×10⁶, Turb. upper 51% e^N, N=9.1
- · - · 22% Flap 4°, Re = 0.2×10⁶, Turb. upper 51% e^N, N=9.1
- · - · 22% Flap 4°, Re = 0.8×10⁶, Turb. upper 51% e^N, N=9.1

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1/9, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:09

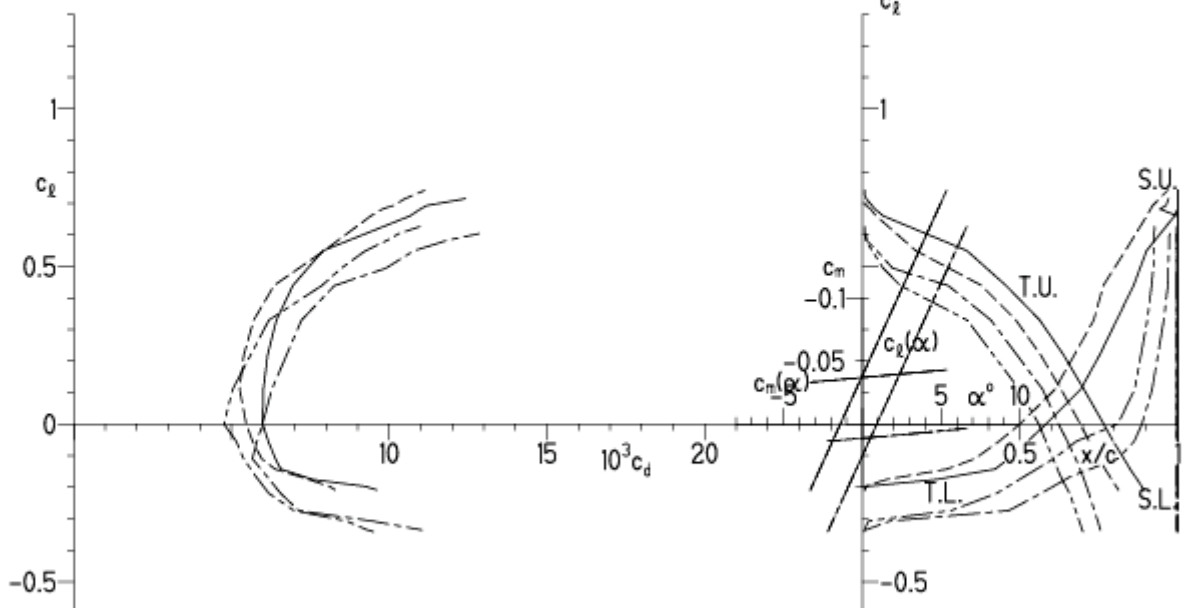


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:09

HQ/ACRO-1/9 9%

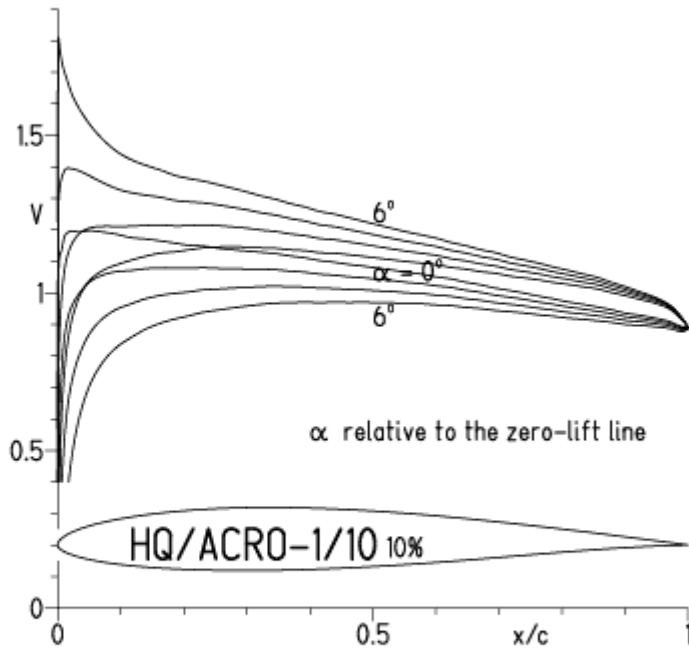
- $Re = 0.6 \times 10^6 e^N, N=11$
- - - $1.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 1.2 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1/10, N=11

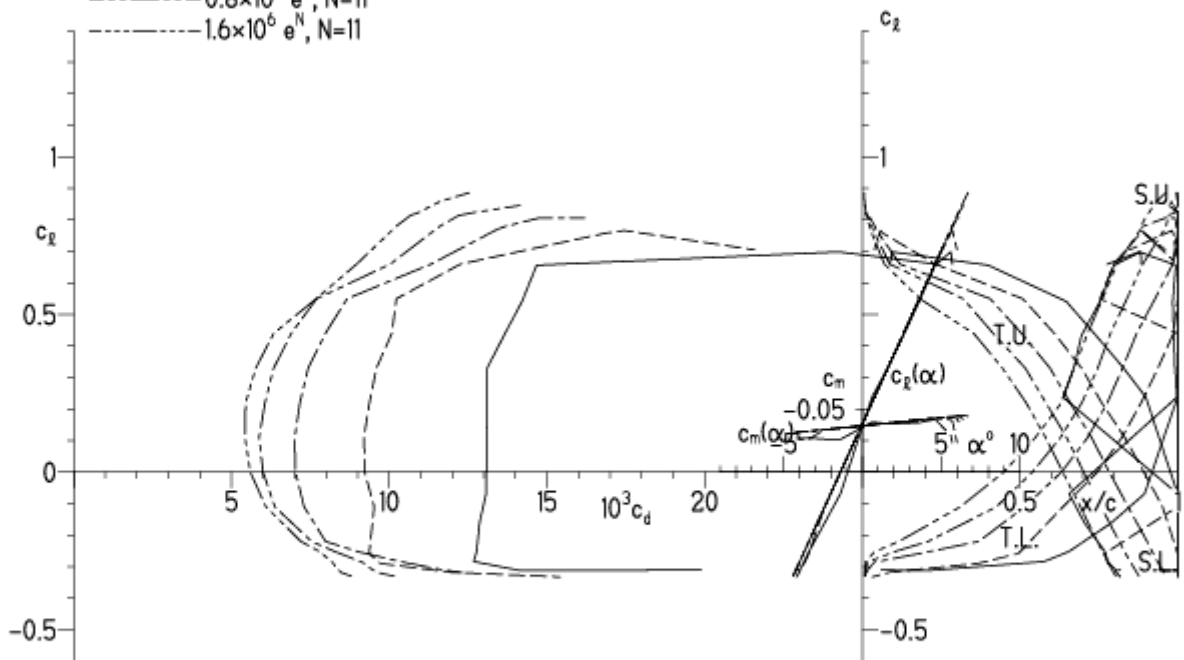
EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:13



EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:13

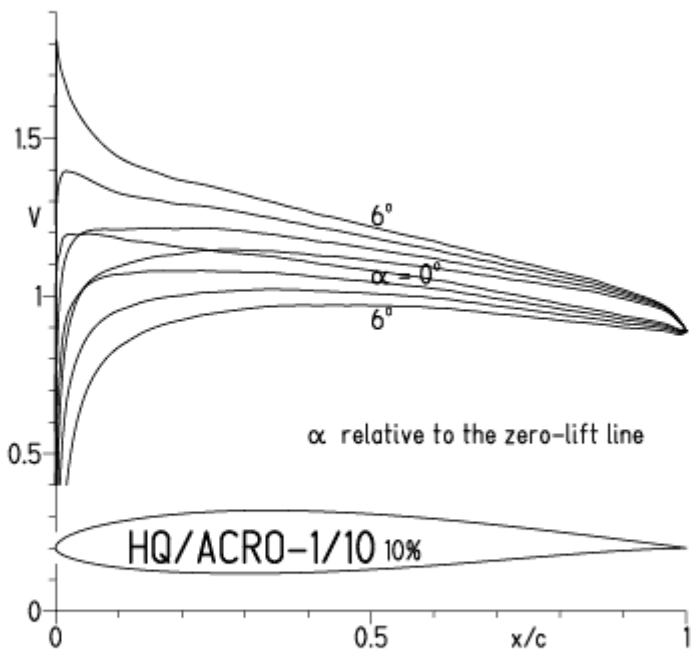
HQ/ACRO-1/10 10%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · · - $0.8 \times 10^6 e^N, N=11$
- · · · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1/10, N=9

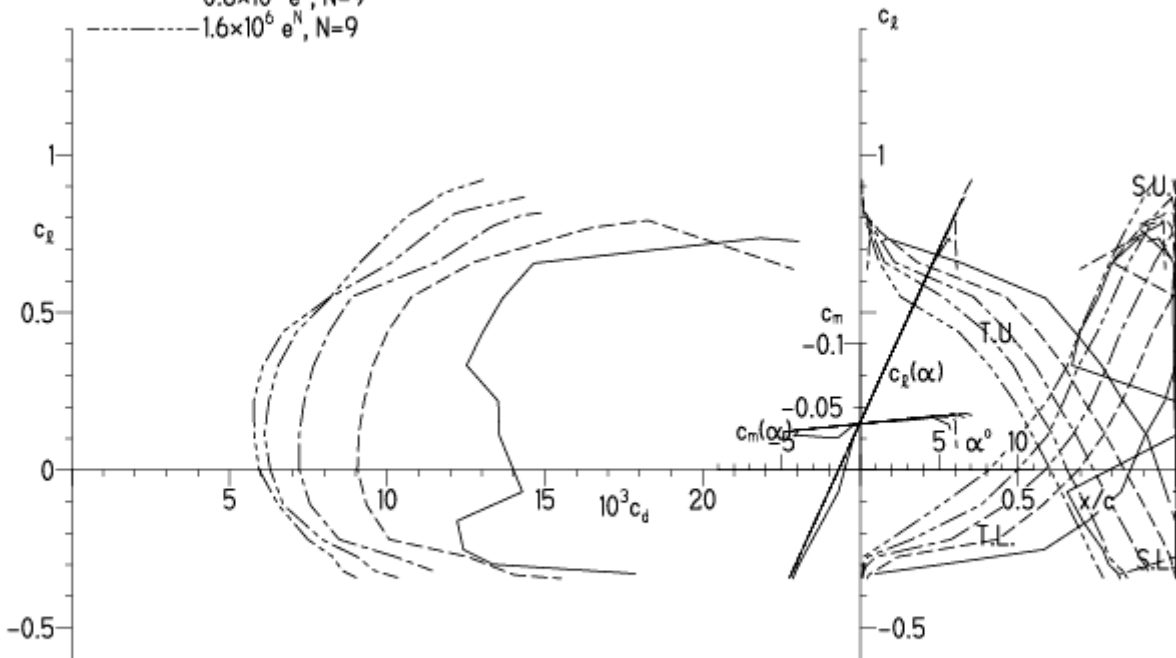
EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:17



EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:17

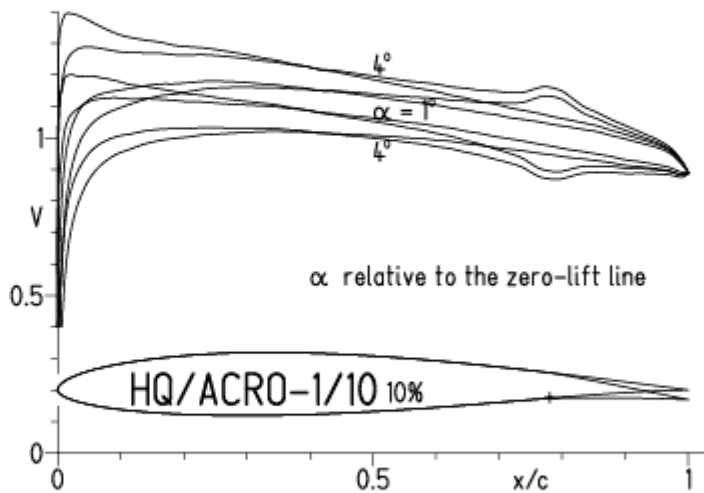
HQ/ACRO-1/10 10%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · · - $0.8 \times 10^6 e^N, N=9$
- · · · - $1.6 \times 10^6 e^N, N=9$

