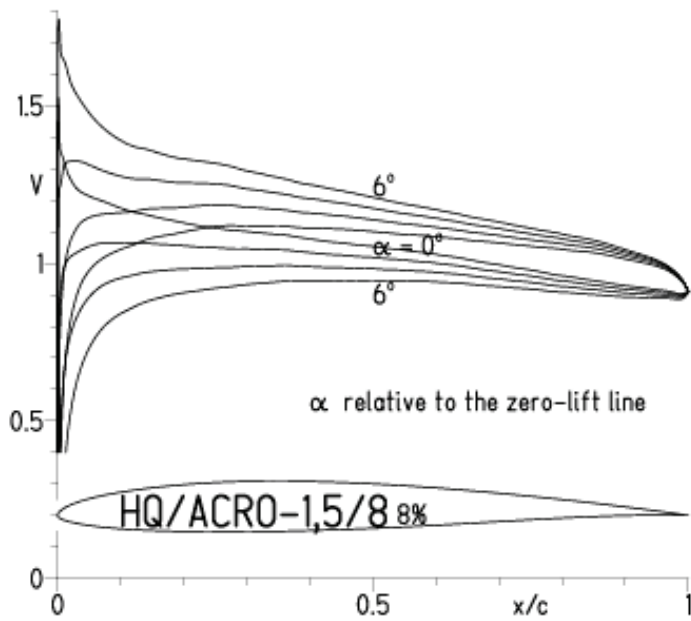


HQ/ACRO-1,5/8, N=11

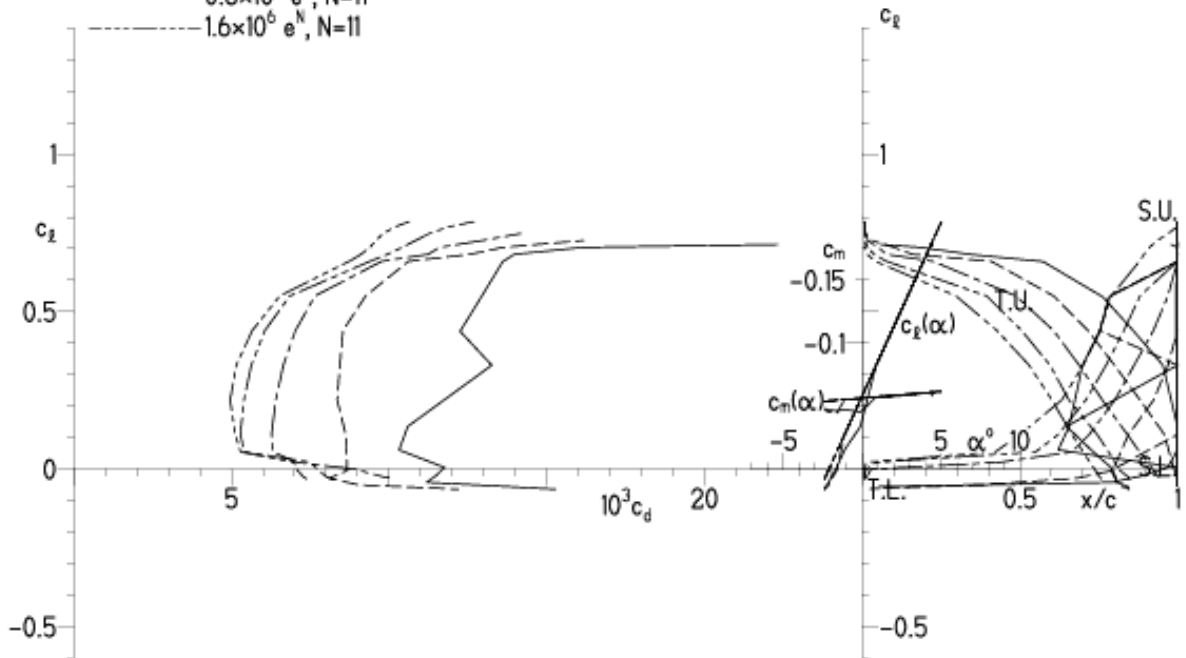
EPPLER 2005 V. 8.5.07 RUN 4.11.11 16:51



EPPLER 2005 V. 8.5.07 RUN 4.11.11 16:51

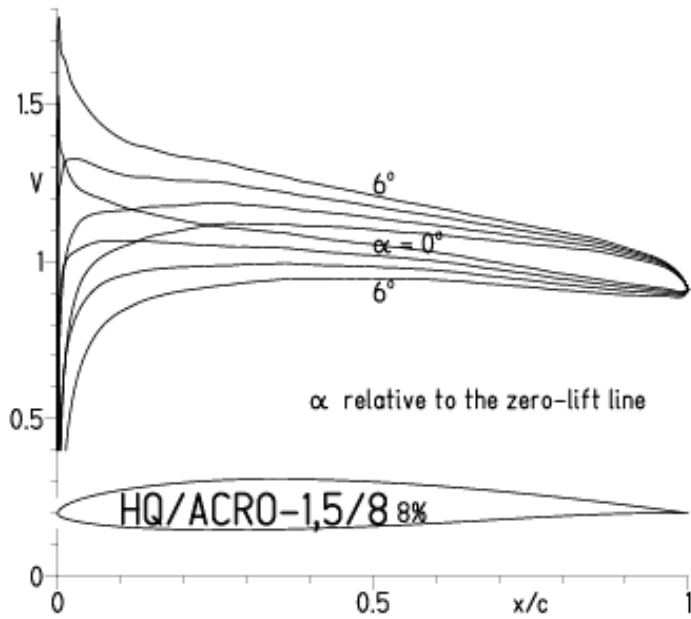
HQ/ACRO-1,5/8 8%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1,5/8, N=9

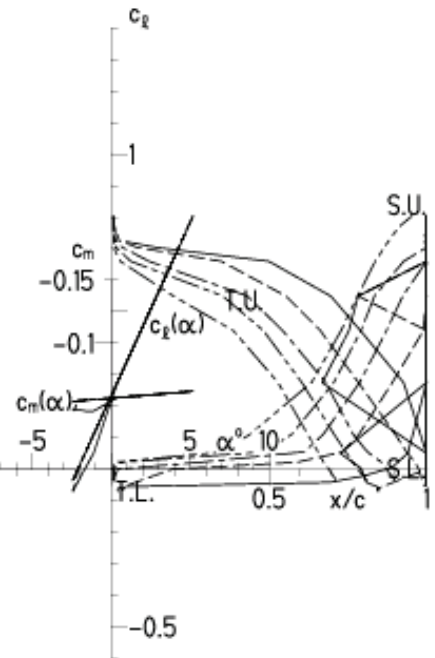
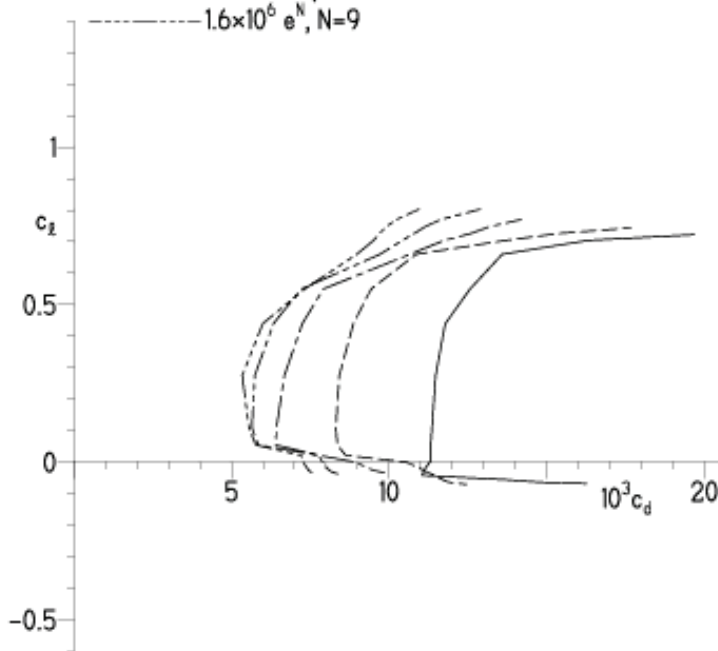
EPPLER 2005 V. 8.5.07 RUN 4.TLIII 16:56



EPPLER 2005 V. 8.5.07 RUN 4.TLIII 16:56

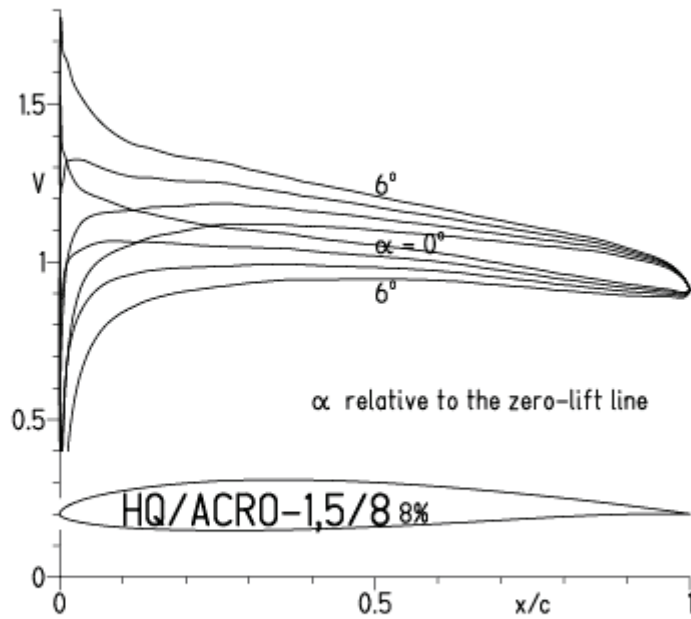
HQ/ACRO-1,5/8 8%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · · - $0.8 \times 10^6 e^N, N=9$
- · · · - $1.6 \times 10^6 e^N, N=9$



HQ/ACRO-1,5/8, N=9, niedrigen Re-Zahlen (schmale Flügelenden im Langsamflug)

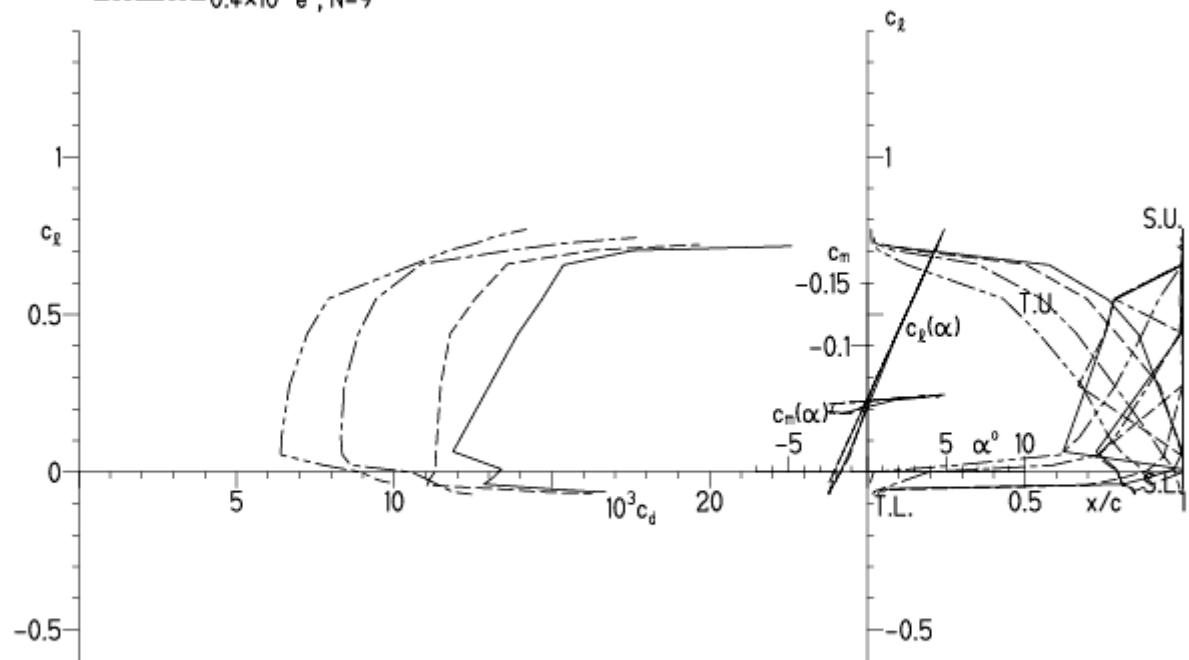
EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:33



EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:33

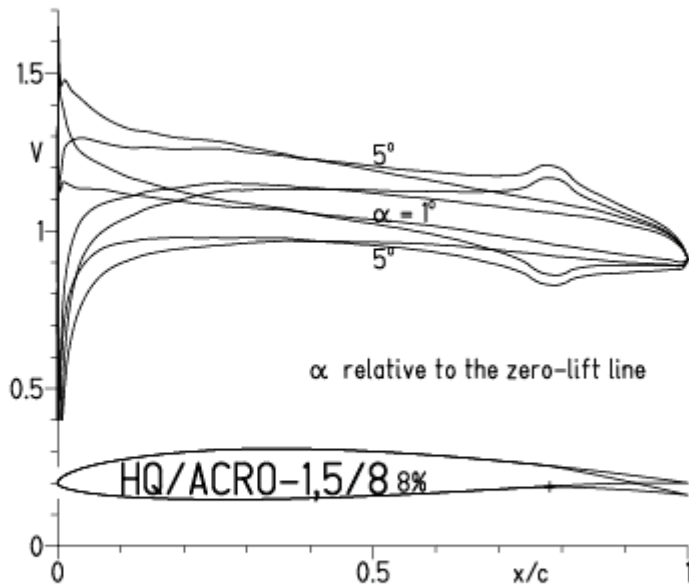
HQ/ACRO-1,5/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/ACRO-1,5/8, N=11, mit 5° Wölbklappenausschlag

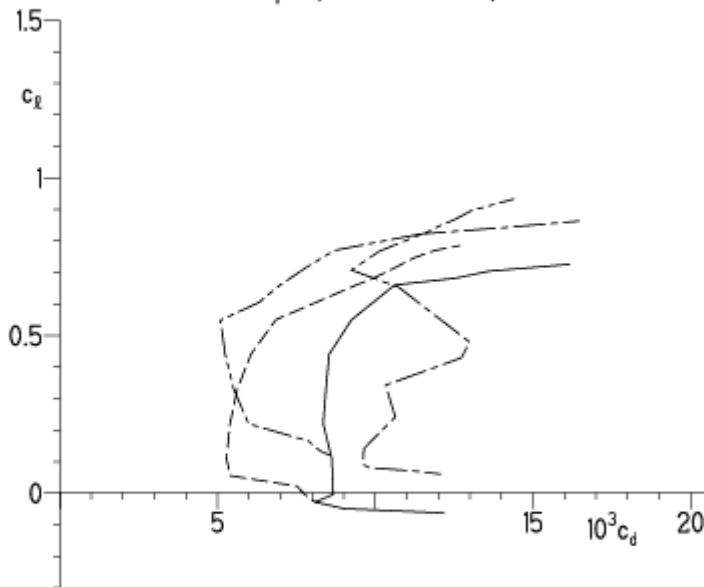
EPPLER 2005 V. 8.5.07 RUN 20.3.12 15:57



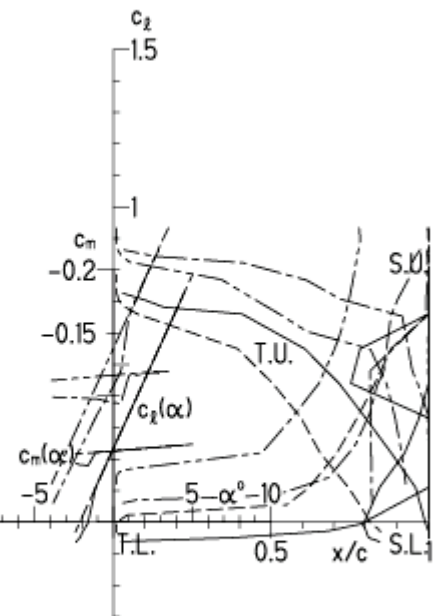
EPPLER 2005 V. 8.5.07 RUN 20.3.12 15:57

HQ/ACRO-1,5/8 8%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.8 \times 10^6 e^N, N=11$
- · - · 22% Flap $5^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $5^\circ, Re = 0.8 \times 10^6 e^N, N=11$

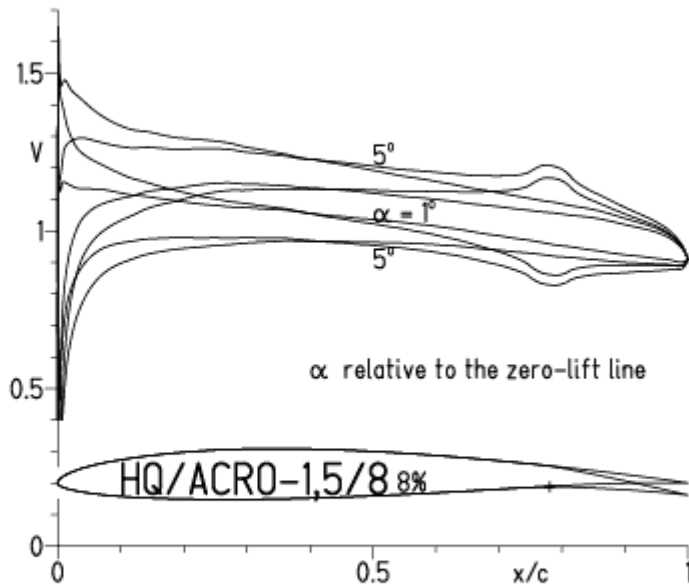


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1,5/8, N=9, mit 5° Wölbklappenausschlag

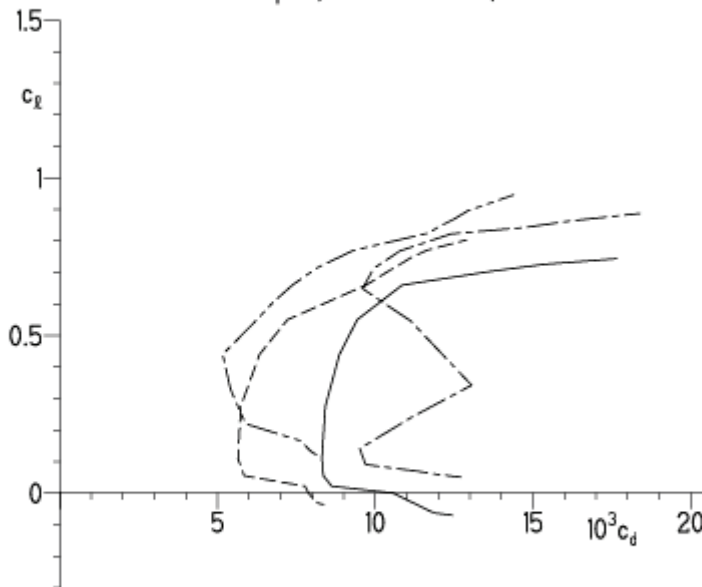
EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:04



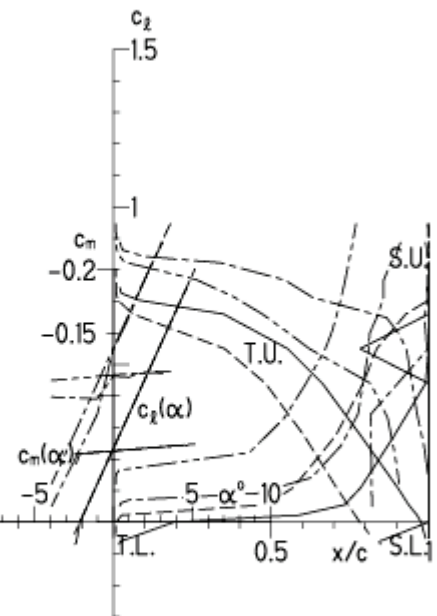
EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:04

HQ/ACRO-1,5/8 8%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 5°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 5°, $Re = 0.8 \times 10^6 e^N, N=9$

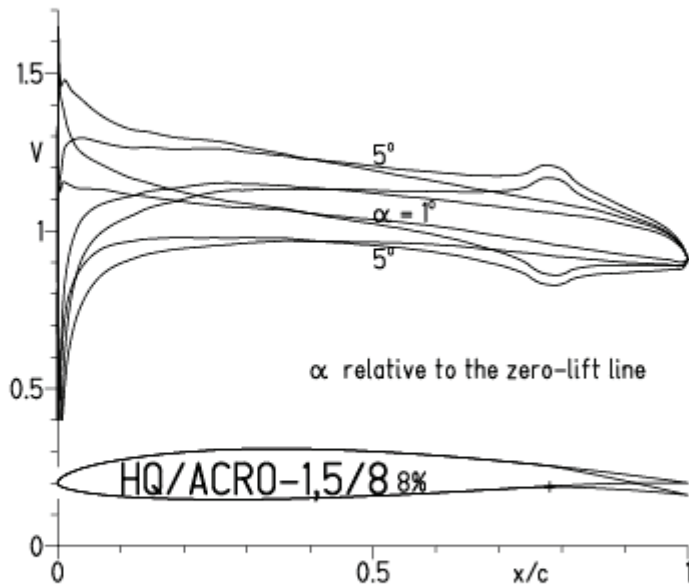


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1,5/8, N=9, mit 5° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

