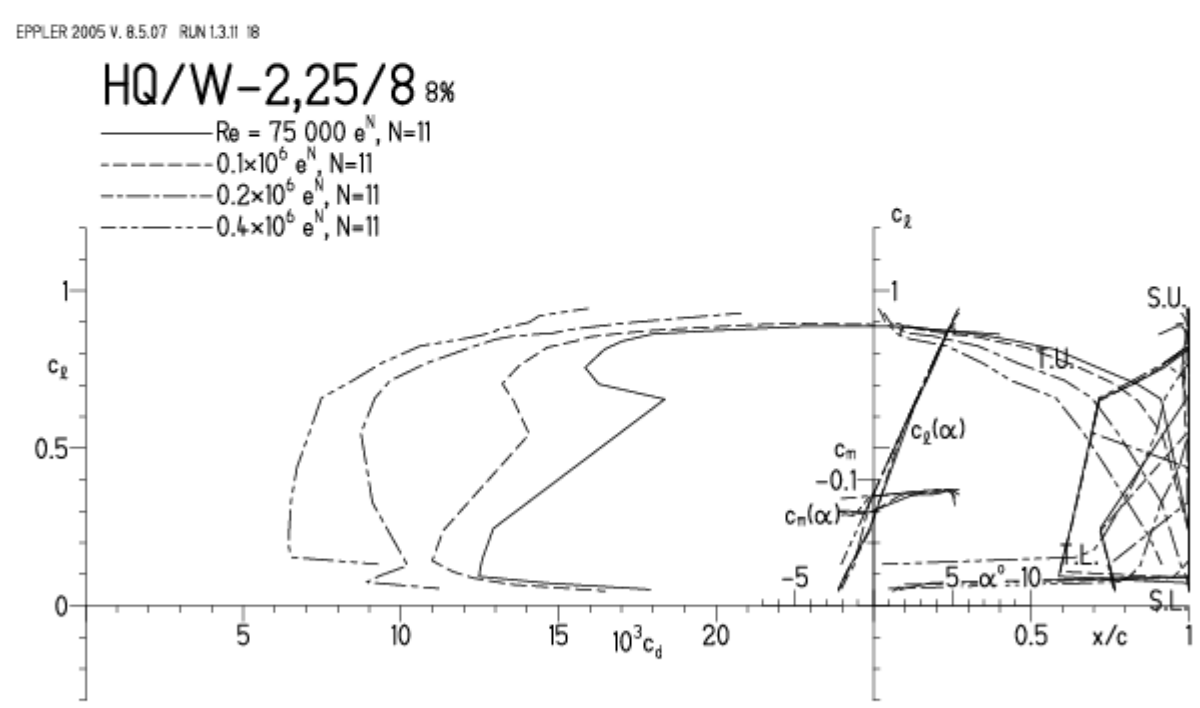
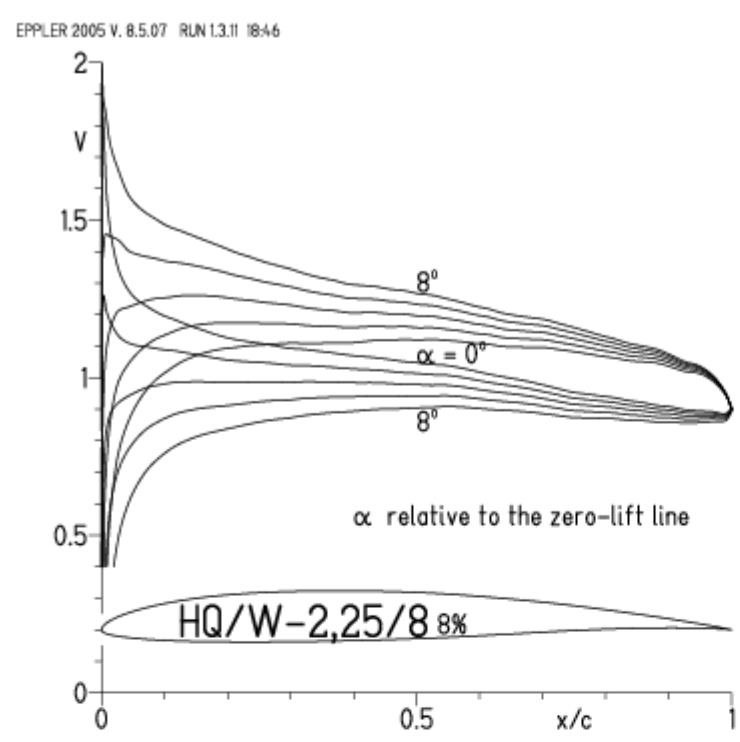


HQ/W-2,25/8, N=11



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2,25/8,5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

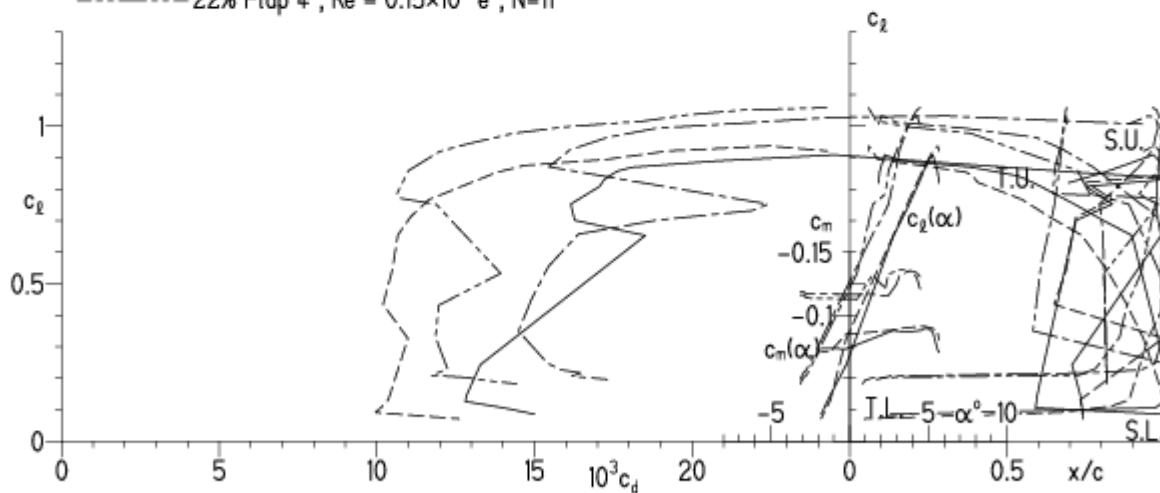


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

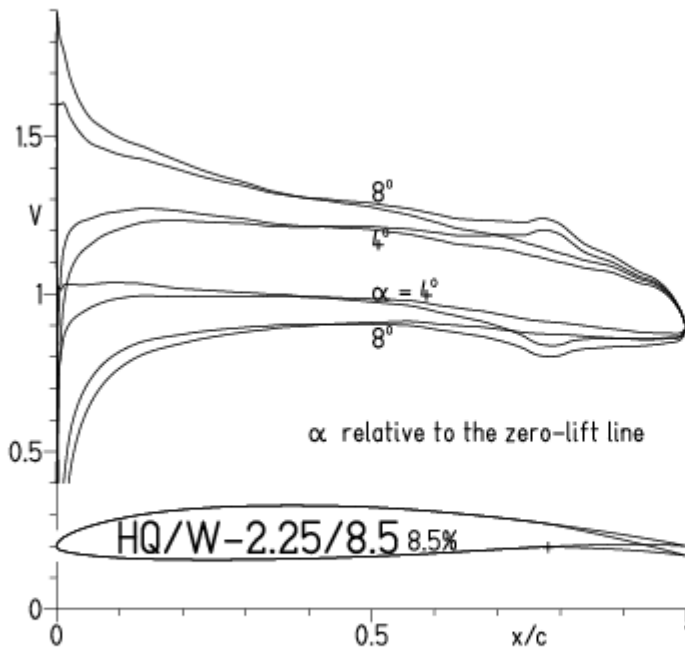
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

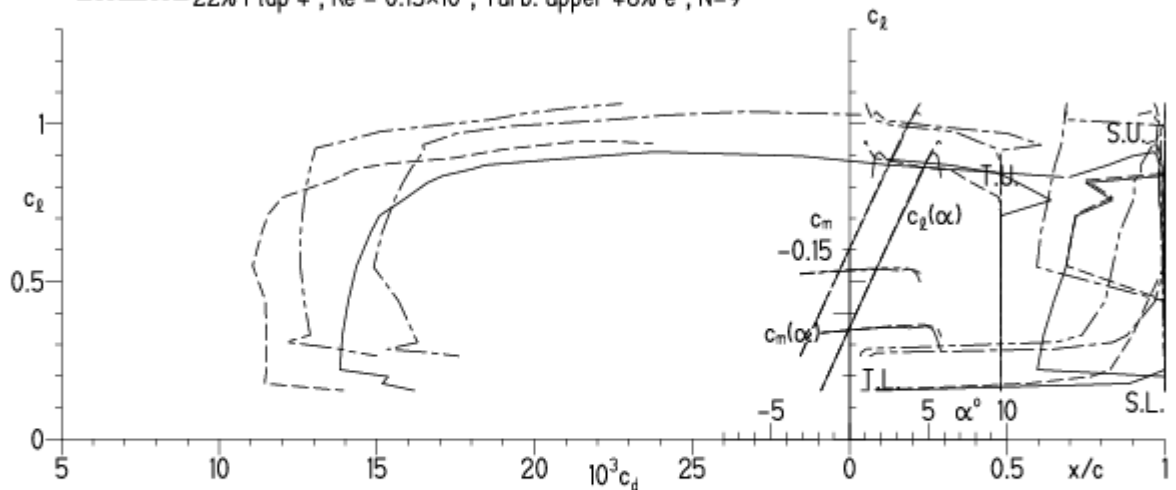


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

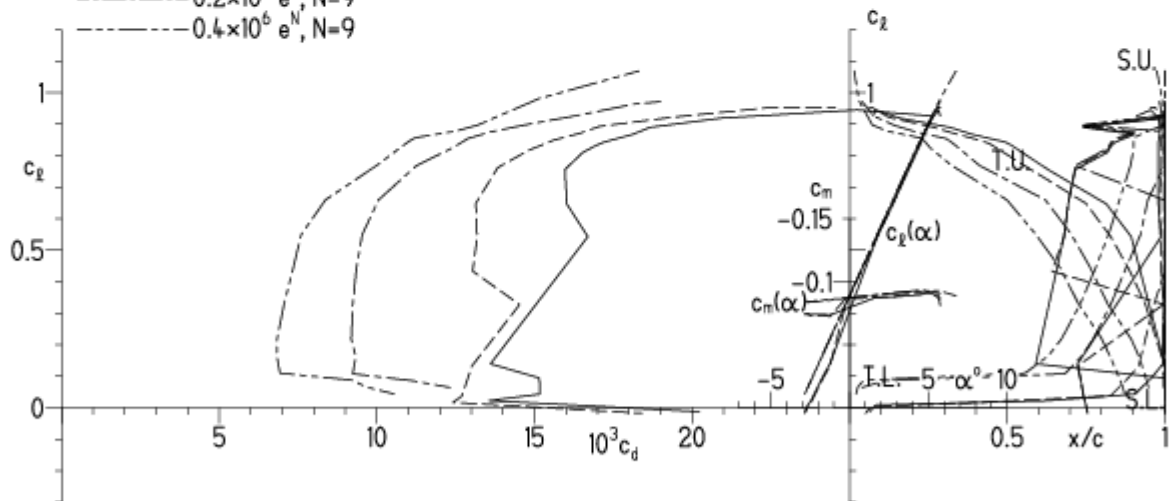
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17

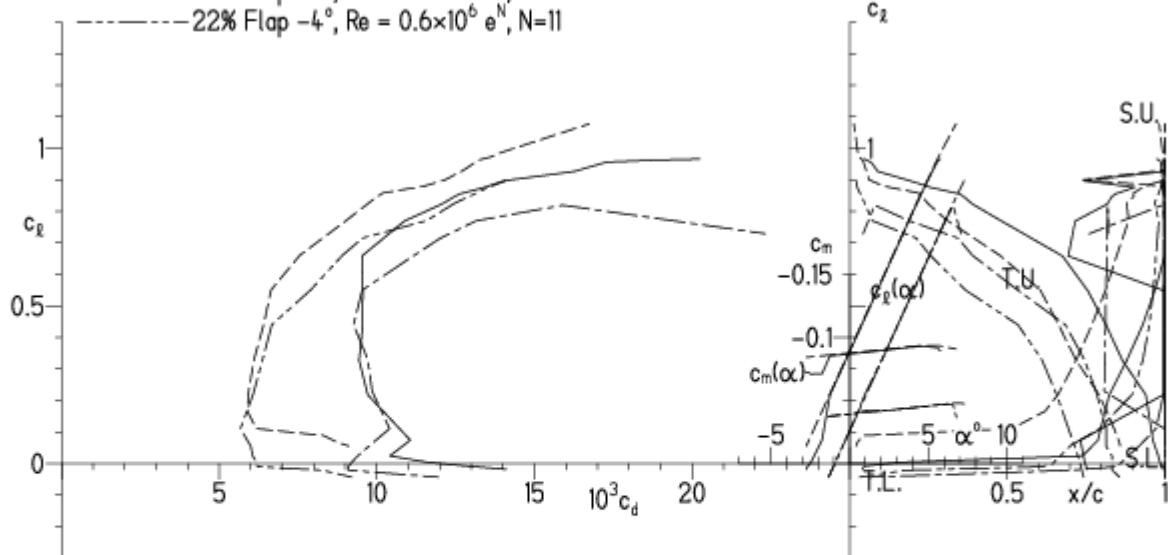


EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

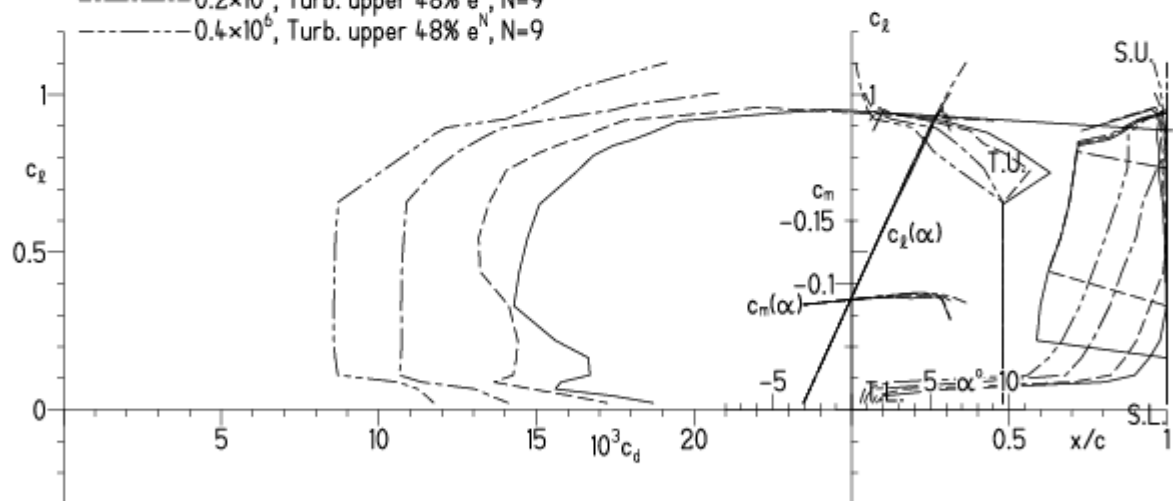
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N$, $N=11$
- - - $0.15 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap 4° , $Re = 75\,000 e^N$, $N=11$
- · - · - 22% Flap 4° , $Re = 0.15 \times 10^6 e^N$, $N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

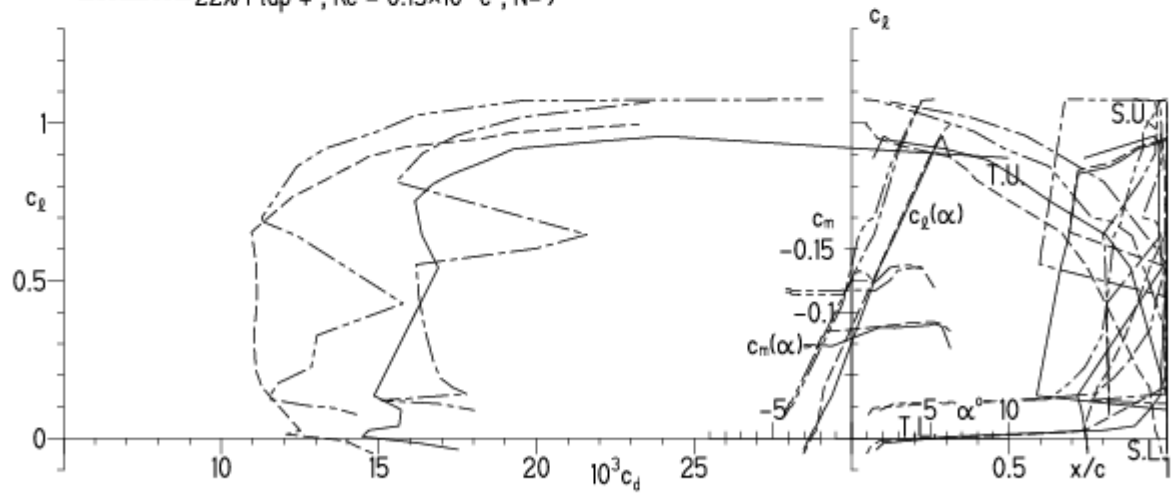


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

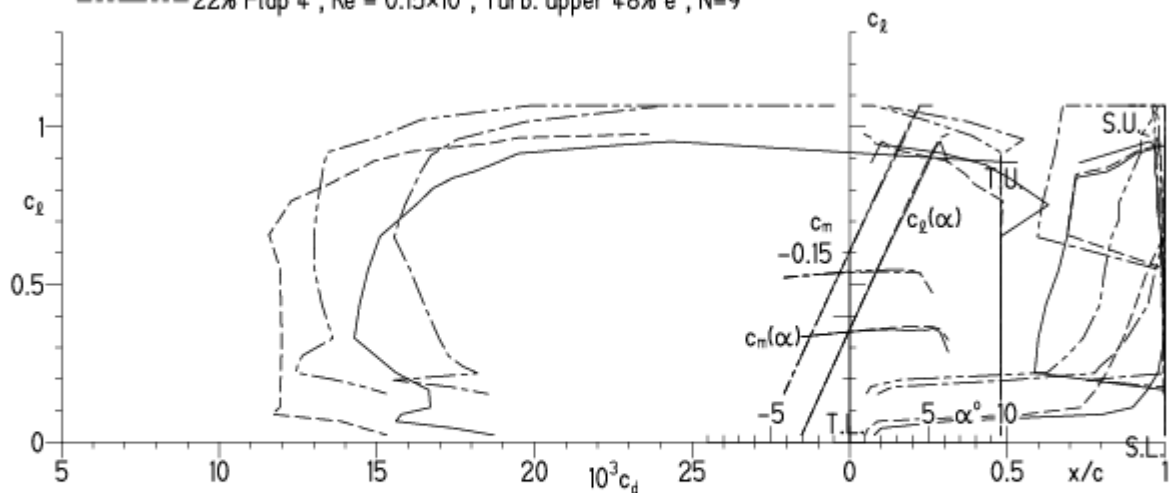


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



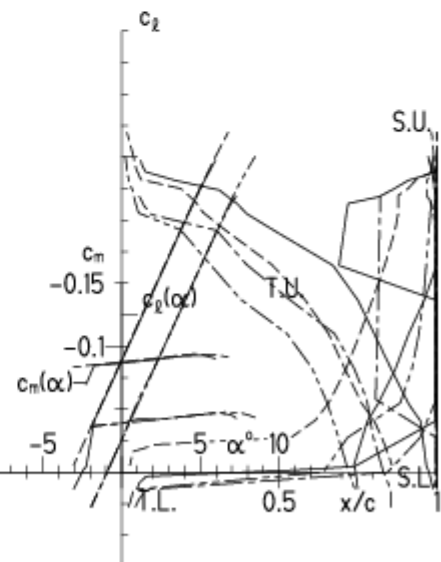
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

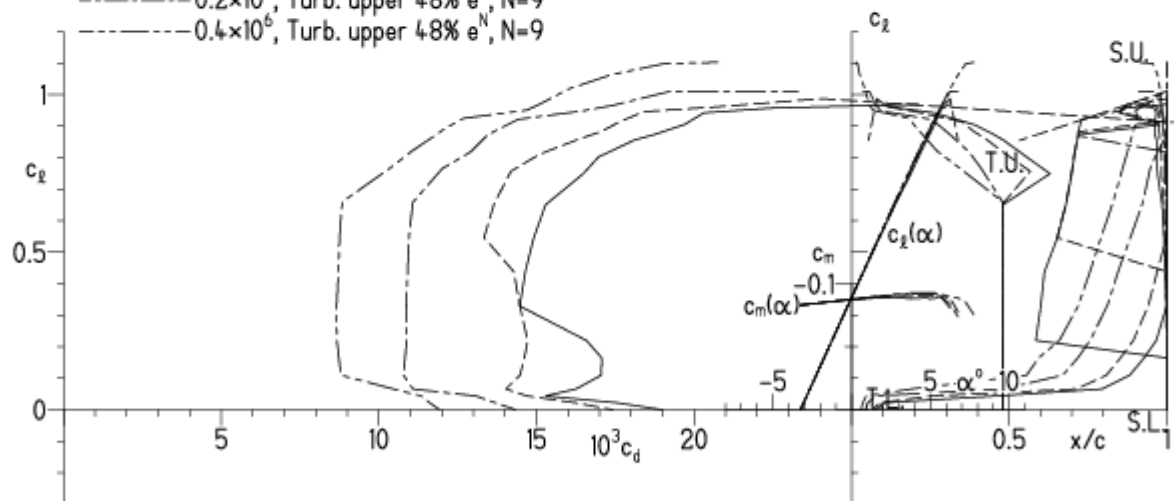
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

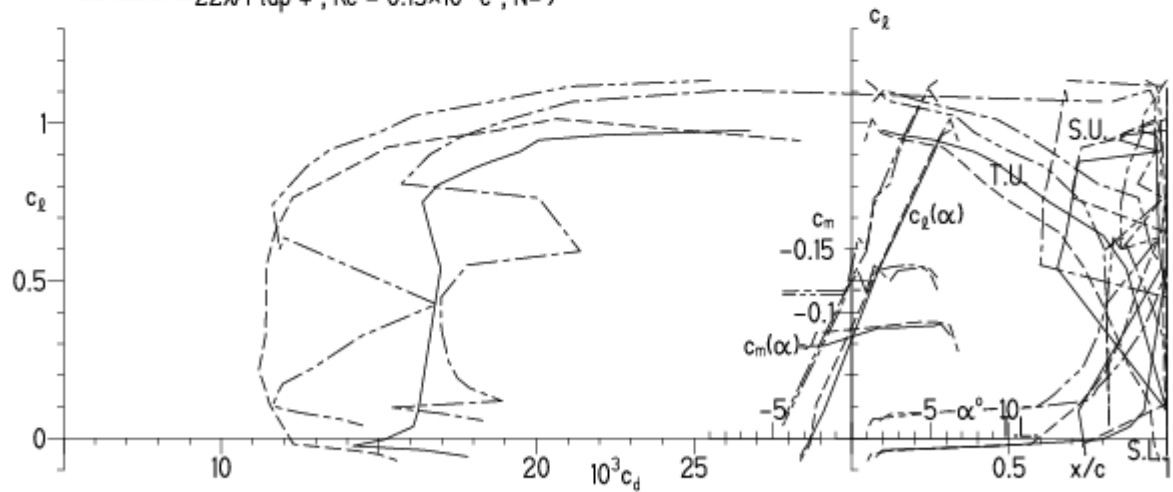


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

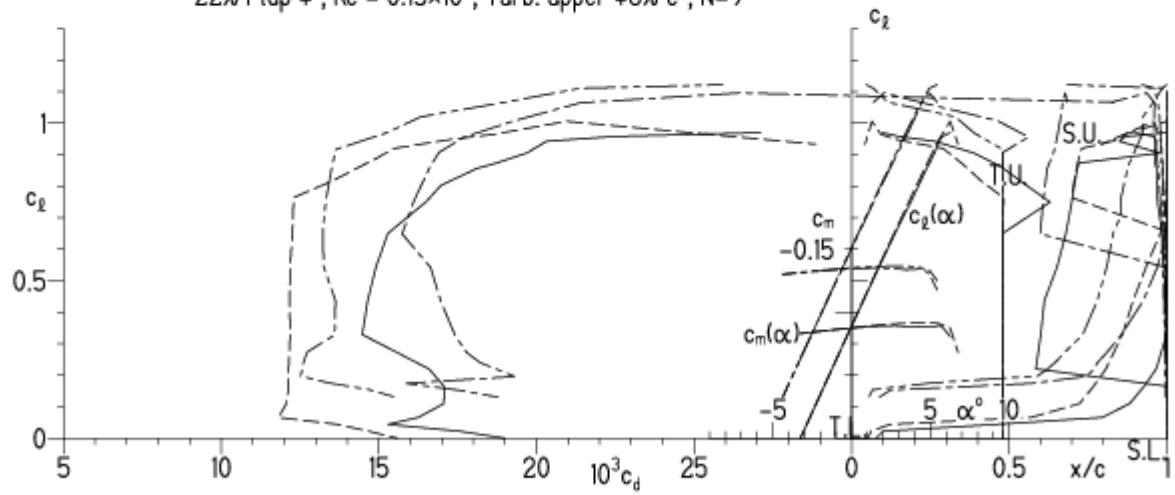


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- Re = 0.2×10^6 e^N, N=9
- - - Re = 0.8×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.2×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.8×10^6 e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

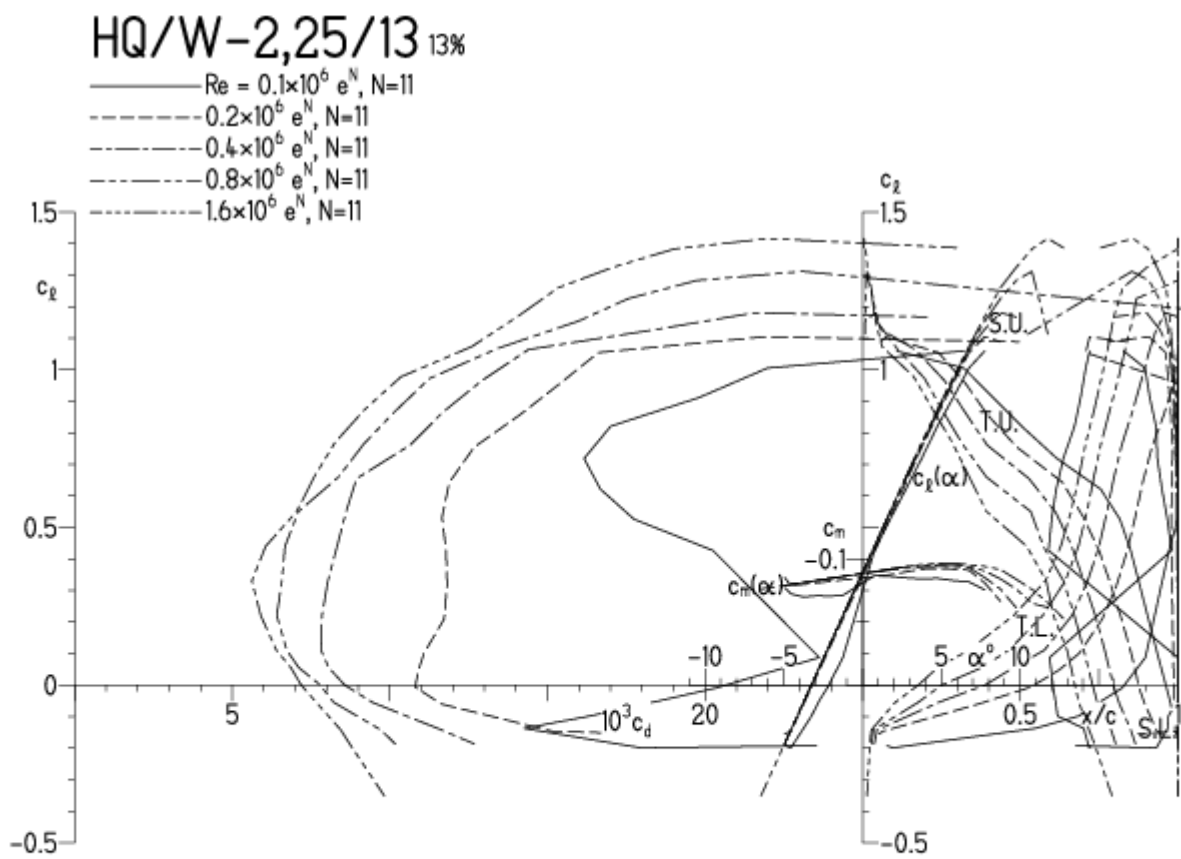


HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

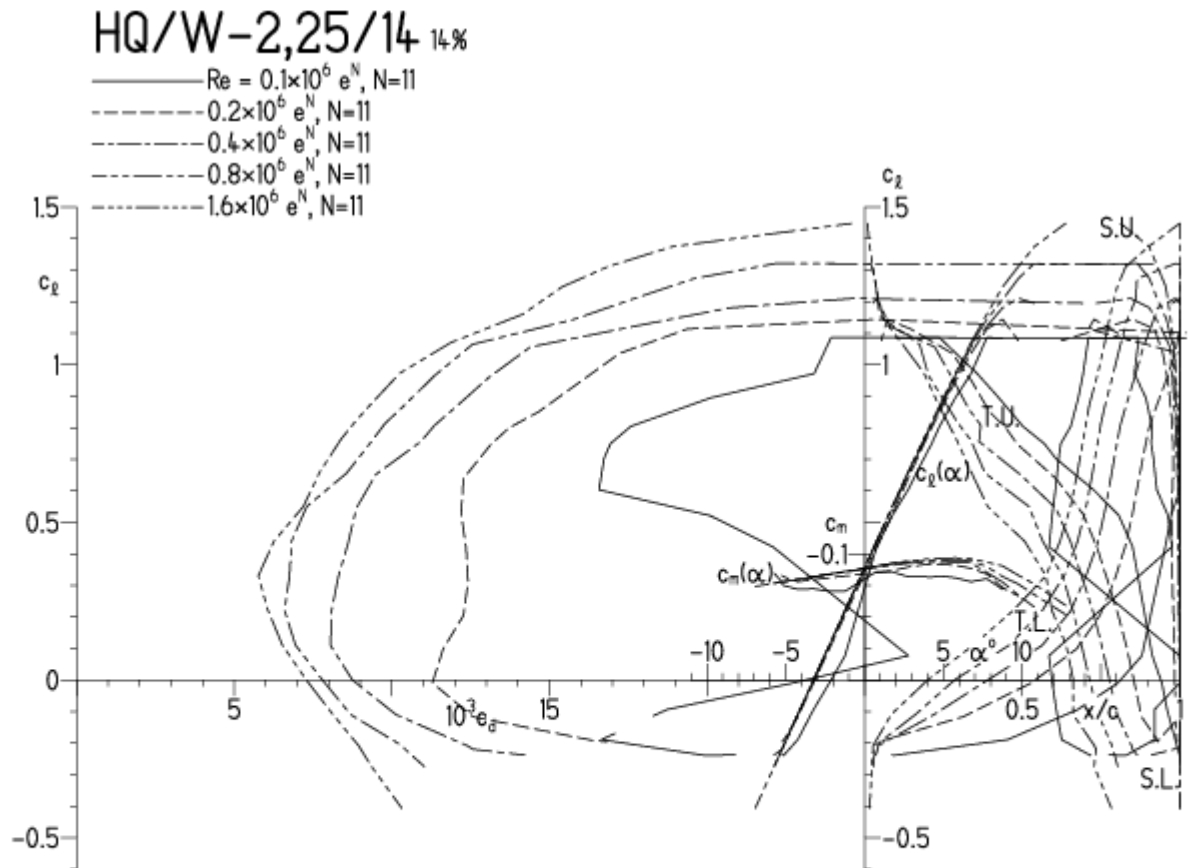


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

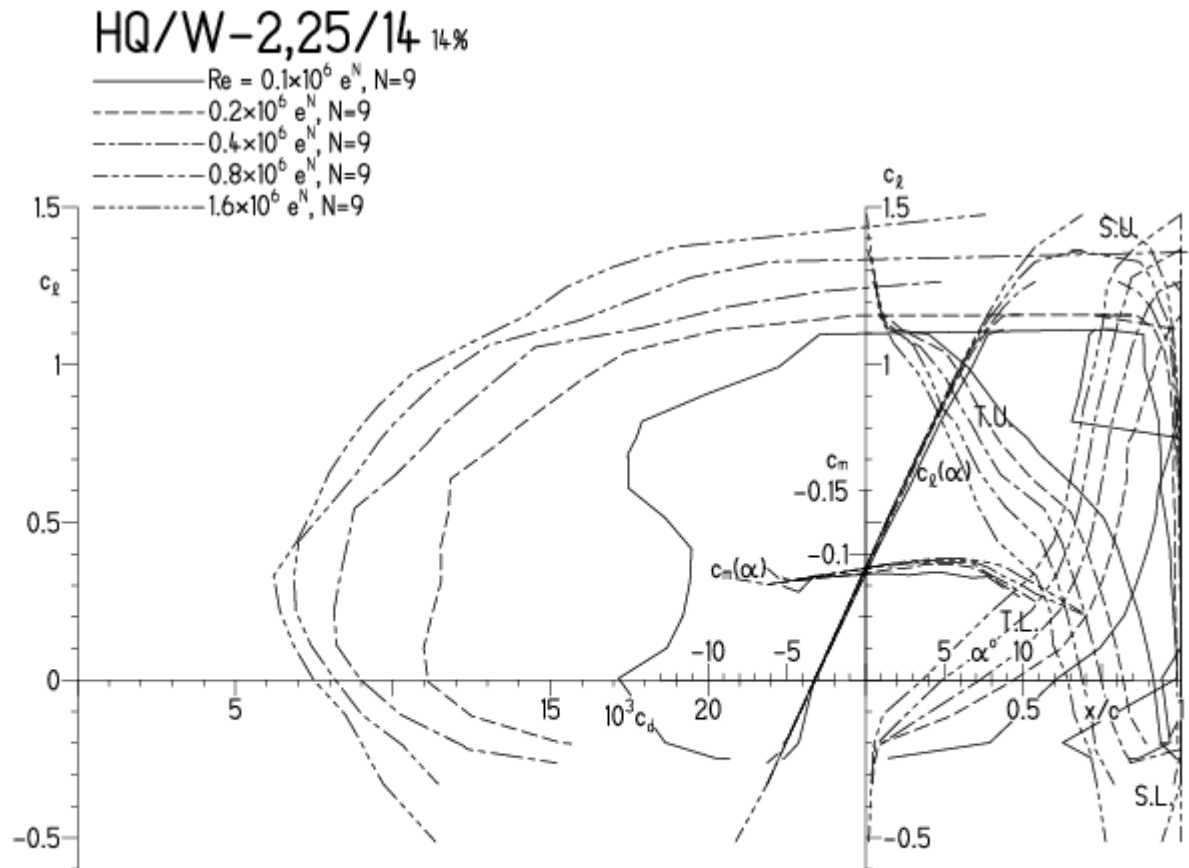


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

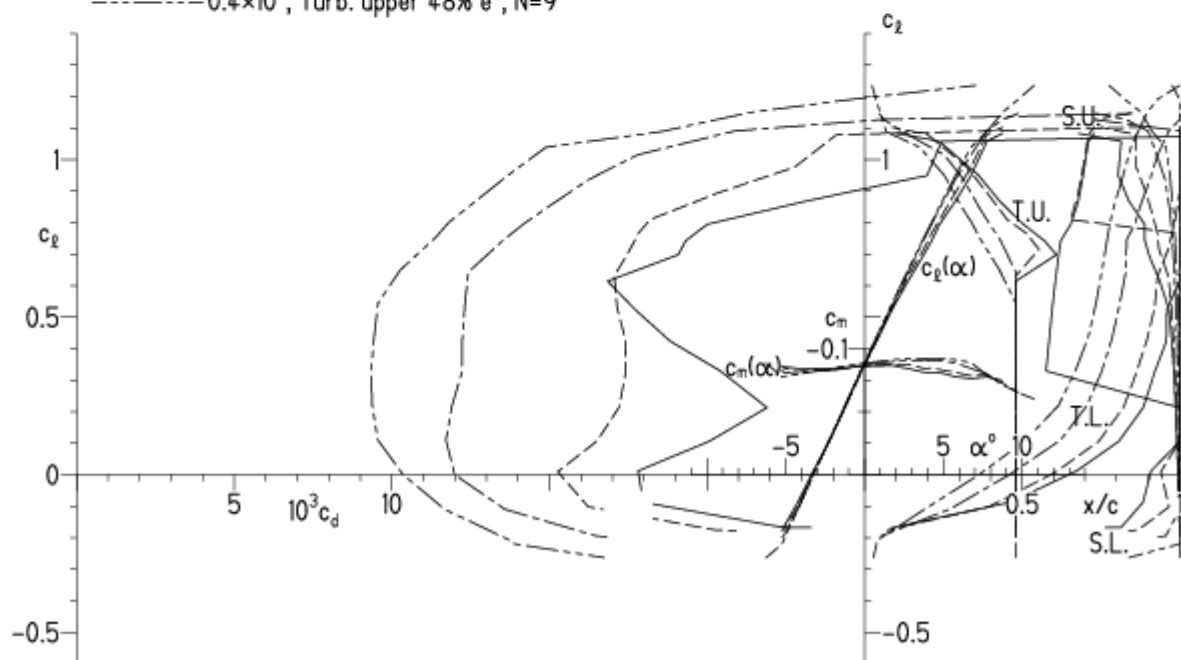
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

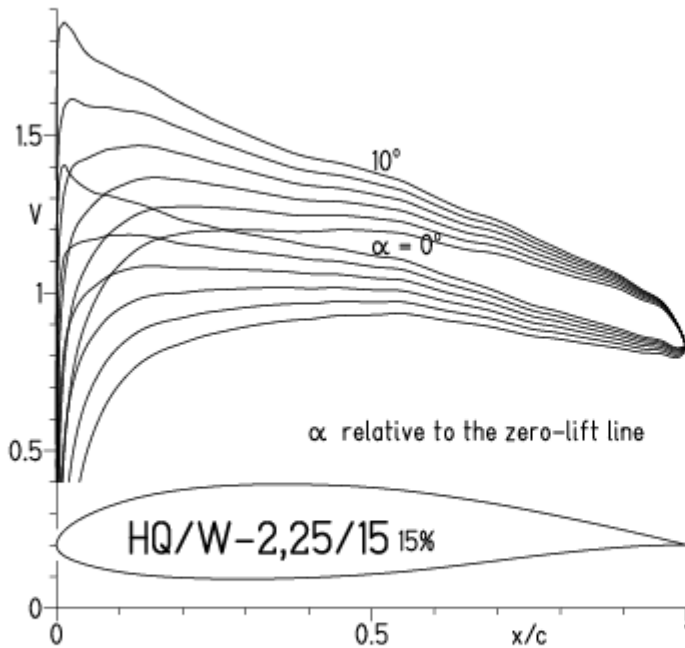


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

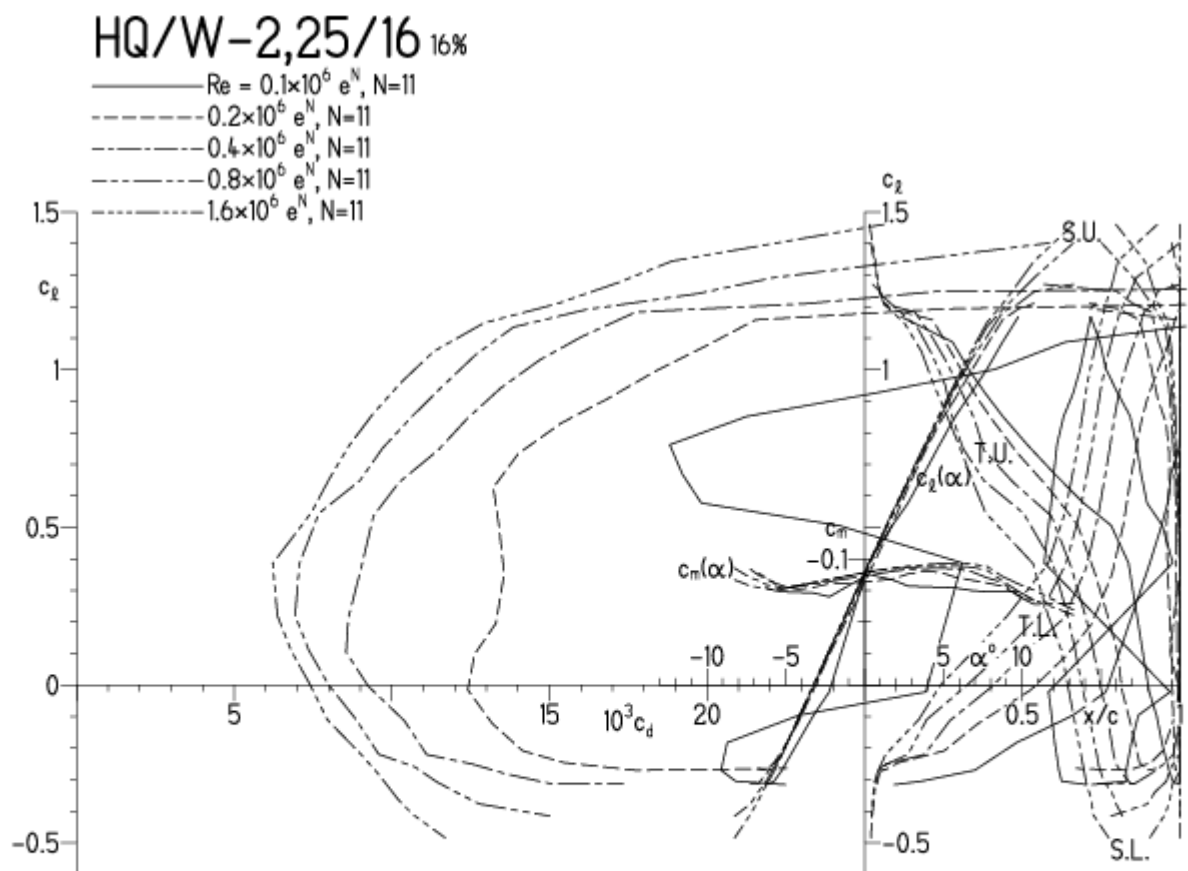


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

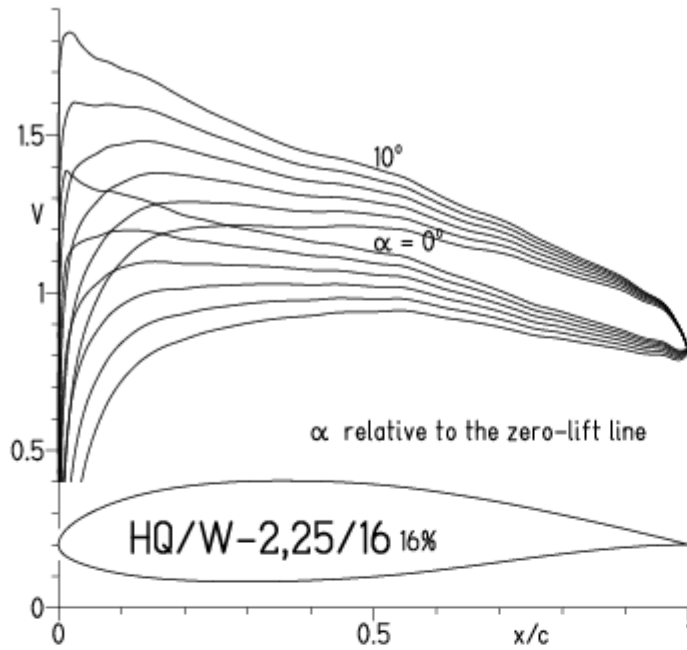
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

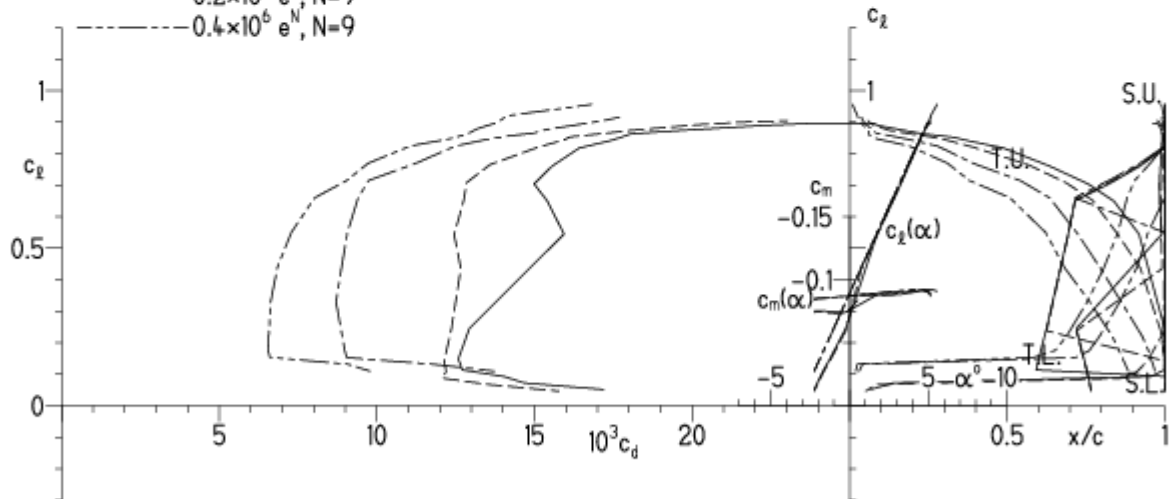
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - · 22% Flap 4°, Re = 75 000 e^N, N=9
- · - · 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2,25/8,5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



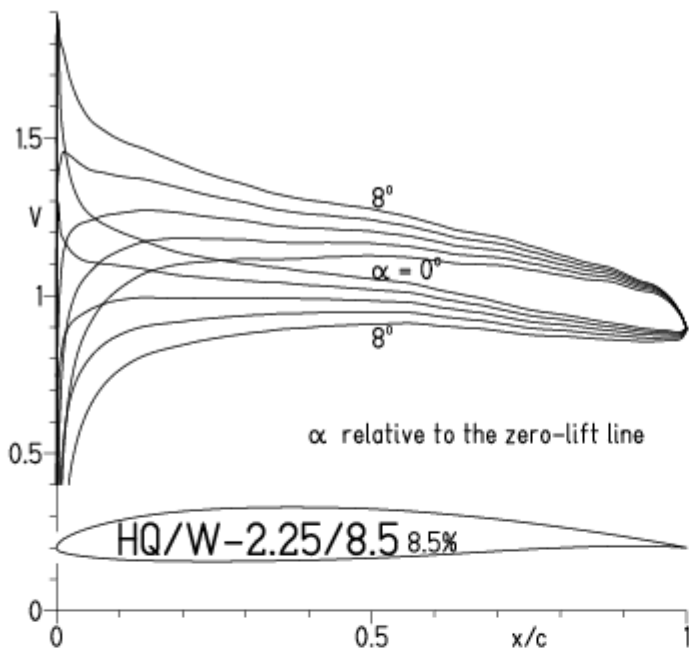
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

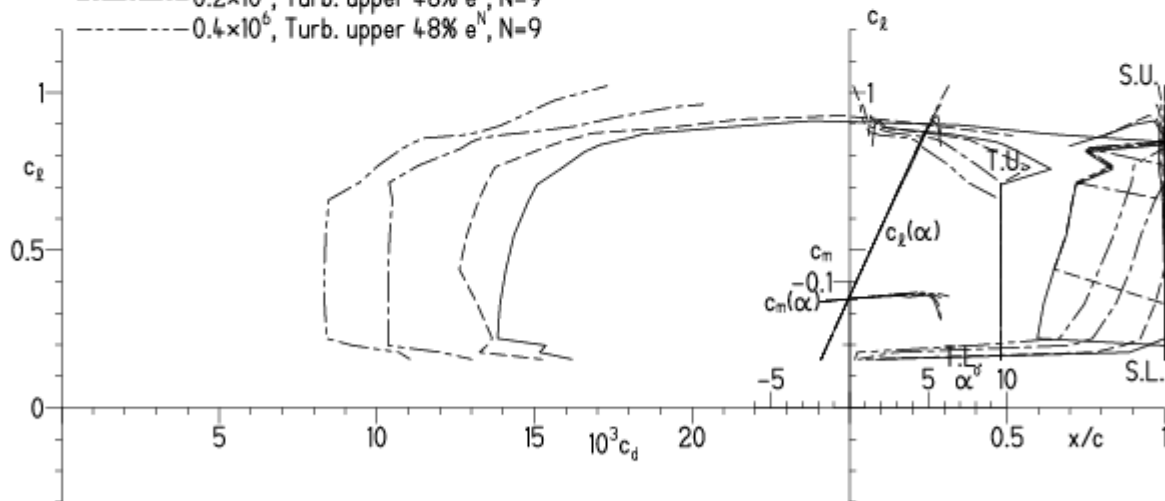
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

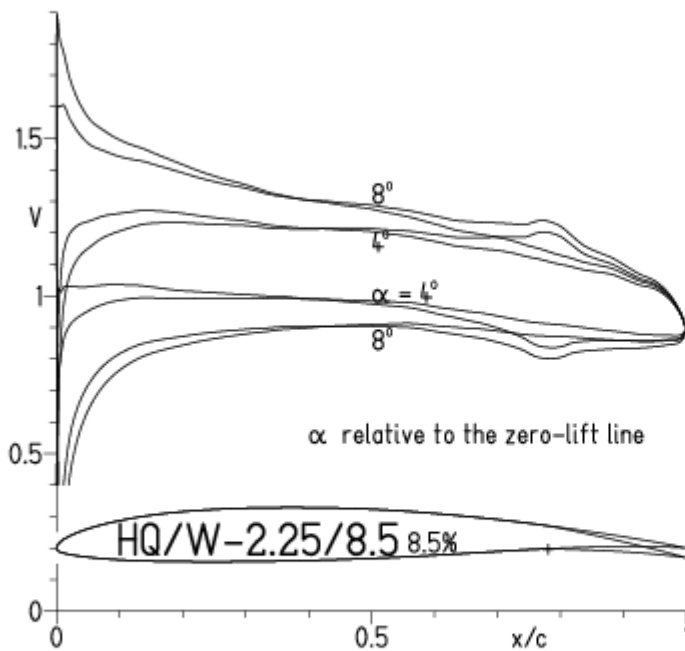
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

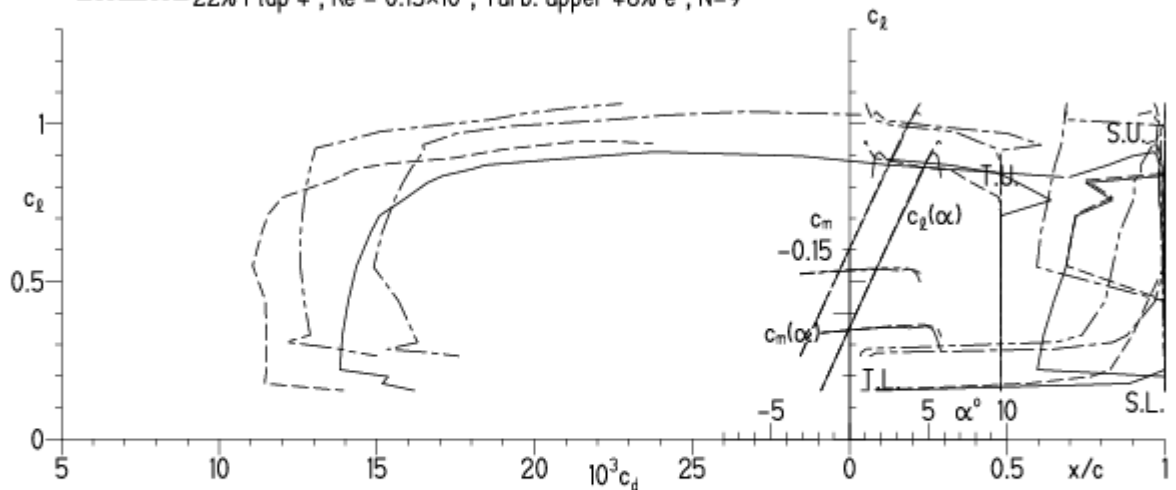


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



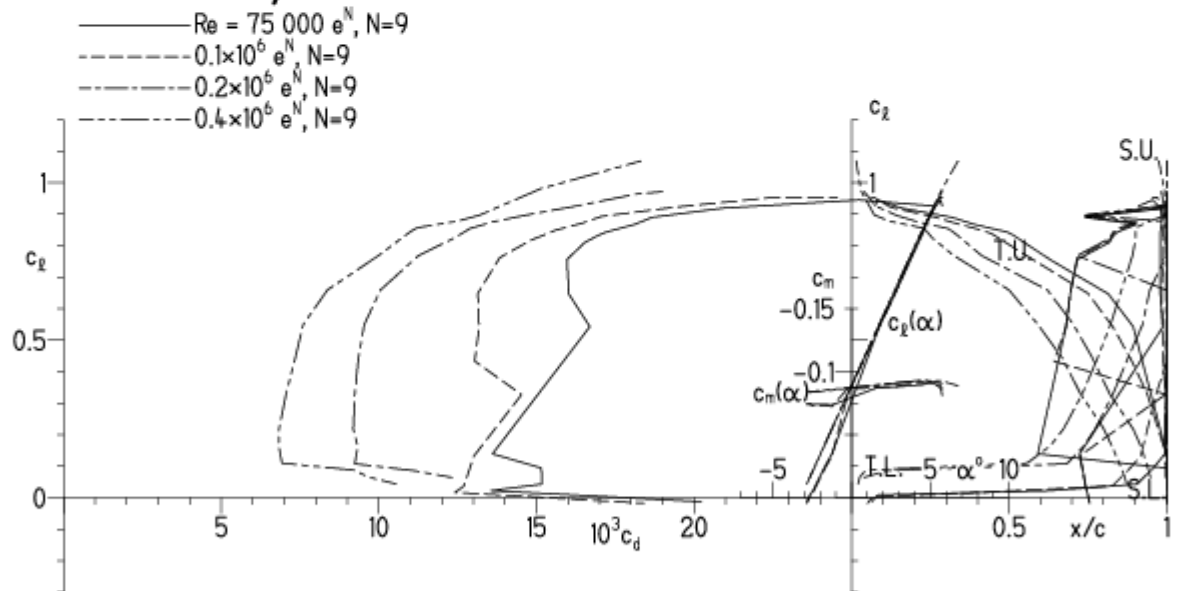
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

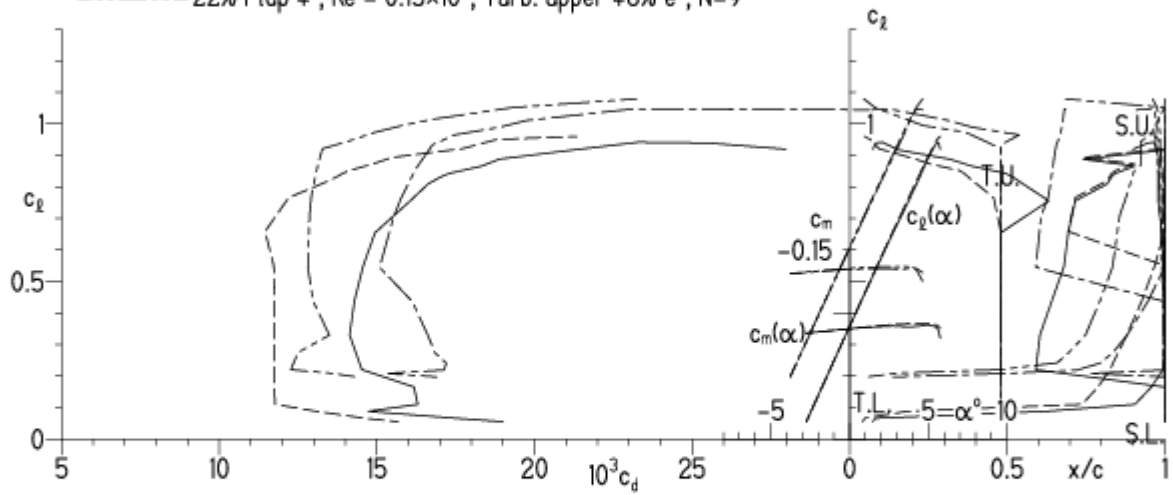


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

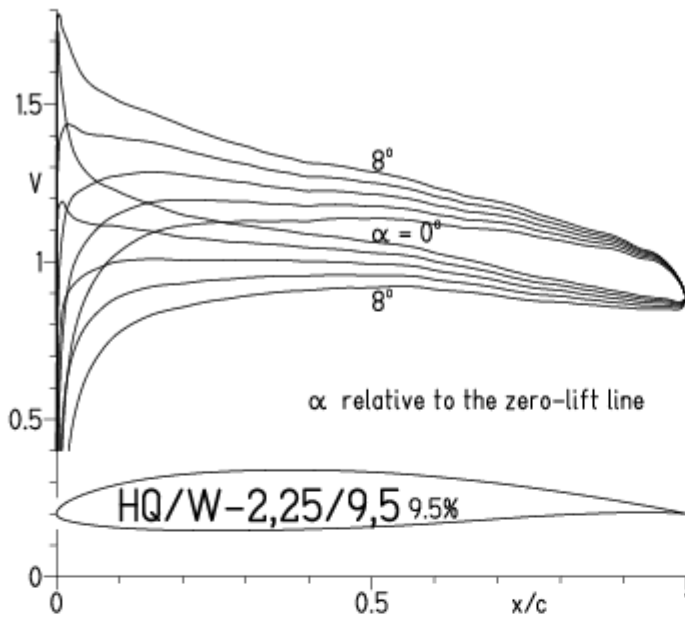
HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

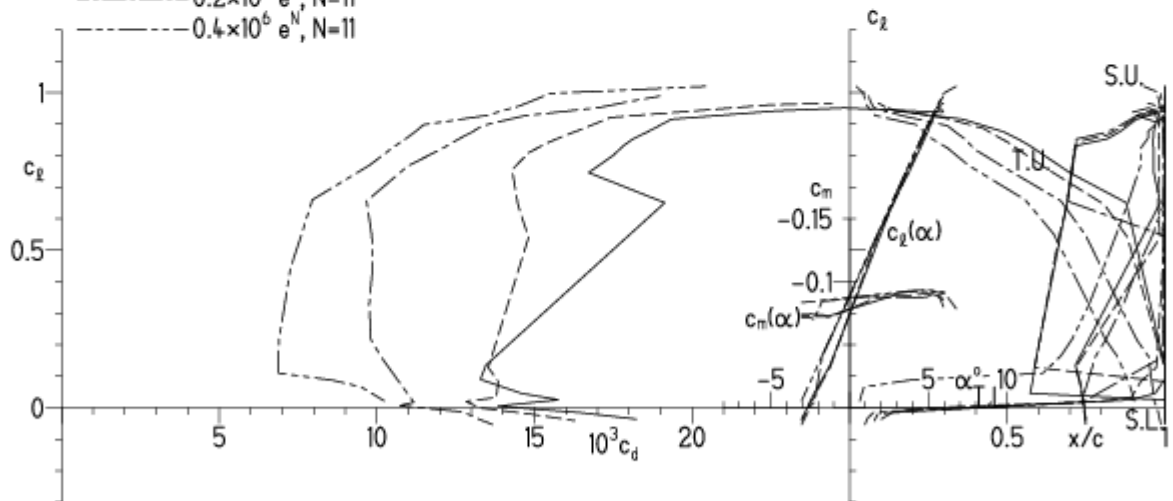
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

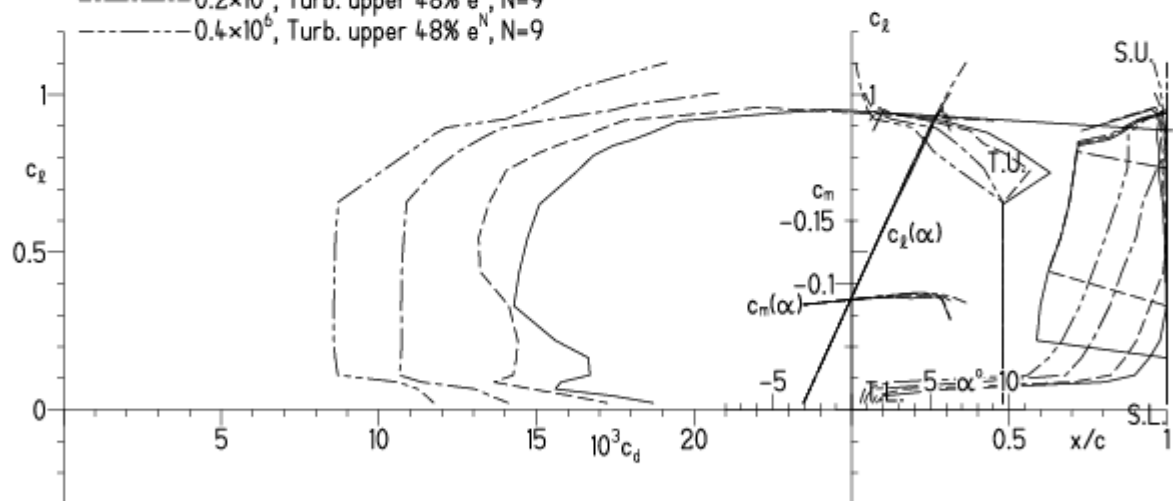
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

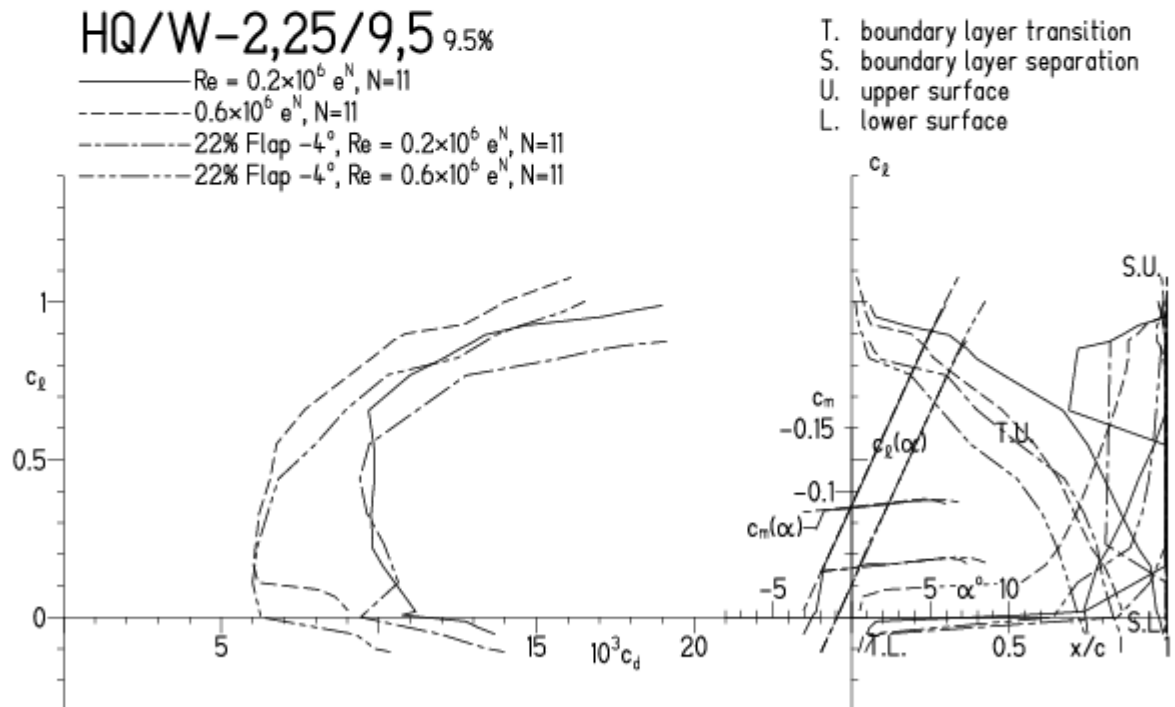


HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

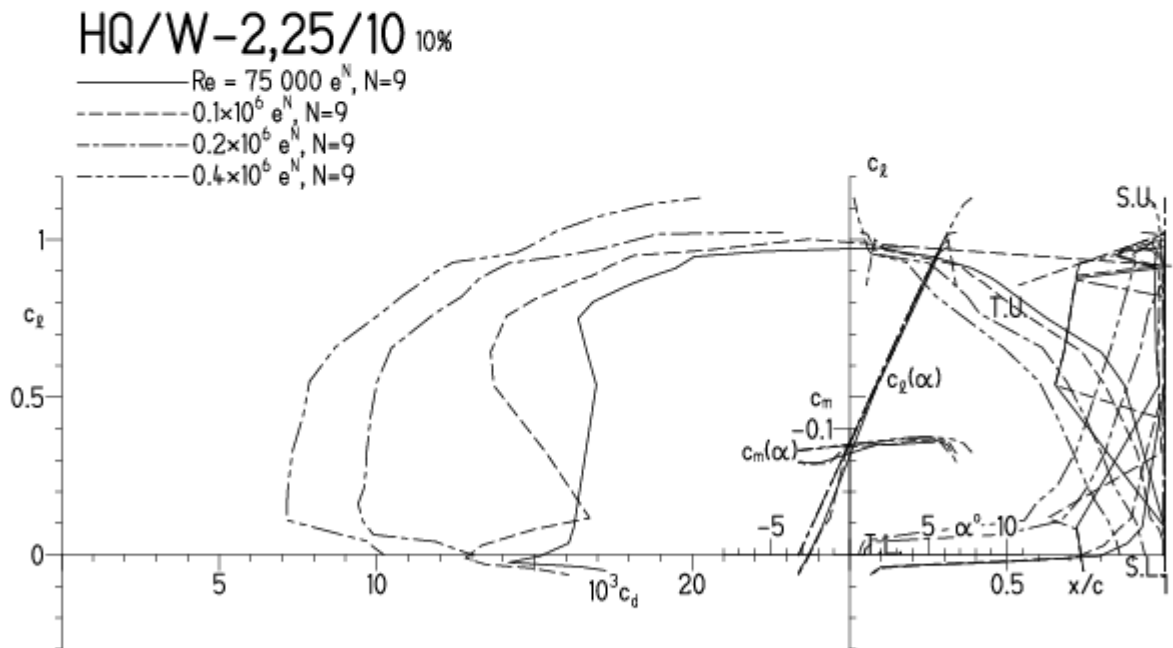


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

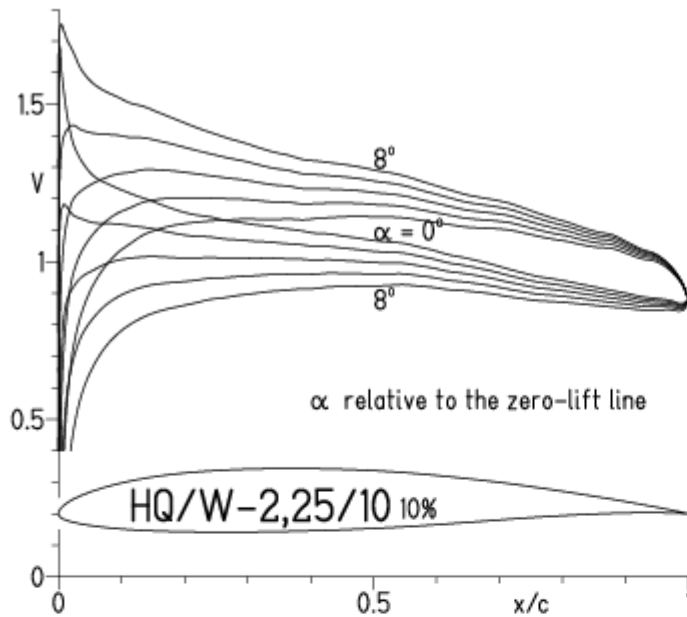


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

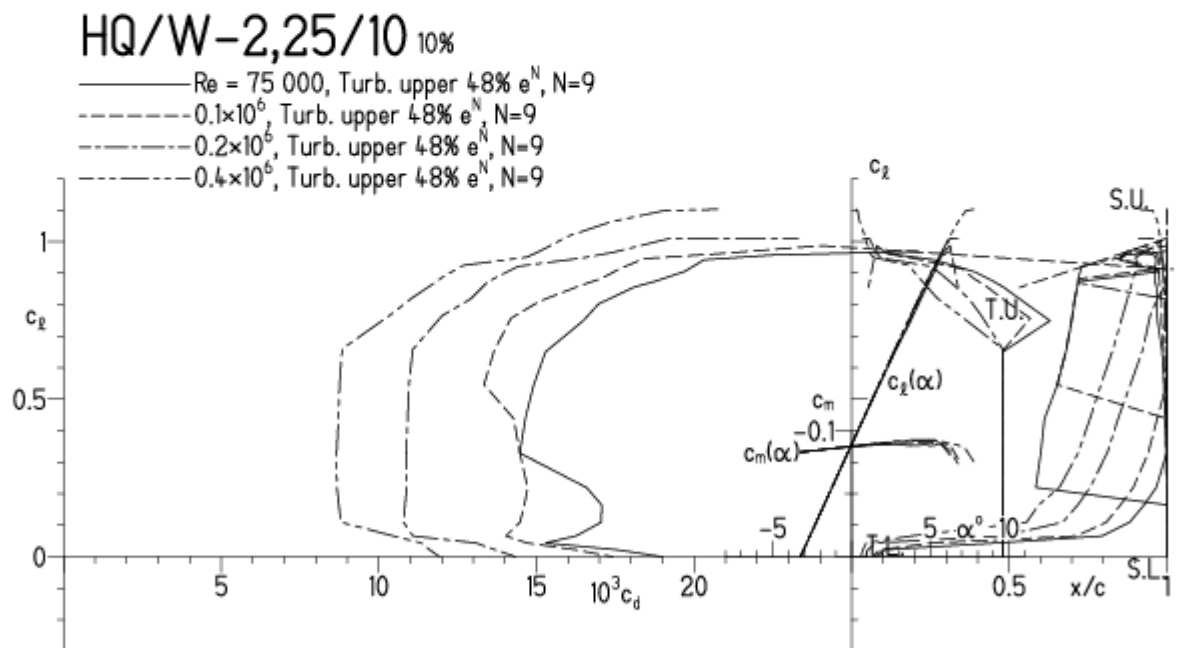


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

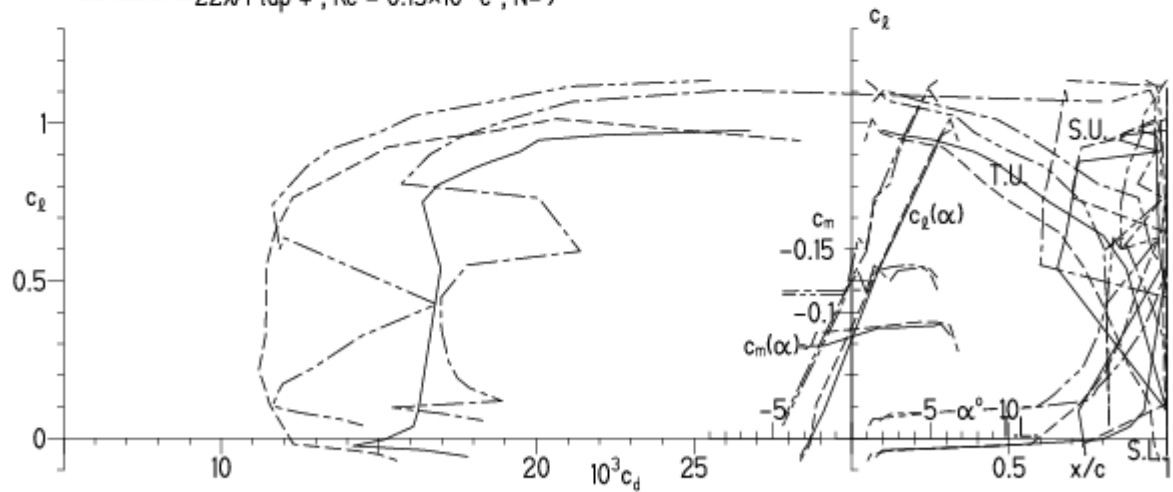


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

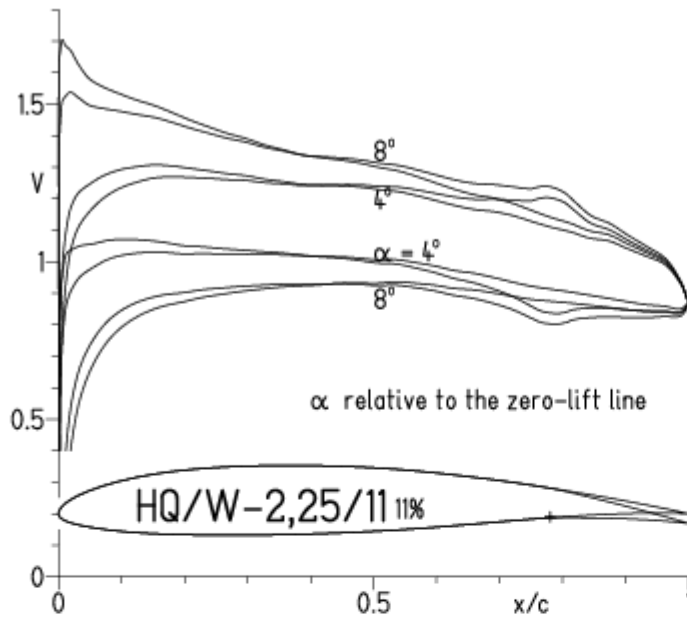
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- Re = 0.2×10^6 e^N, N=9
- - - Re = 0.8×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.2×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.8×10^6 e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

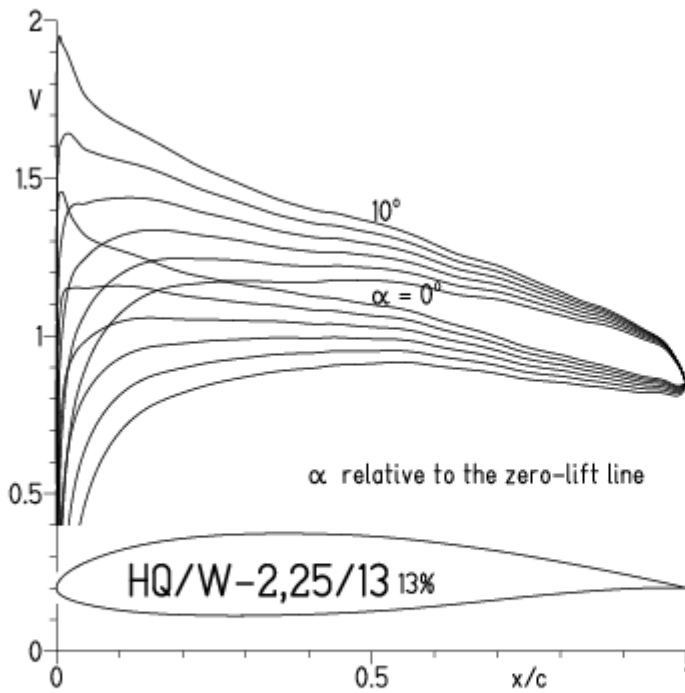


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

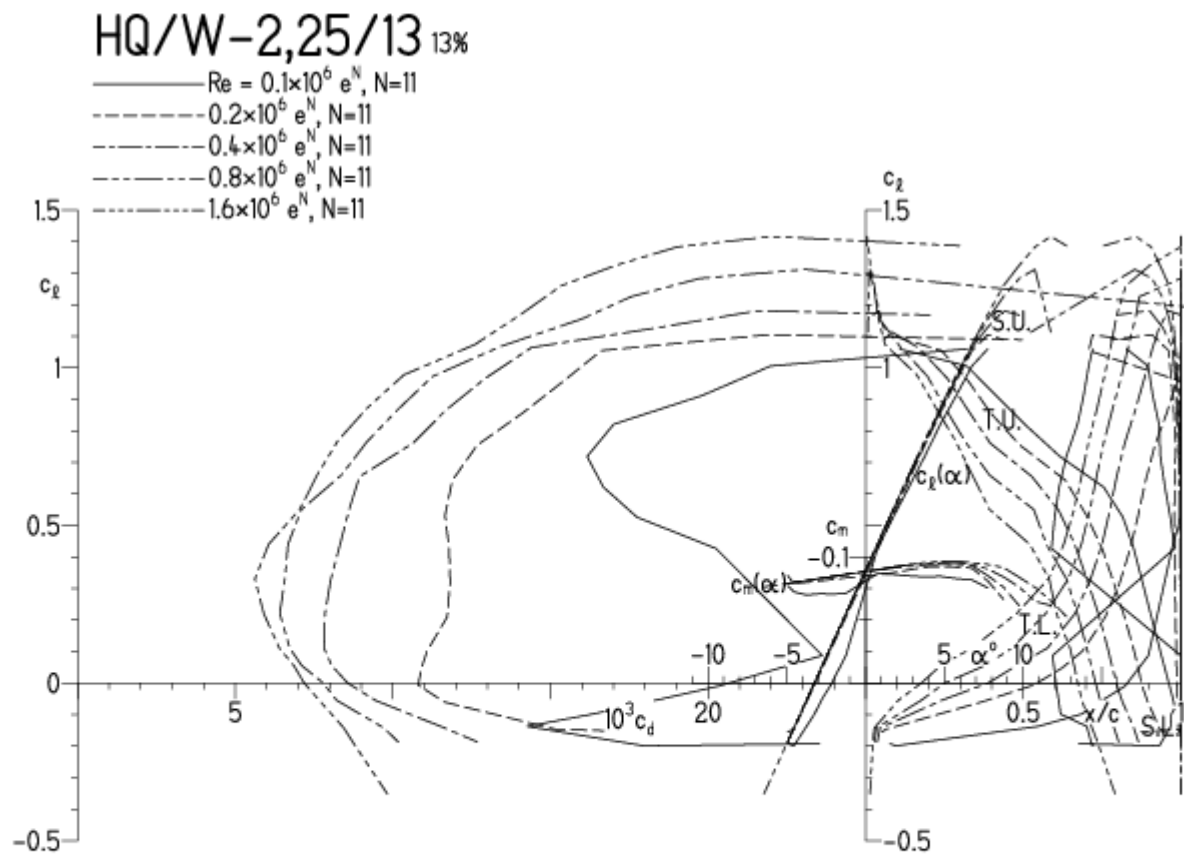


HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

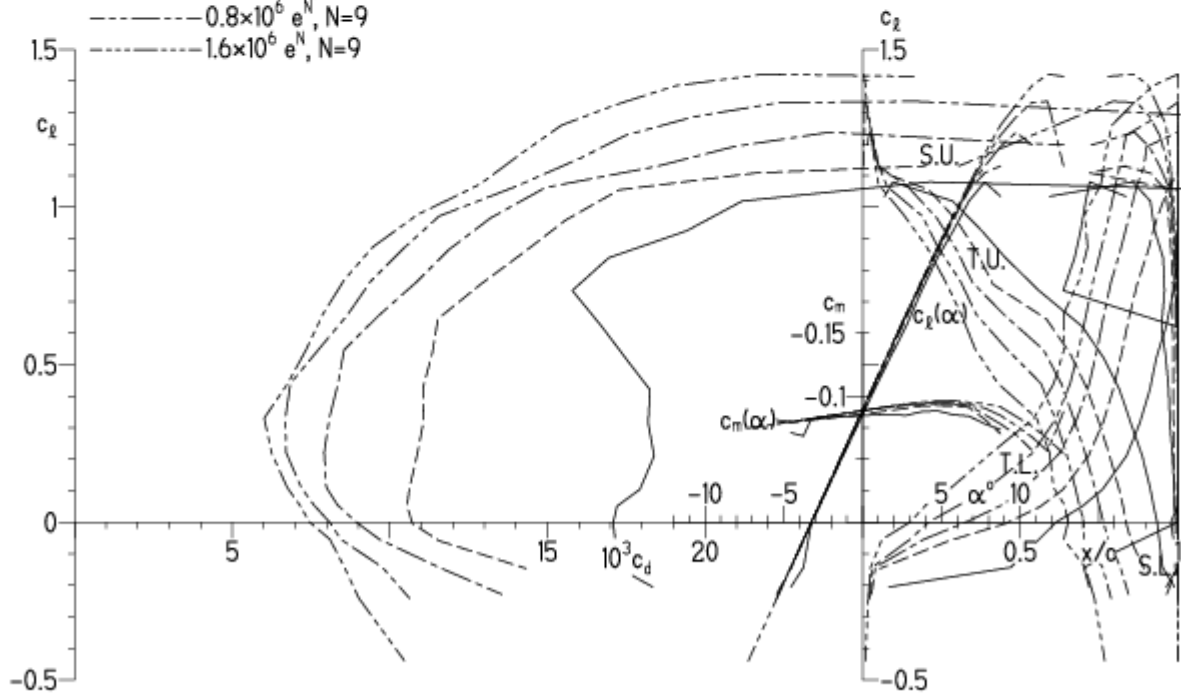
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

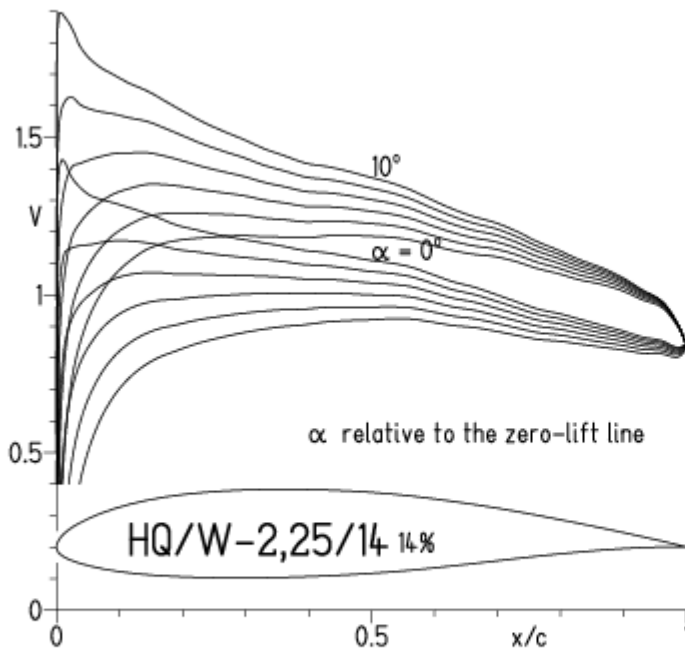


EPPLER 2005 V. 8.