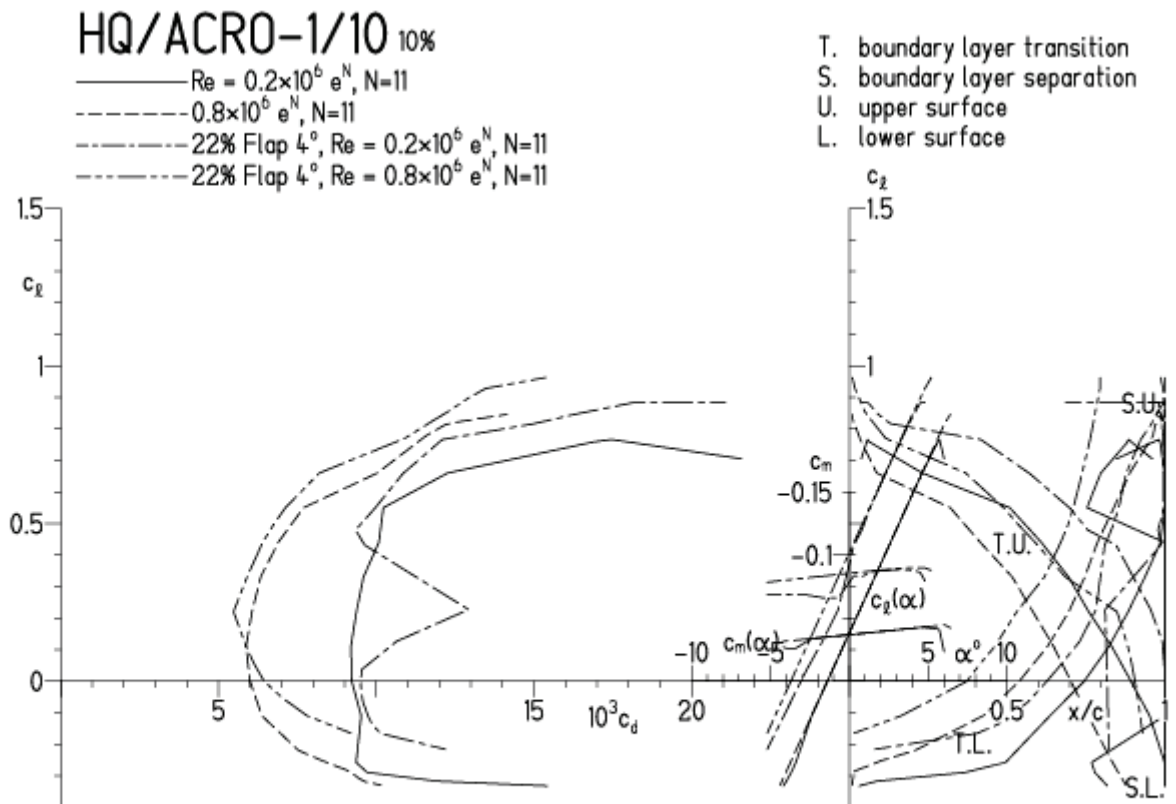


HQ/ACRO-1/10, N=11, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:19

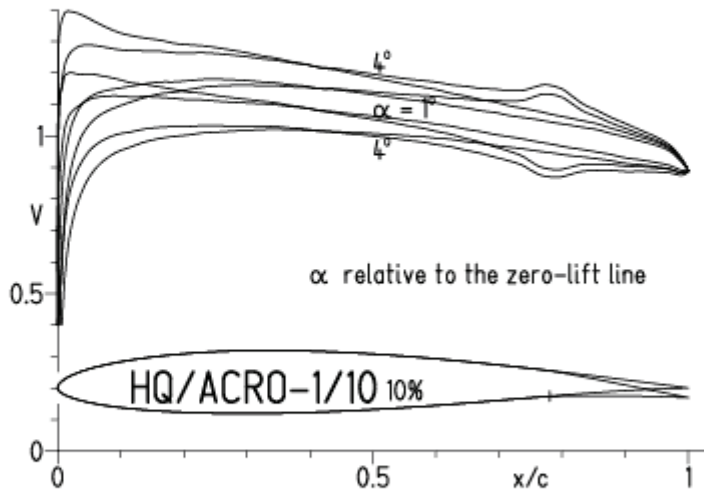


EPPLER 2005 V. 8.5.07 RUN 2

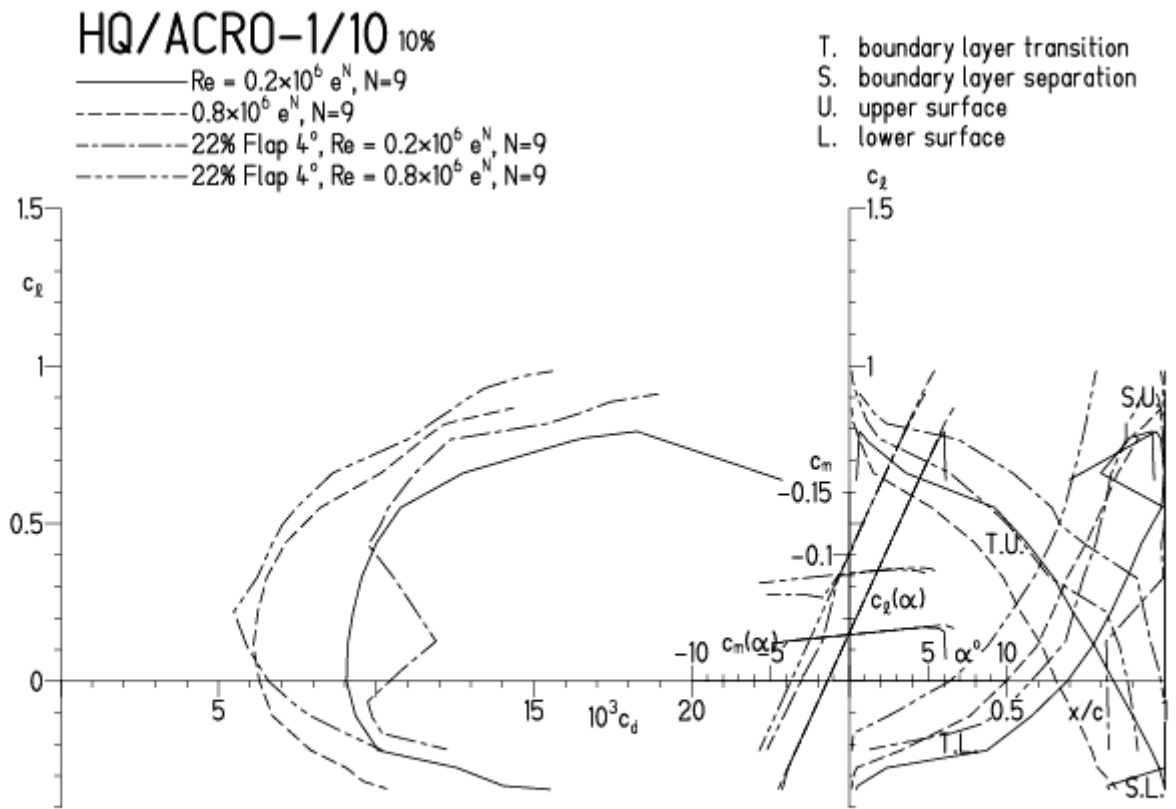


HQ/ACRO-1/10, N=9, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:24

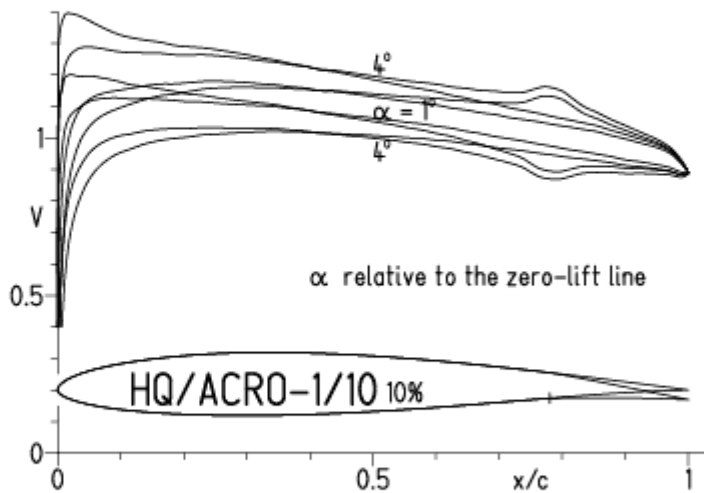


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:24

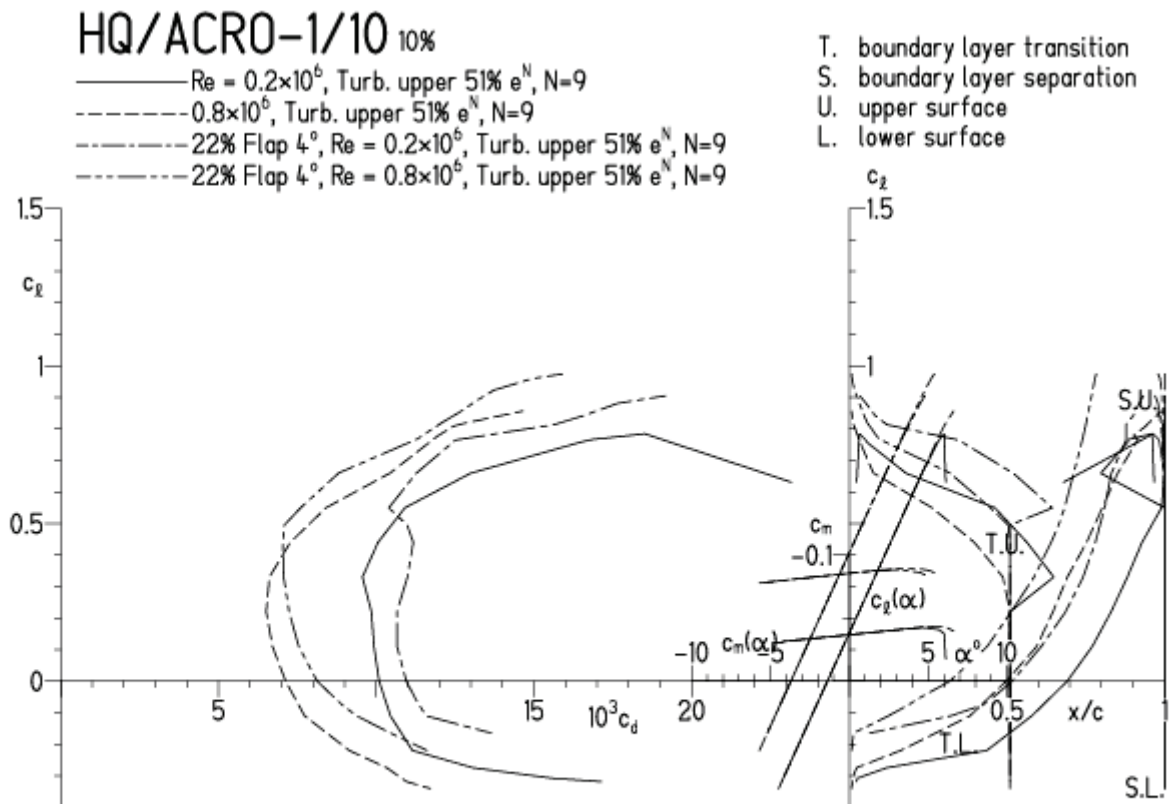


HQ/ACRO-1/10, N=9, mit 5° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:26

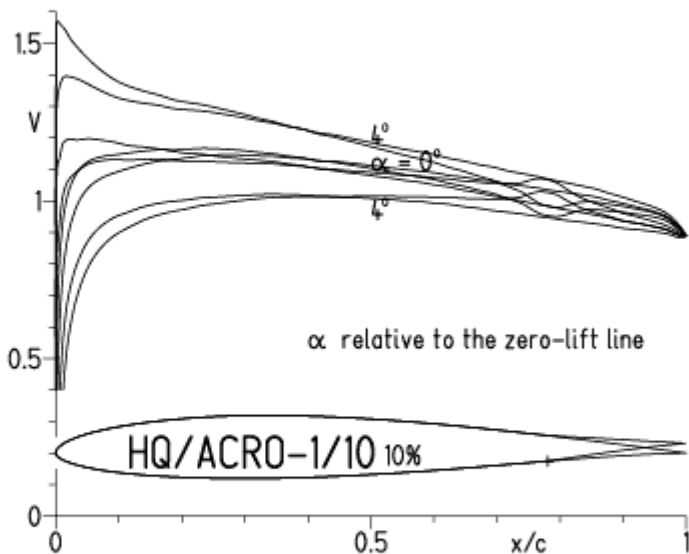


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:26



HQ/ACRO-1/10, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 v. 8.5.07 RUN 20.3.12 12:30

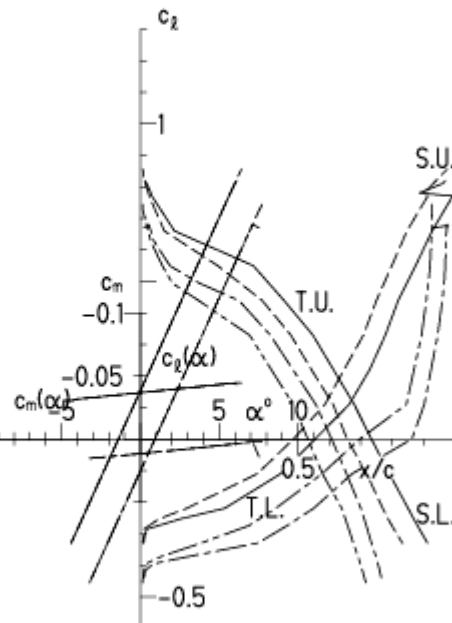
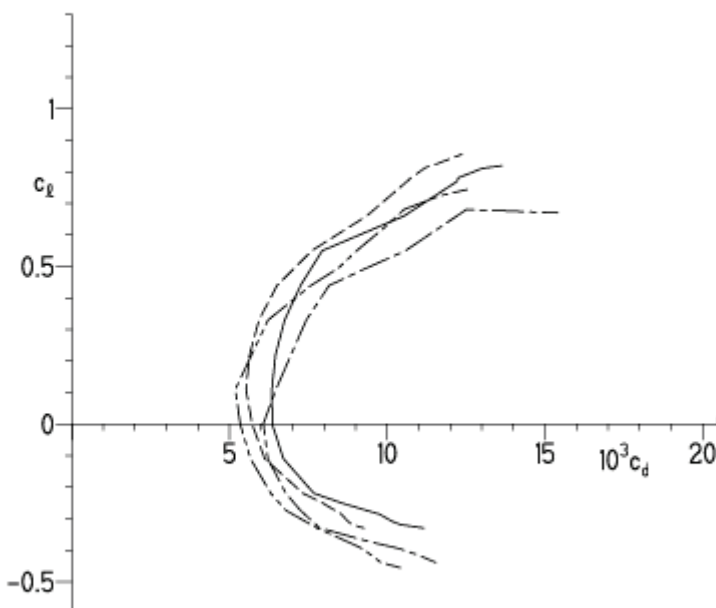