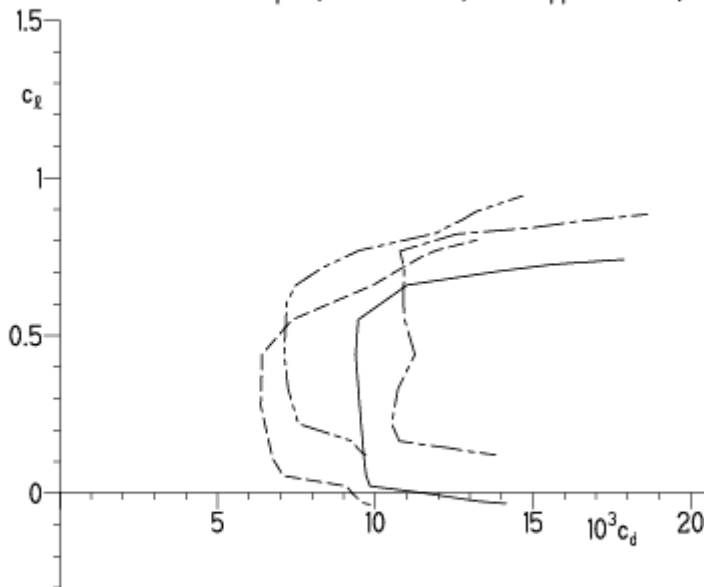
EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:06



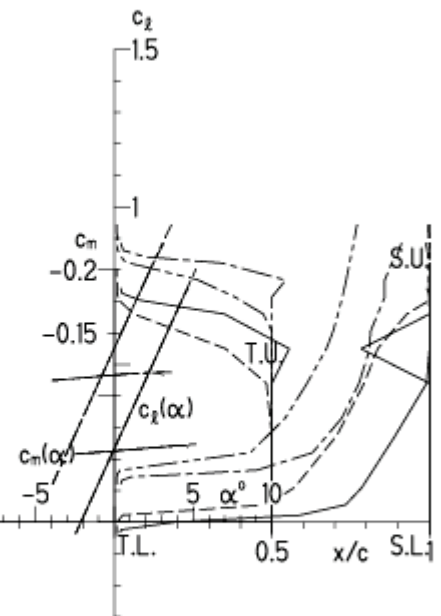
EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:06

HQ/ACRO-1,5/8 8%

- $Re = 0.2 \times 10^6$, Turb. upper 50% e^N , N=9
- - - 0.8×10^6 , Turb. upper 50% e^N , N=9
- · - · - 22% Flap 5°, $Re = 0.2 \times 10^6$, Turb. upper 50% e^N , N=9
- · - · - 22% Flap 5°, $Re = 0.8 \times 10^6$, Turb. upper 50% e^N , N=9

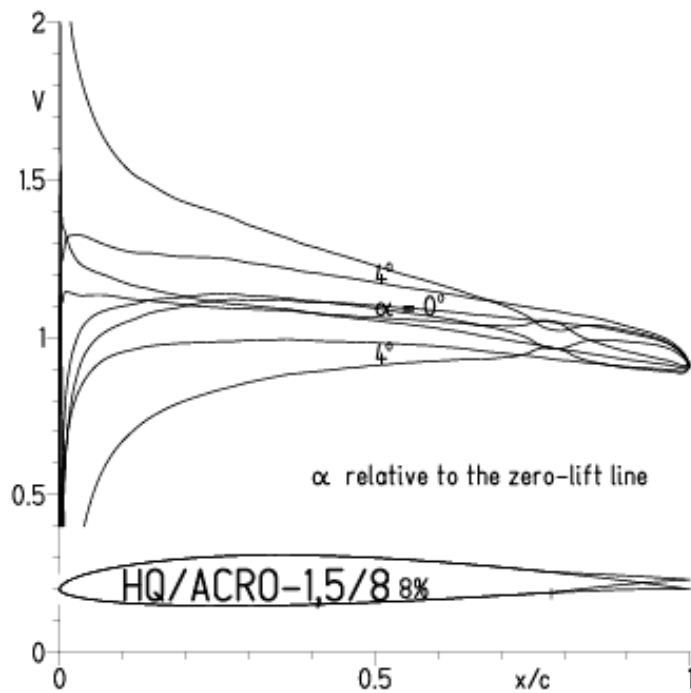


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1,5/8, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 V. 8.5.07 RUN 4.TLIII 18:10

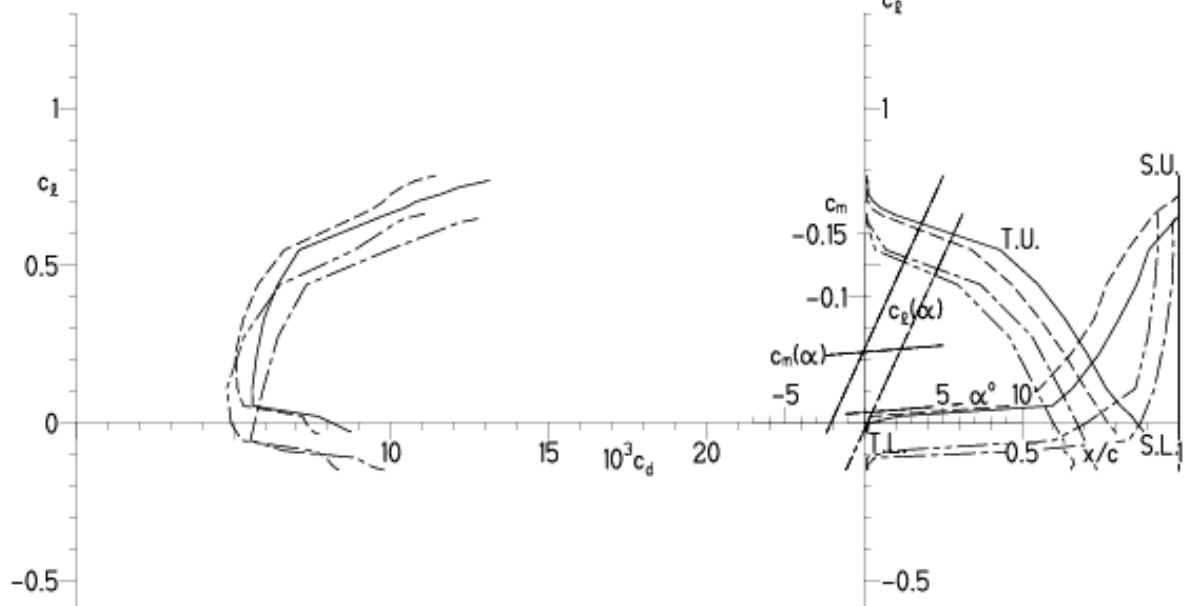


EPPLER 2005 V. 8.5.07 RUN 4.TLIII 18:10

HQ/ACRO-1,5/8 8%

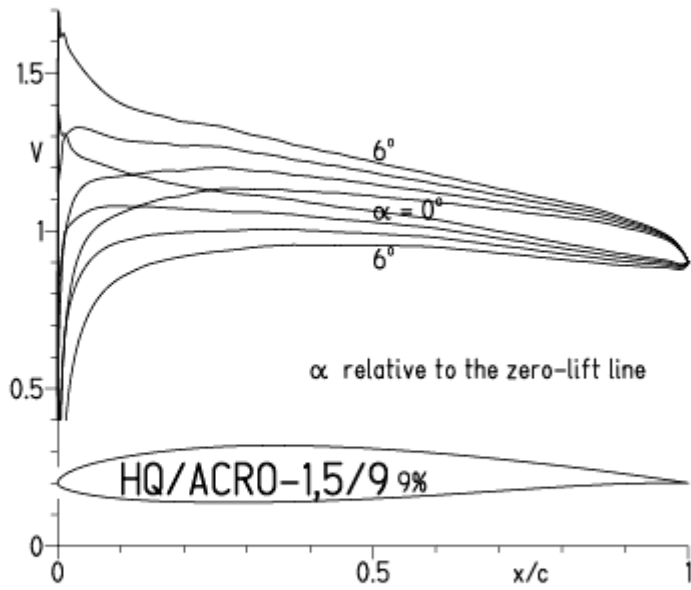
- $Re = 0.6 \times 10^6$ e^N, N=11
- - - 1.2×10^6 e^N, N=11
- · - · - 22% Flap -4° , $Re = 0.6 \times 10^6$ e^N, N=11
- · - · - 22% Flap -4° , $Re = 1.2 \times 10^6$ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1,5/9, N=11

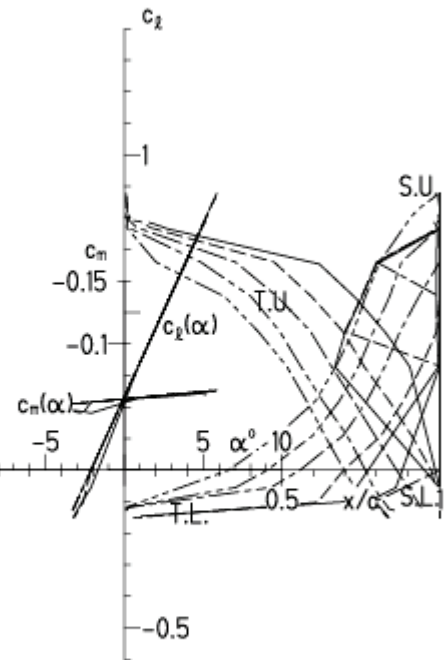
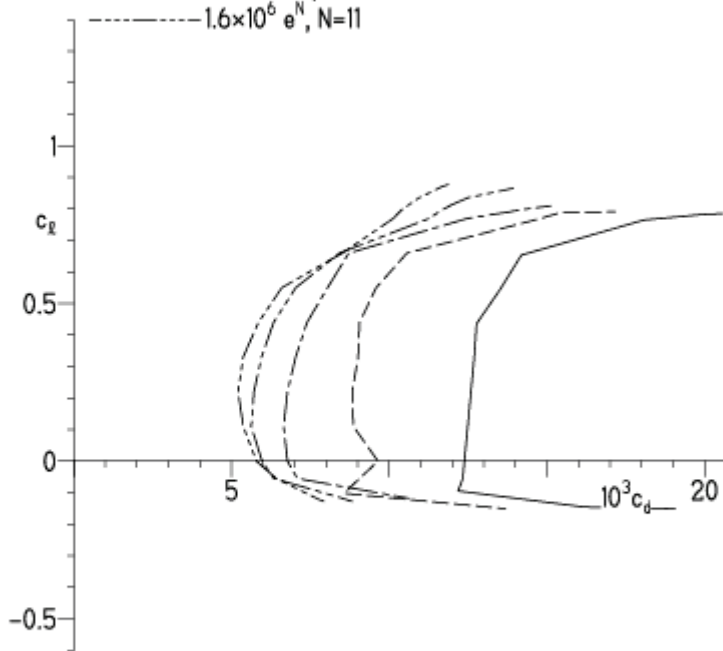
EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:21



EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:21

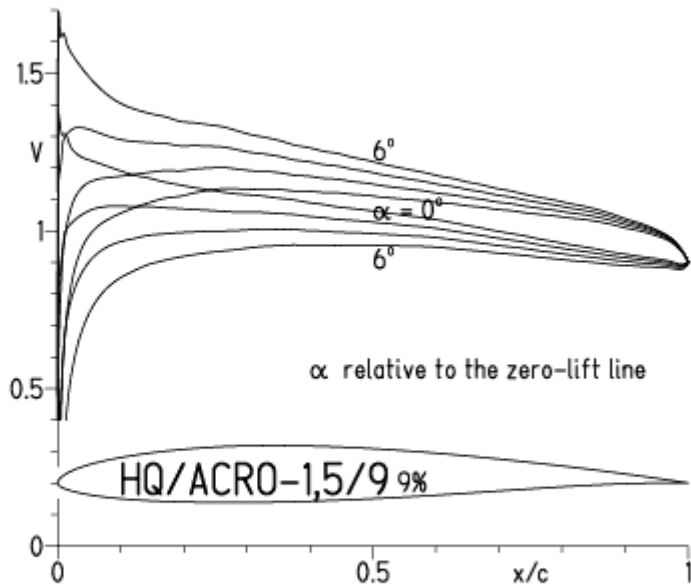
HQ/ACRO-1,5/9 9%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · · - $0.8 \times 10^6 e^N, N=11$
- · · · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1,5/9, N=9

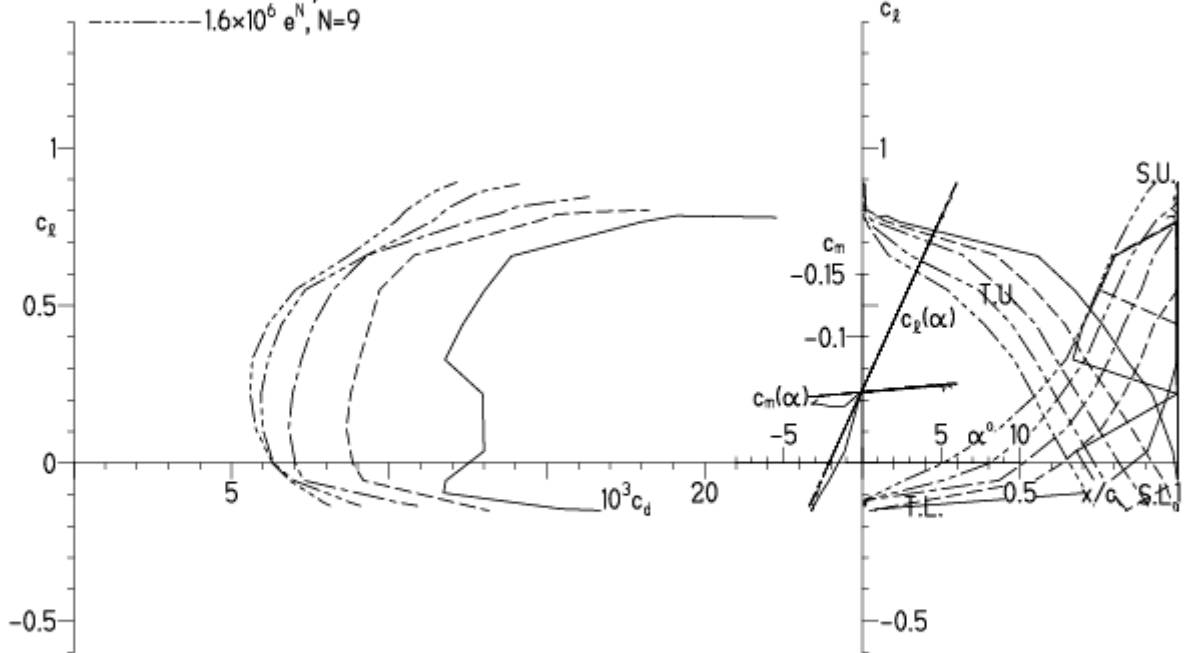
EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:24



EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:24

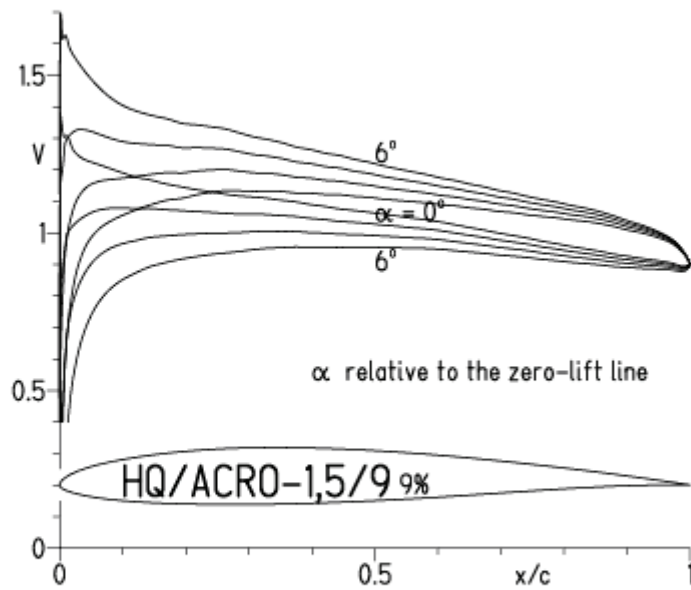
HQ/ACRO-1,5/9 9%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/ACRO-1,5/9, N=9, niedrigen Re-Zahlen (schmale Flügelenden im Langsamflug)

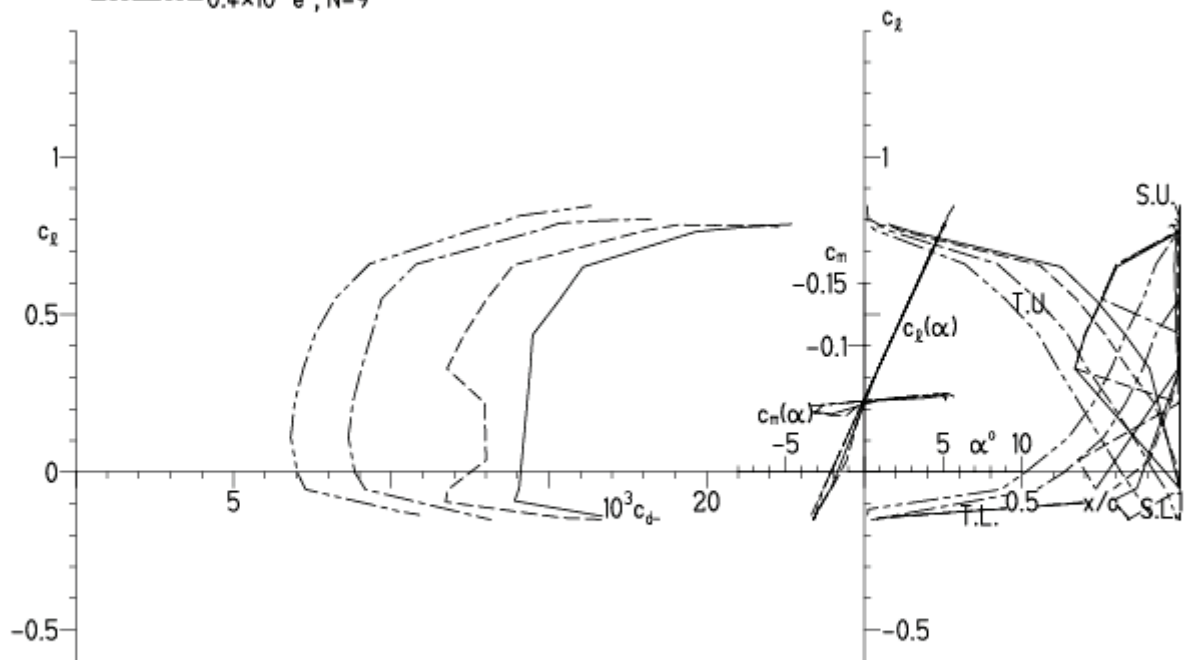
EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:30



EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:30

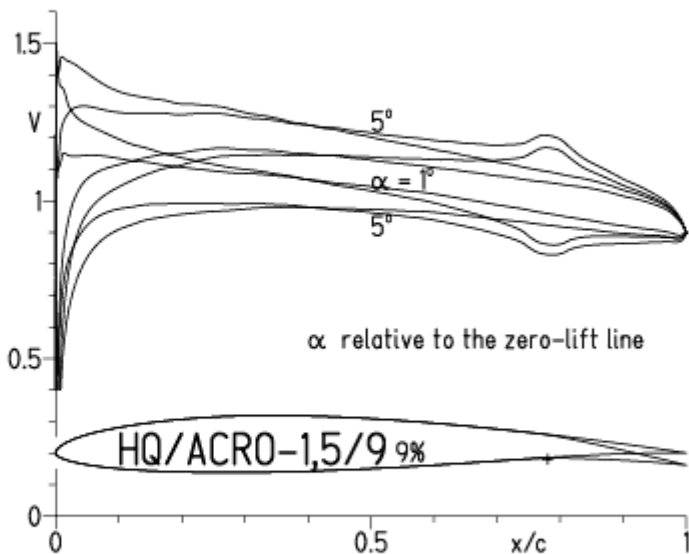
HQ/ACRO-1,5/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/ACRO-1,5/9, N=11, mit 5° Wölbklappenausschlag