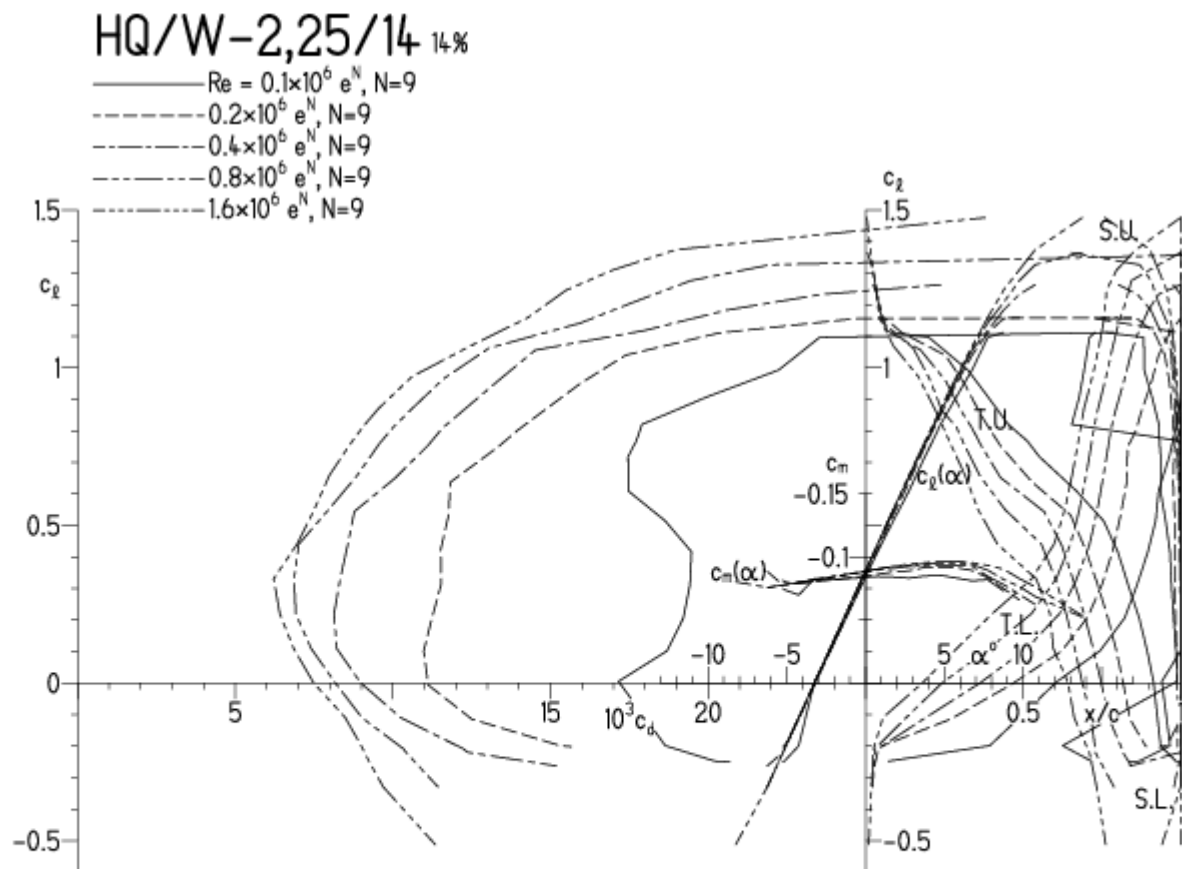


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

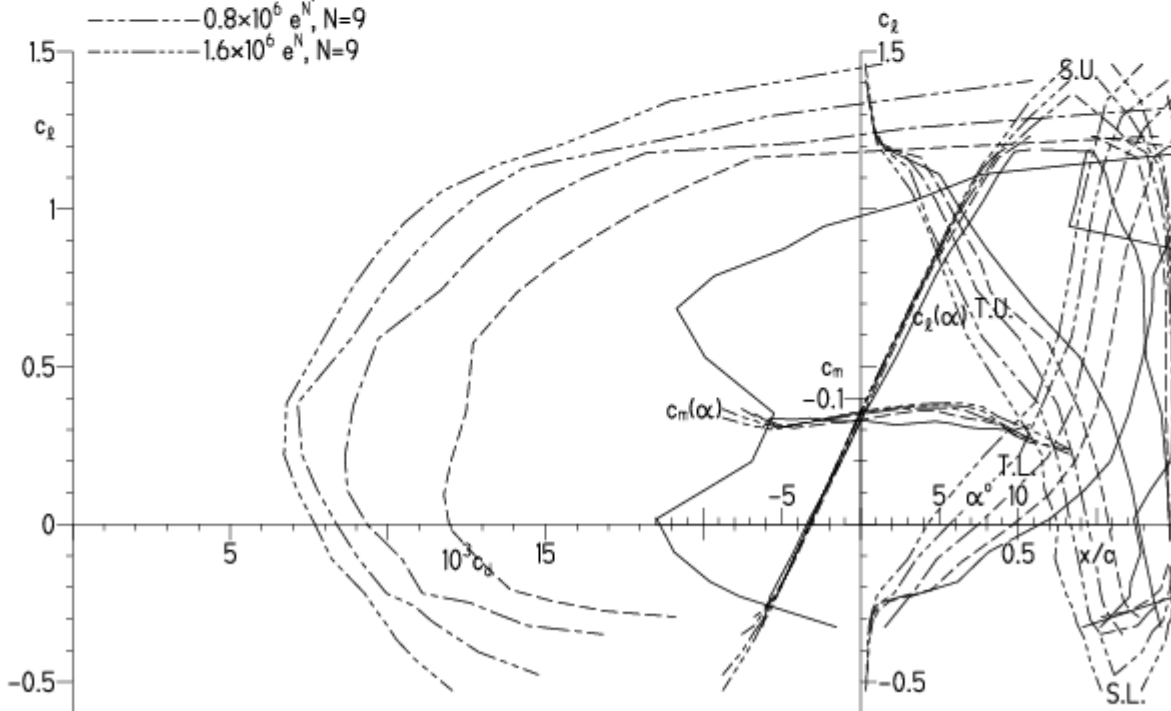
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

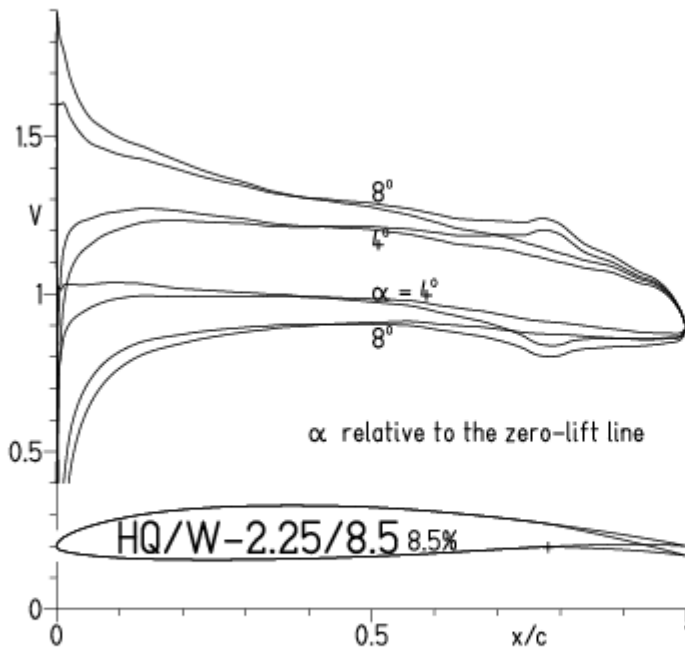
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

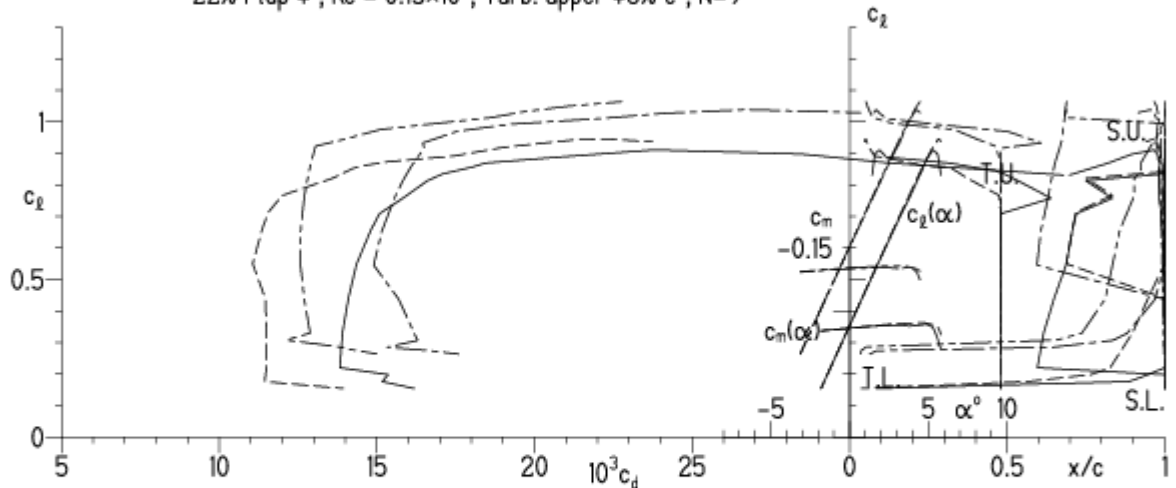


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

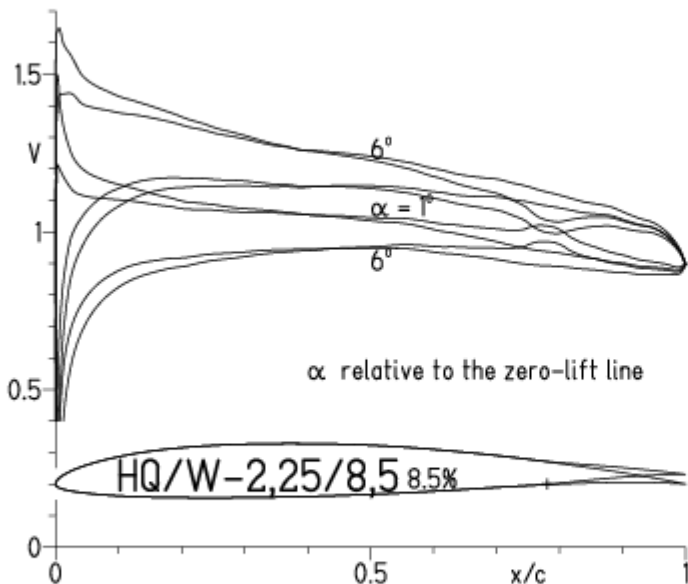
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

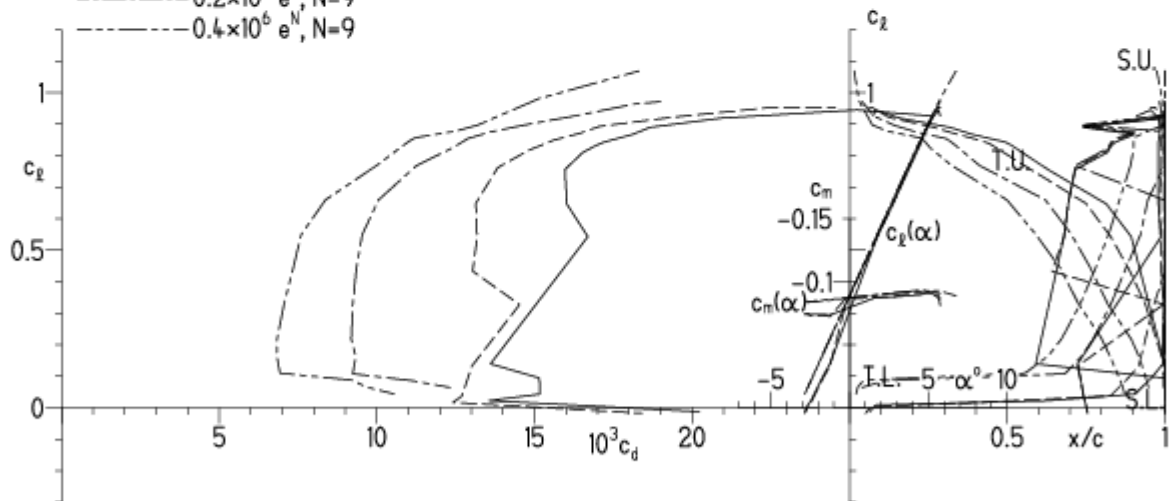
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

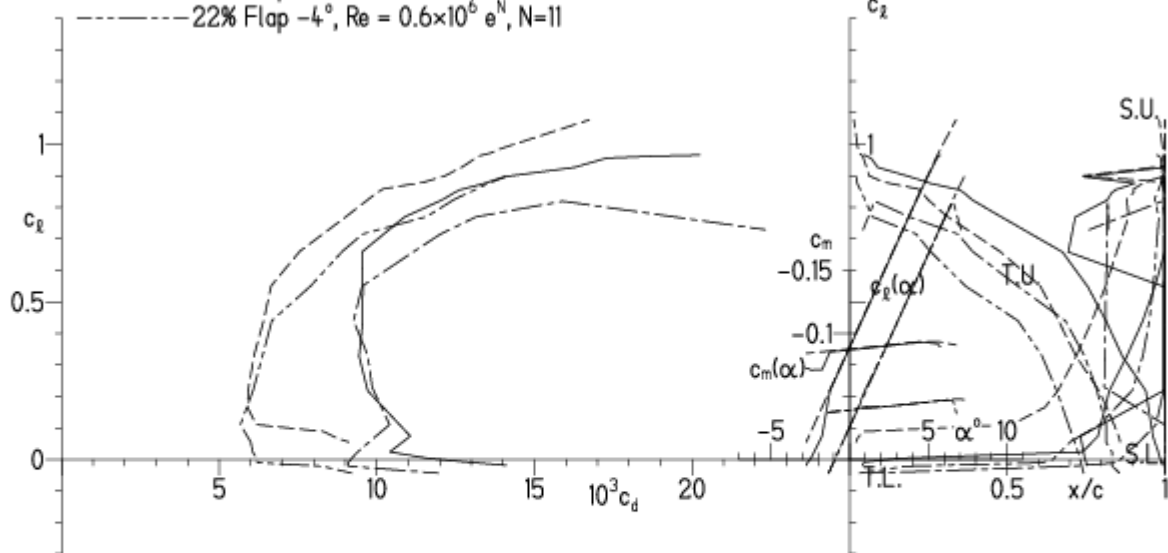
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

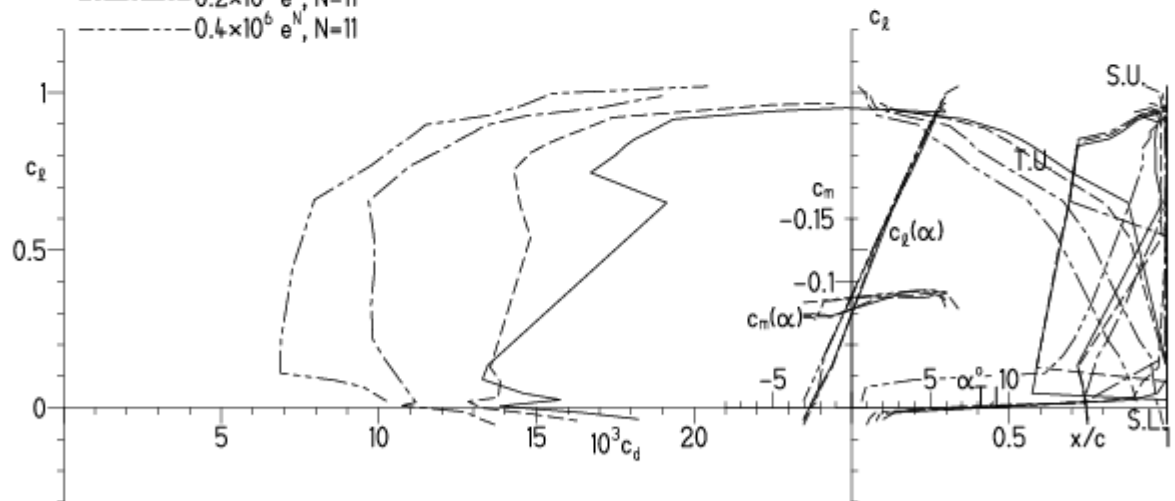
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- Re = 75 000 e^N, N=9
- - - 0.15x10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

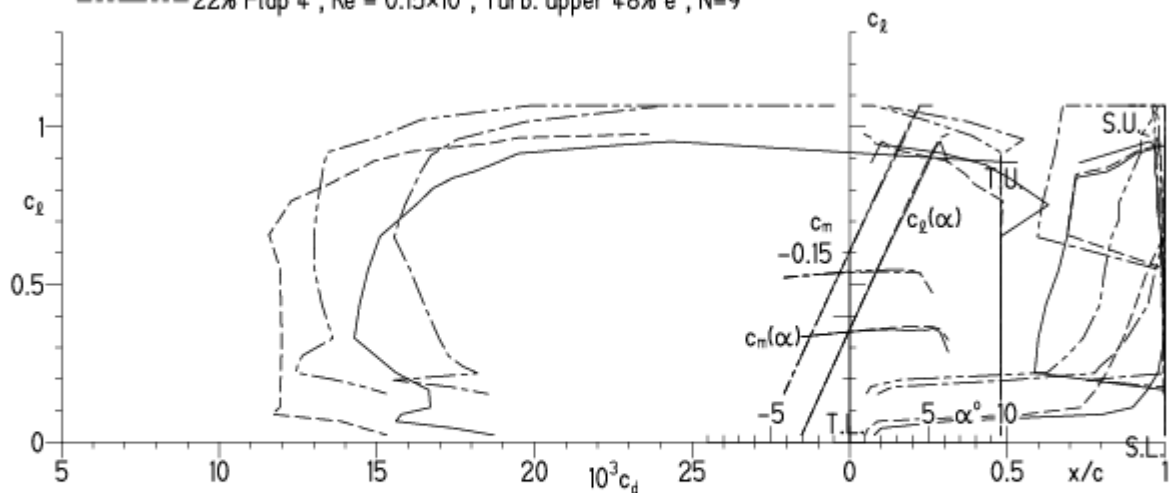


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



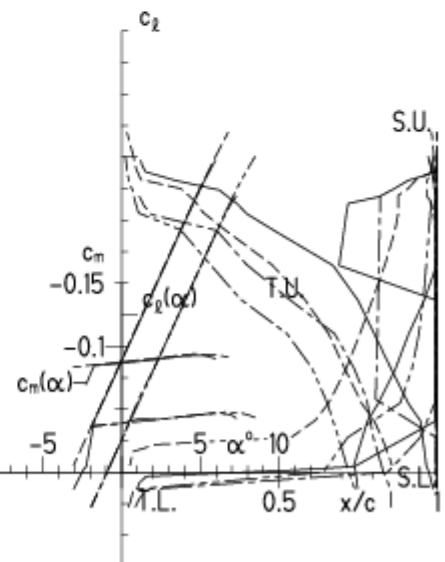
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

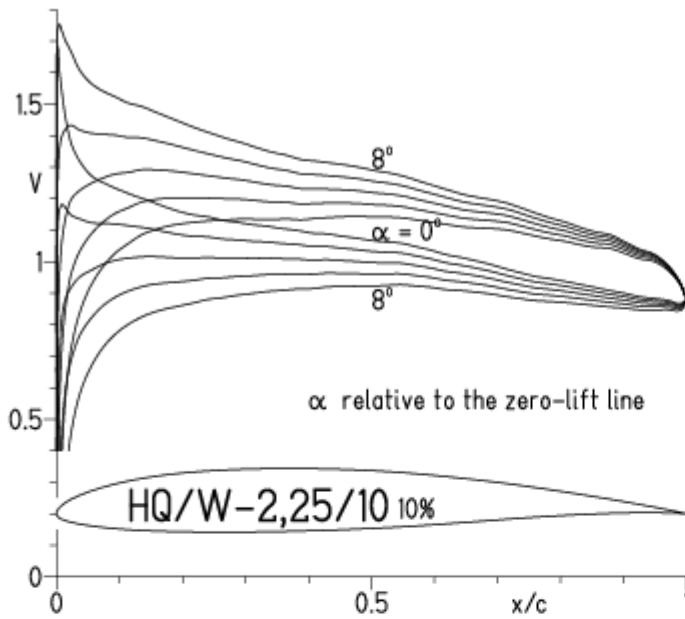


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

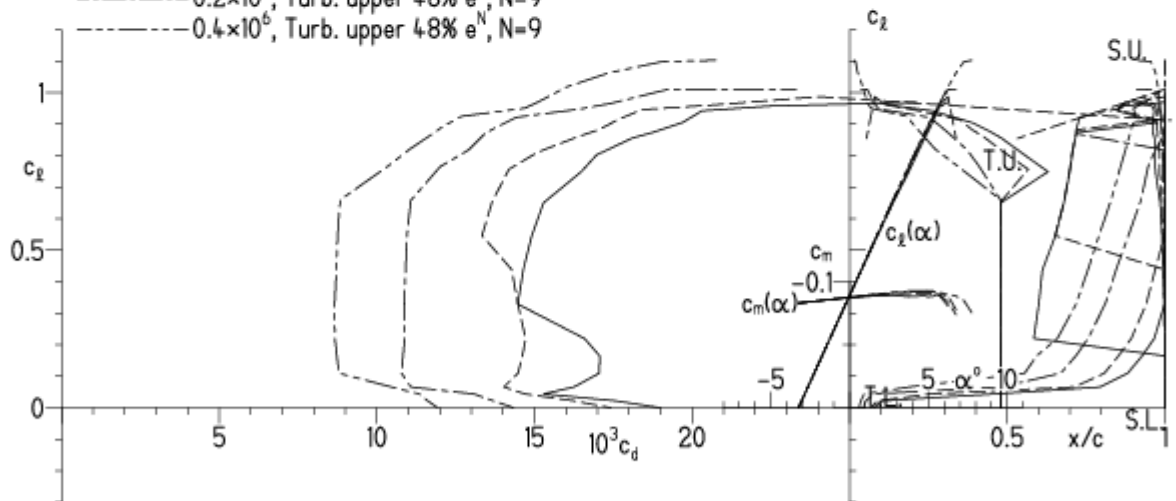
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

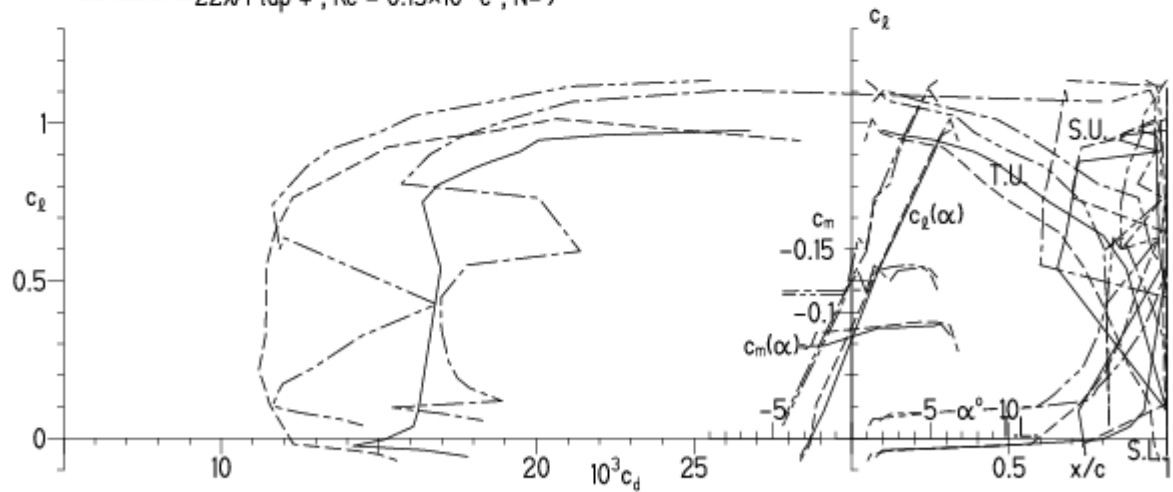


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6$, e^N , $N=9$
- - - 0.2×10^6 , e^N , $N=9$
- · - 0.4×10^6 , e^N , $N=9$
- · - · 0.8×10^6 , e^N , $N=9$
- · - · - 1.6×10^6 , e^N , $N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · · - $0.8 \times 10^6 e^N, N=9$
- · · · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

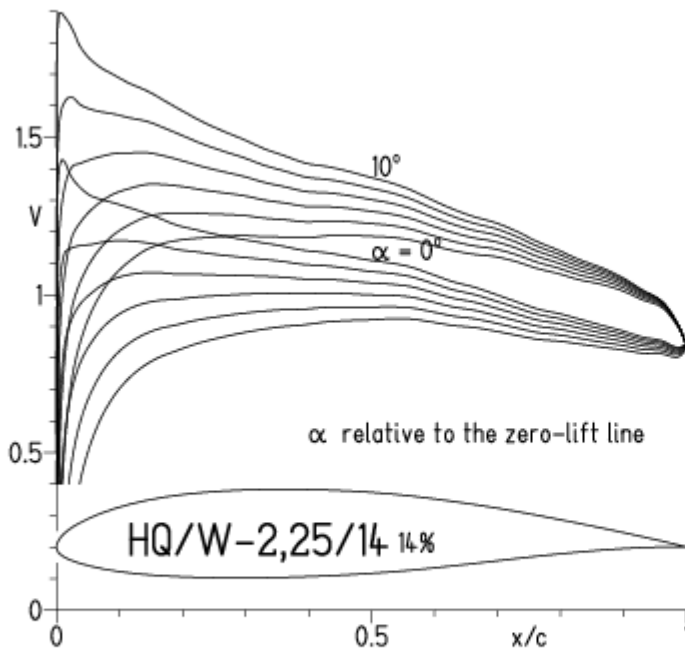


EPPLER 2005 V. 8.

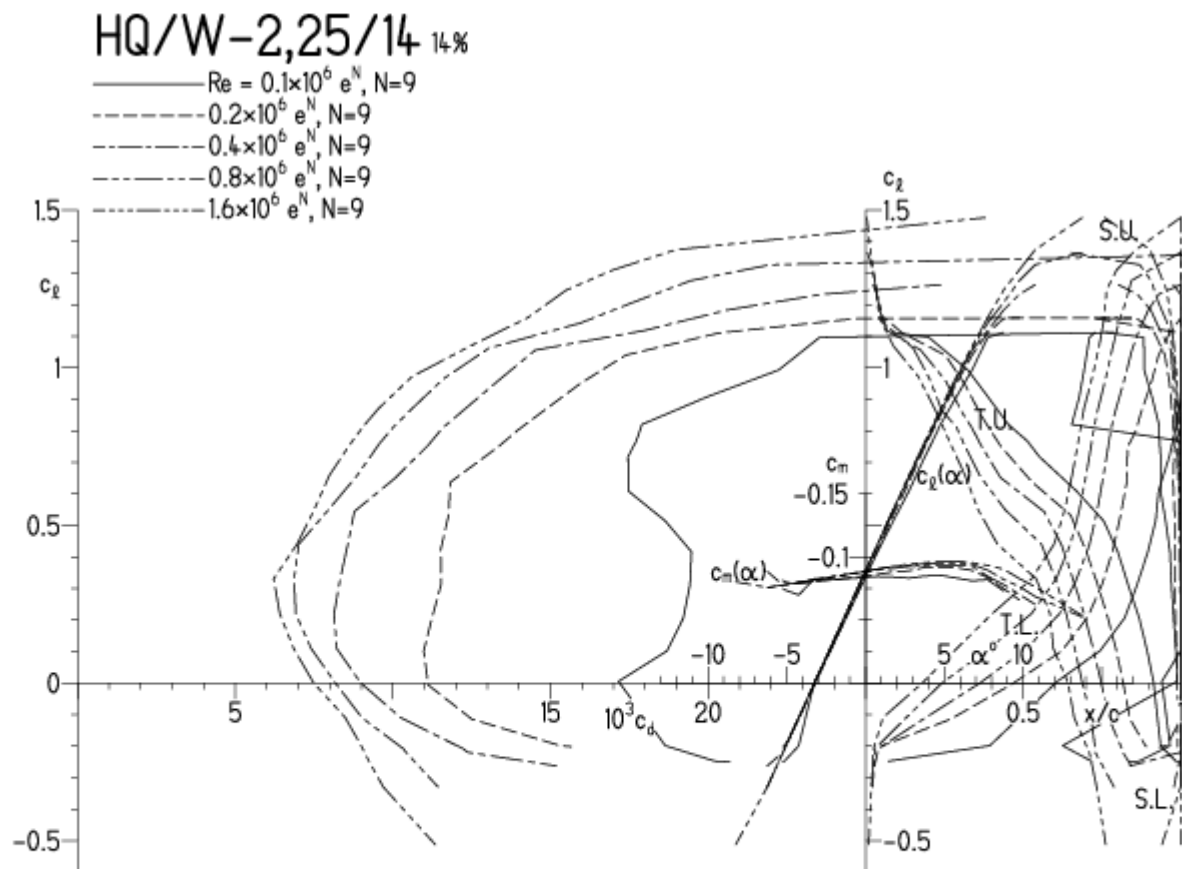


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

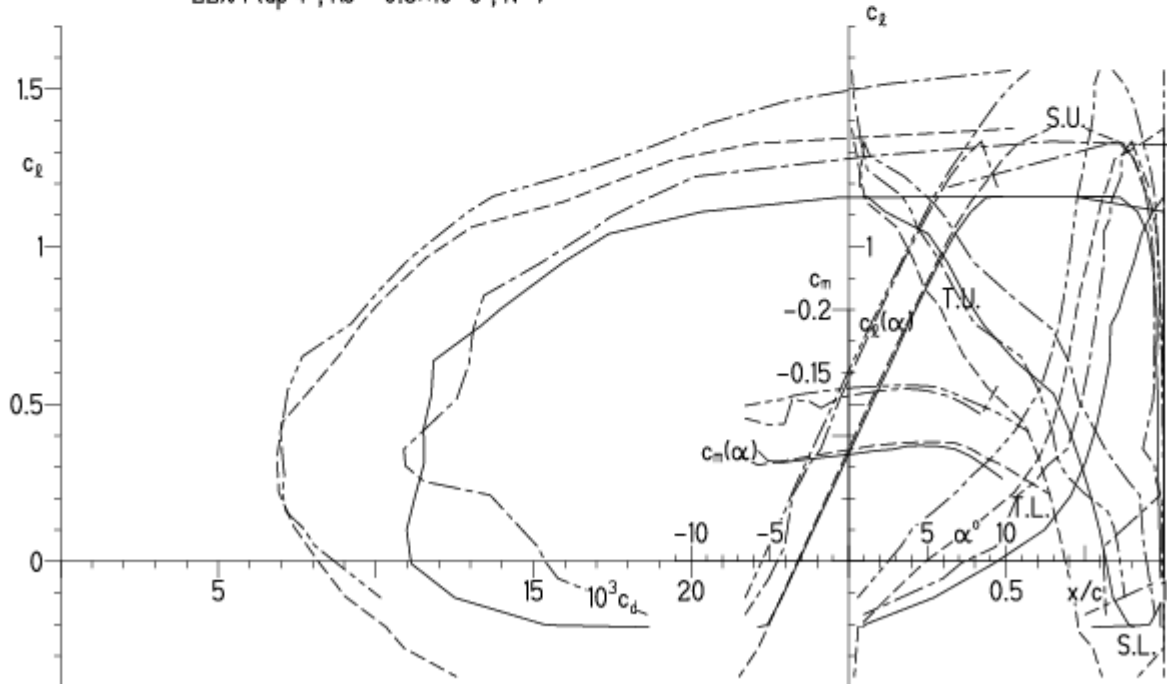


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

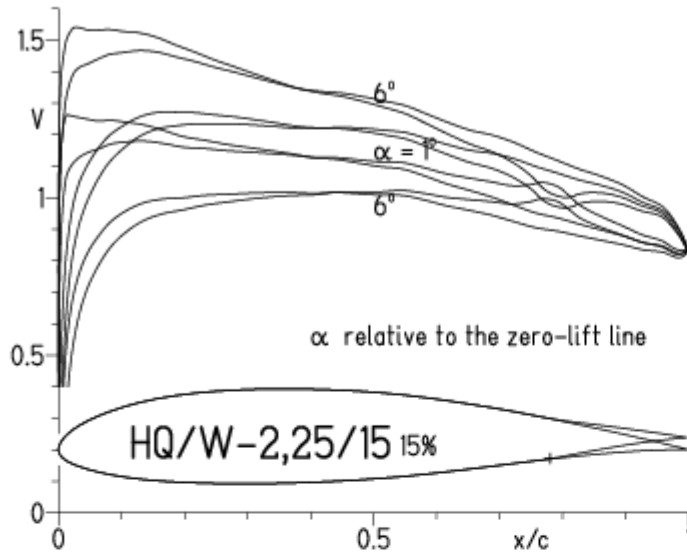


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

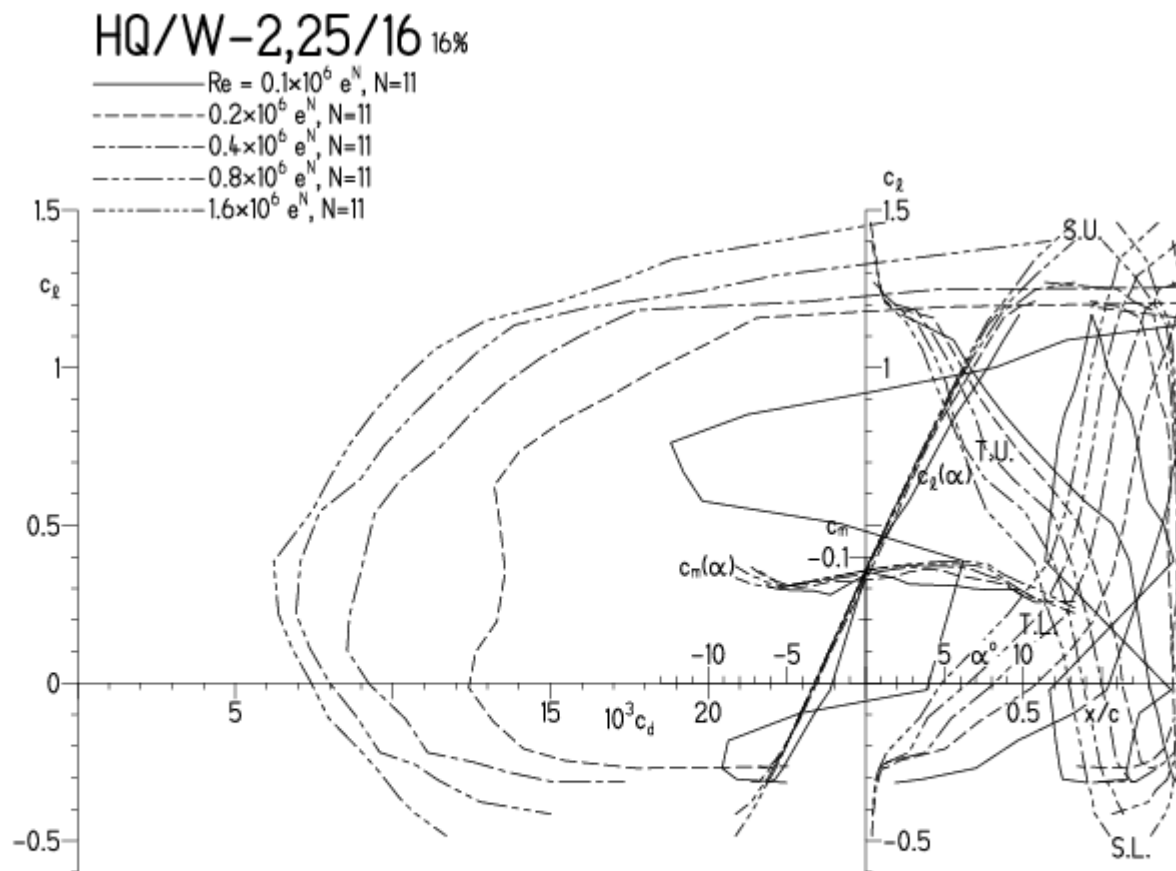


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



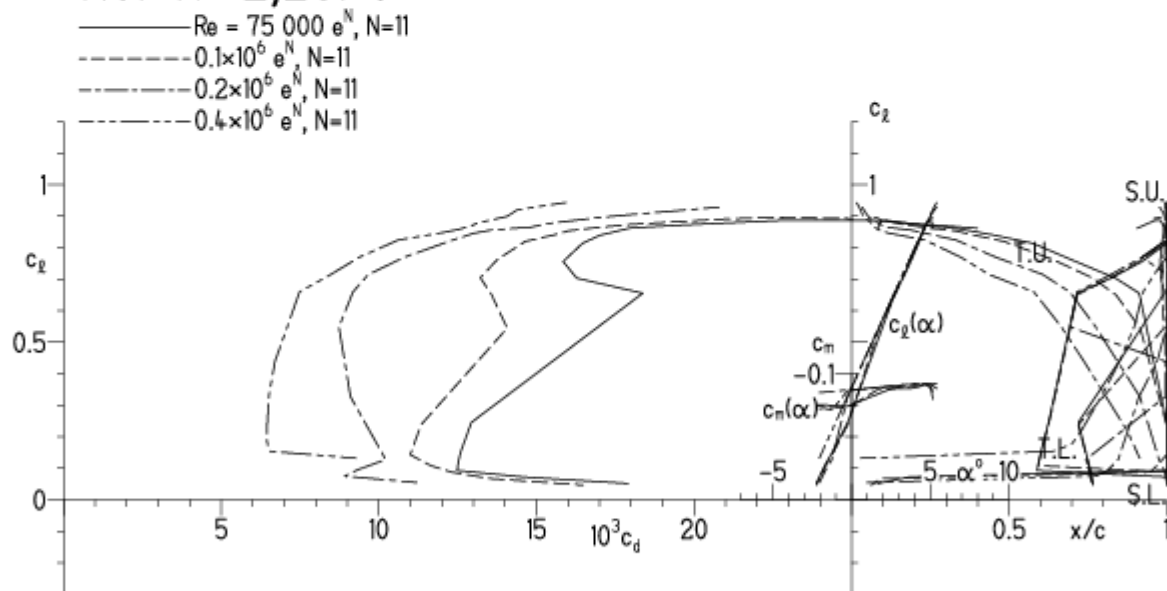
HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

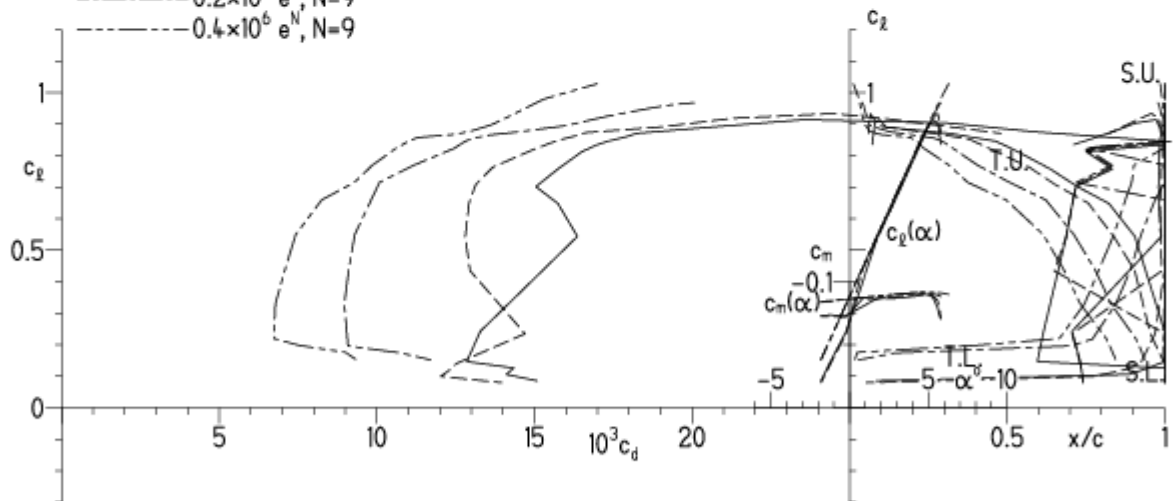
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2,25/8,5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

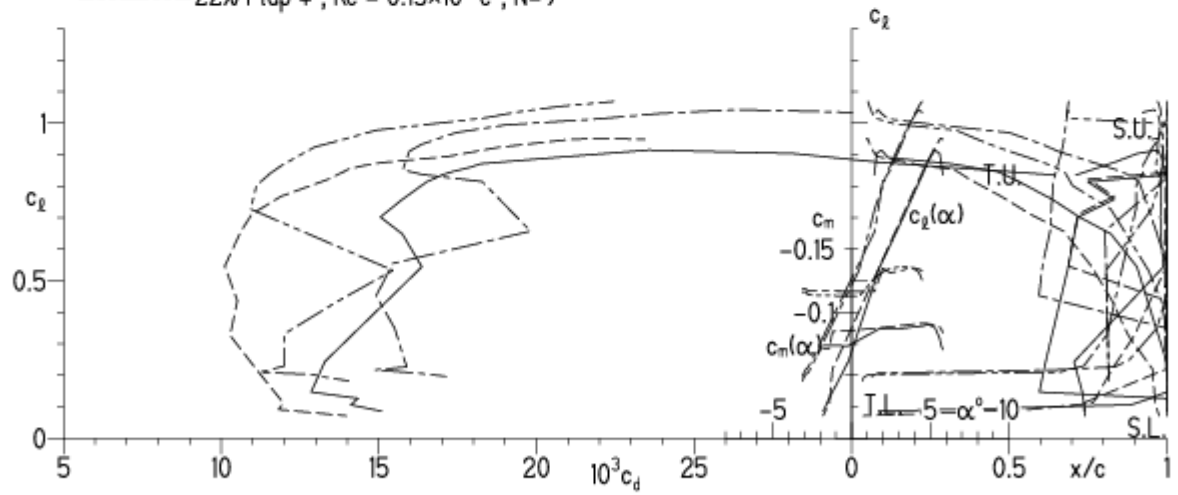


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



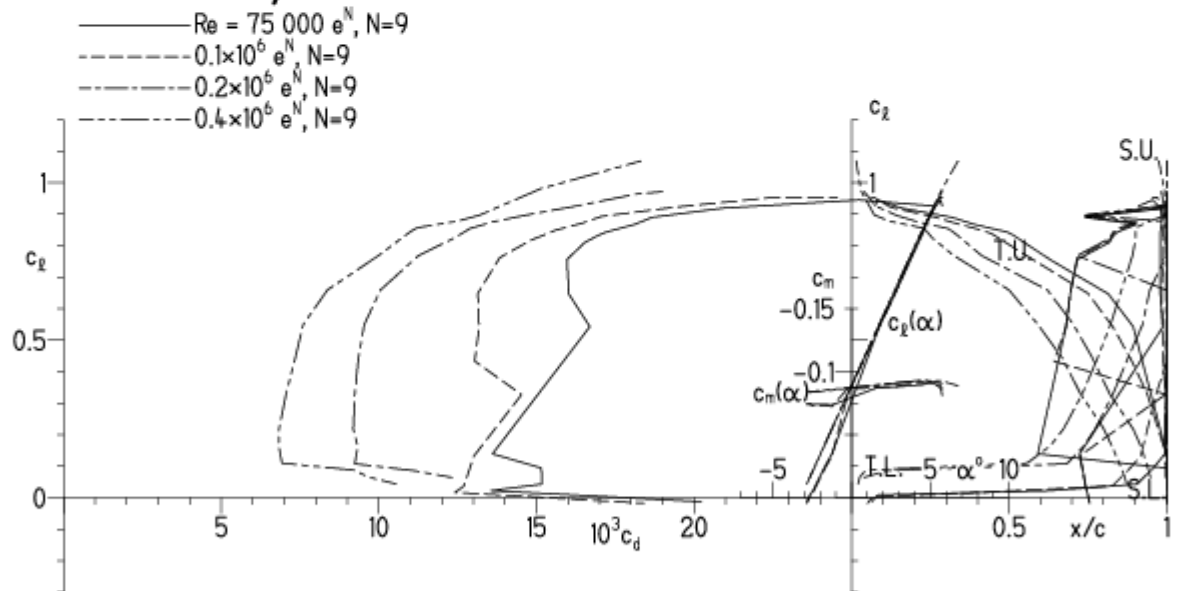
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



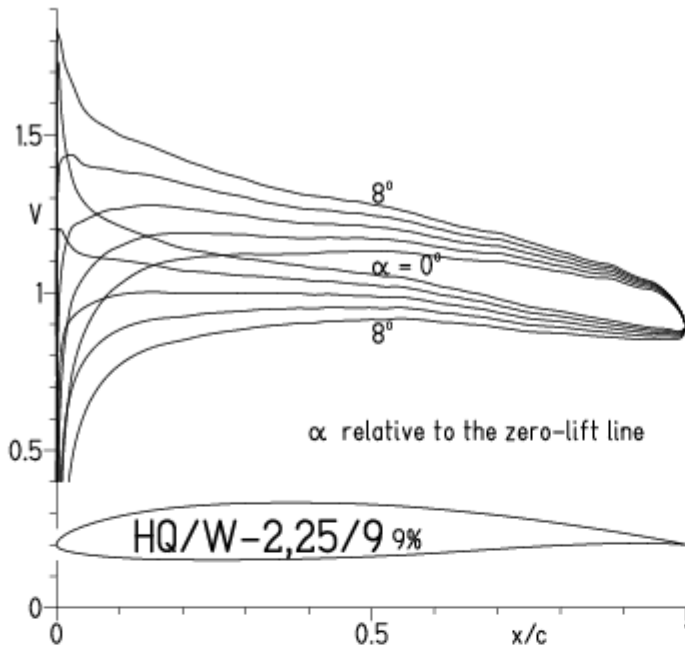
EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

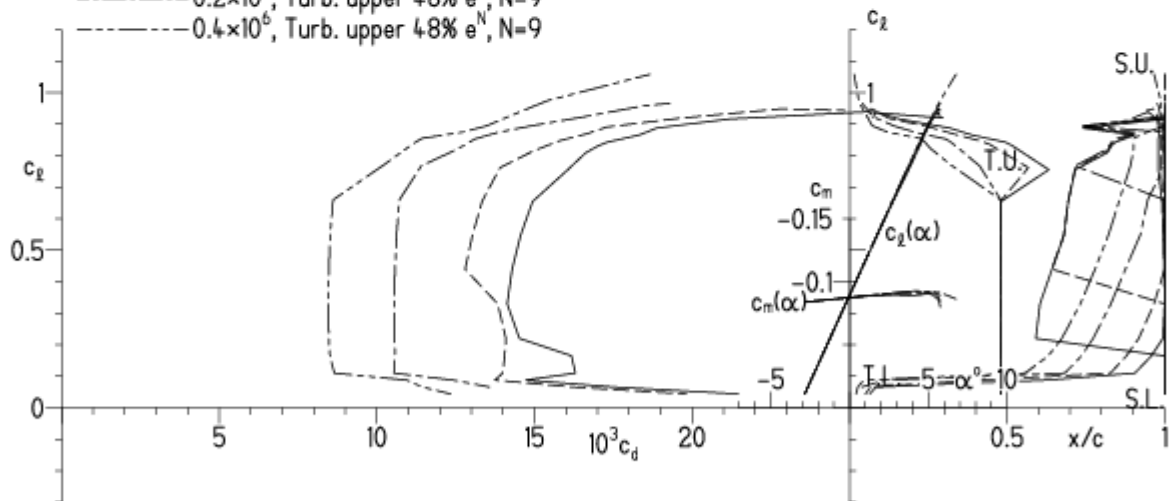
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2 × 10⁶ e^N, N=11
- - - 0.6 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.2 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.6 × 10⁶ e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

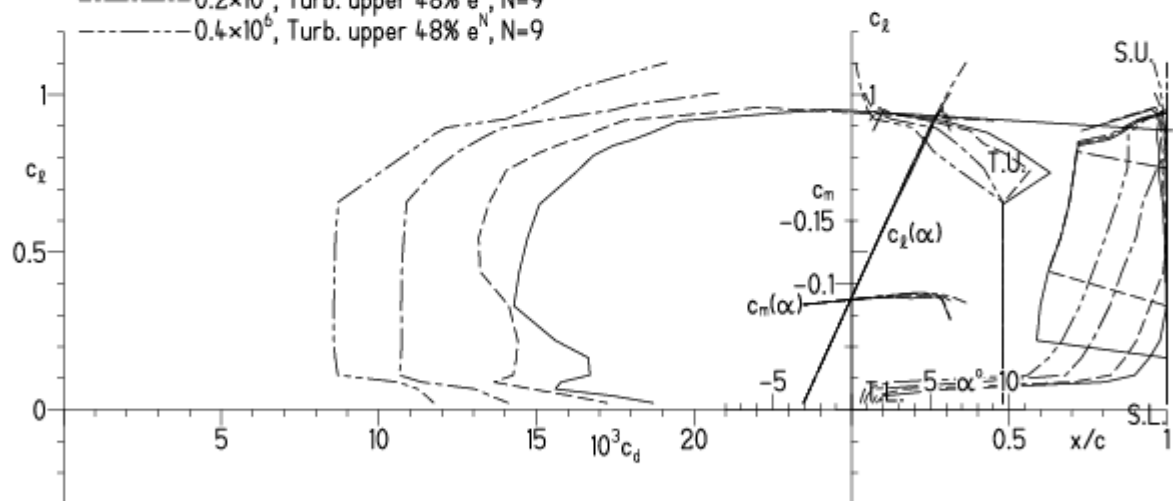
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
(Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

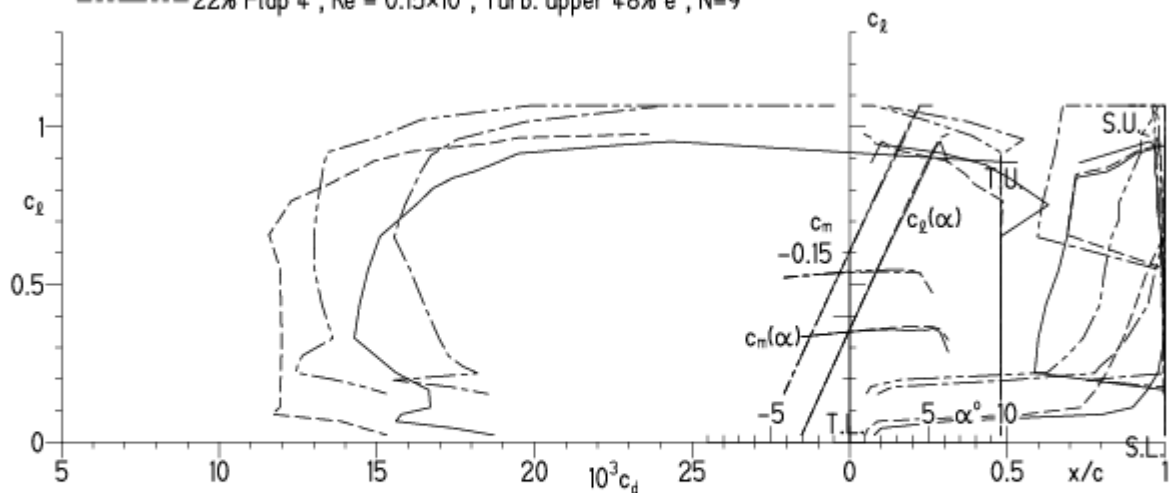


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



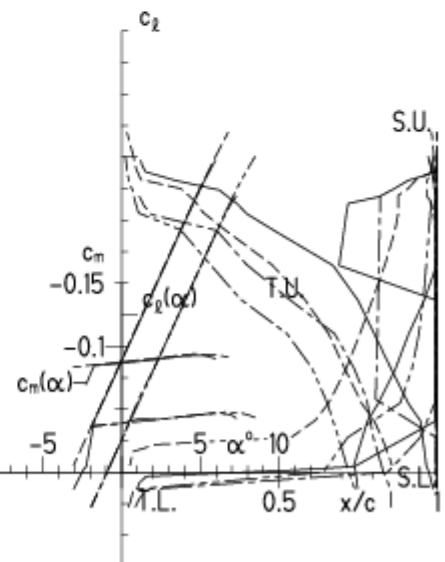
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

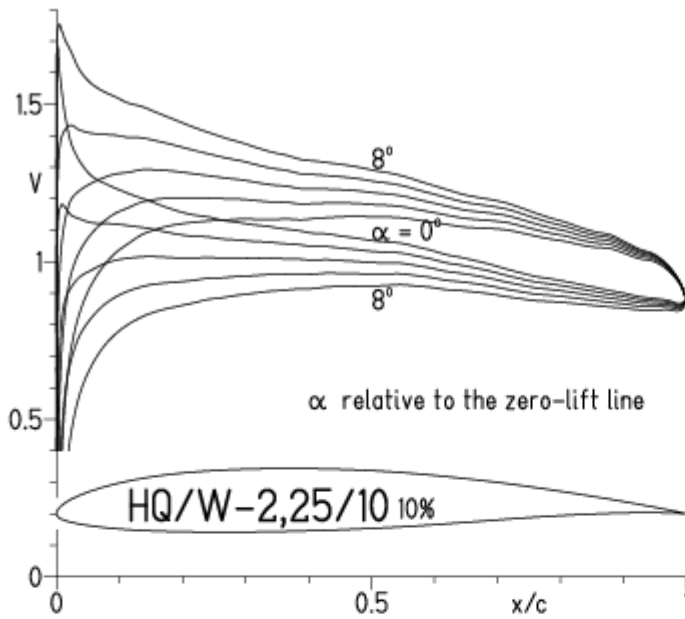


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

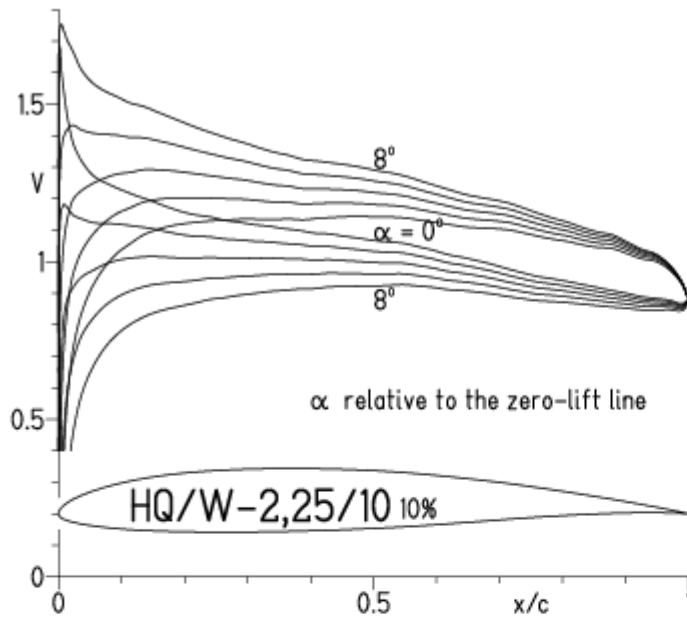


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

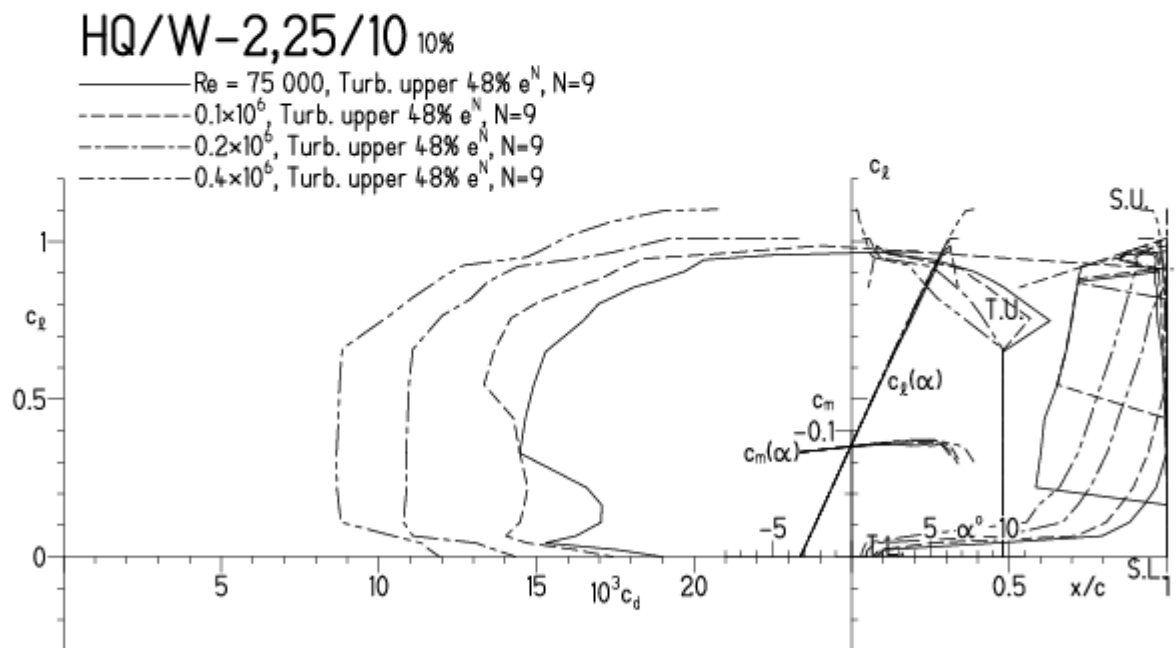


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

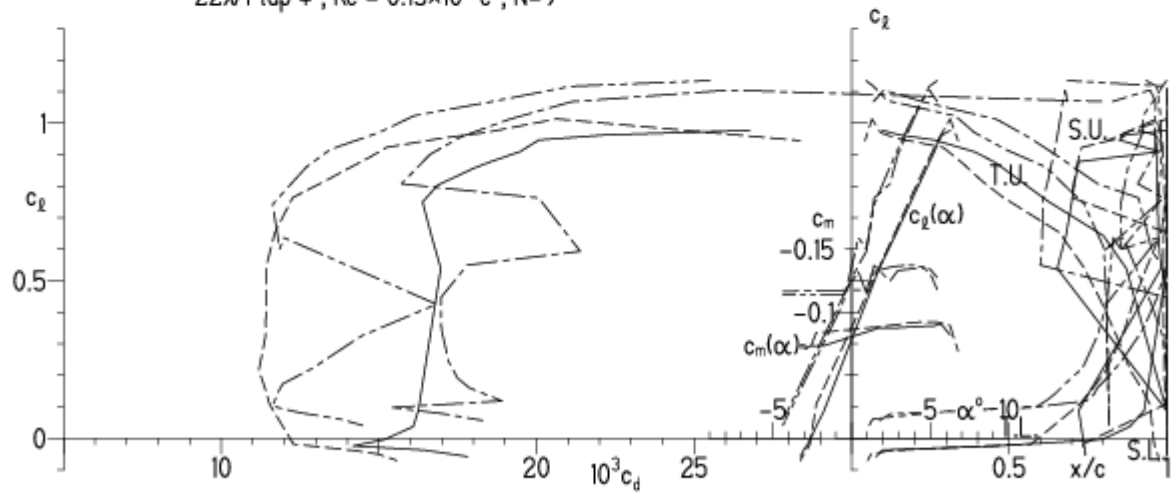


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

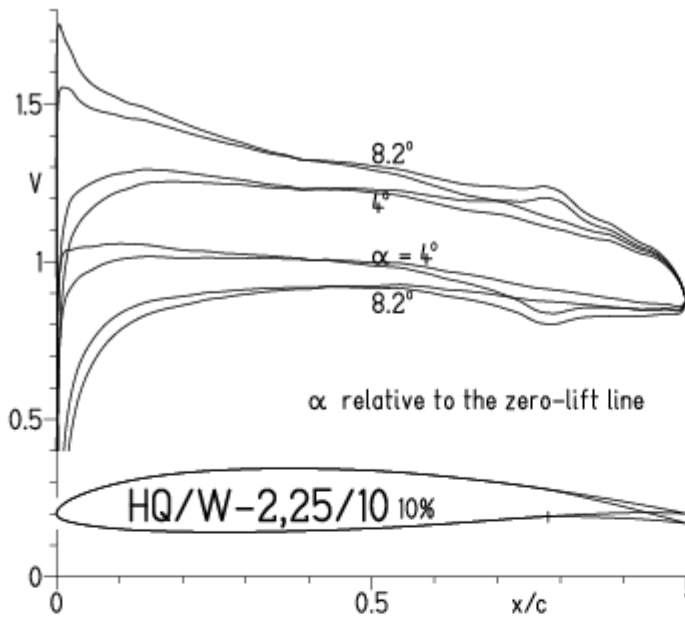
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

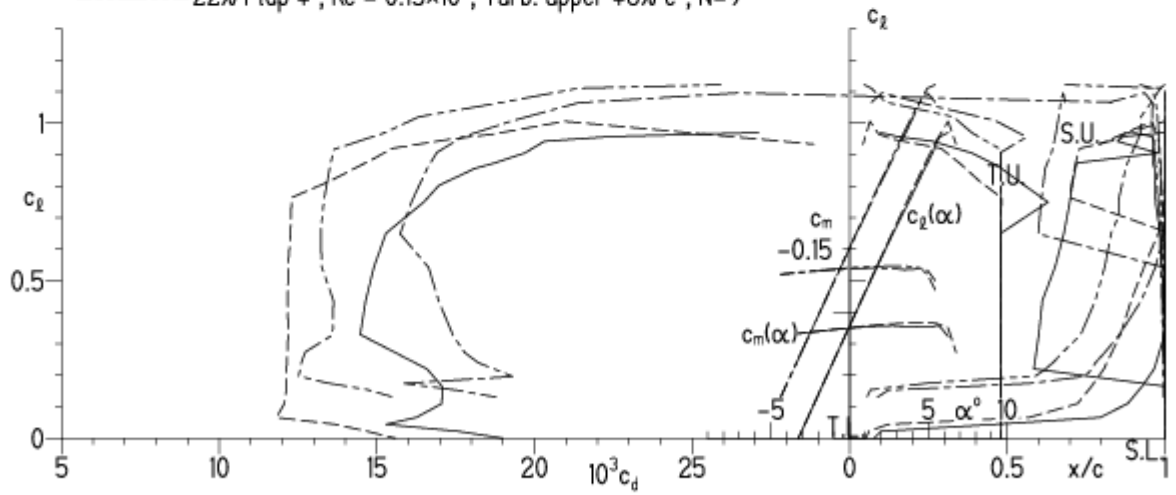


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

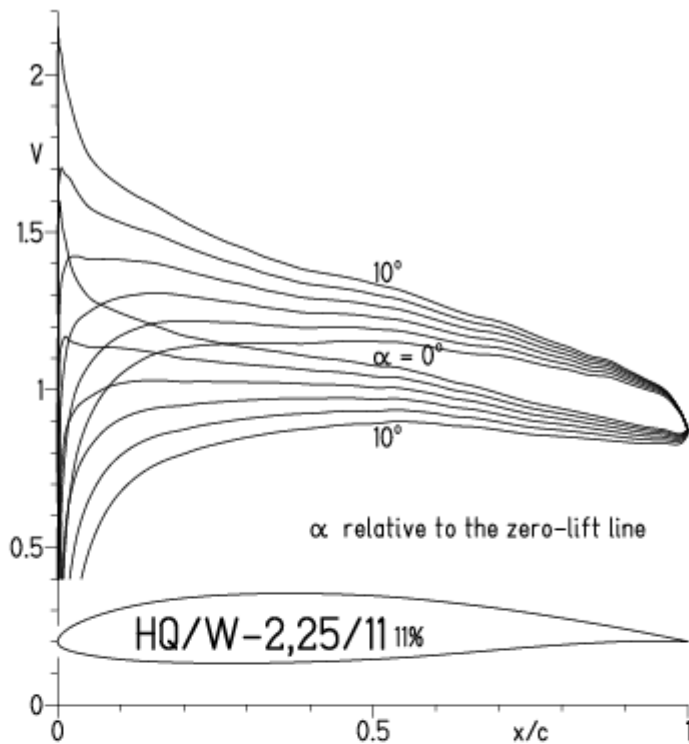


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6$, e^N , $N=9$
- - - 0.2×10^6 , e^N , $N=9$
- · - 0.4×10^6 , e^N , $N=9$
- · - · 0.8×10^6 , e^N , $N=9$
- · - · - 1.6×10^6 , e^N , $N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

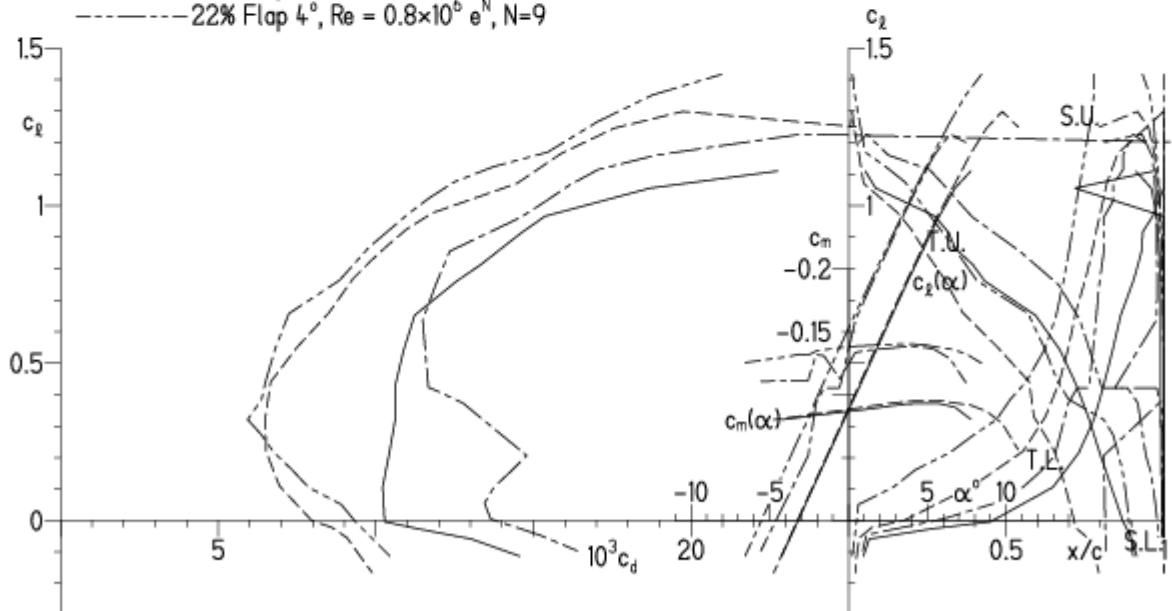


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11

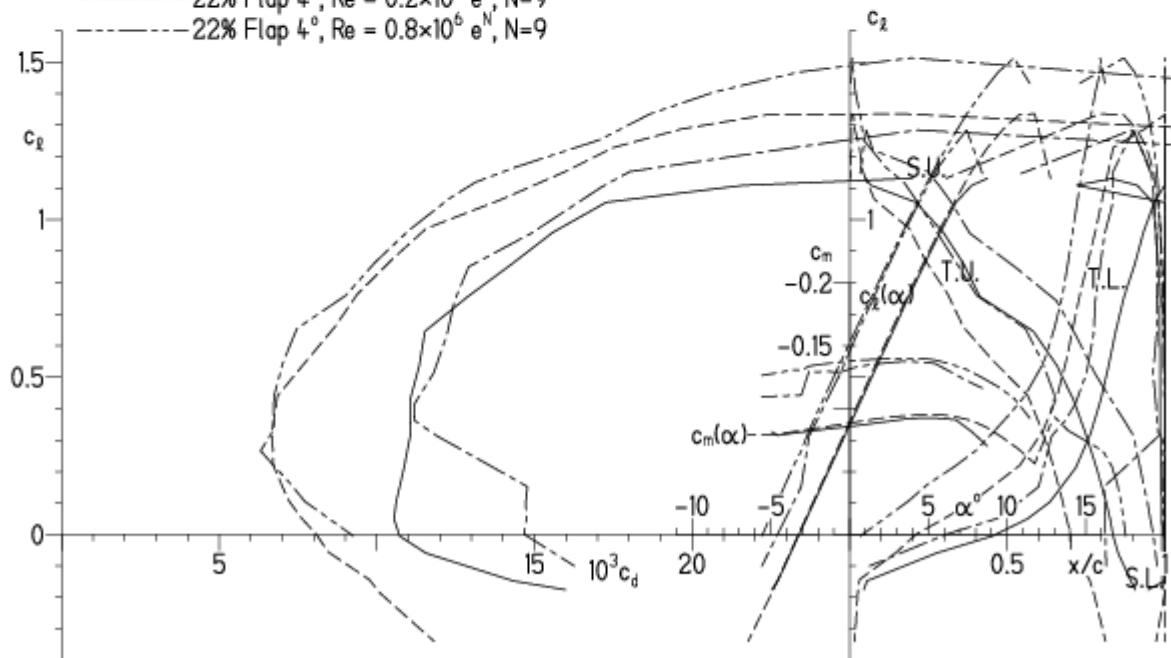


EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

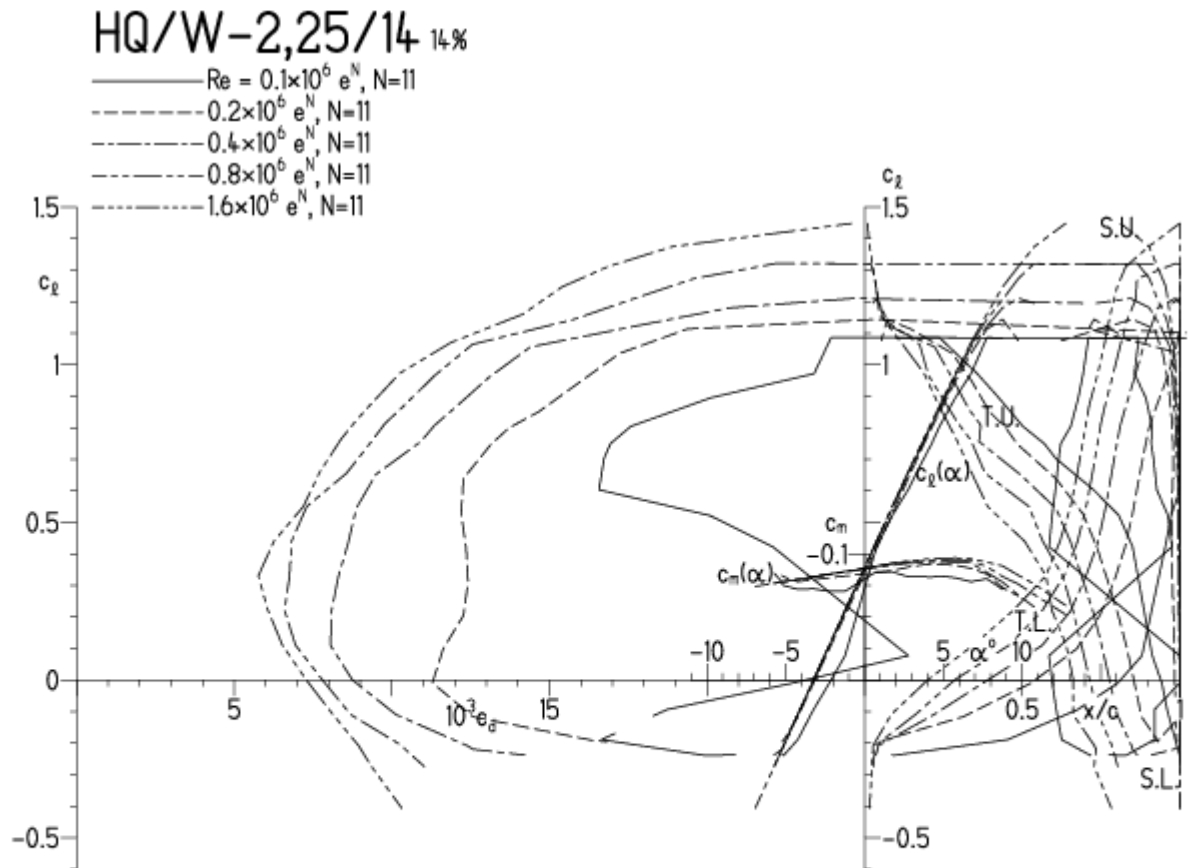


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

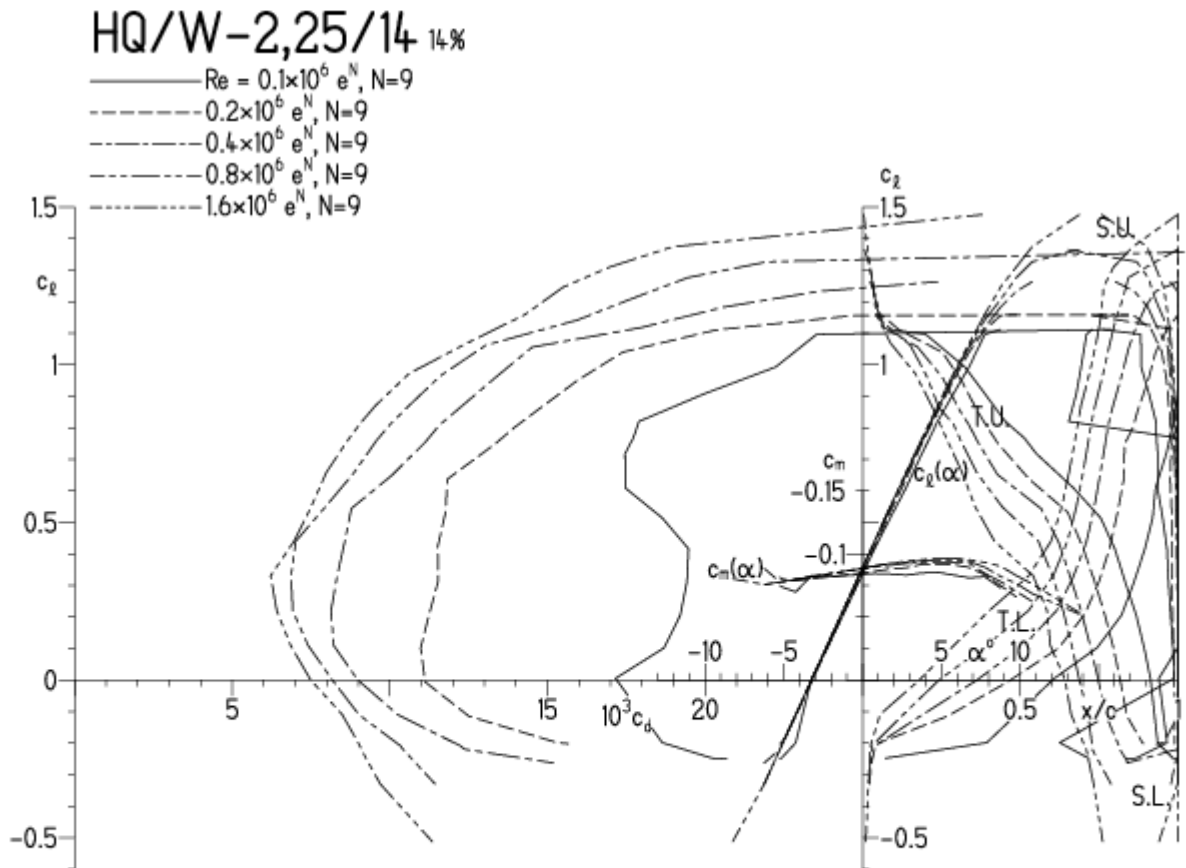


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

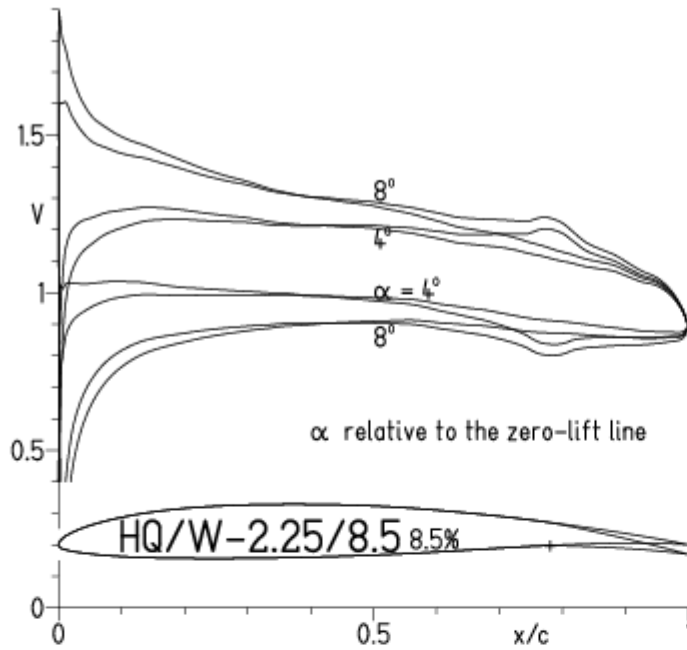
HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