EPPLER 2005 v. 8.5.07 RUN 20.3.12 12:30

HQ/ACRO-1/10 10%

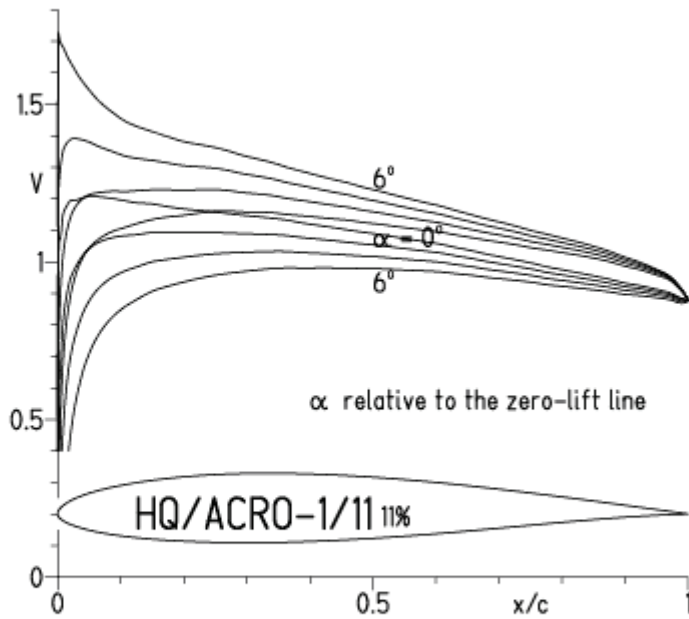
- $Re = 0.6 \times 10^6 e^N$, N=11
- - - $1.2 \times 10^6 e^N$, N=11
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N$, N=11
- · - · - 22% Flap -4°, $Re = 1.2 \times 10^6 e^N$, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

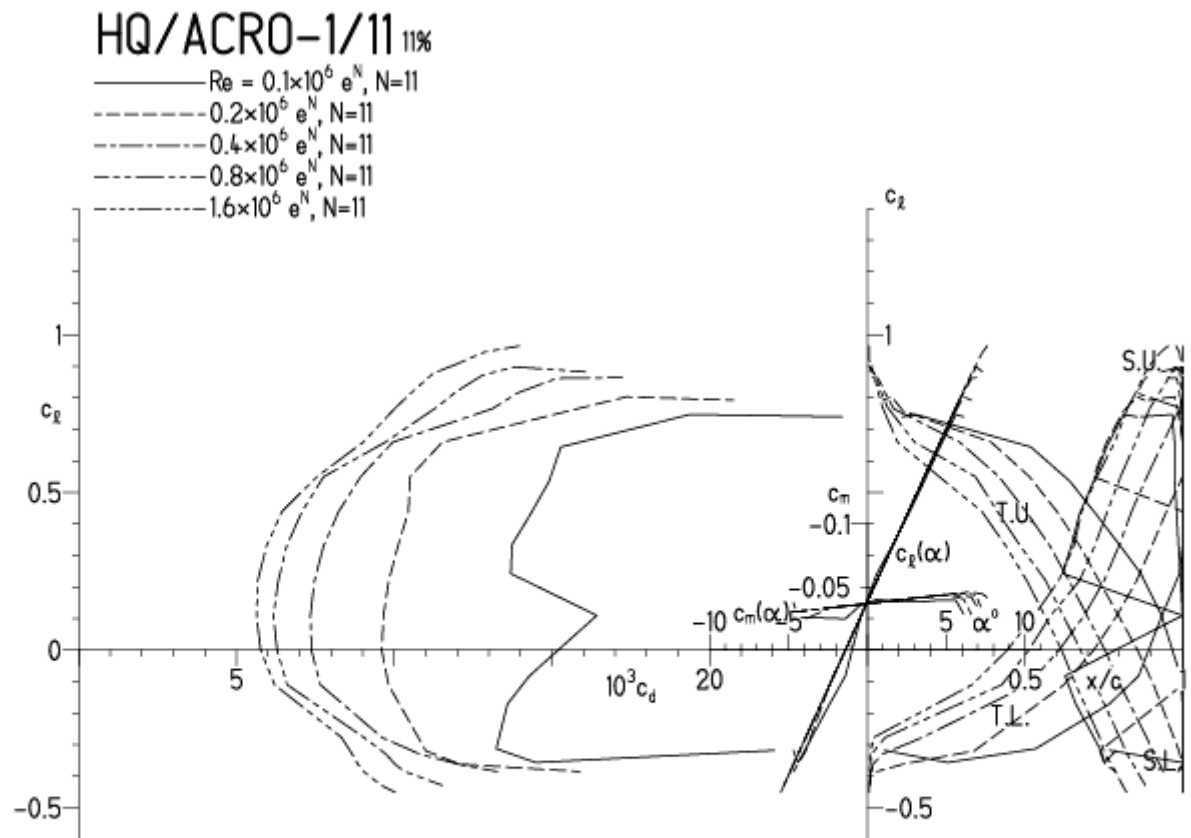


HQ/ACRO-1/11, N=11

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:33

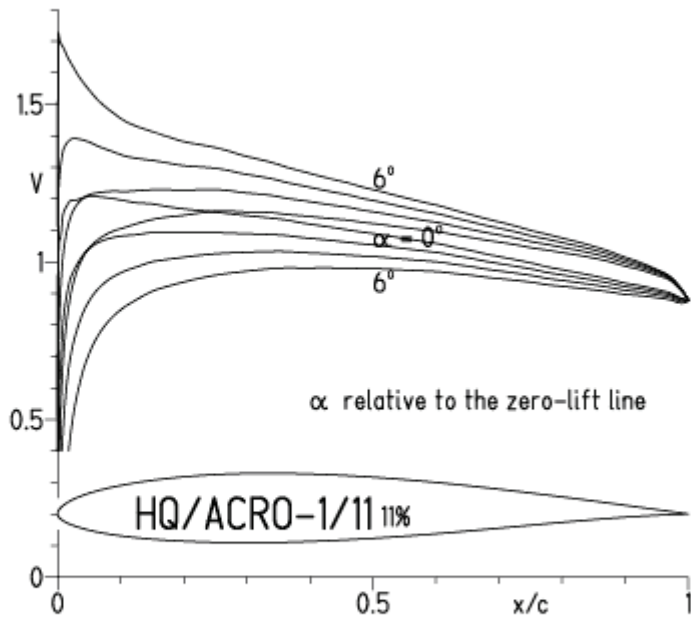


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:33

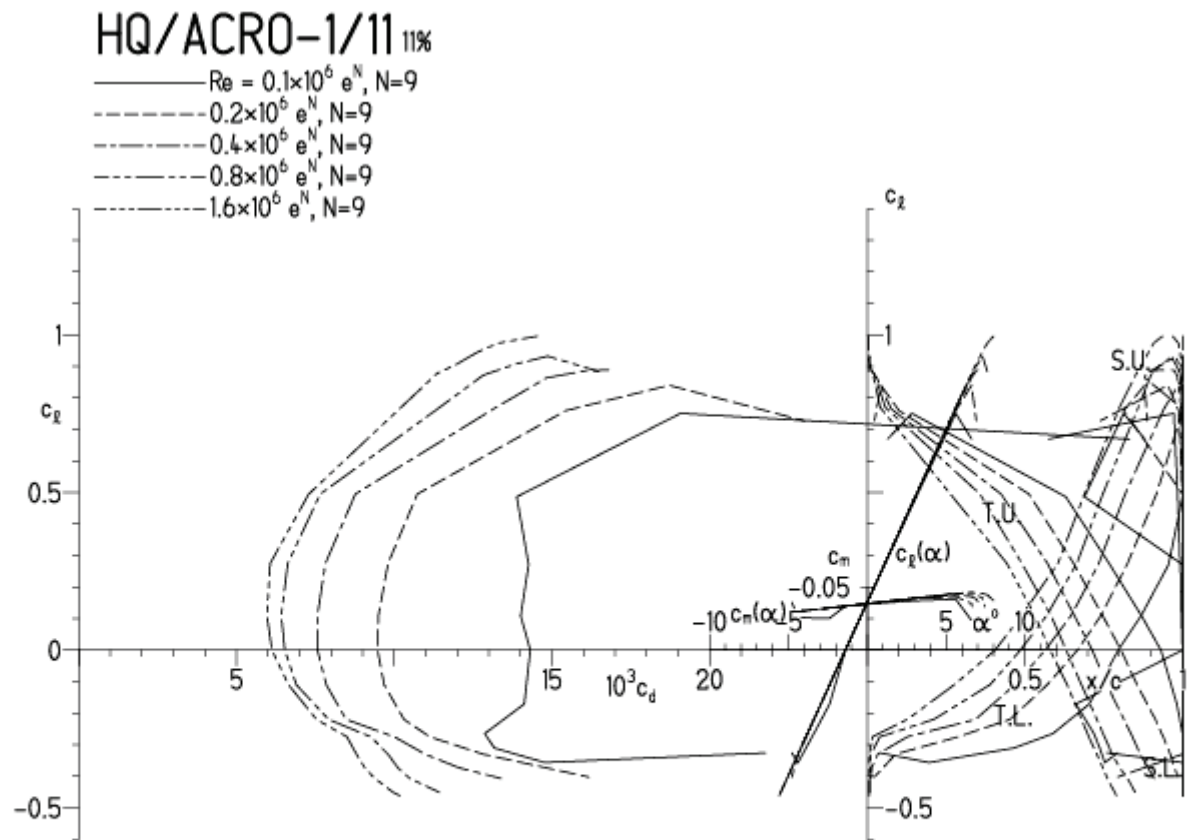


HQ/ACRO-1/11, N=9

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:36

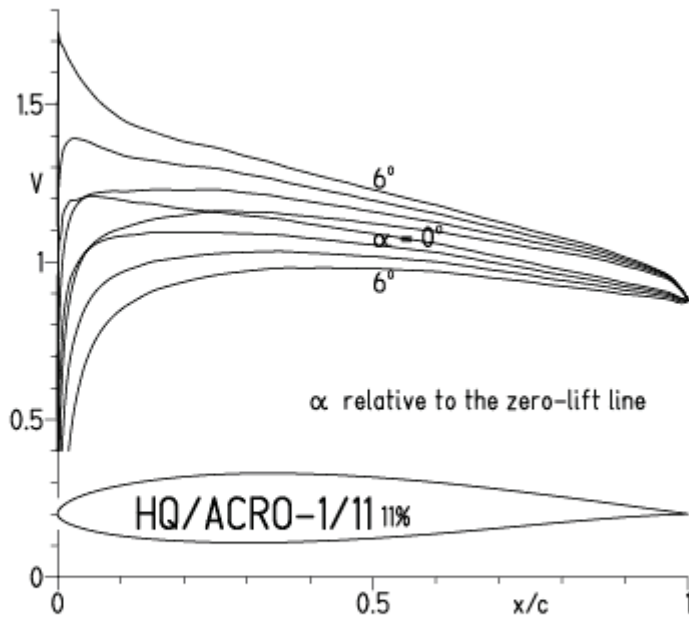


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:36



HQ/ACRO-1/11, N=9, Turbulatoreffekt bei niedrigen Re-Zahlen
 (optimale Turbulatorposition bei 45 - 55% der Profiltiefe)