EPPLER 2005 v. 8.5.07 RUN 20.3.12 16:40

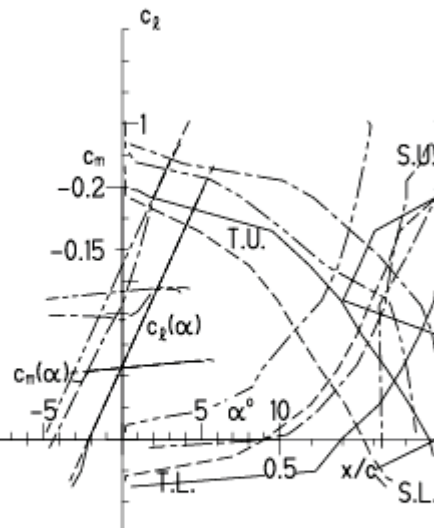
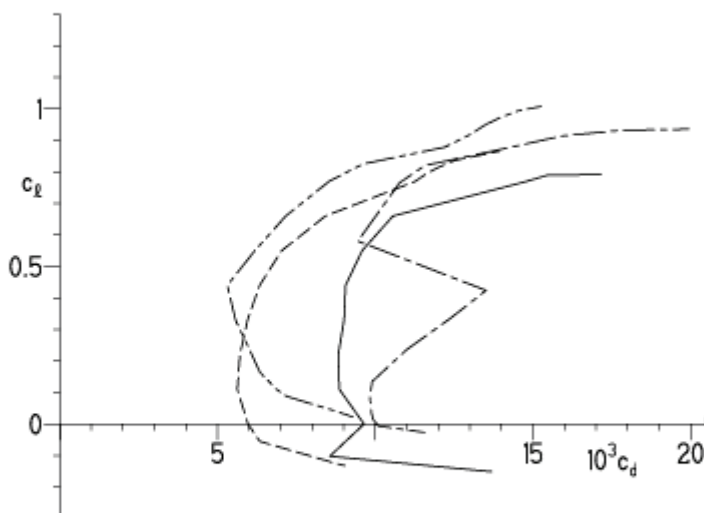


EPPLER 2005 v. 8.5.07 RUN 20.3.12 16:40

HQ/ACRO-1,5/9 9%

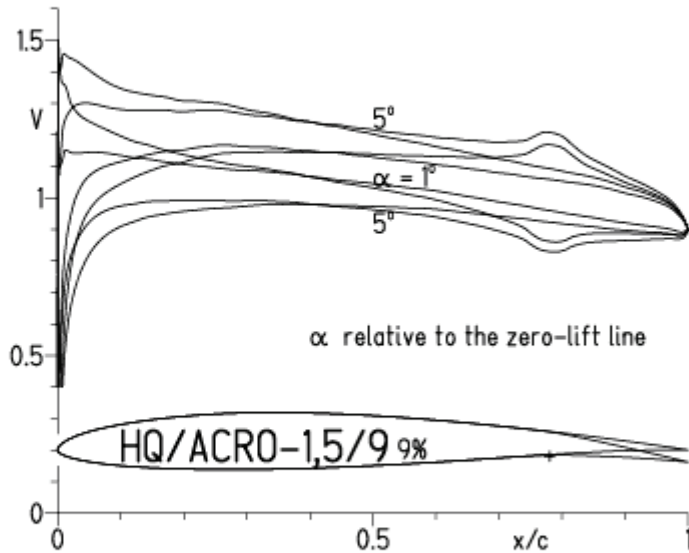
- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.8 \times 10^6 e^N, N=11$
- · - · 22% Flap $5^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $5^\circ, Re = 0.8 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

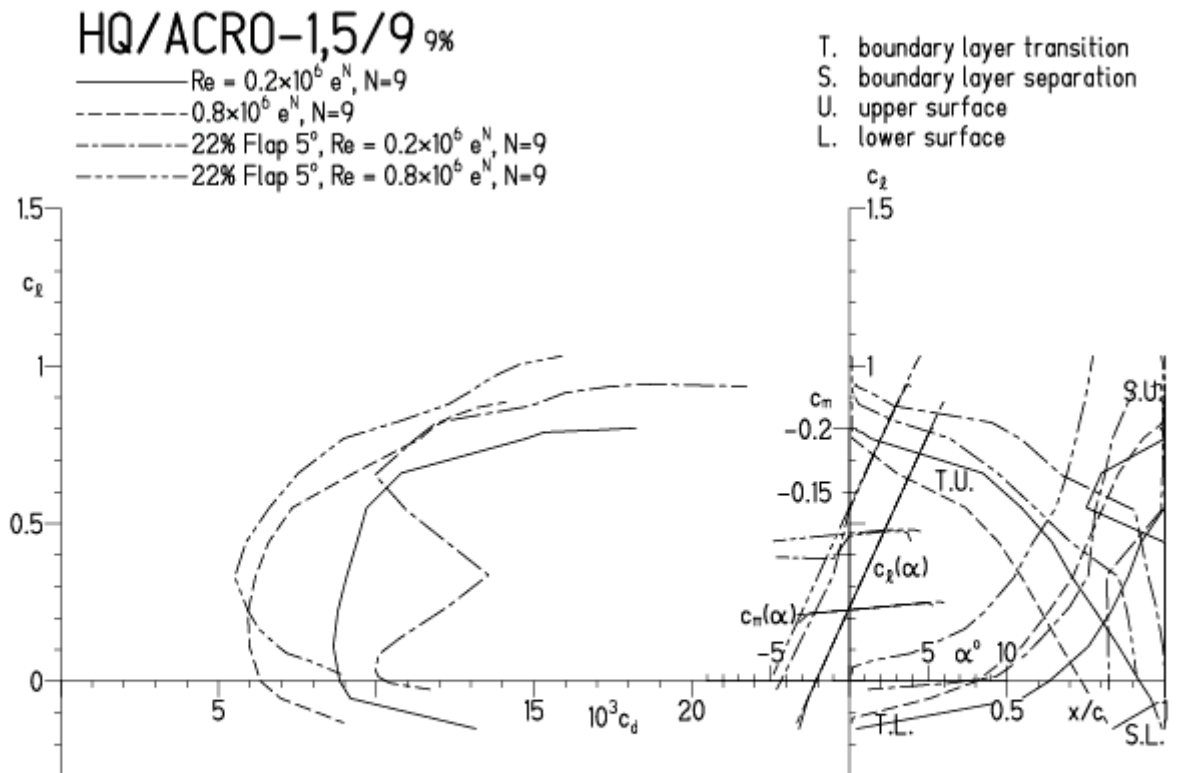


HQ/ACRO-1,5/9, N=9, mit 5° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:46

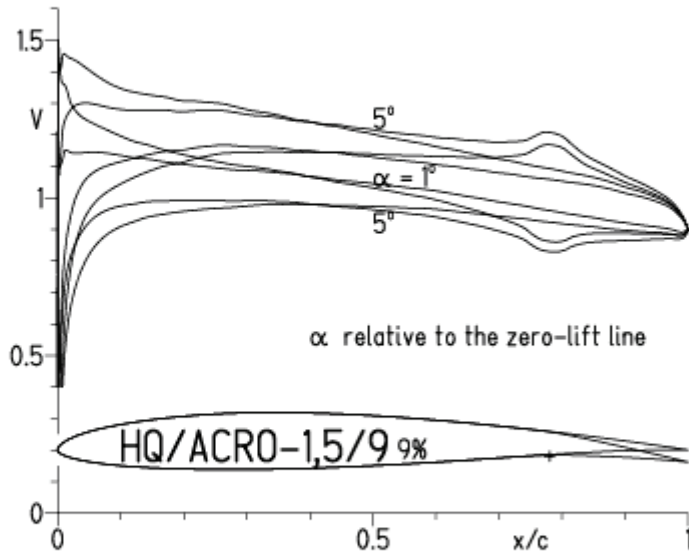


EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:46



HQ/ACRO-1,5/9, N=9, mit 5° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:49

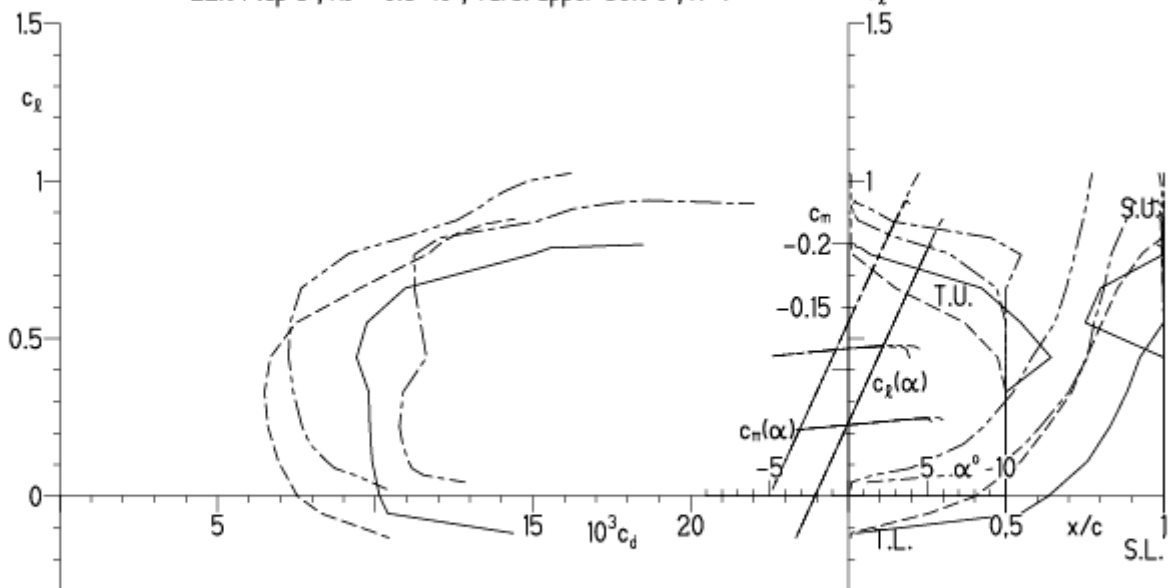


EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:49

HQ/ACRO-1,5/9 9%

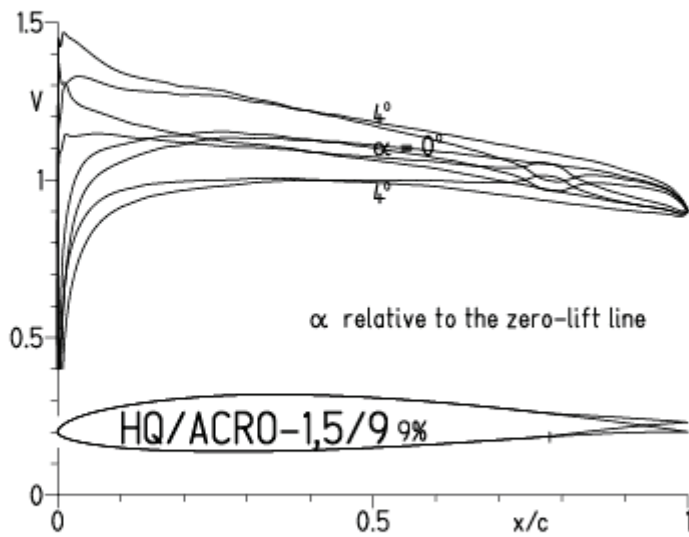
- $Re = 0.2 \times 10^6$, Turb. upper 50% e^N , N=9
- - - 0.8×10^6 , Turb. upper 50% e^N , N=9
- · - · 22% Flap 5°, $Re = 0.2 \times 10^6$, Turb. upper 50% e^N , N=9
- · - · 22% Flap 5°, $Re = 0.8 \times 10^6$, Turb. upper 50% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1,5/9, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:56

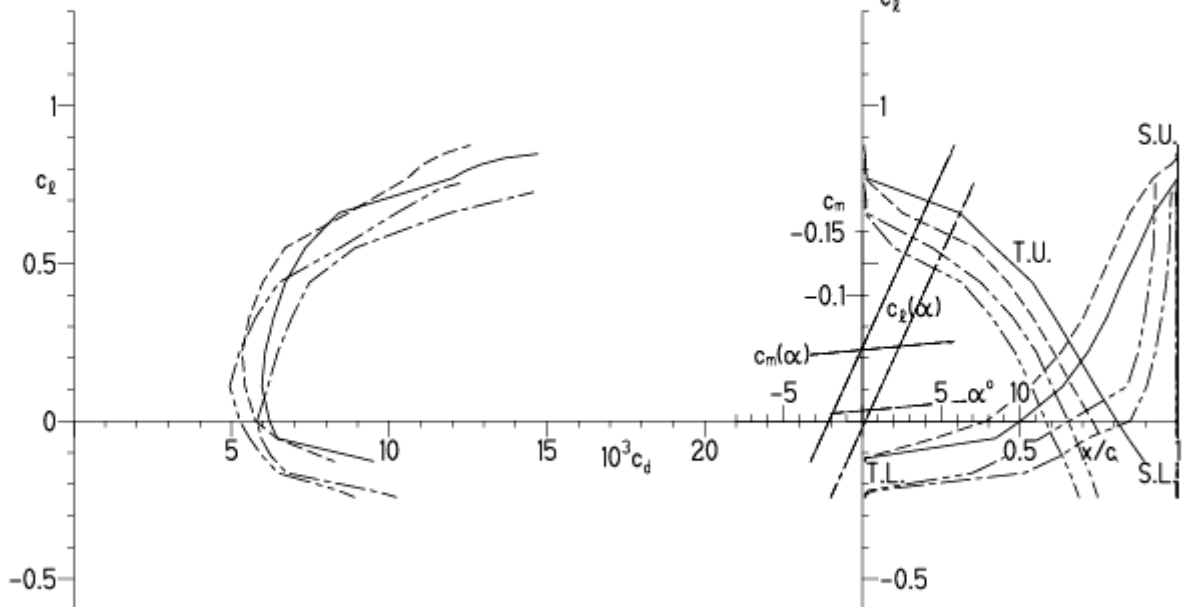


EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:56

HQ/ACRO-1,5/9 9%

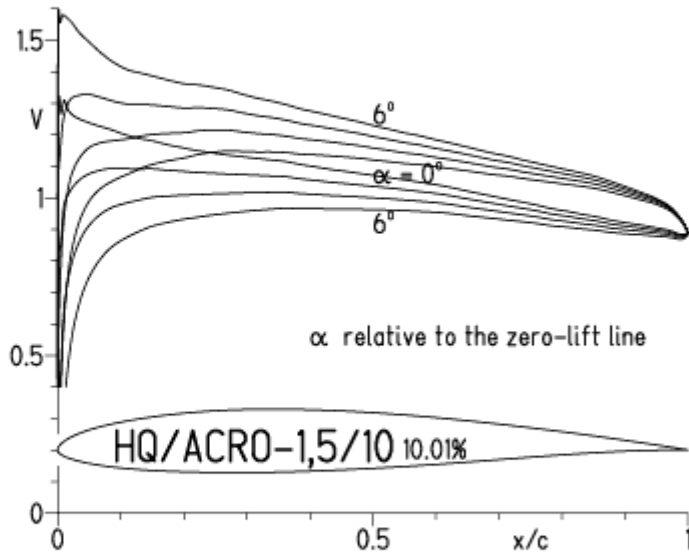
- $Re = 0.6 \times 10^6 e^N, N=11$
- - - $1.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 1.2 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1,5/10, N=11

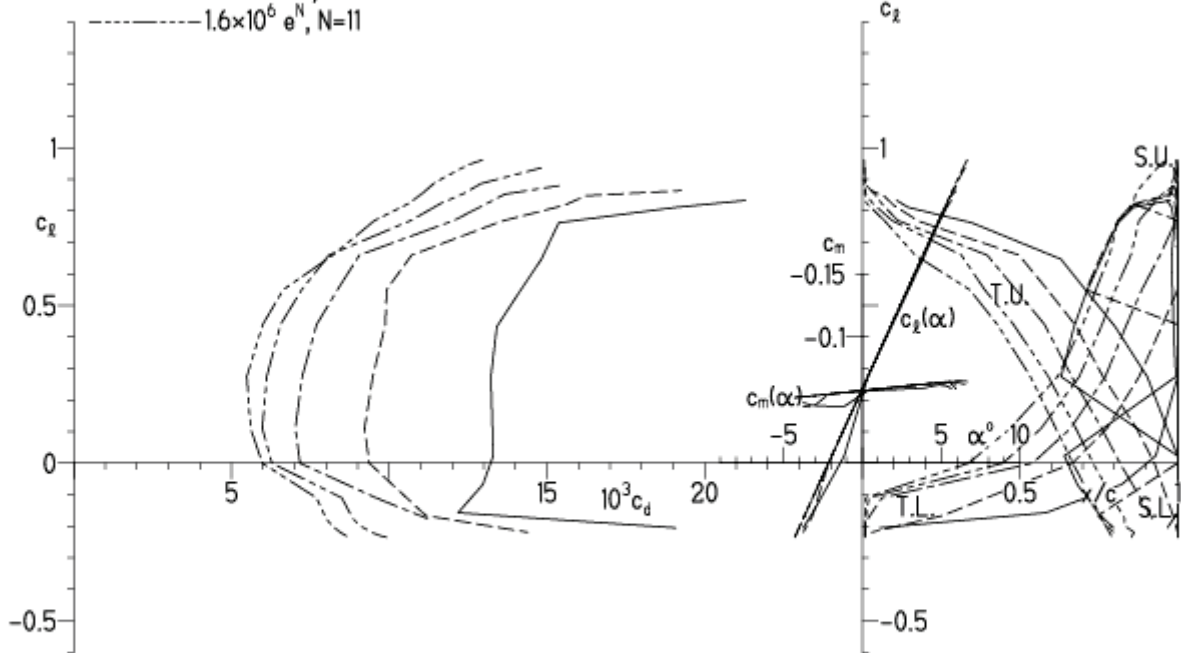
EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:59



EPPLER 2005 V. 8.5.07 RUN 20.3.12 16:59

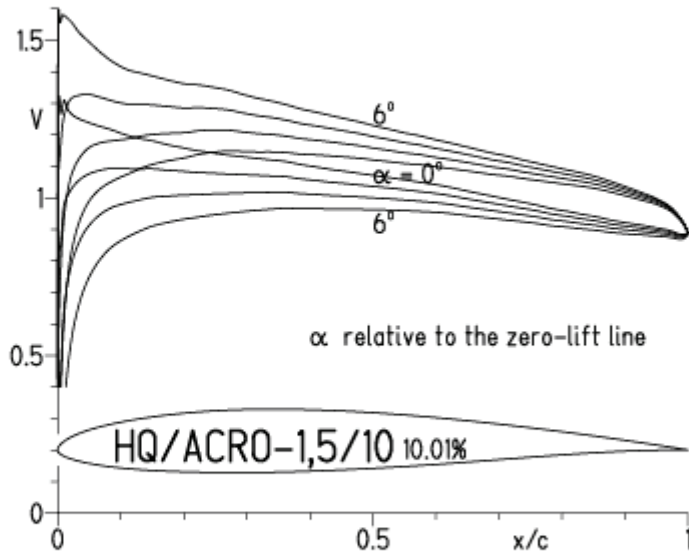
HQ/ACRO-1,5/10 10.01%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · · - $0.8 \times 10^6 e^N, N=11$
- · · · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1,5/10, N=9

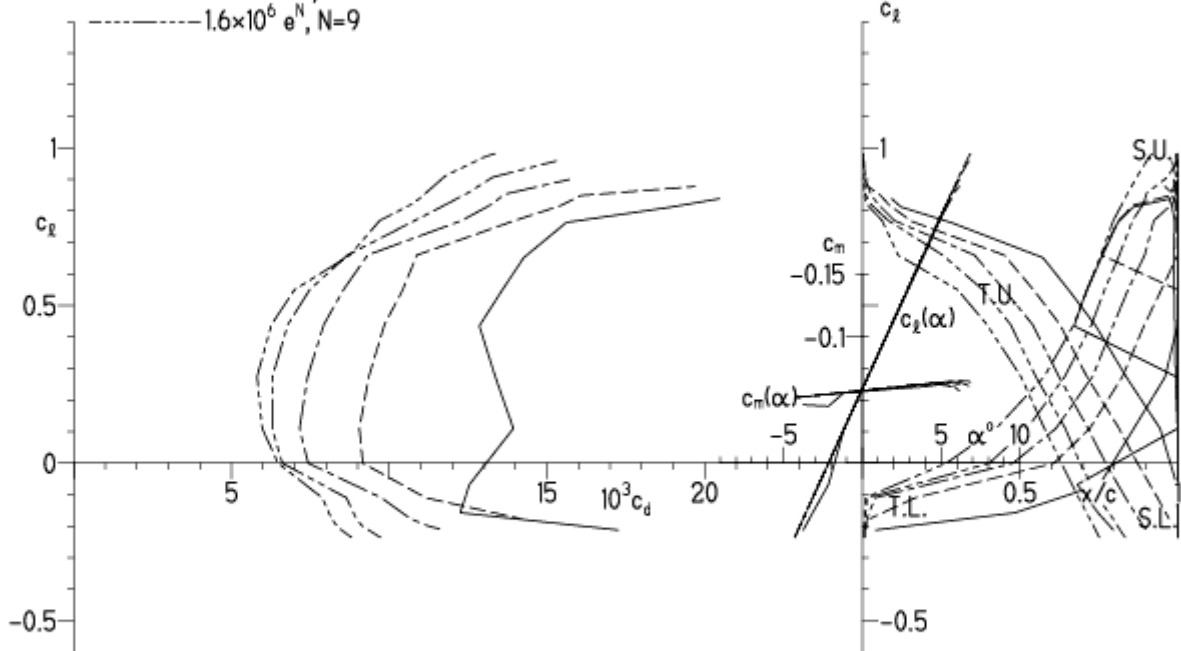
EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:09



EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:09

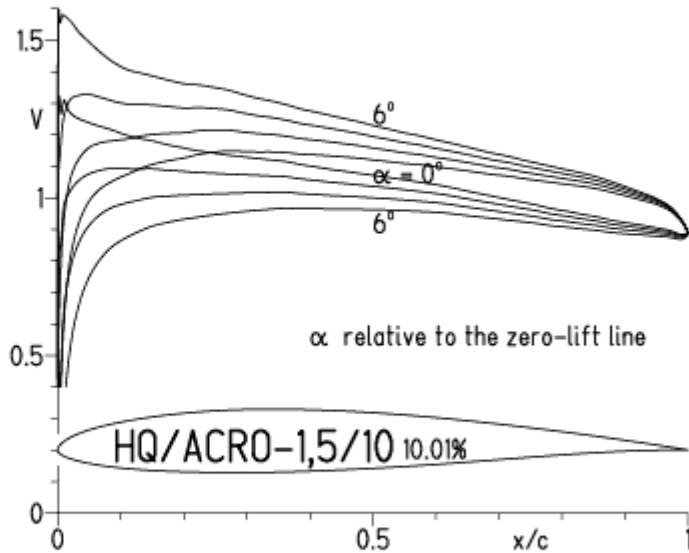
HQ/ACRO-1,5/10 10.01%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · · - $0.8 \times 10^6 e^N, N=9$
- · · · - $1.6 \times 10^6 e^N, N=9$



HQ/ACRO-1,5/10, N=9, Turbulatoreffekt bei niedrigen Re-Zahlen
 (optimale Turbulatorposition bei 45 - 55% der Profiltiefe)

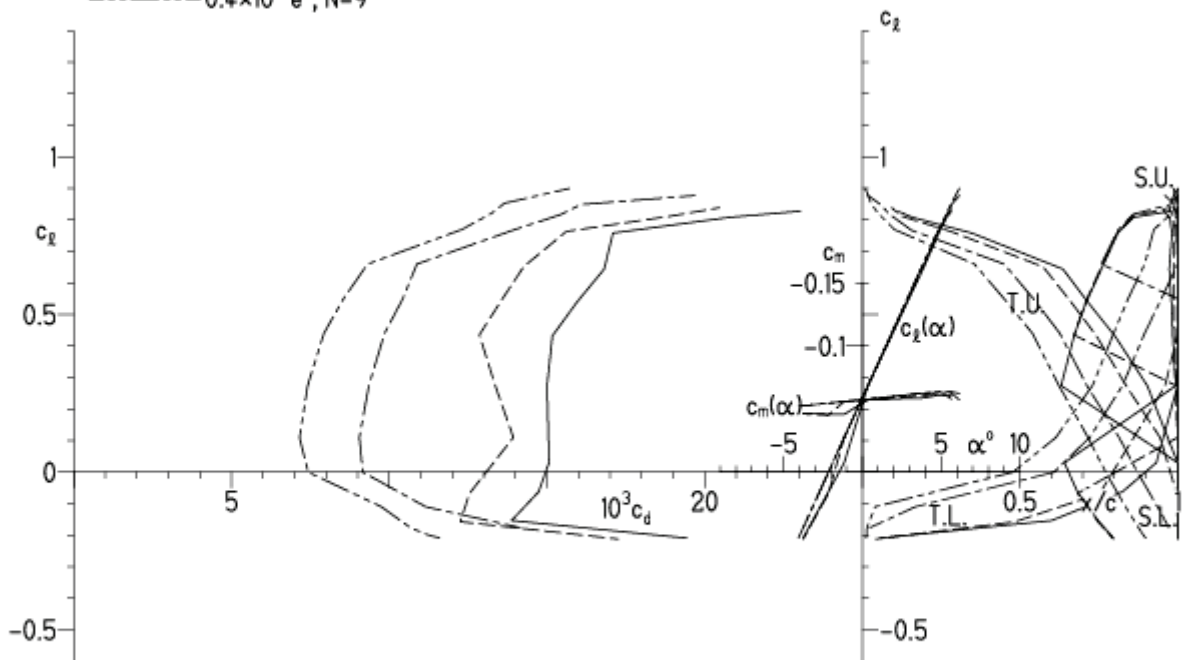
EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:13



EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:13

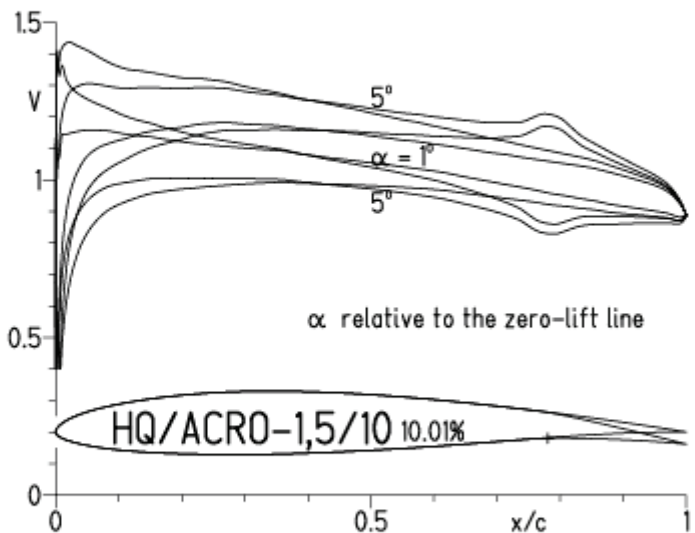
HQ/ACRO-1,5/10 10.01%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/ACRO-1,5/10, N=11, mit 5° Wölbklappenausschlag

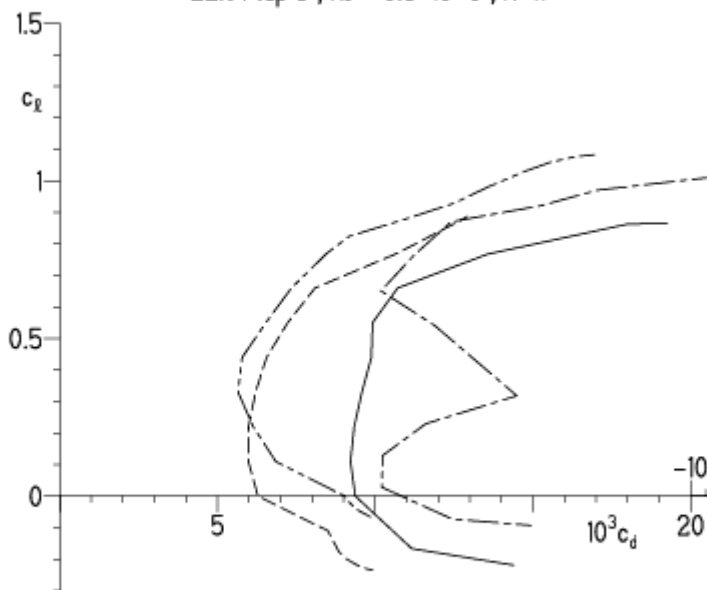
EPPLER 2005 v. 8.5.07 RUN 20.3.12 17:20



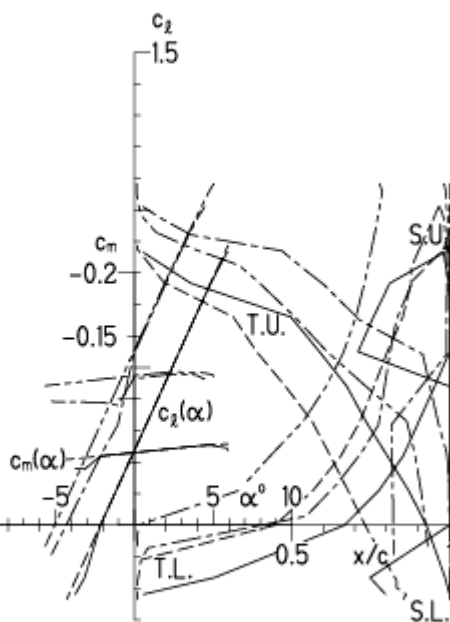
EPPLER 20

HQ/ACRO-1,5/10 10.01%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.8 \times 10^6 e^N, N=11$
- · - · 22% Flap $5^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $5^\circ, Re = 0.8 \times 10^6 e^N, N=11$

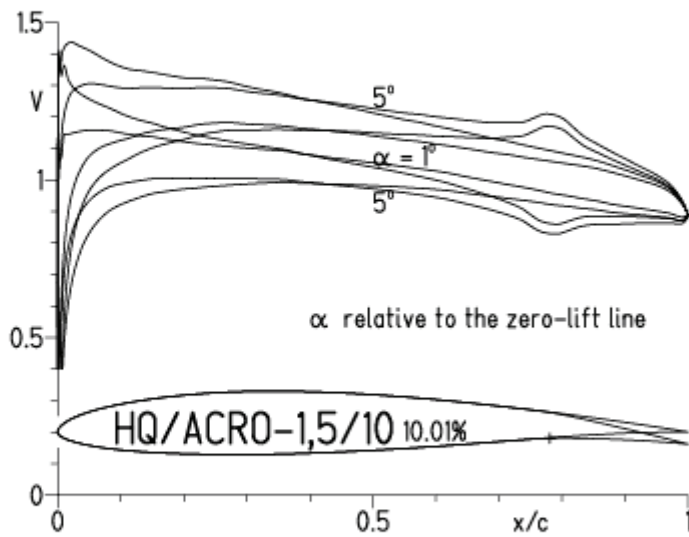


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

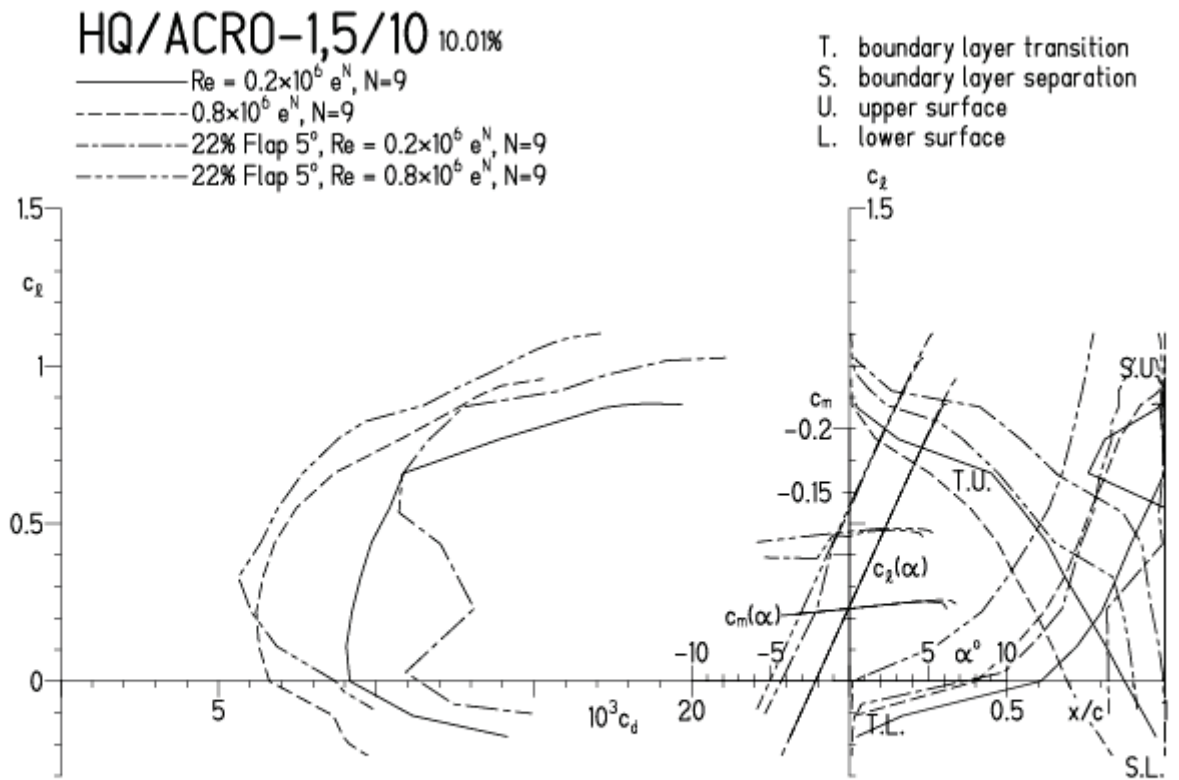


HQ/ACRO-1,5/10, N=9, mit 5° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:27

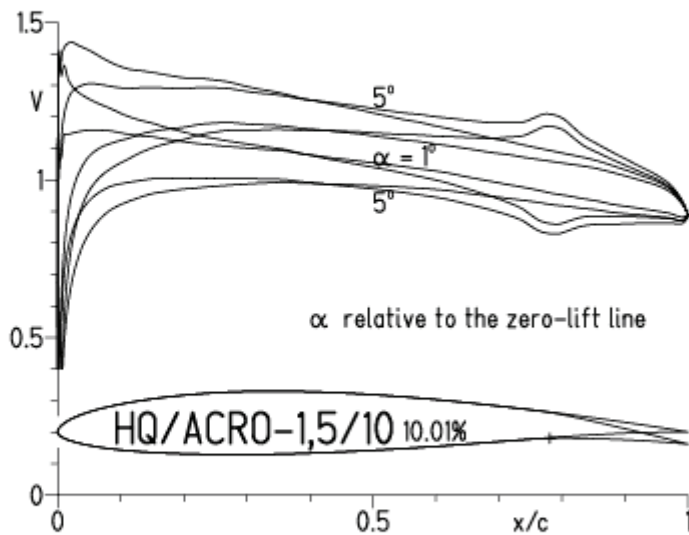


EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:27

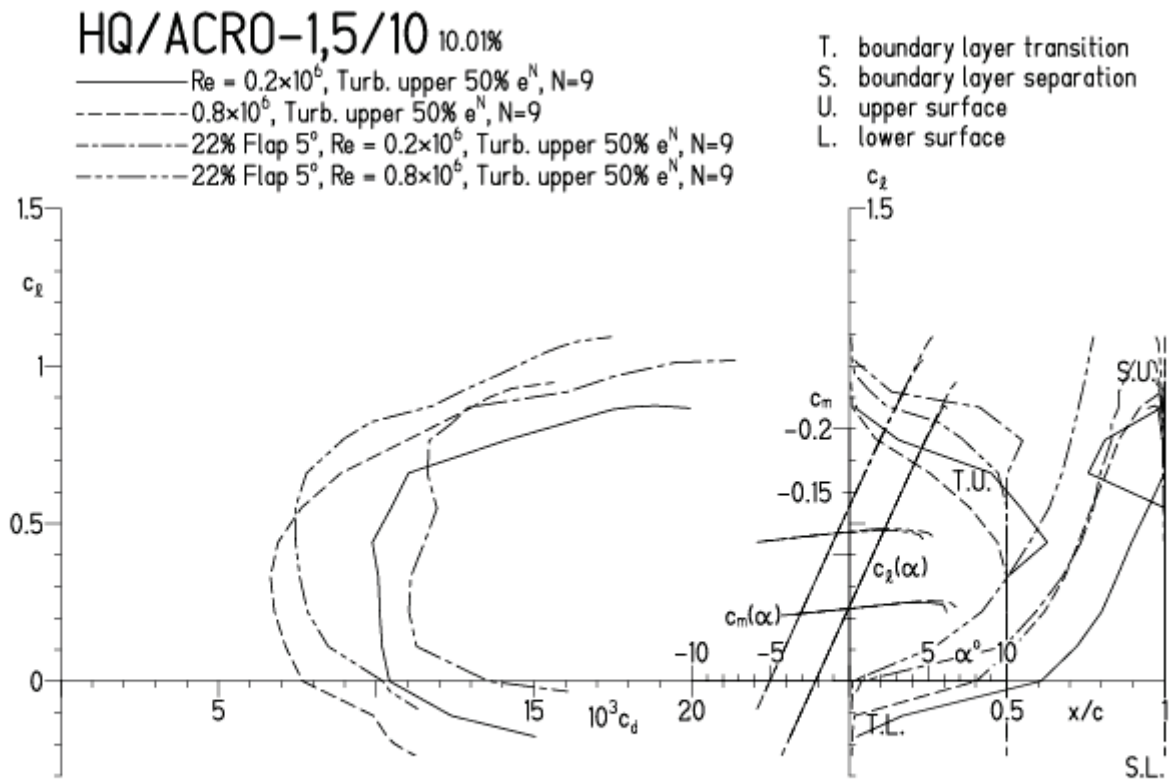


HQ/ACRO-1,5/10, N=9, mit 5° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:30

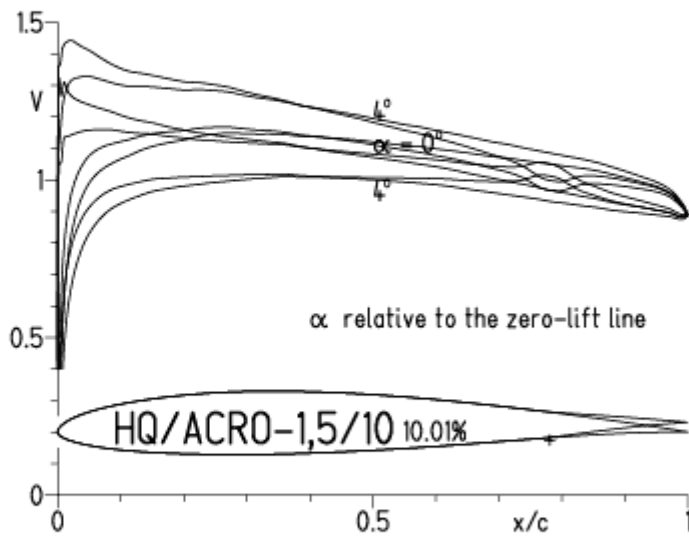


EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:30



HQ/ACRO-1,5/10, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:37

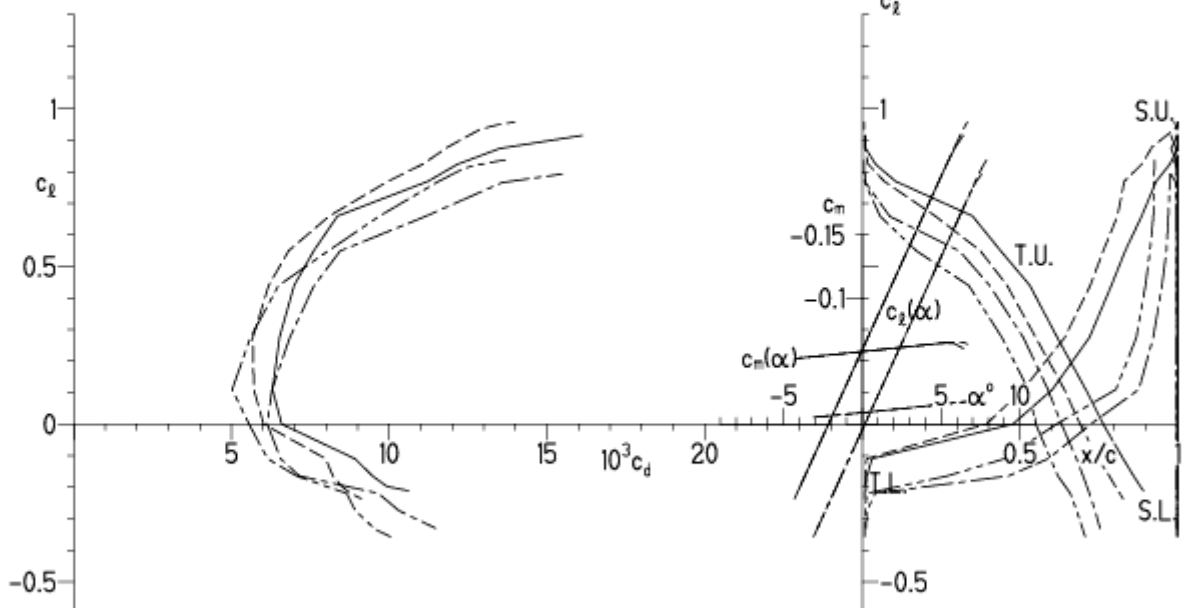


EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:37

HQ/ACRO-1,5/10 10.01%

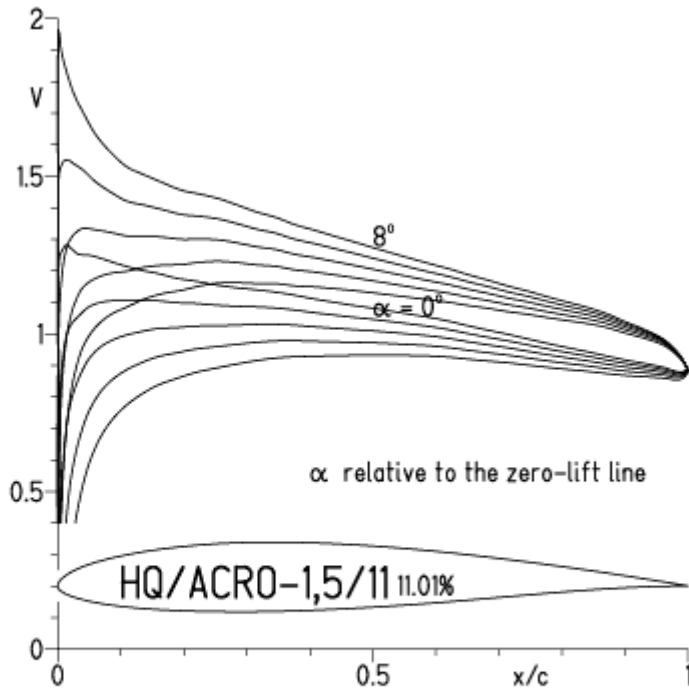
- $Re = 0.6 \times 10^6 e^N, N=11$
- - - $1.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 1.2 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1,5/11, N=11