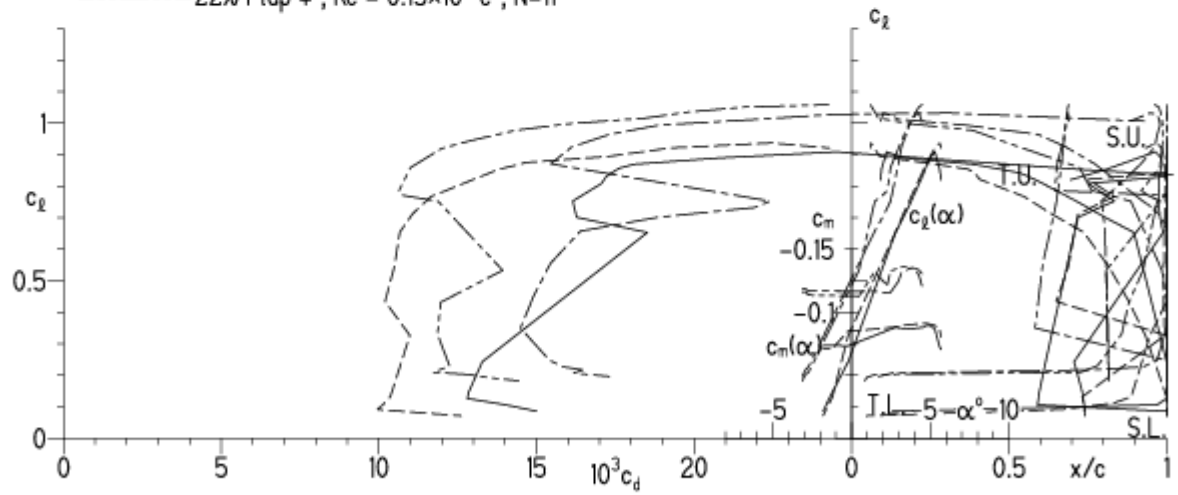


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



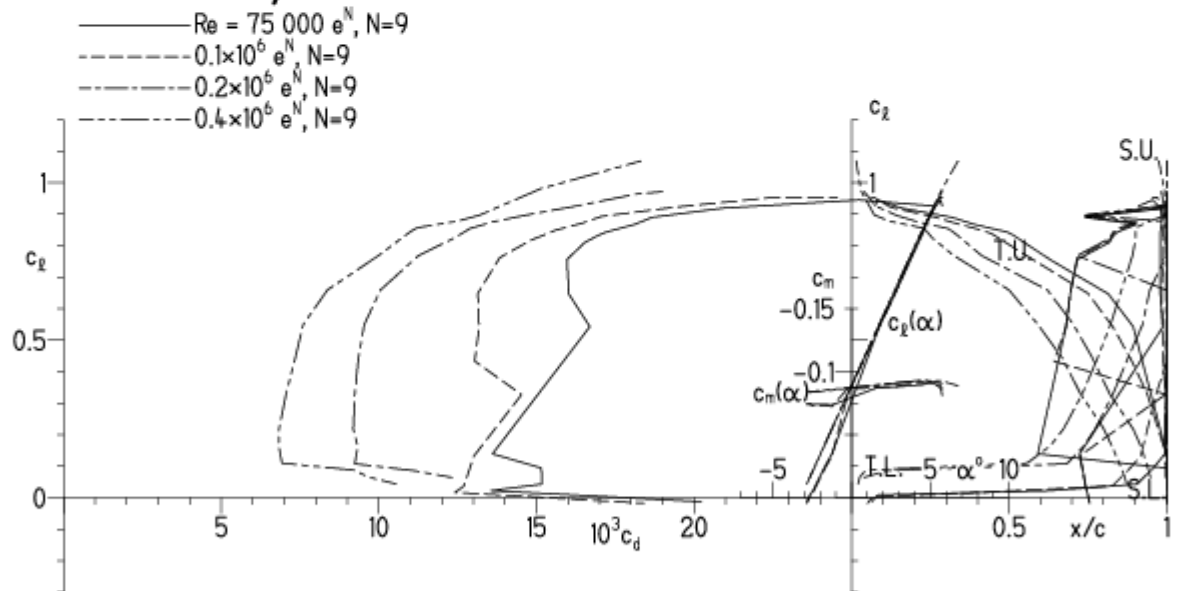
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

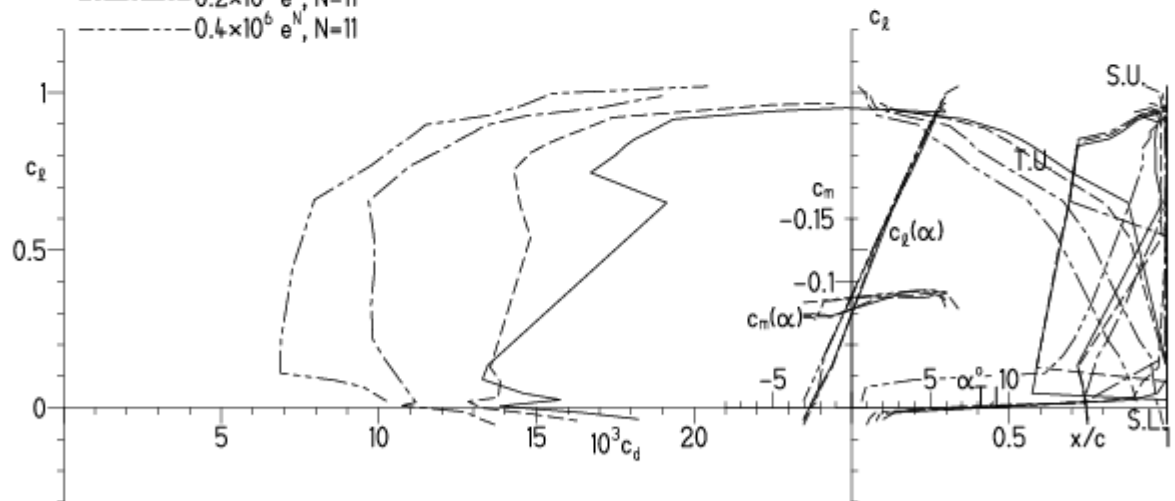
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

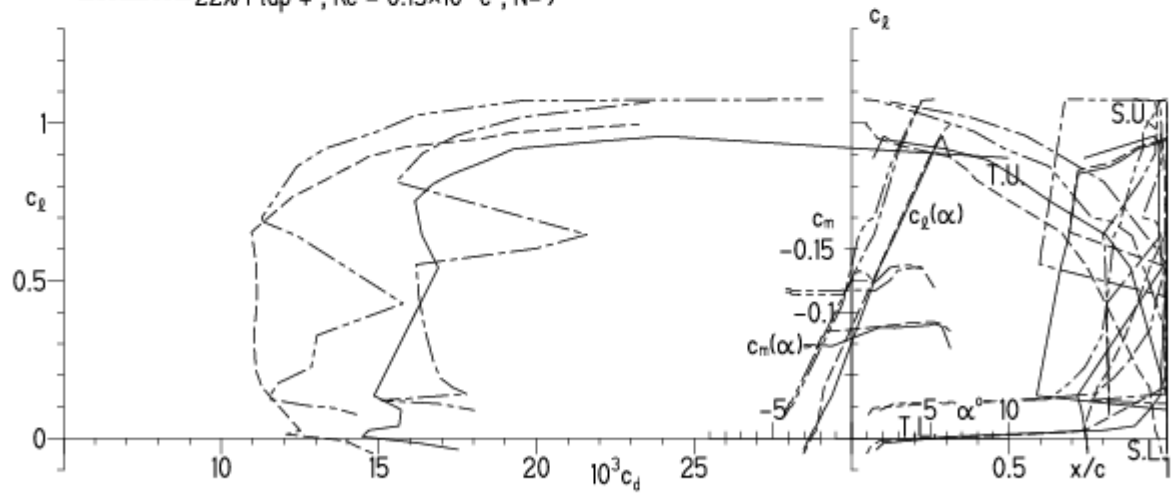


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

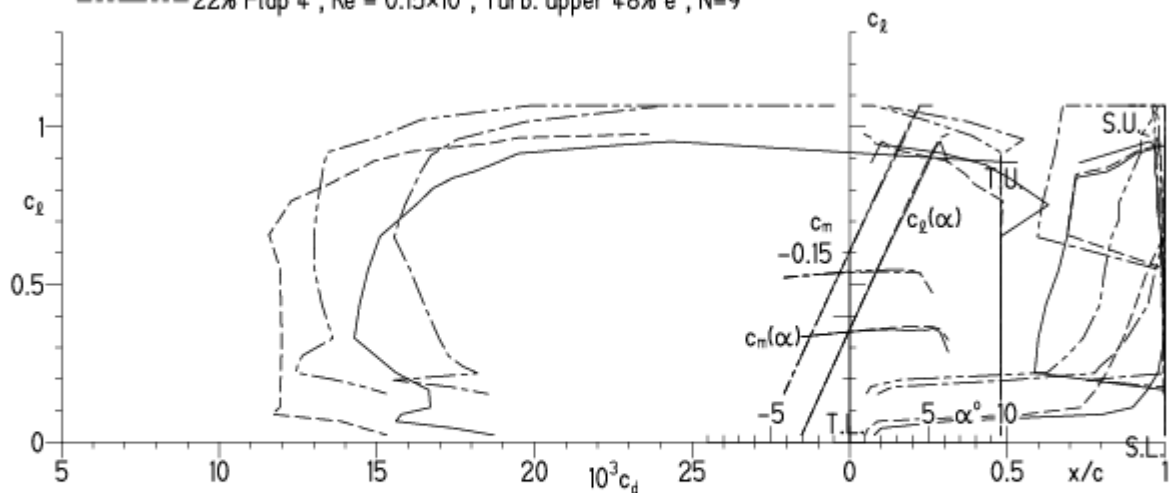


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

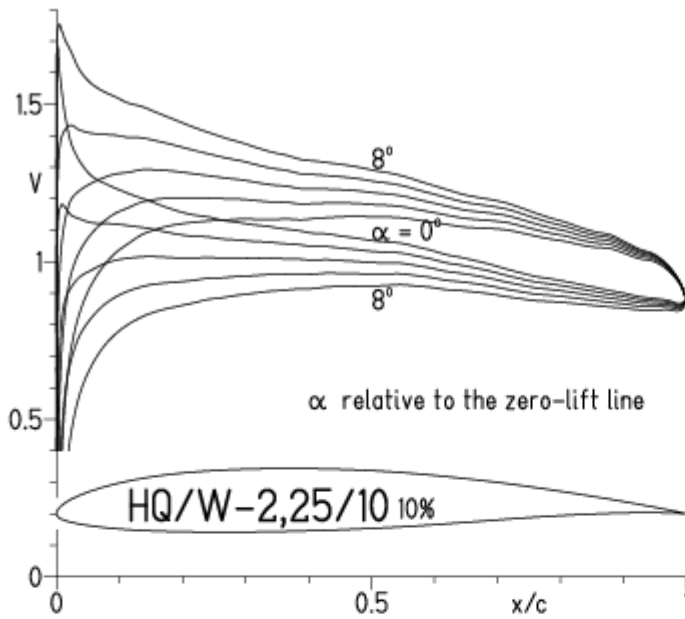


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

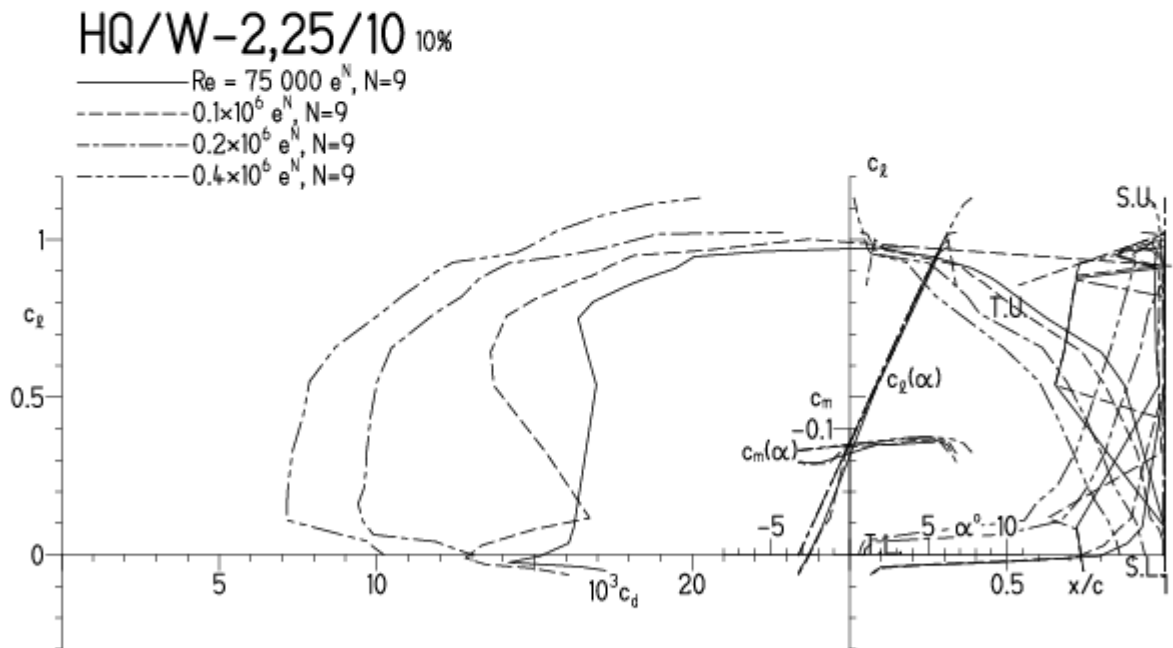


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

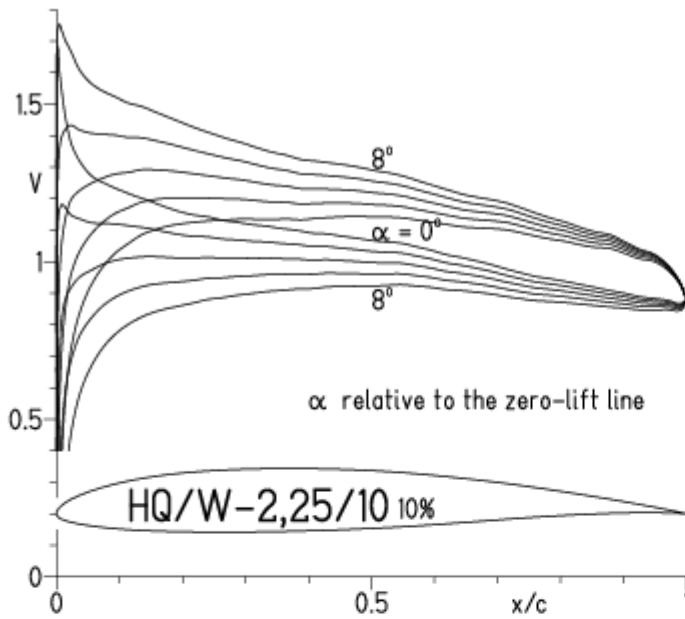


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

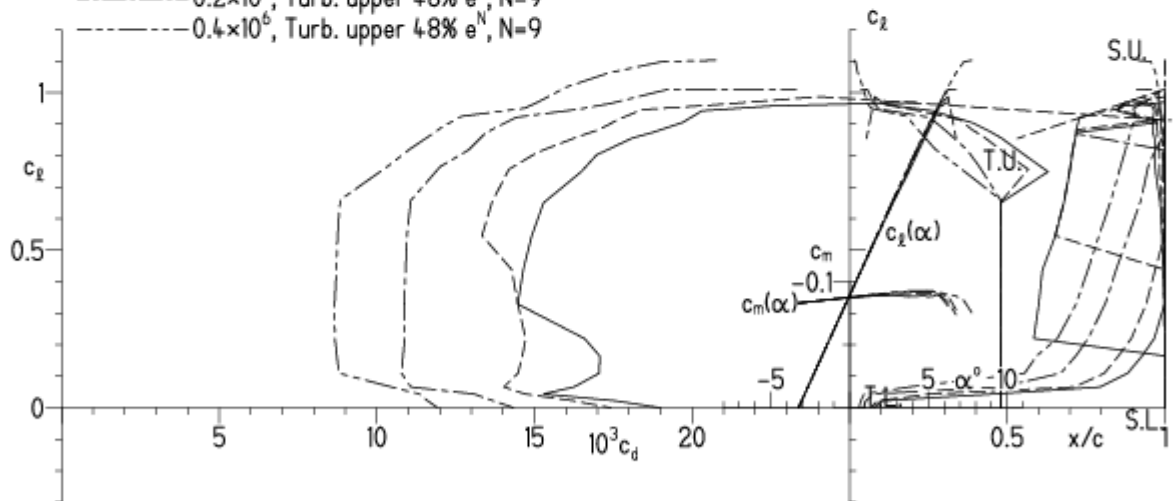
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

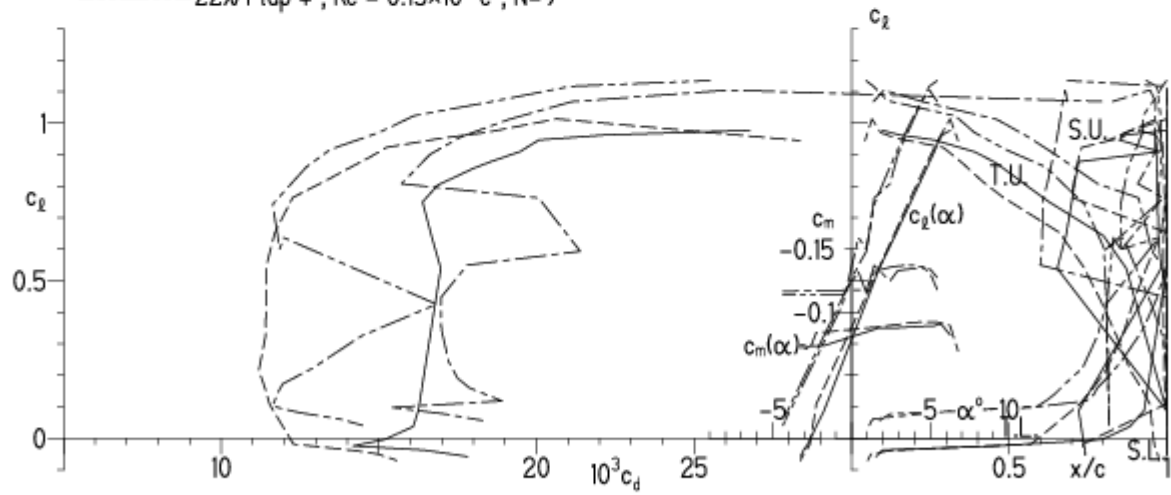


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

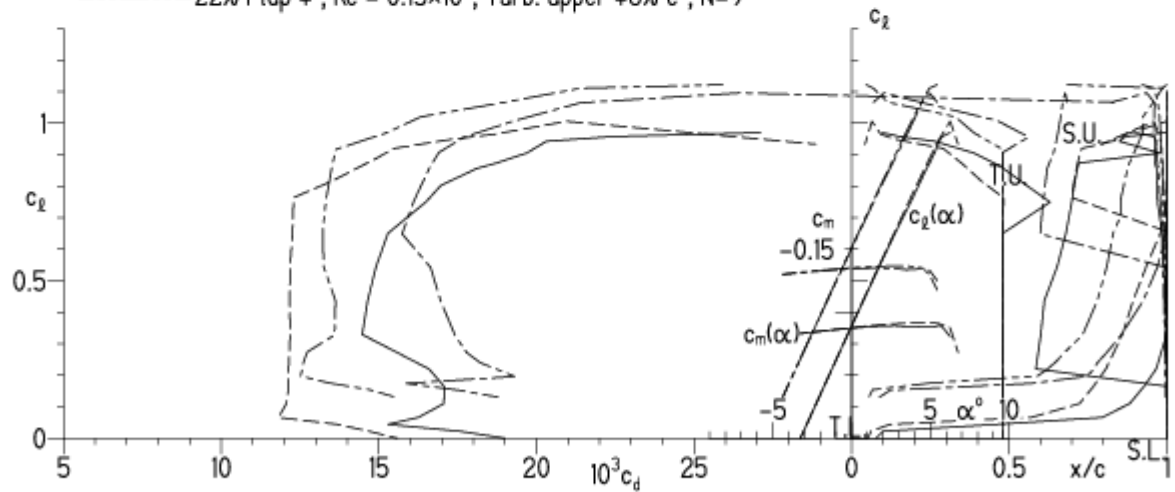


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

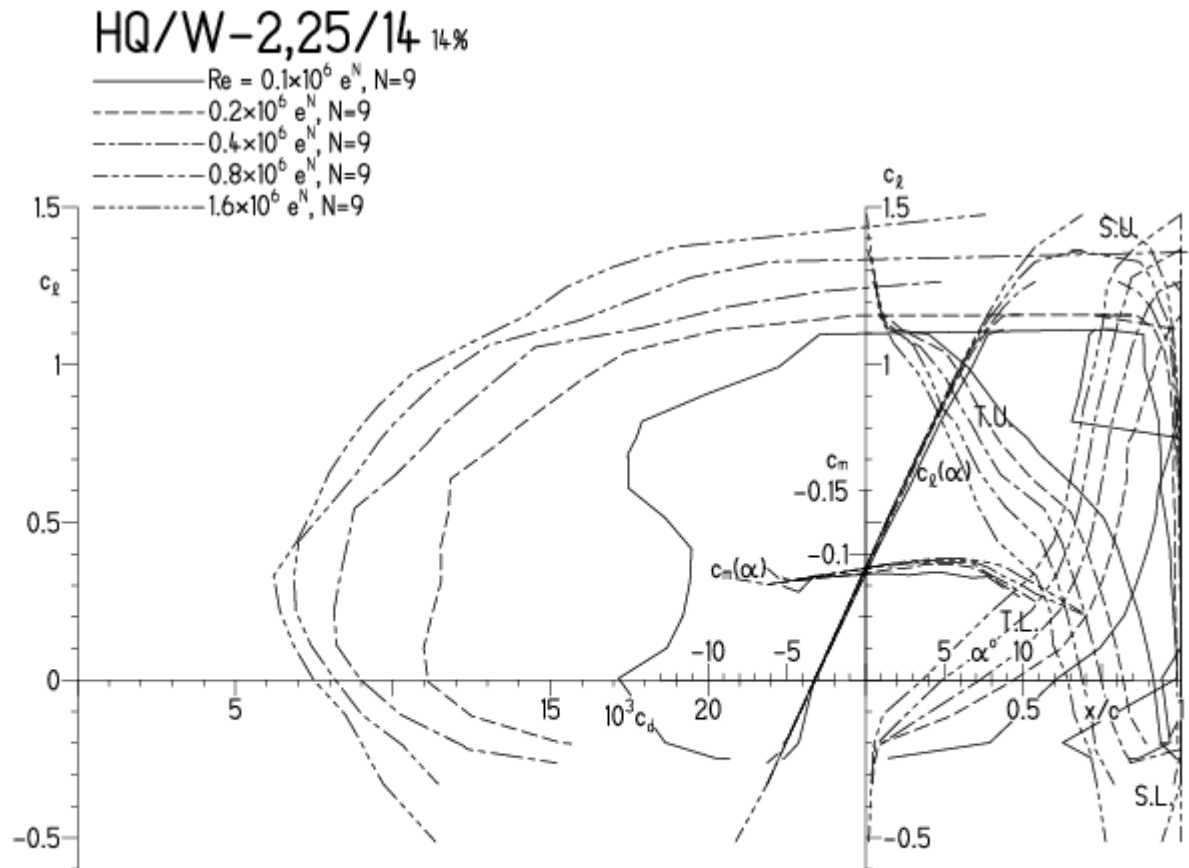


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

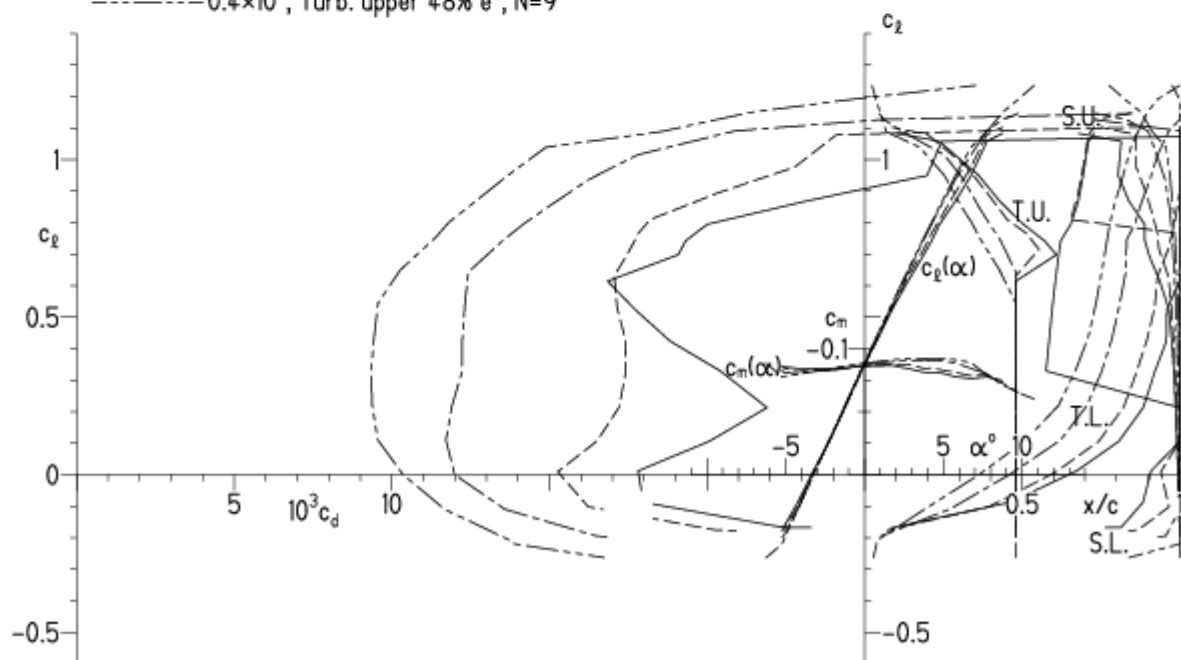
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

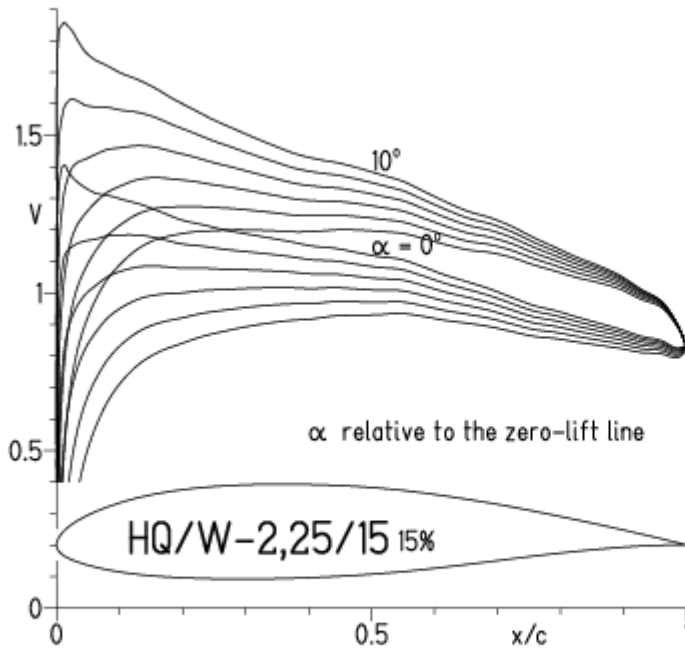


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

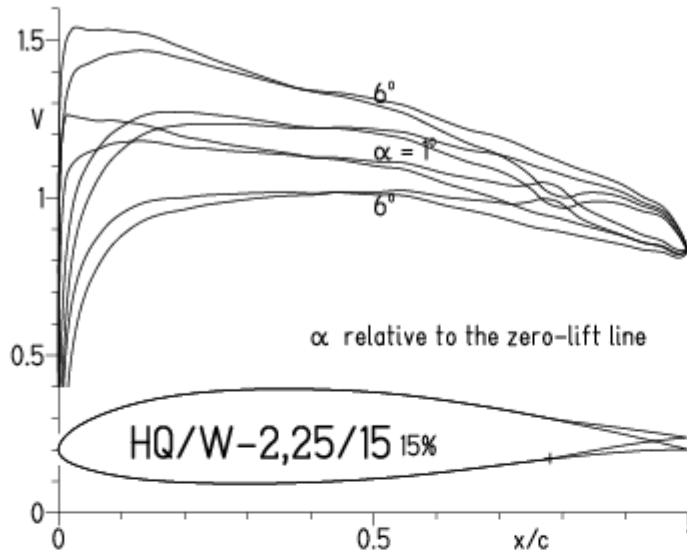


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

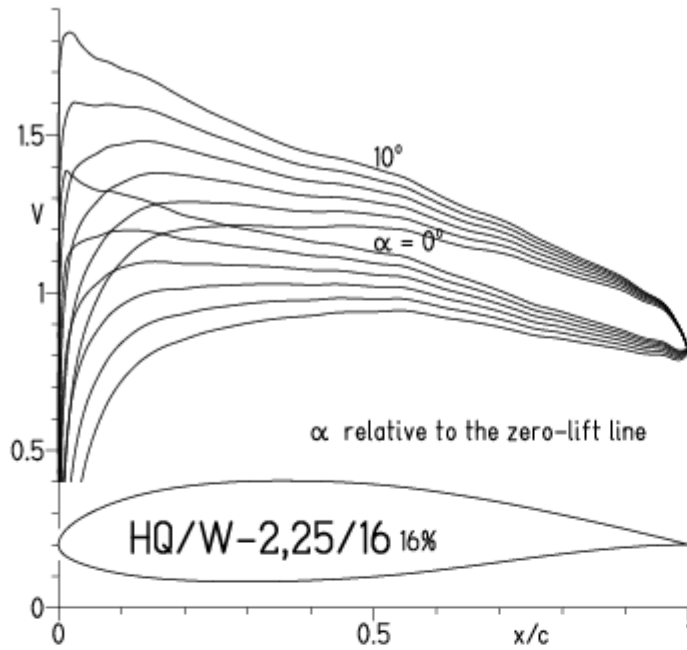
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · · - $0.8 \times 10^6 e^N, N=9$
- · · · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41

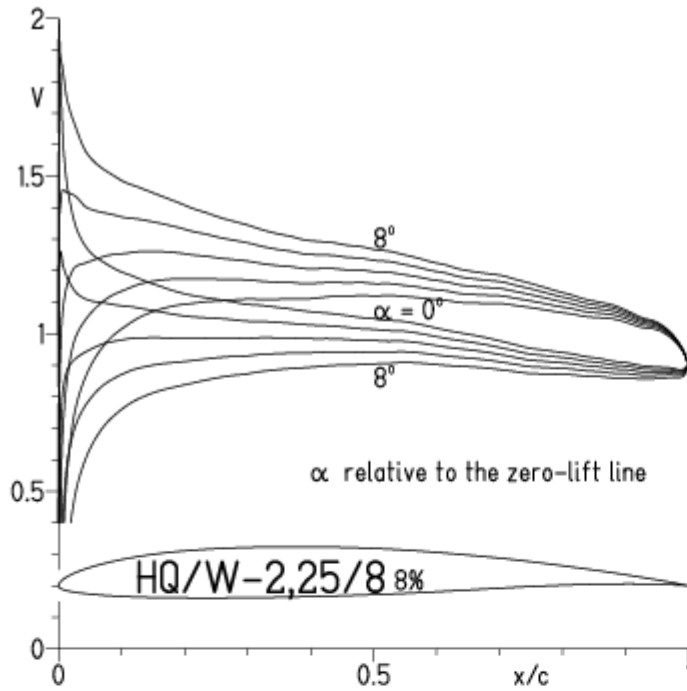


EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

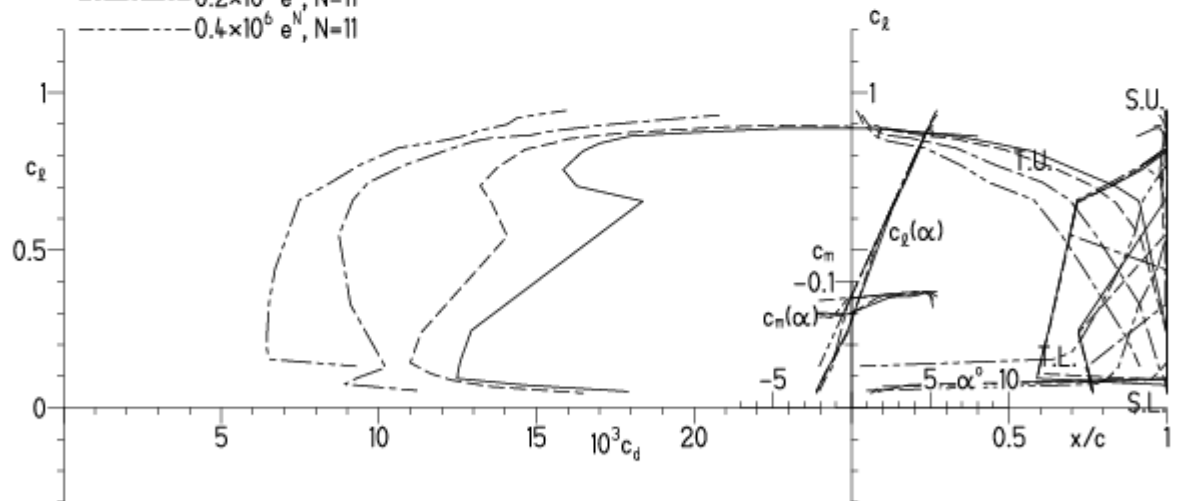
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

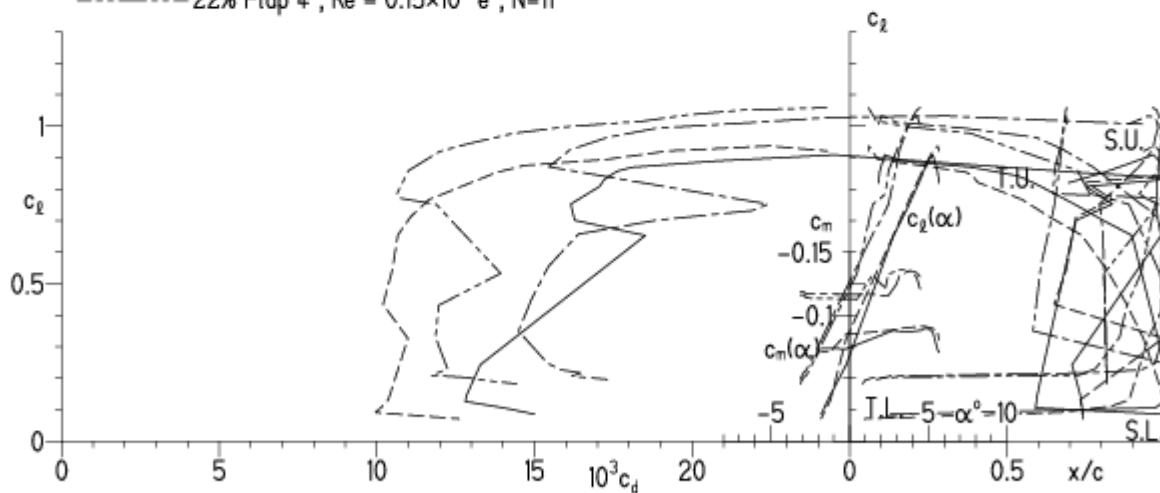


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

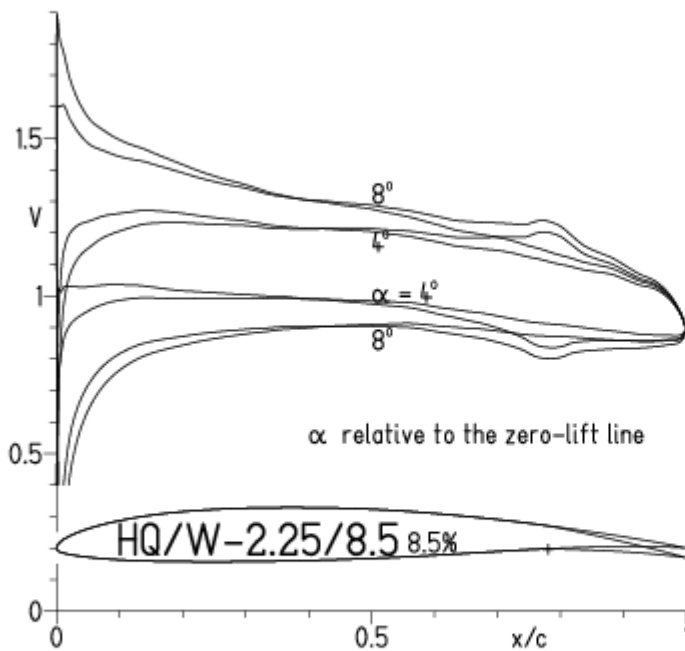
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

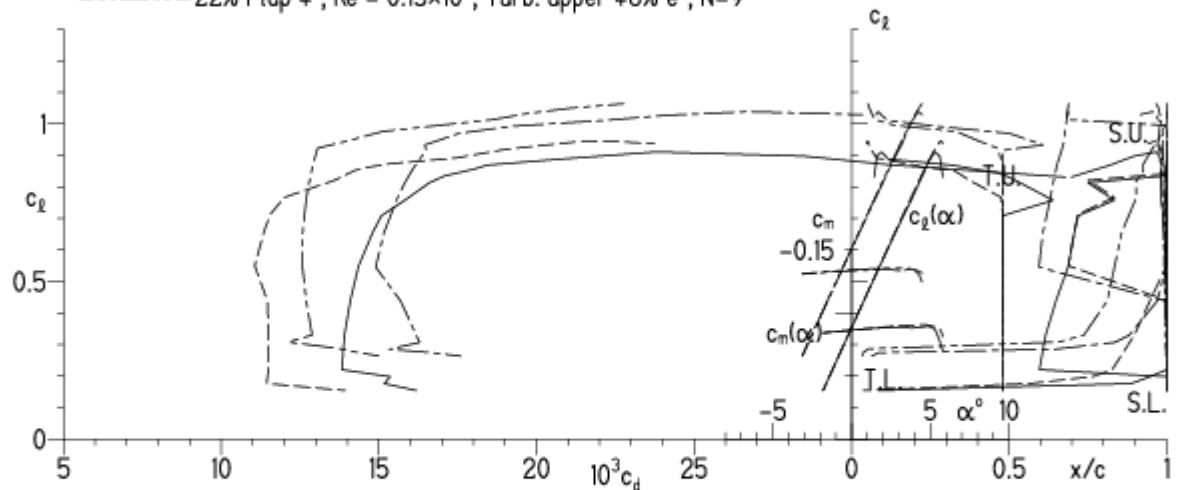


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

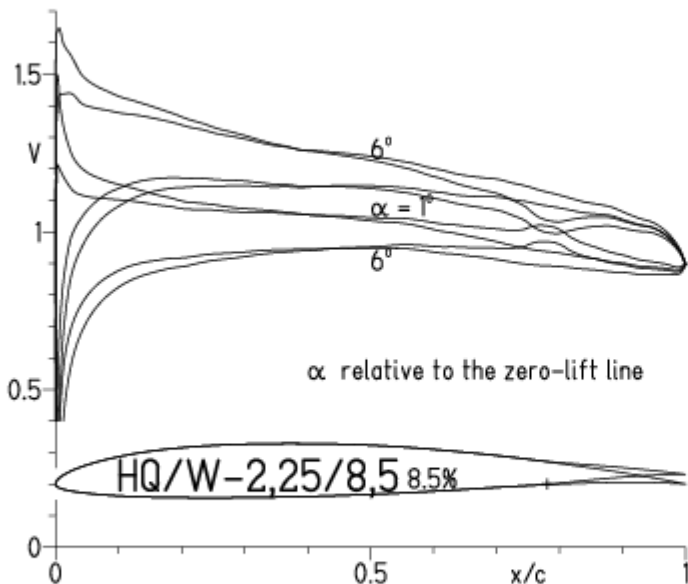
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$

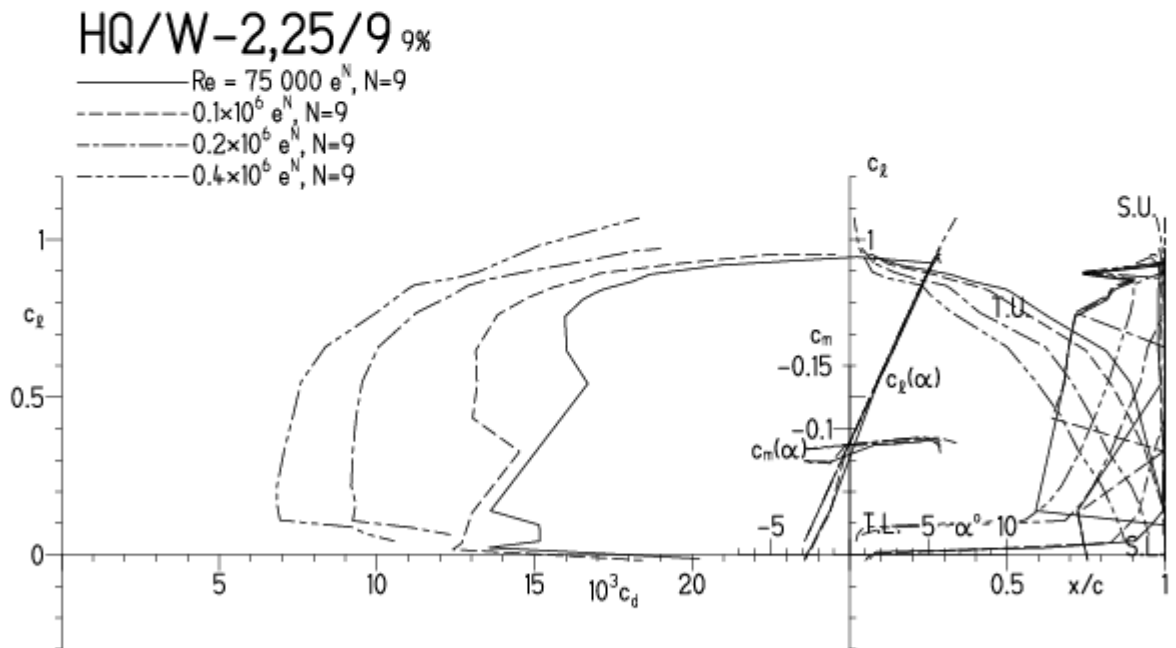


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

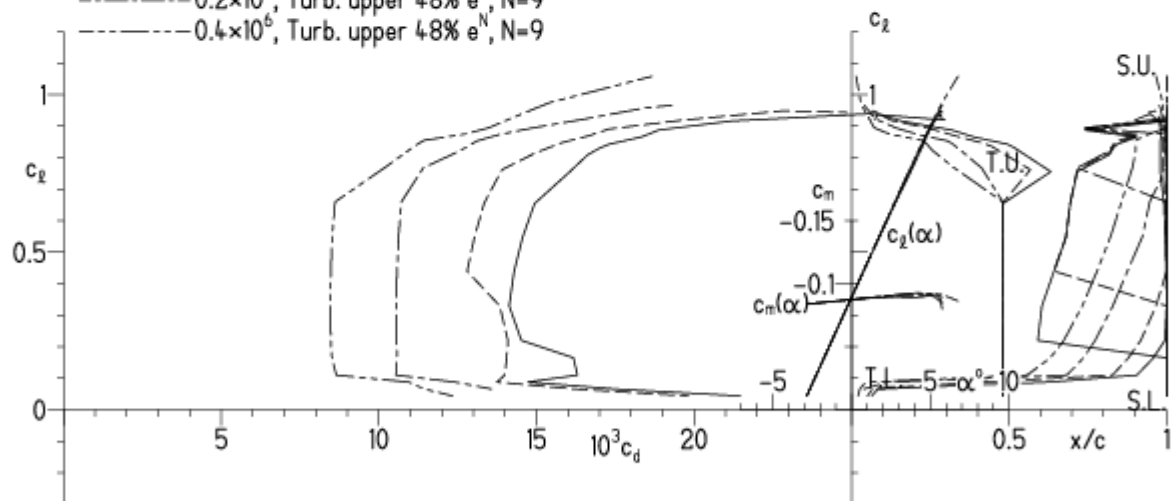
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

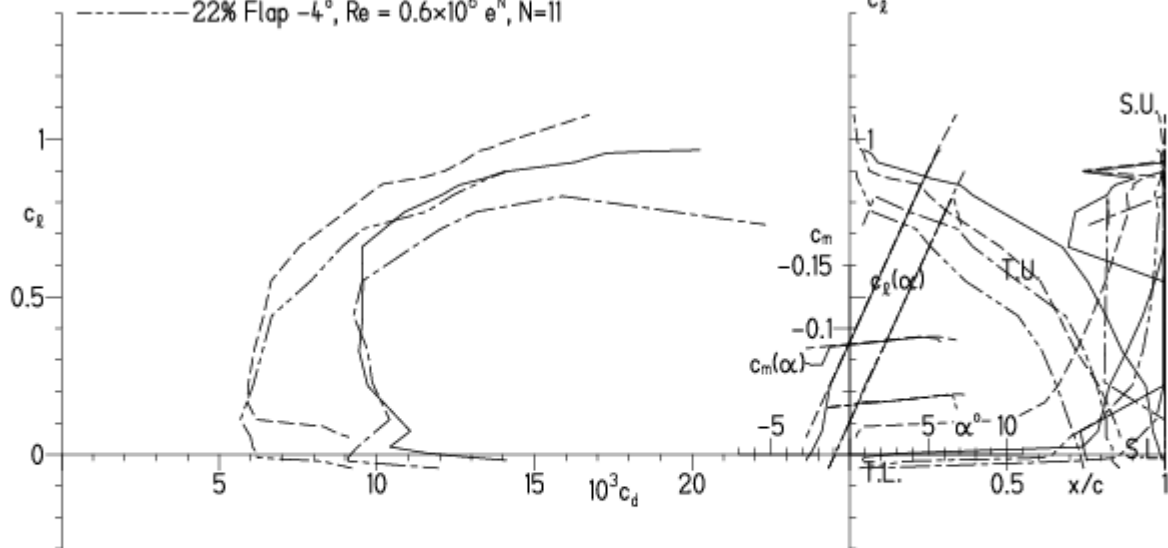
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2 × 10⁶ e^N, N=11
- - - 0.6 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.2 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.6 × 10⁶ e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



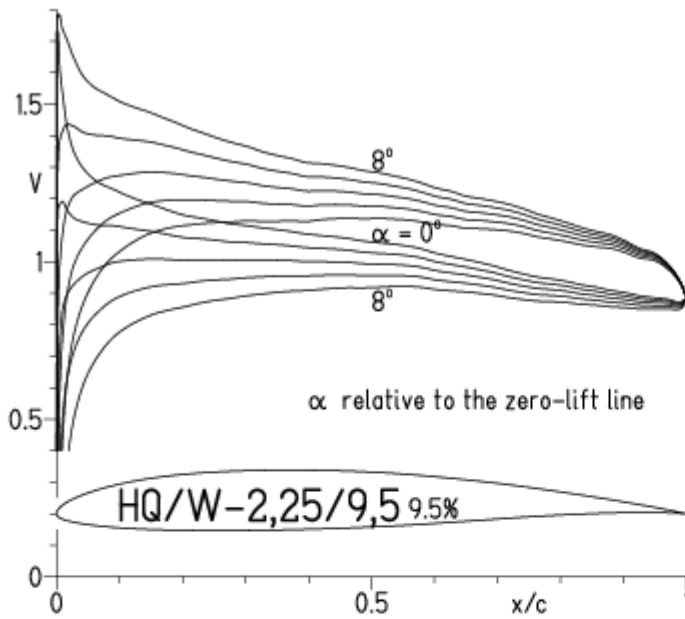
EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

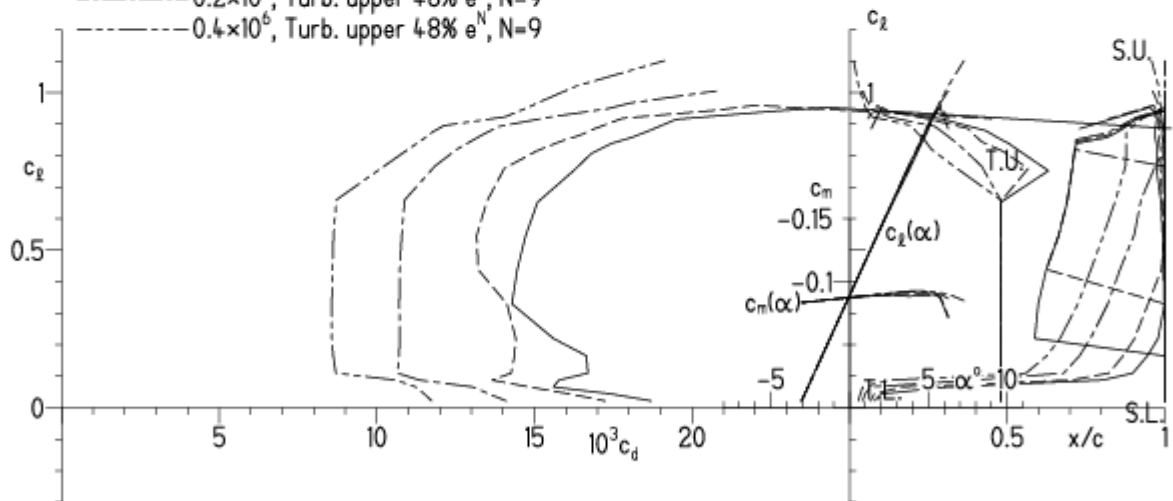
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

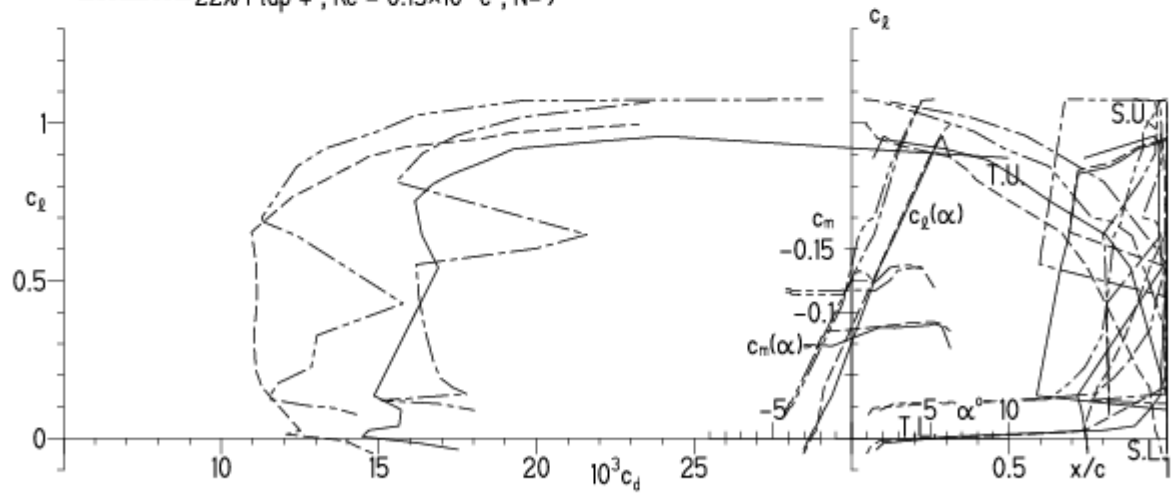


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

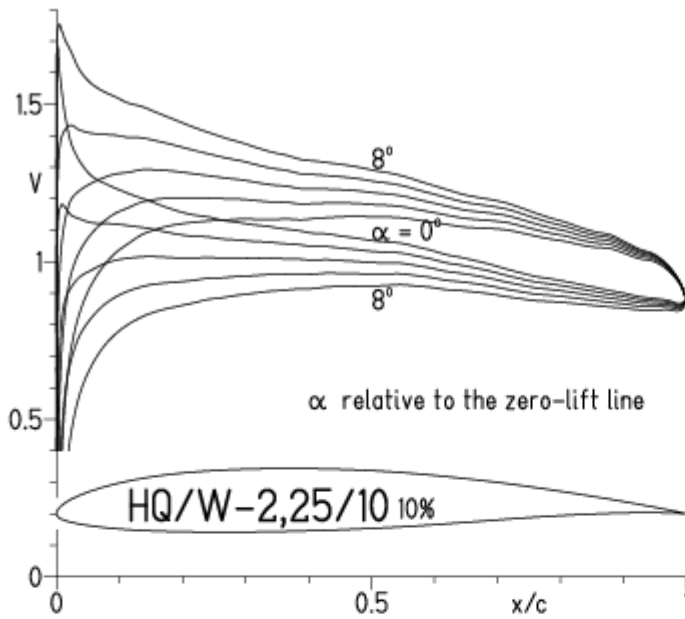


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

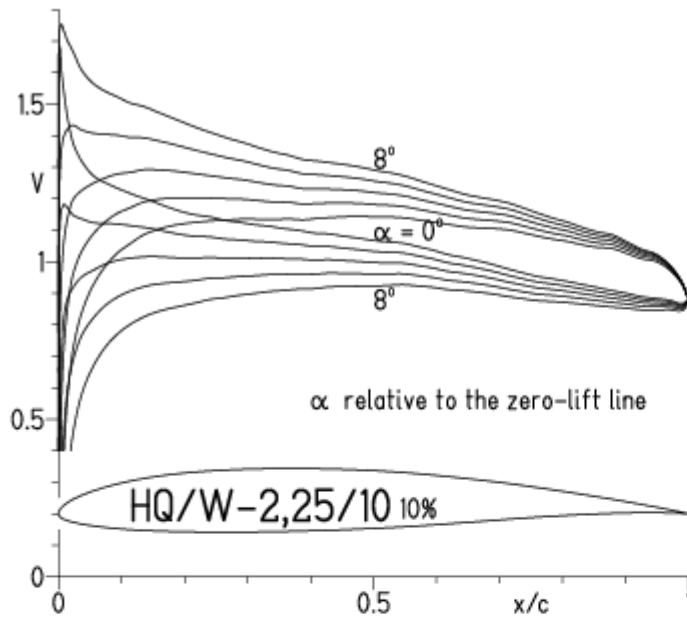


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

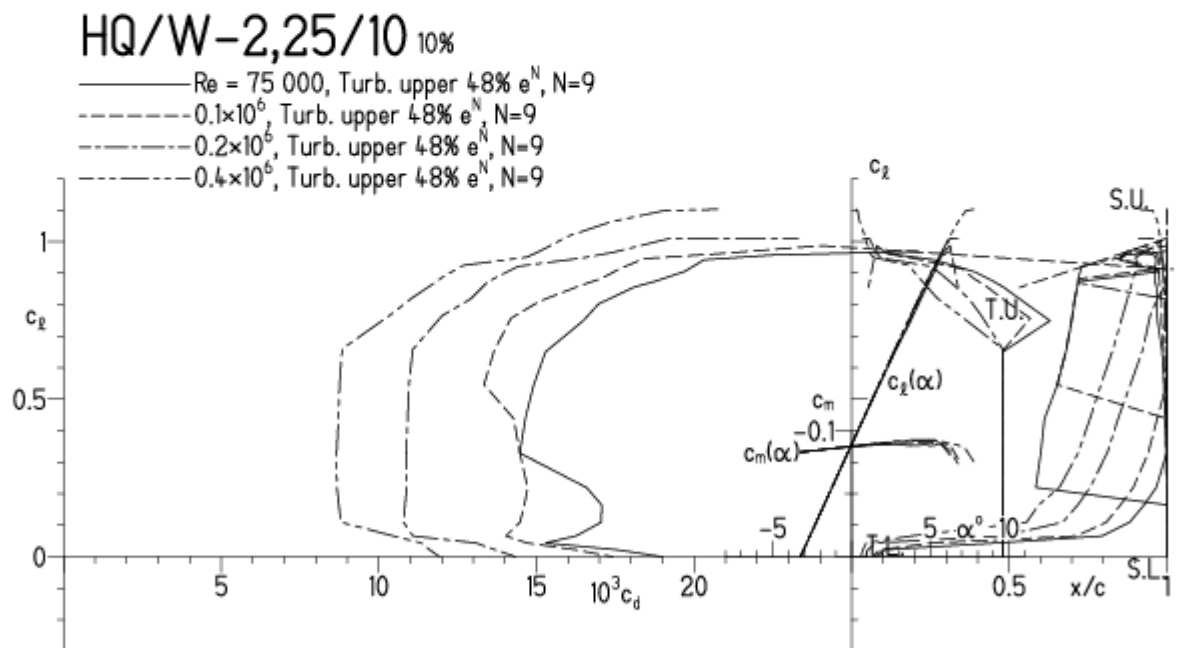


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

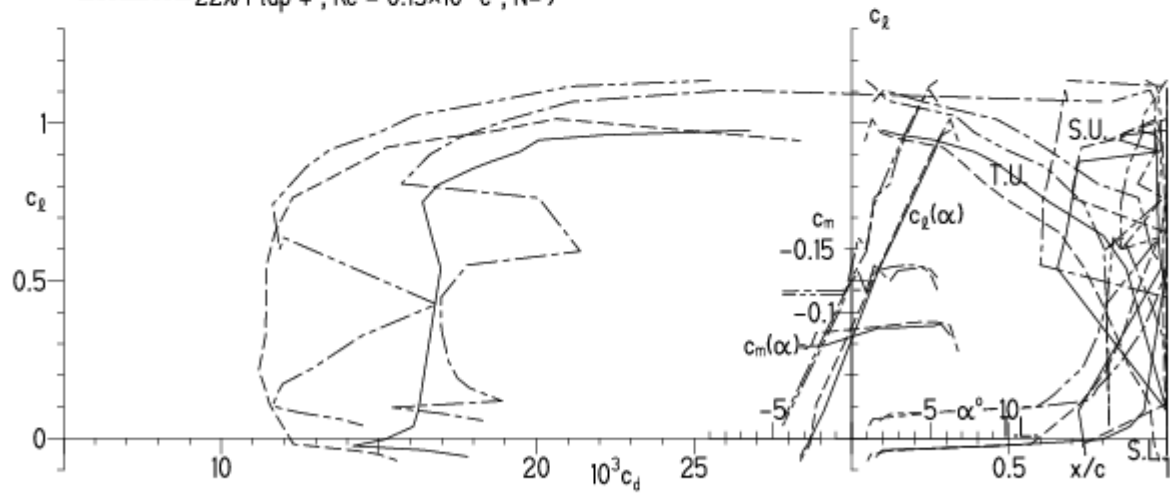


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

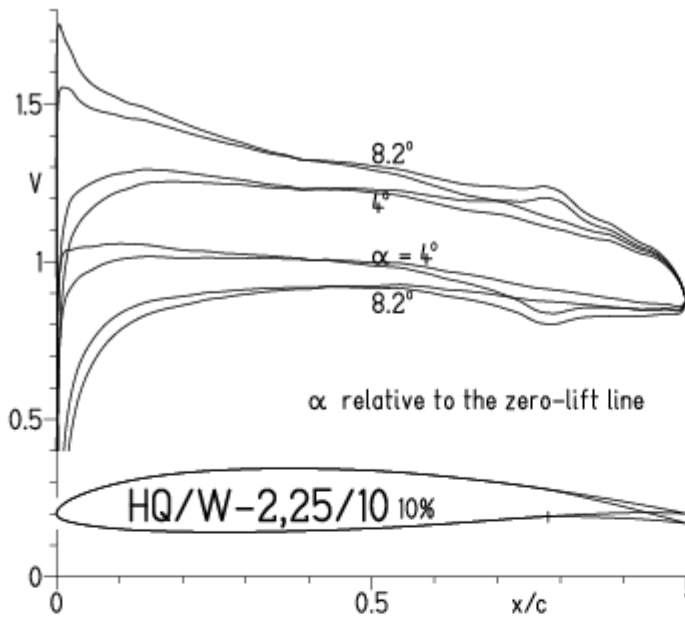
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

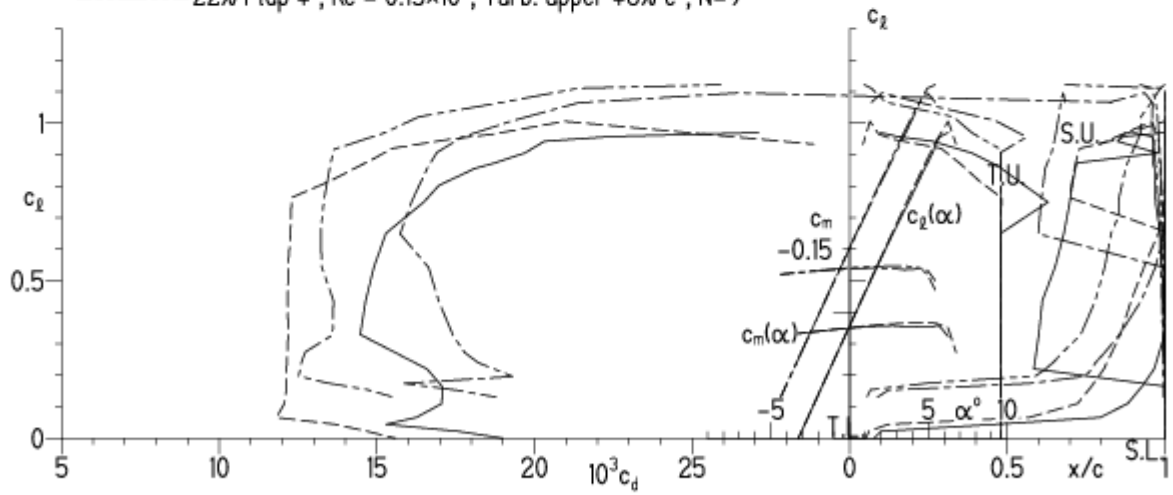


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

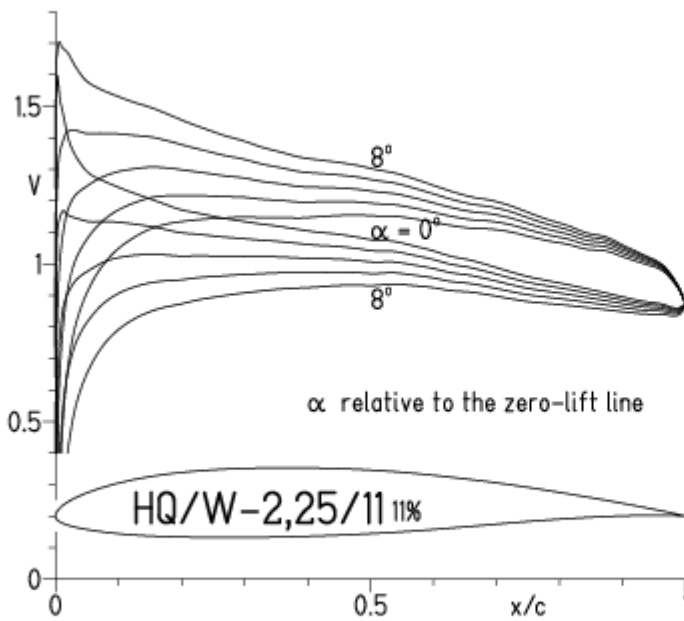


EPPLER 2005 V. 8.5.07 RUN

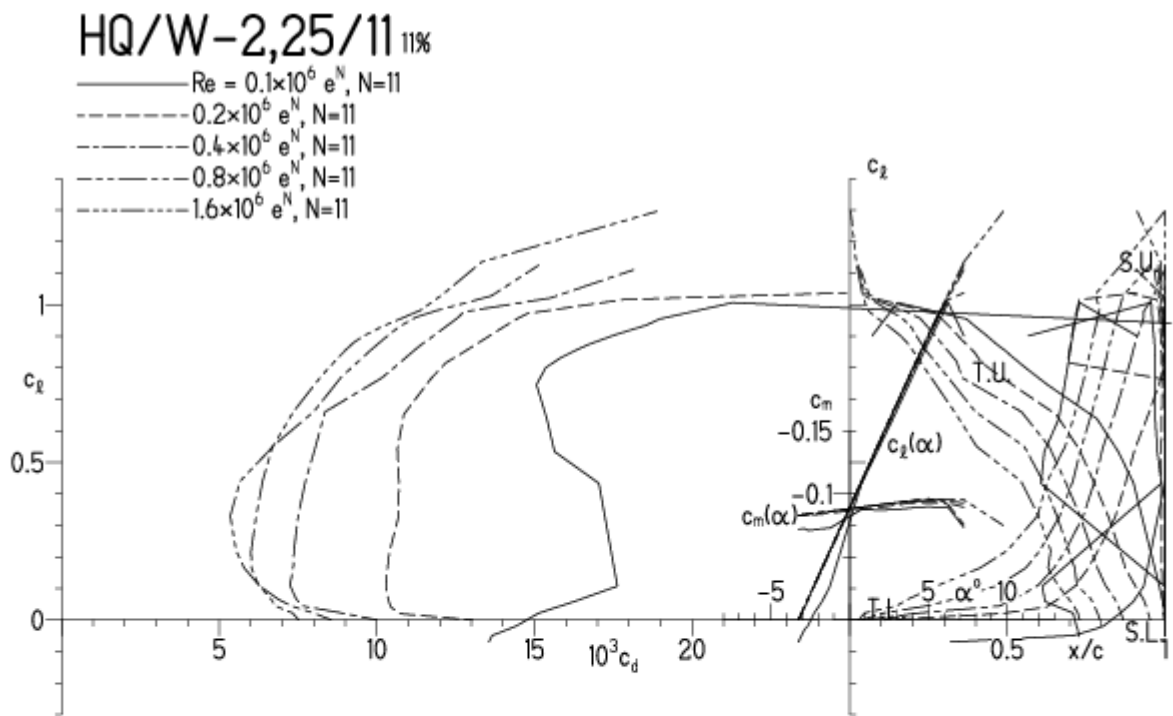


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

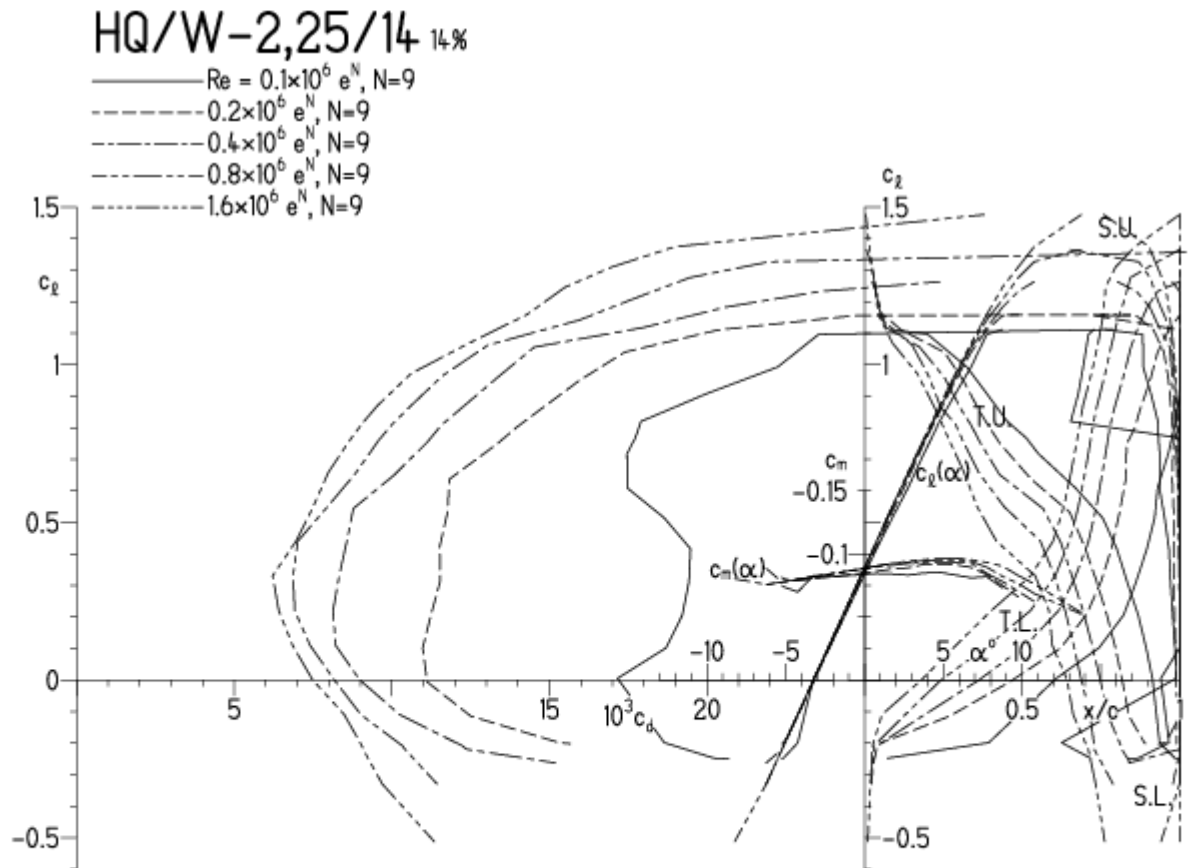


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

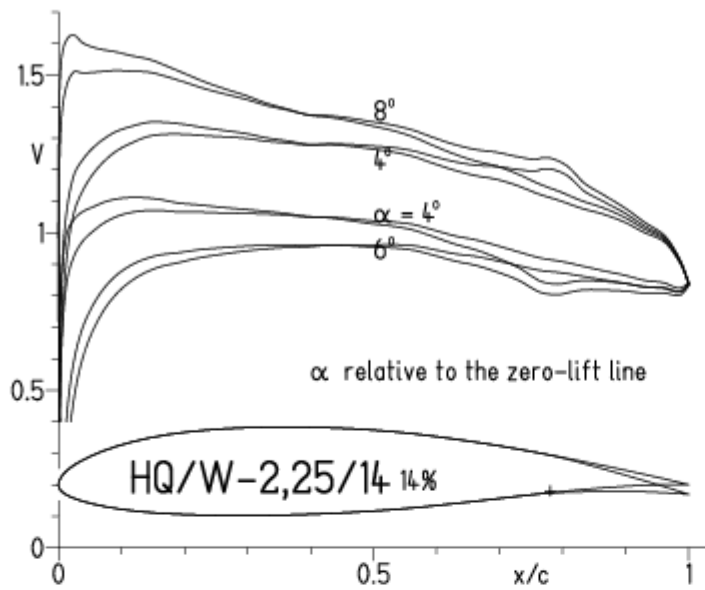
HQ/W-2,25/14 14%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