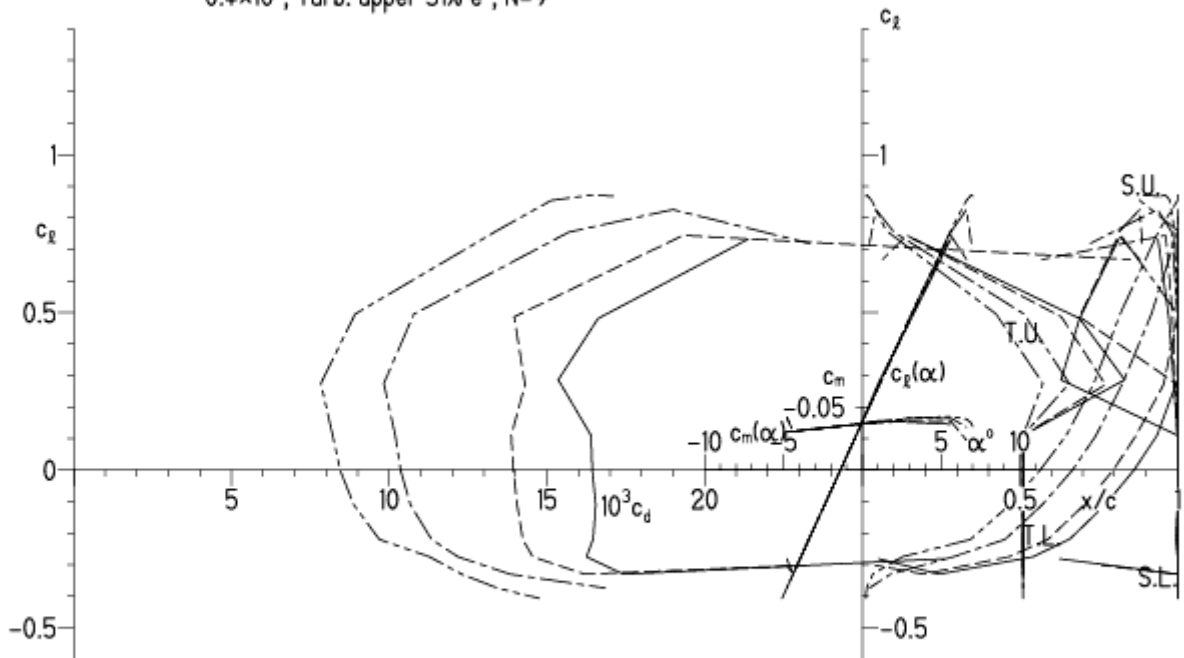
EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:39



EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:39

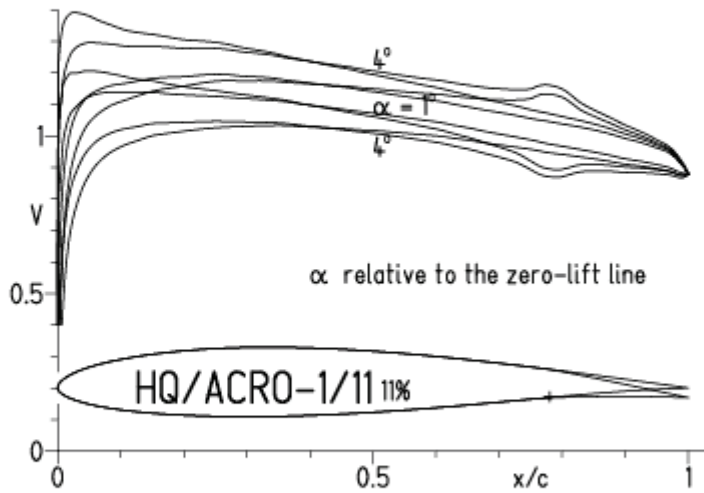
HQ/ACRO-1/11 11%

- Re = 75 000, Turb. upper 51% e^N, N=9
- - - 0.1 × 10⁶, Turb. upper 51% e^N, N=9
- · - 0.2 × 10⁶, Turb. upper 51% e^N, N=9
- - - 0.4 × 10⁶, Turb. upper 51% e^N, N=9