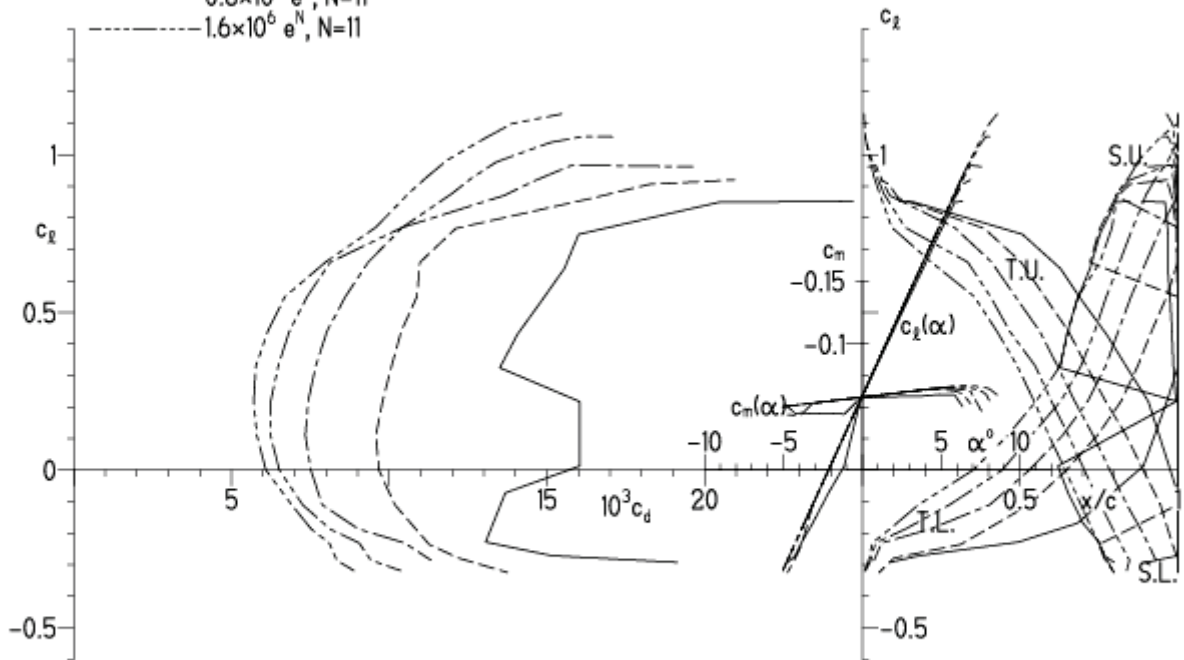
EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:43



EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:43

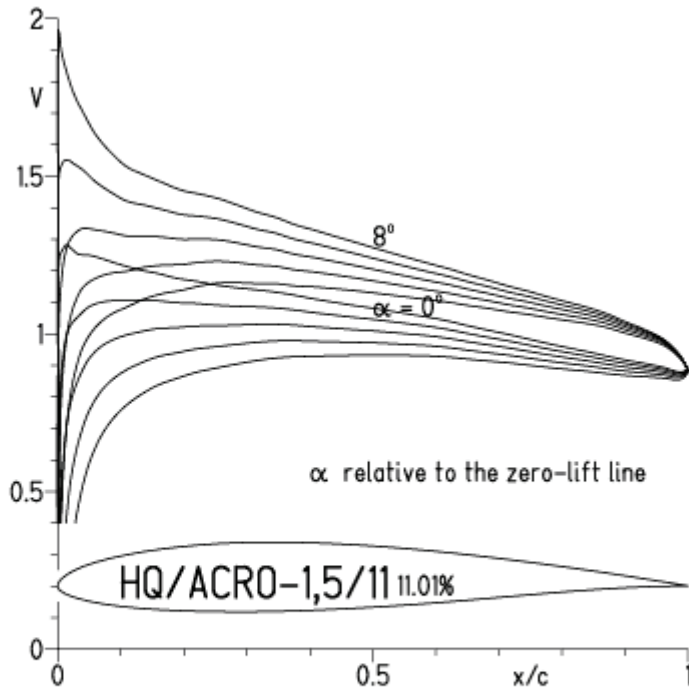
HQ/ACRO-1,5/11 11.01%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1,5/11, N=9

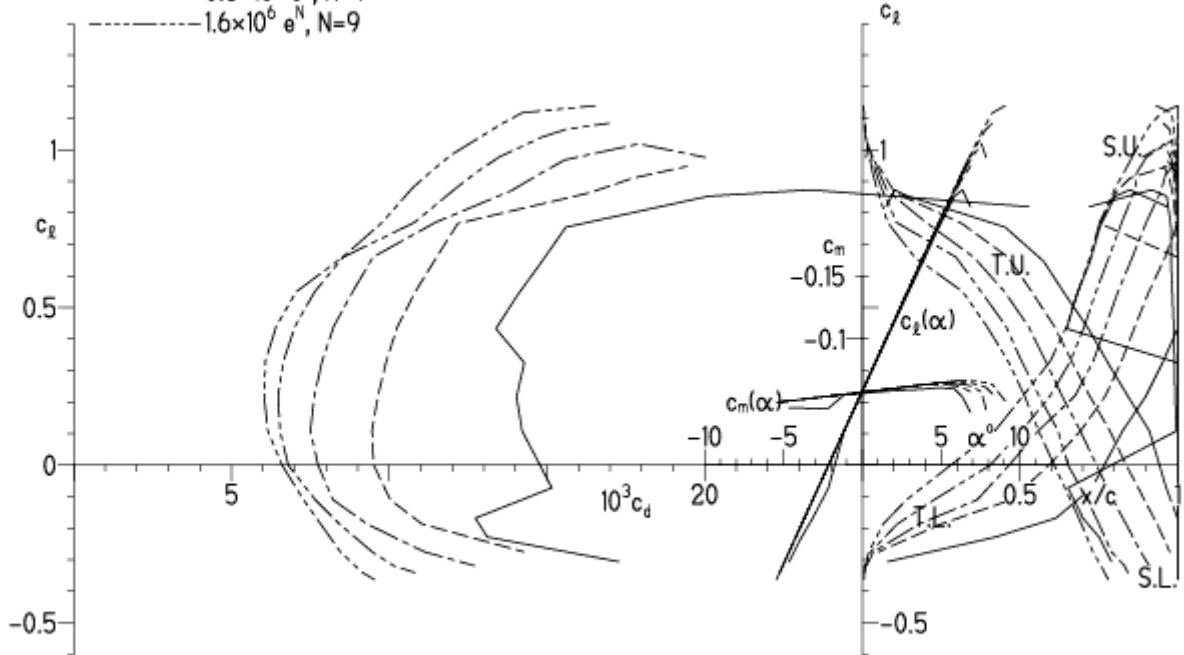
EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:48



EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:48

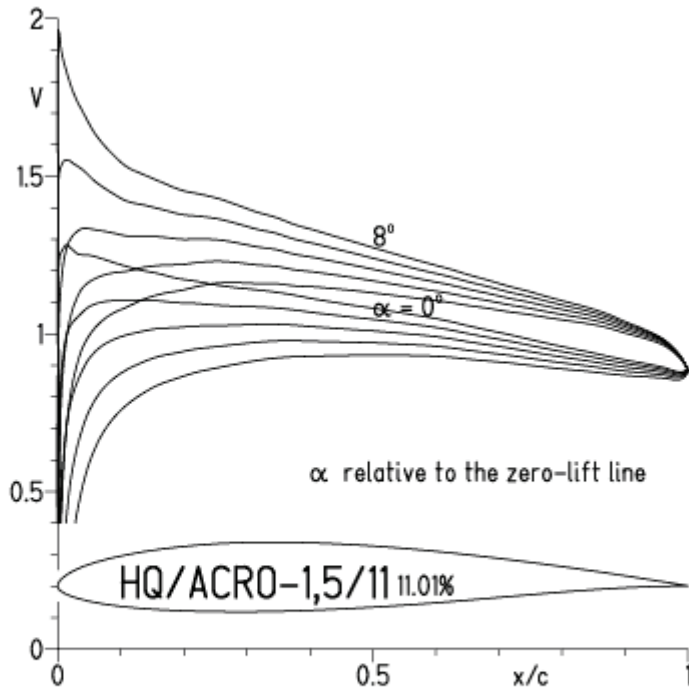
HQ/ACRO-1,5/11 11.01%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/ACRO-1,5/11, N=9, Turbulatoreffekt bei niedrigen Re-Zahlen
 (optimale Turbulatorposition bei 45 -55% der Profiltiefe)

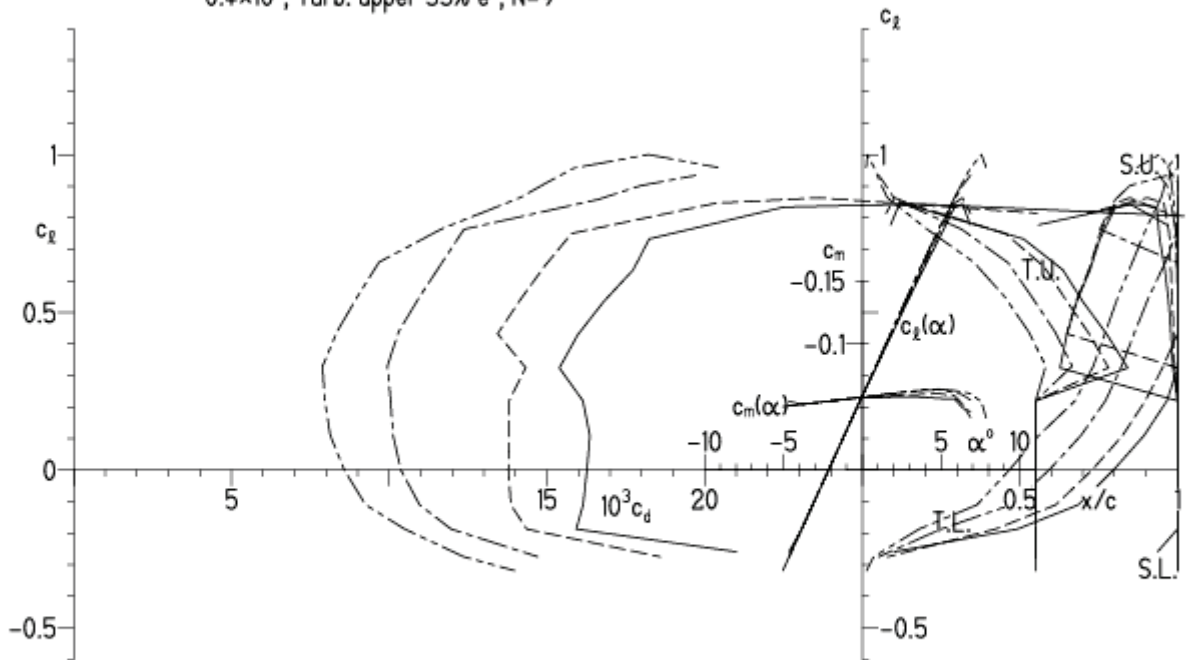
EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:53



EPPLER 2005 V. 8.5.07 RUN 20.3.12 17:53

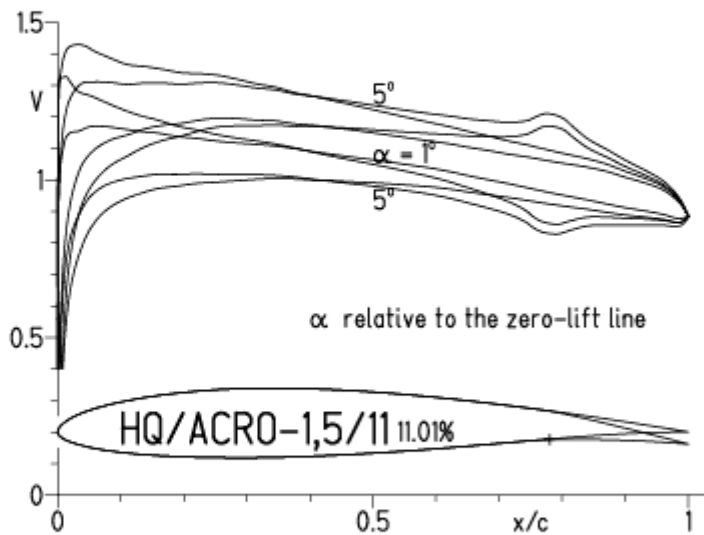
HQ/ACRO-1,5/11 11.01%

- $Re = 75\,000$, Turb. upper 55% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 55% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 55% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 55% e^N , $N=9$

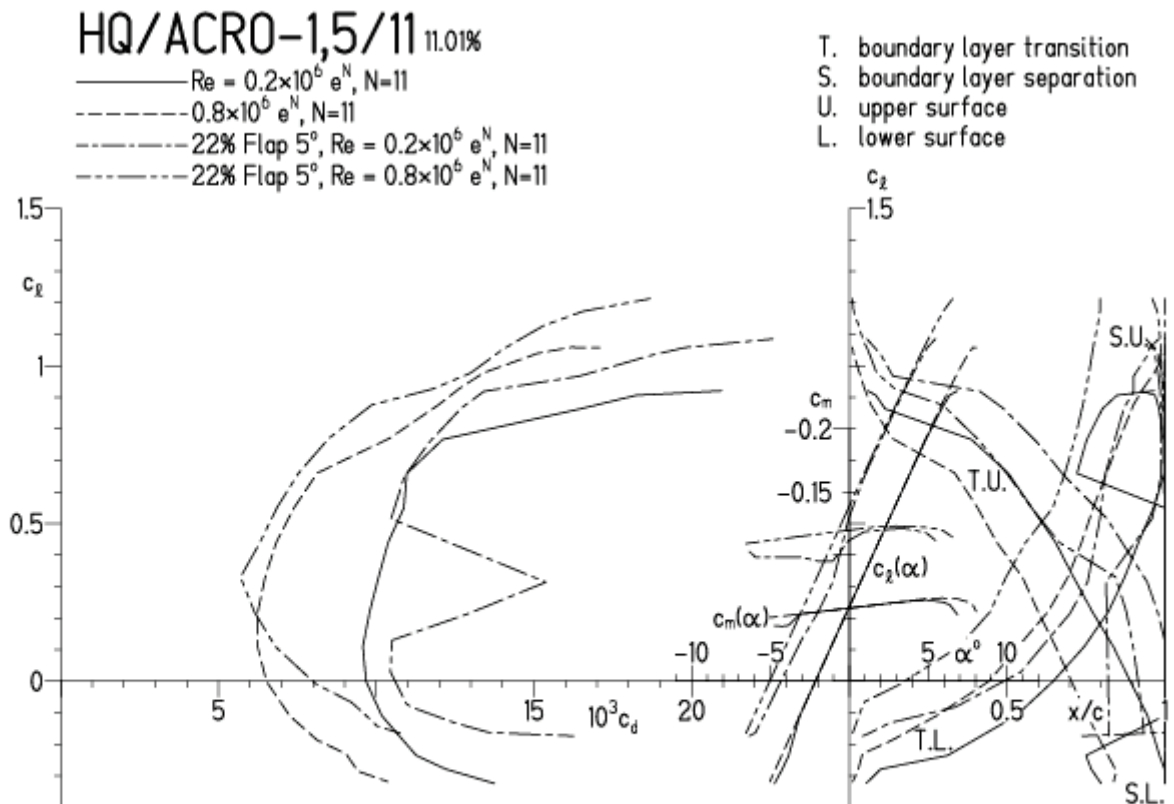


HQ/ACRO-1,5/11, N=11, mit 5° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:00

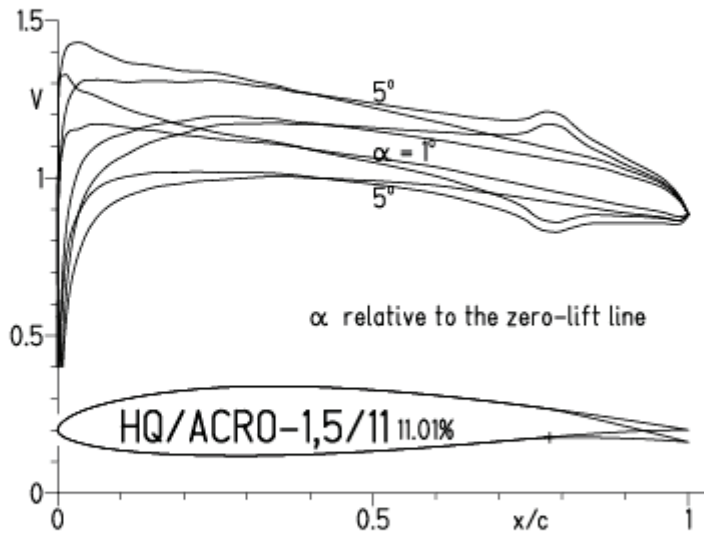


EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:00

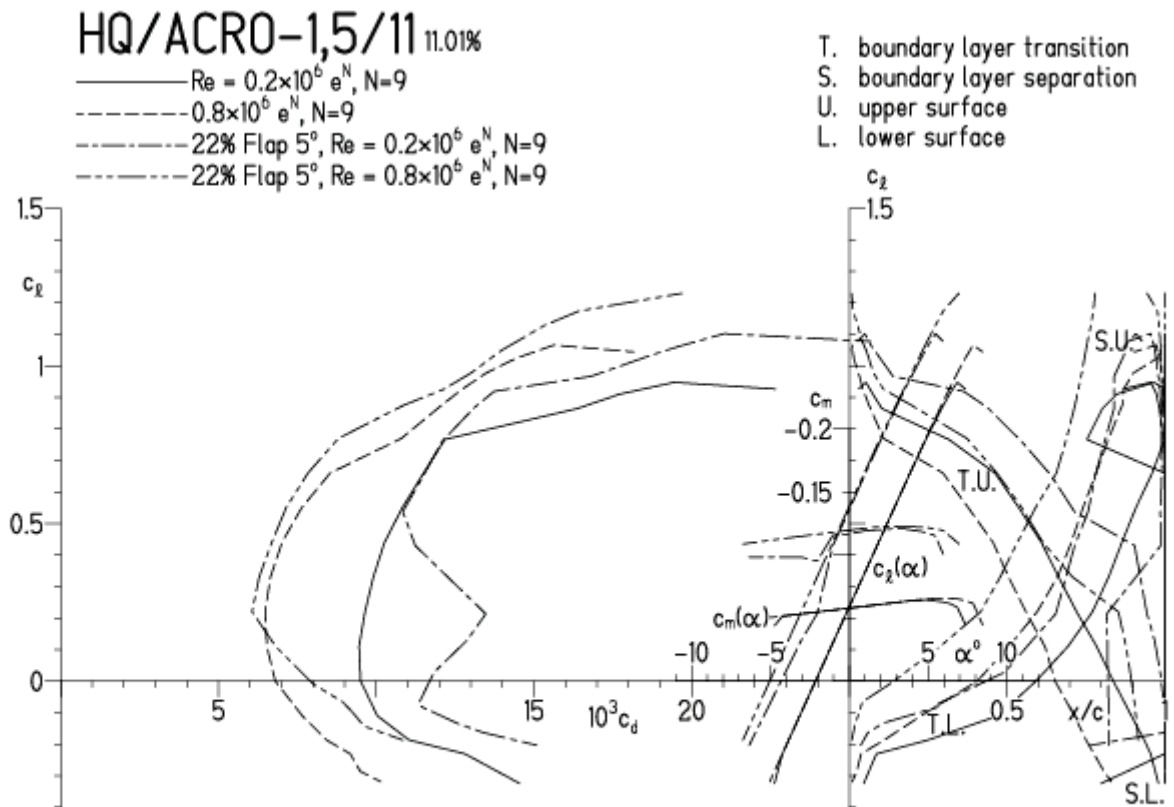


HQ/ACRO-1,5/11, N=9, mit 5° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:11