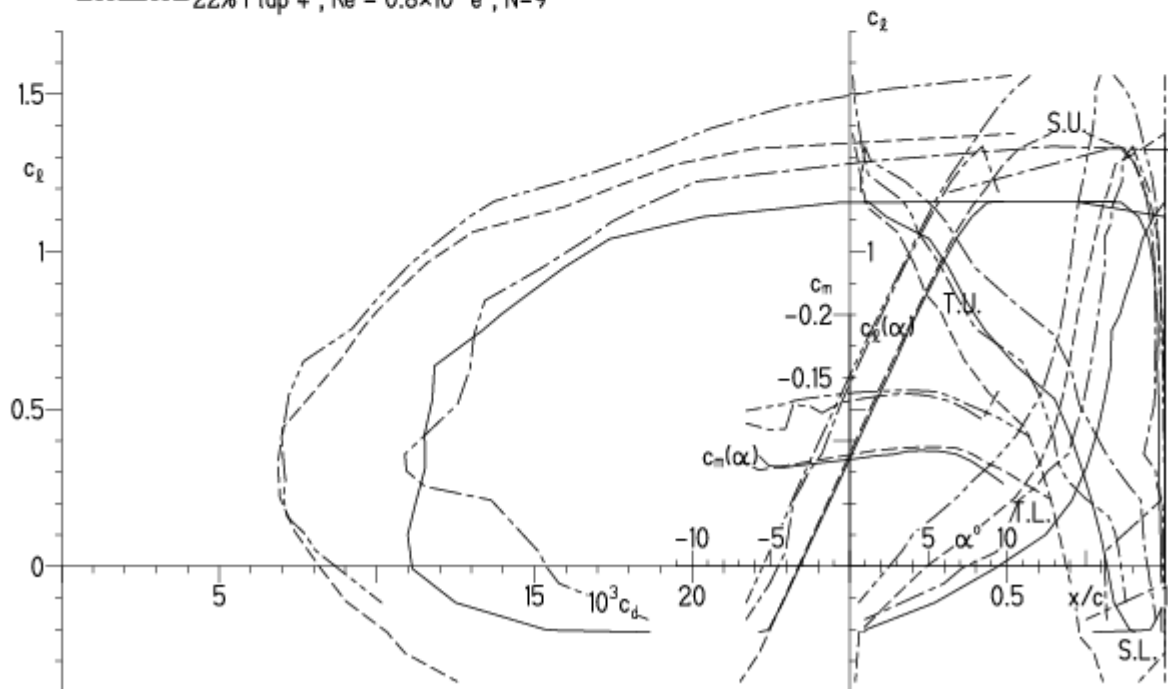


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

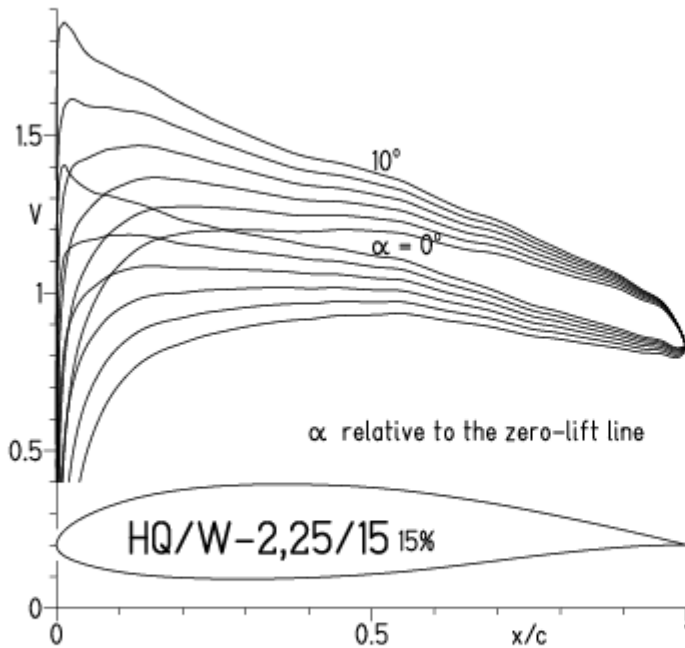


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

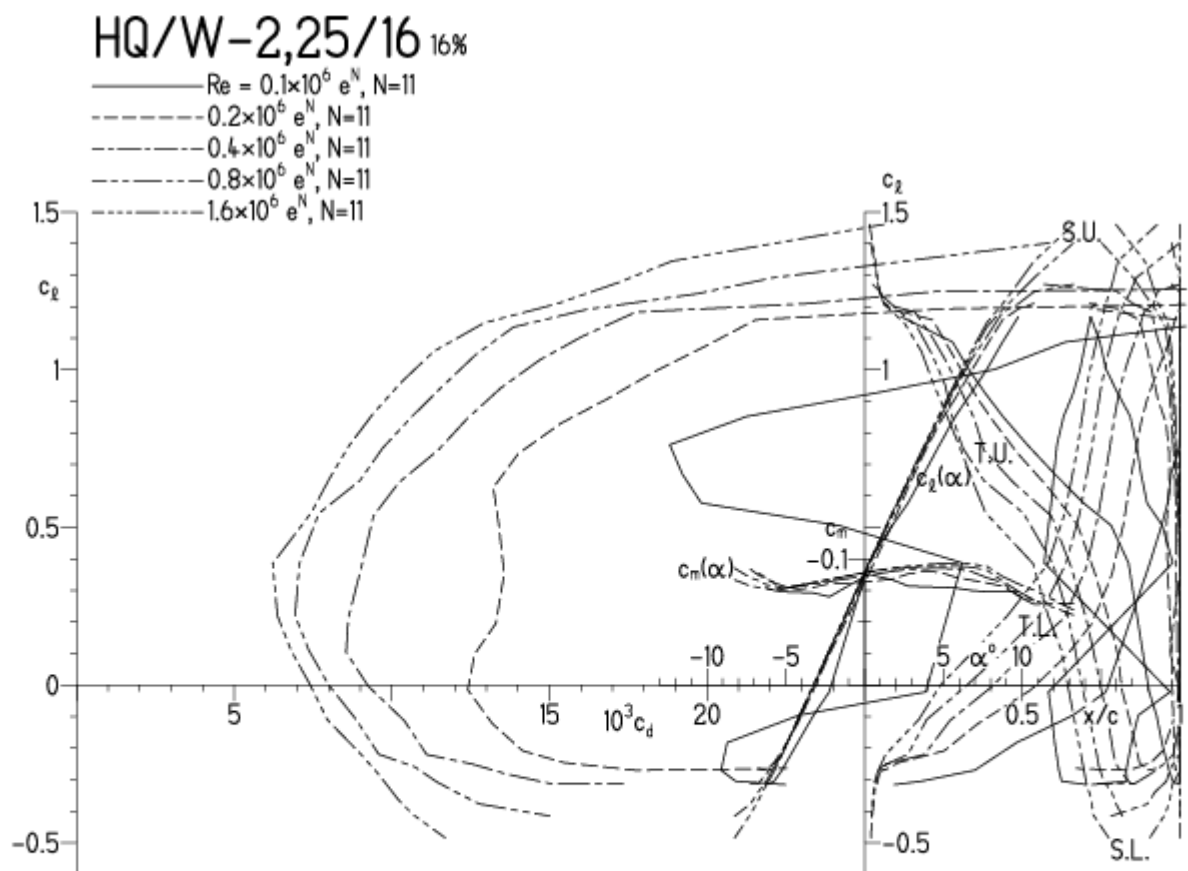


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

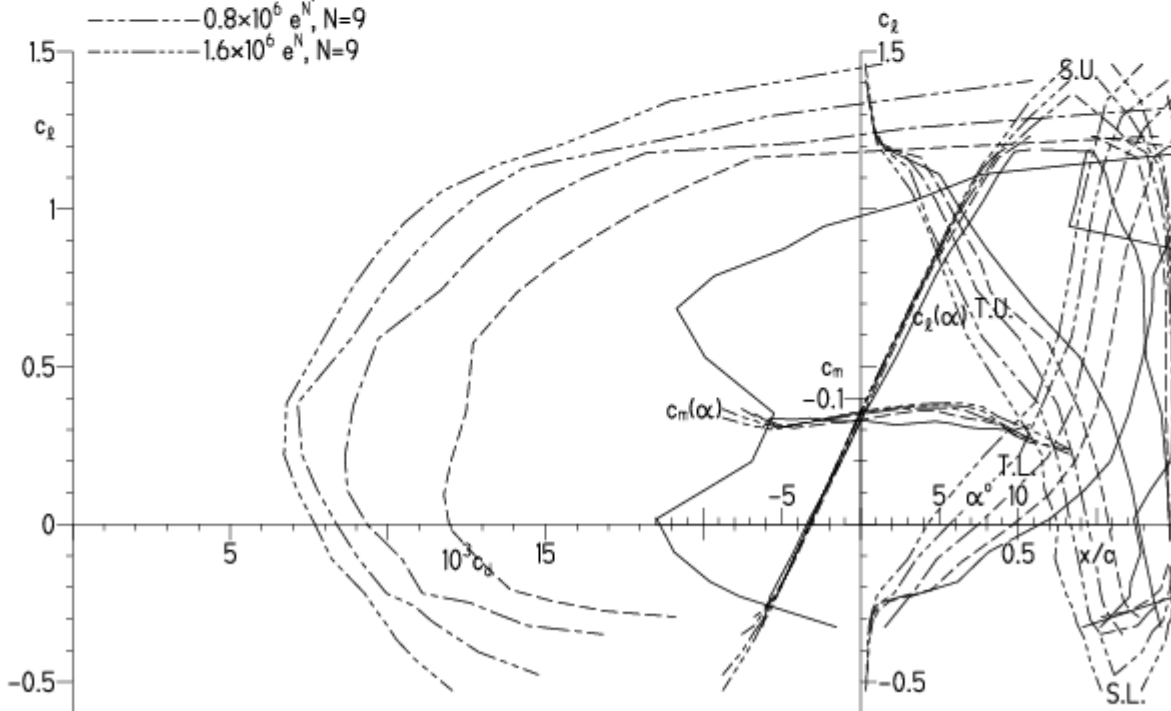
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

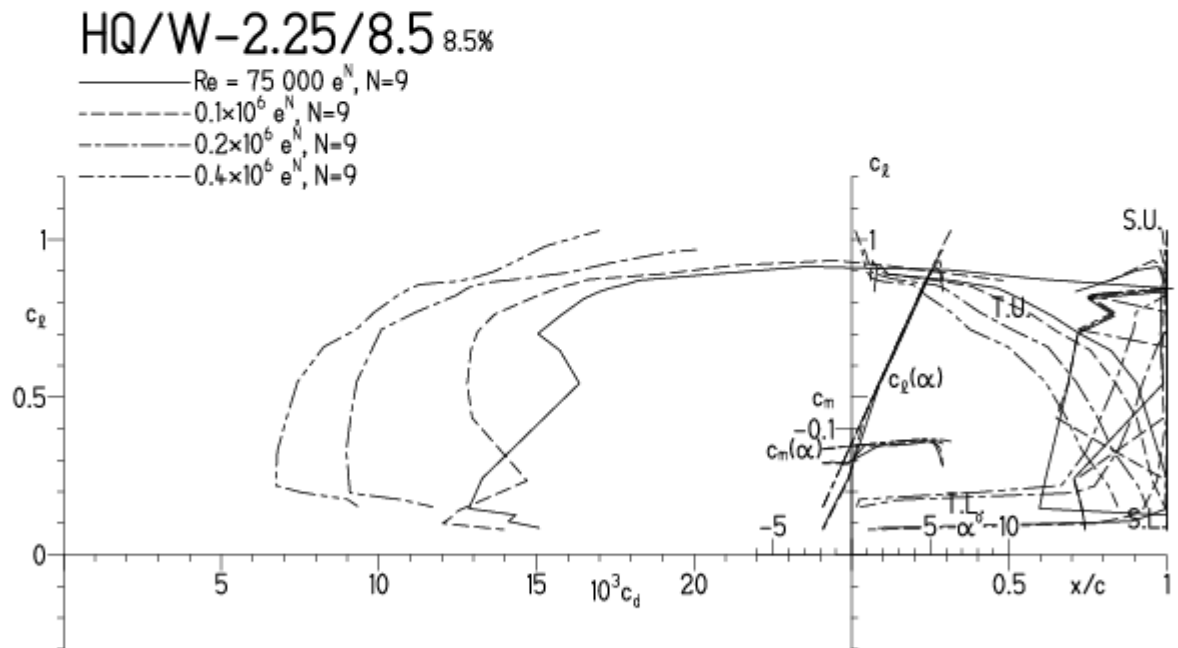


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

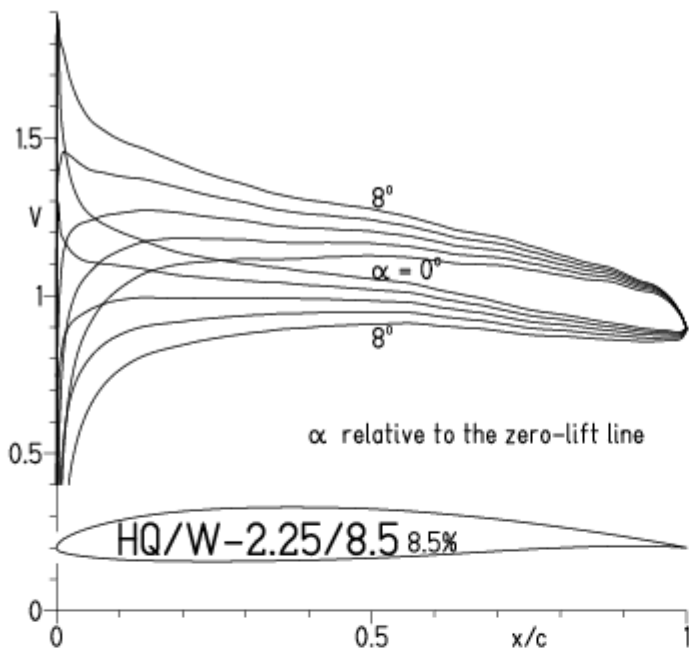


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

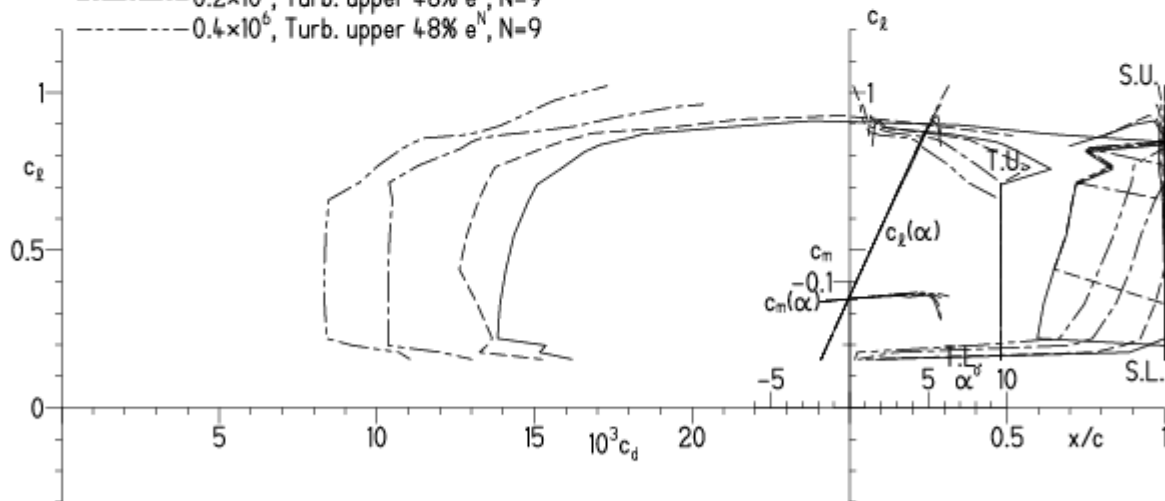
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - · 22% Flap 4°, Re = 75 000 e^N, N=11
- · - · 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

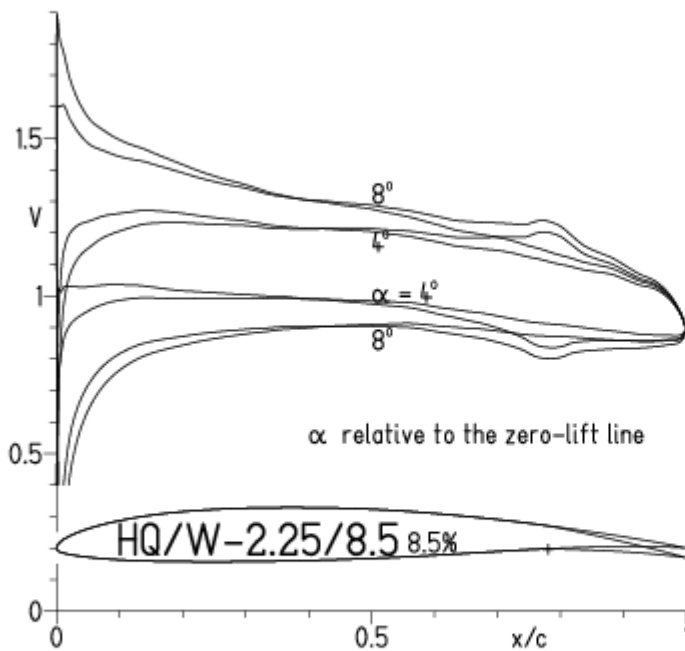
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

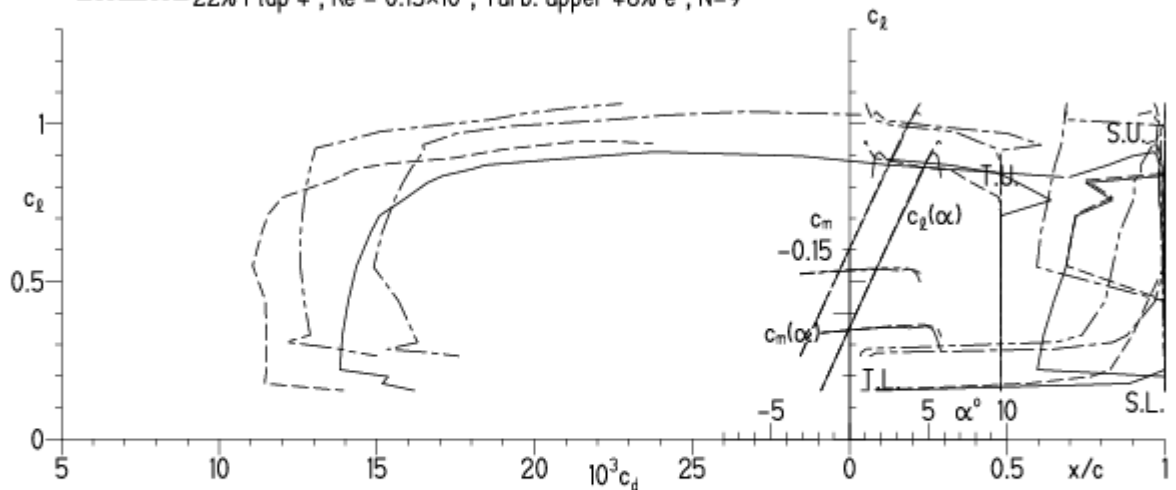


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

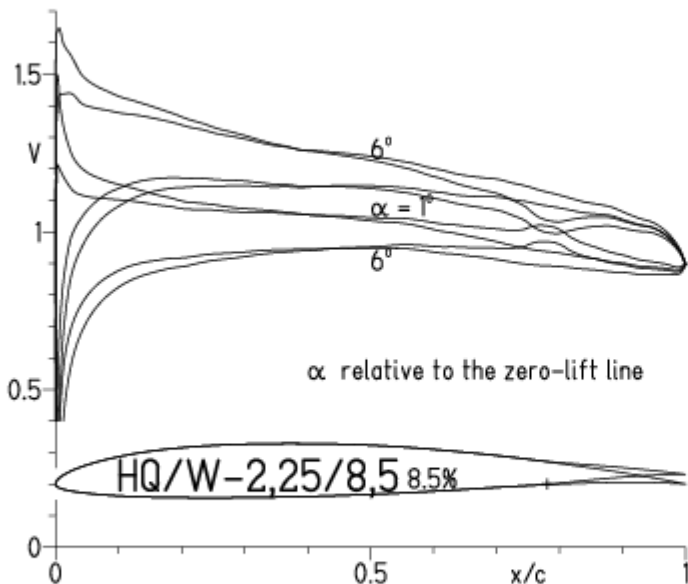
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

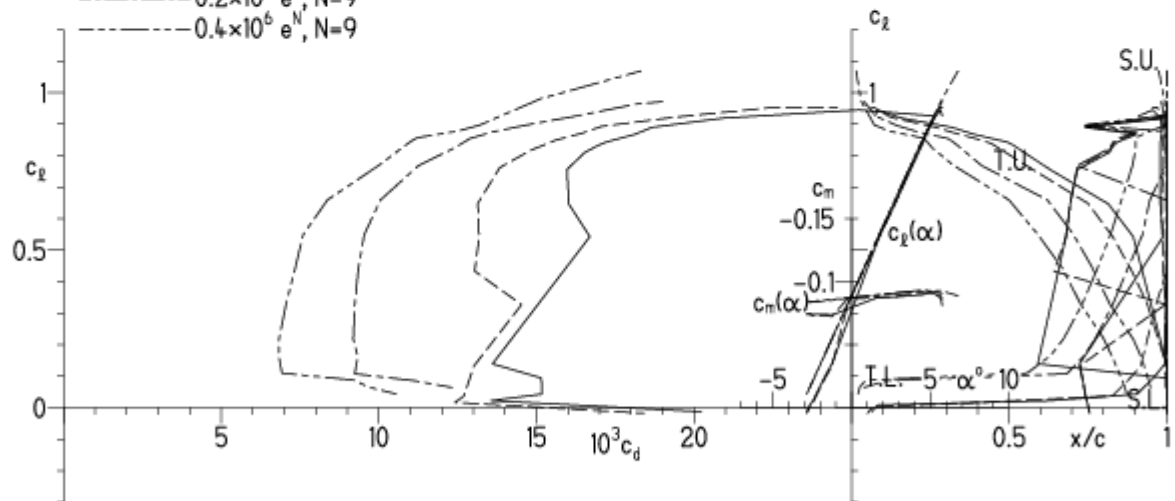
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

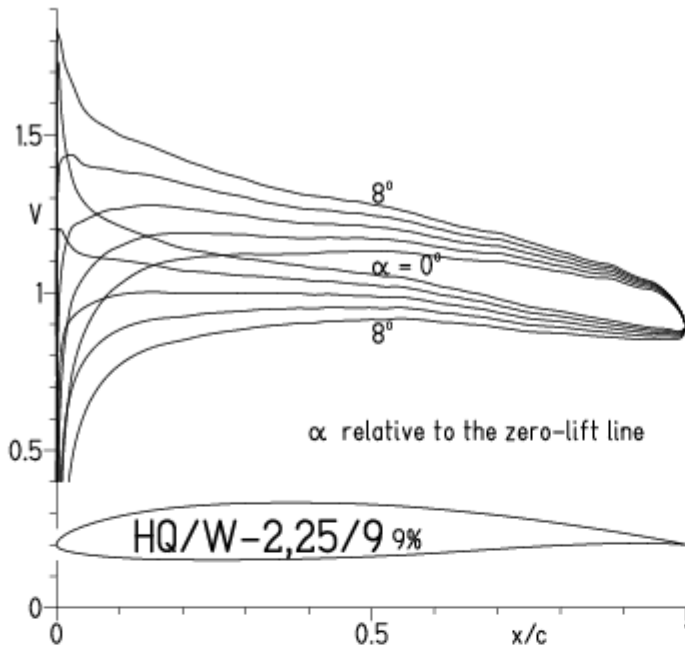
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

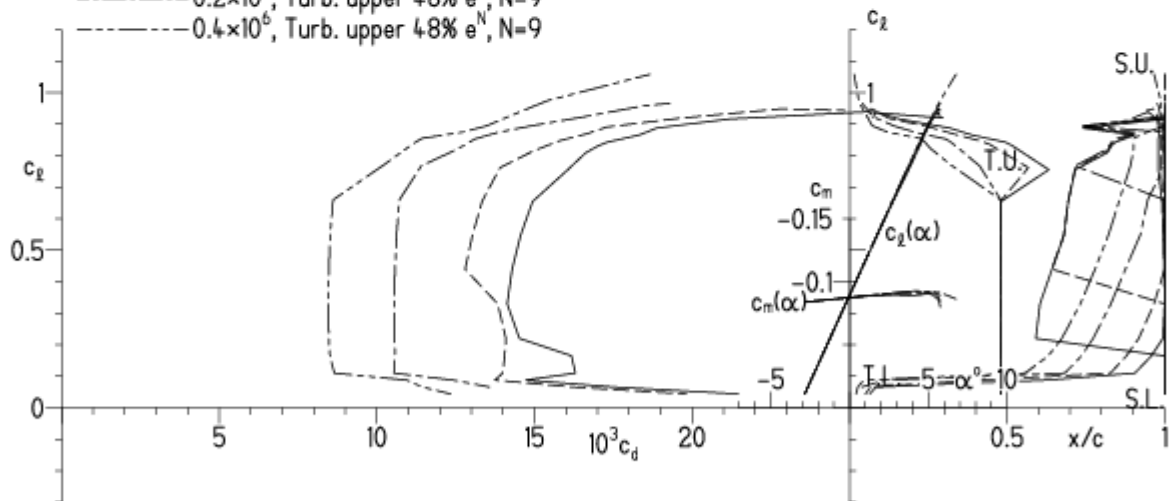
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

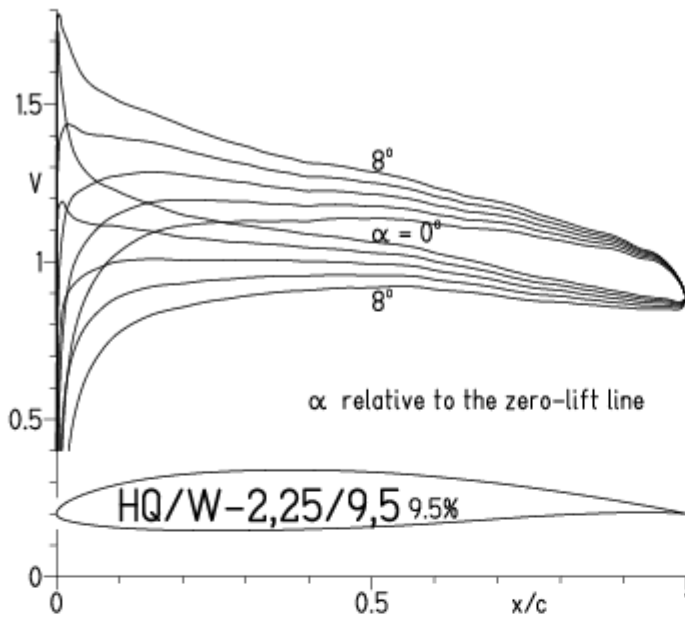
HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

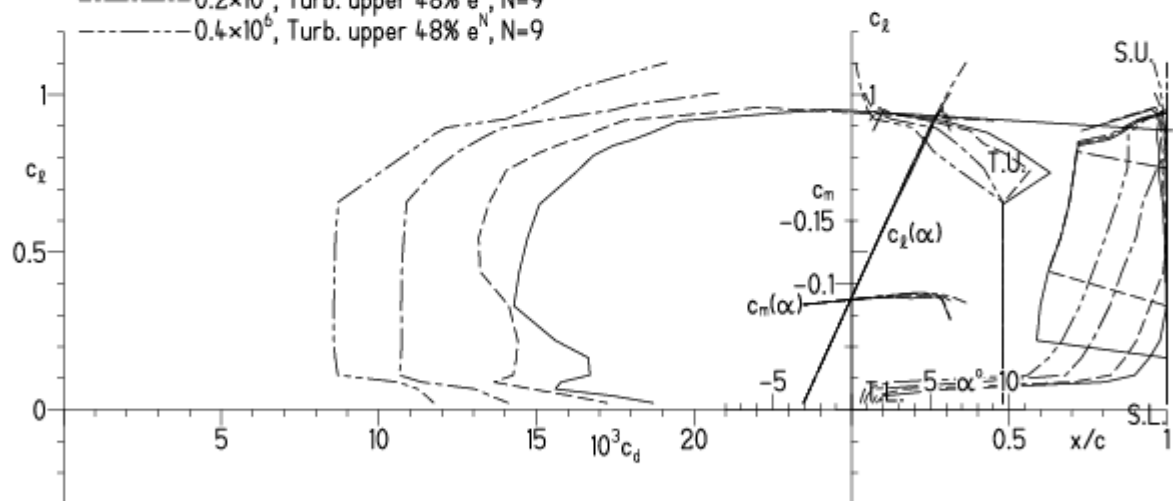
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

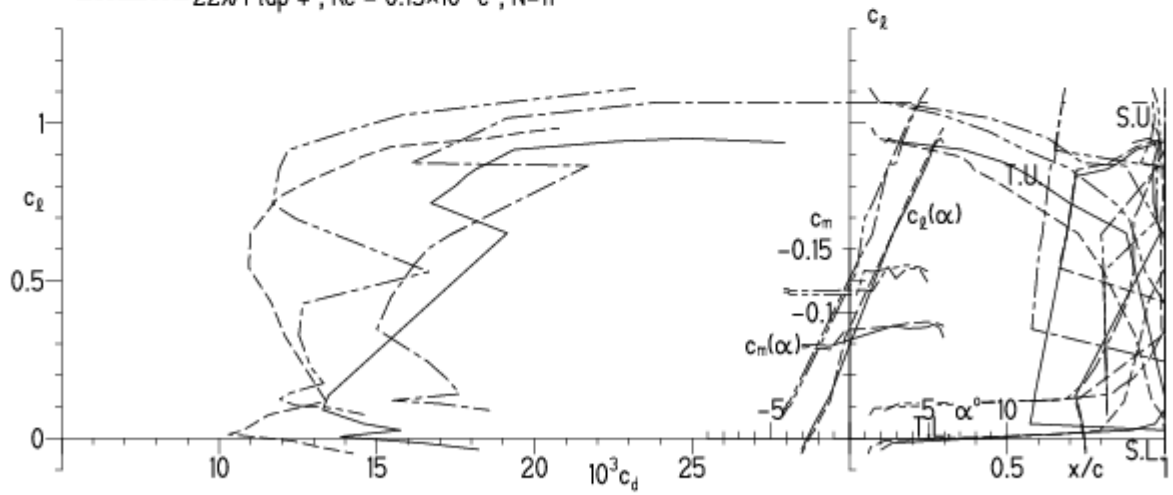


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



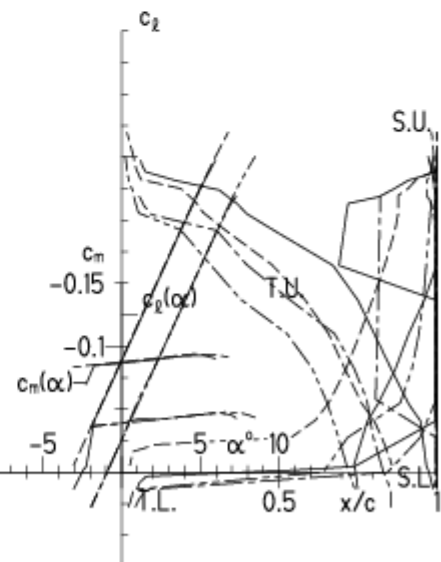
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

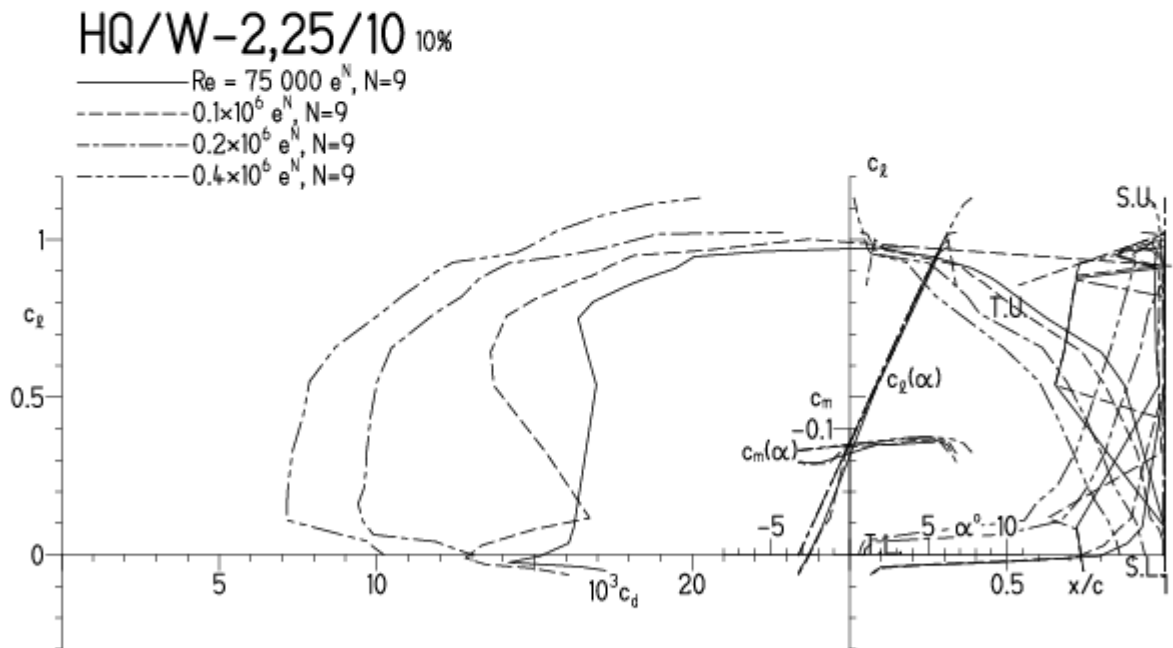


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

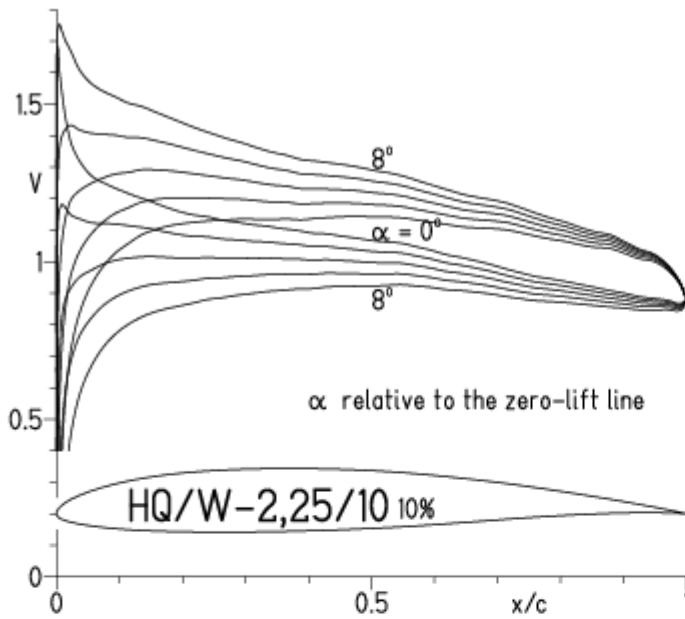


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

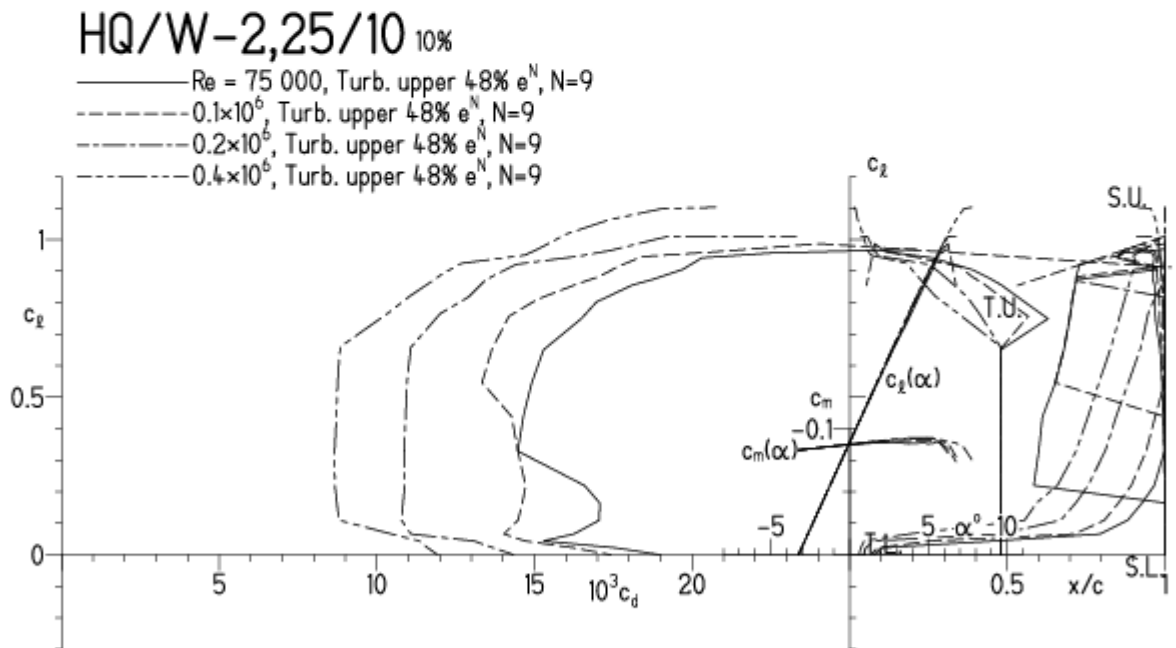


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

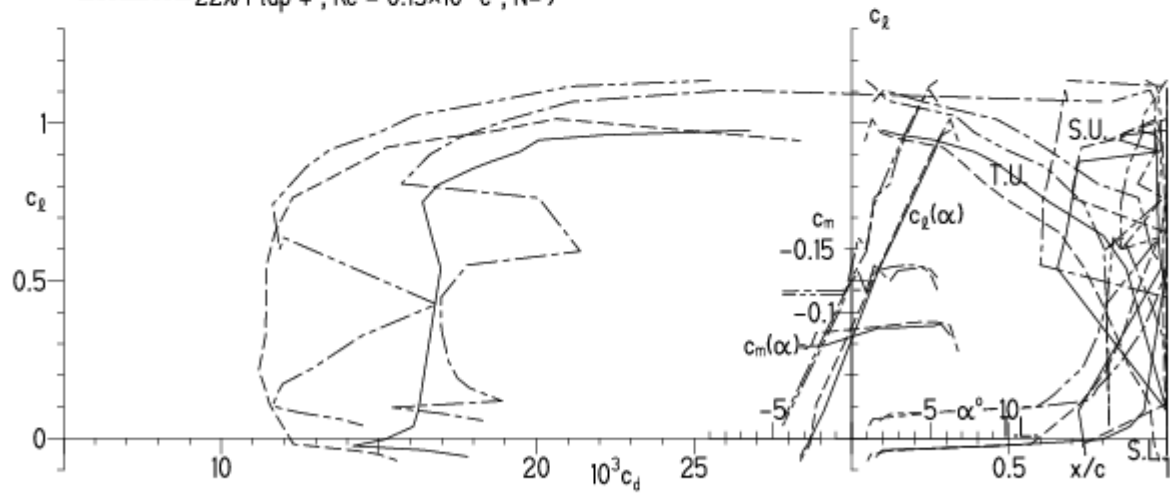


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

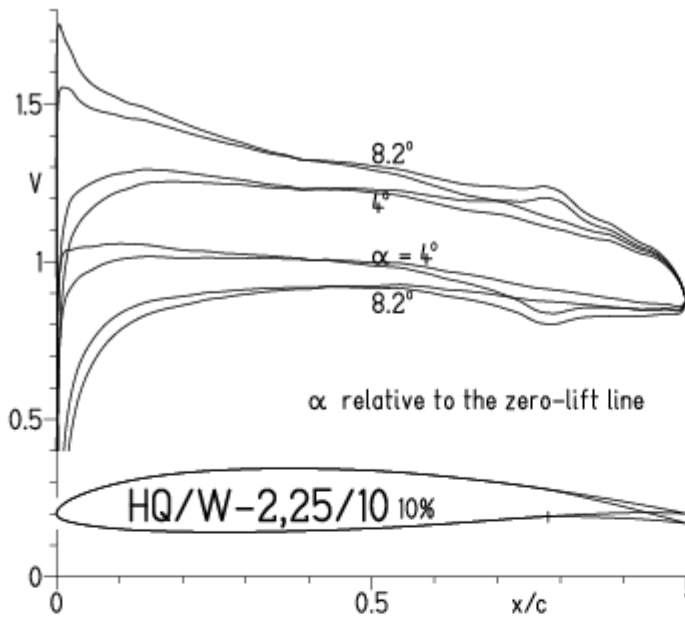
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

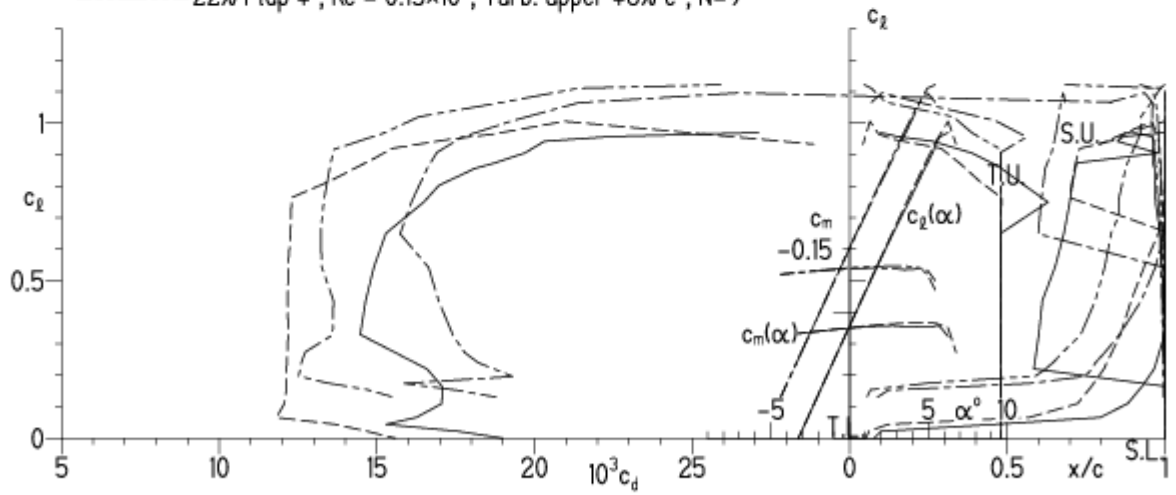


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

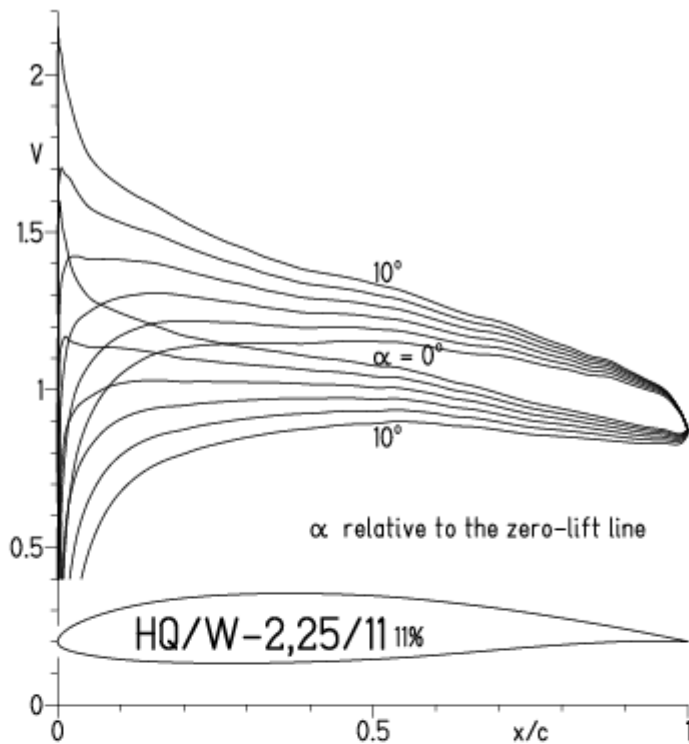


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

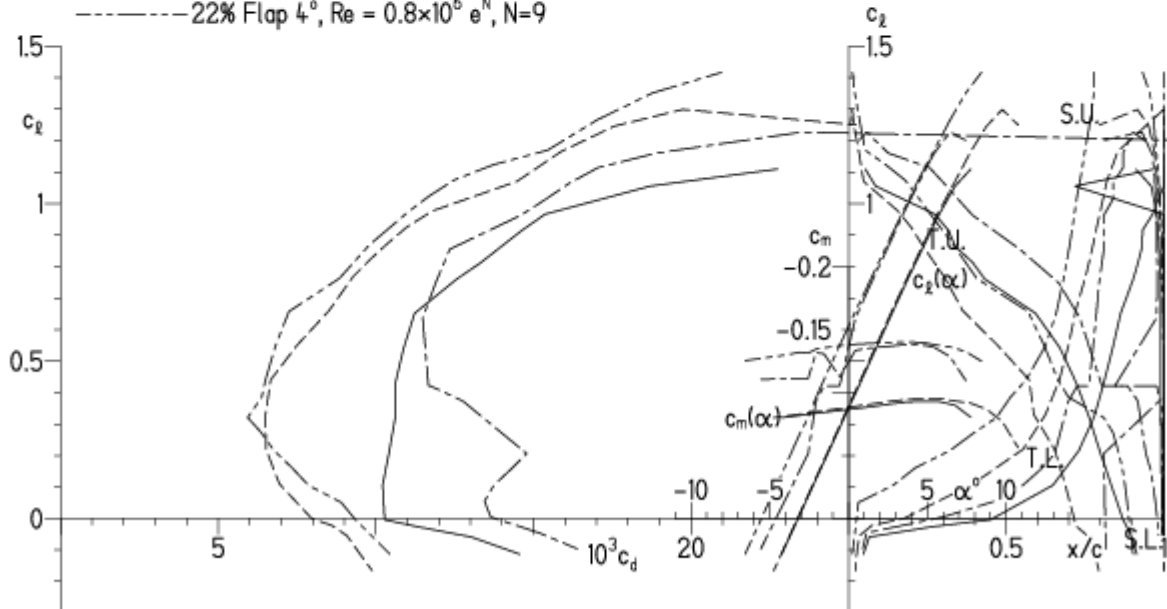


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- Re = 0.2×10^6 e^N, N=9
- - - Re = 0.8×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.2×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.8×10^6 e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

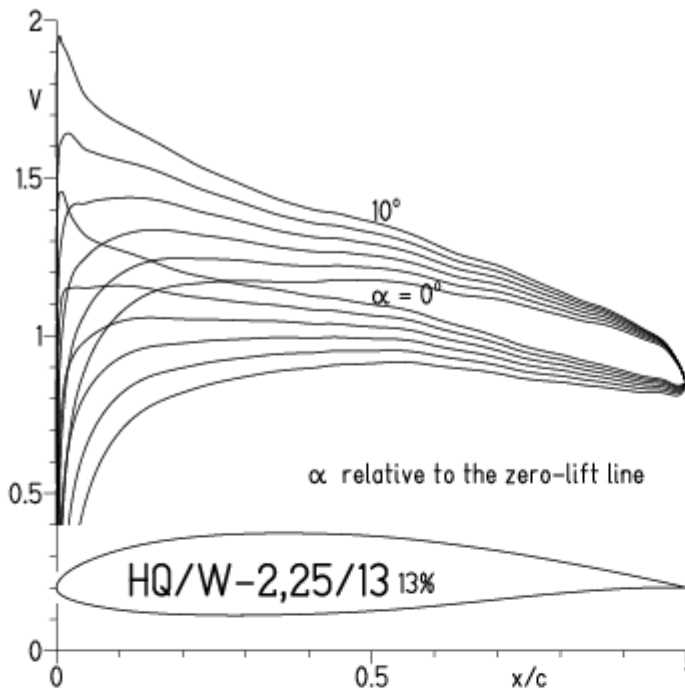
HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

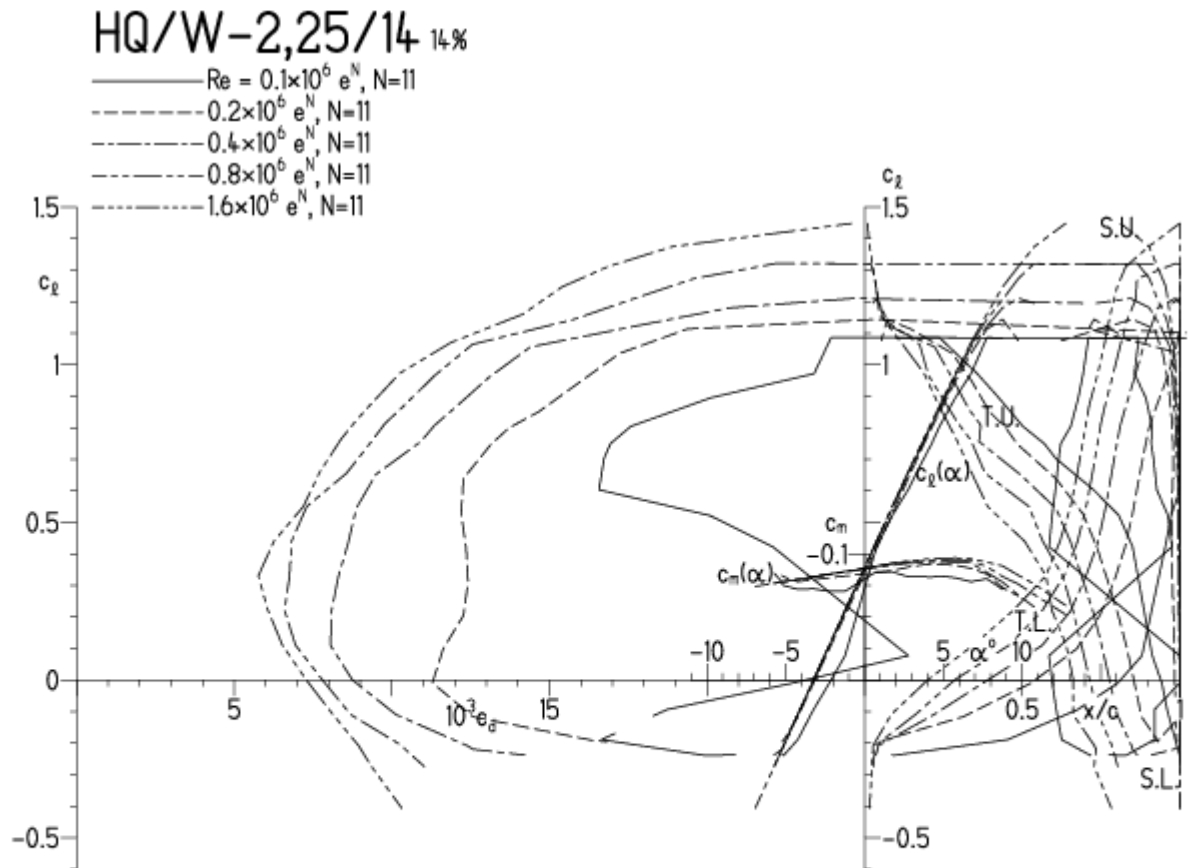


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

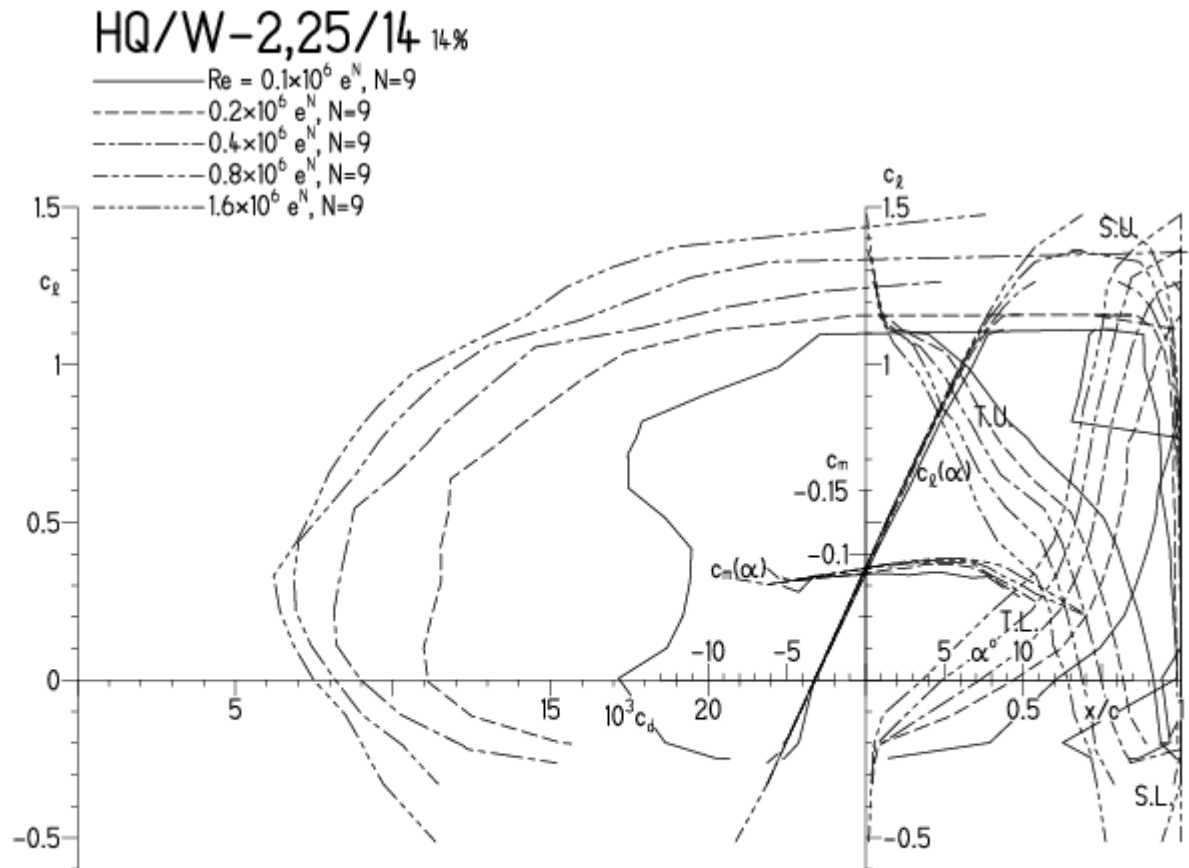


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

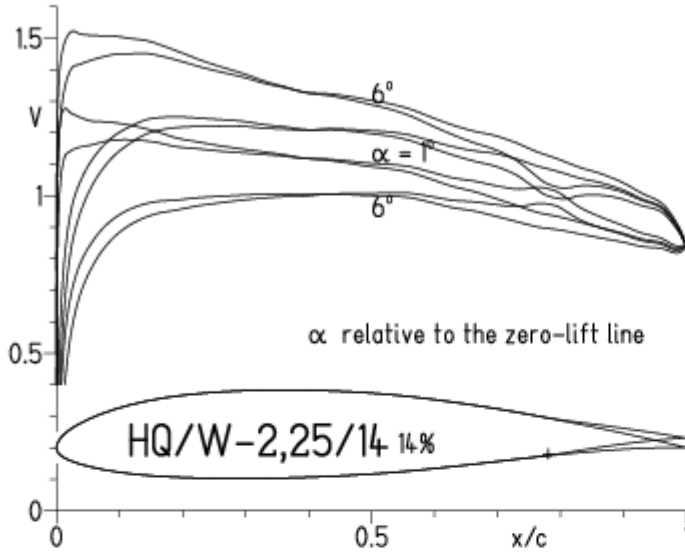
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

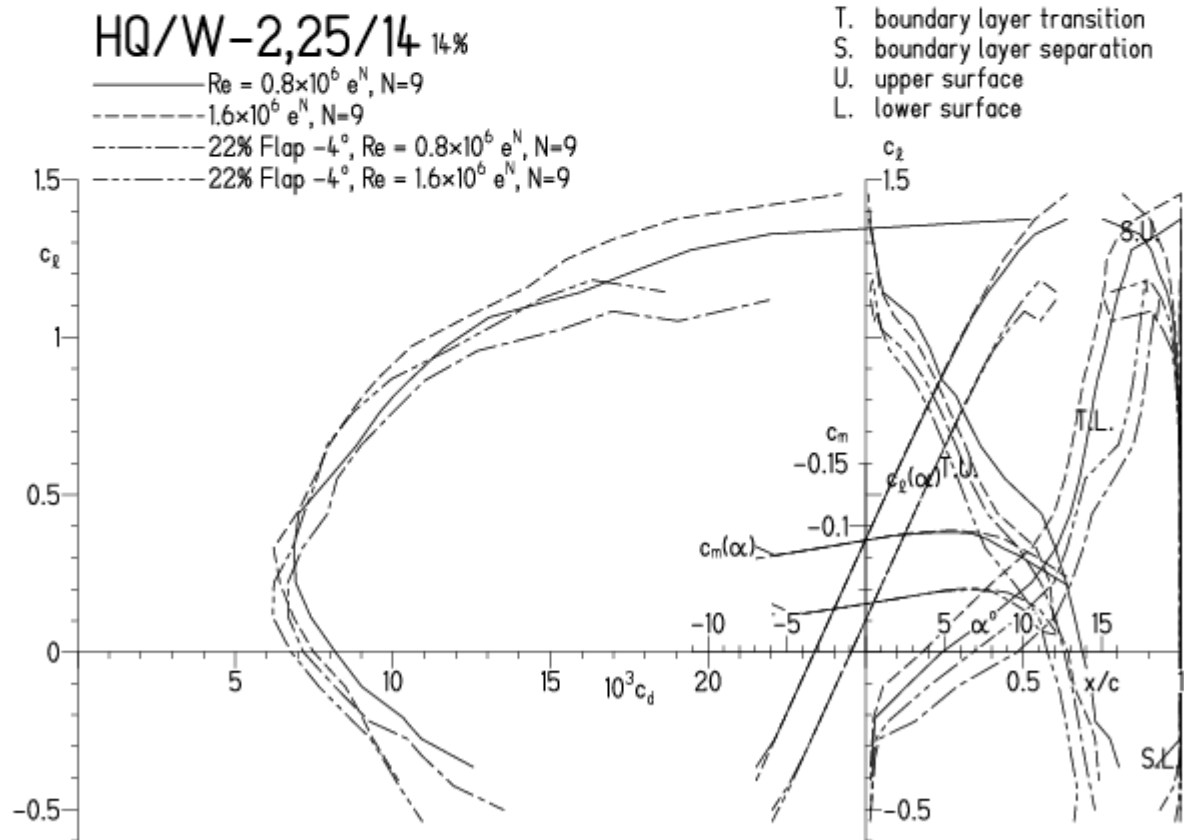


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

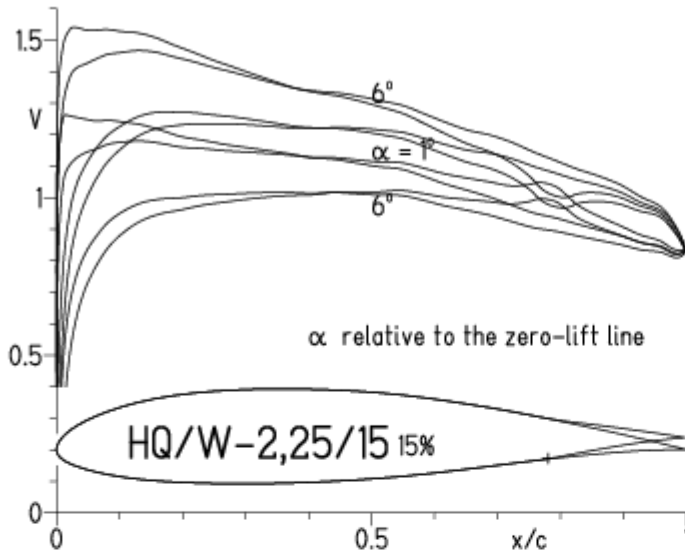


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

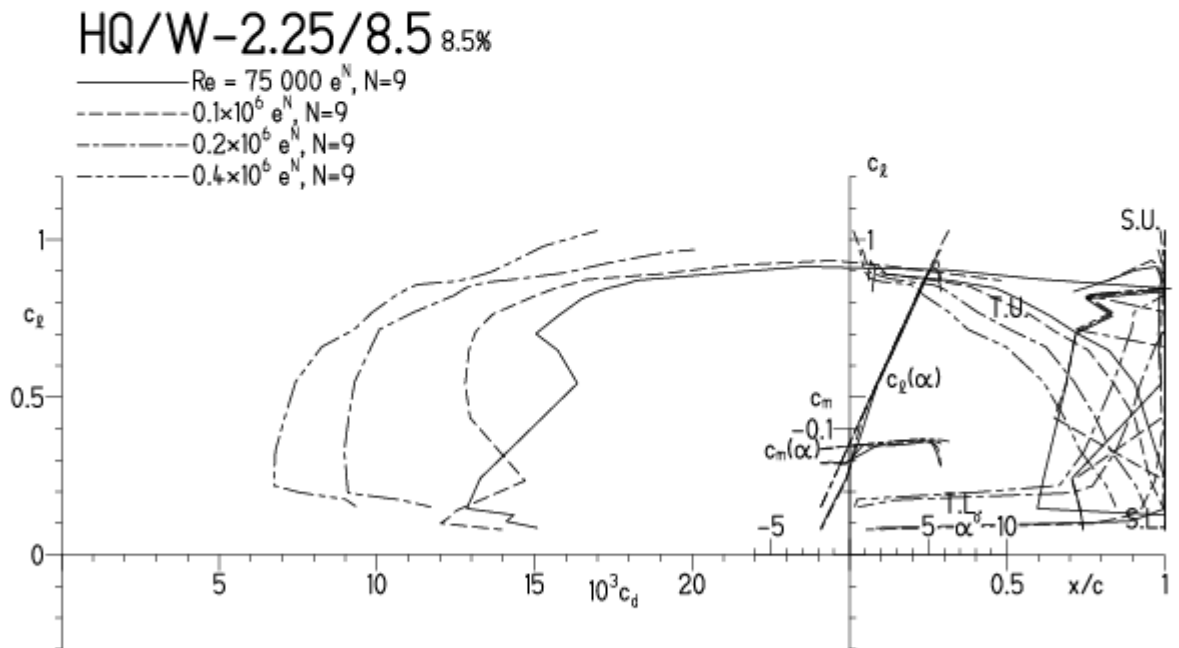


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



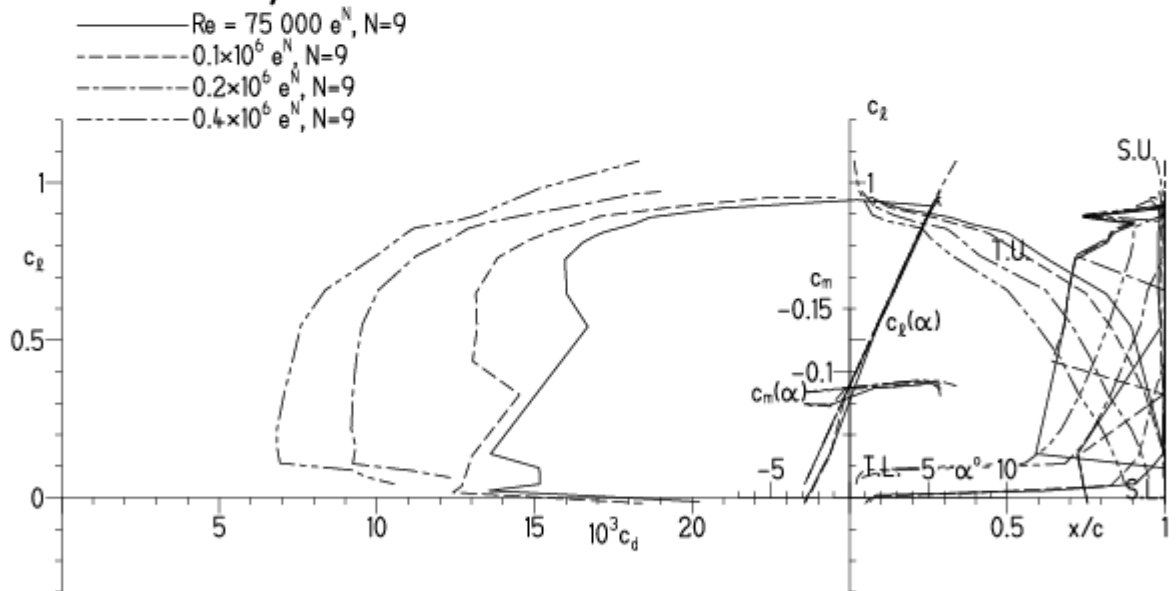
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

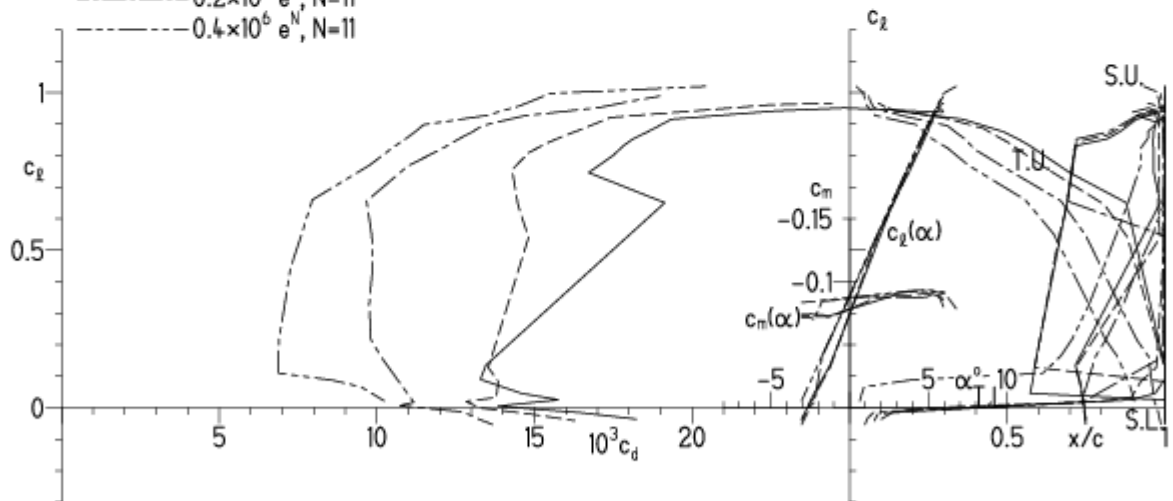
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

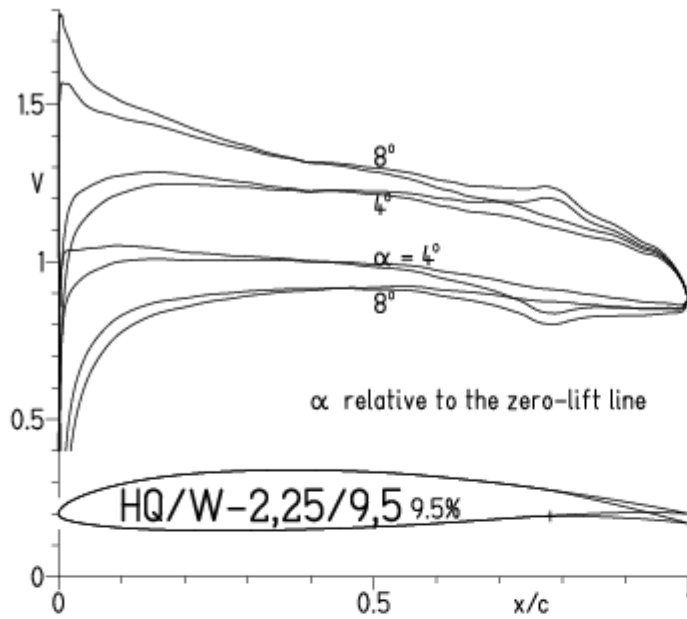
- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

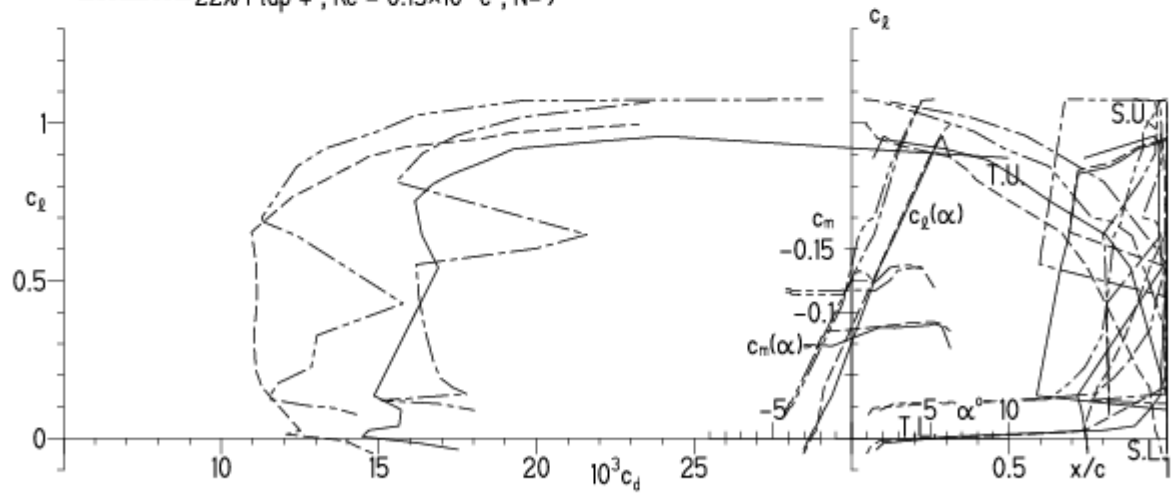


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
(Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



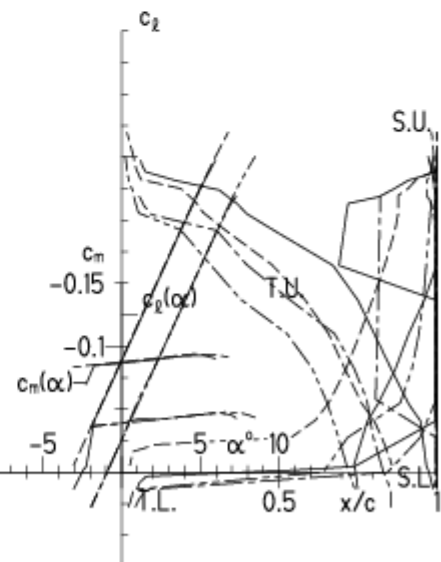
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

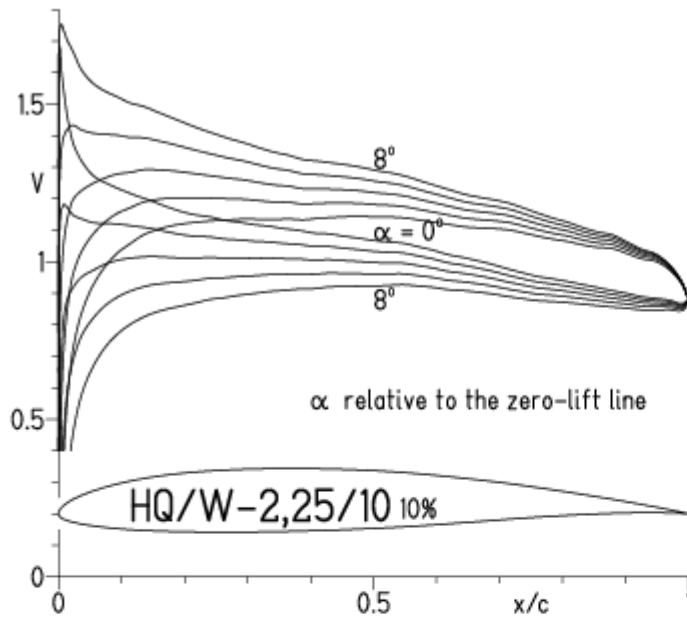


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

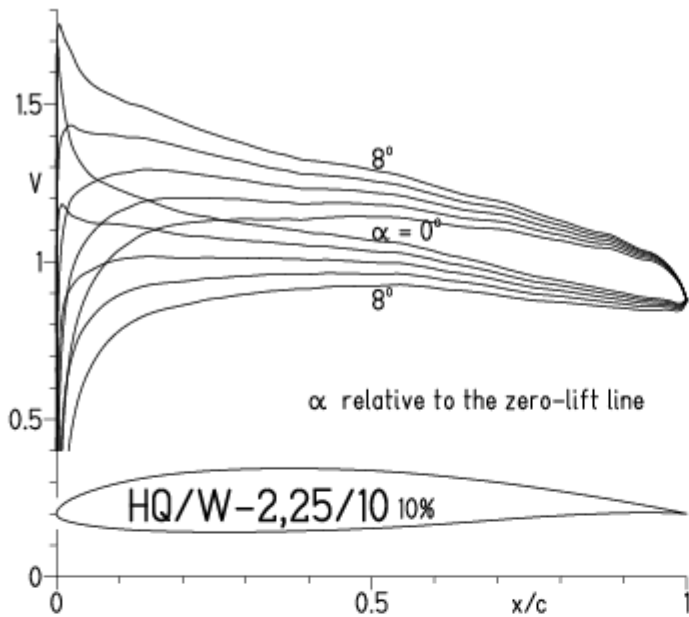


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

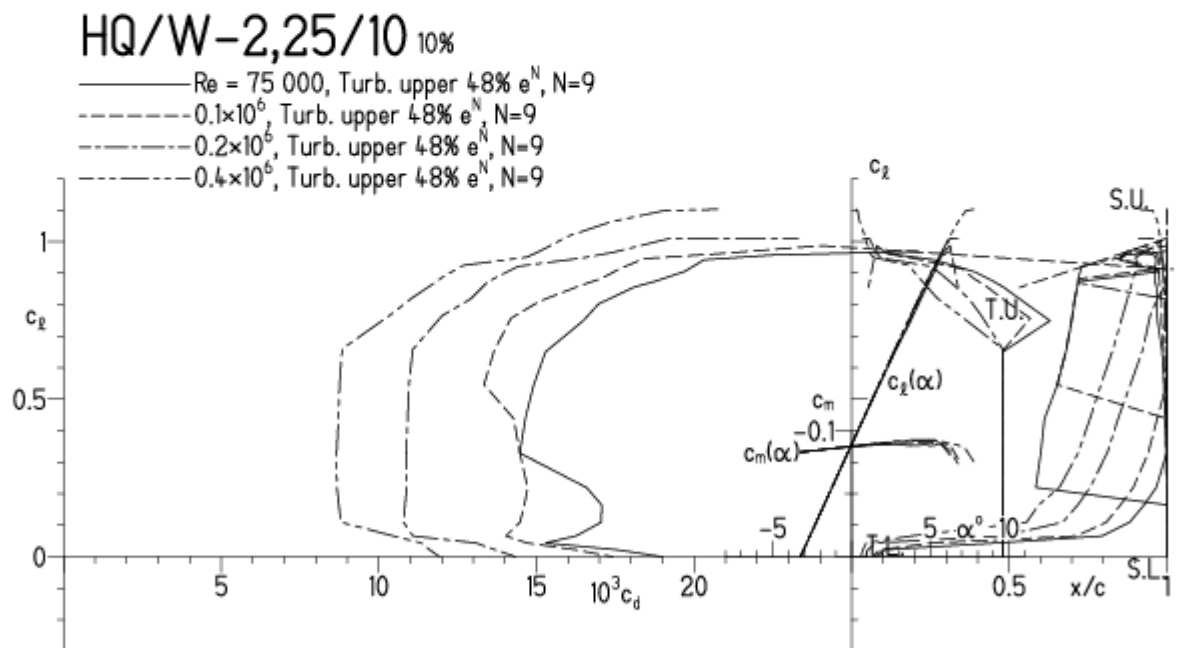


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

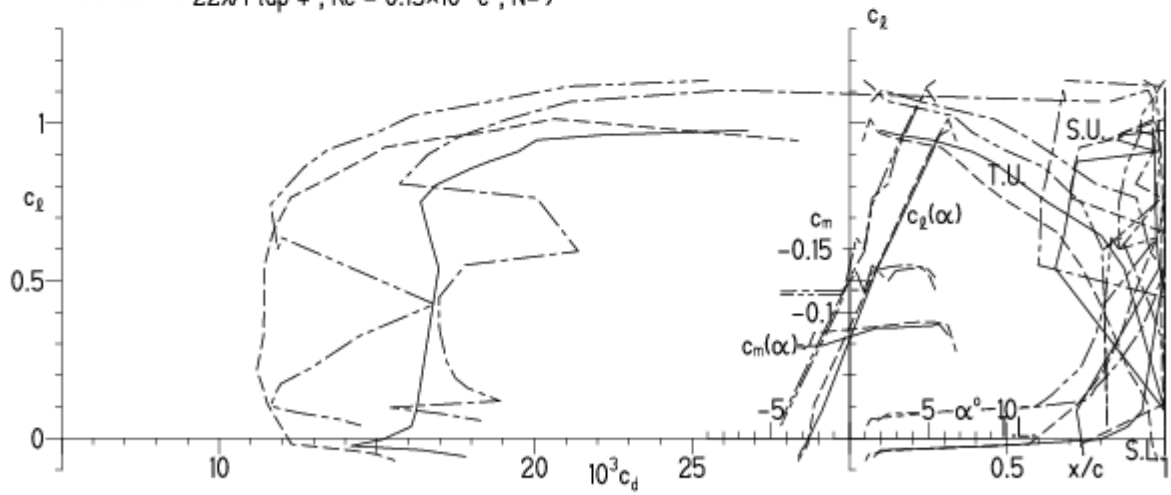


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

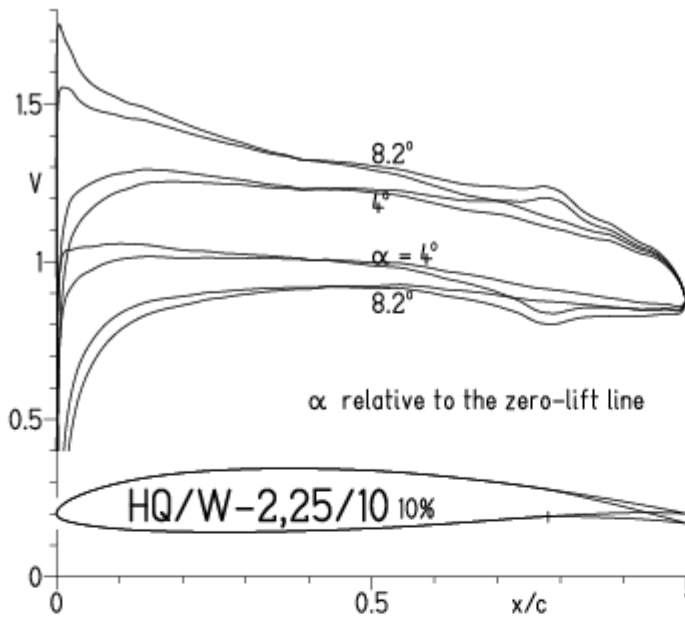
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

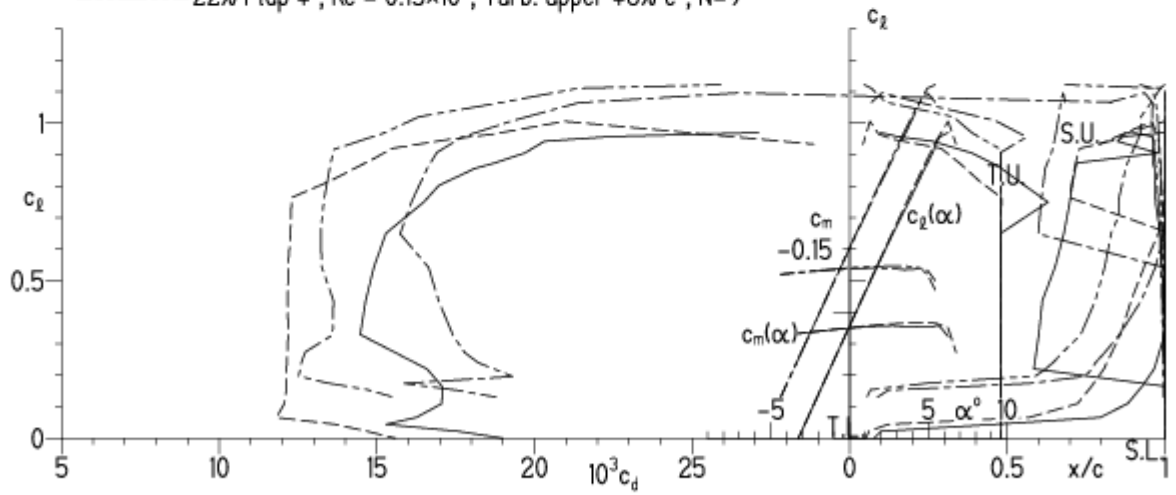


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

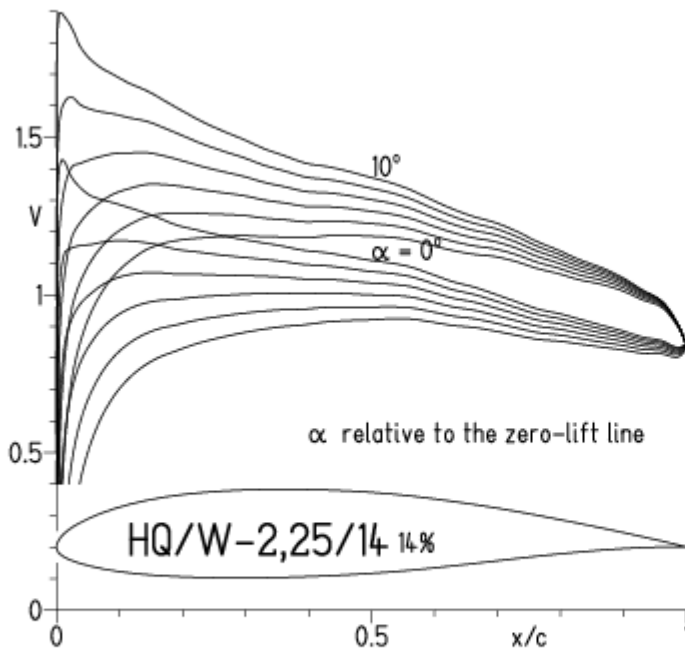


EPPLER 2005 V. 8.