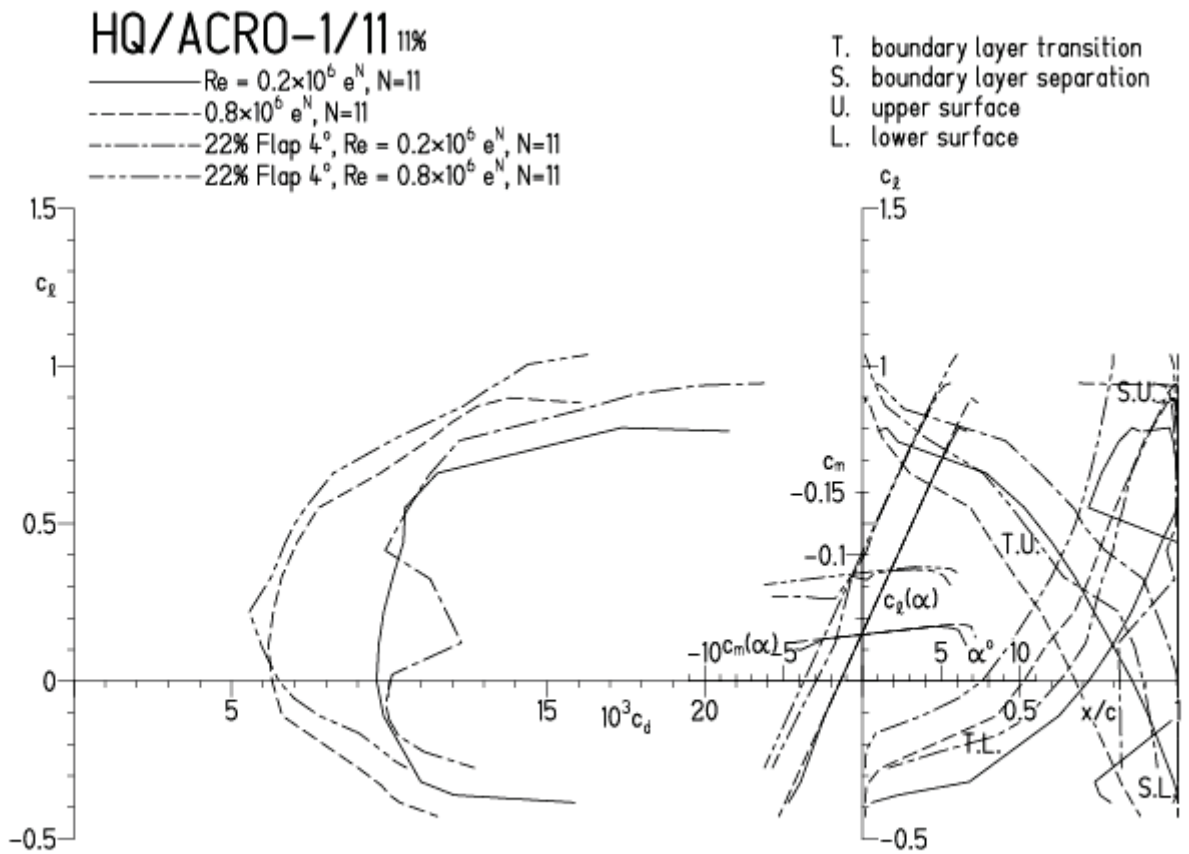


HQ/ACRO-1/11, N=11, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:42

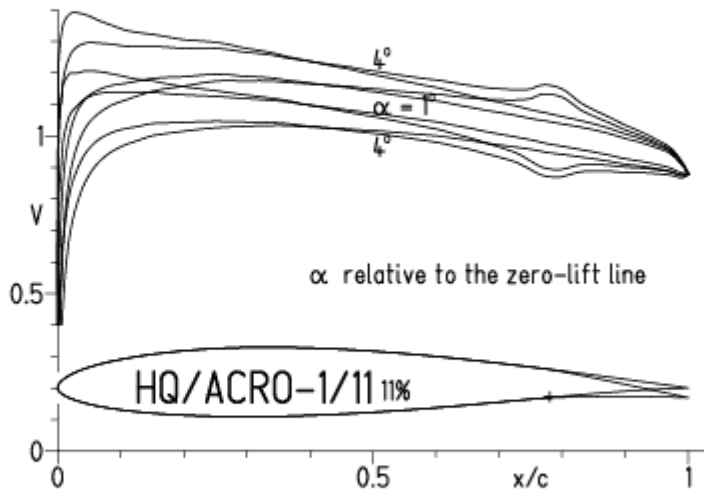


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:42

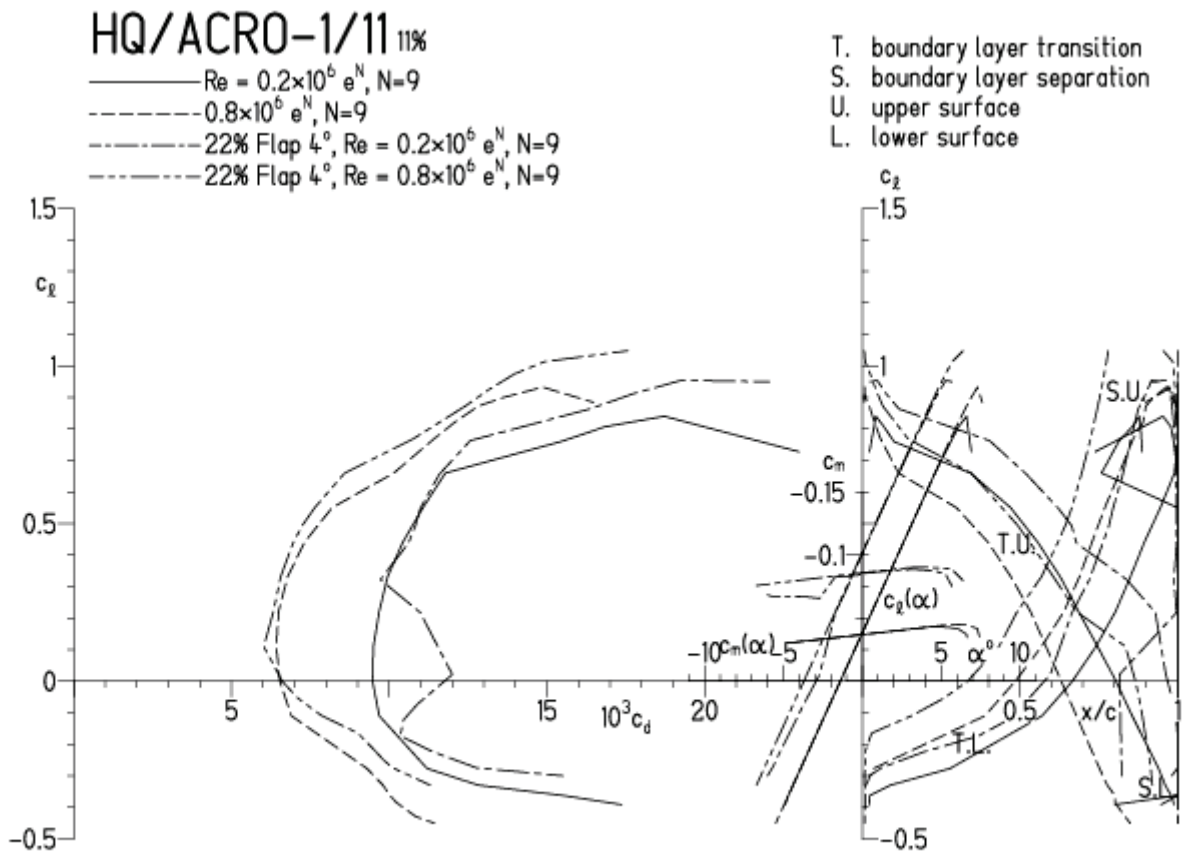


HQ/ACRO-1/11, N=9, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:45

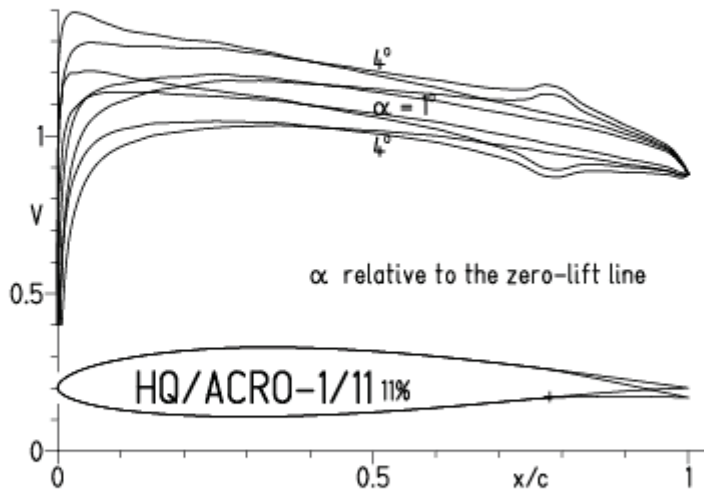


EPPLER 2005 V. 8.5.07 RUN 20.3.1

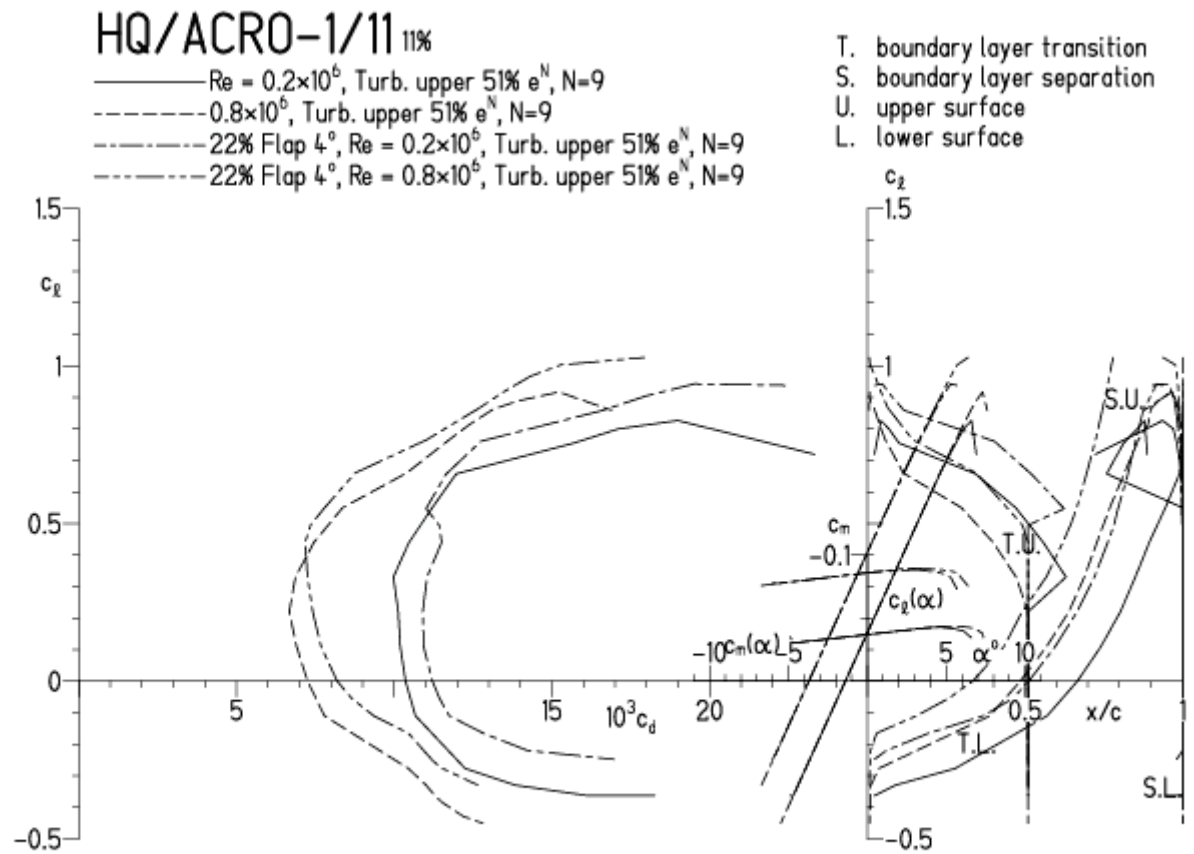


HQ/ACRO-1/11, N=9, mit 4° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:47