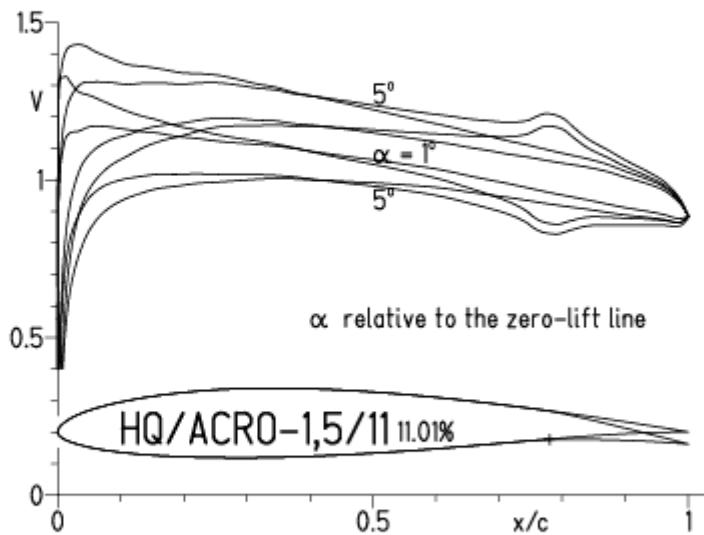


EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:11

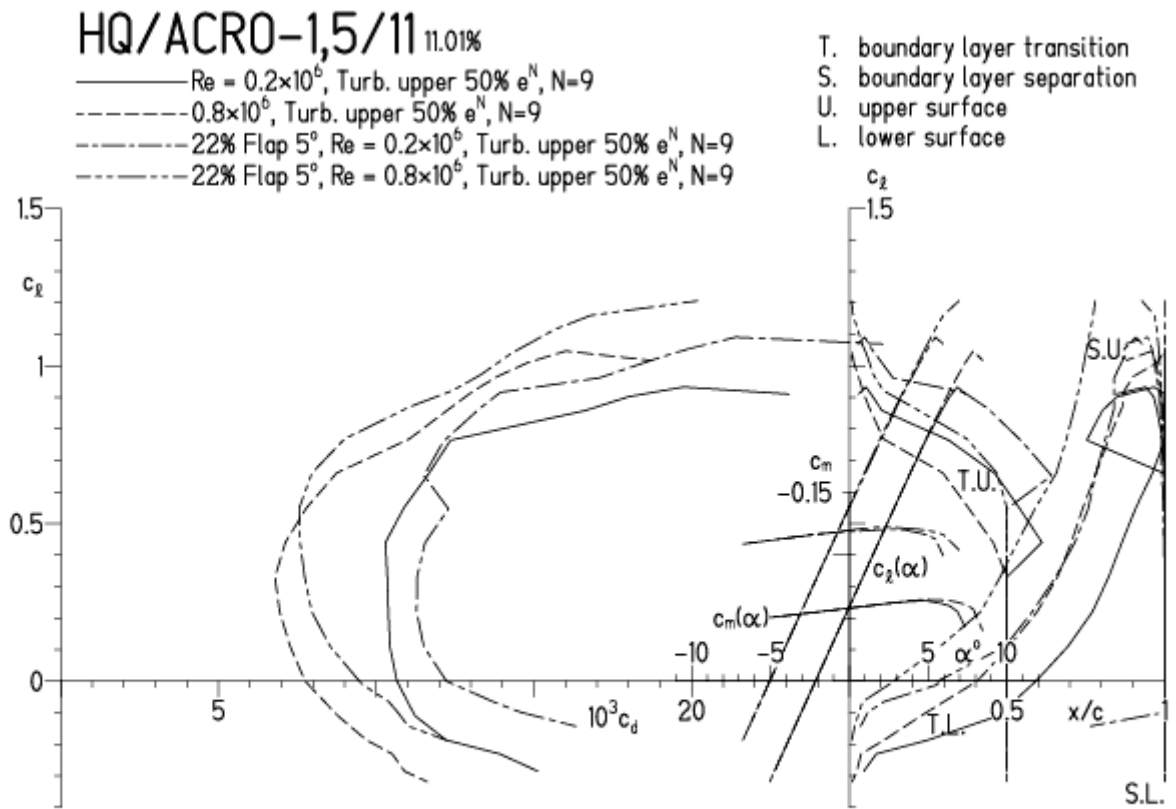


HQ/ACRO-1,5/11, N=9, mit 5° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:16

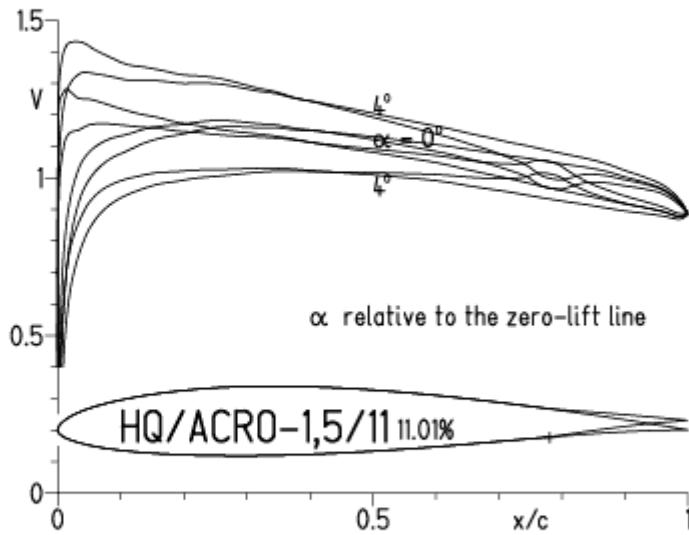


EPPLER 2005 V. 8.5.07 RUN 20.3.12 18



HQ/ACRO-1,5/11, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:24

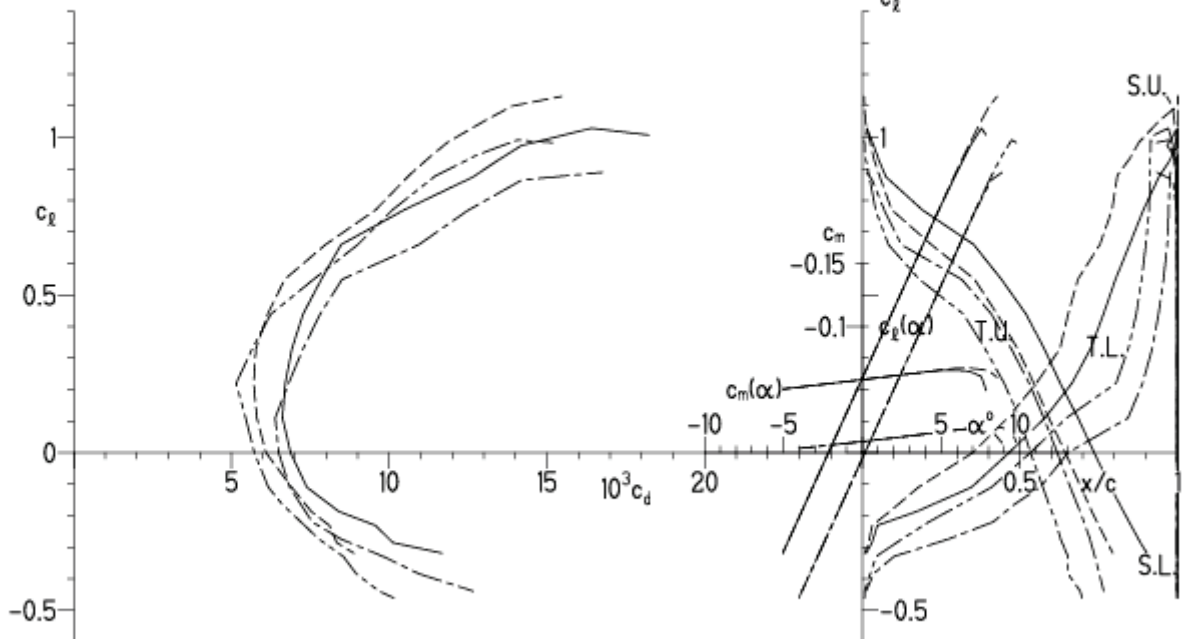


EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:24

HQ/ACRO-1,5/11 11.01%

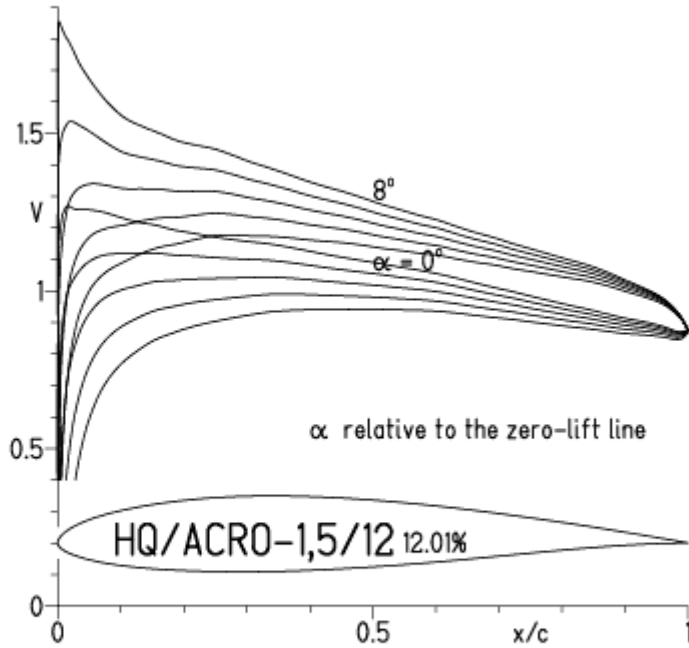
- $Re = 0.6 \times 10^6 e^N, N=11$
- - - $1.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 1.6 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1,5/12, N=11

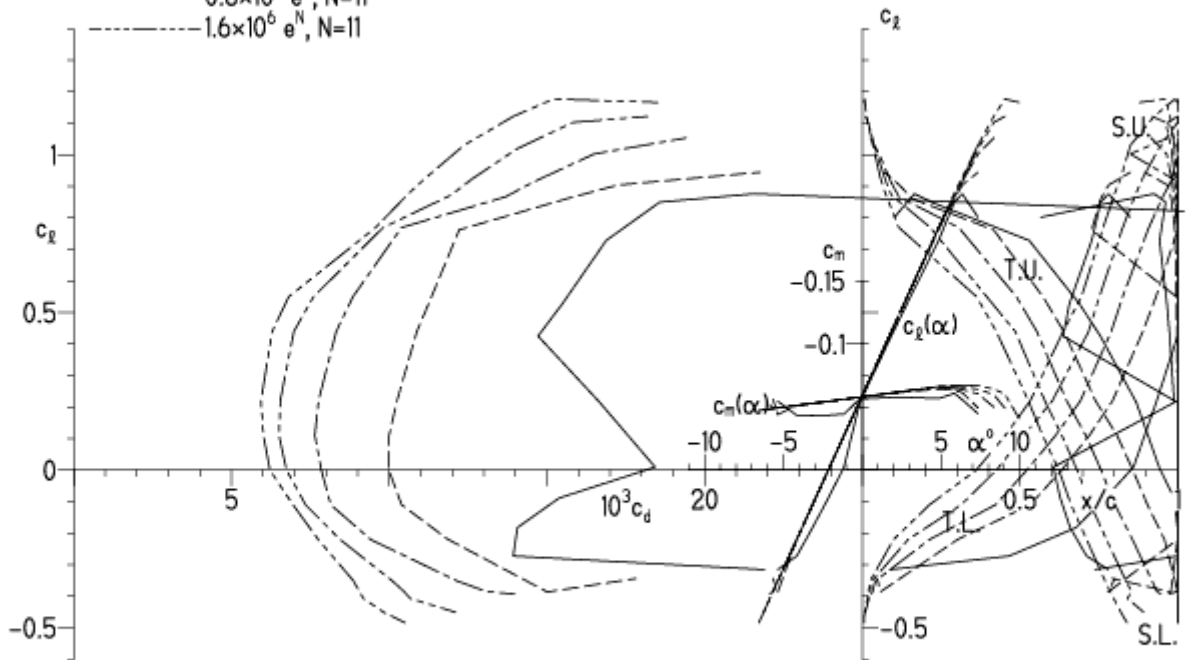
EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:33



EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:33

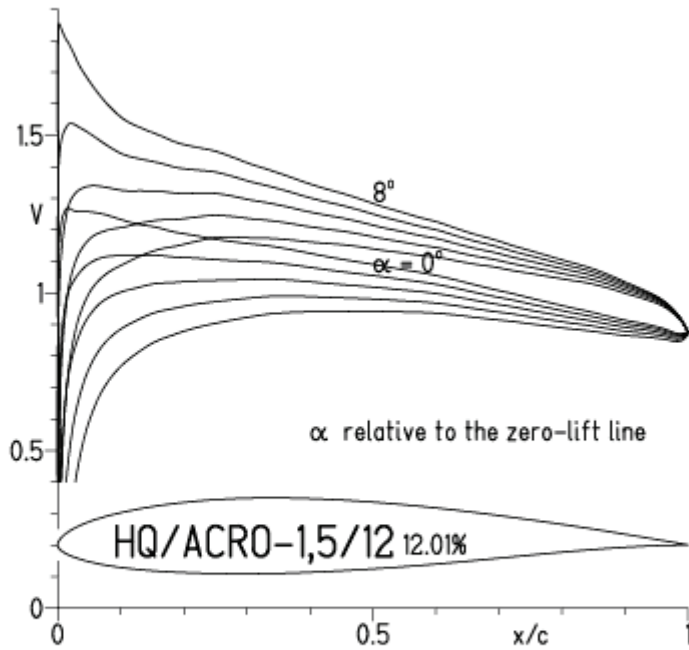
HQ/ACRO-1,5/12 12.01%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · · - $0.8 \times 10^6 e^N, N=11$
- · · · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1,5/12, N=9

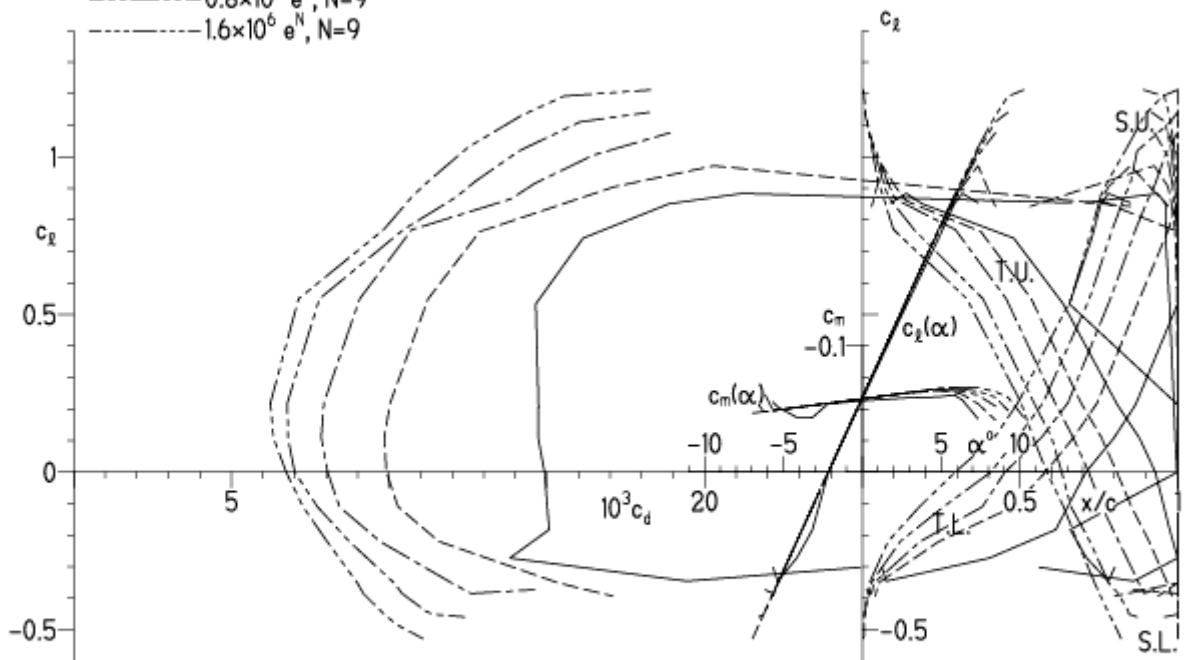
EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:36



EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:36

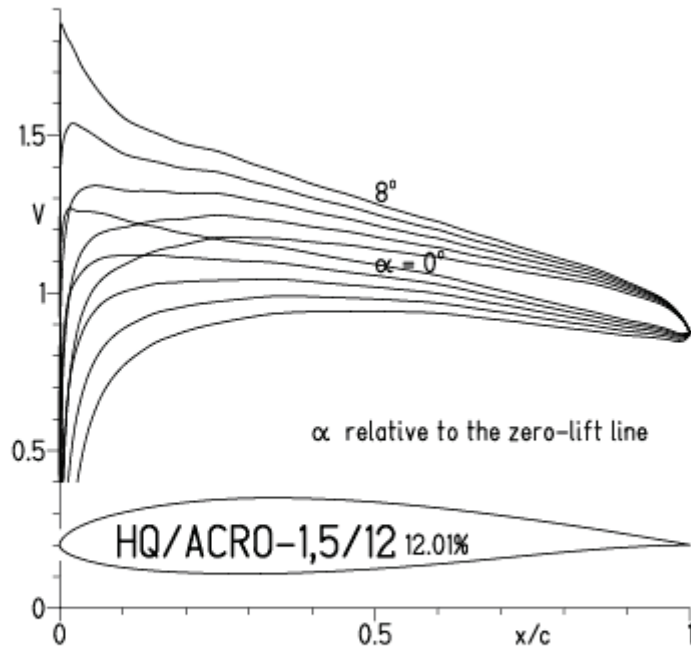
HQ/ACRO-1,5/12 12.01%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/ACRO-1,5/12, $N=9$, Turbulatoreffekt bei niedrigen Re-Zahlen
(optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

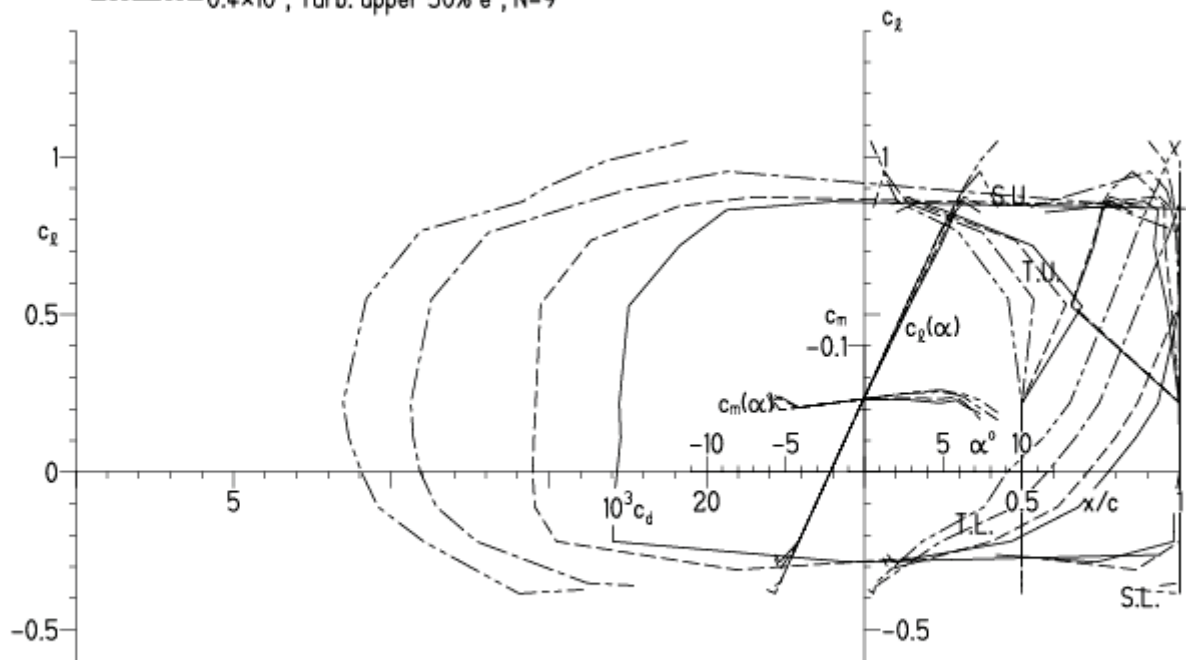
EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:42