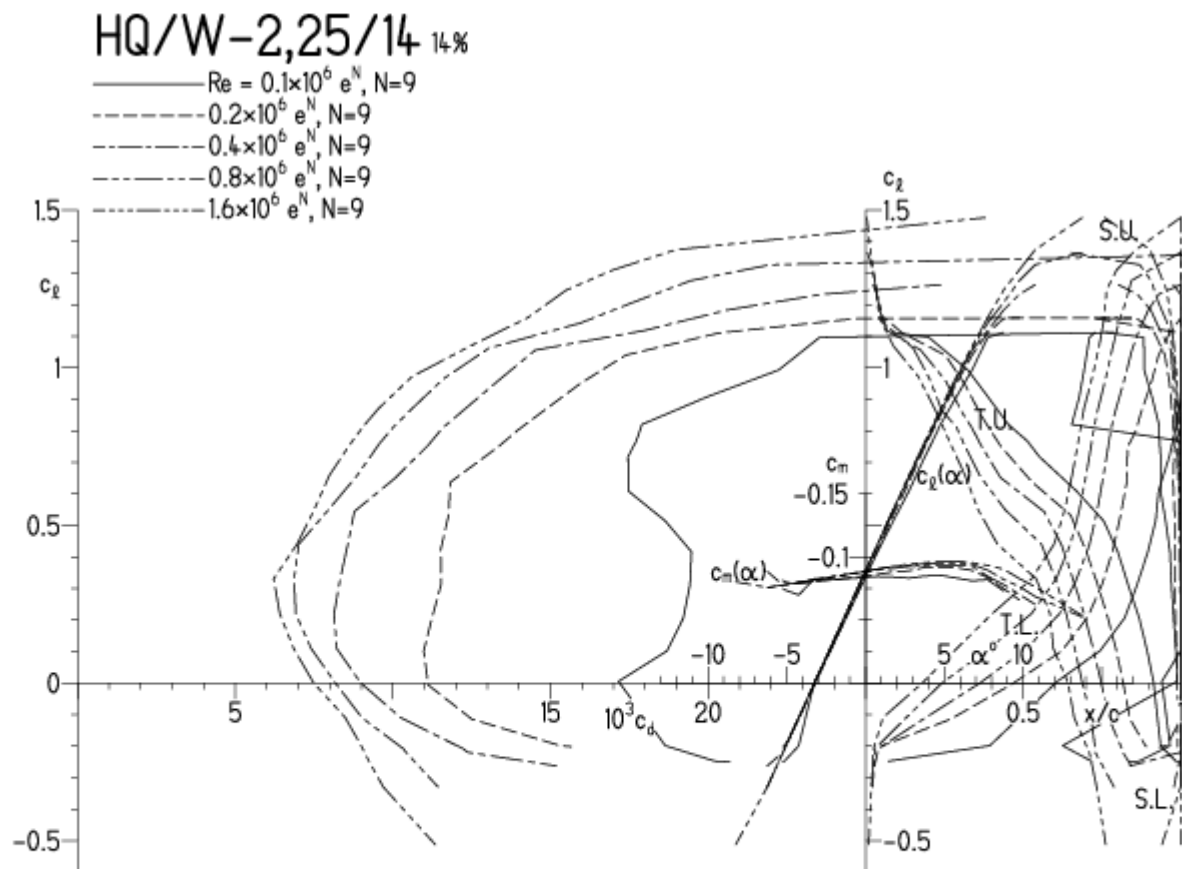


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

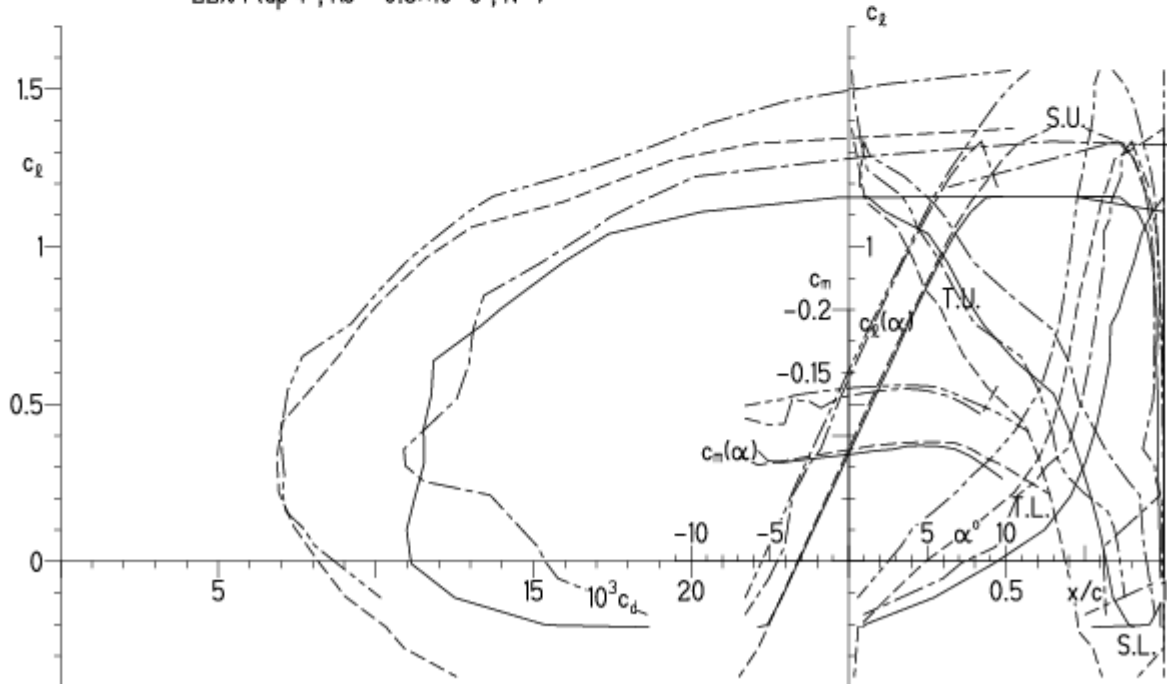


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

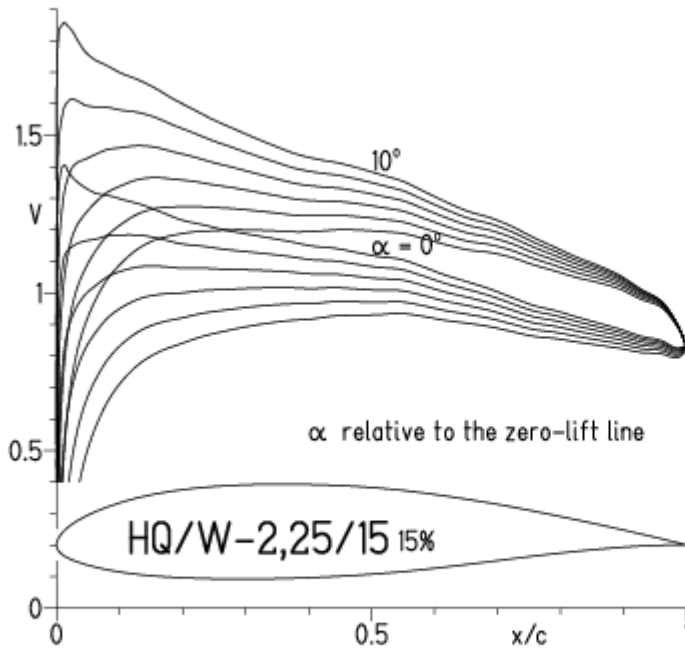


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



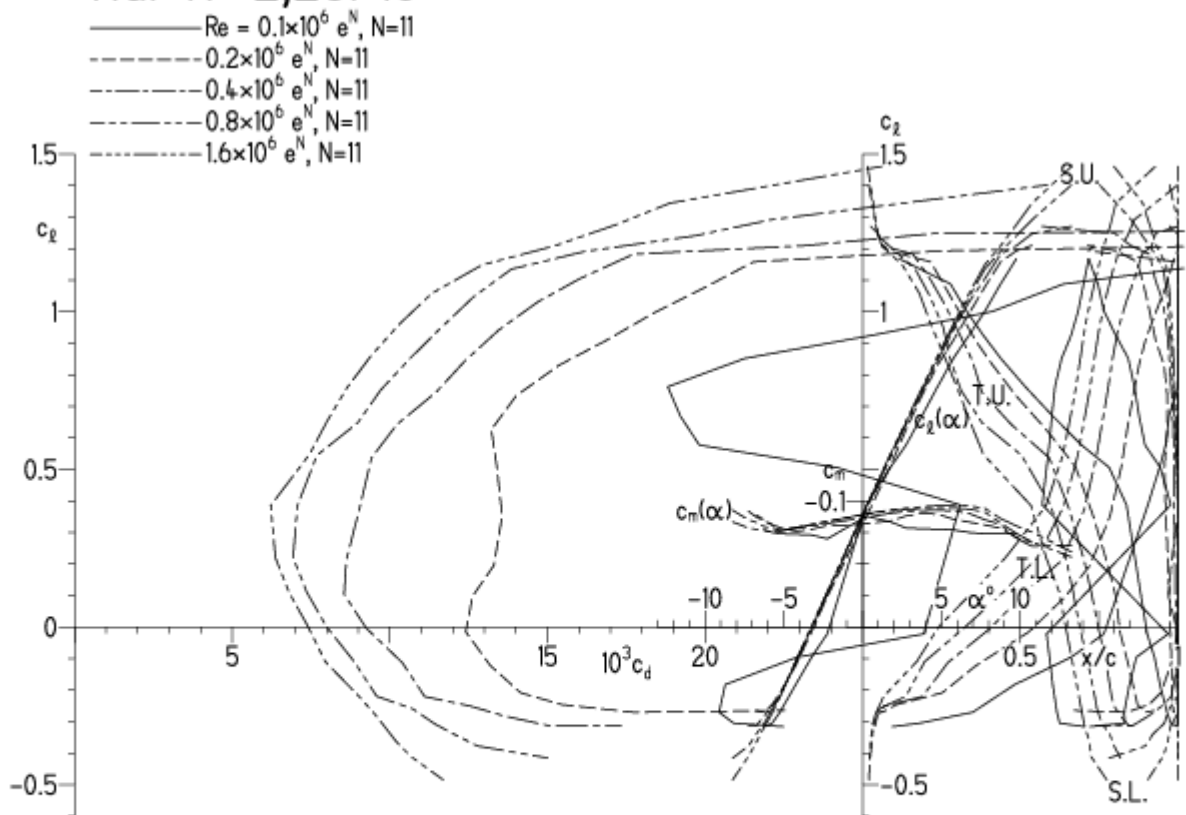
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

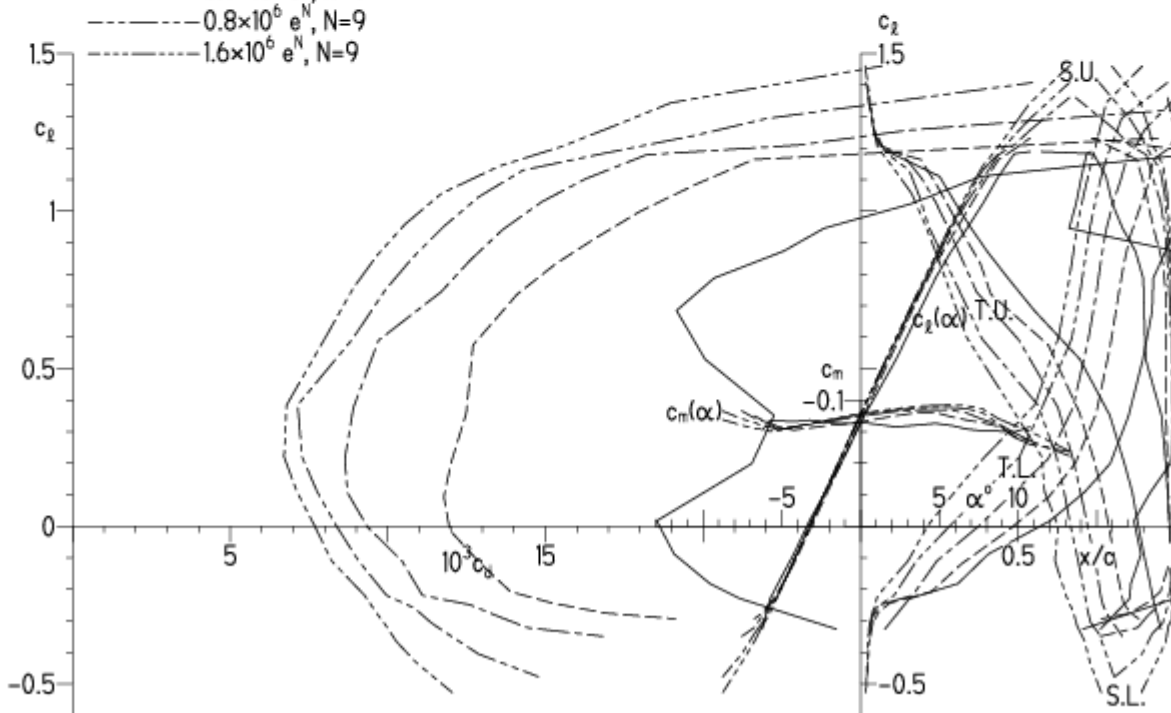
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

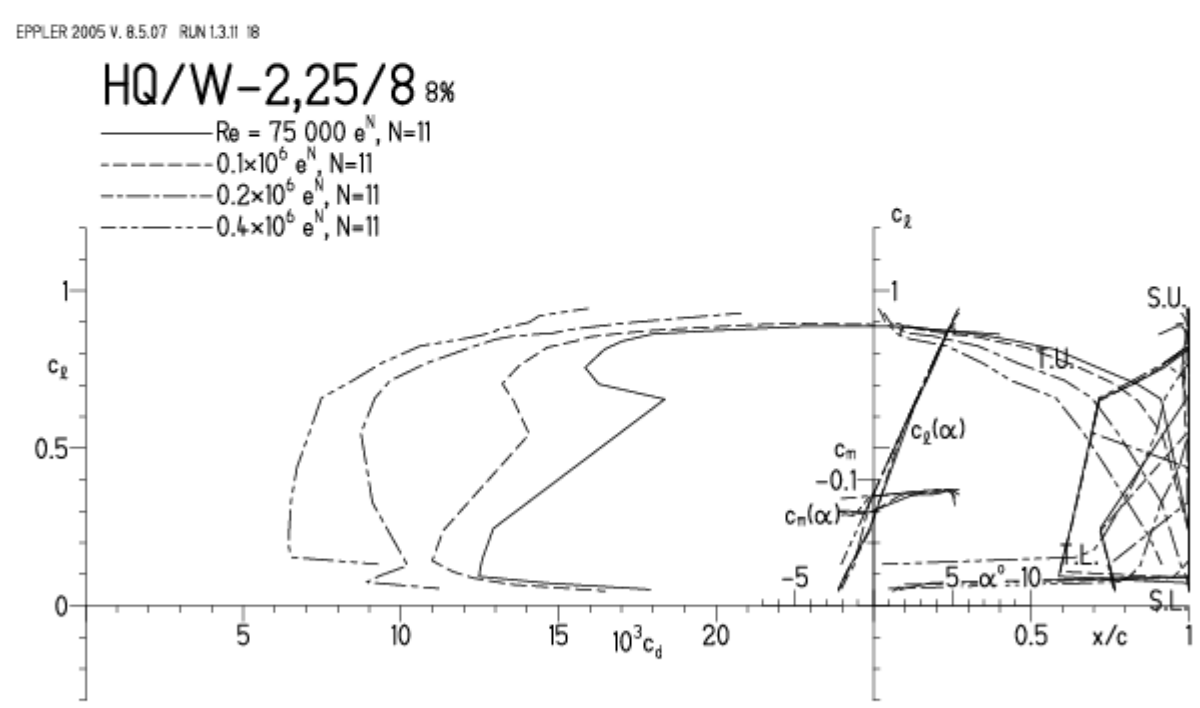
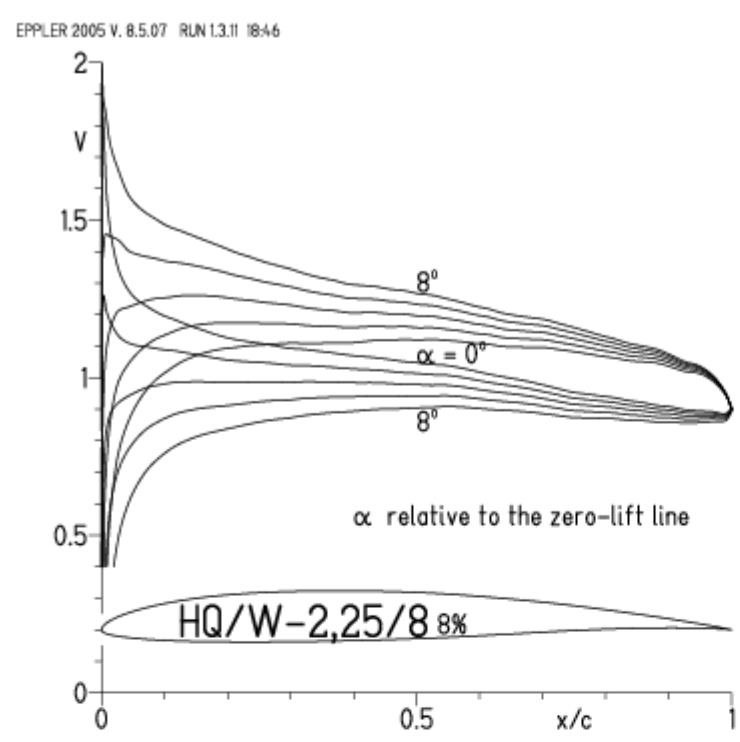
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11



HQ/W-2,25/8, N=9

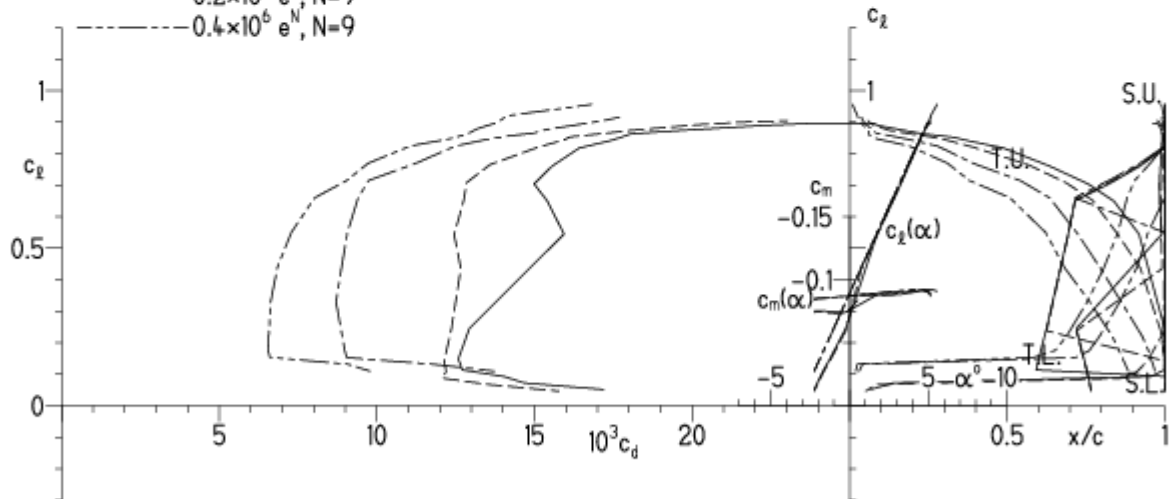
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

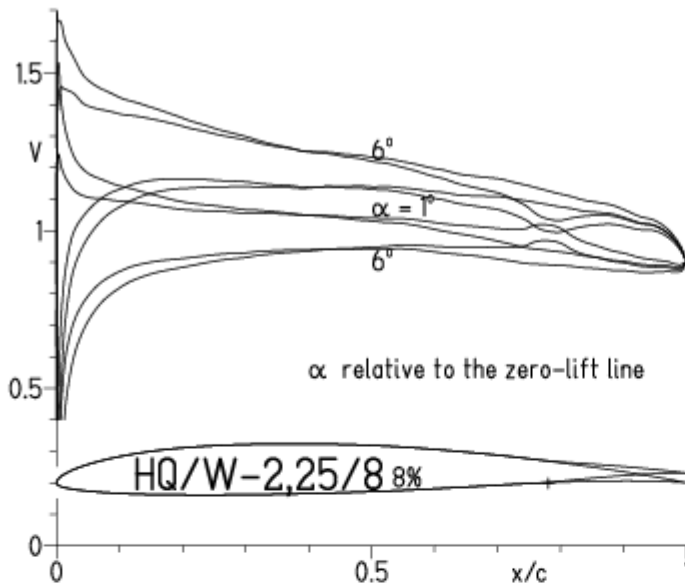
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

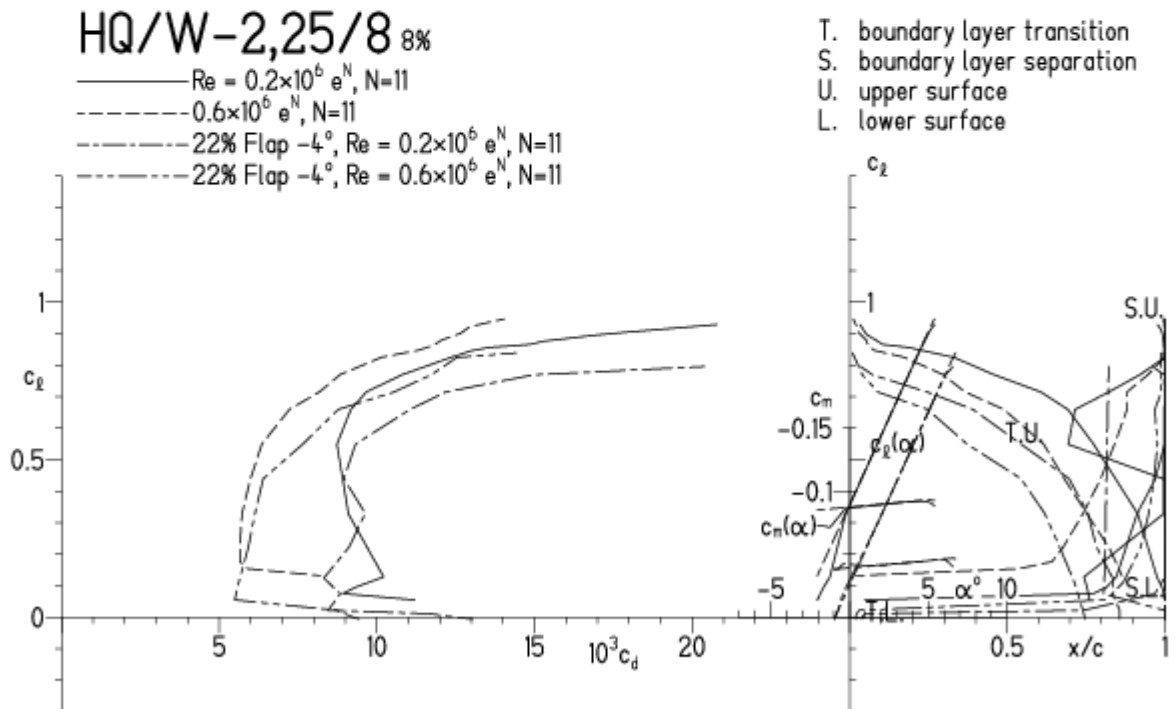


HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



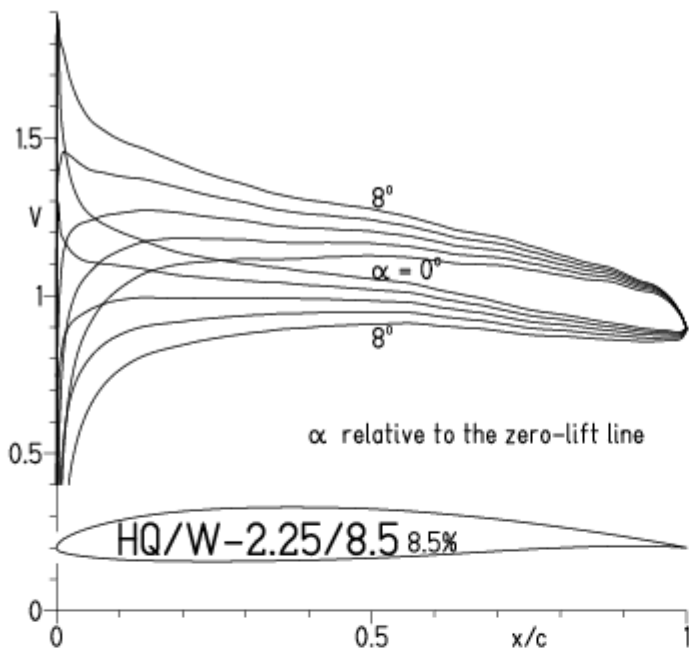
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

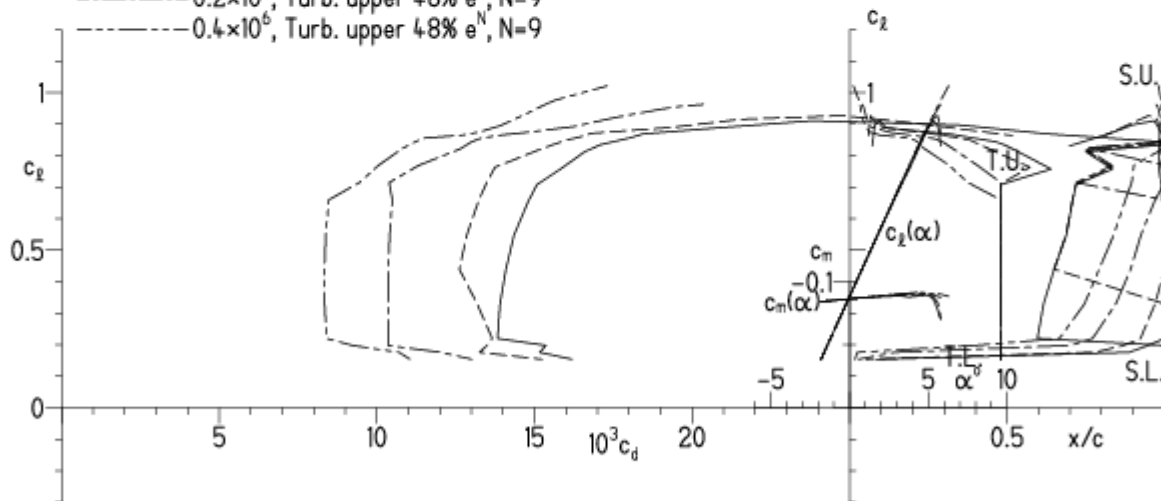
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

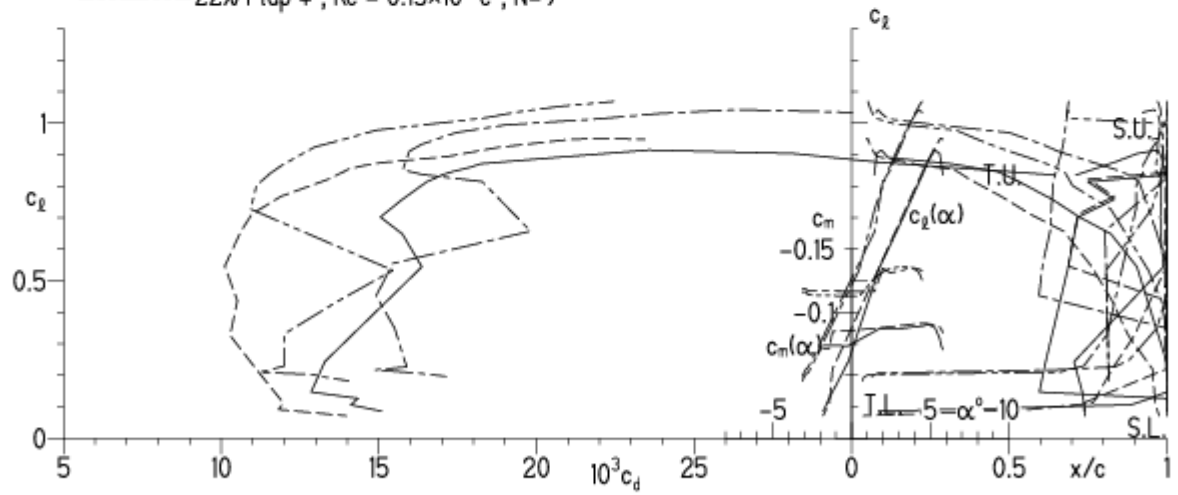


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

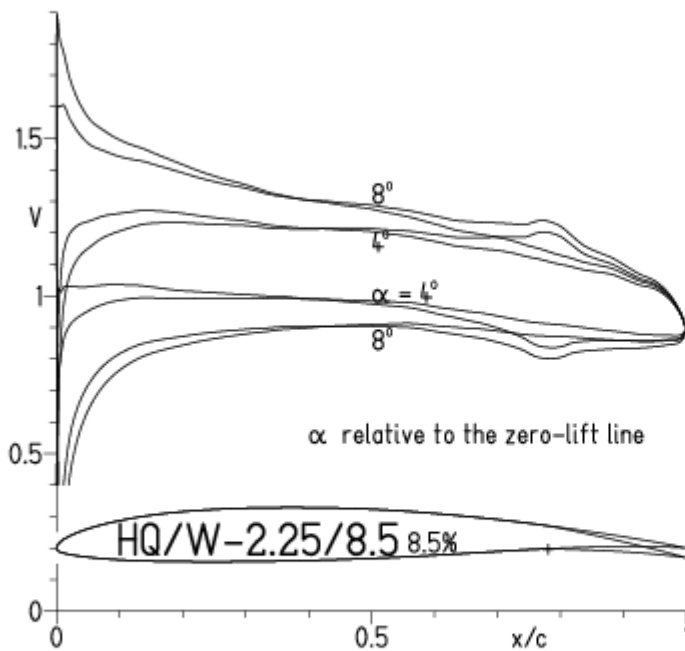
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

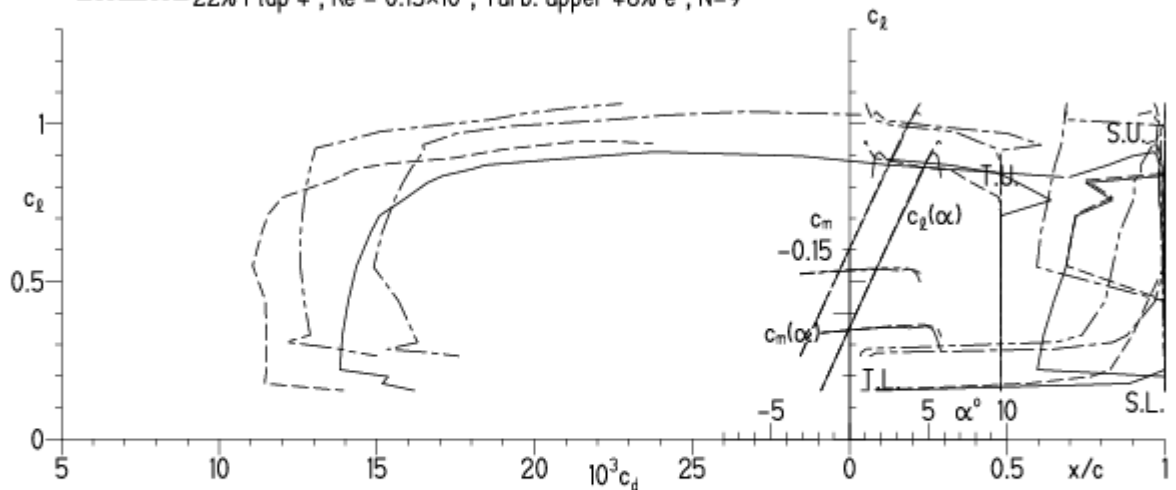


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

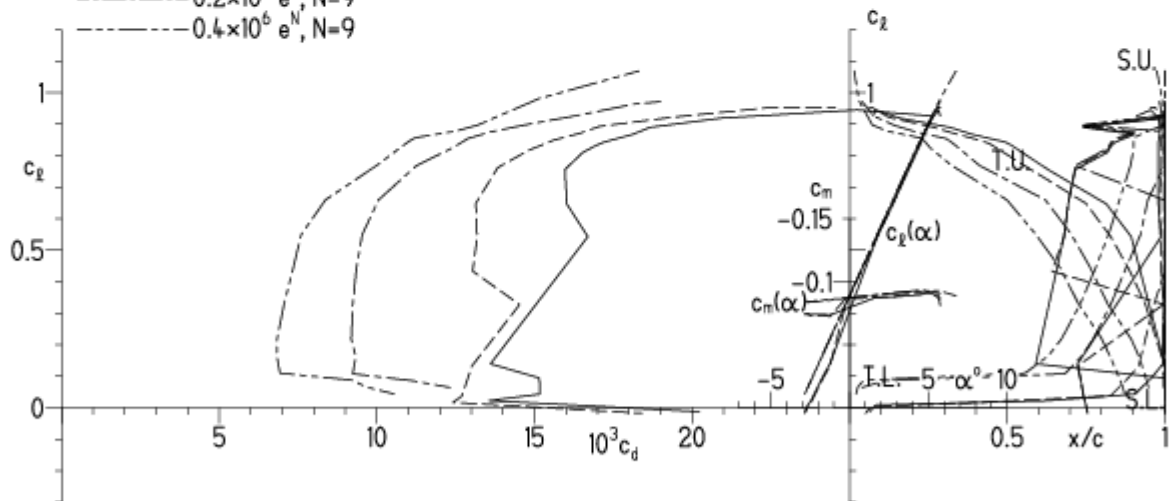
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

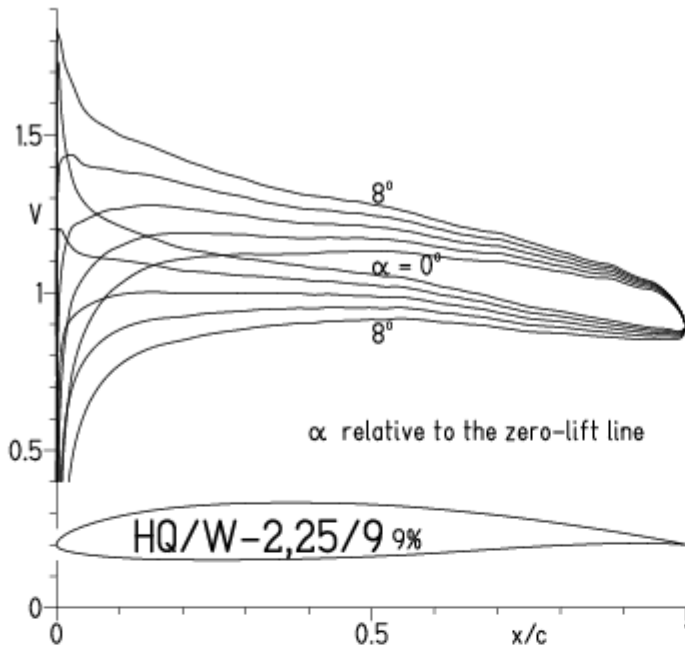
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

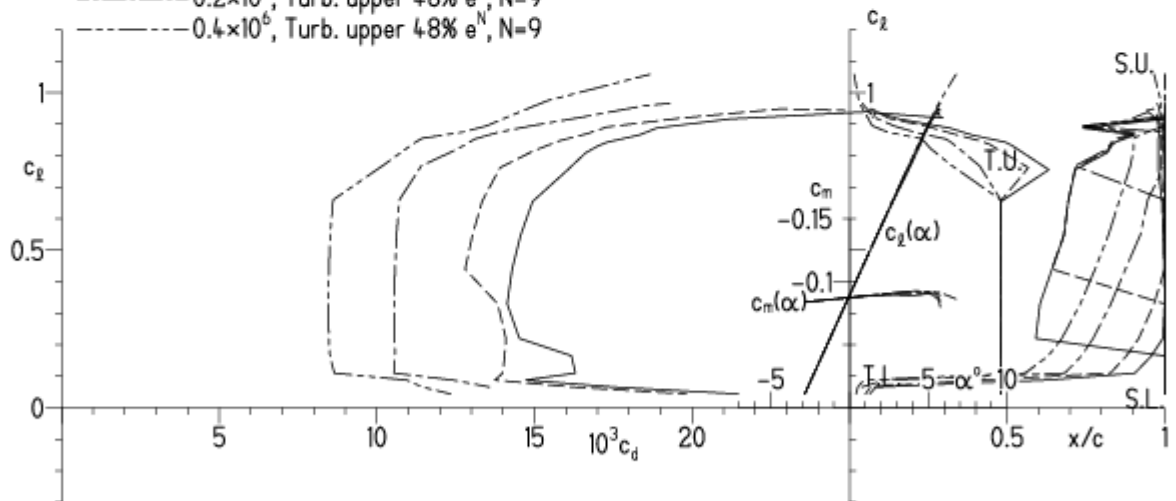
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

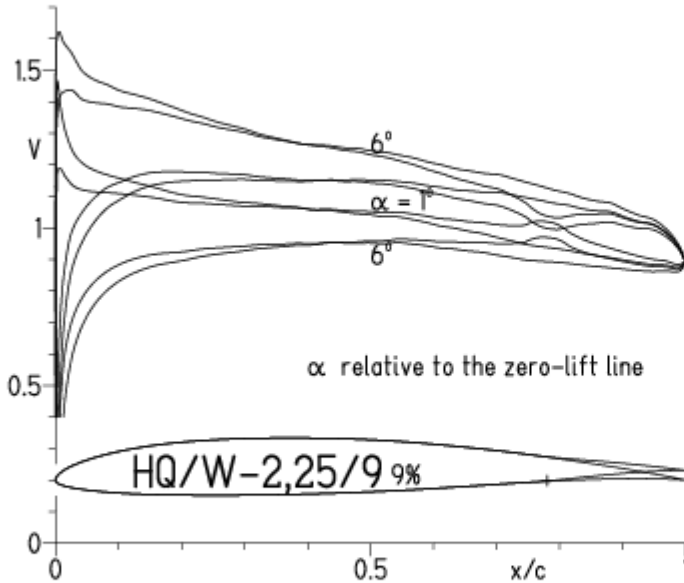
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

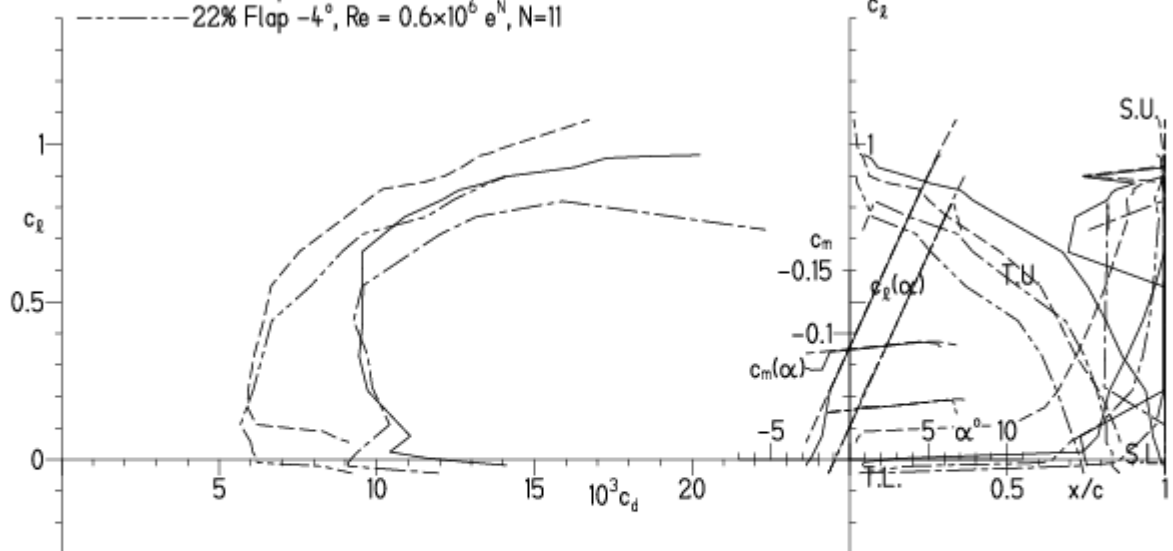
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$

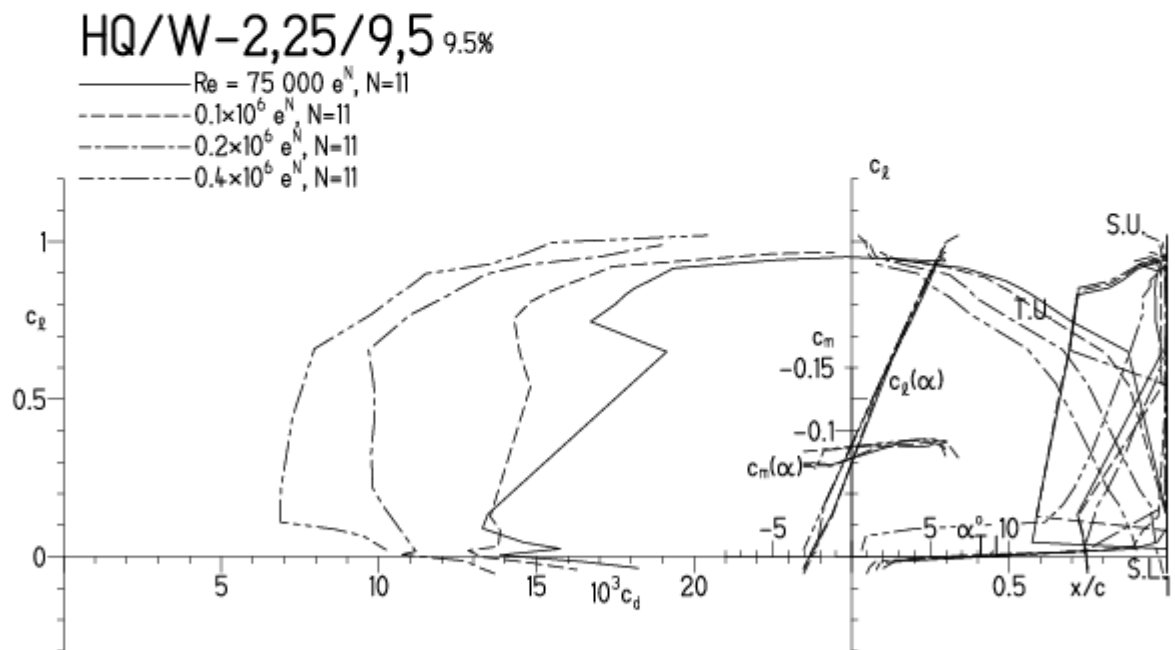


HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

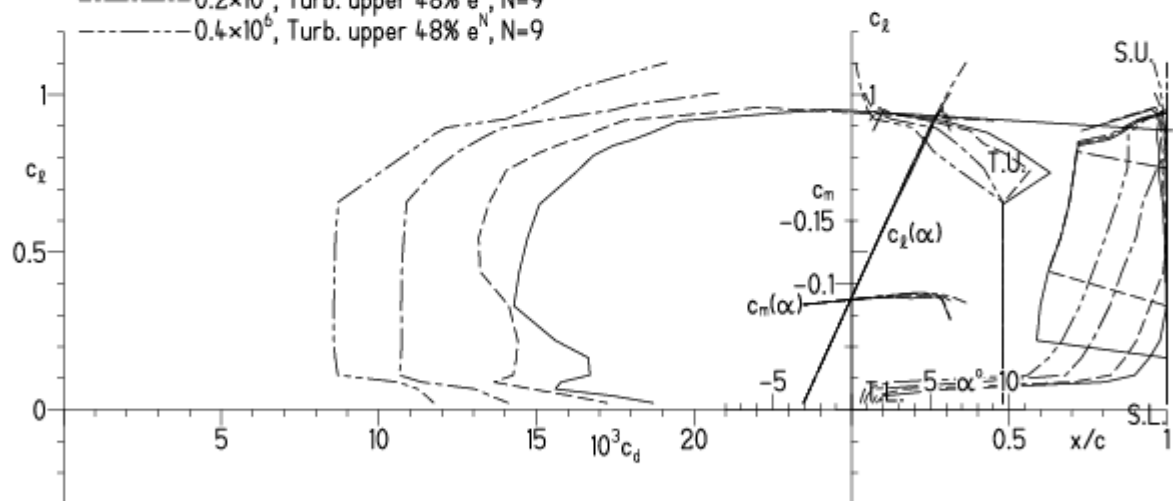
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

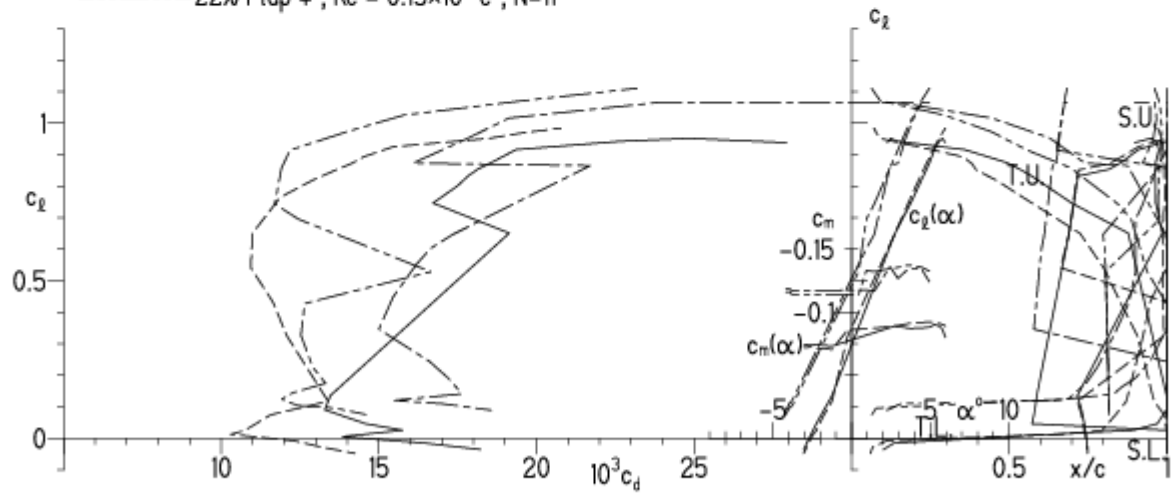


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

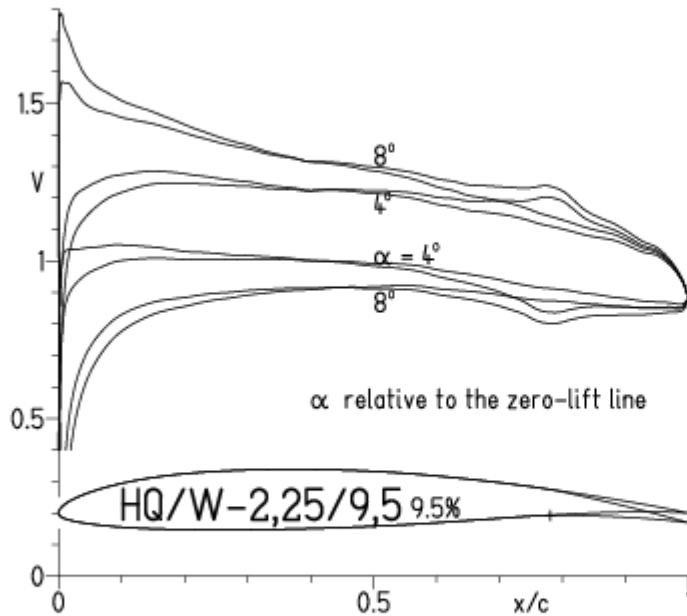
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

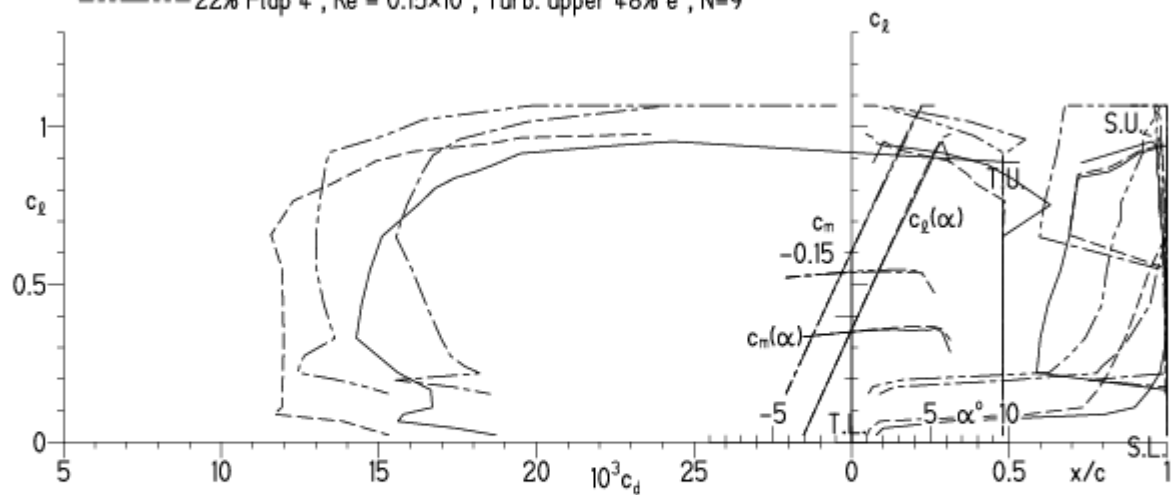


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



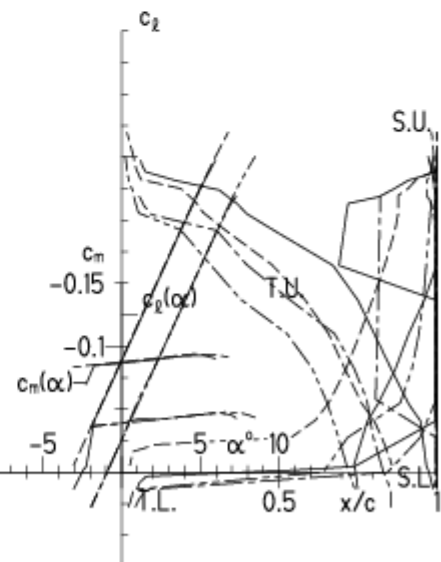
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

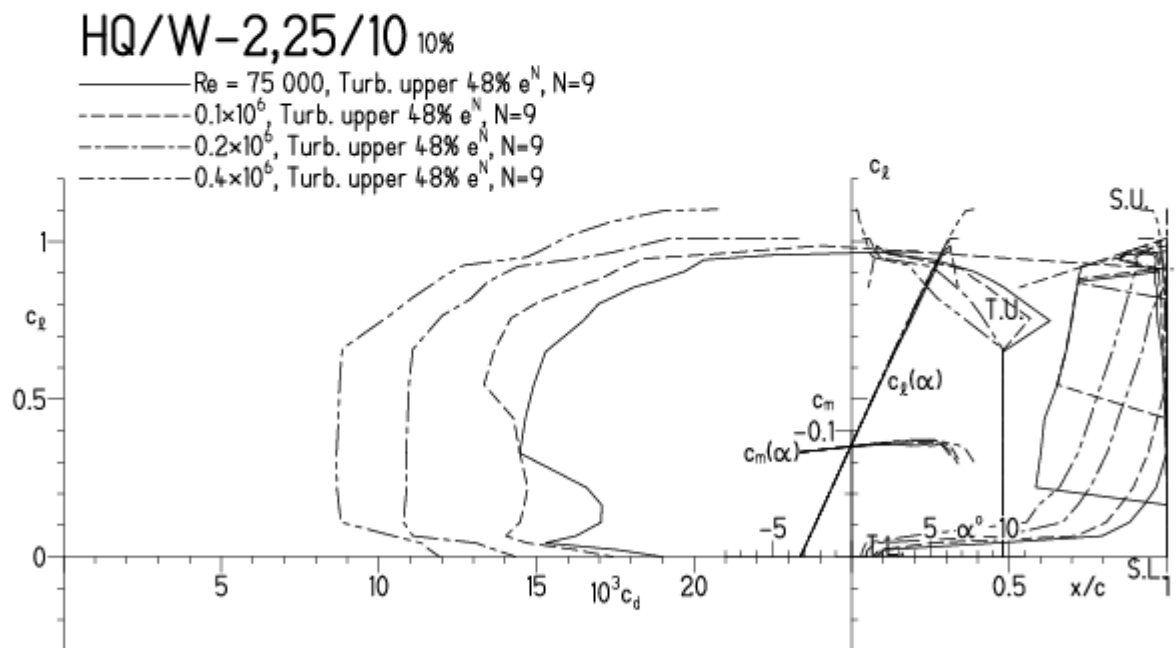


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

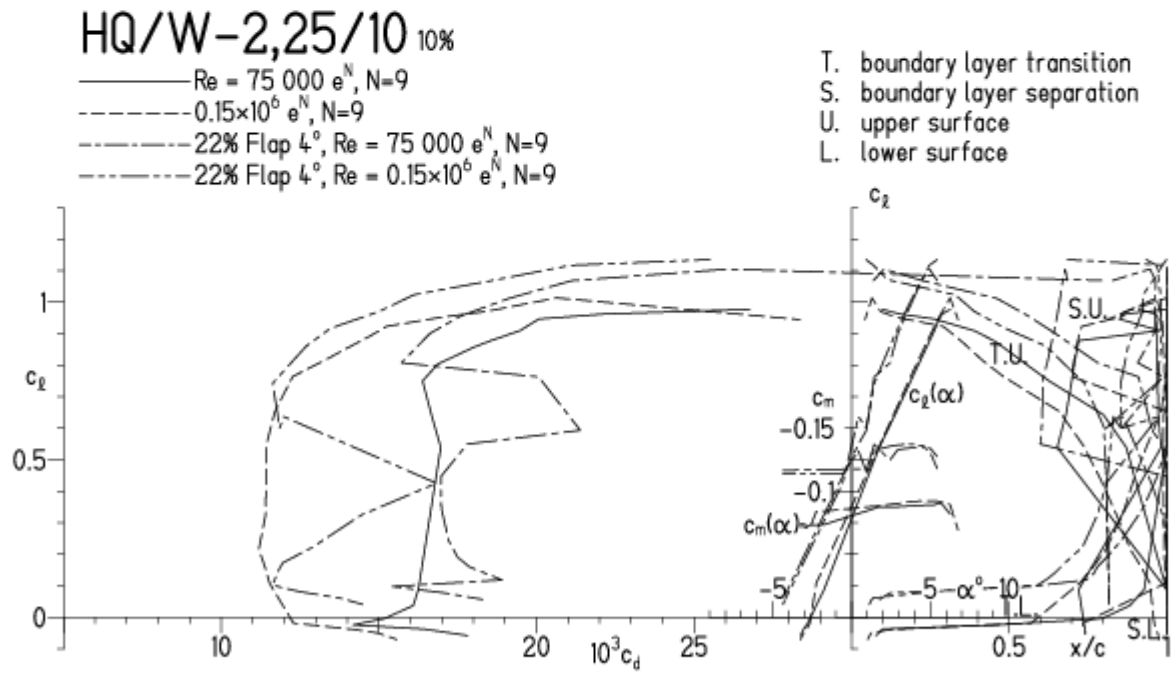


HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

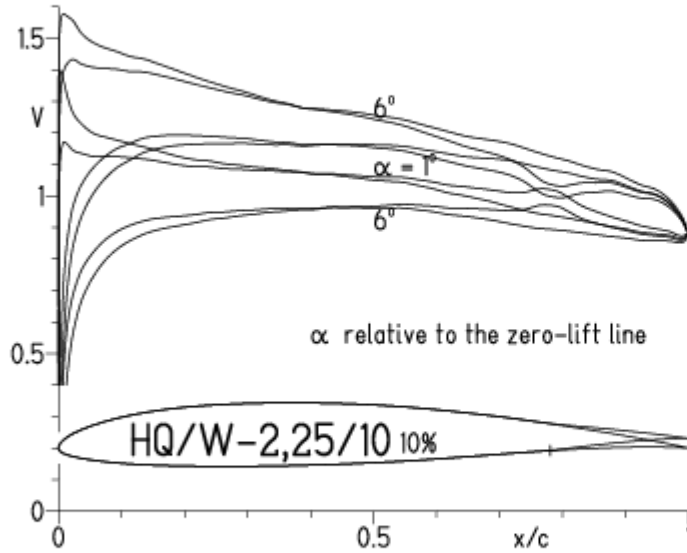
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

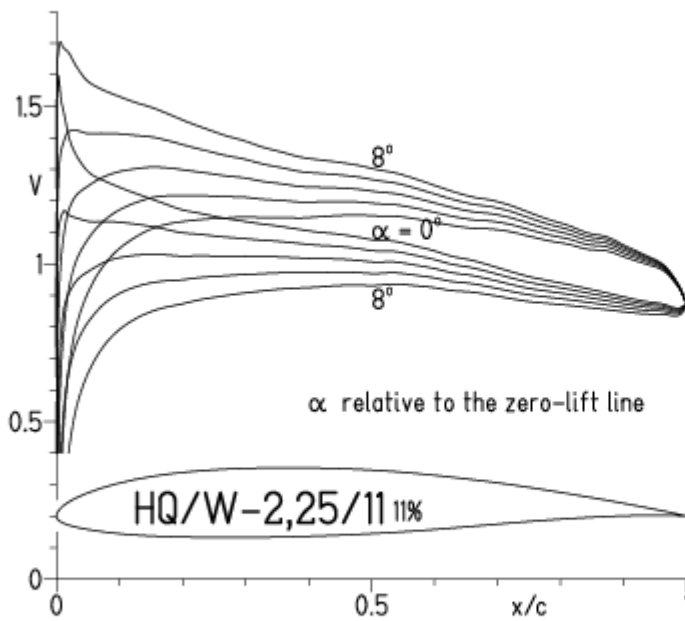


EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

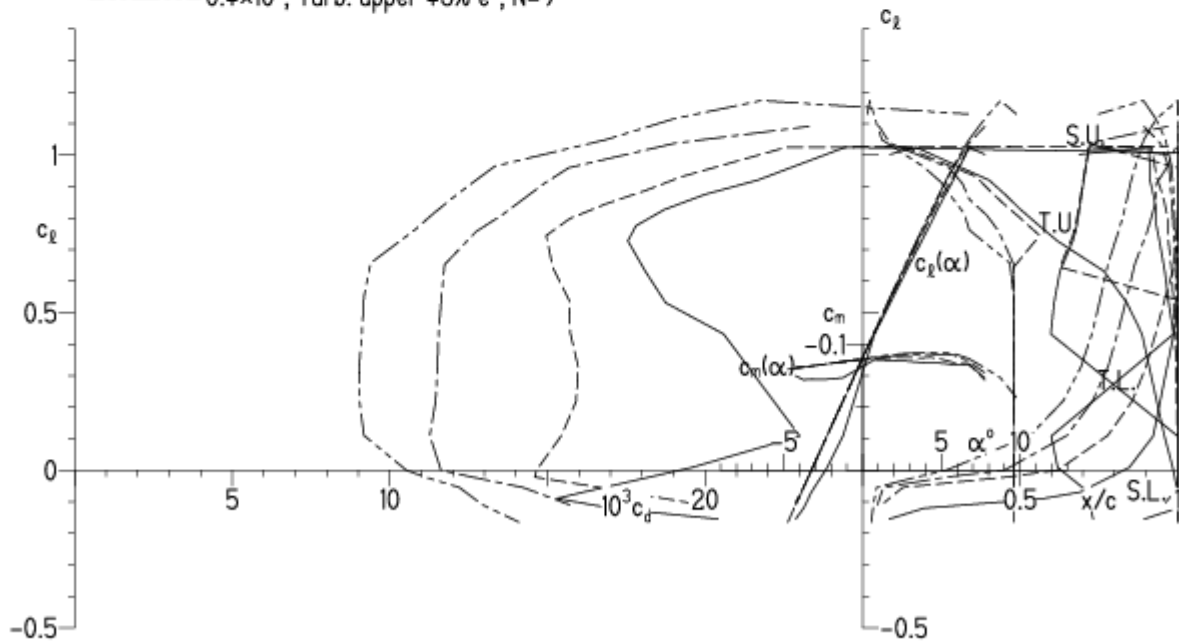
EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

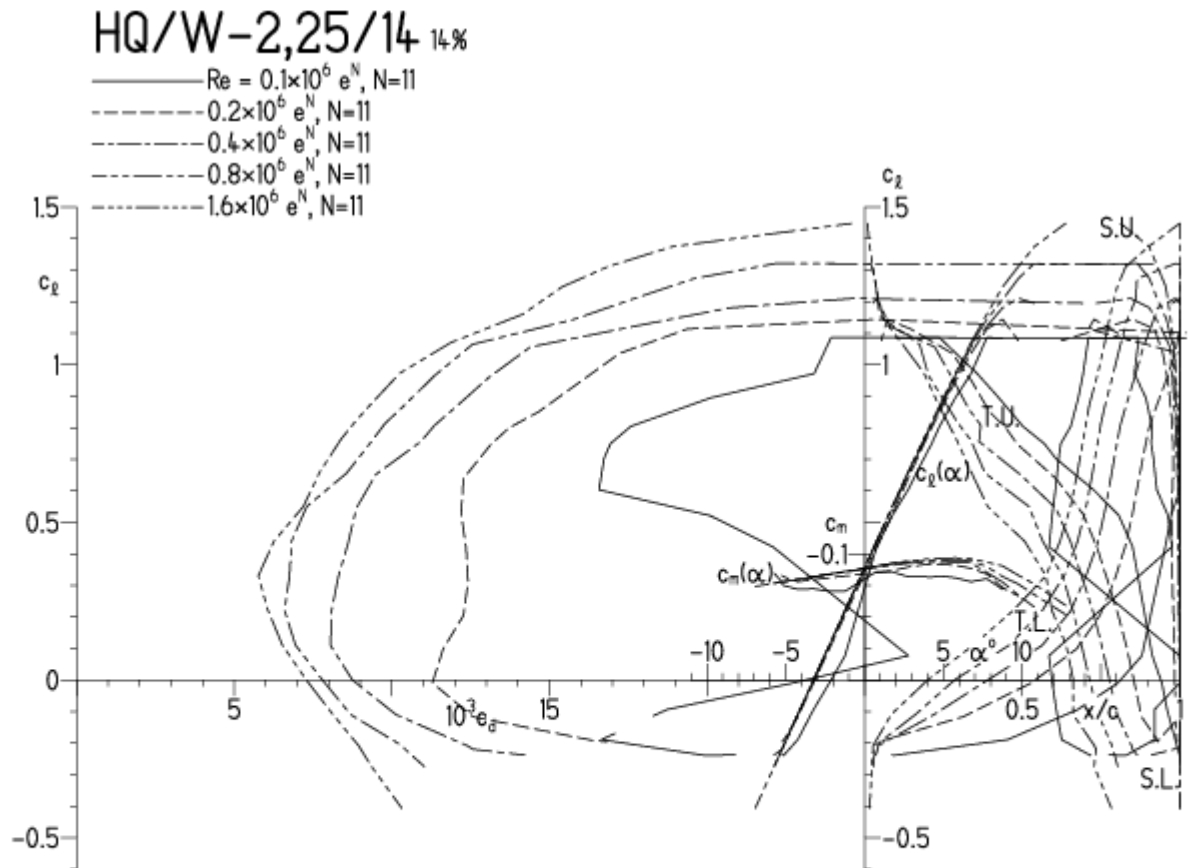


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

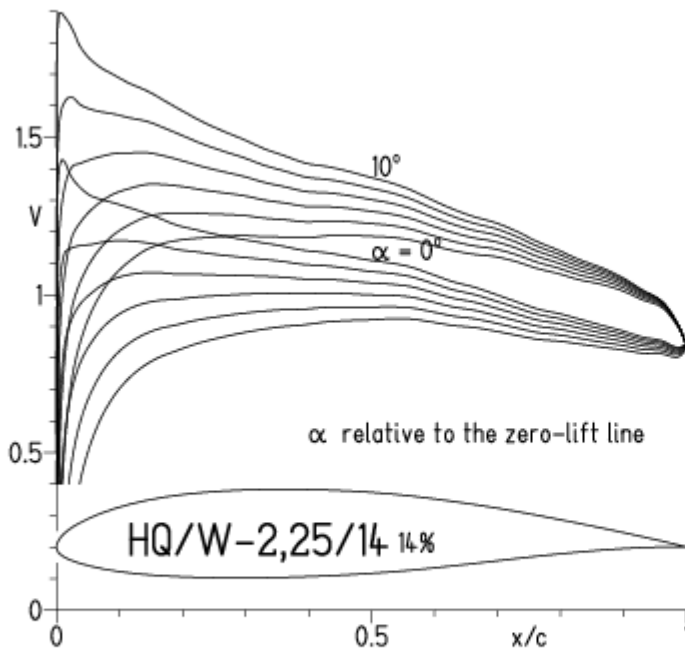


EPPLER 2005 V. 8.