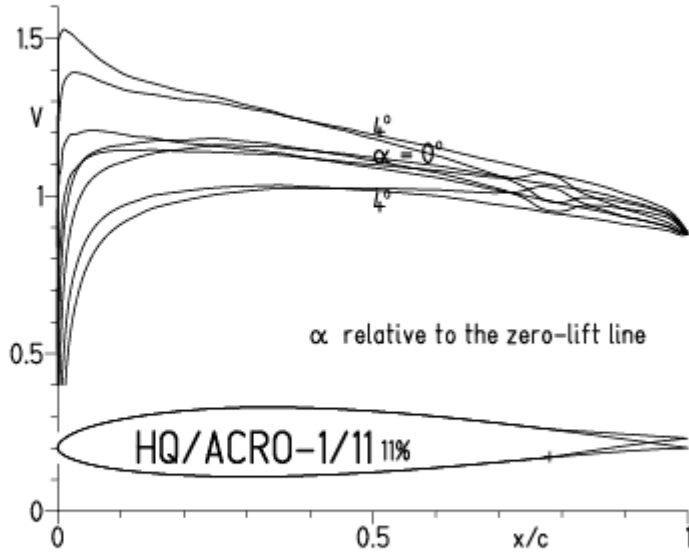


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:47

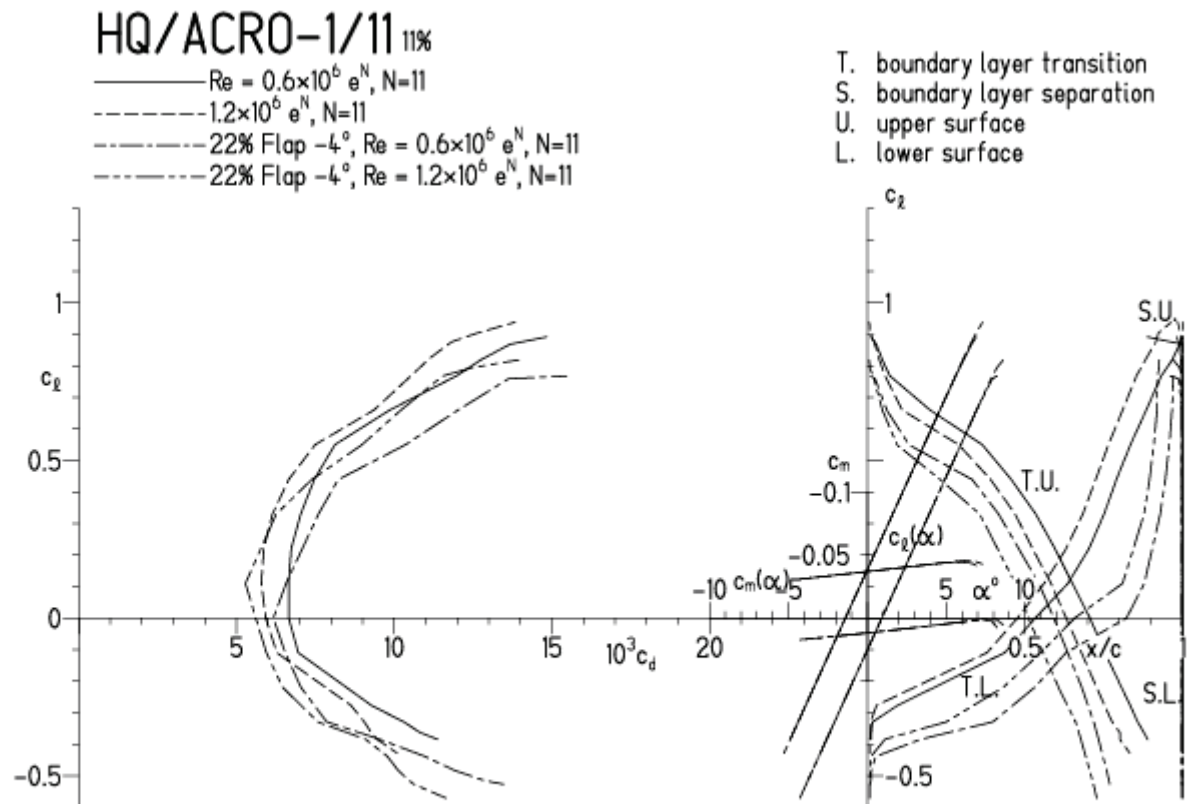


HQ/ACRO-1/11, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:51

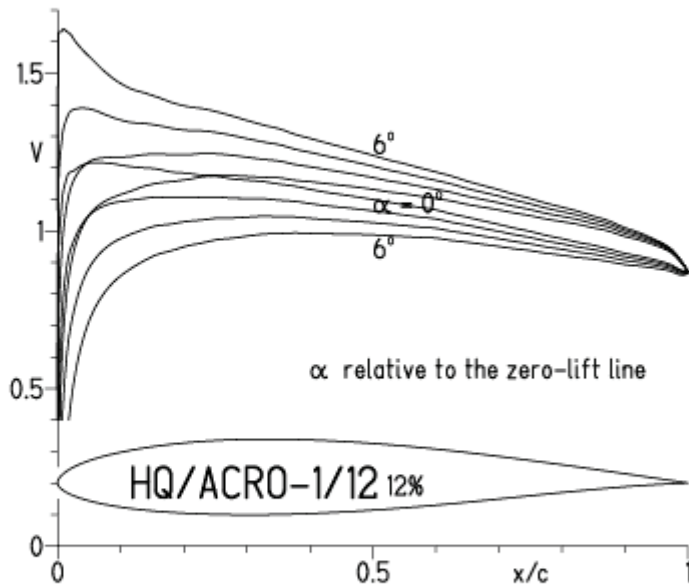


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:51

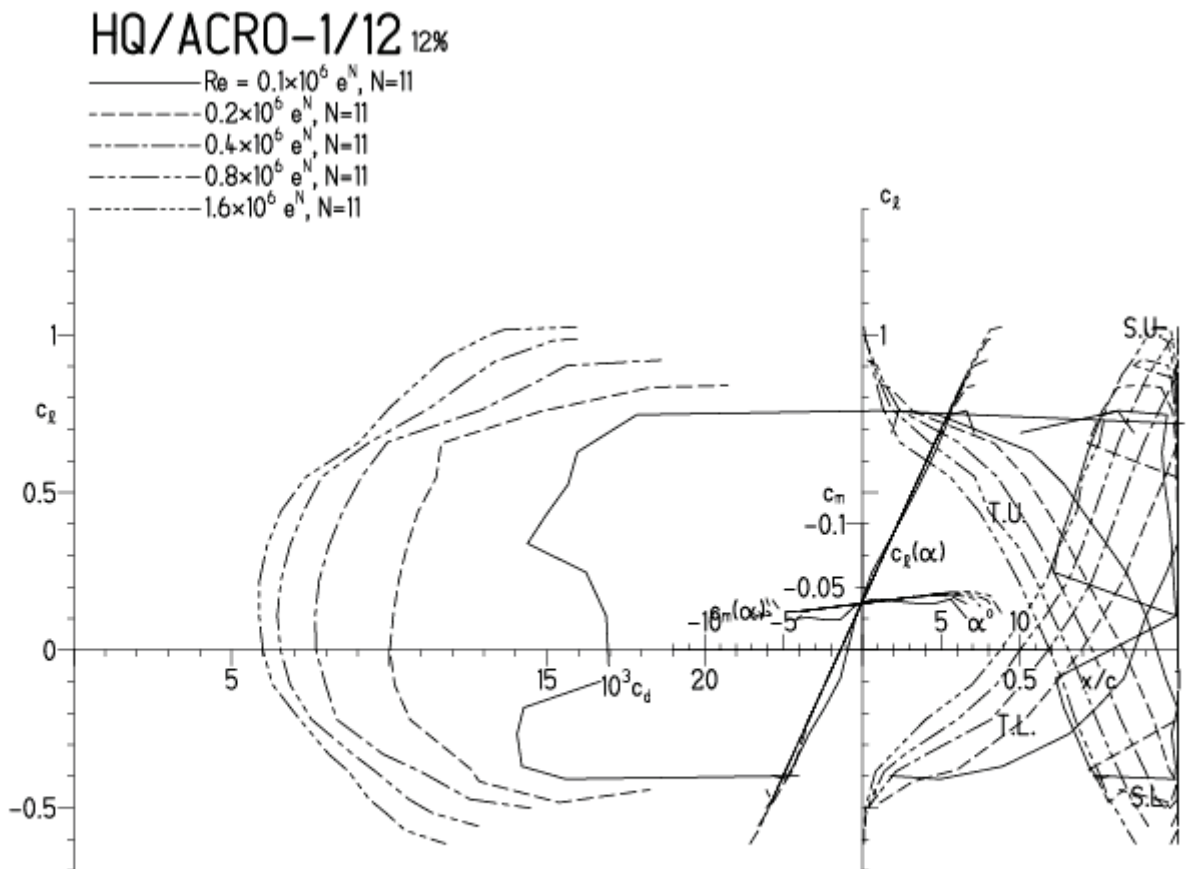


HQ/ACRO-1/12, N=11

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:54

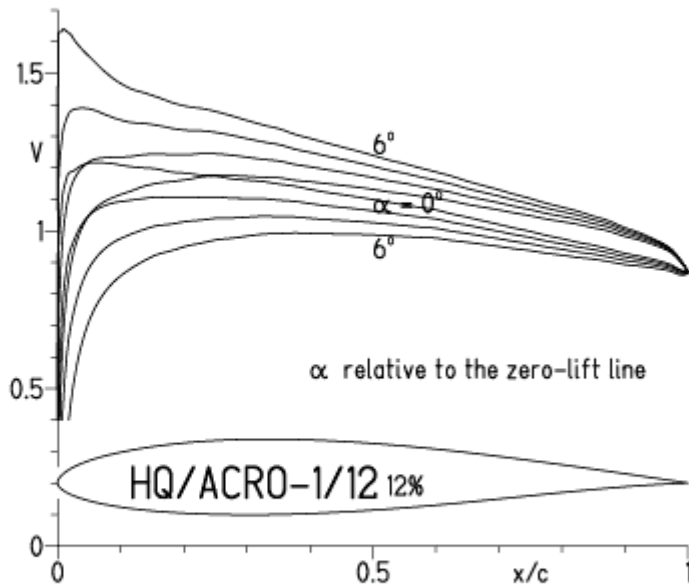


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:54

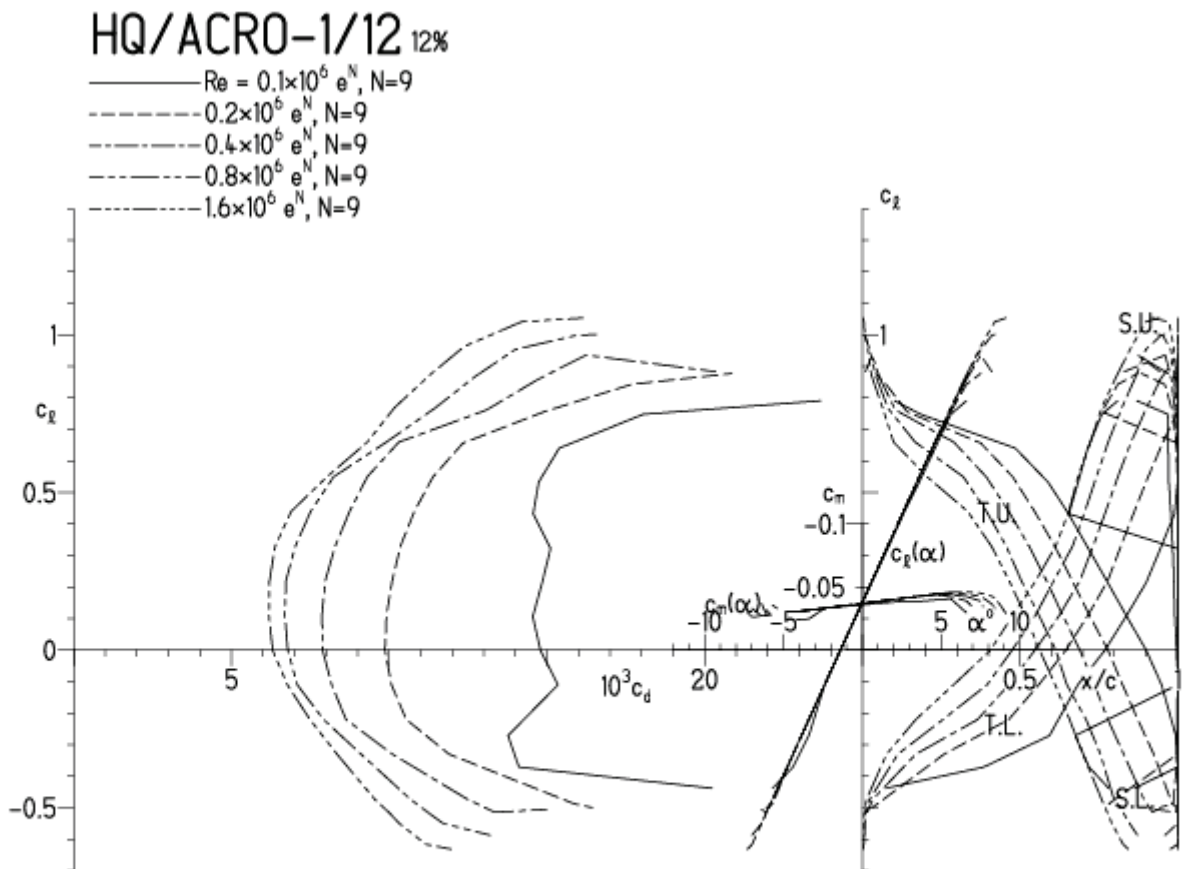


HQ/ACRO-1/12, N=9

EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:57

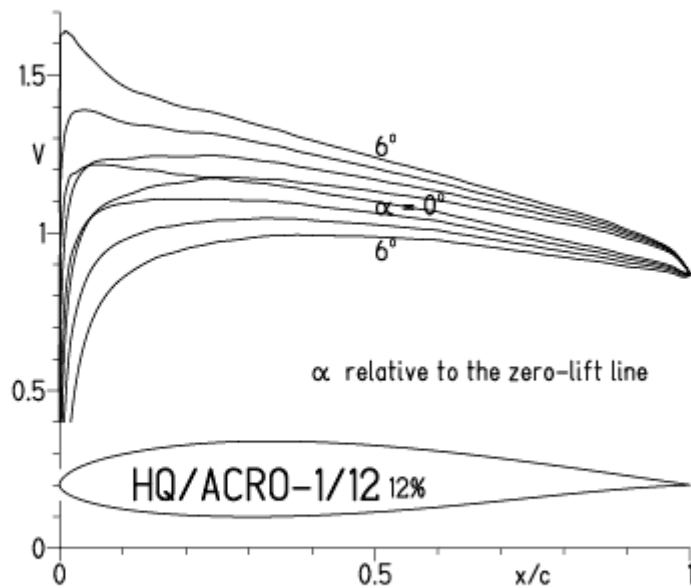


EPPLER 2005 V. 8.5.07 RUN 20.3.12 12:57



HQ/ACRO-1/12, N=9, Turbulatoreffekt bei niedrigen Re-Zahlen
(optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

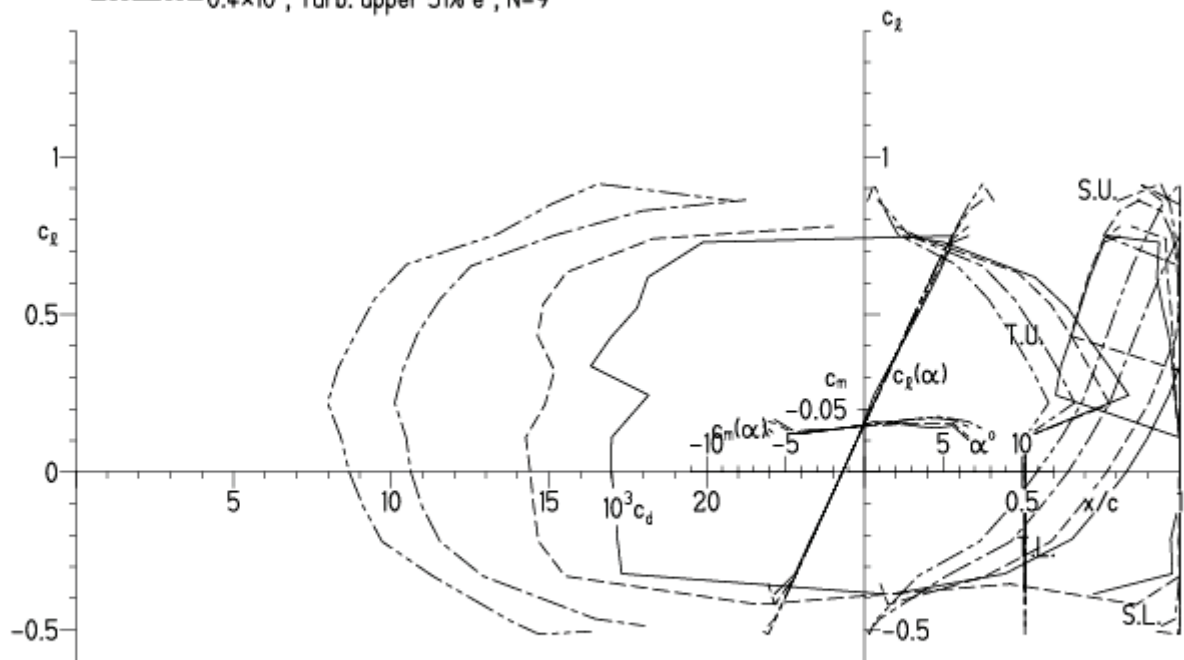
EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:00



EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:00

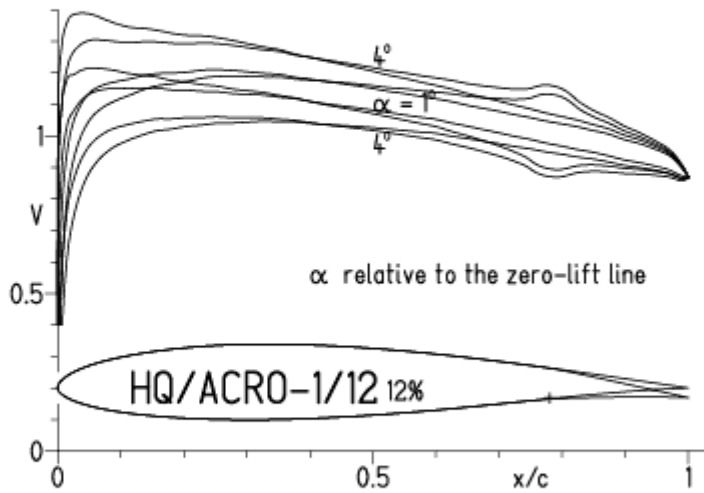
HQ/ACRO-1/12 12%

- $Re = 75\,000$, Turb. upper 51% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 51% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 51% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 51% e^N , $N=9$