EPPLER 2005 V. 8.5.07 RUN 20.3.12 18:42

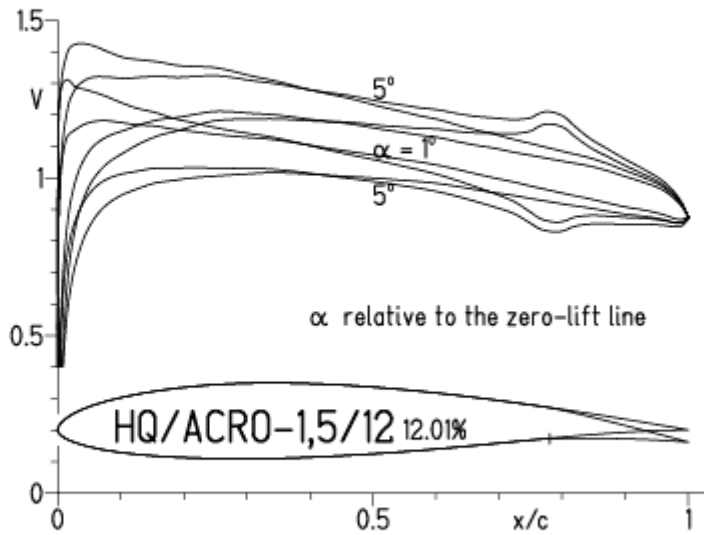
HQ/ACRO-1,5/12 12.01%

- $Re = 75\,000$, Turb. upper 50% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 50% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 50% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 50% e^N , $N=9$

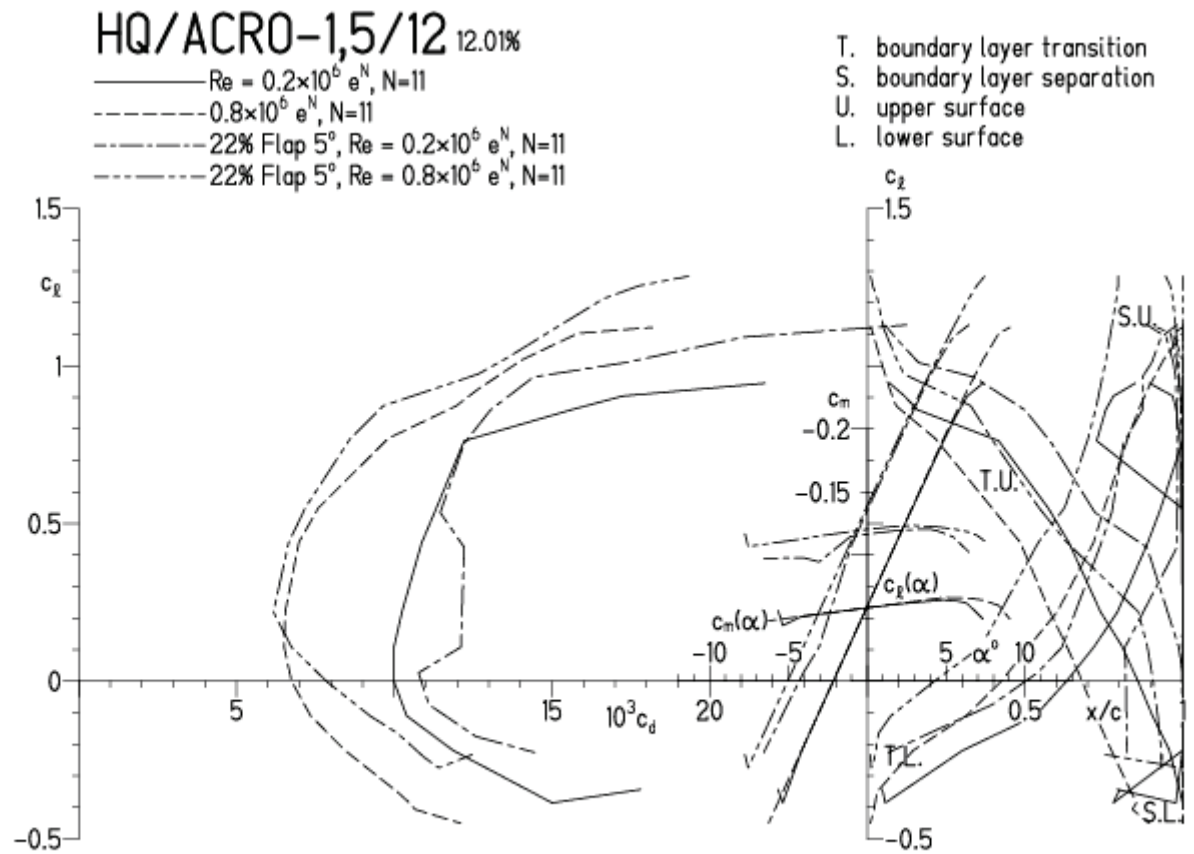


HQ/ACRO-1,5/12, N=11, mit 5° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.3.12 19:11

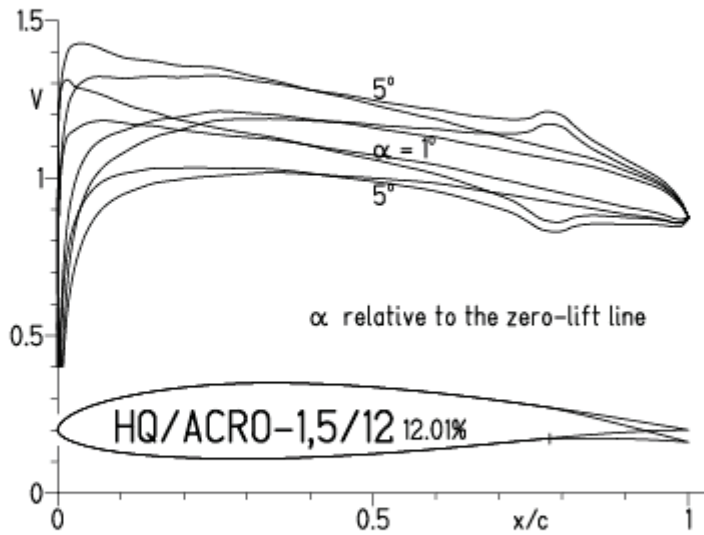


EPPLER 2005 V. 8.5.07 RUN 20.3.12 19:11

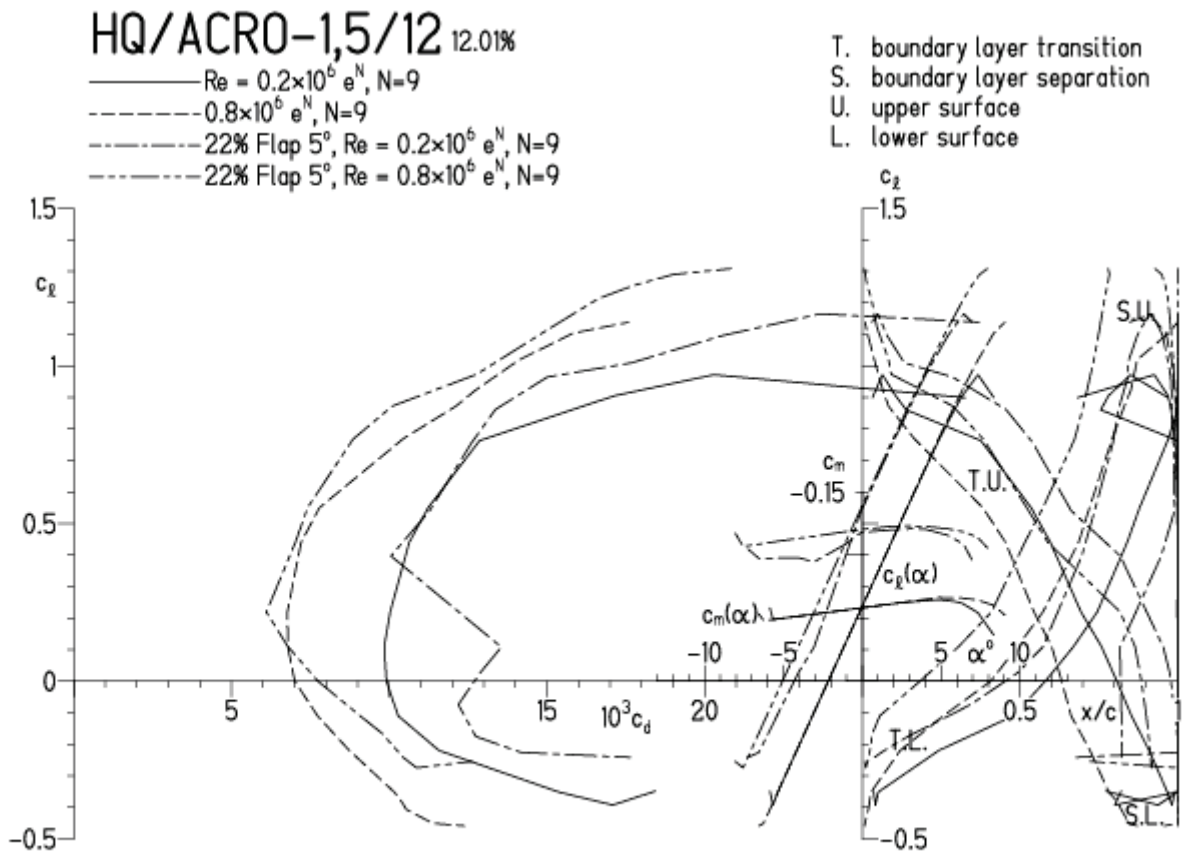


HQ/ACRO-1,5/12, N=9, mit 5° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.3.12 9:28

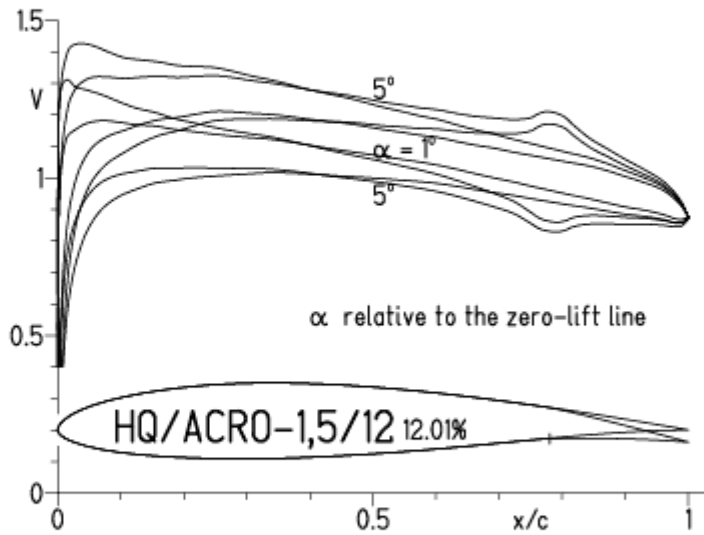


EPPLER 2005 V. 8.5.07 RUN 21

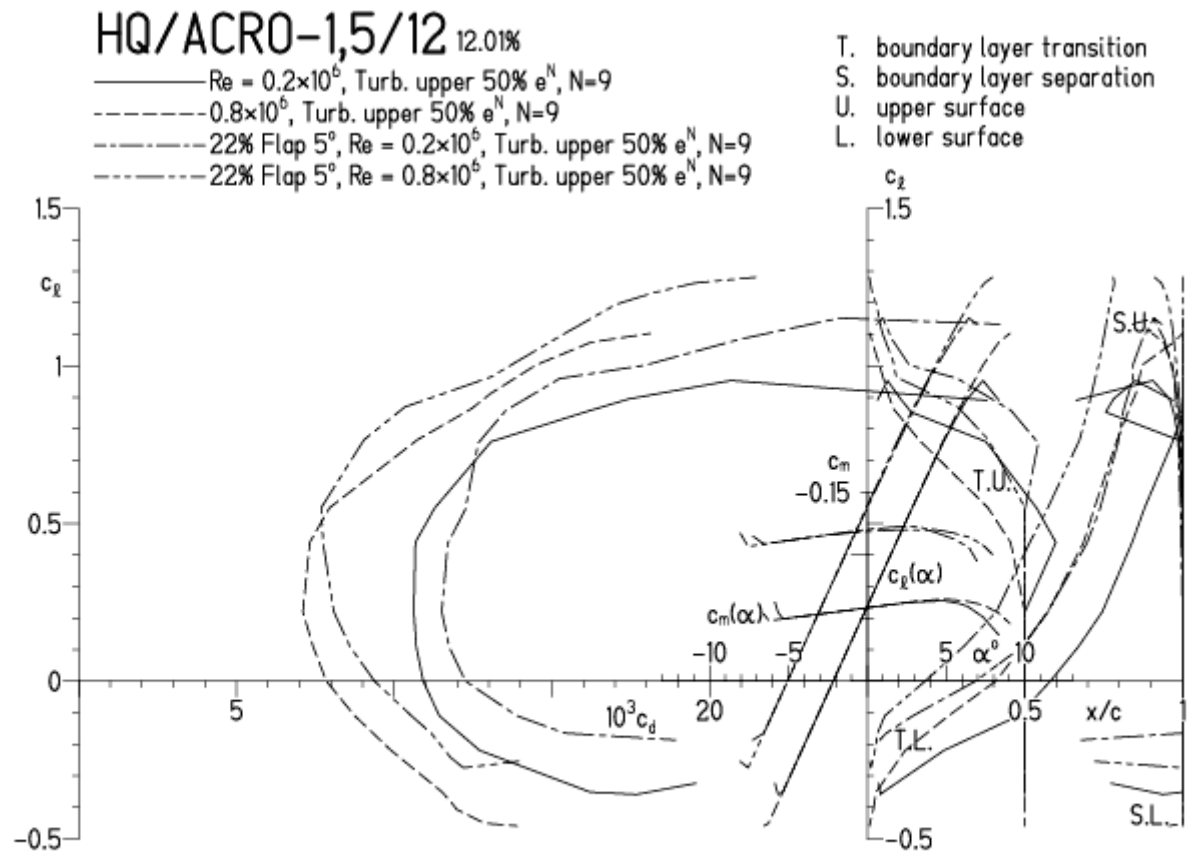


HQ/ACRO-1,5/12, N=9, mit 5° Wölbklappenausschlag, Turbulatoreffekt
 (optimale Turbulatorposition bei 45 - 55 % der Profiltiefe)

EPPLER 2005 V. 8.5.07 RUN 21.3.12 9:31

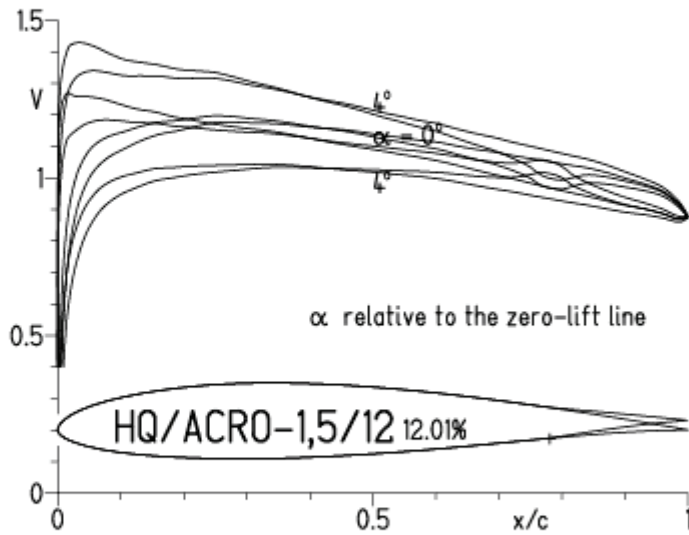


EPPLER 2005 V. 8.5.07 RUN 21.3.12 9:31



HQ/ACRO-1,5/12, N=11, mit -4° Wölbklappenausschlag (Schnellflug)

EPPLER 2005 V. 8.5.07 RUN 21.3.12 9:40

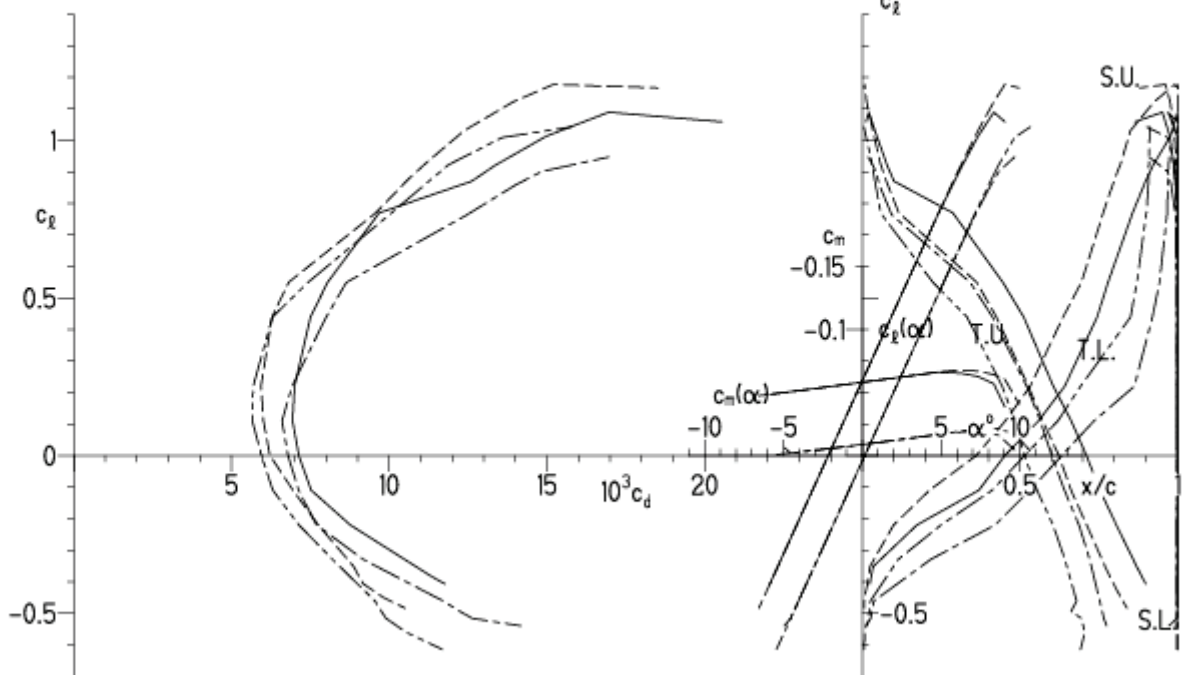


EPPLER 2005 V. 8.5.07 RUN 21.3.12 9:40

HQ/ACRO-1,5/12 12.01%

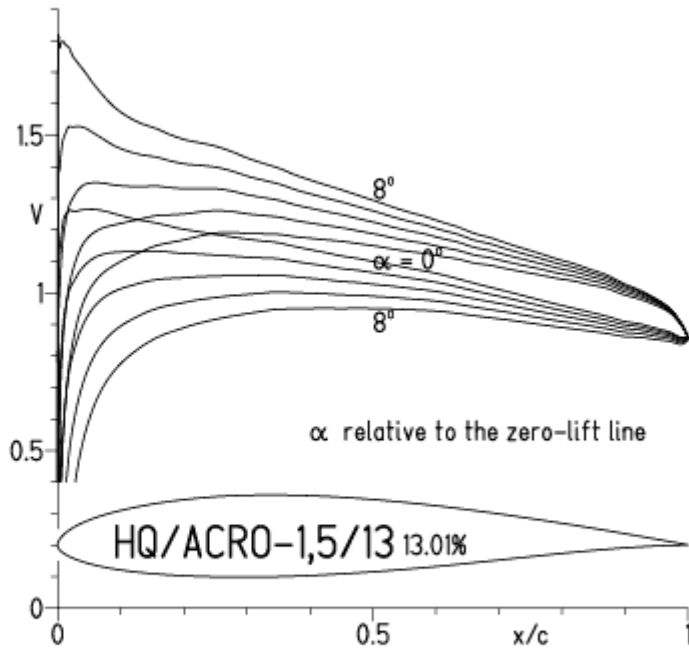
- $Re = 0.6 \times 10^6 e^N$, N=11
- - - $1.6 \times 10^6 e^N$, N=11
- · - · 22% Flap -4° , $Re = 0.6 \times 10^6 e^N$, N=11
- · - · 22% Flap -4° , $Re = 1.6 \times 10^6 e^N$, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/ACRO-1,5/13, N=11