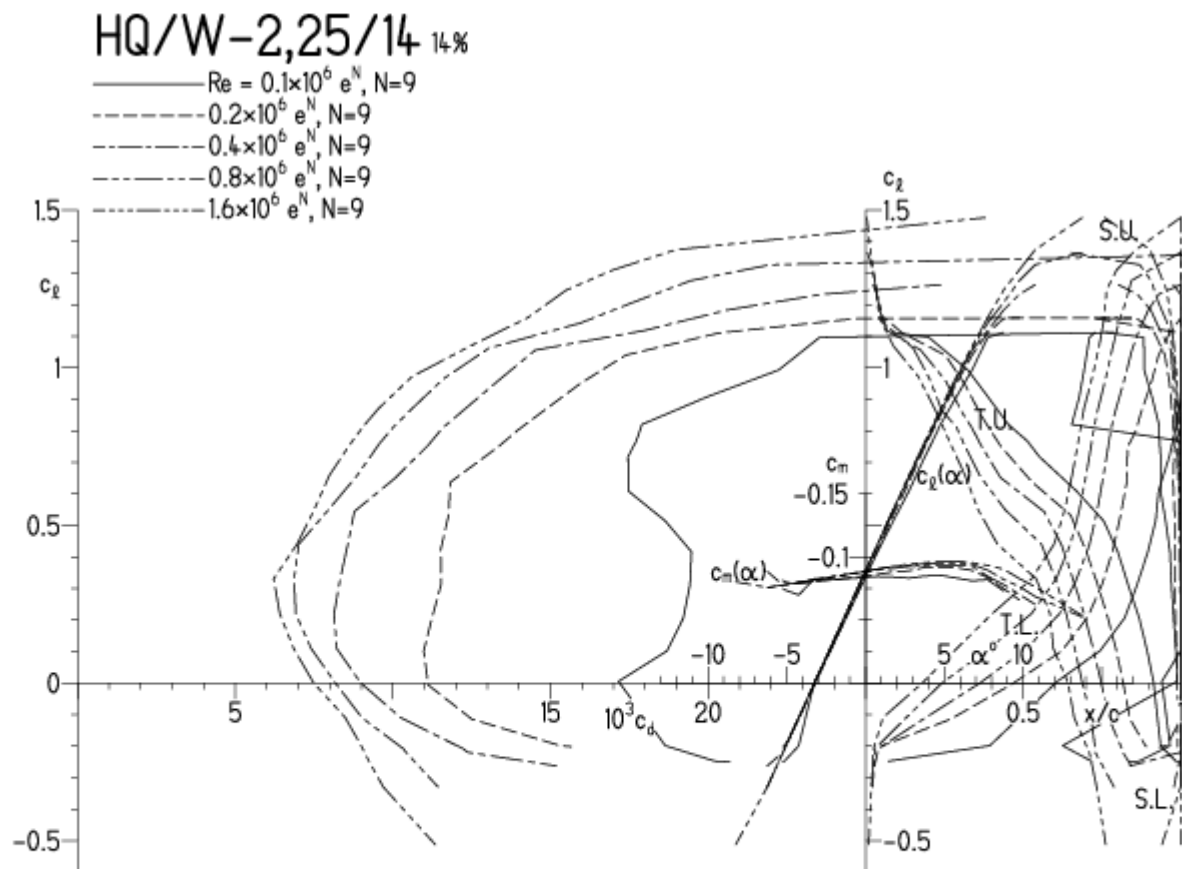


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

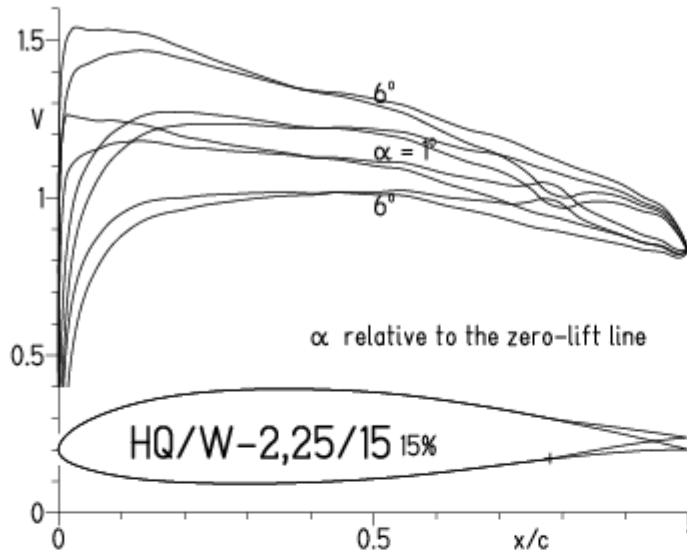


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2,25/8,5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

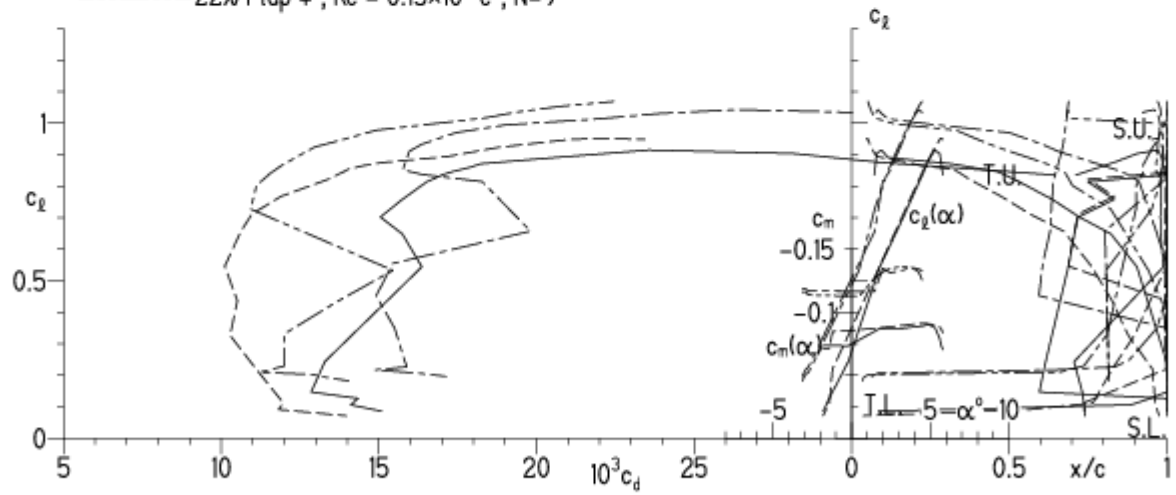


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

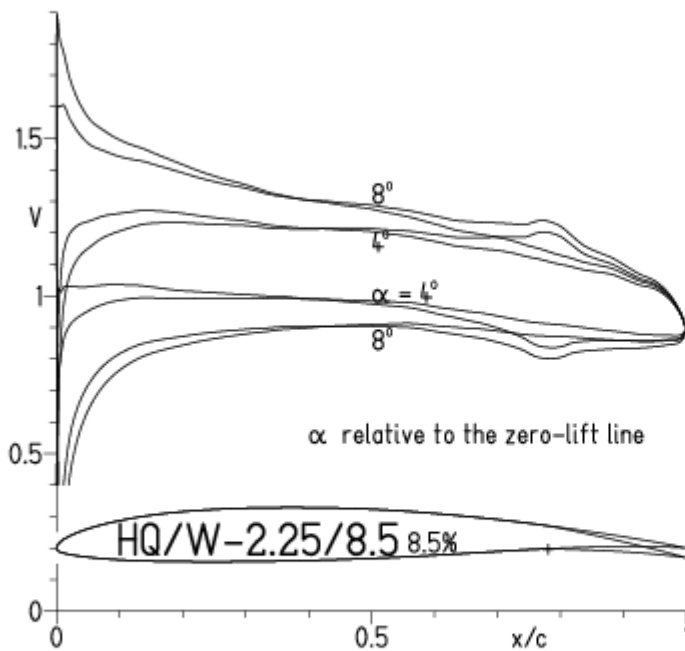
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

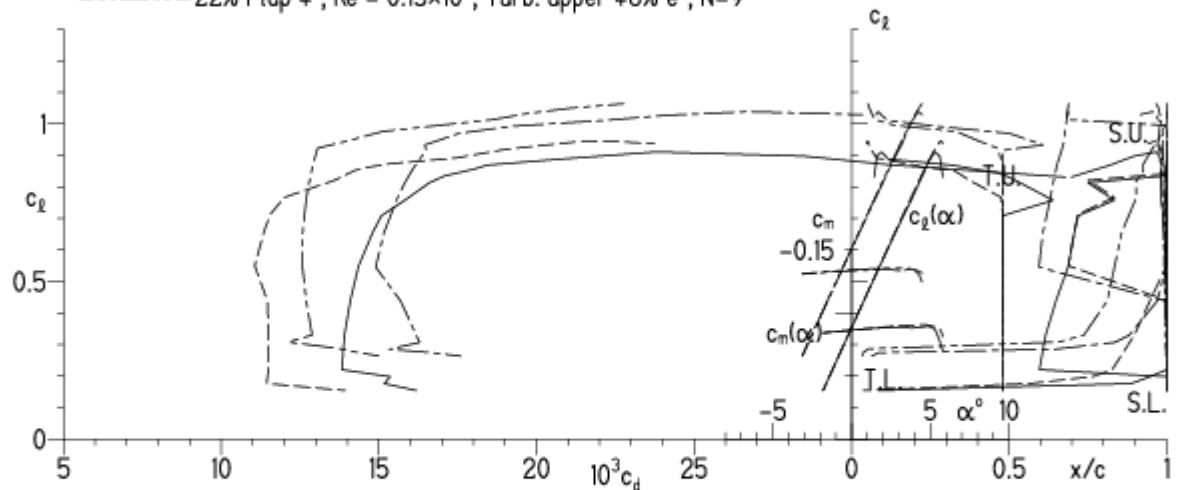


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

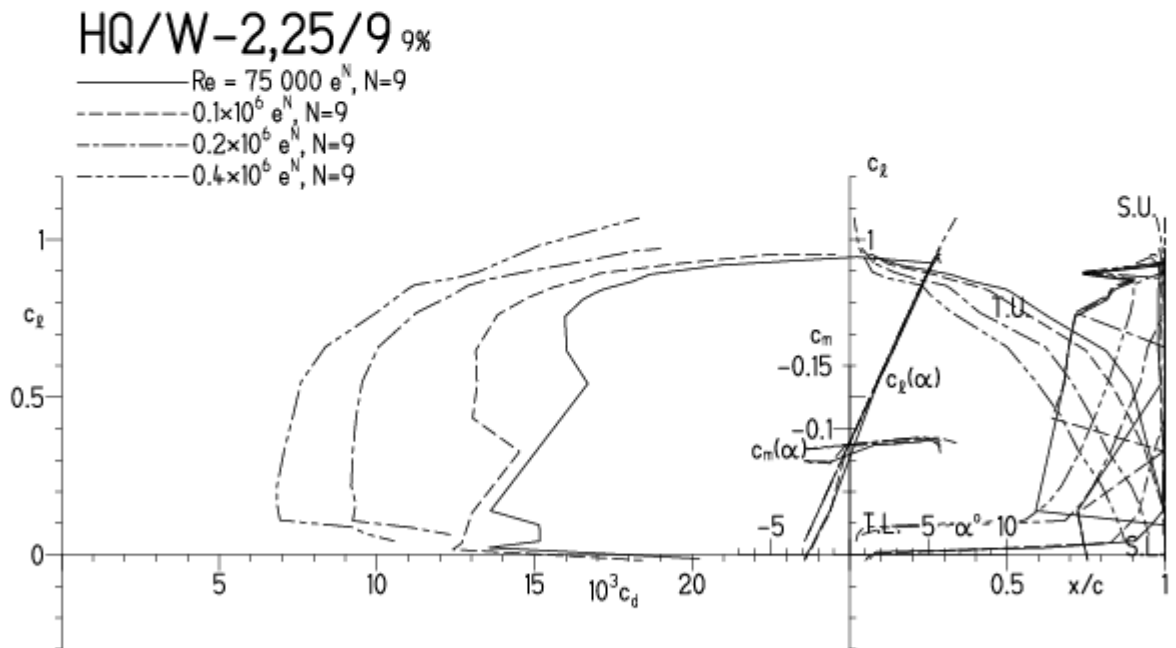


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

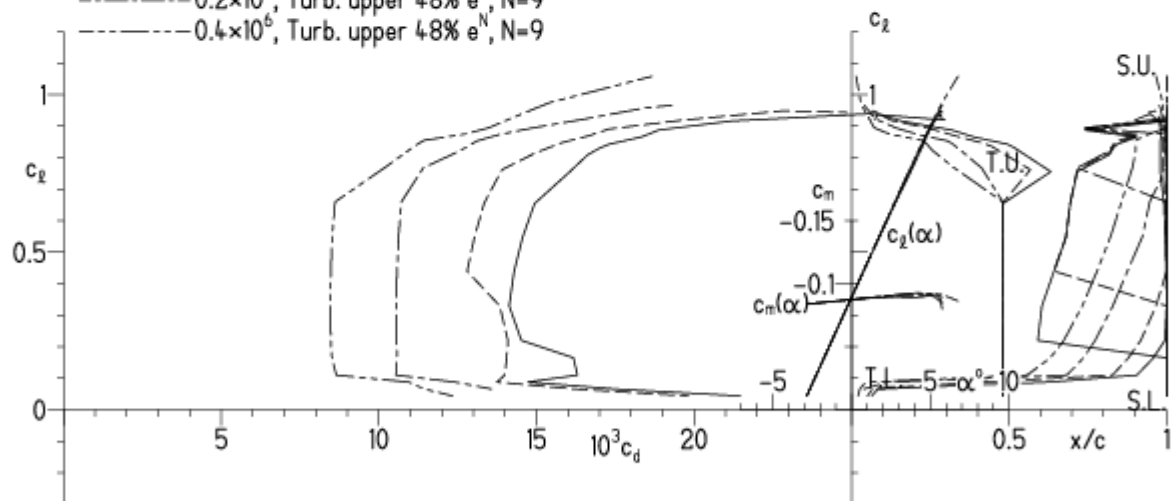
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- Re = 75 000 e^N, N=9
- - - 0.15x10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

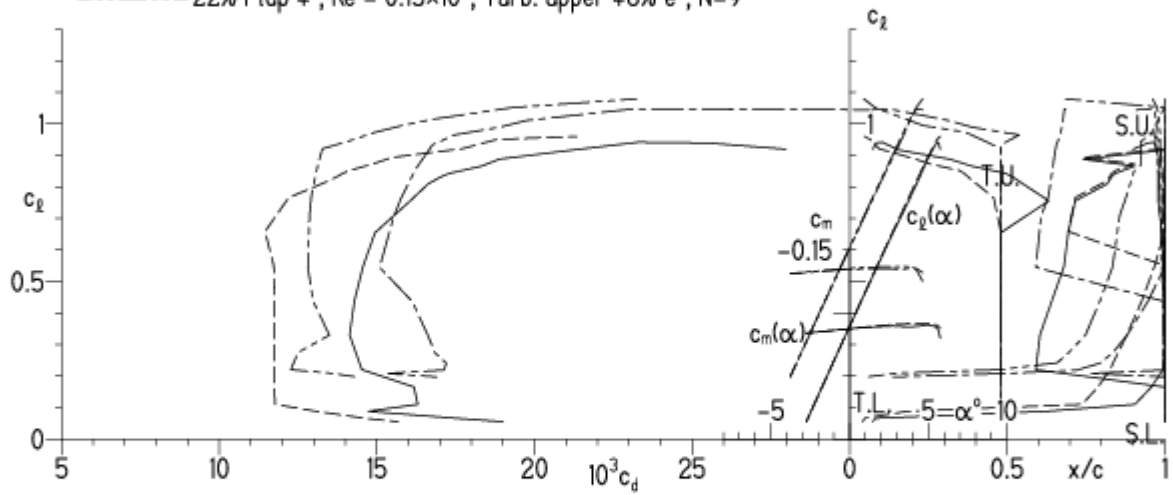


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



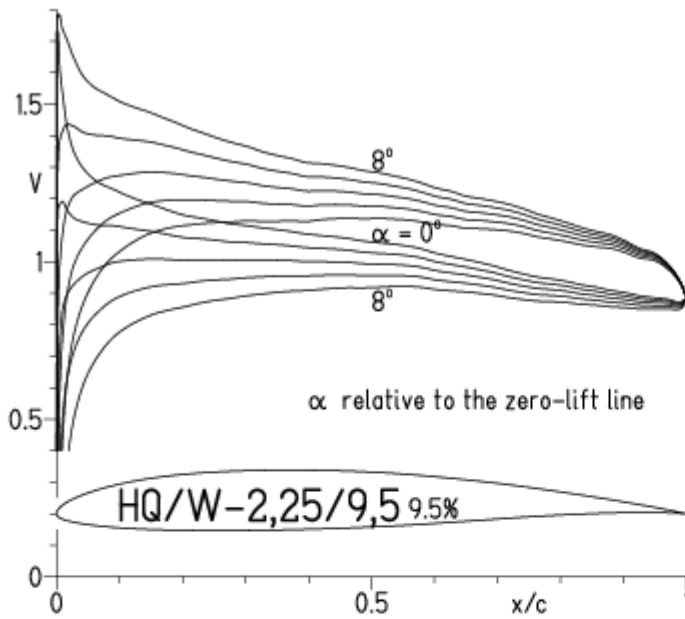
EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

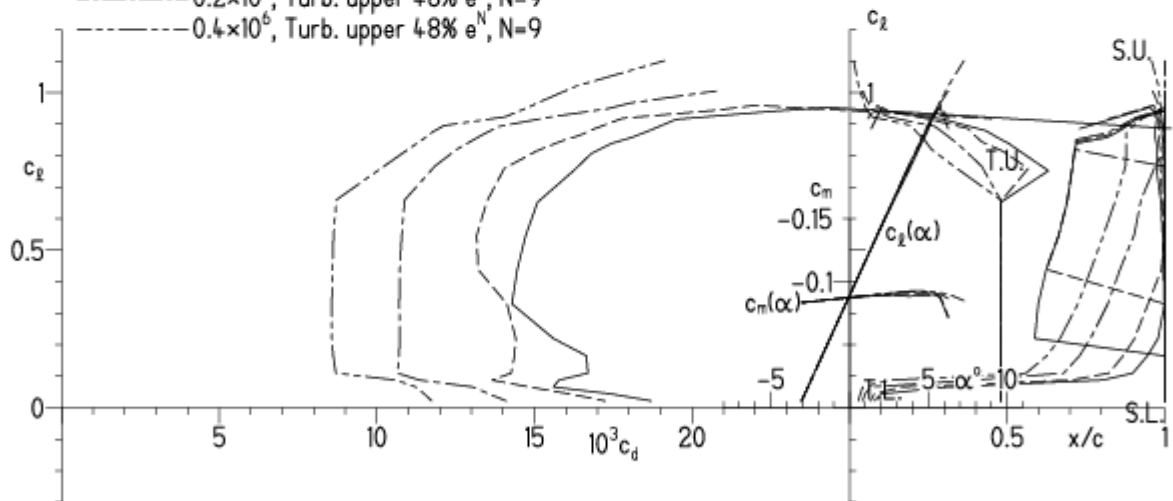
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

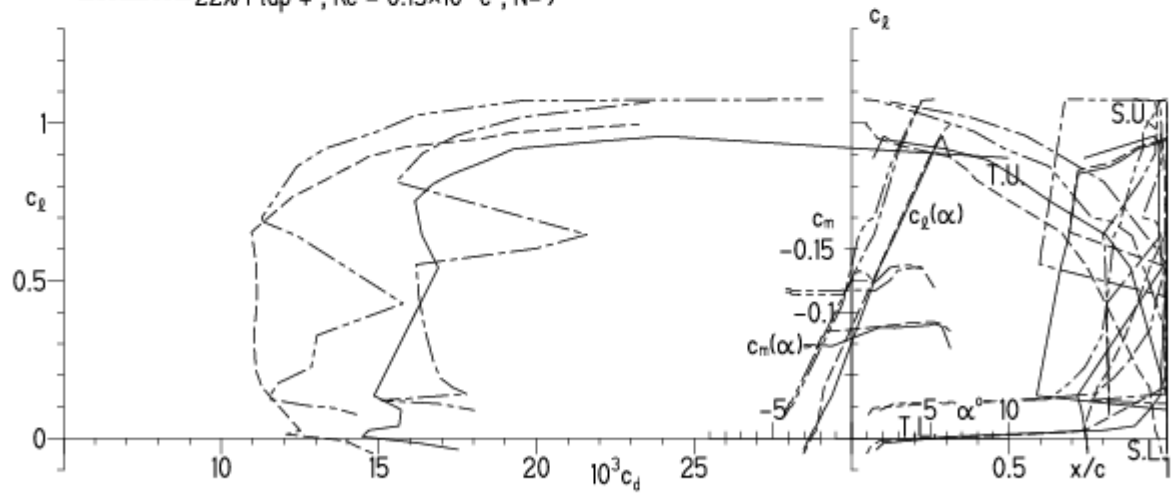


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

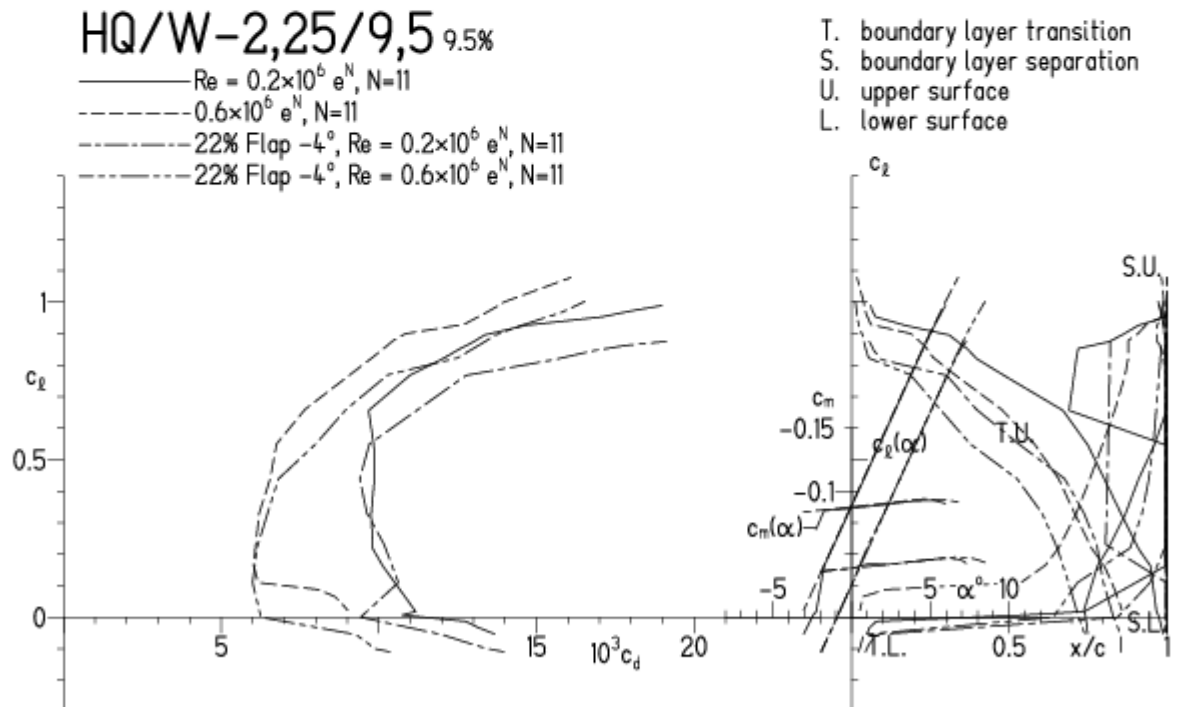


HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

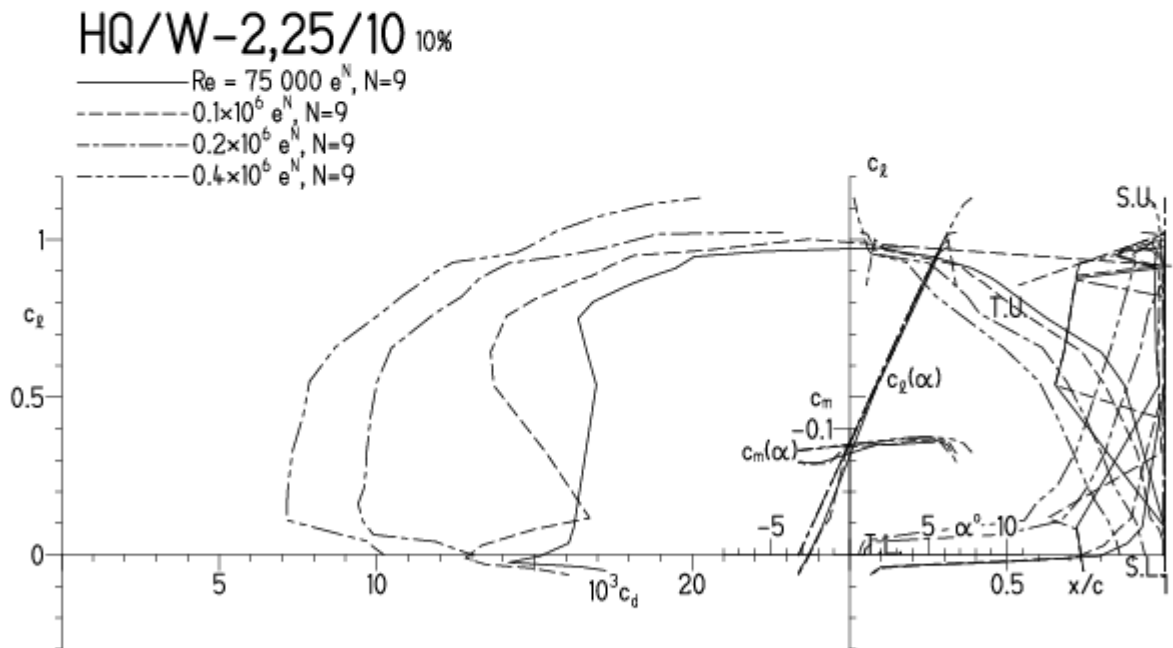


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

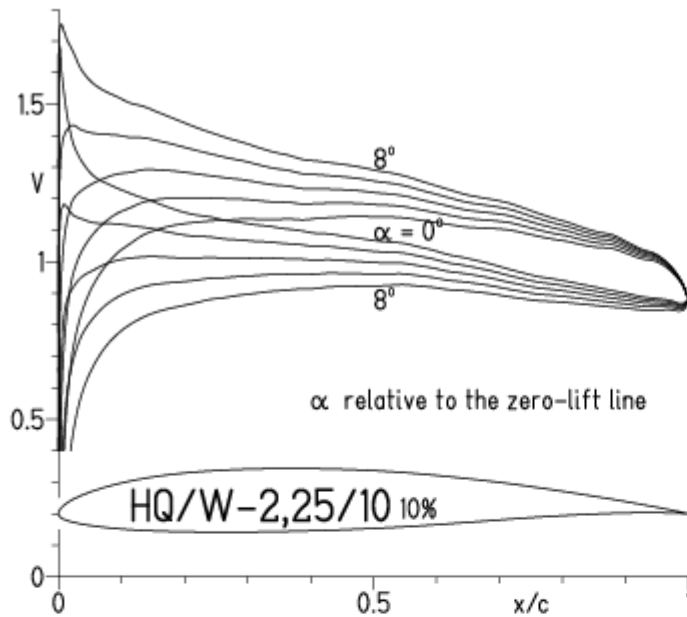


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

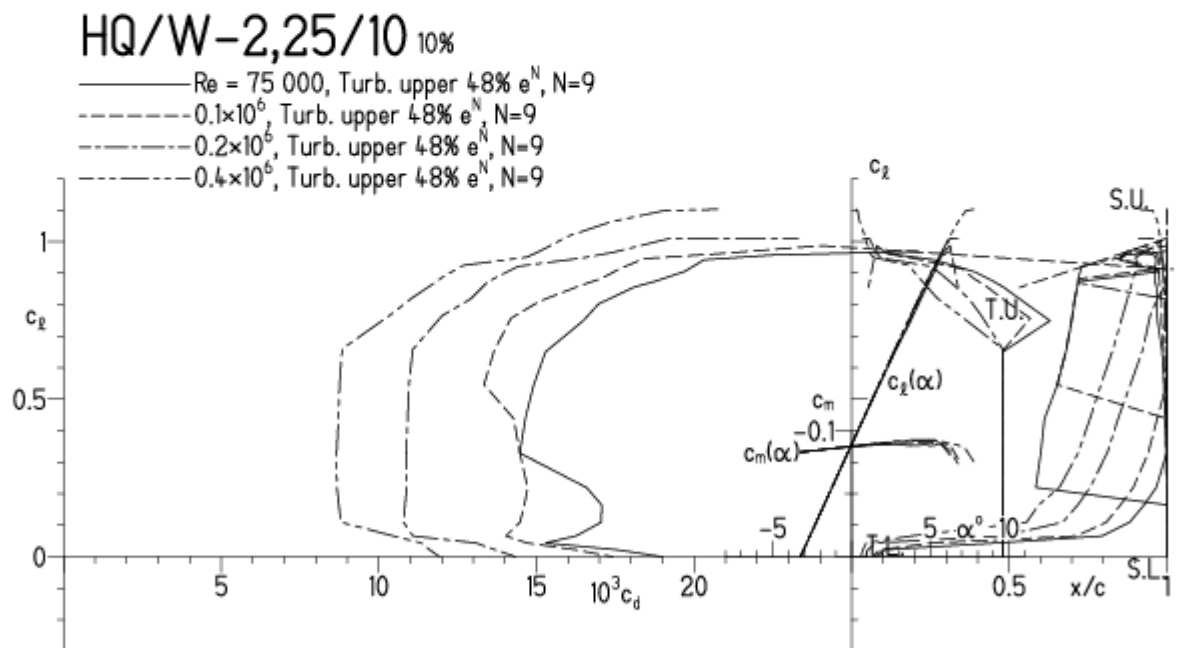


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

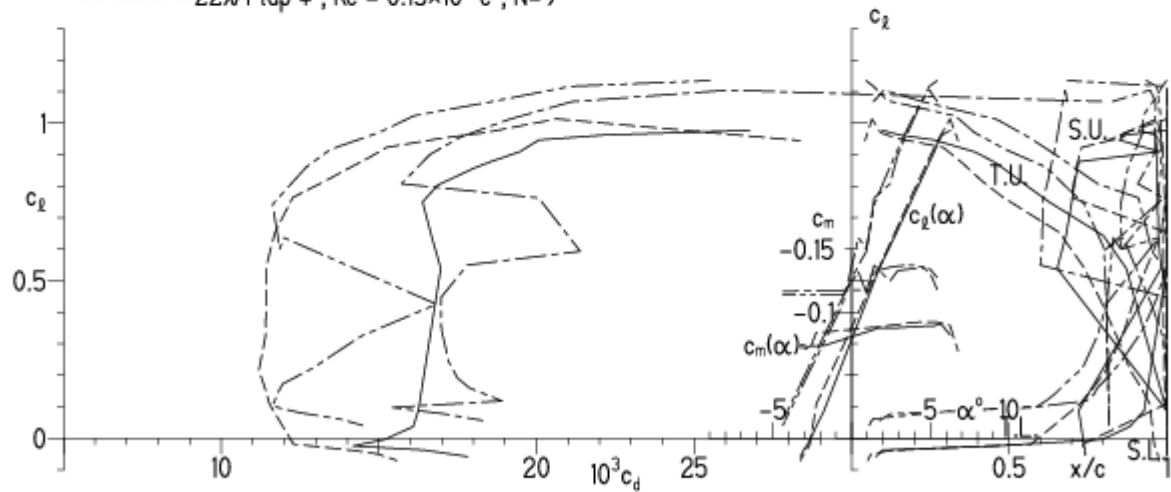


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

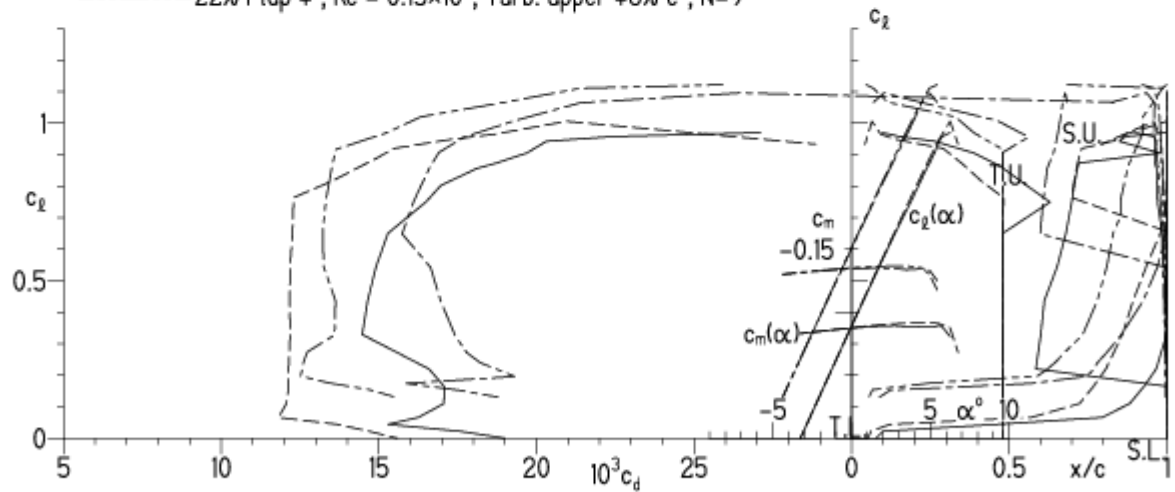


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

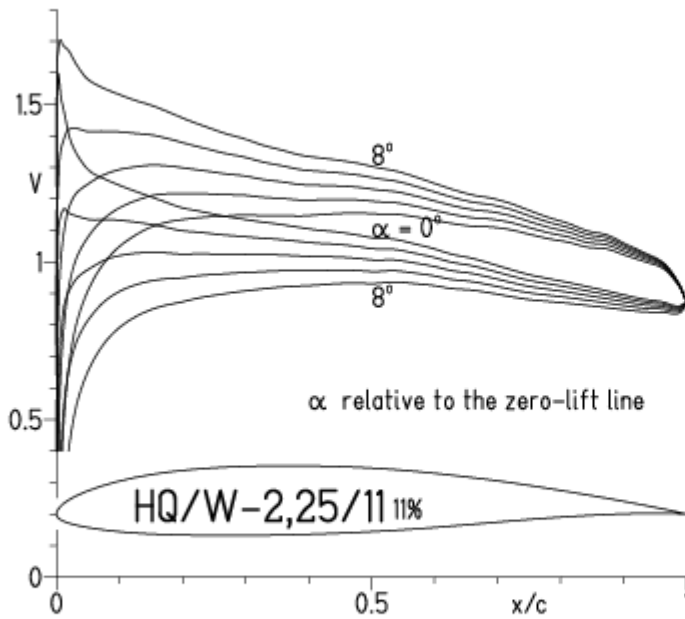


EPPLER 2005 V. 8.5.07 RUN

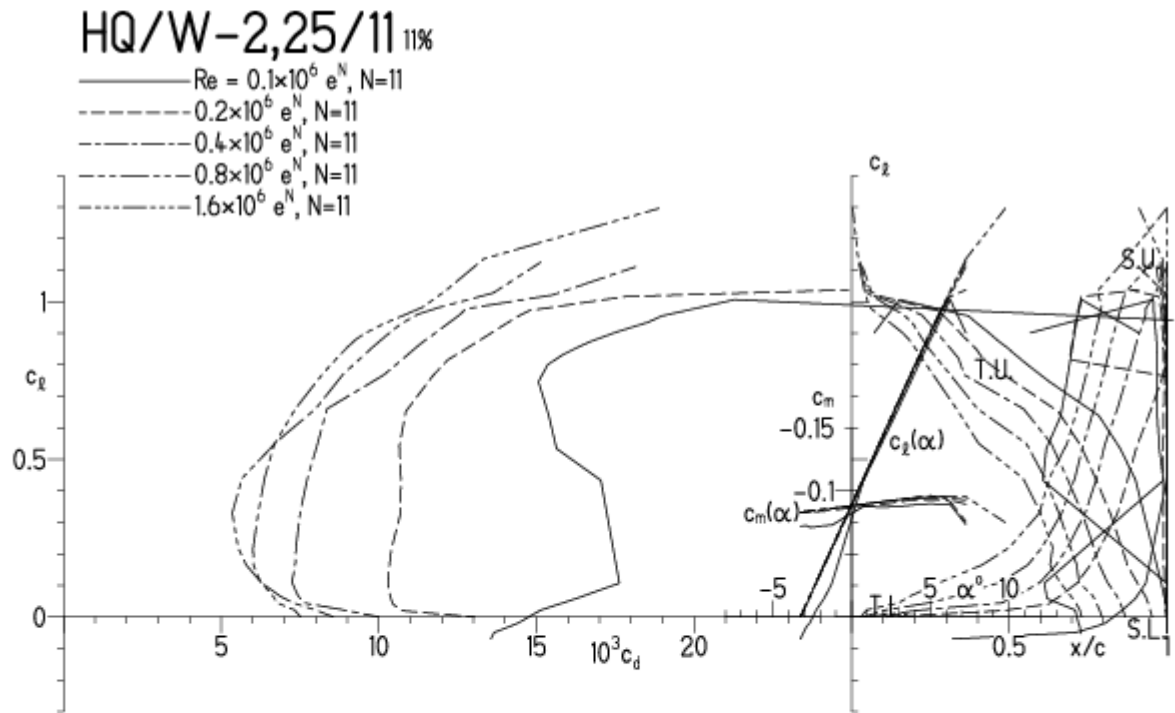


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

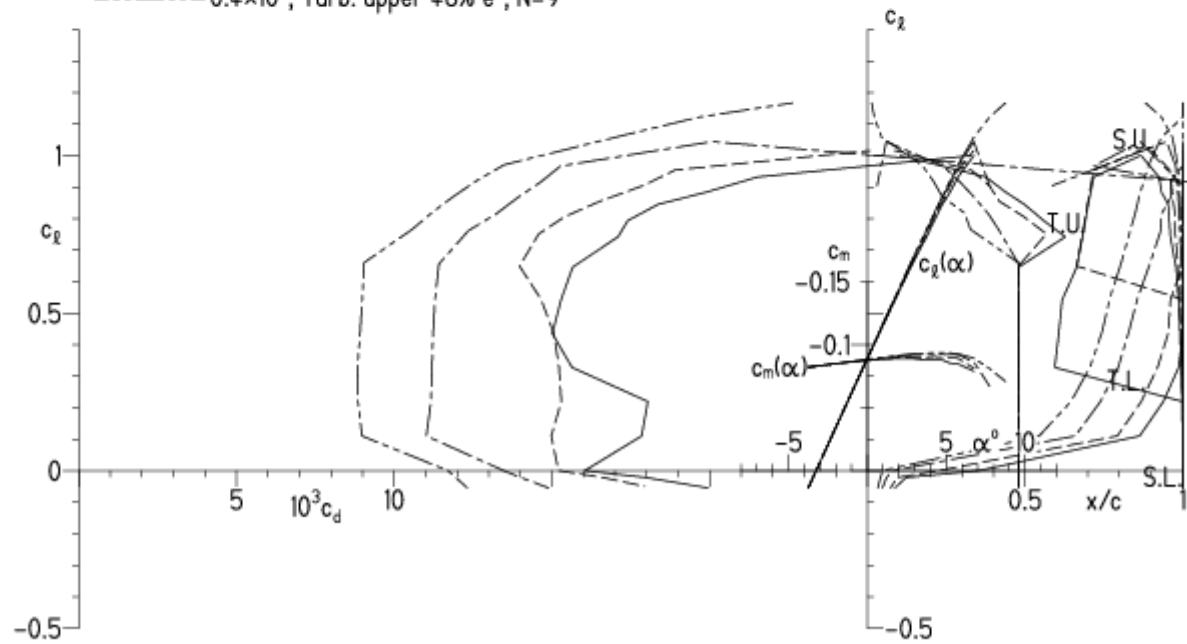
EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

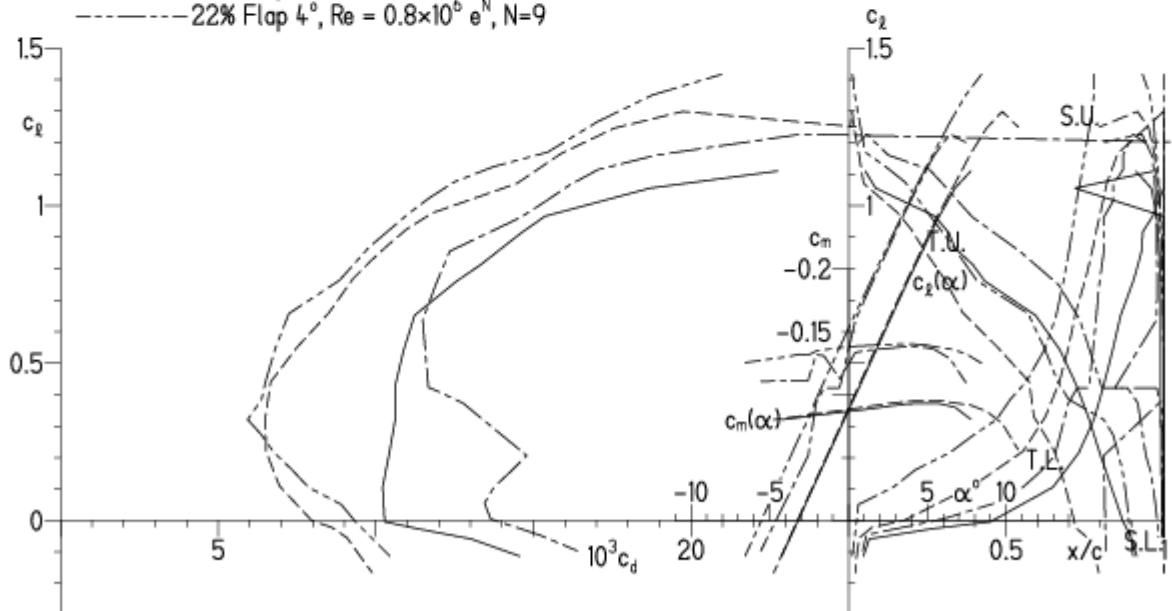


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

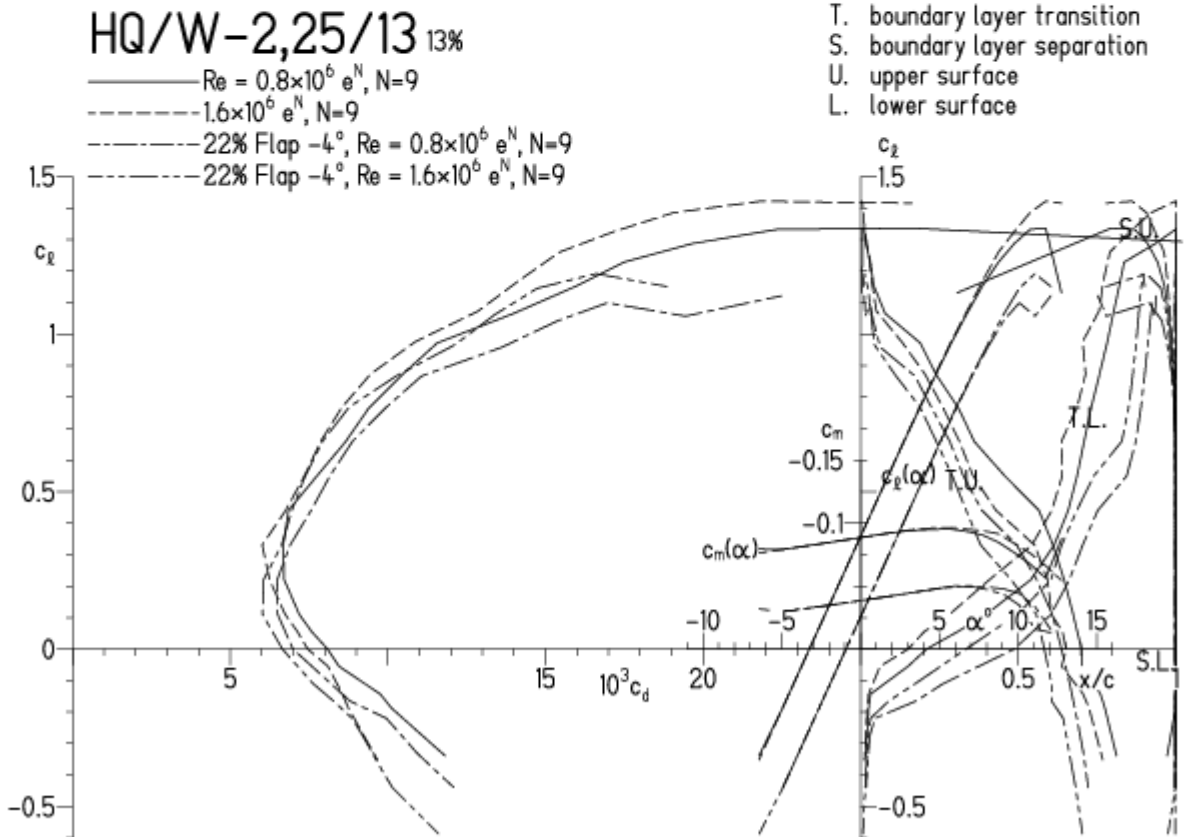


HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

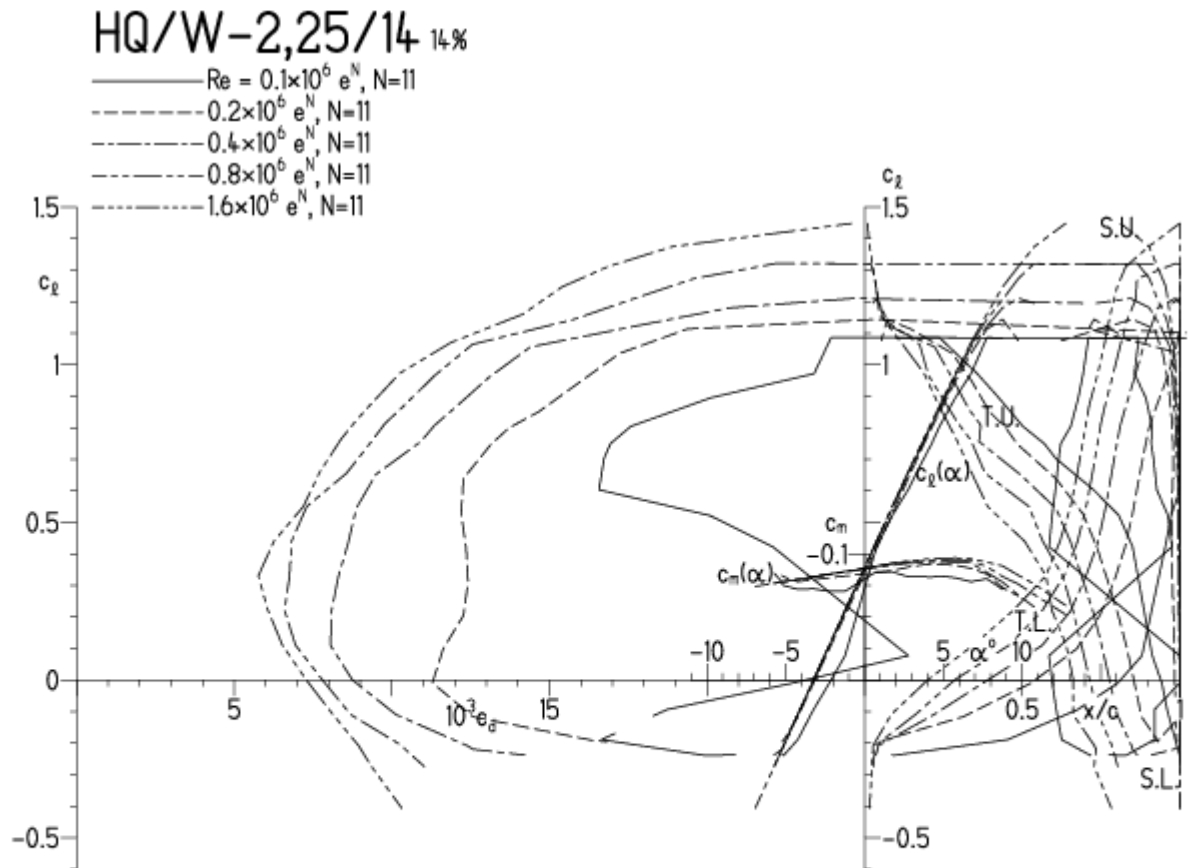


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

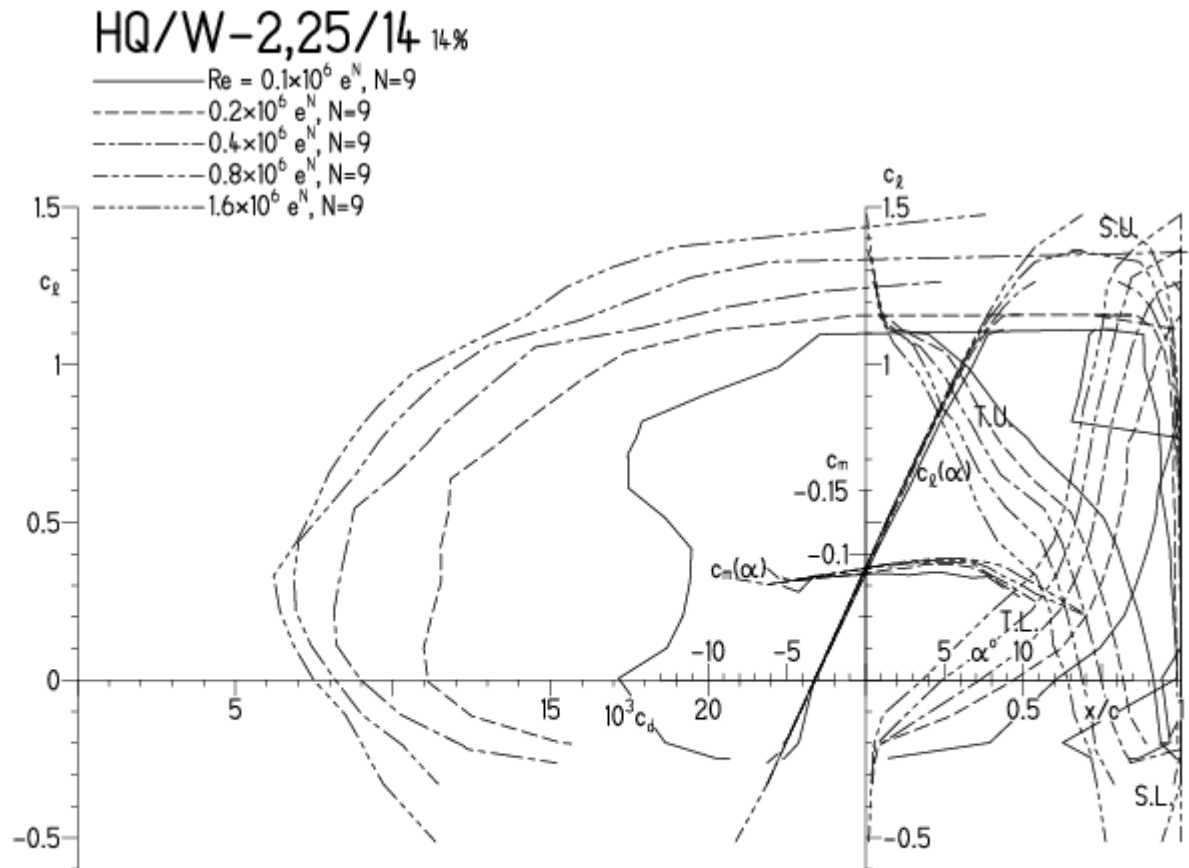


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

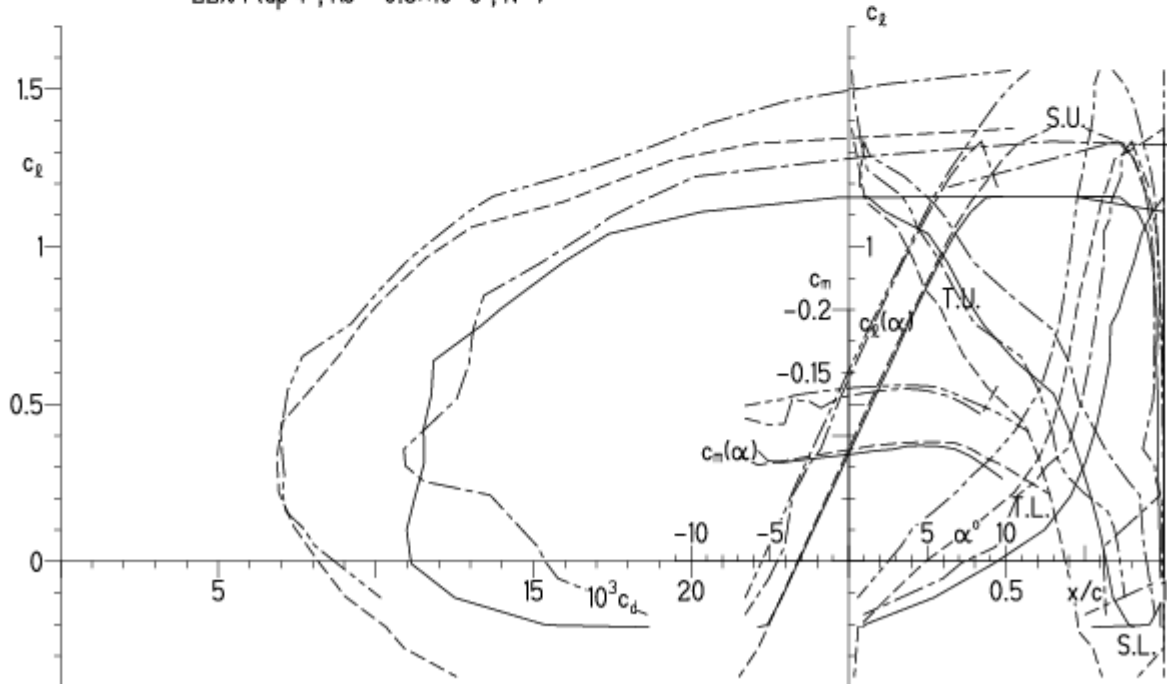


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

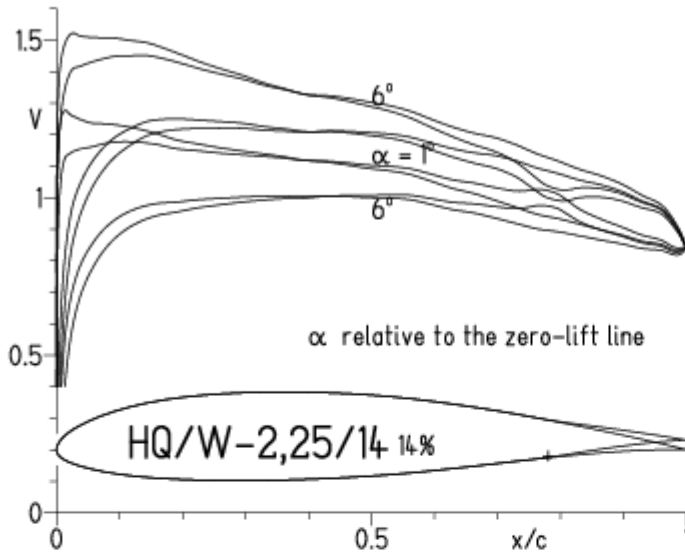
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

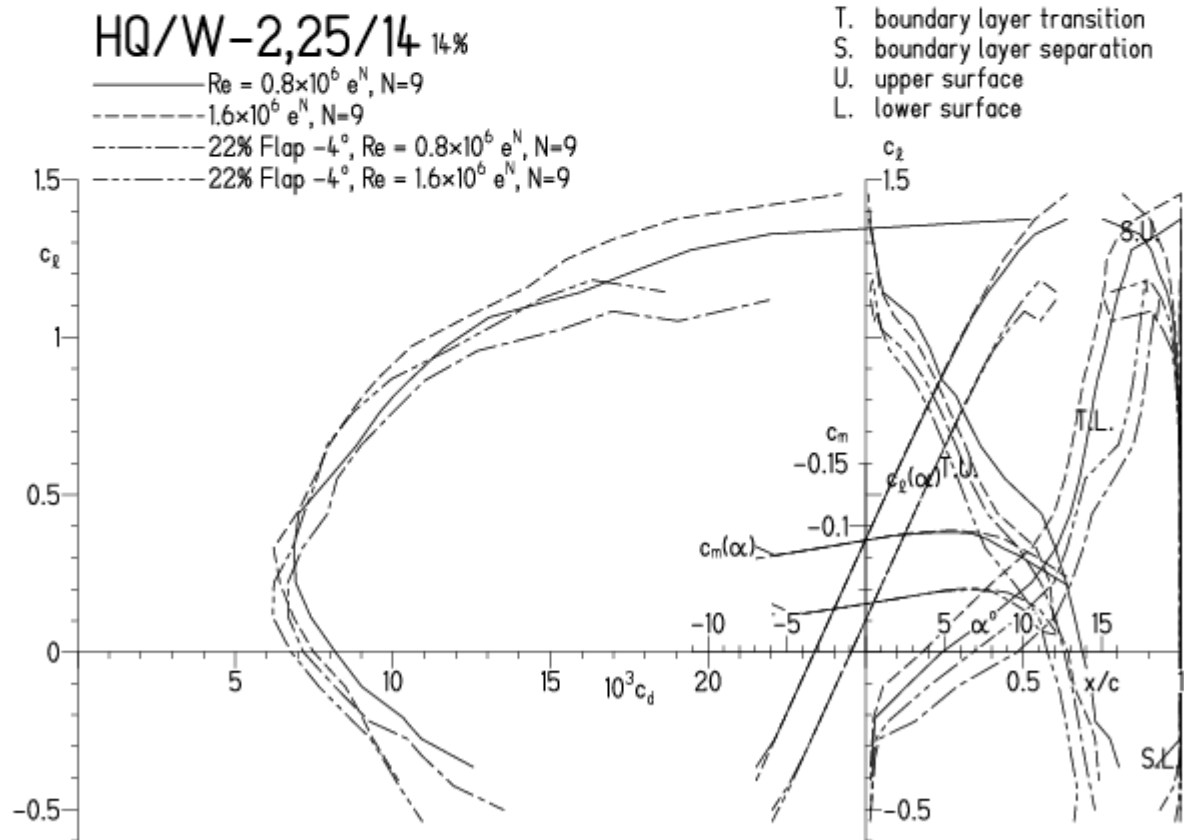


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

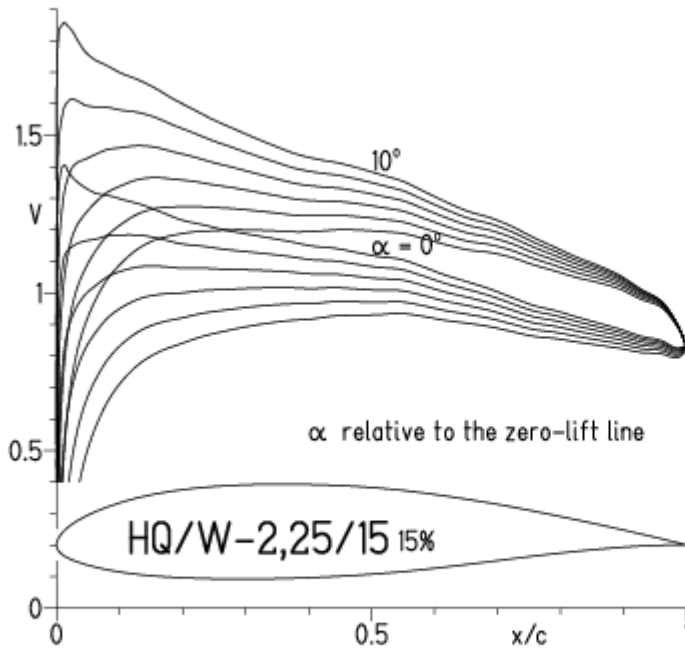


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

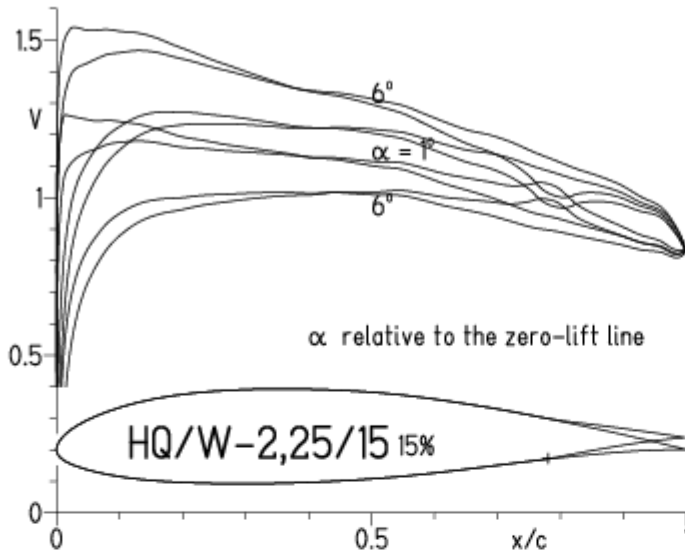


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

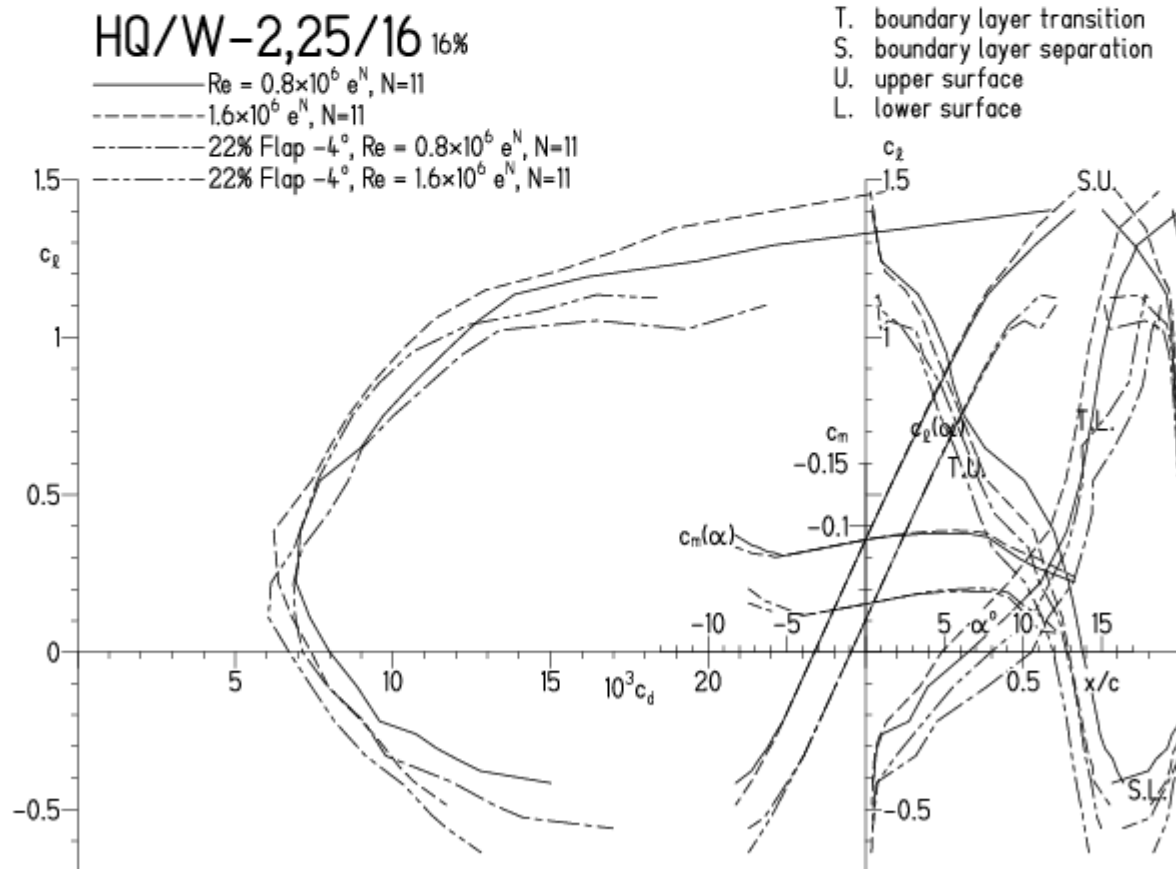
Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2,25/8,5 8.5%

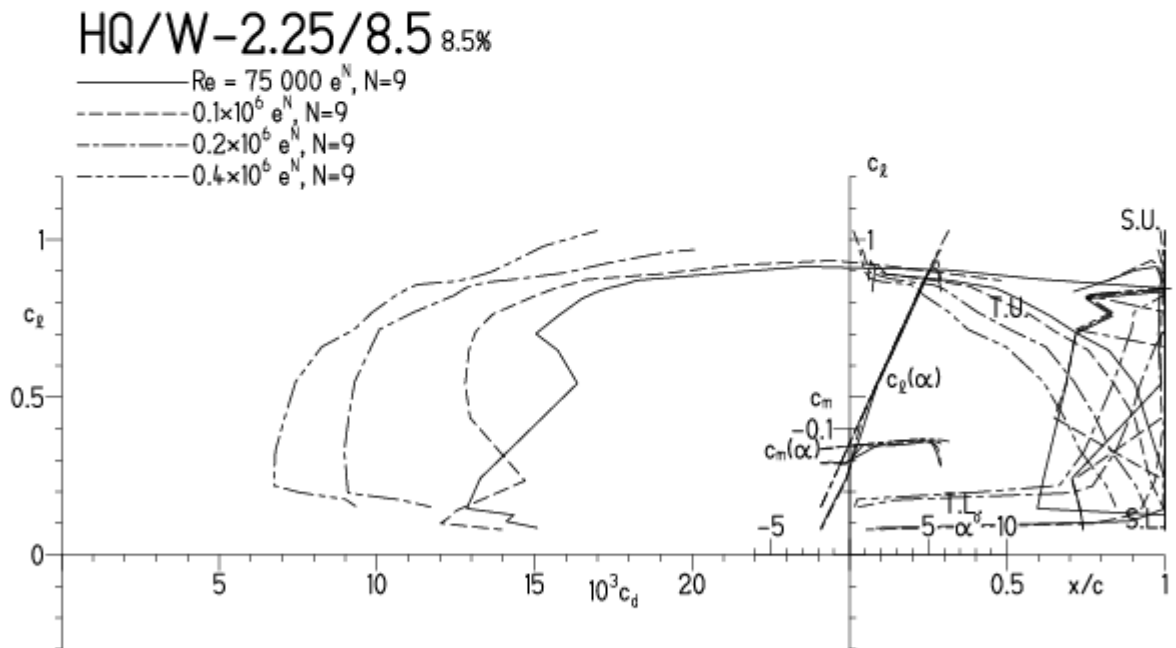


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

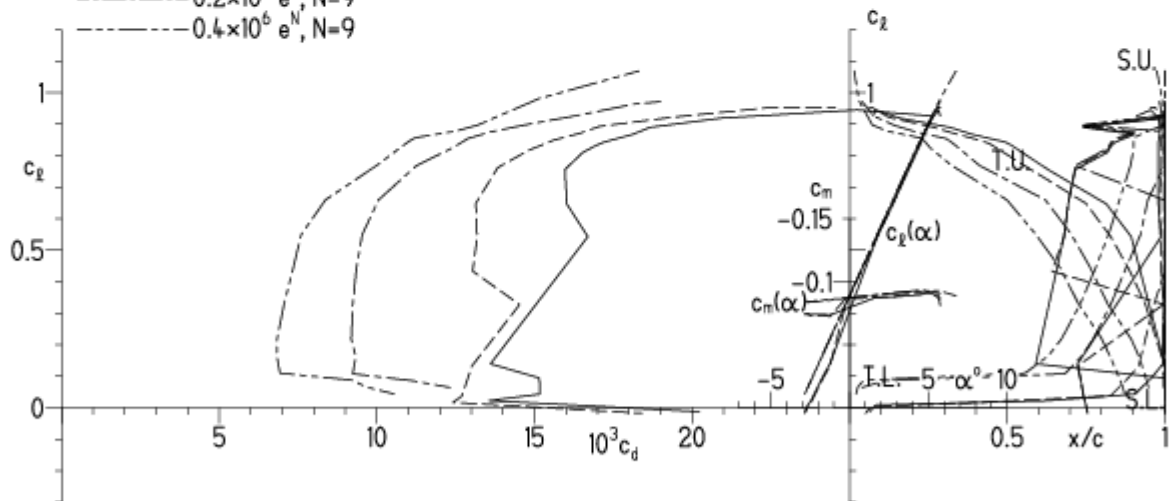
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

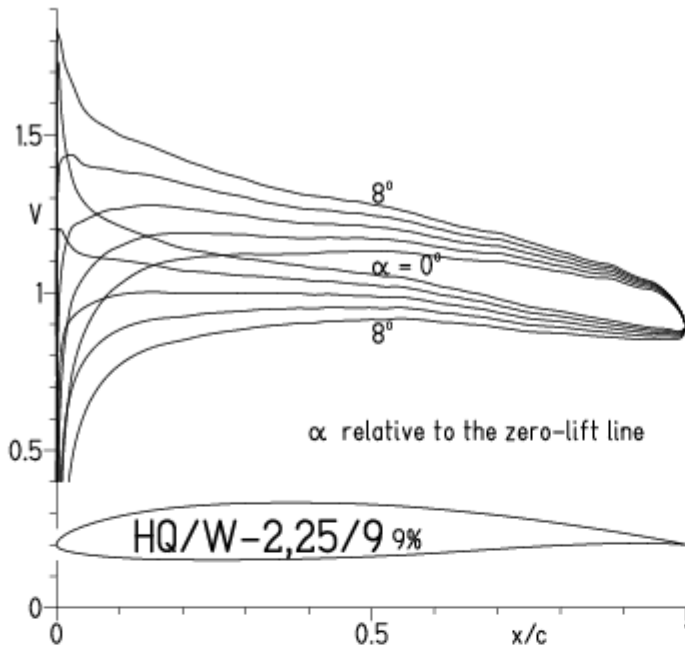
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

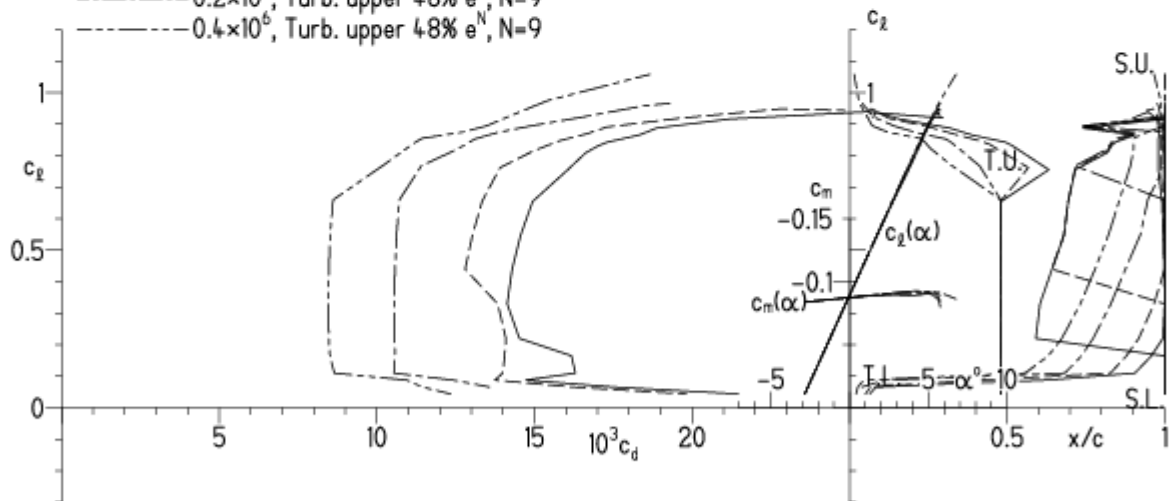
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

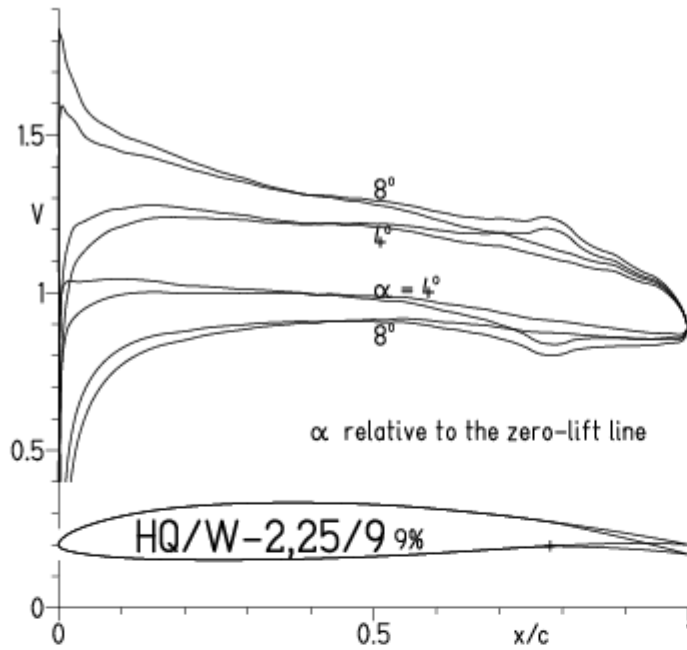
- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48

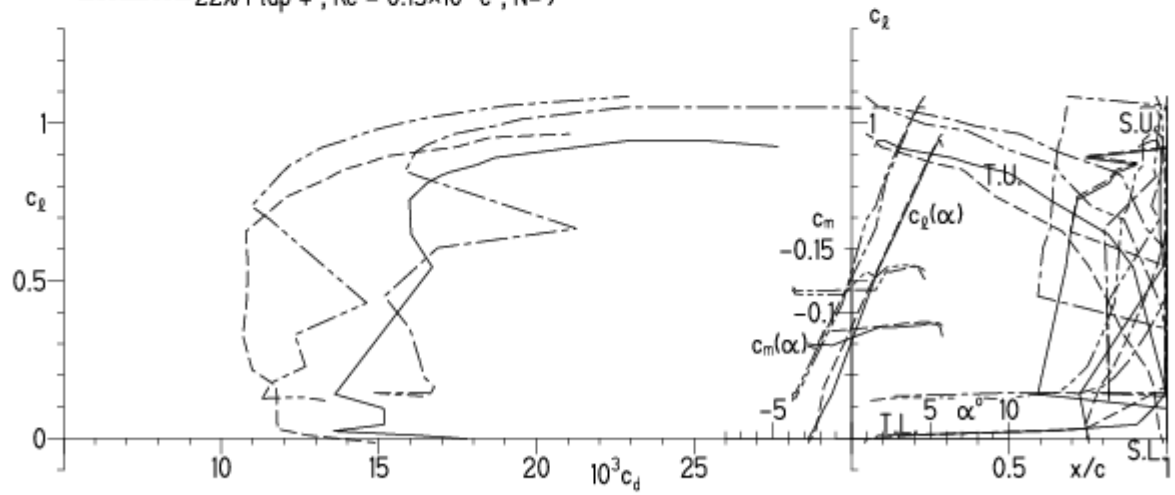


EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

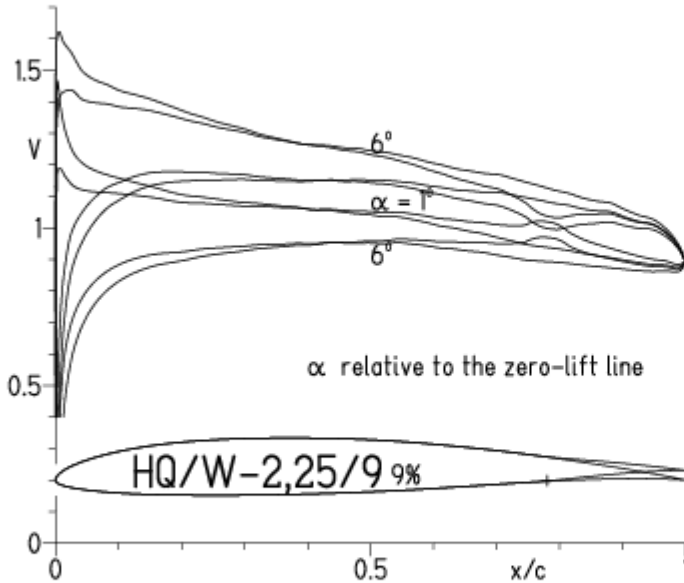
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

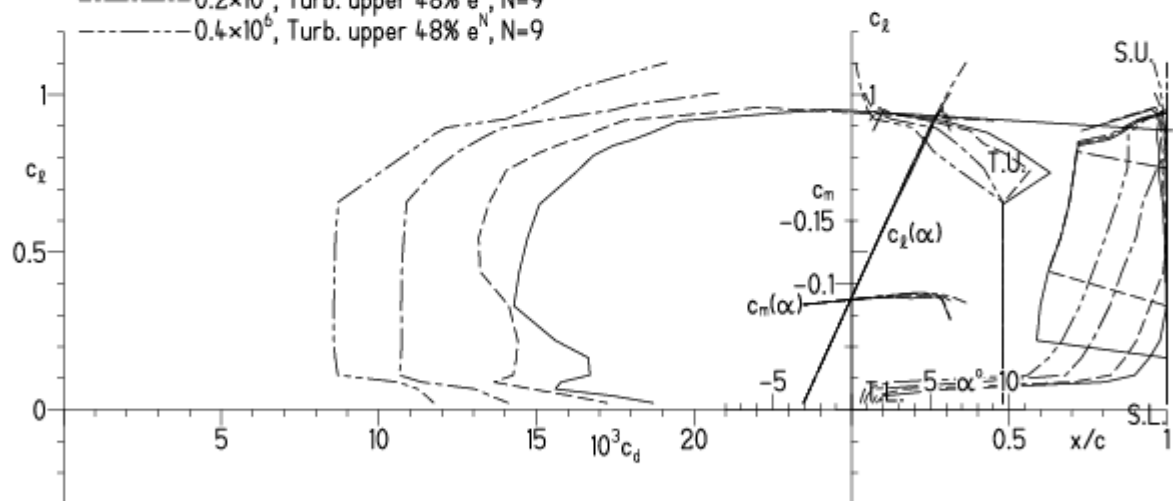
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

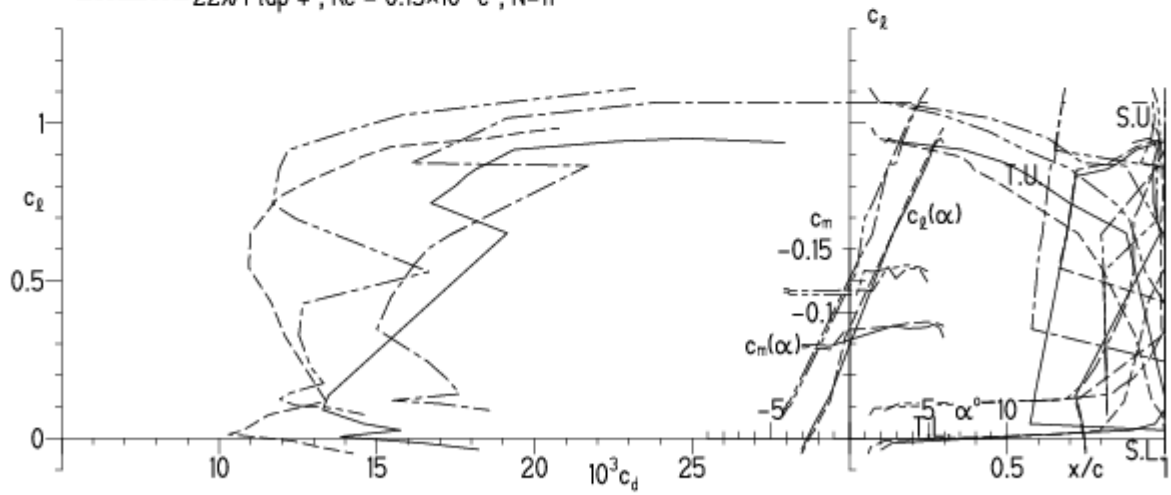


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

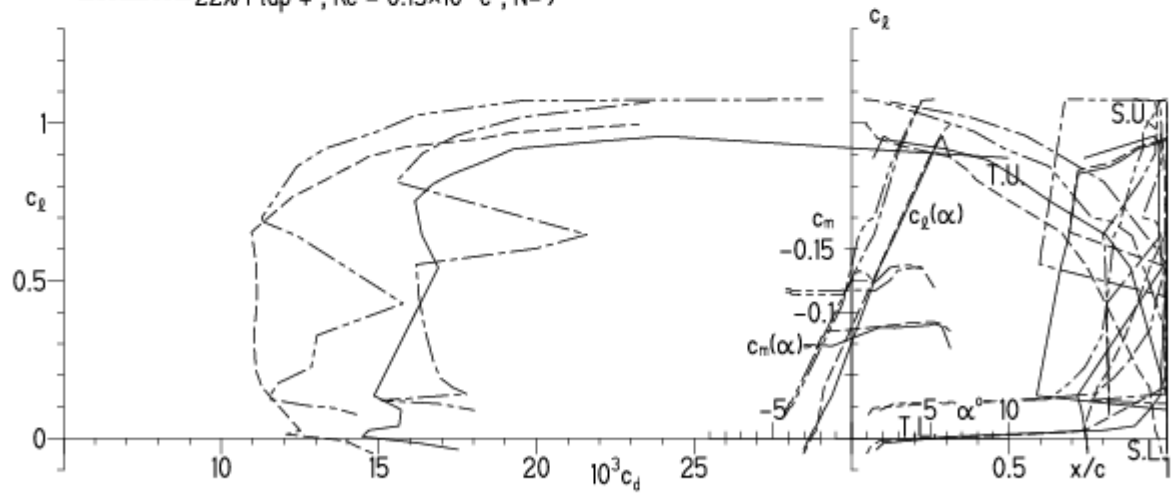


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

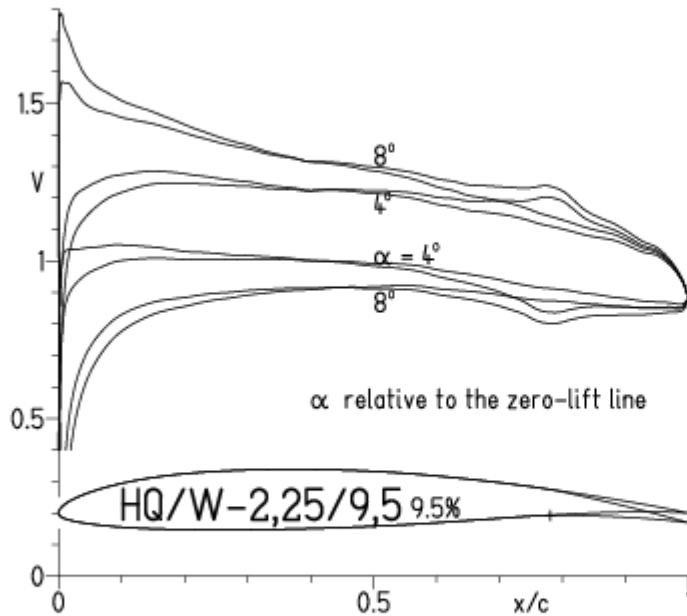
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