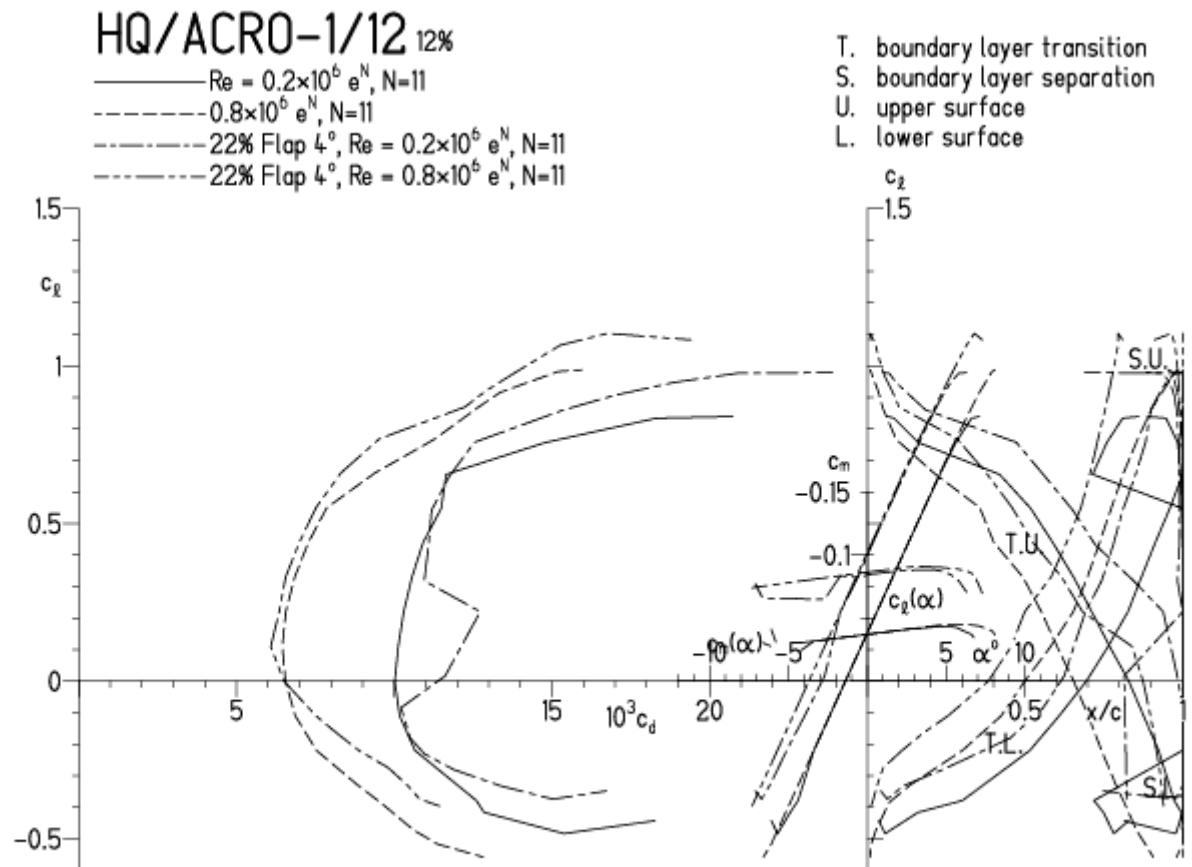


HQ/ACRO-1/12, N=11, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:03

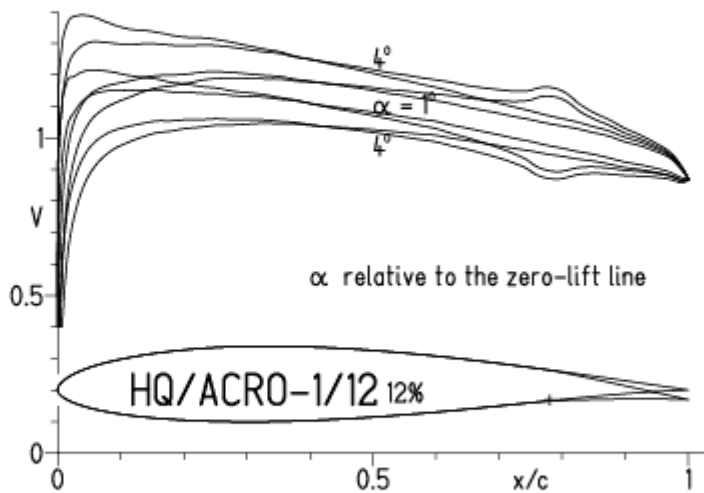


EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:03

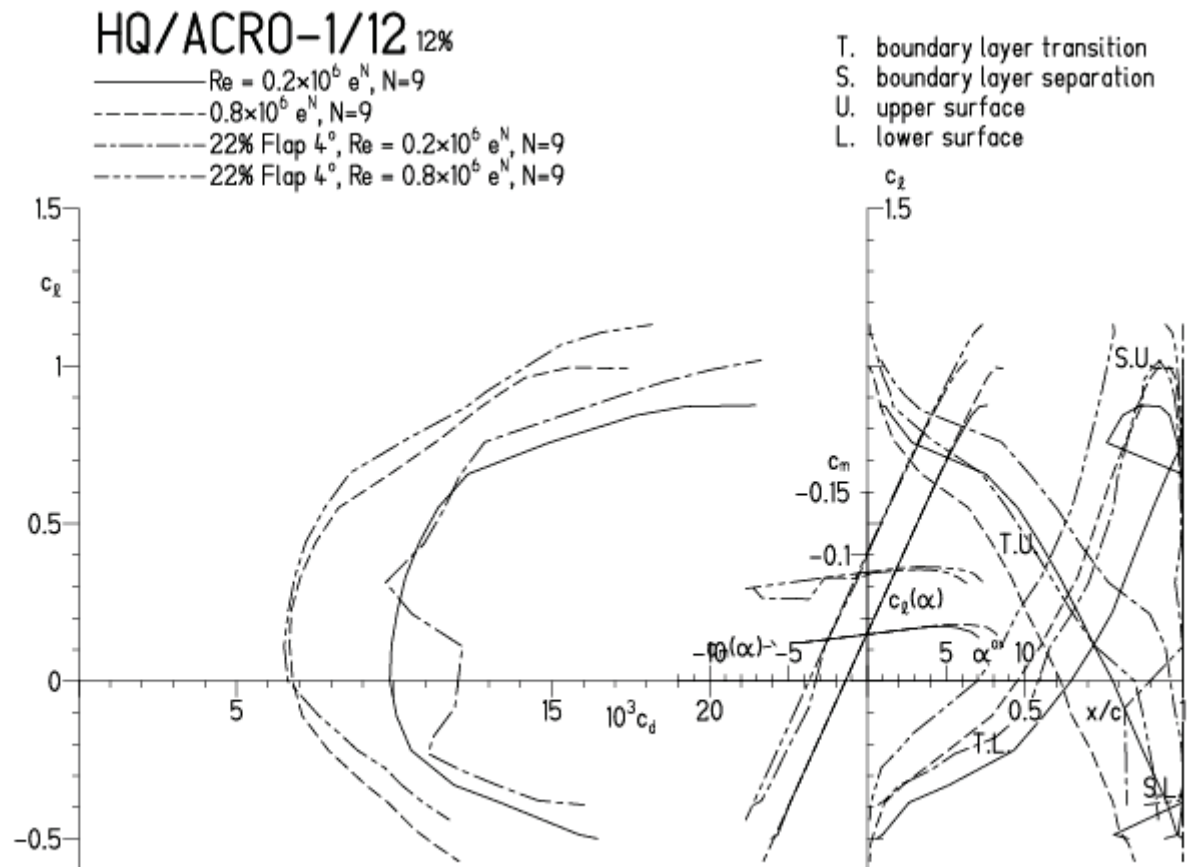


HQ/ACRO-1/12, N=9, mit 4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:06

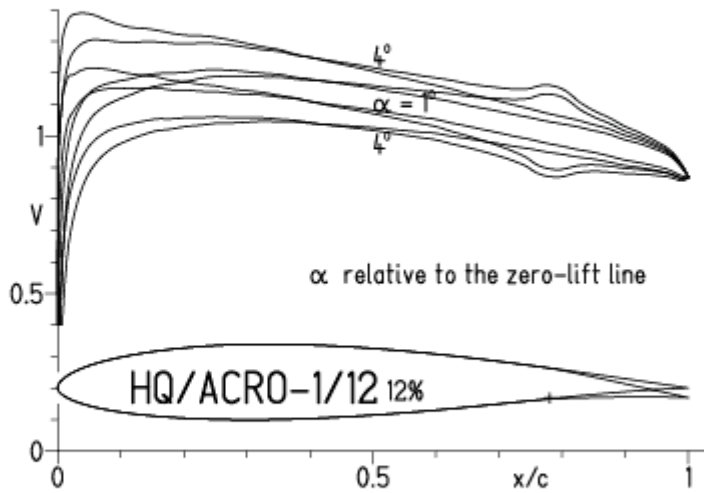


EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:06

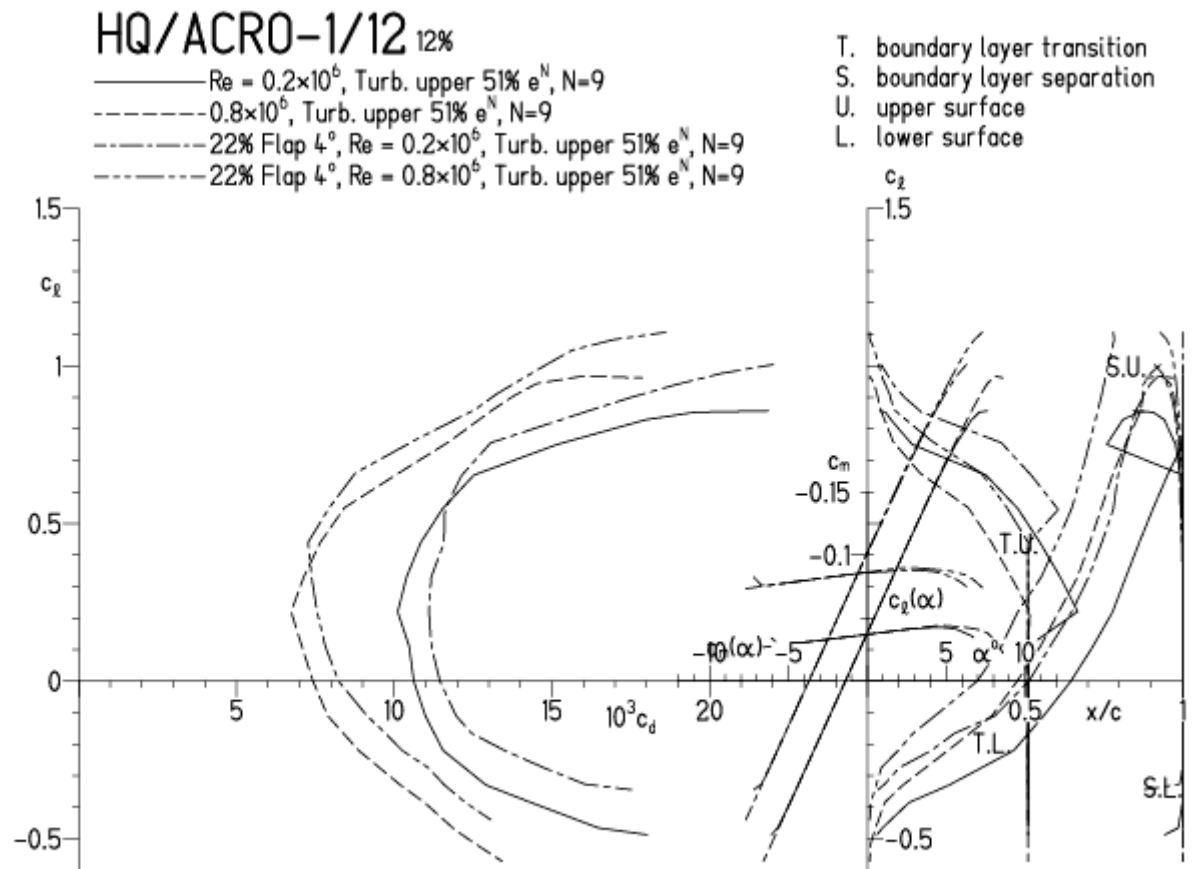


HQ/ACRO-1/12, N=9, mit 4° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:08

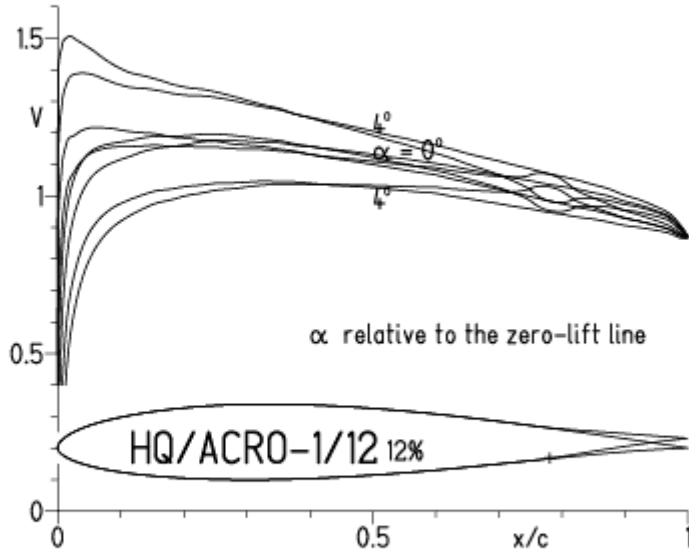


EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:08



HQ/ACRO-1/12, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 v. 8.5.07 RUN 20.3.12 13:11

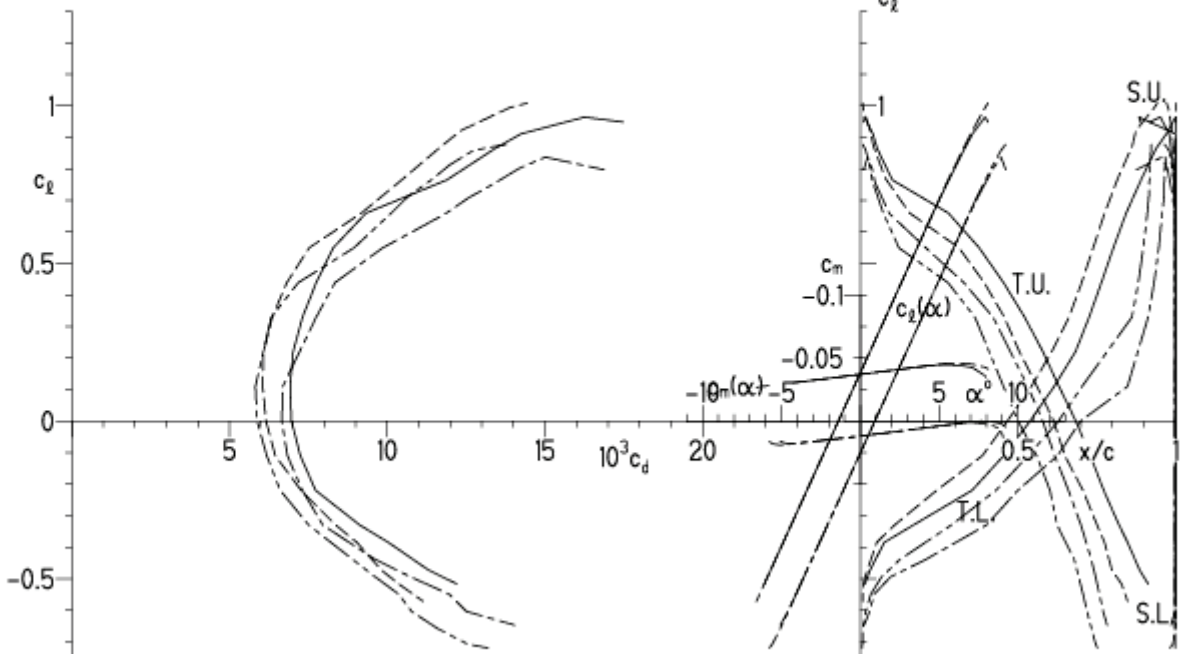


EPPLER 2005 v. 8.5.07 RUN 20.3.12 13:11

HQ/ACRO-1/12 12%

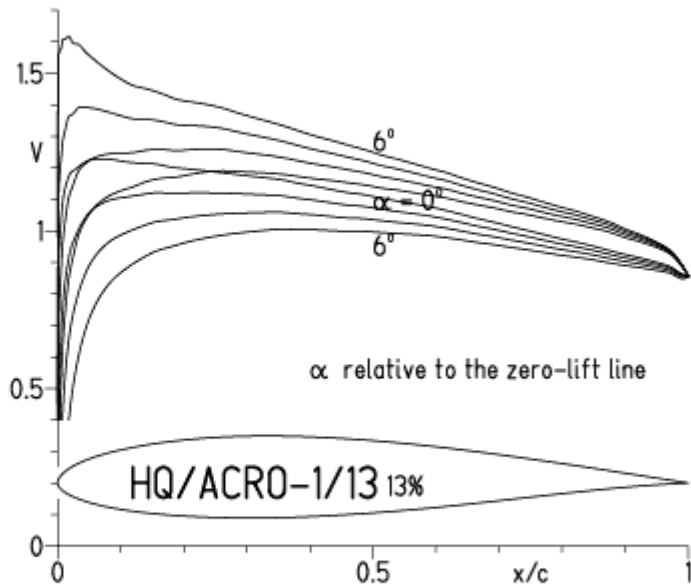
- $Re = 0.6 \times 10^6 e^N$, $N=11$
- - - $1.2 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 1.2 \times 10^6 e^N$, $N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1/13, N=11