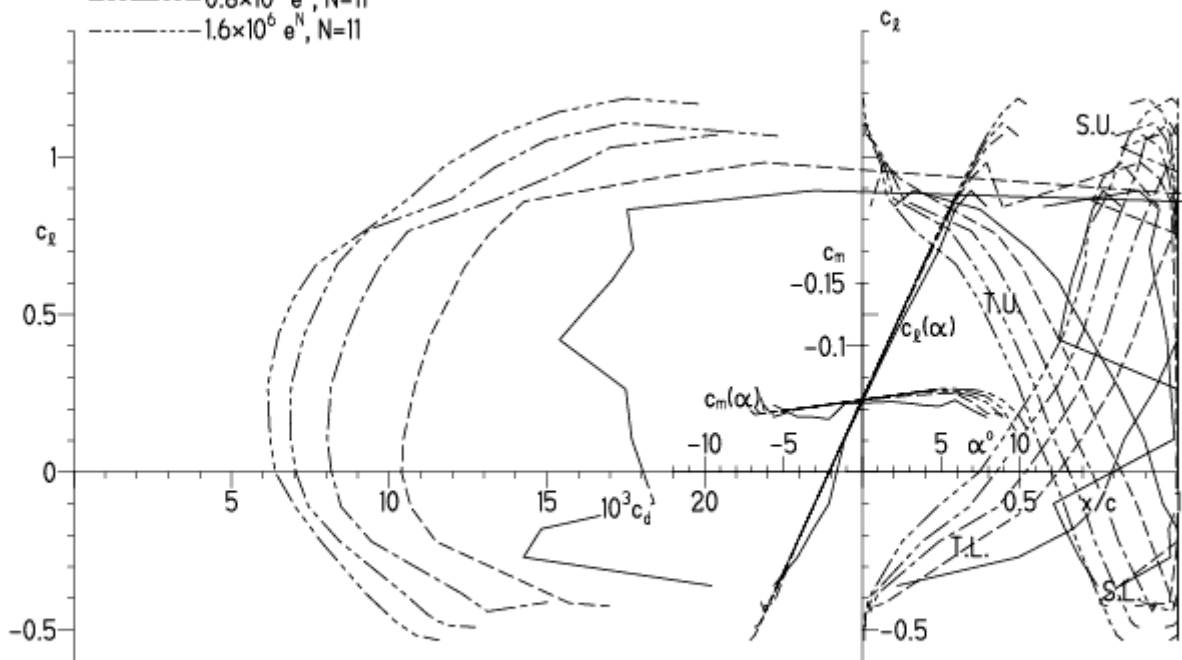
EPPLER 2005 V. 8.5.07 RUN 21.3.12 9:45



EPPLER 2005 V. 8.5.07 RUN 21.3.12 9:45

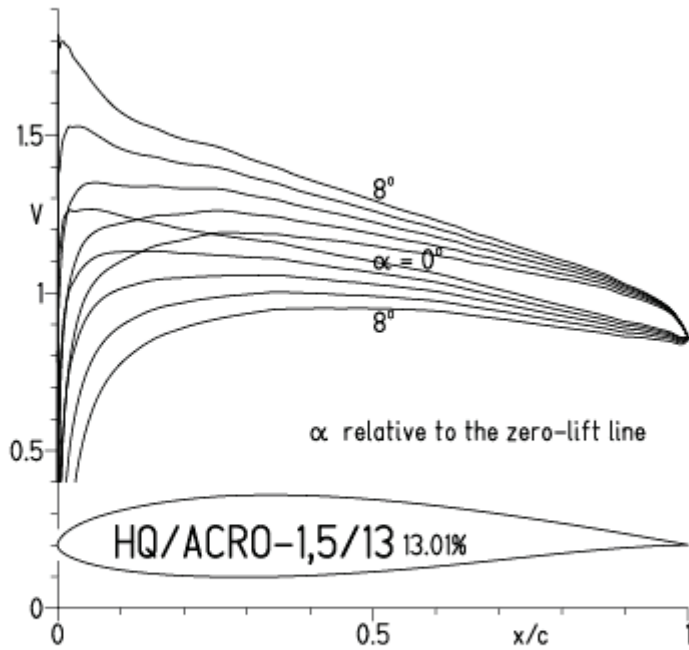
HQ/ACRO-1,5/13 13.01%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · · - $0.8 \times 10^6 e^N, N=11$
- · · · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1,5/13, N=9

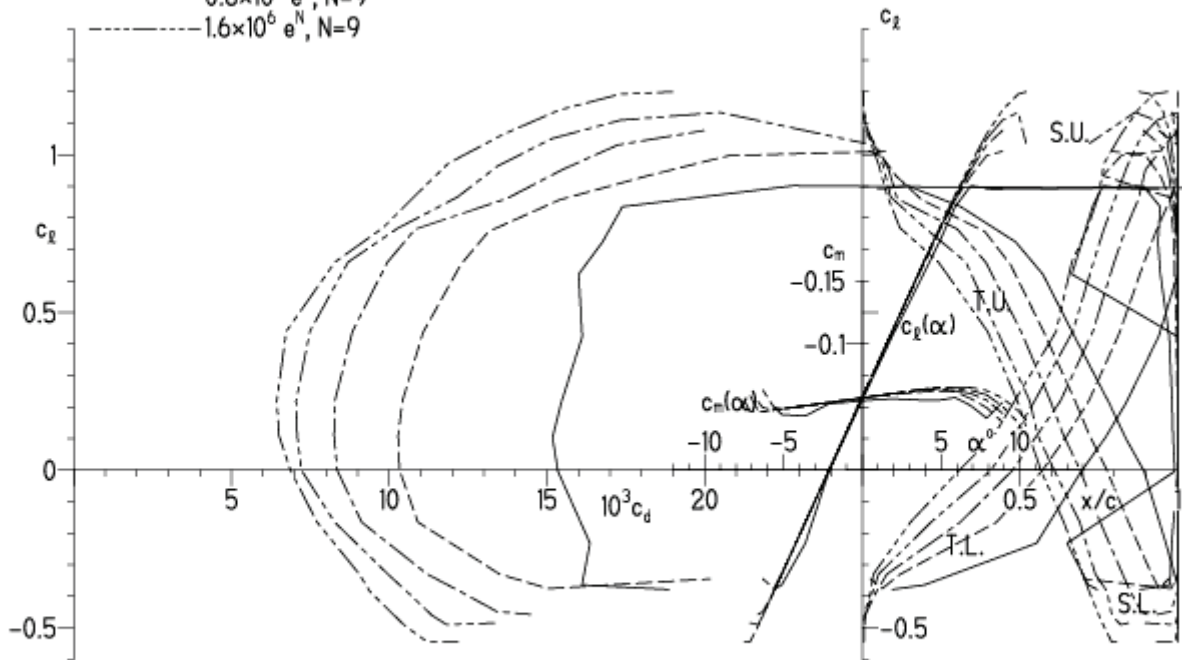
EPPLER 2005 V. 8.5.07 RUN 21.3.12 10:22



EPPLER 2005 V. 8.5.07 RUN 21.3.12 10:22

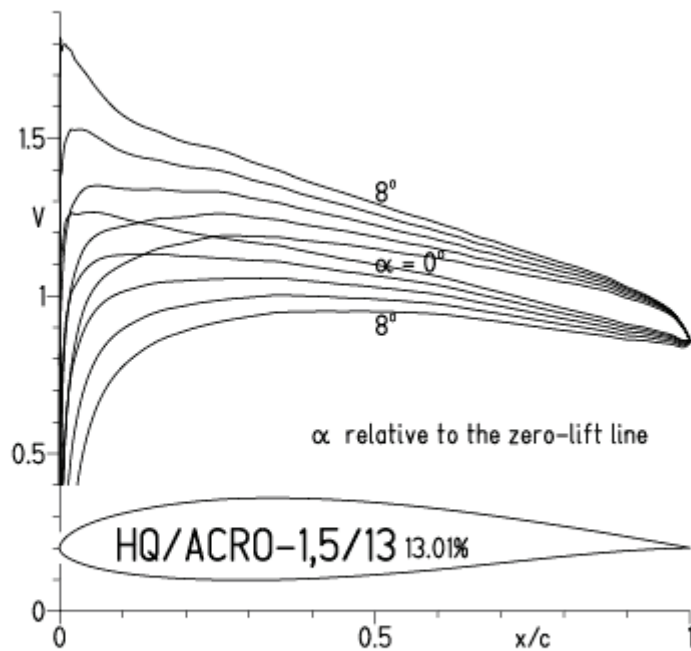
HQ/ACRO-1,5/13 13.01%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · · - $0.8 \times 10^6 e^N, N=9$
- · · · - $1.6 \times 10^6 e^N, N=9$



HQ/ACRO-1,5/13, N=9, Turbulatoreffekt bei niedrigen Re-Zahlen

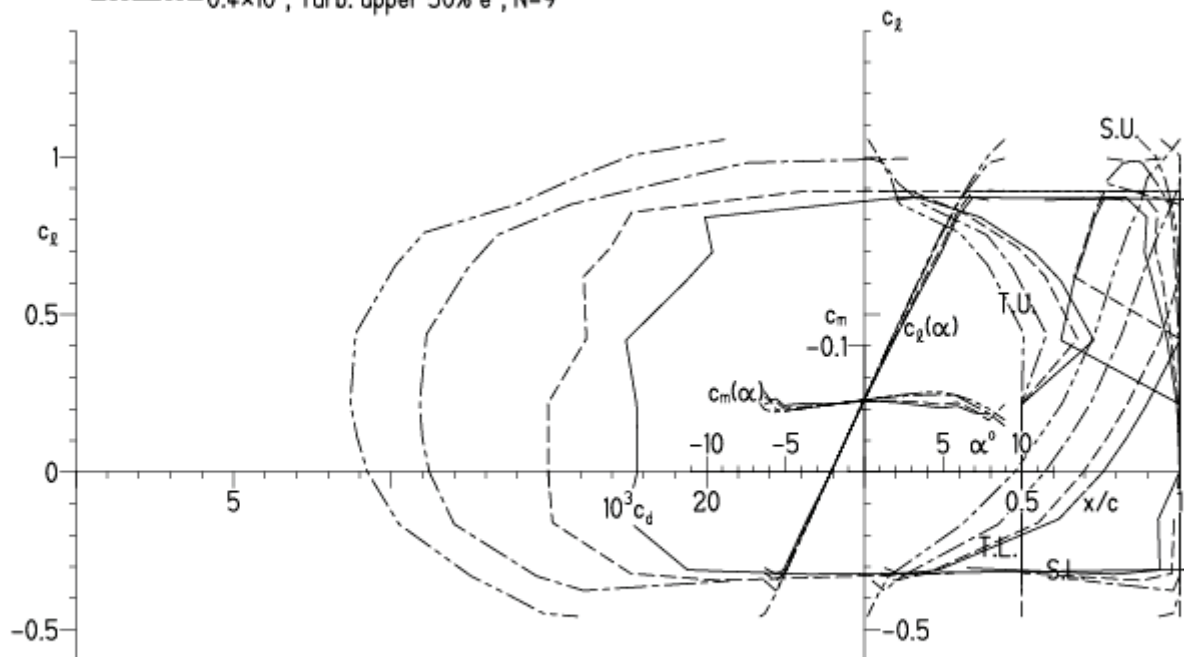
EPPLER 2005 V. 8.5.07 RUN 21.3.12 10:28



EPPLER 2005 V. 8.5.07 RUN 21.3.12 10:28

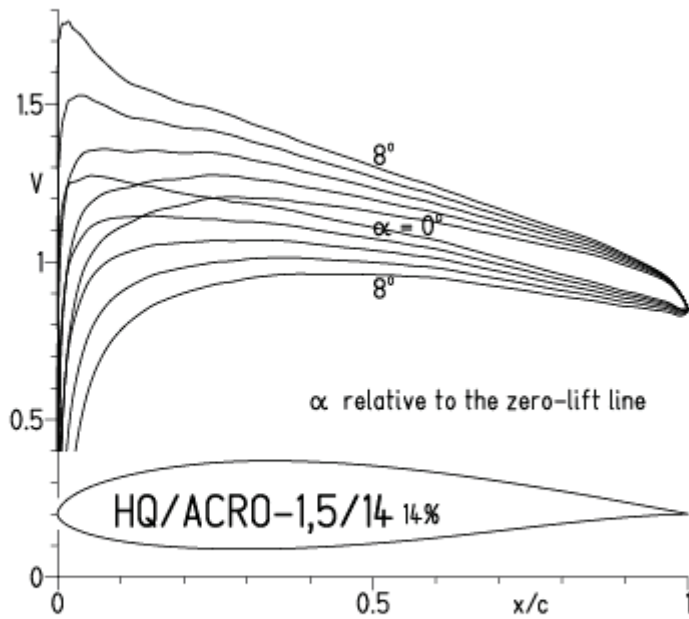
HQ/ACRO-1,5/13 13.01%

- $Re = 75\,000$, Turb. upper 50% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 50% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 50% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 50% e^N , $N=9$



HQ/ACRO-1,5/14, N=11

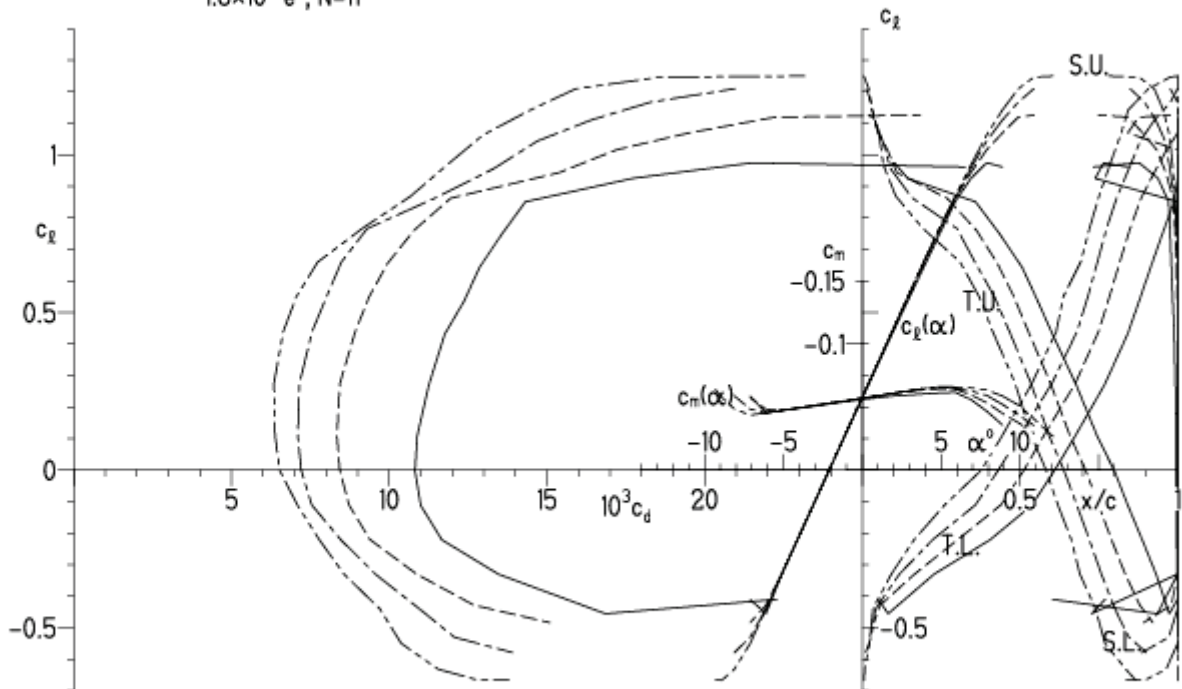
EPPLER 2005 V. 8.5.07 RUN 21.3.12 10:43



EPPLER 2005 V. 8.5.07 RUN 21.3.12 10:43

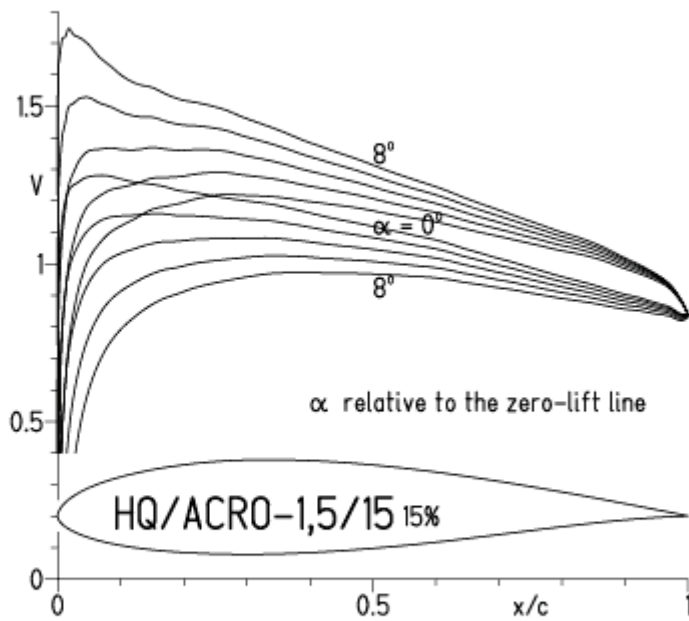
HQ/ACRO-1,5/14 14%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$
- · - $0.8 \times 10^6 e^N, N=11$
- - - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1,5/15, N=11

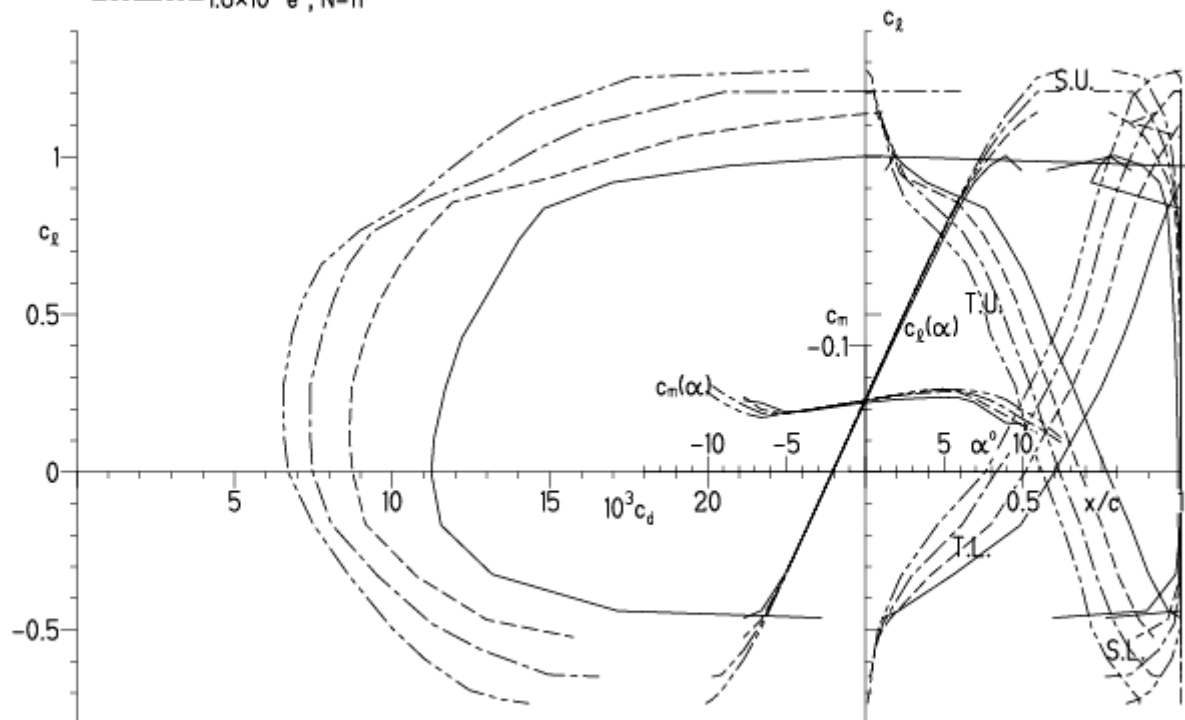
EPPLER 2005 V. 8.5.07 RUN 21.3.12 10:56



EPPLER 2005 V. 8.5.07 RUN 21.3.12 10:56

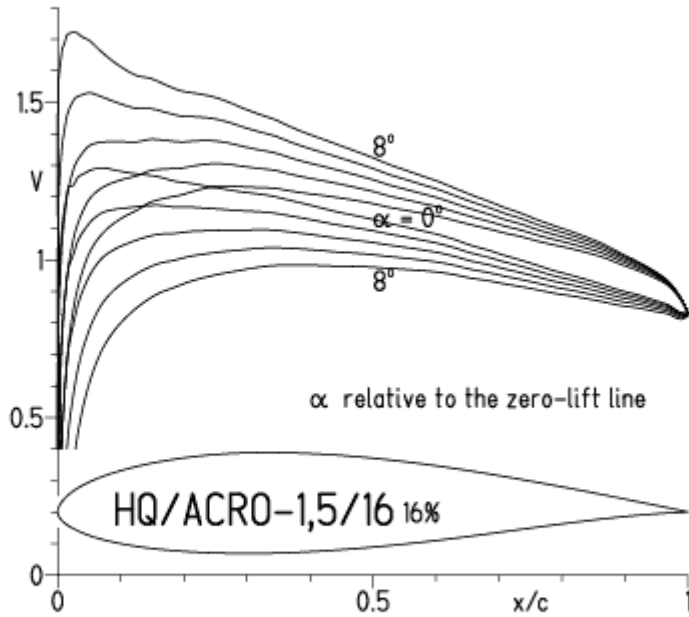
HQ/ACRO-1,5/15 15%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$
- · - $0.8 \times 10^6 e^N, N=11$
- · · - $1.6 \times 10^6 e^N, N=11$



HQ/ACRO-1,5/16, N=11

EPPLER 2005 V. 8.5.07 RUN 21.3.12 11:01



EPPLER 2005 V. 8.5.07 RUN 21.3.12 11:01

HQ/ACRO-1,5/16 16%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$
- $0.8 \times 10^6 e^N, N=11$
- - - $1.6 \times 10^6 e^N, N=11$