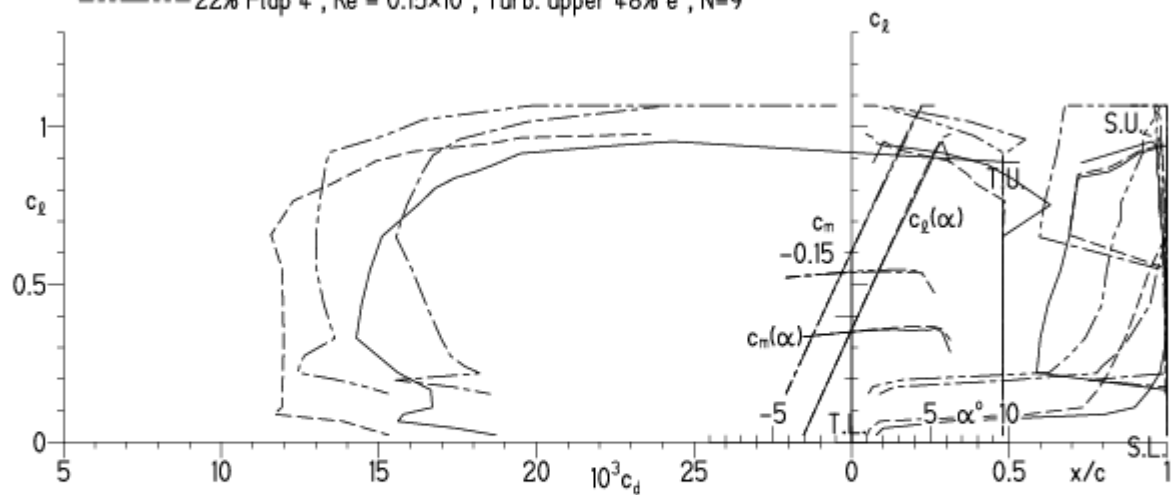


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

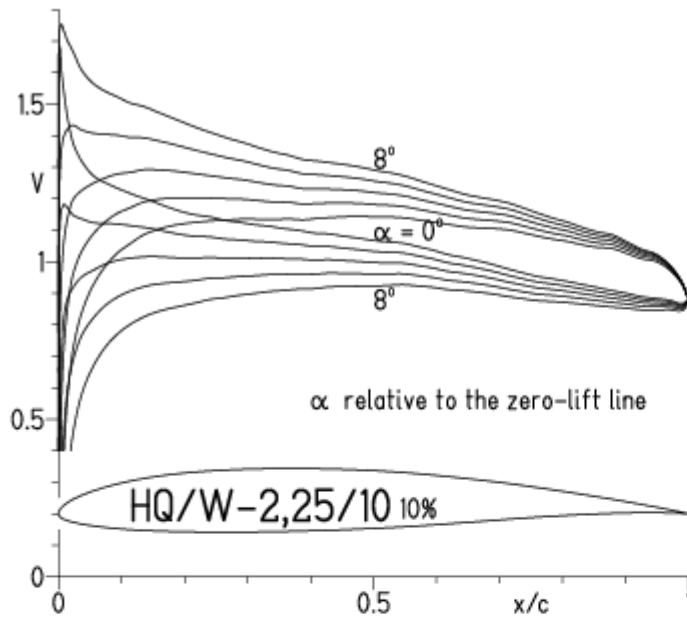


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

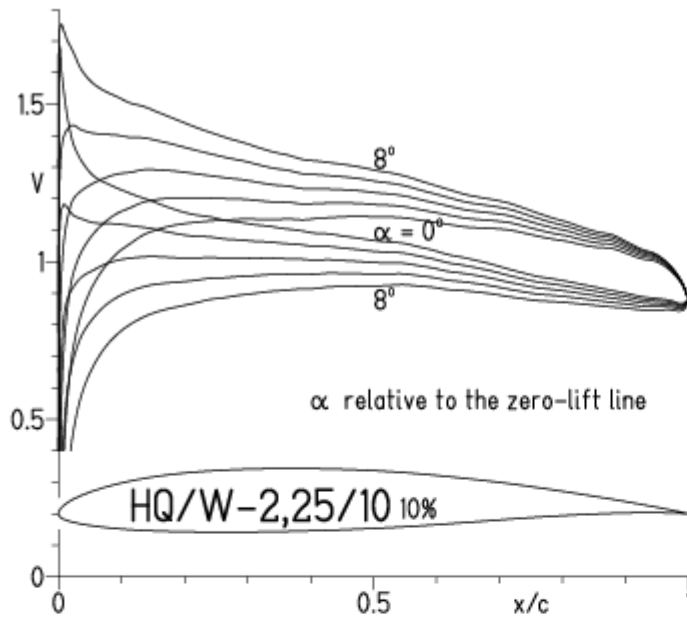


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

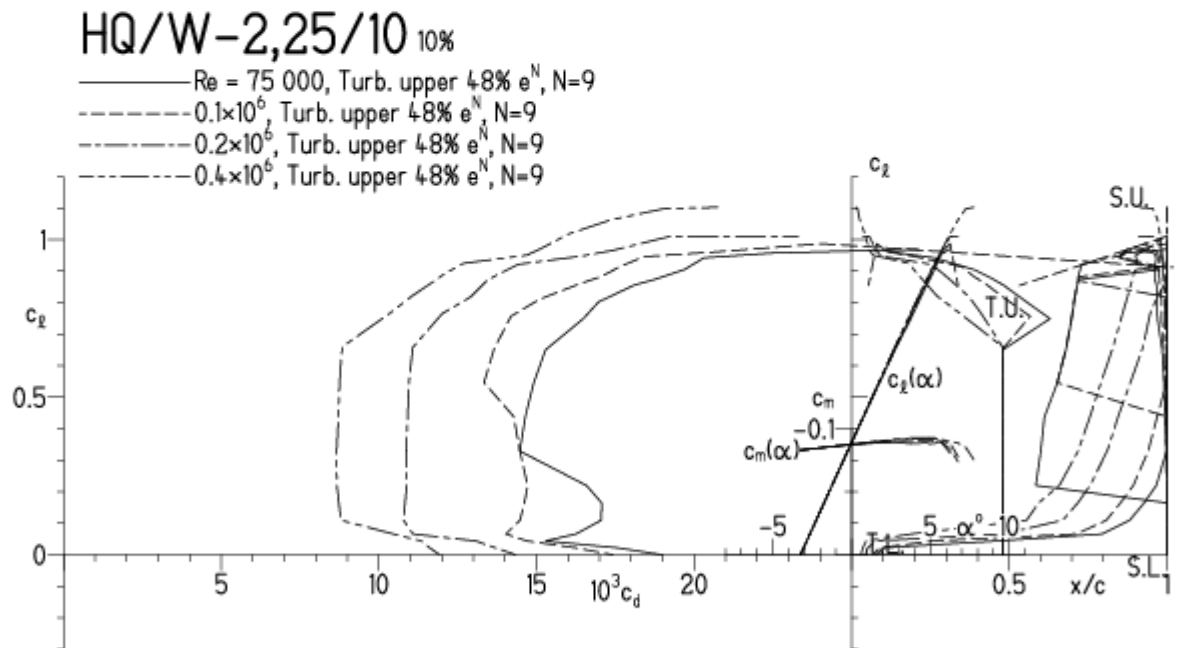


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

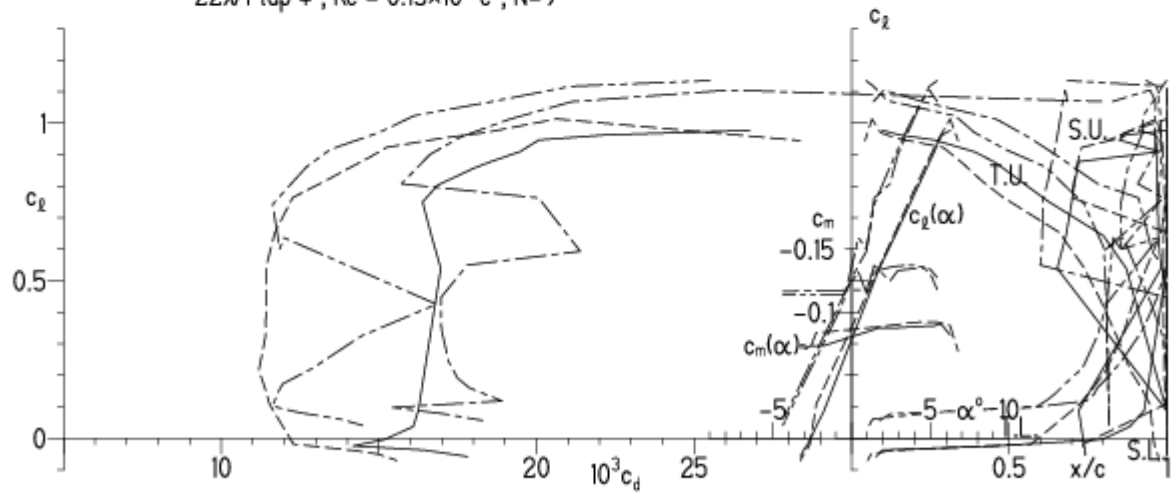


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

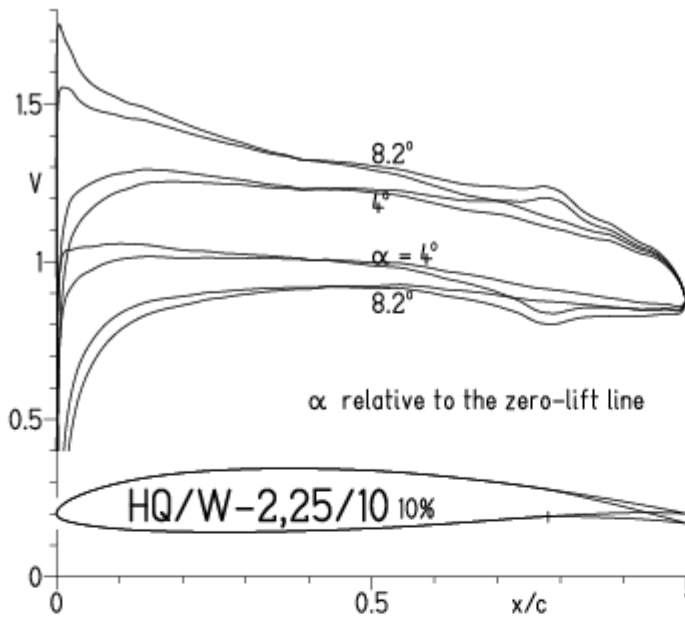
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

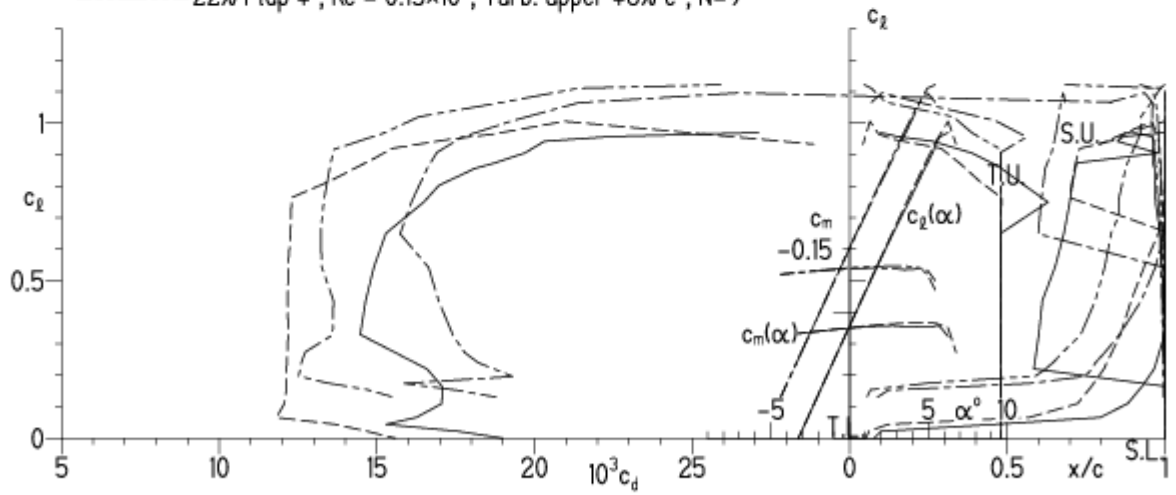


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

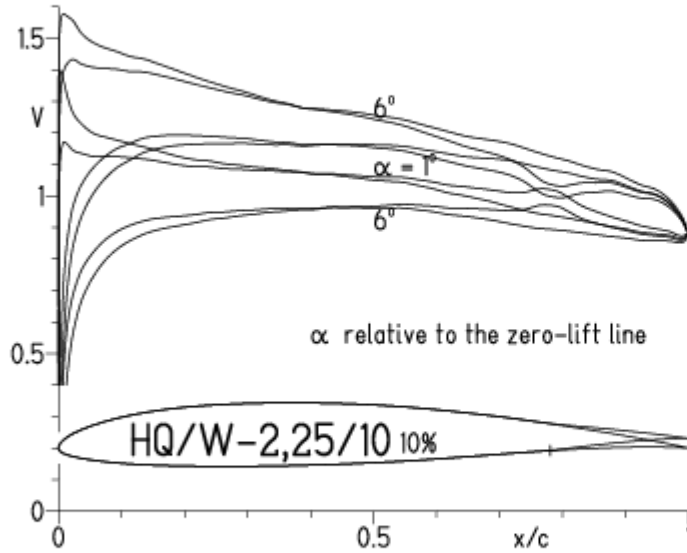
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

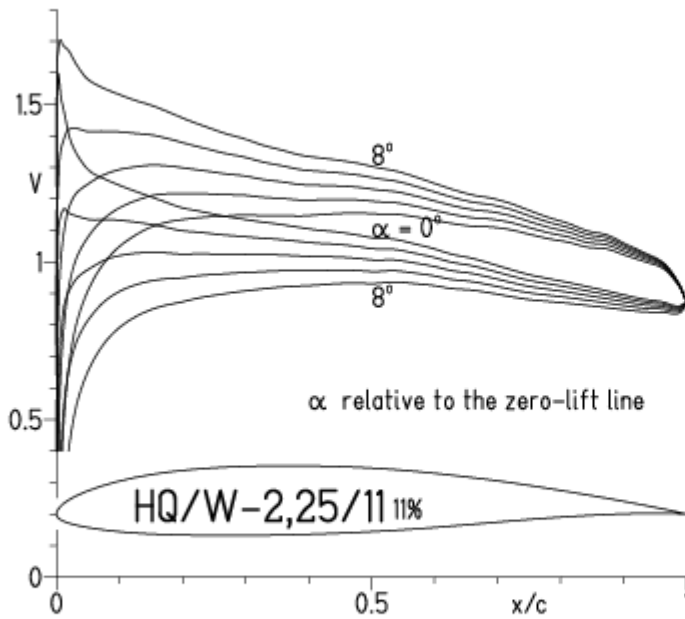


EPPLER 2005 V. 8.5.07 RUN

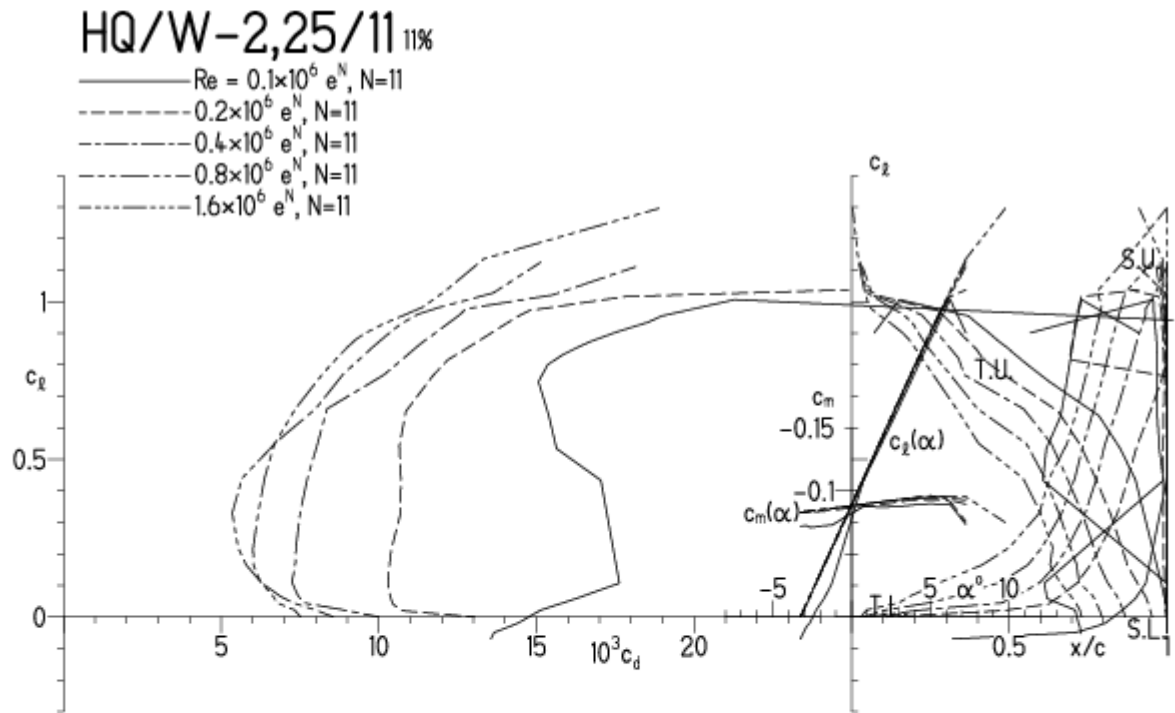


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

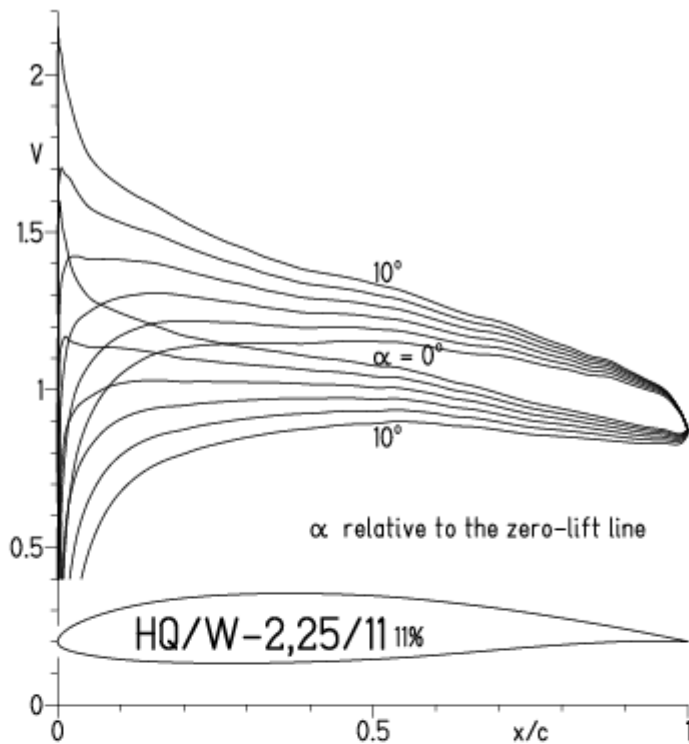


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

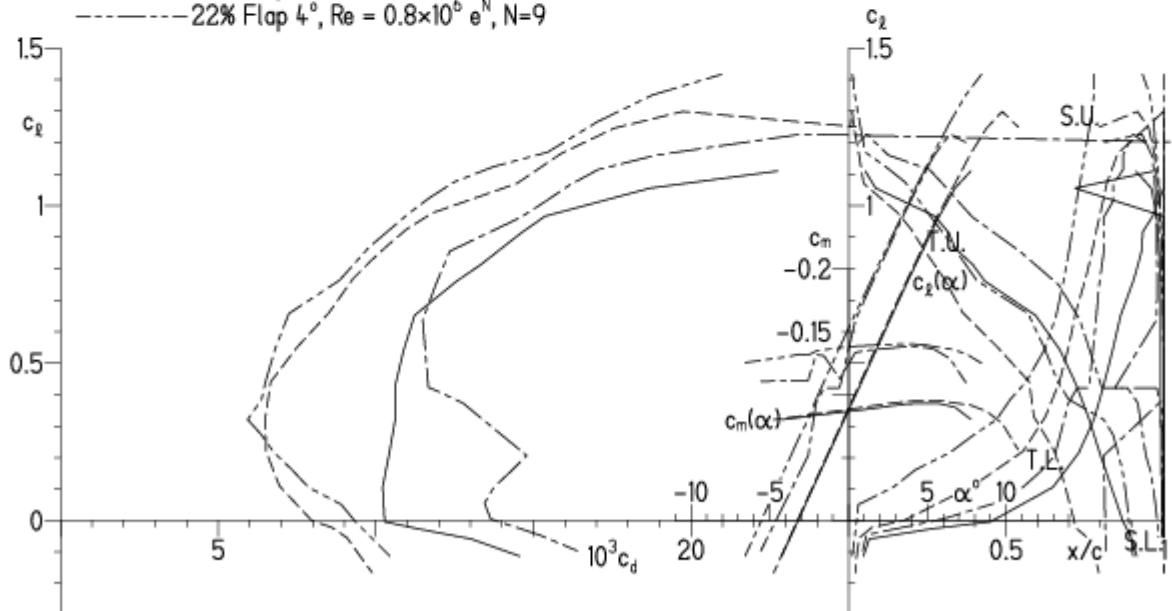


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

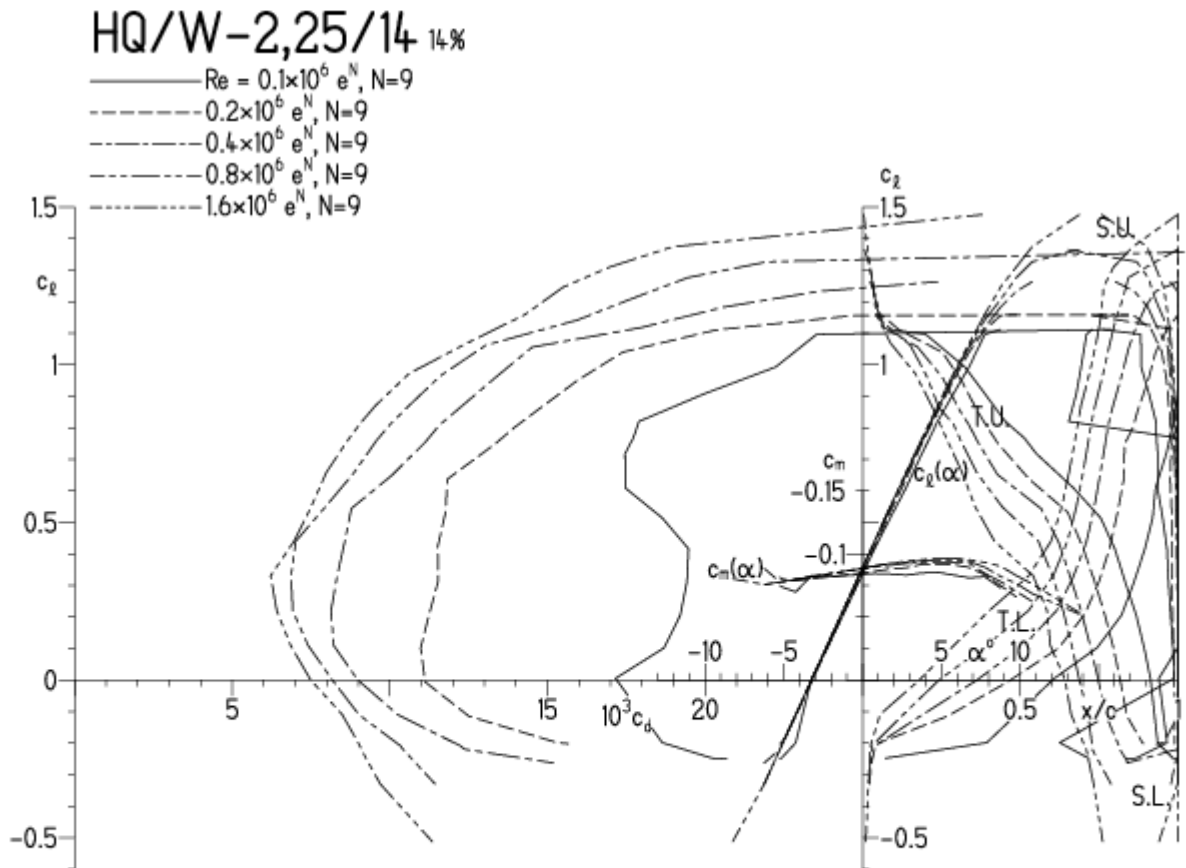


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

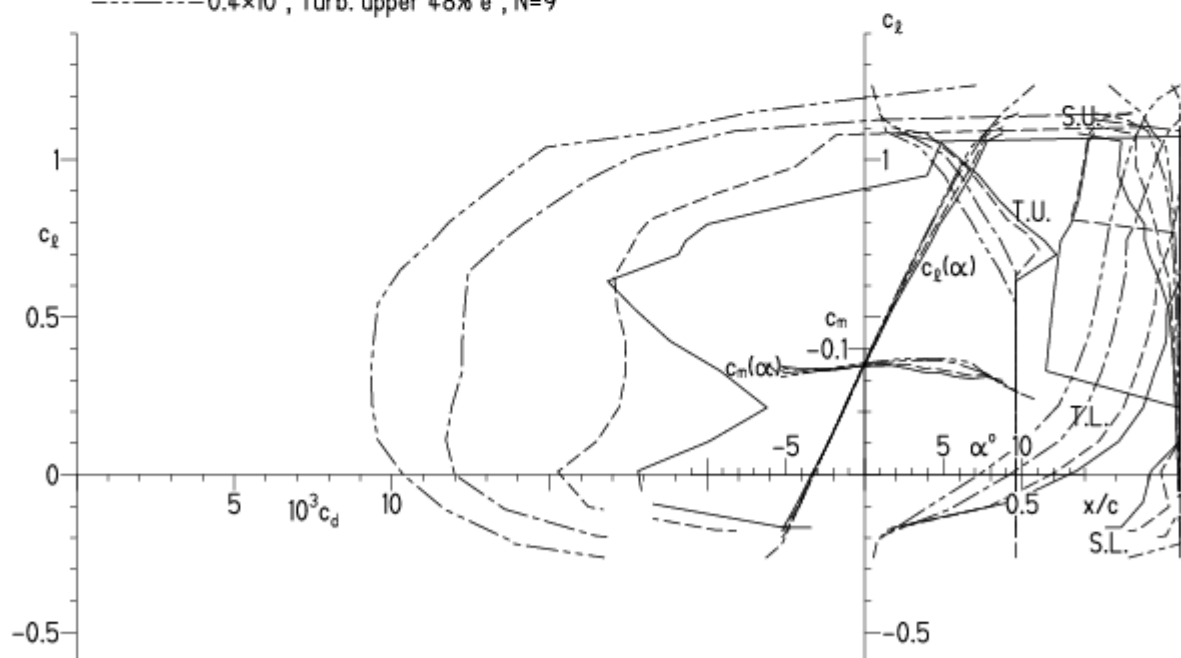
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

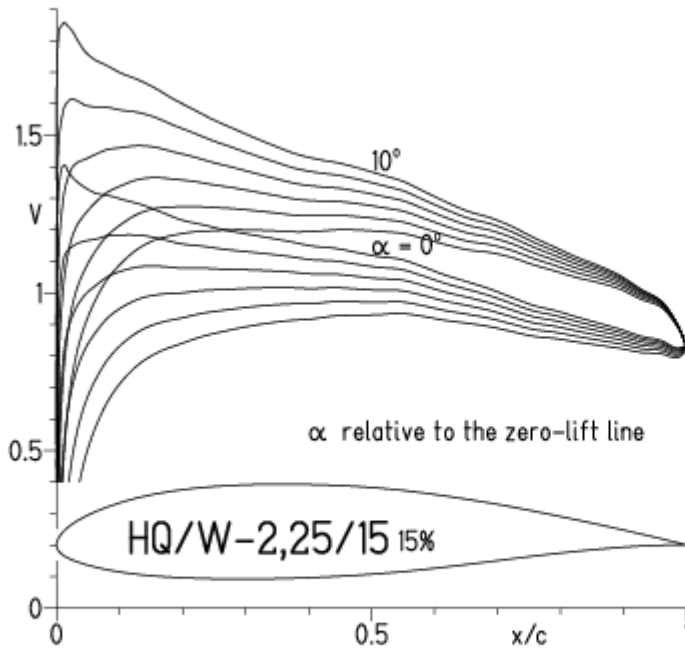


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

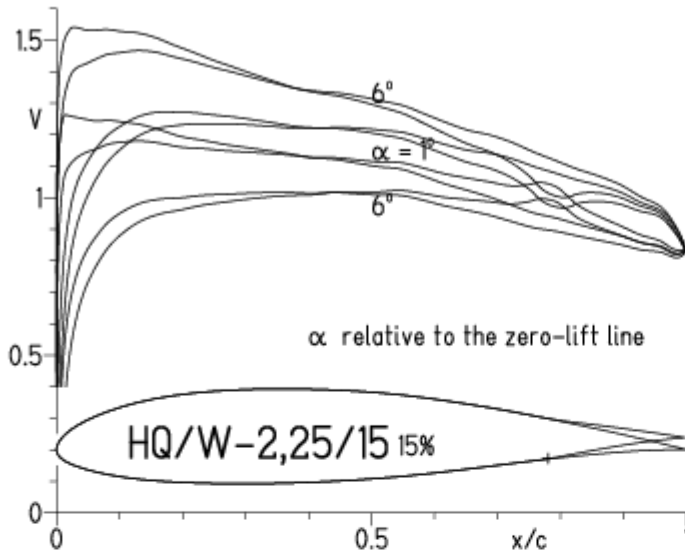


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

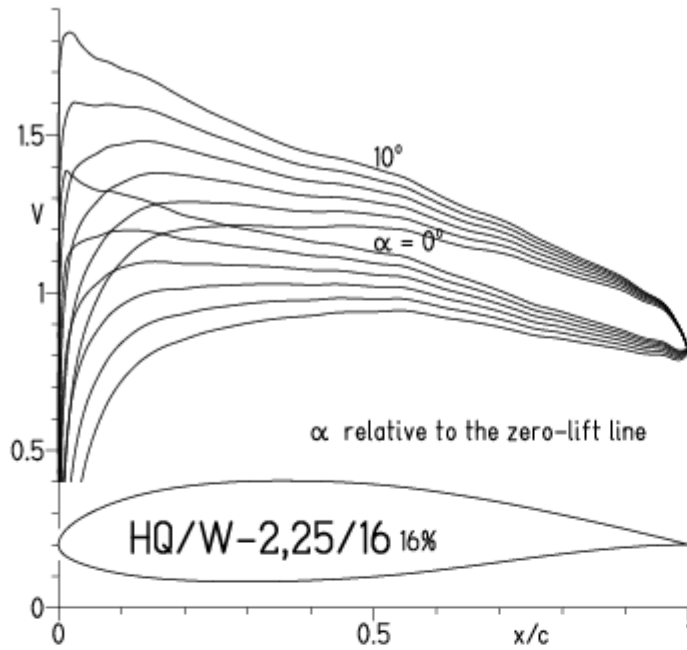
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

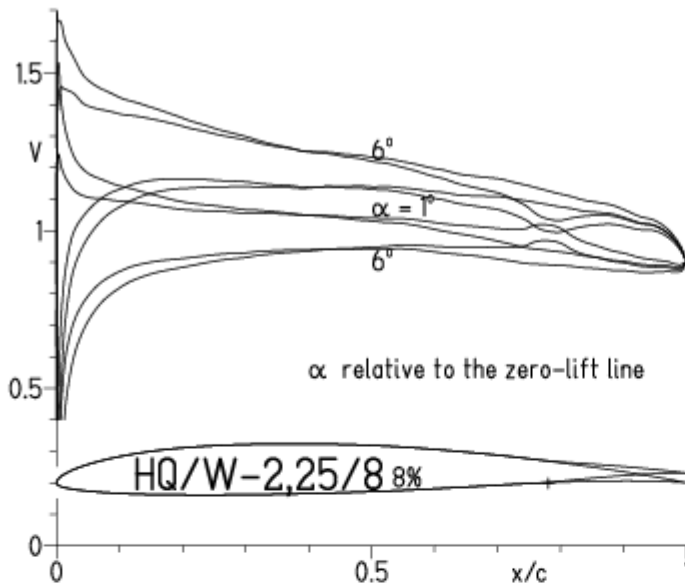
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

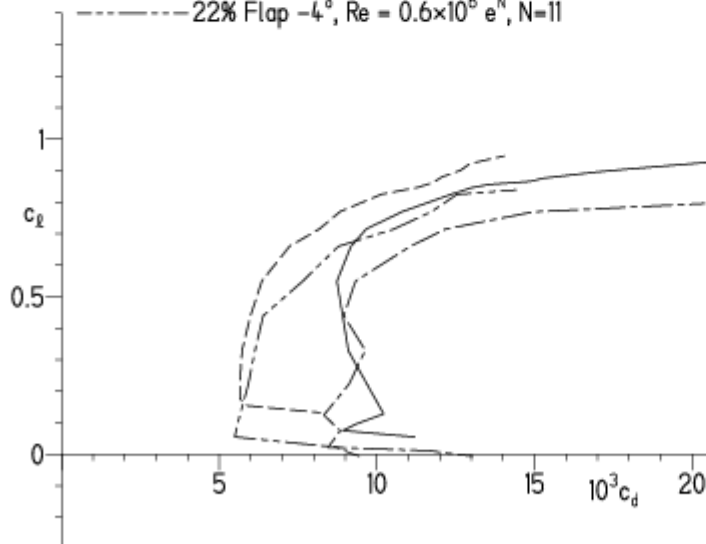
EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



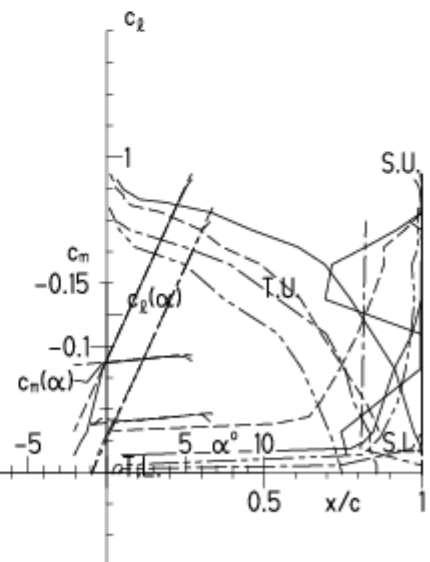
EPPLER 2005 V. 8.5.07 RUN 3.3.11 1

HQ/W-2,25/8 8%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

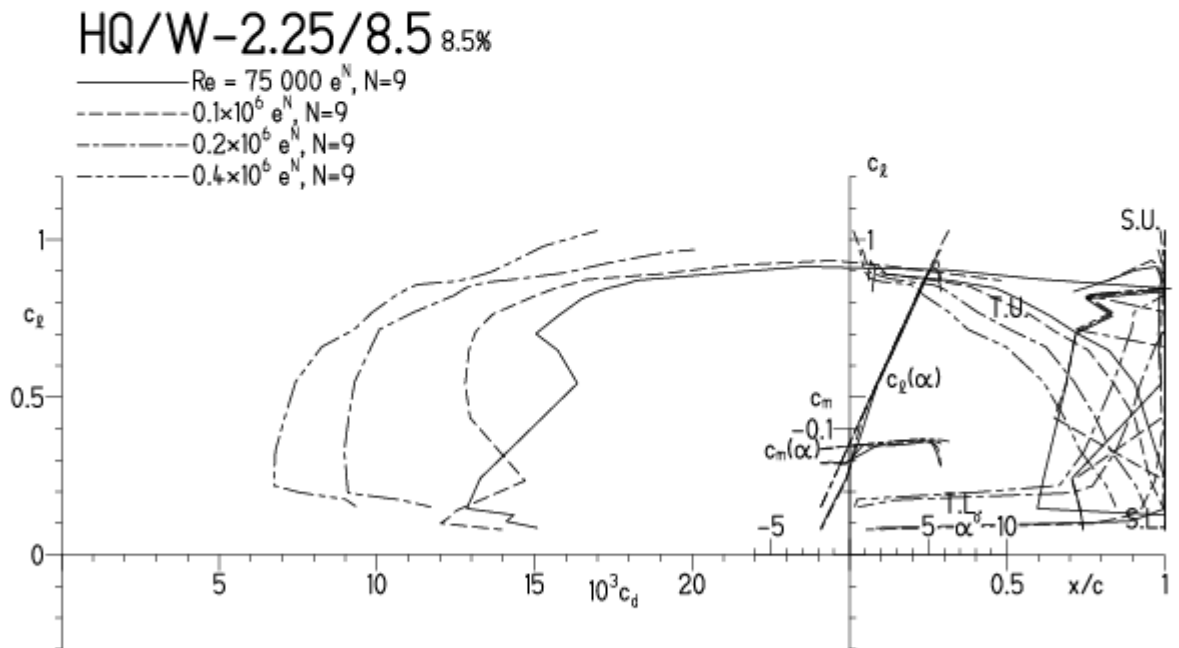


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4°, $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

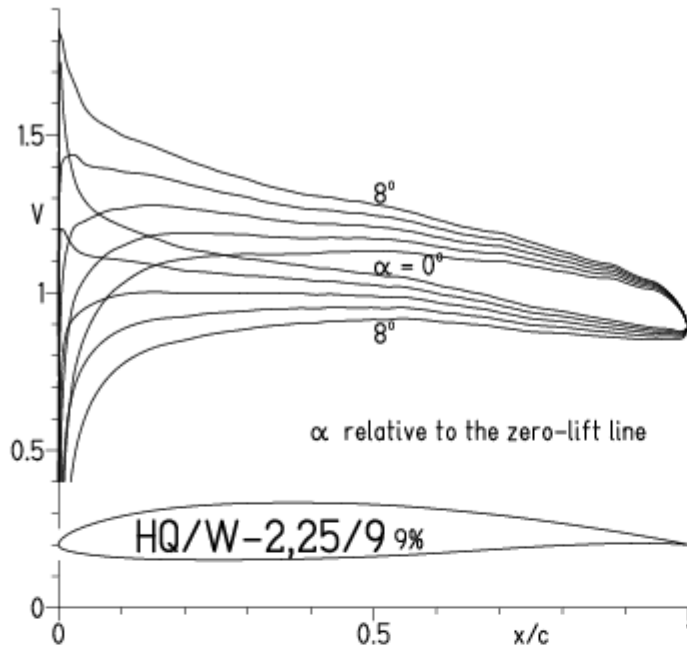


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

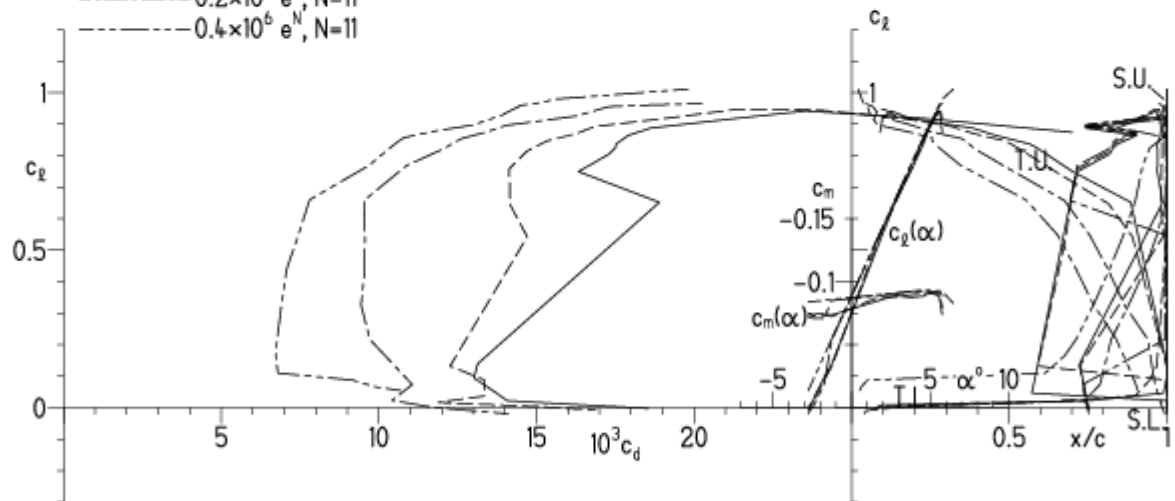
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

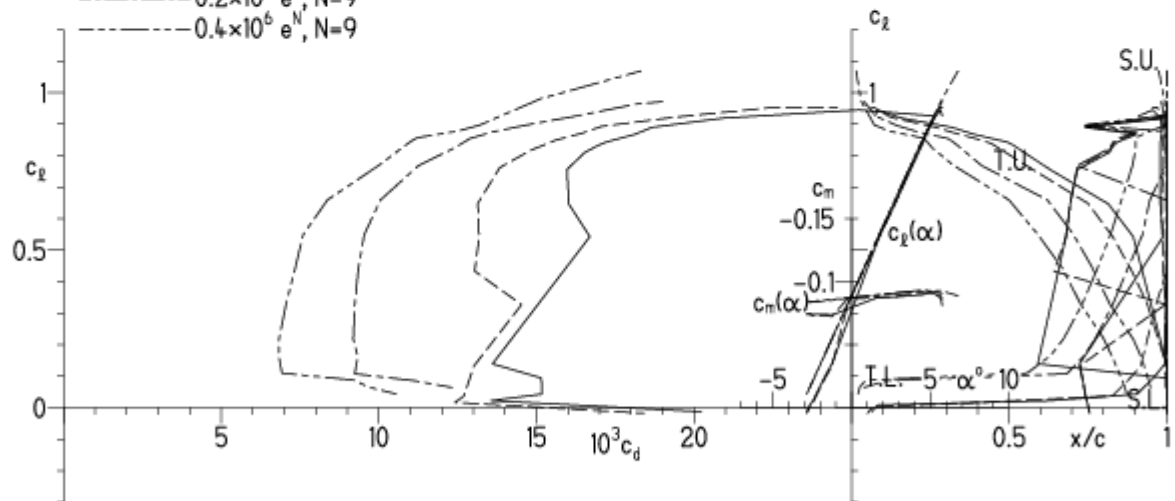
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

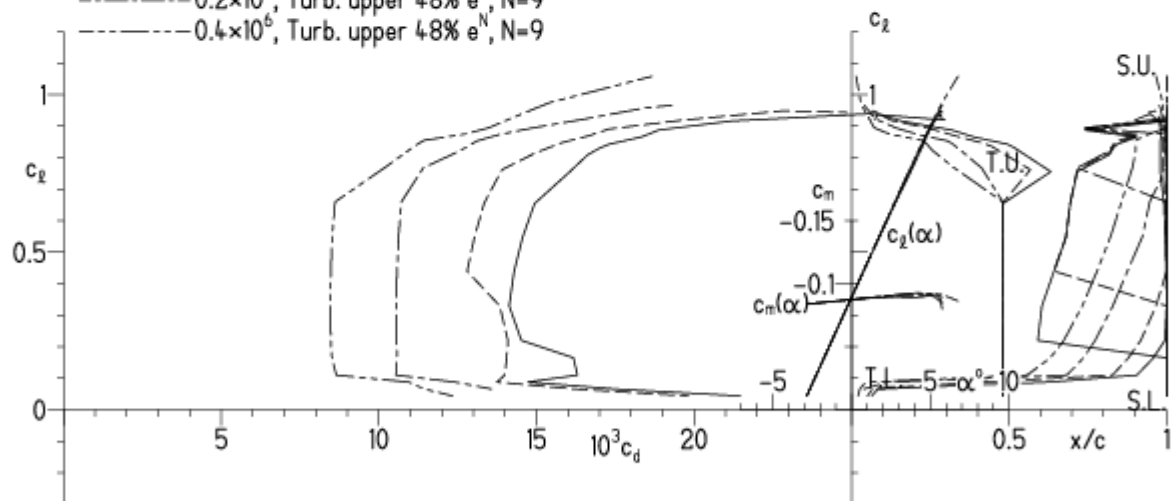
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

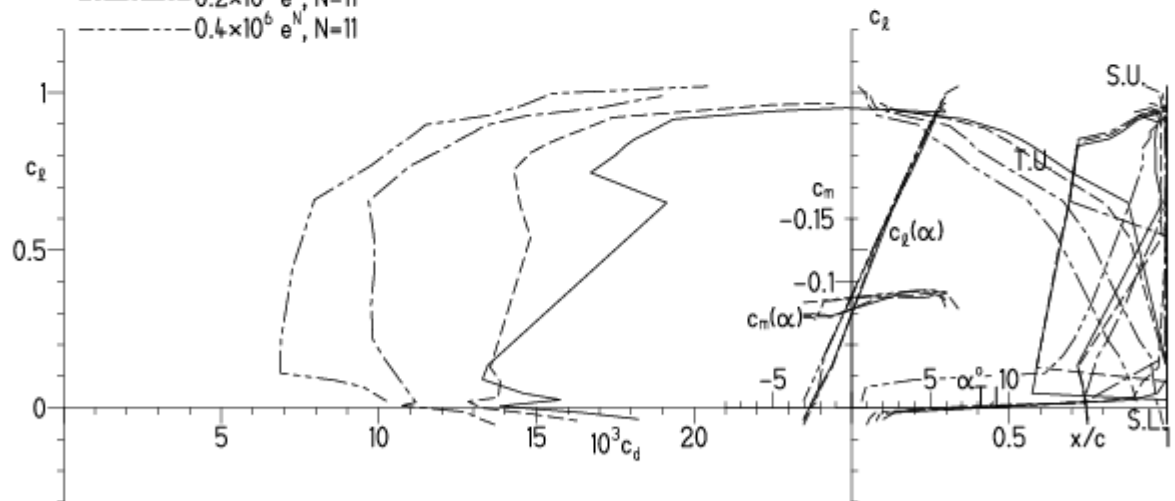
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

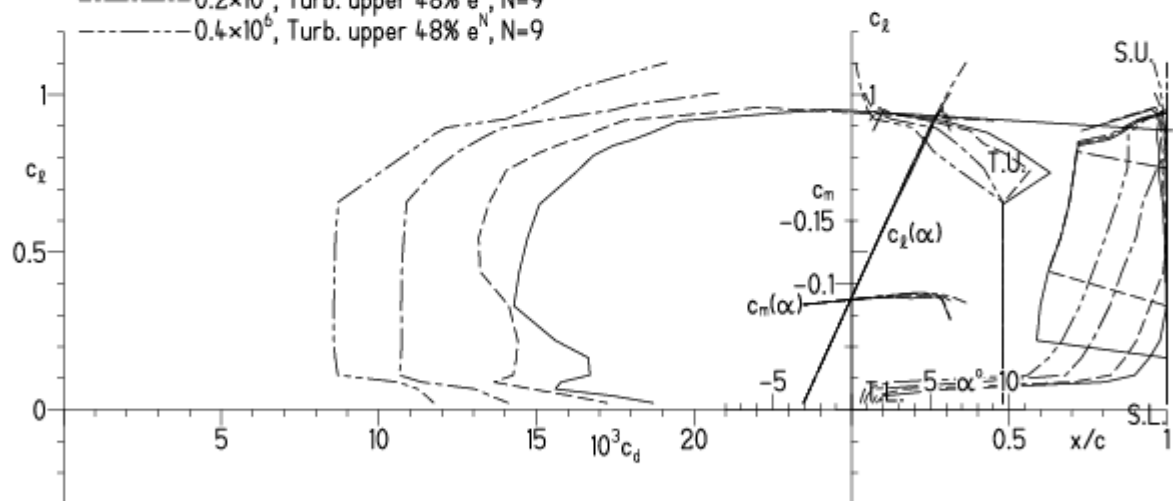
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

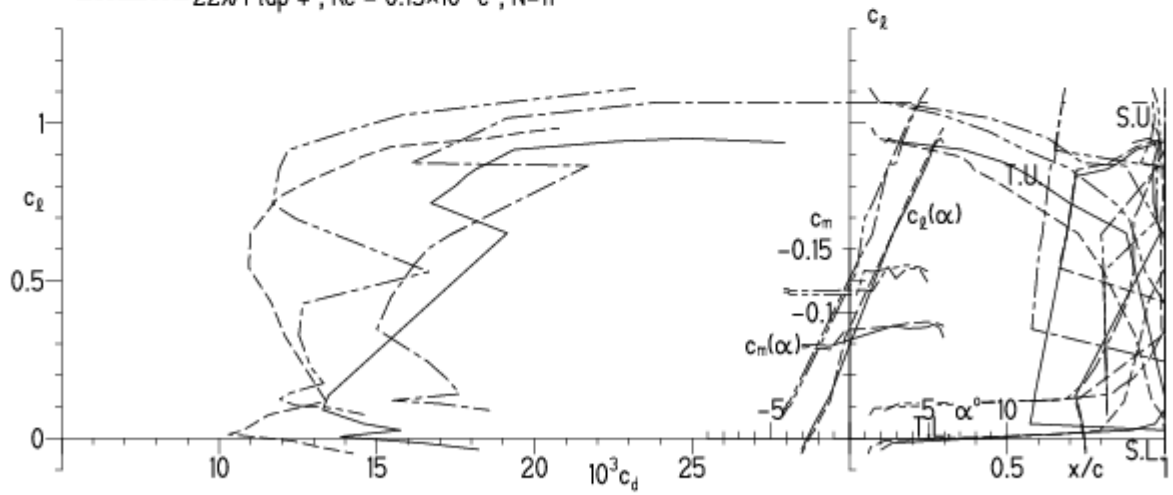


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



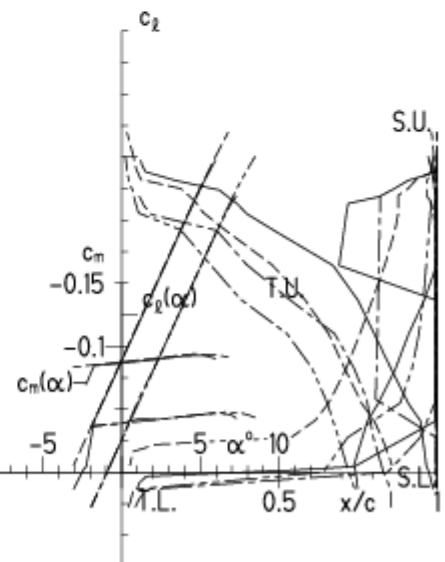
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

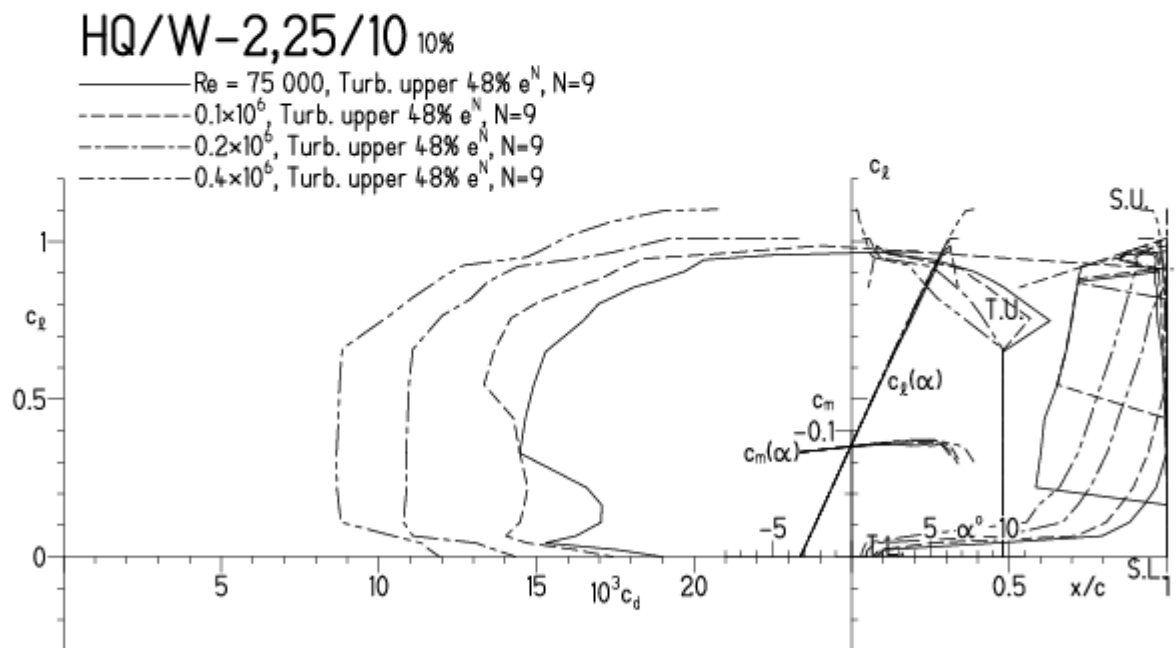


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

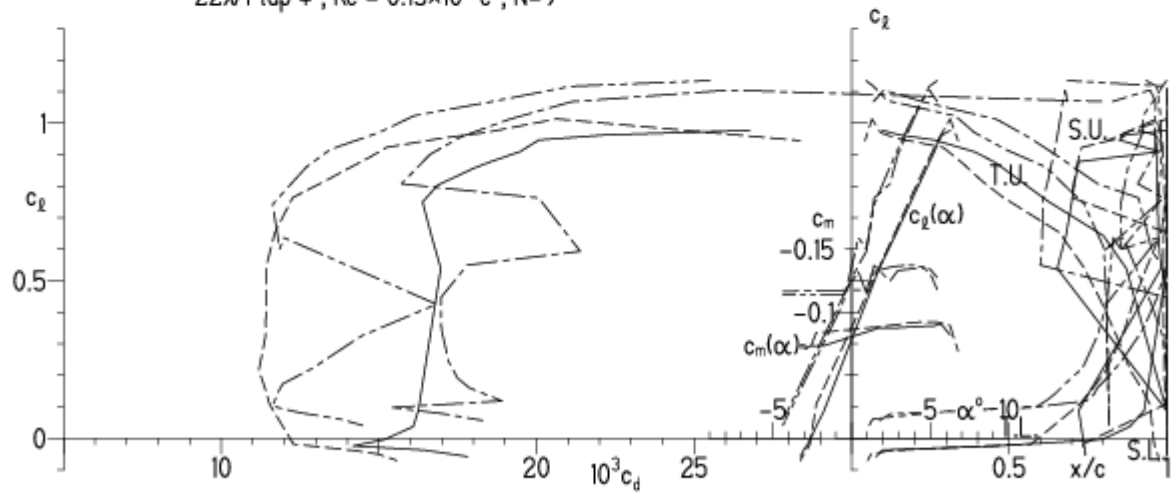


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

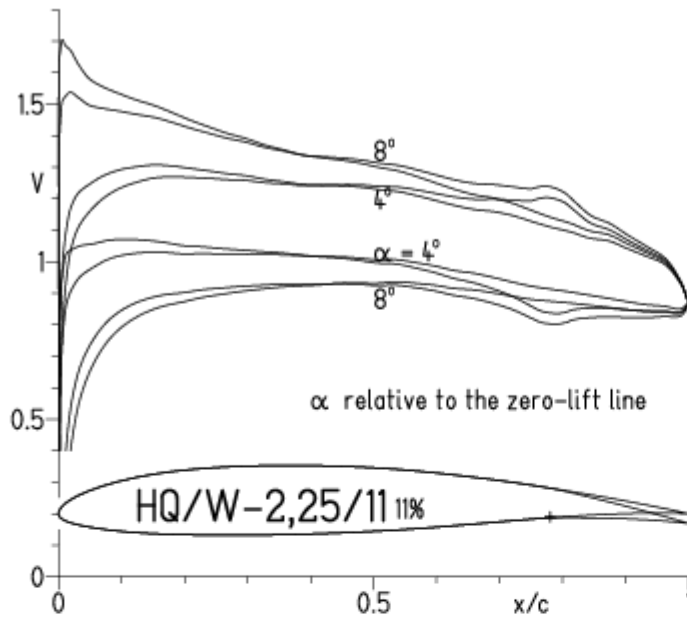
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

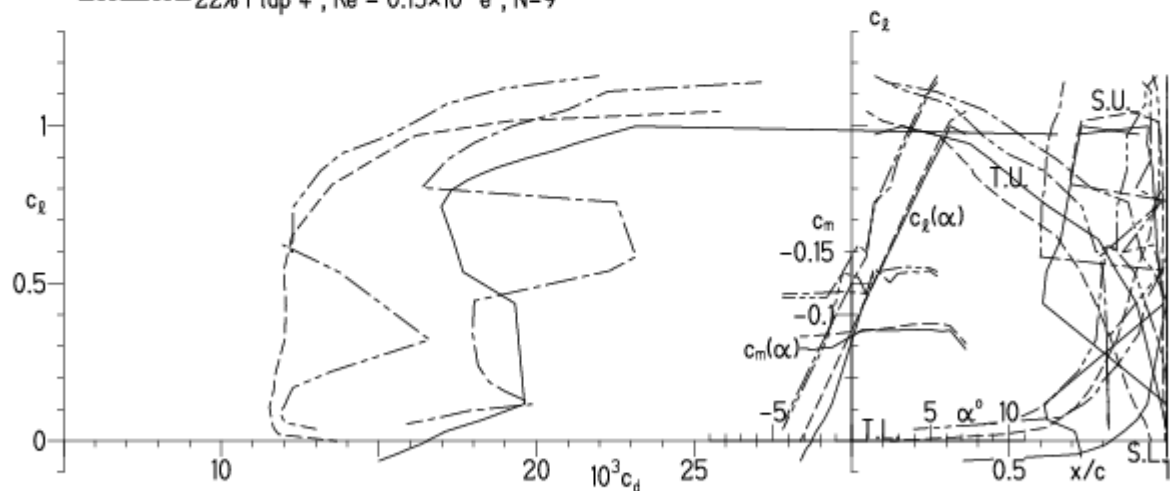


EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

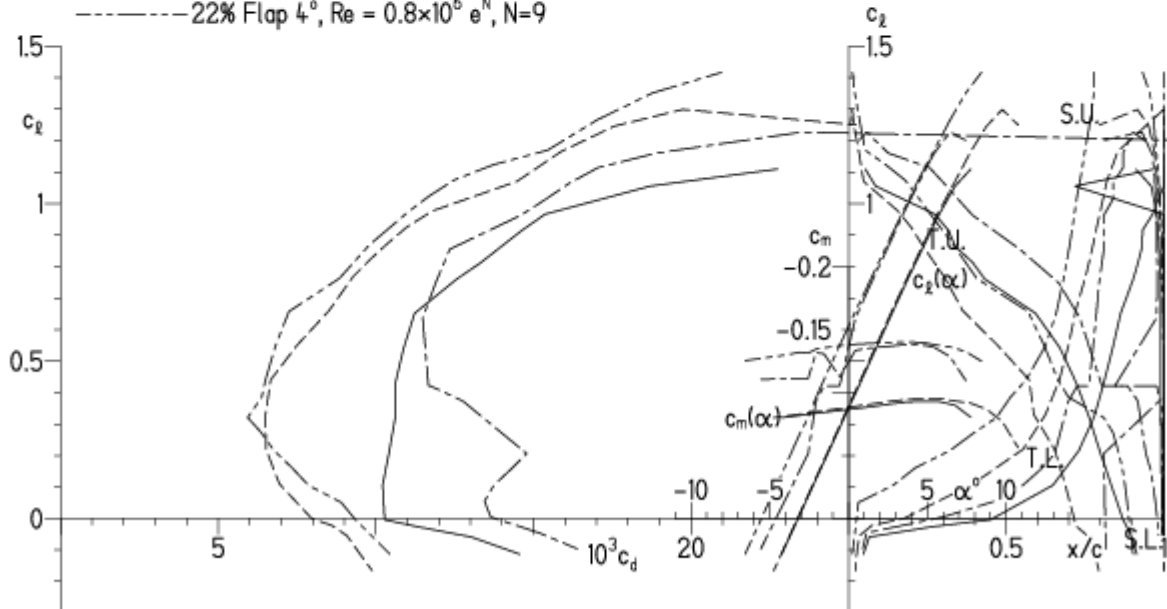


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

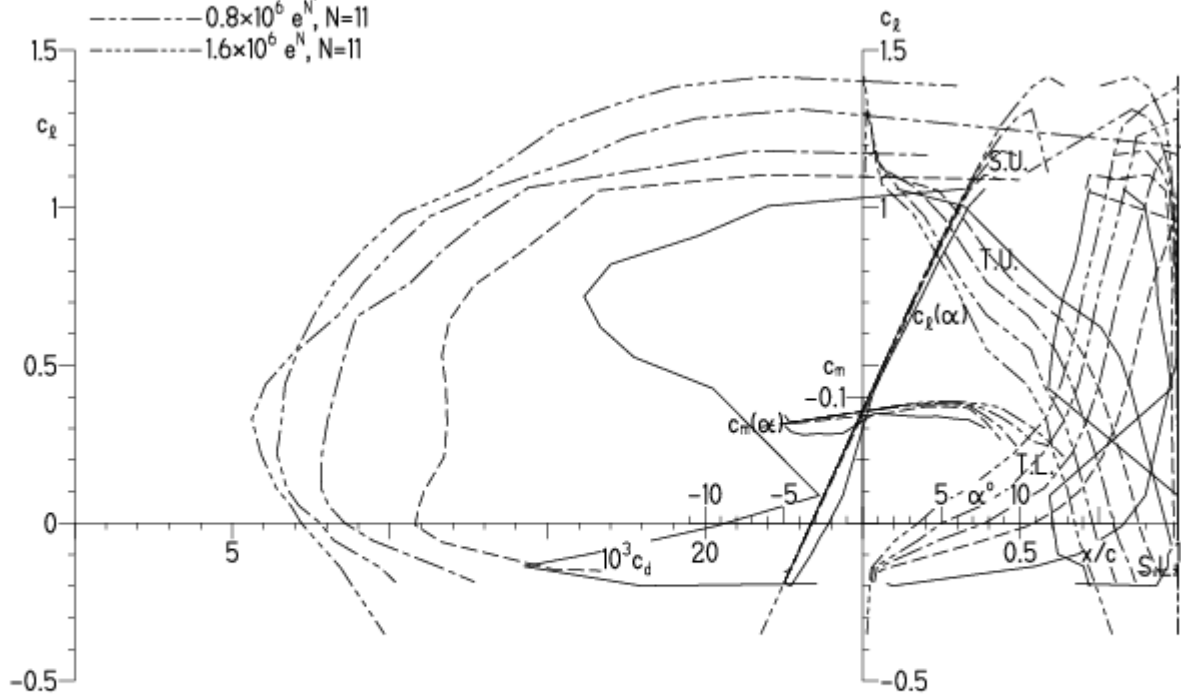
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

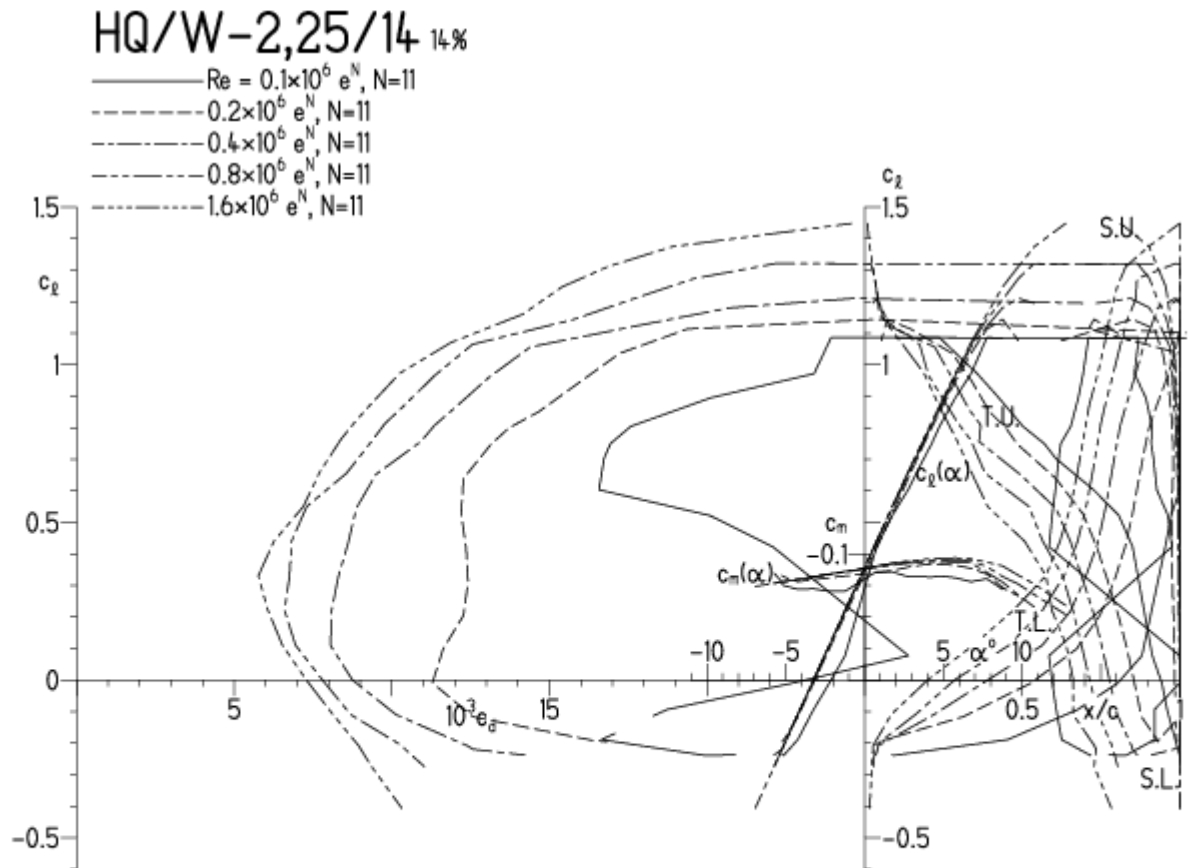


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

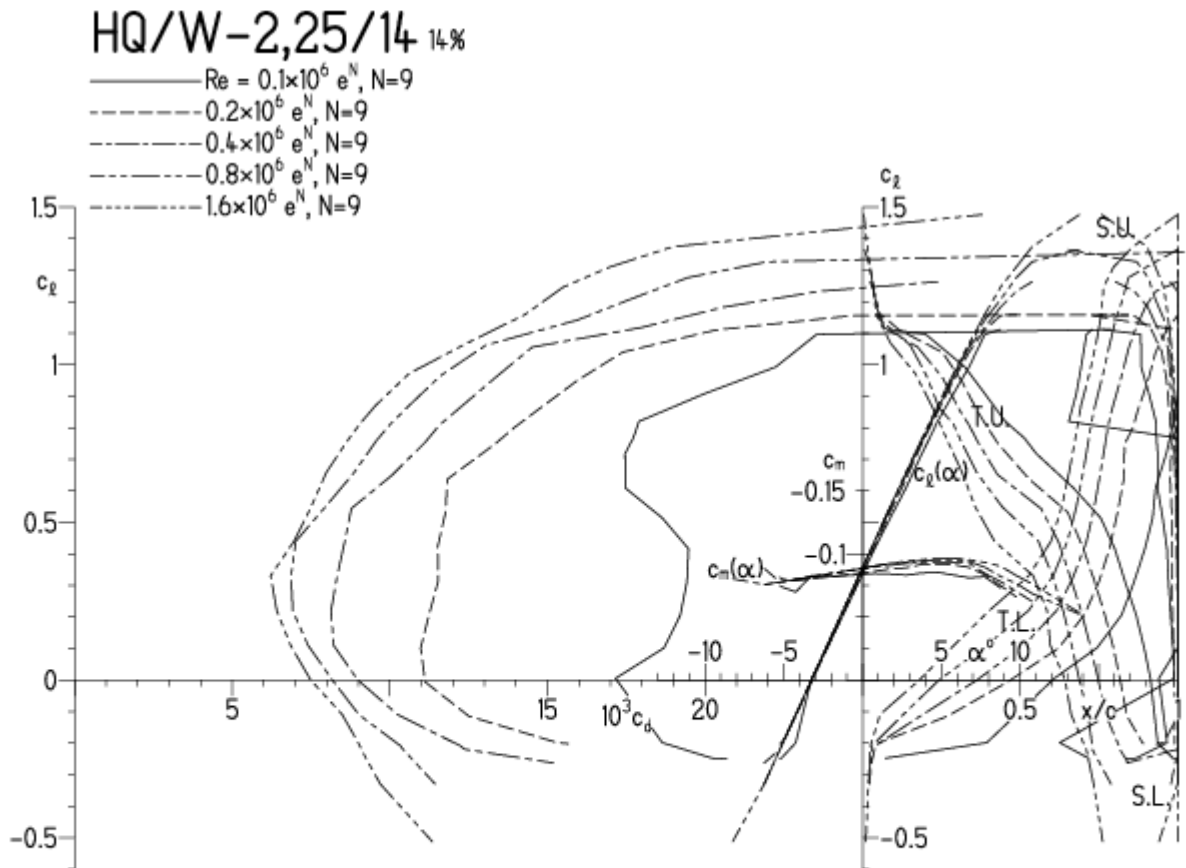


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

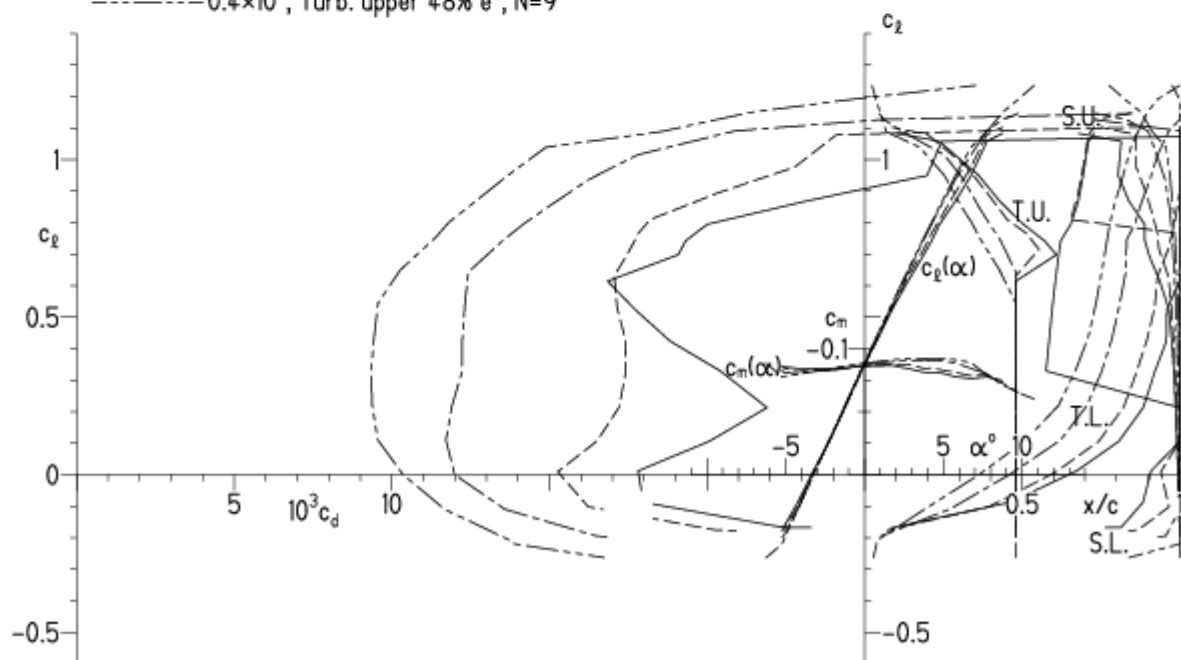
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

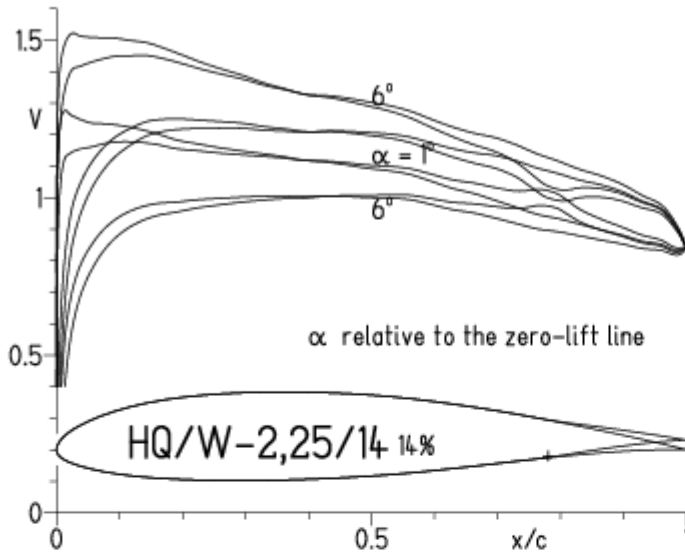
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

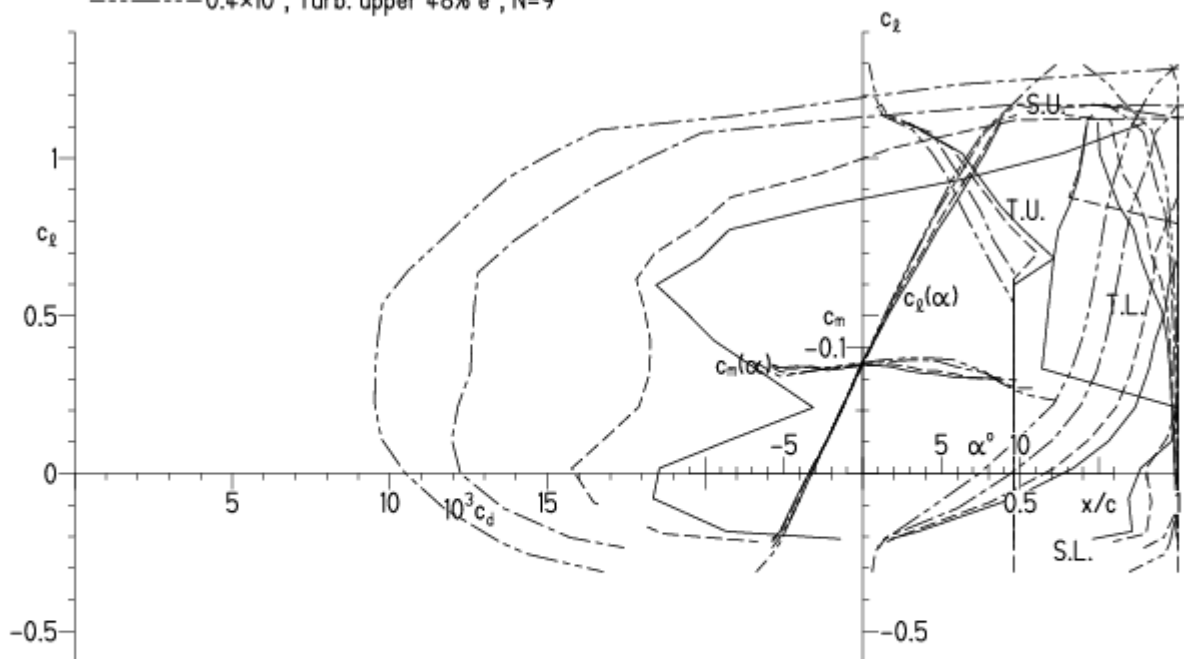
EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

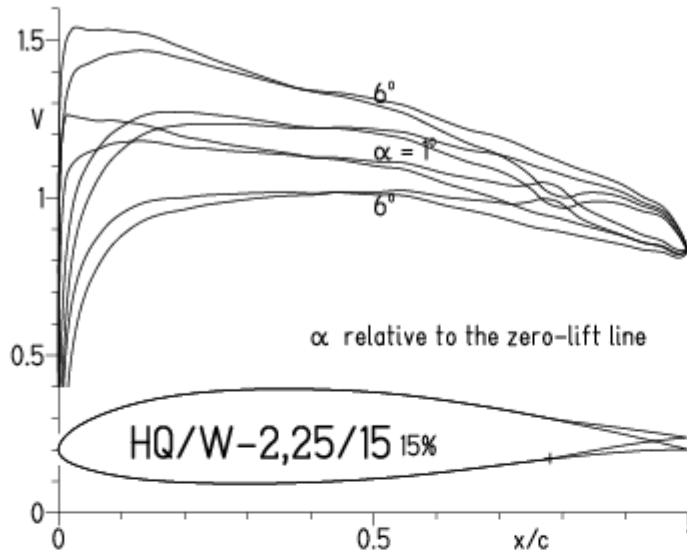


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

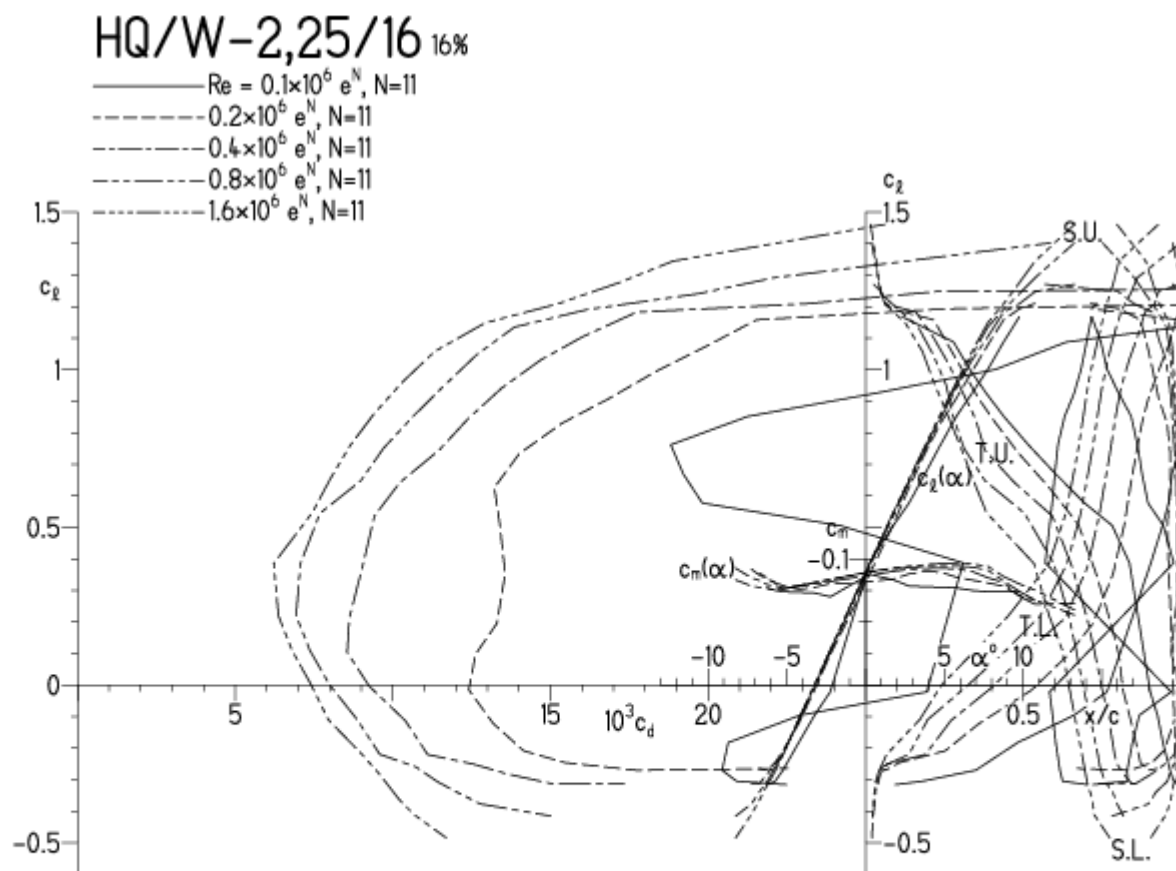


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

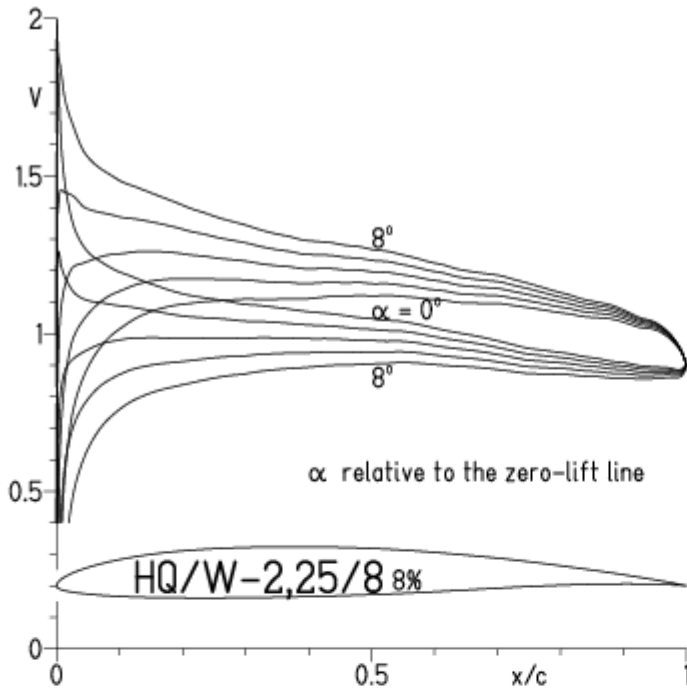
HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