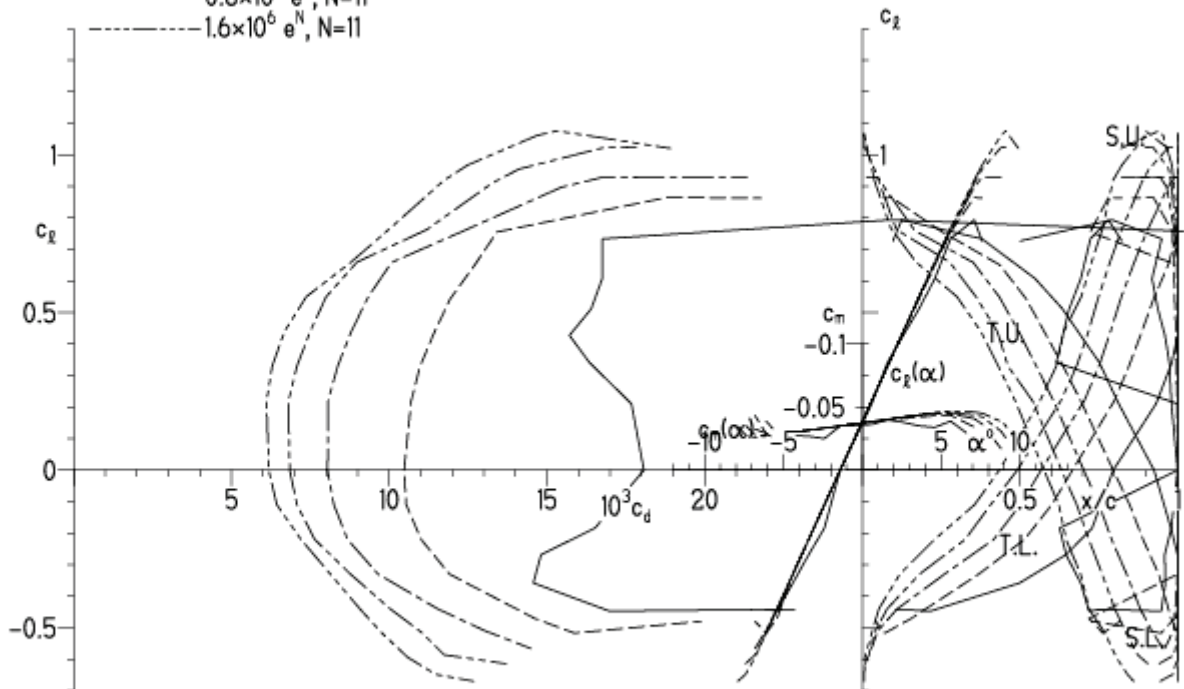
EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:34



EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:34

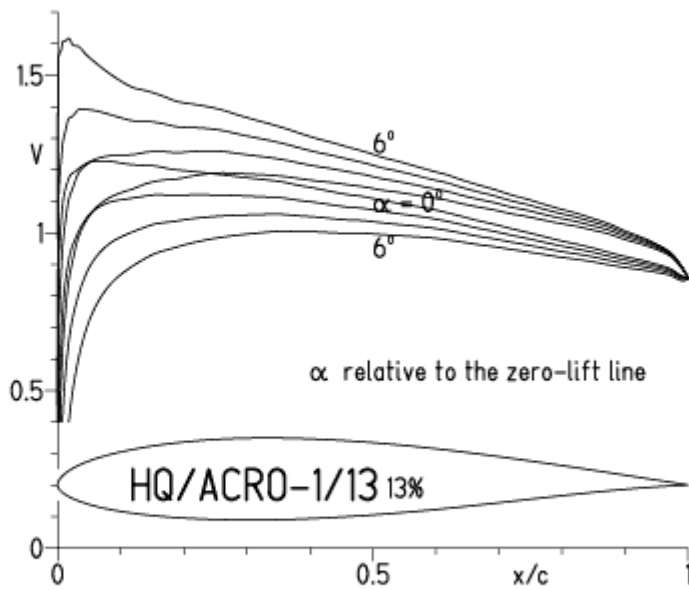
HQ/ACRO-1/13 13%

- $Re = 0.1 \times 10^6$, e^N , $N=11$
- - - 0.2×10^6 , e^N , $N=11$
- · - 0.4×10^6 , e^N , $N=11$
- · - 0.8×10^6 , e^N , $N=11$
- · - 1.6×10^6 , e^N , $N=11$

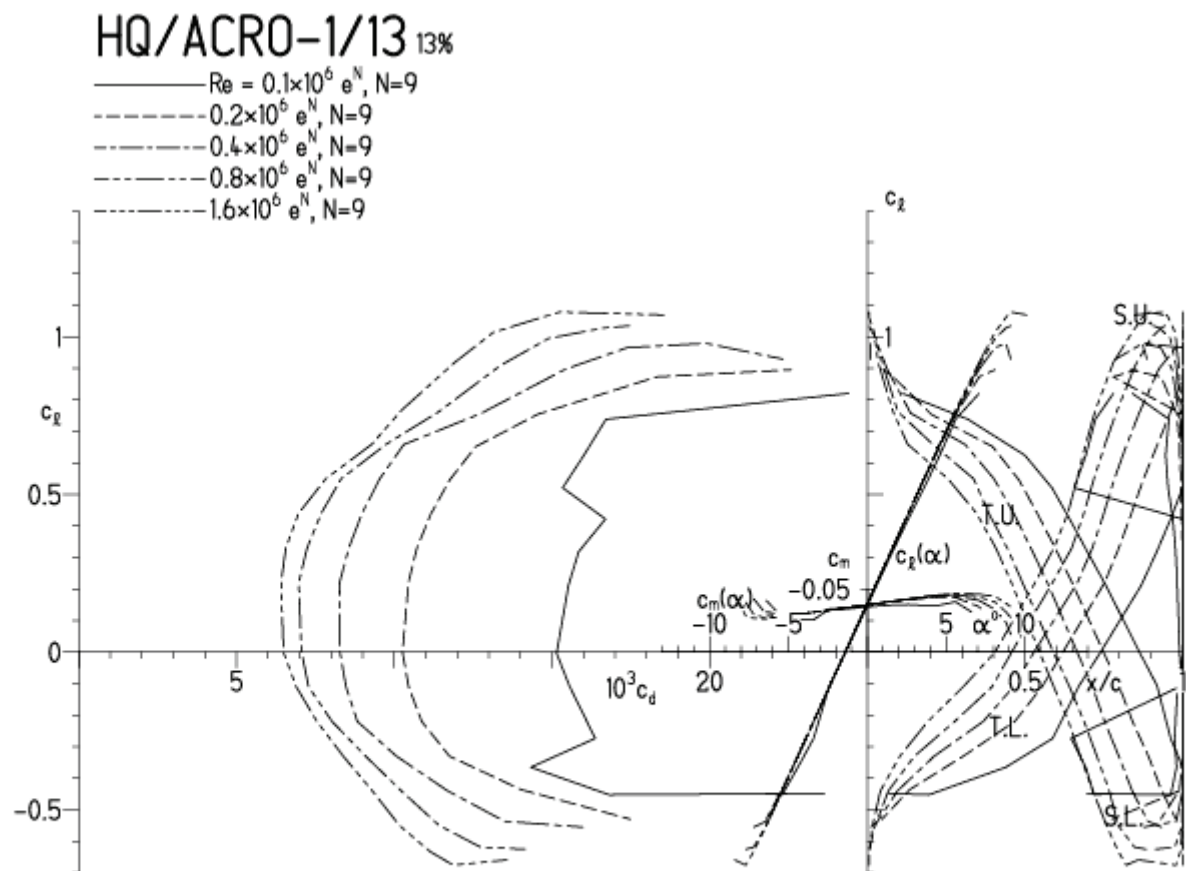


HQ/ACRO-1/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:16

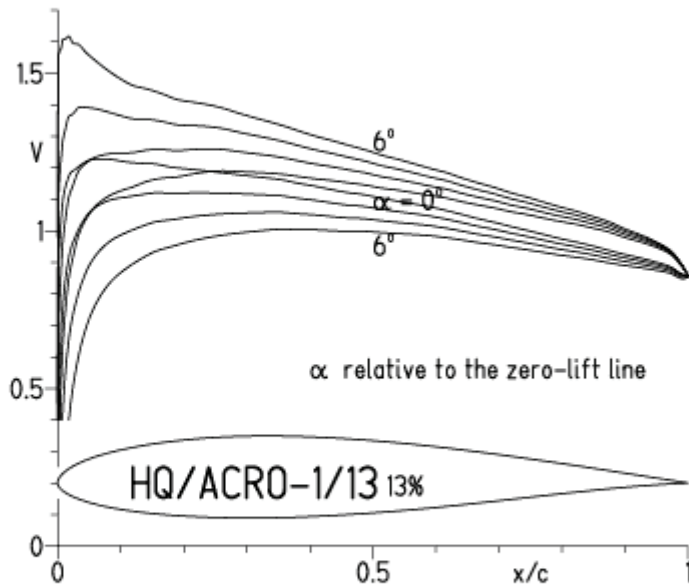


EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:16



HQ/ACRO-1/13, N=9, Turbulatoreffekt bei niedrigen Re-Zahlen
 (optimale Turbulatorposition bei 45 - 50 % der Profiltiefe)

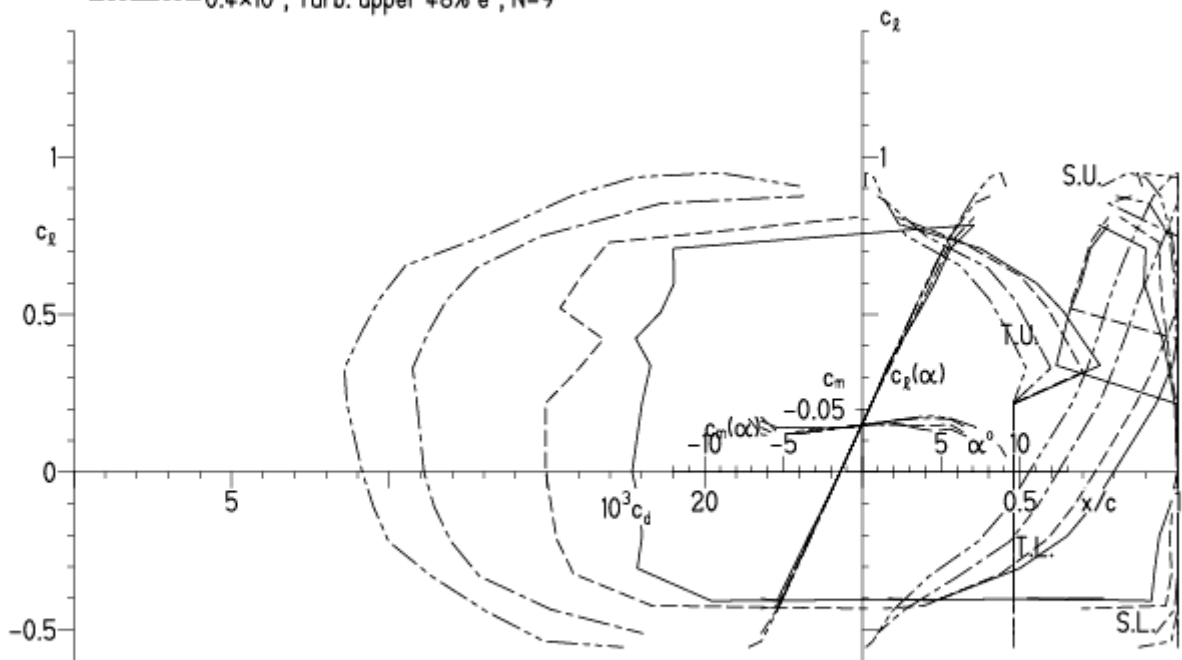
EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:23



EPPLER 2005 V. 8.5.07 RUN 20.3.12 13:23

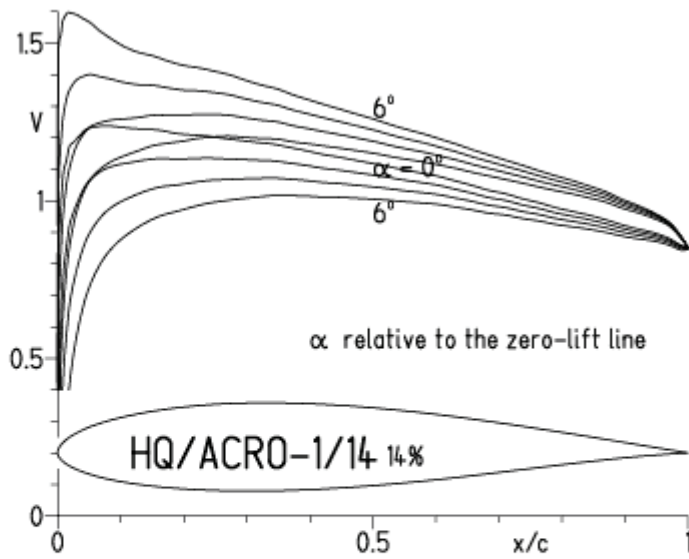
HQ/ACRO-1/13 13%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/ACRO-1/14, N=11

EPPLER 2005 V. 8.5.07 RUN 13.3.12 15:59



EPPLER 2005 V. 8.5.07 RUN 13.3.12 15:59

HQ/ACRO-1/14 14%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$