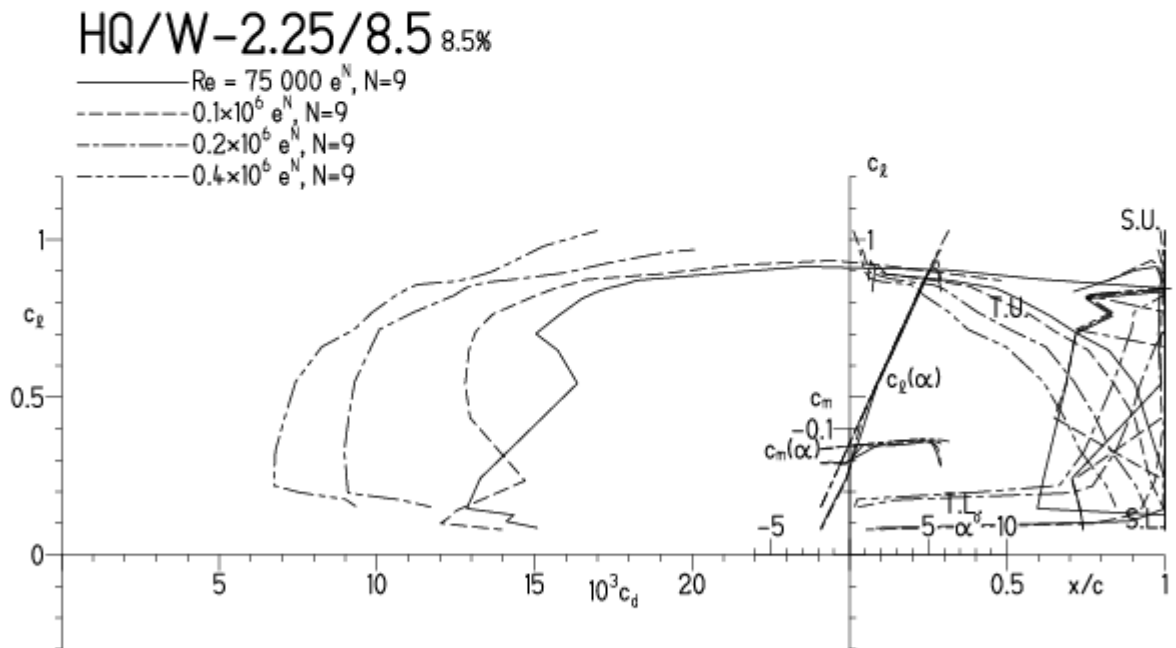


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

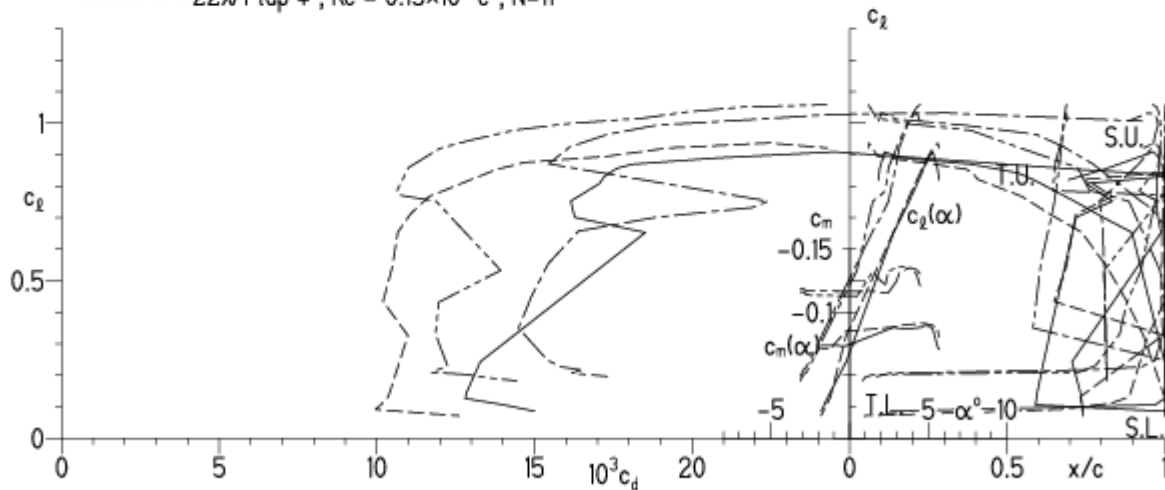


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

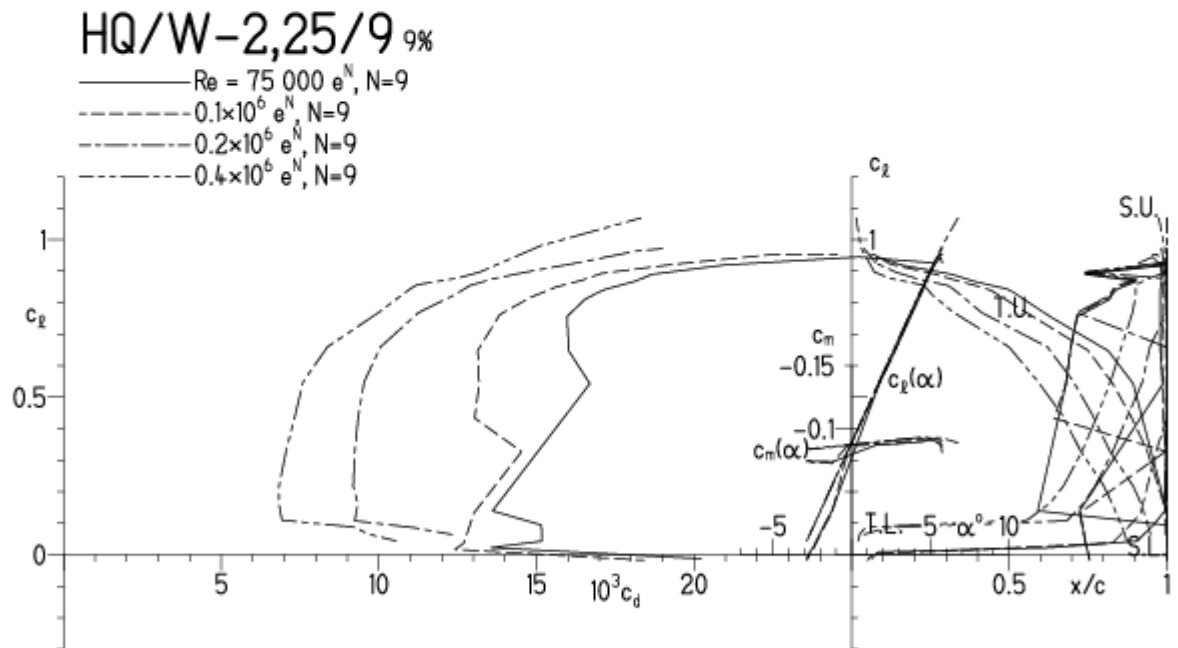


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

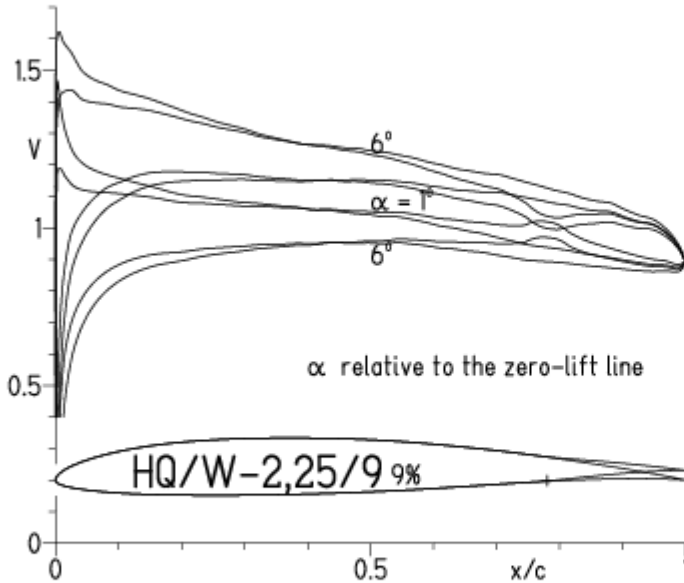
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



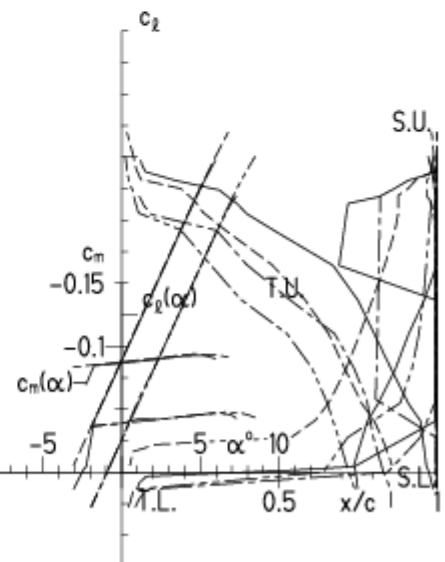
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N$, $N=11$
- - - $0.6 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 0.2 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N$, $N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

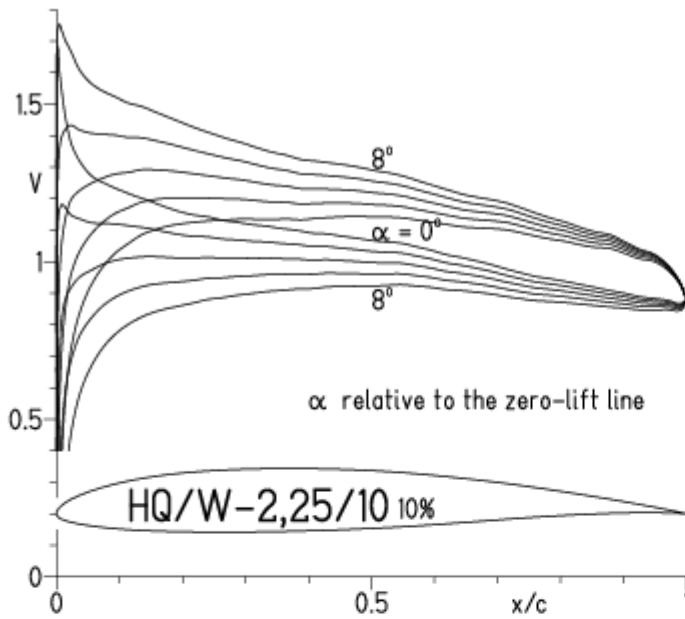


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

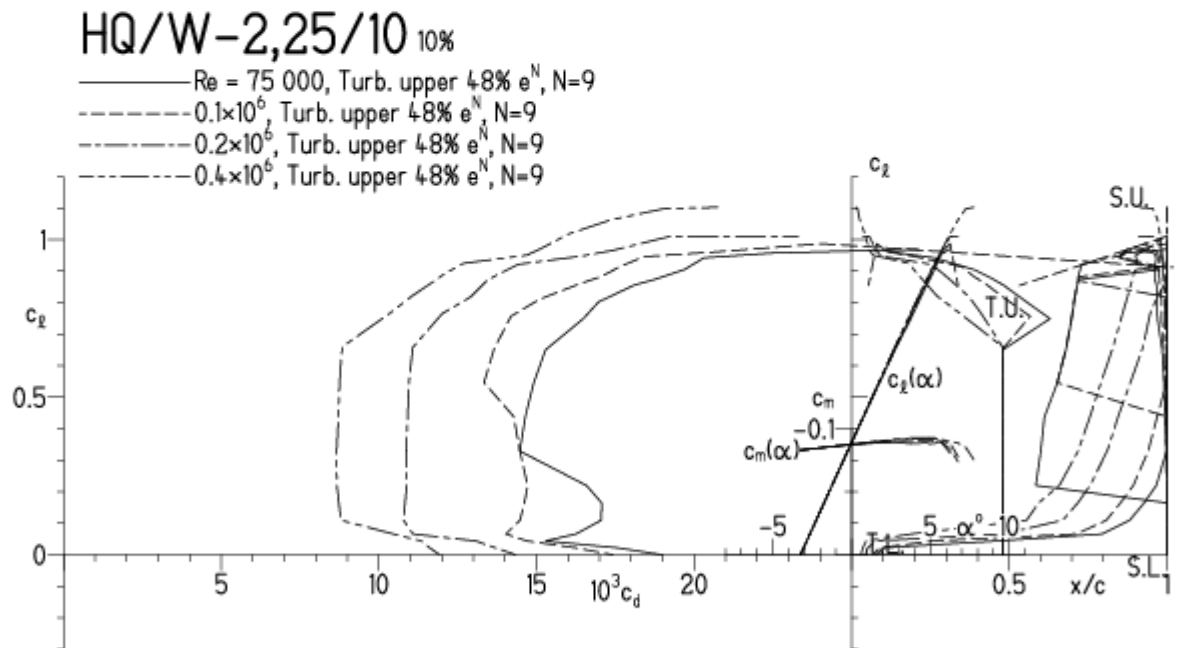


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

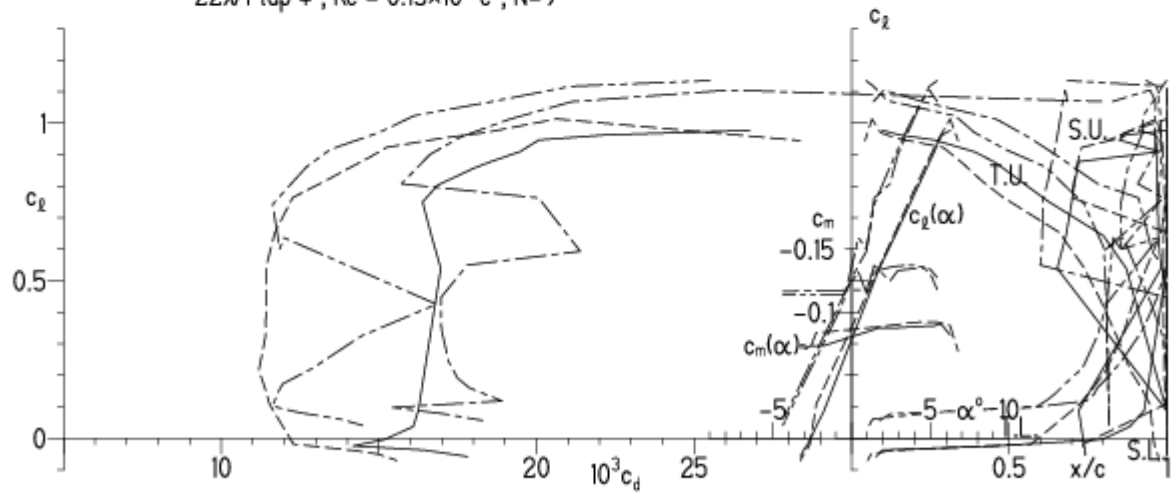


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

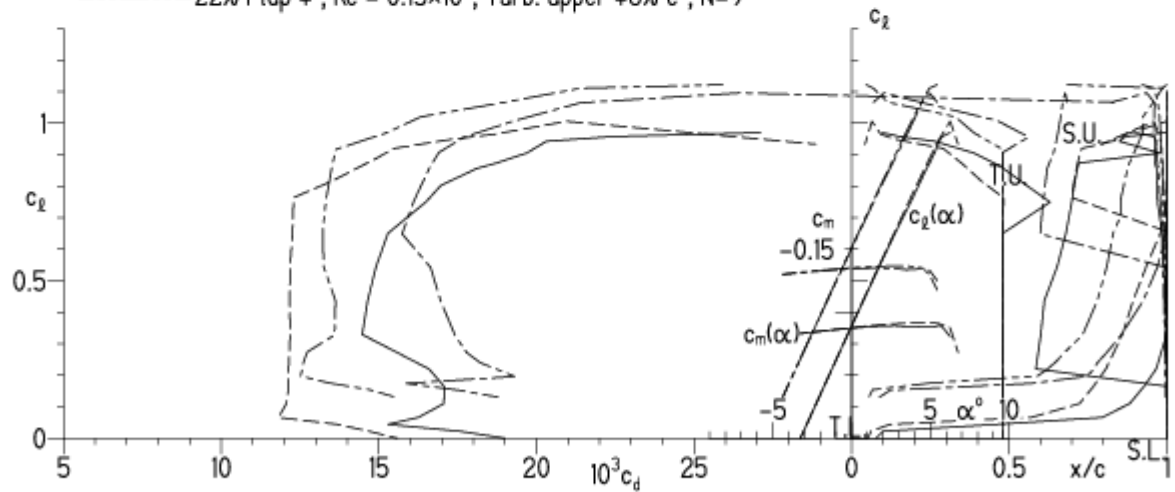


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

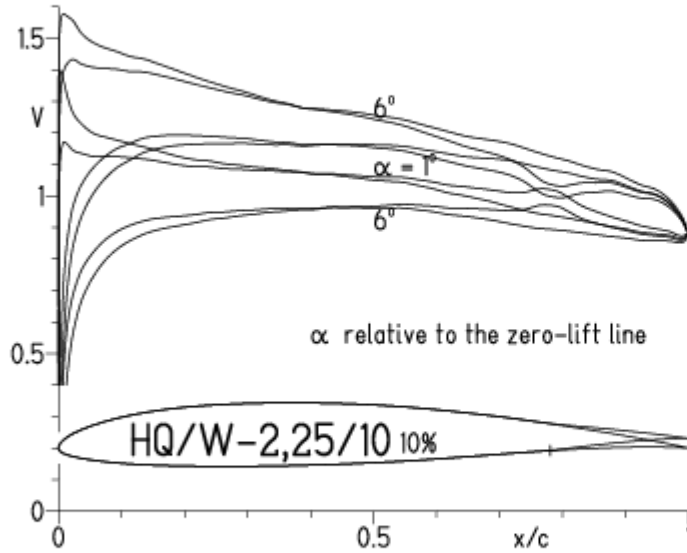
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

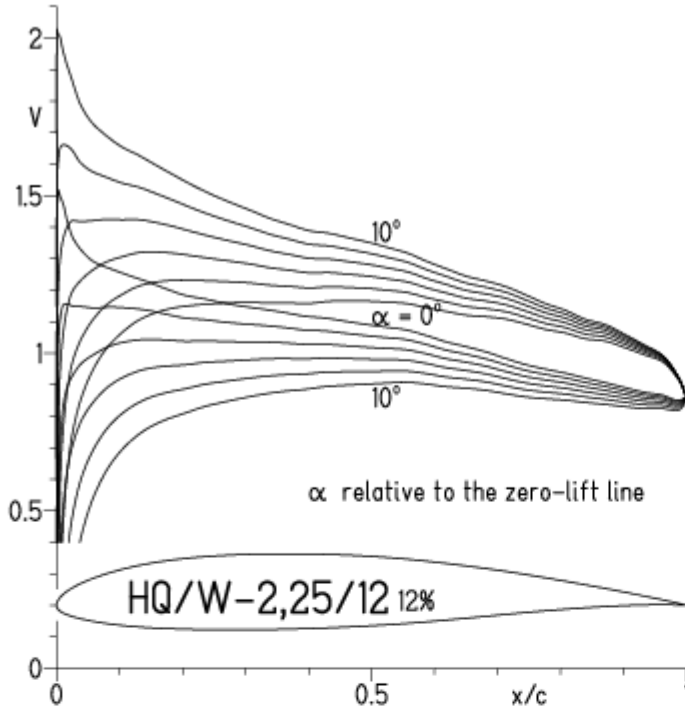
HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- Re = 75 000 e^N, N=9
- - - 0.1×10^6 , Turb. upper 48% e^N, N=9
- · - 0.2×10^6 , Turb. upper 48% e^N, N=9
- - - 0.4×10^6 , Turb. upper 48% e^N, N=9



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

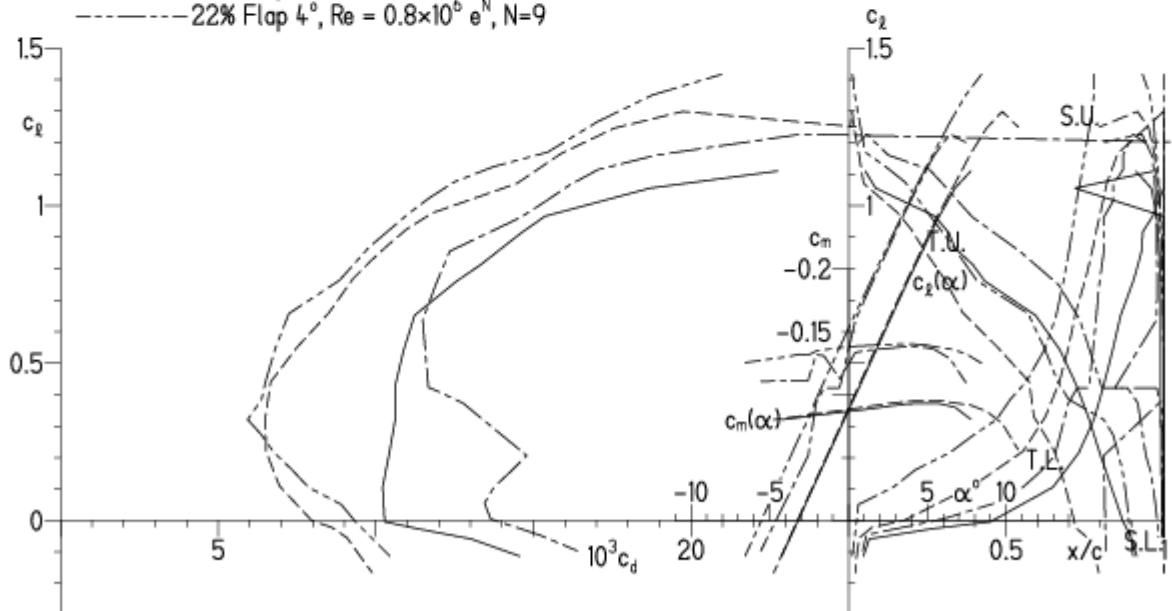


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - $0.8 \times 10^6 e^N, N=9$
- · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00

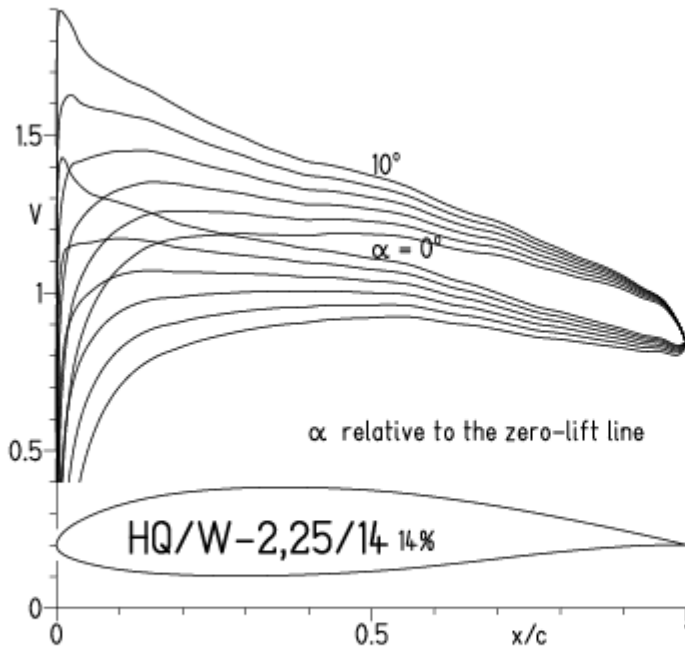


EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

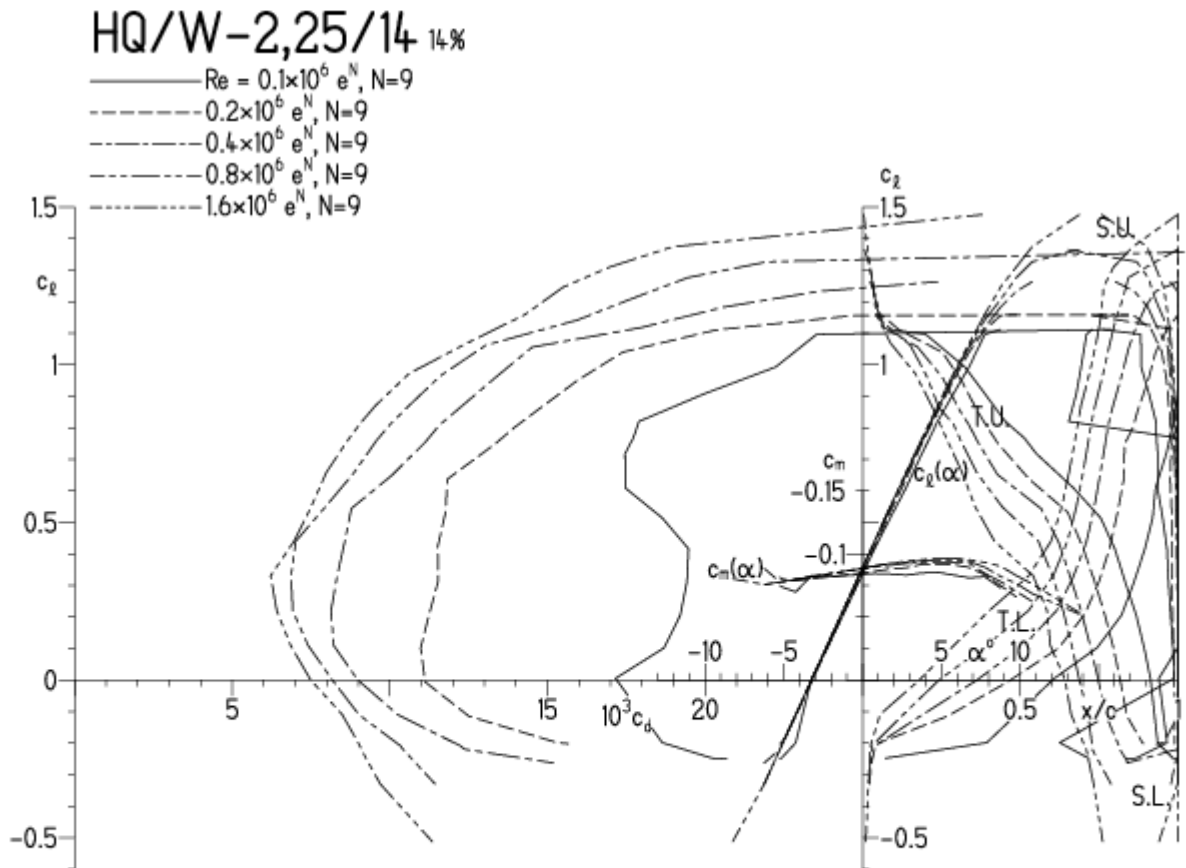


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

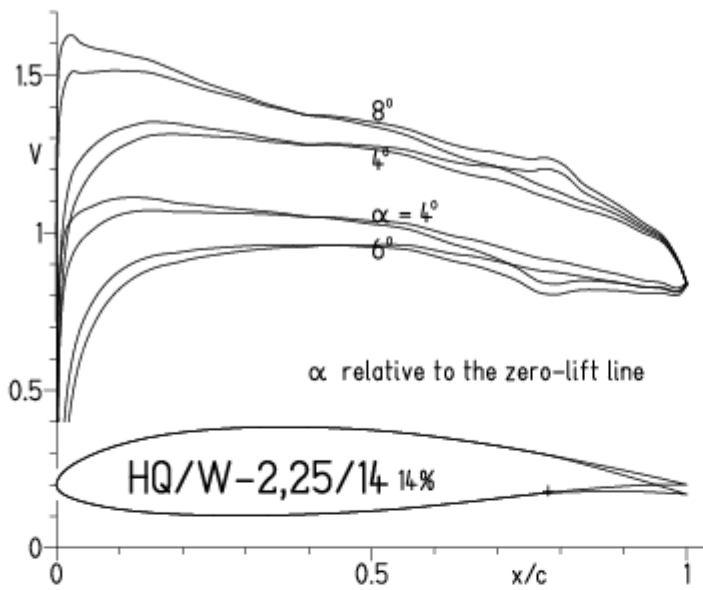
HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

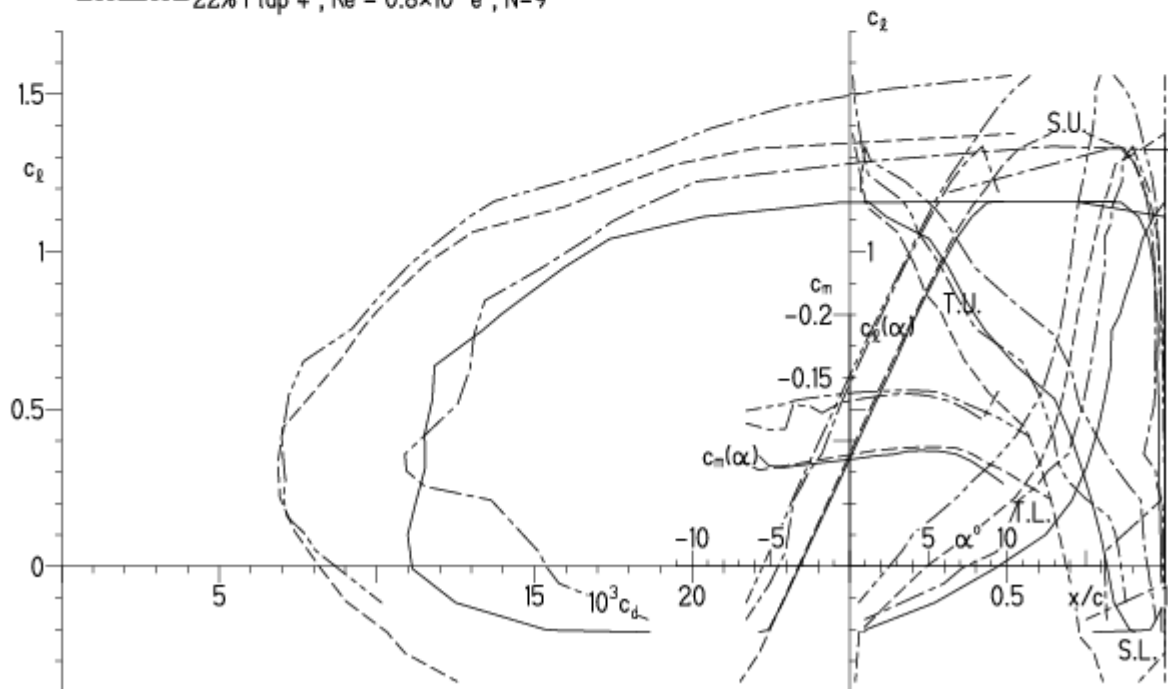


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

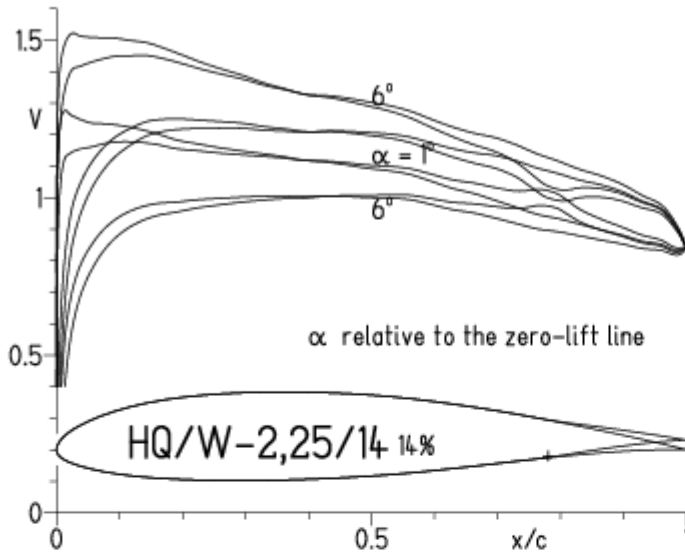
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

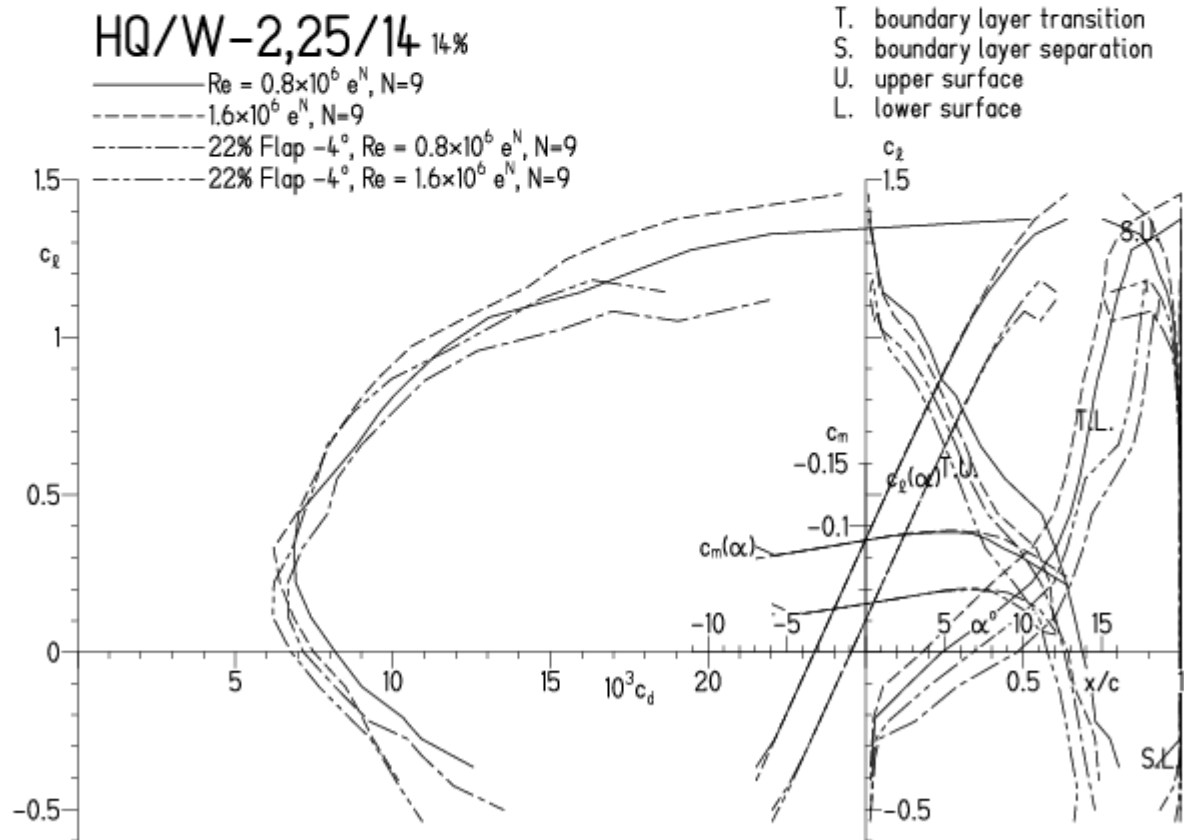


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

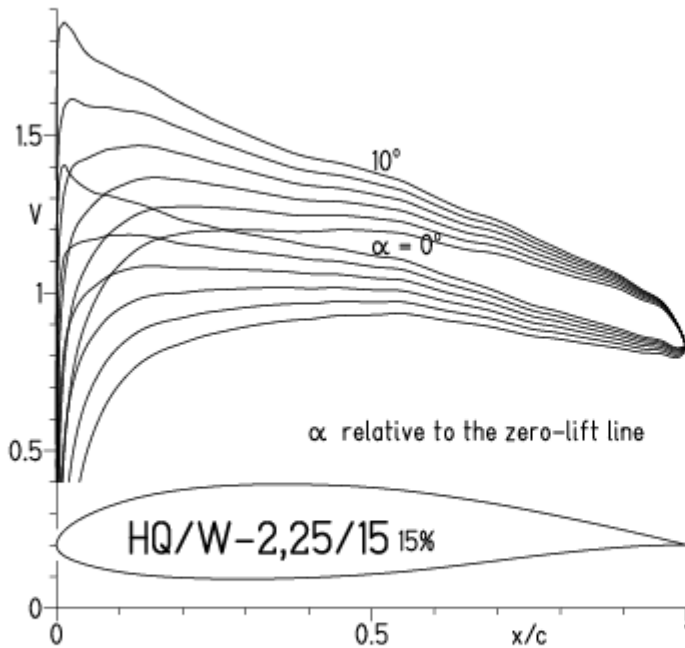


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

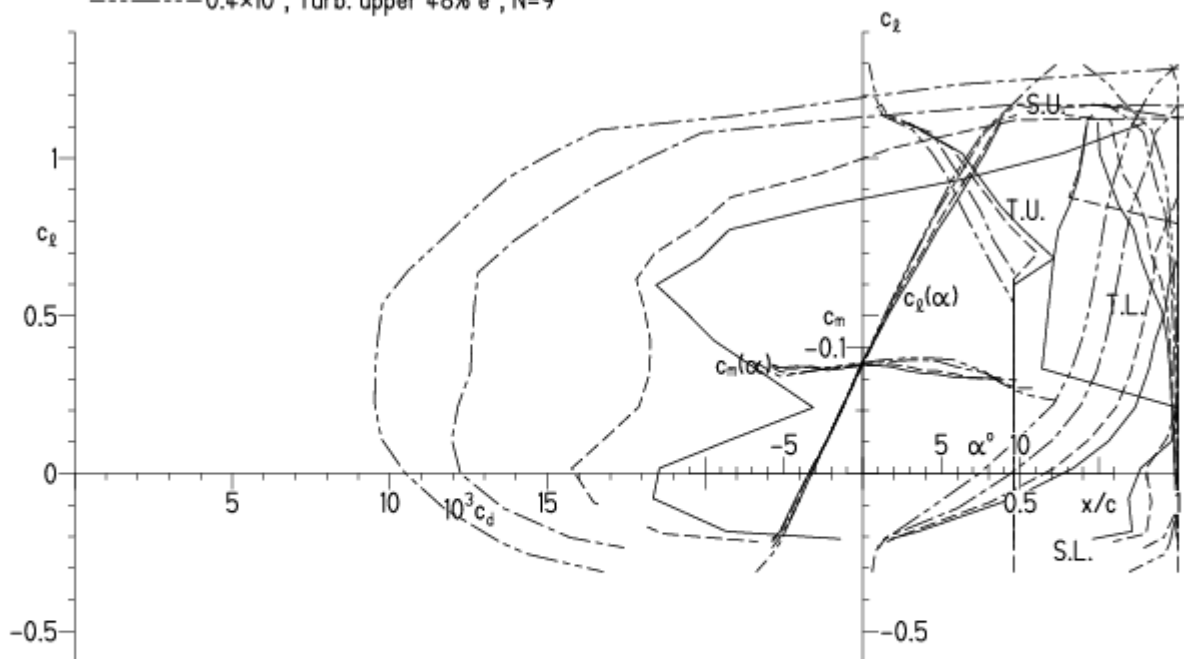
EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

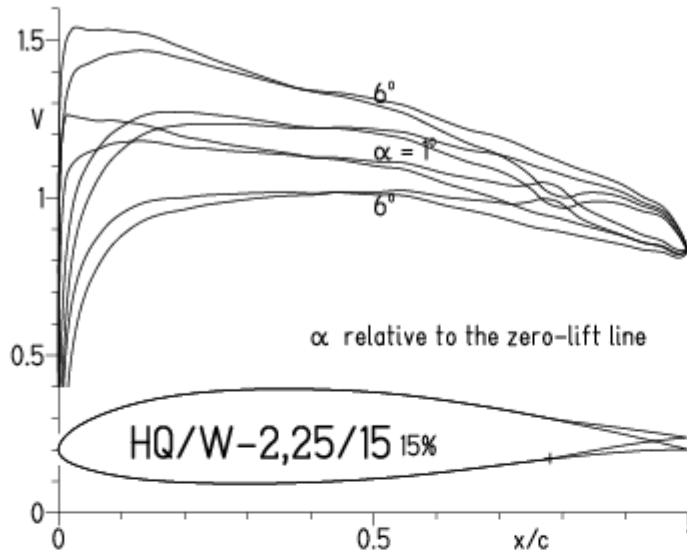


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

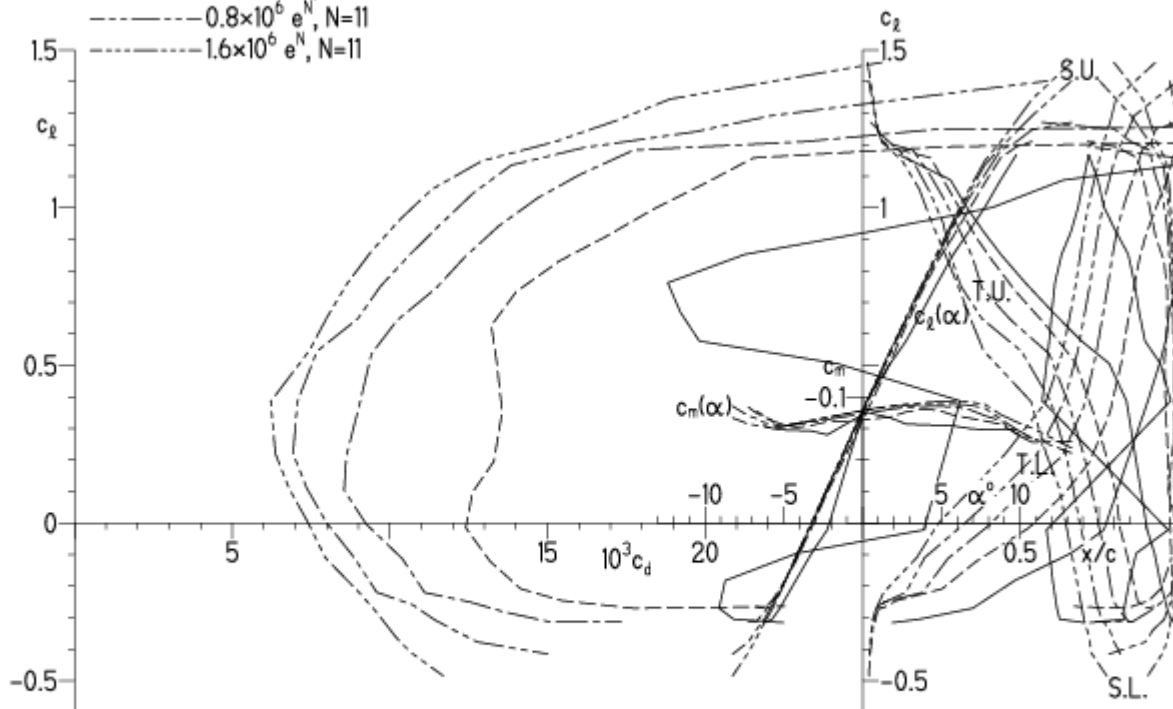
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/16, N=9

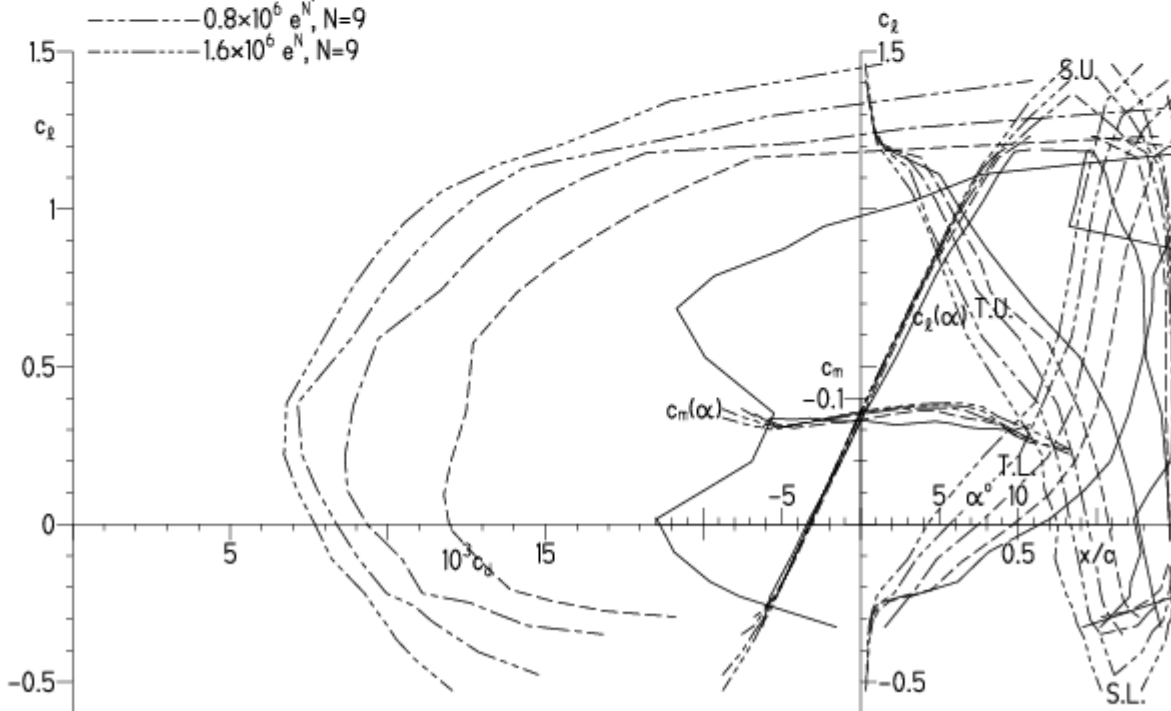
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

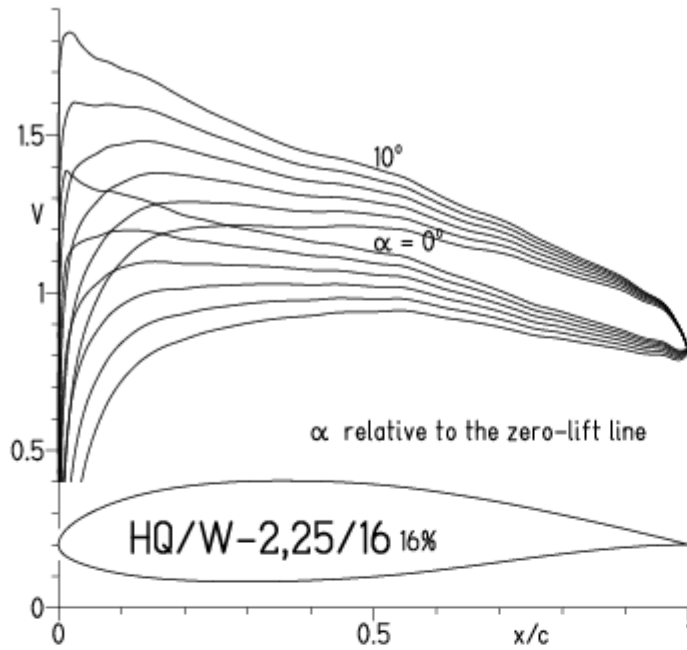
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

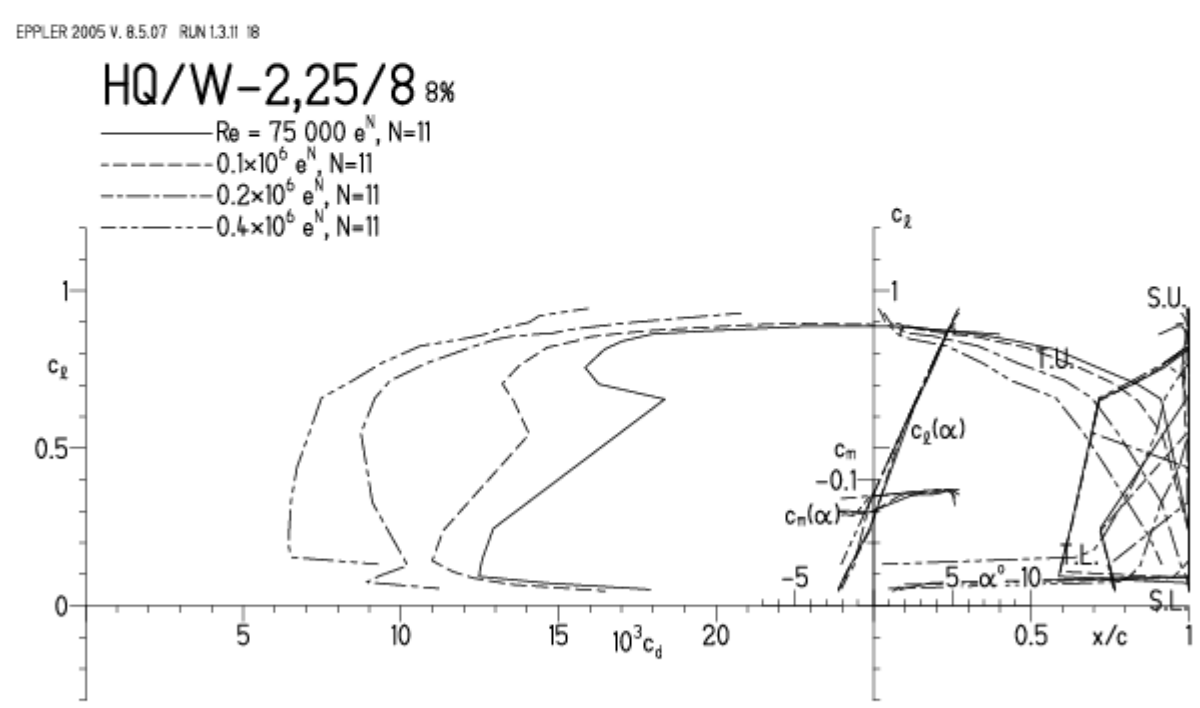
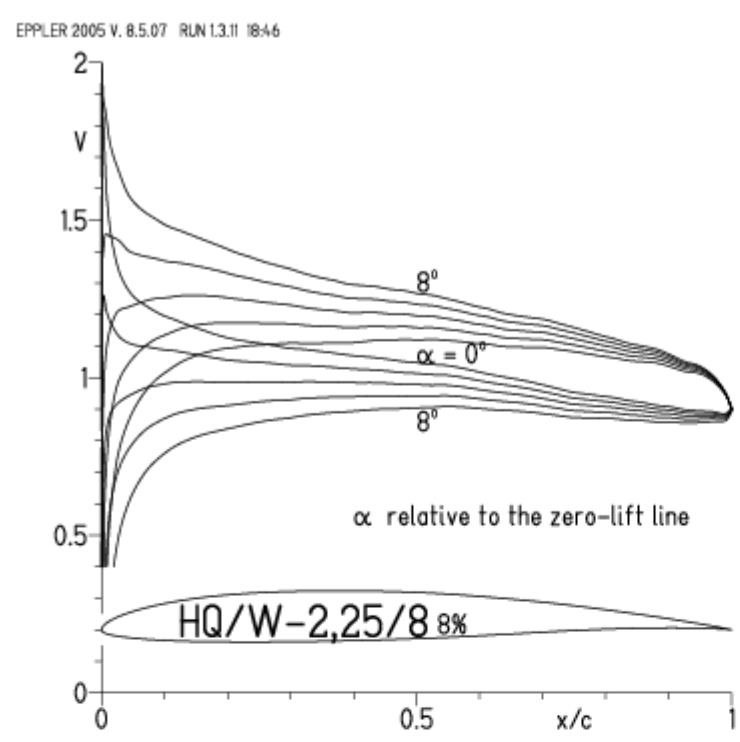
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11



HQ/W-2,25/8, N=9

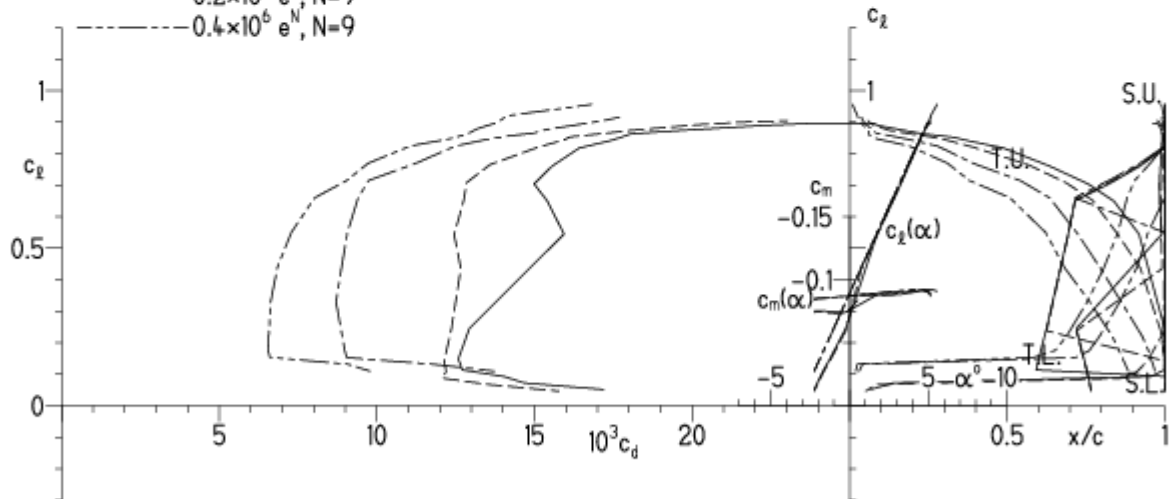
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

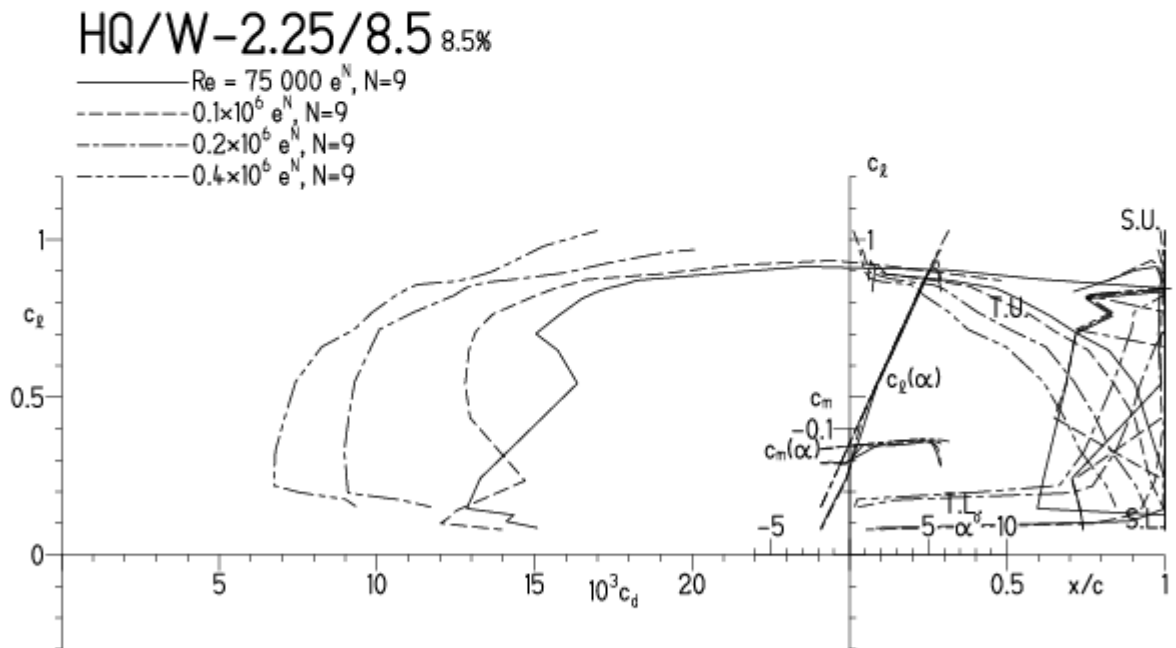


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

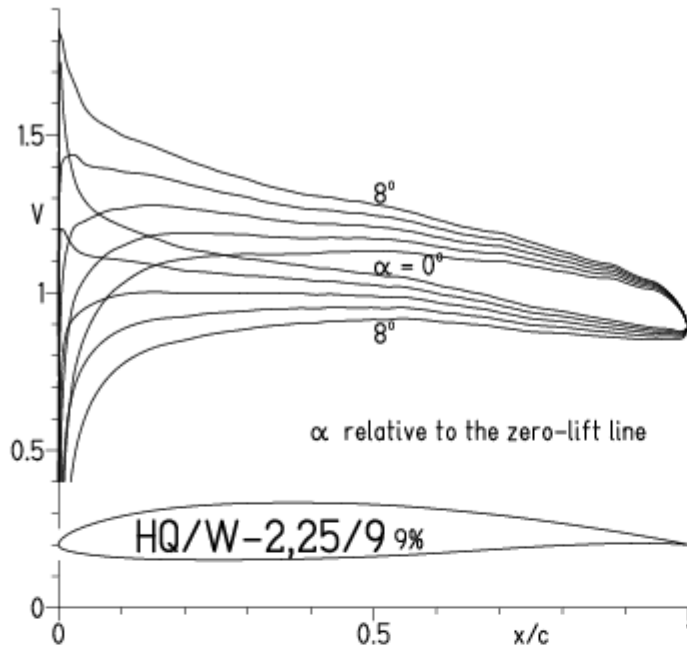


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

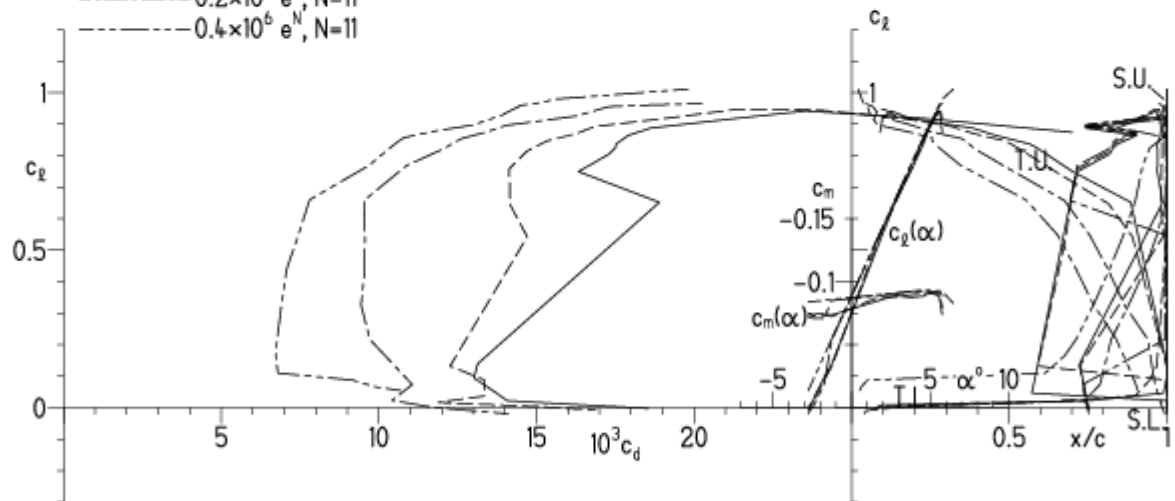
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

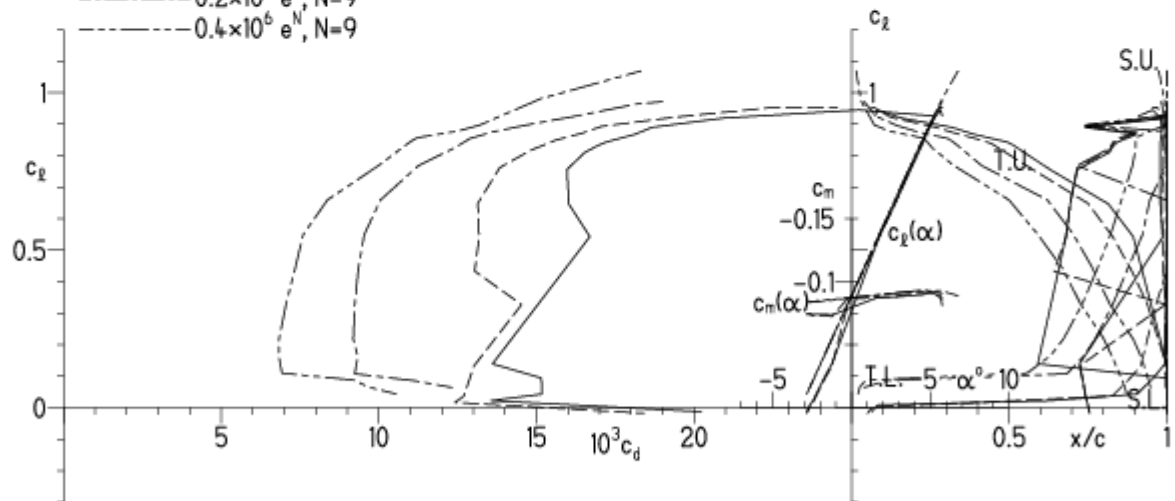
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

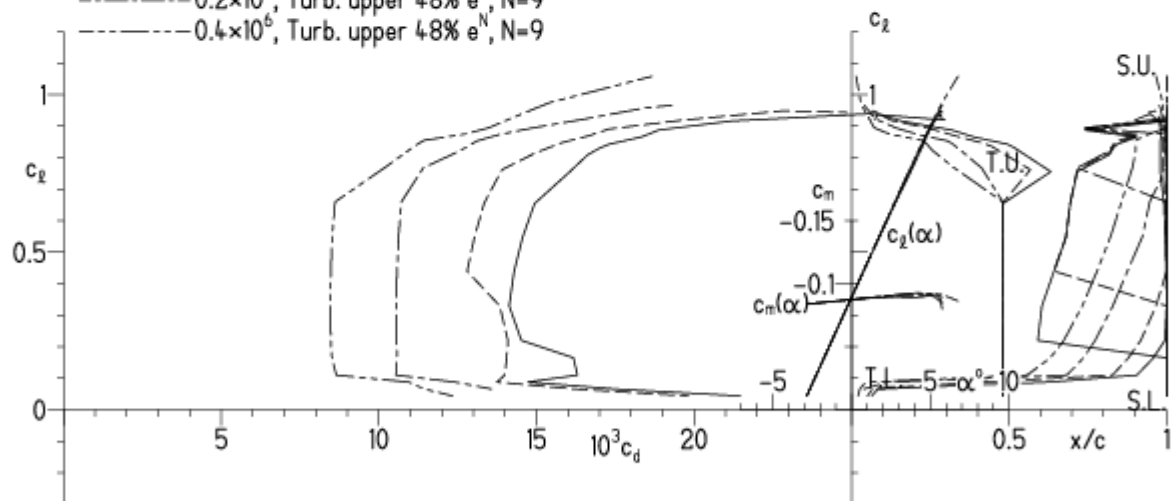
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

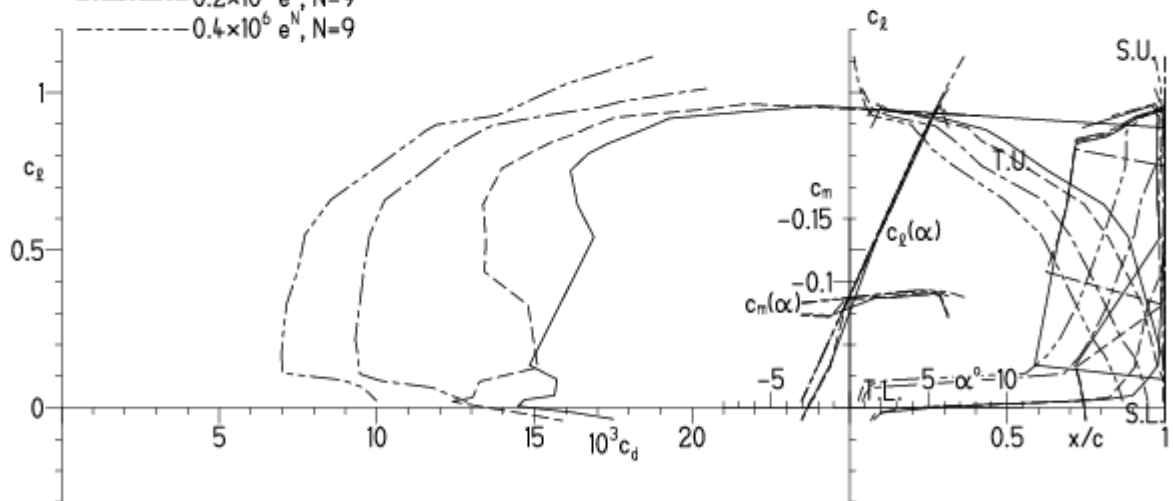
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

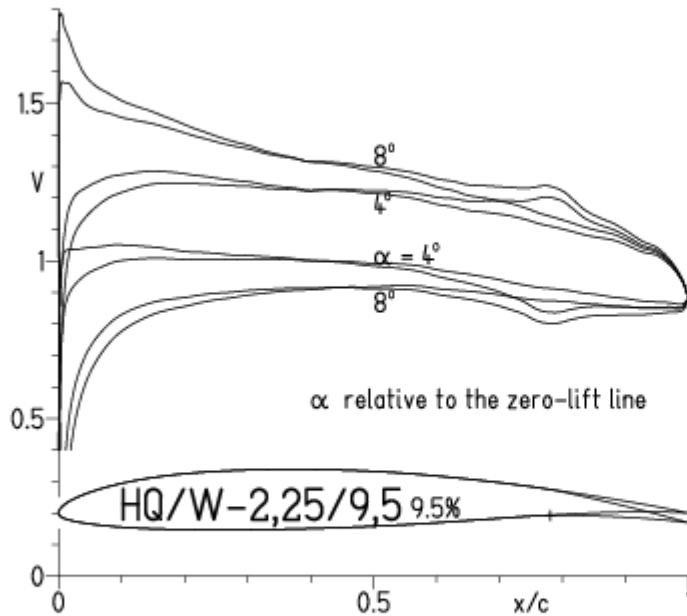
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
(Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

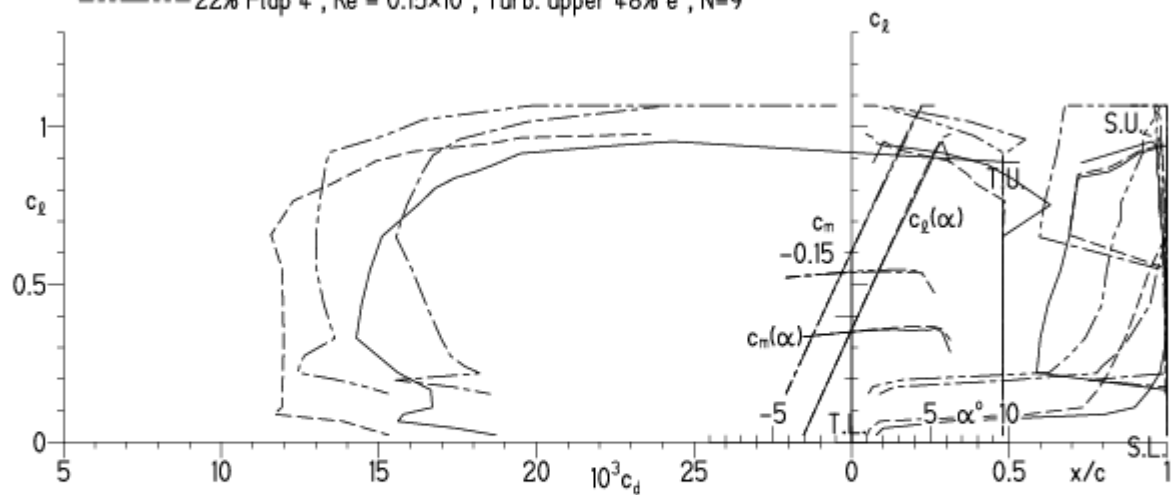


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

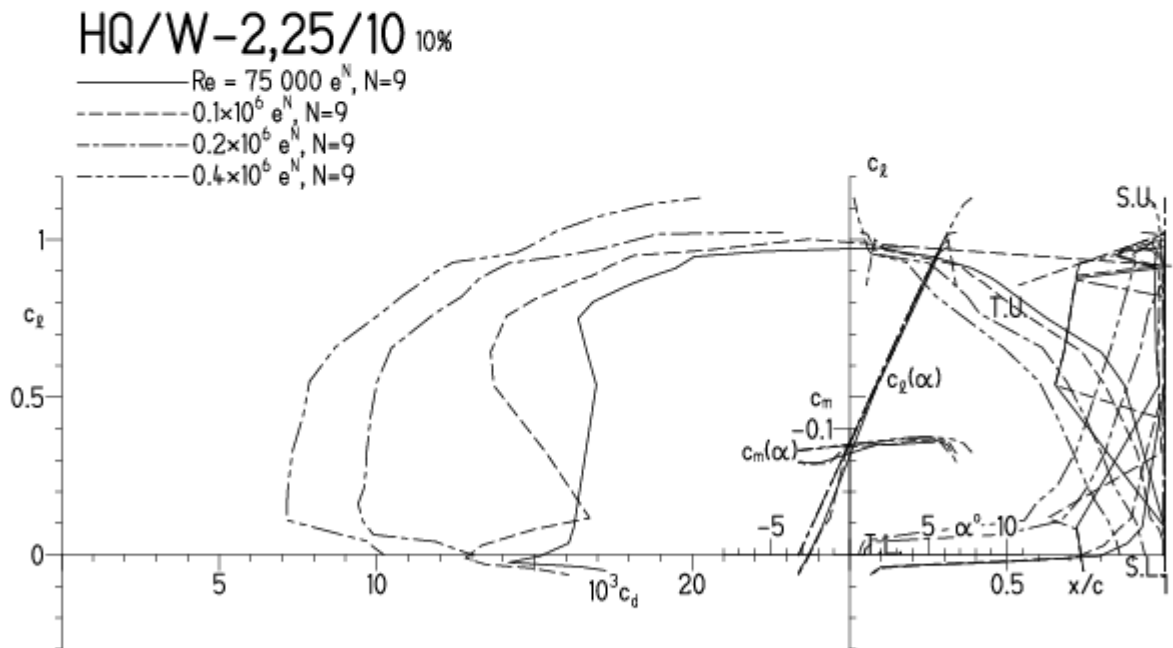


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

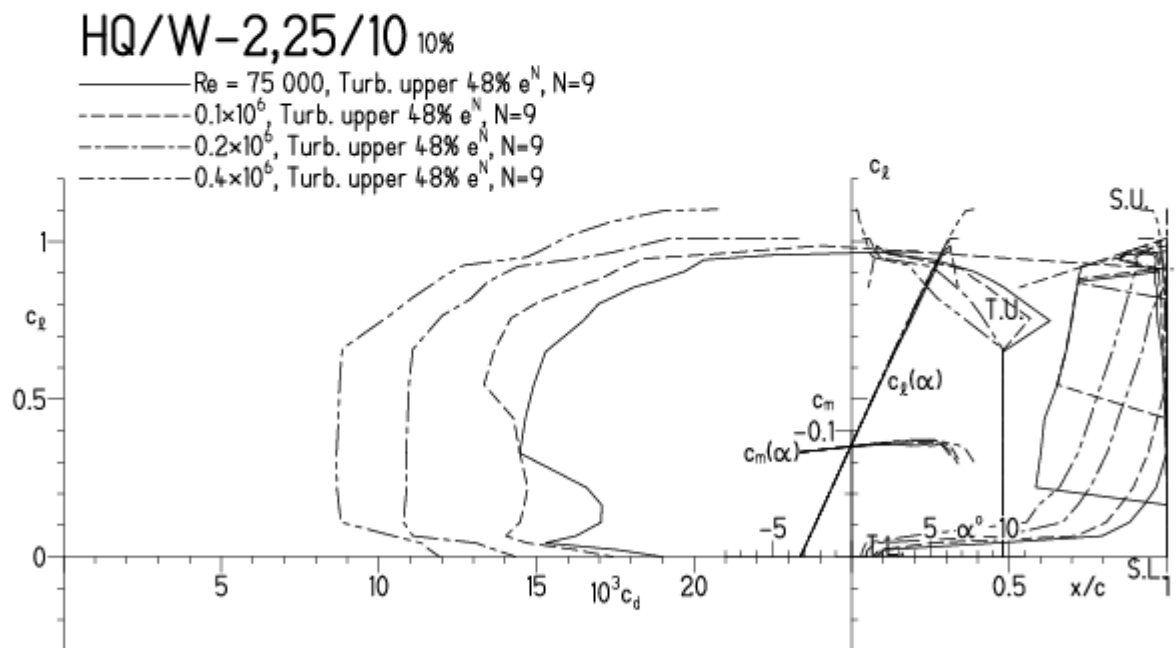


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

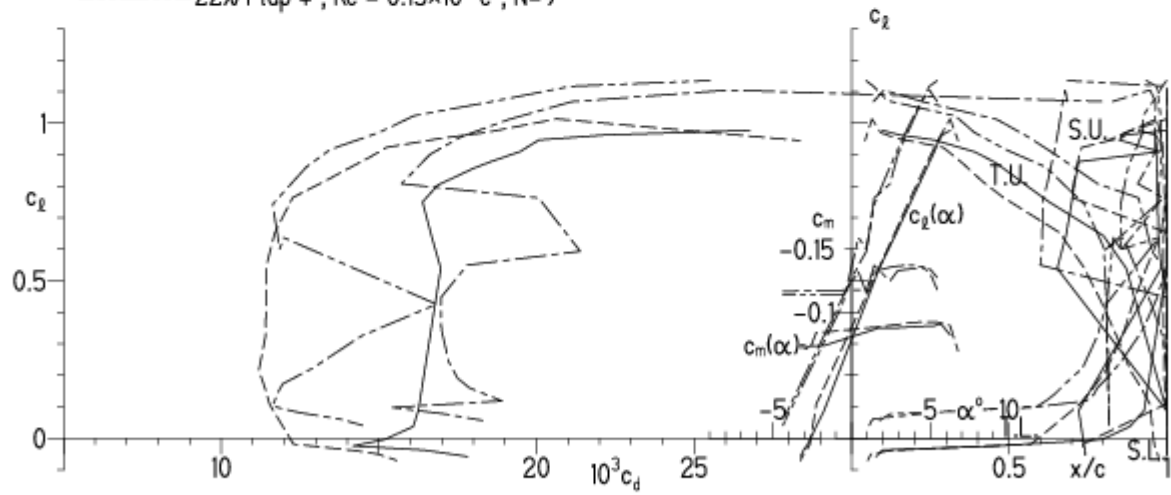


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

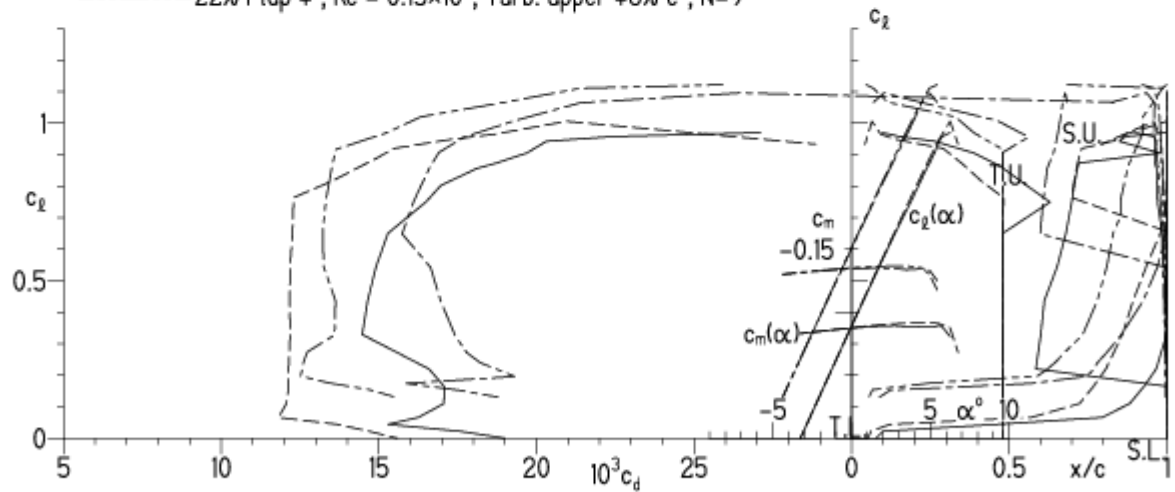


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

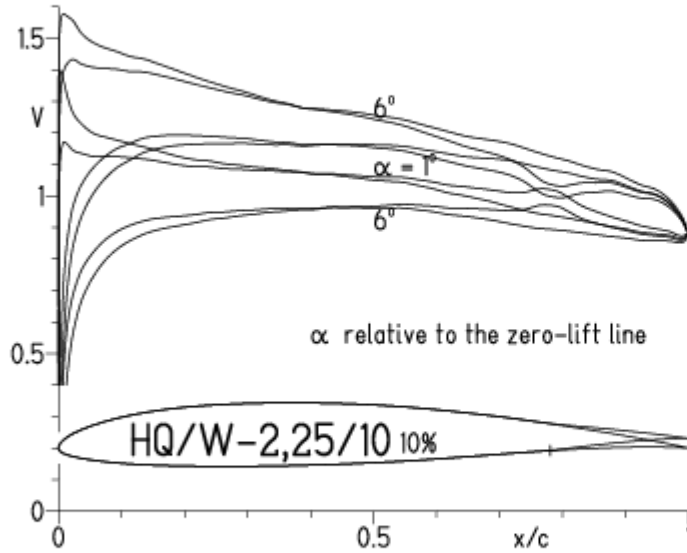
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

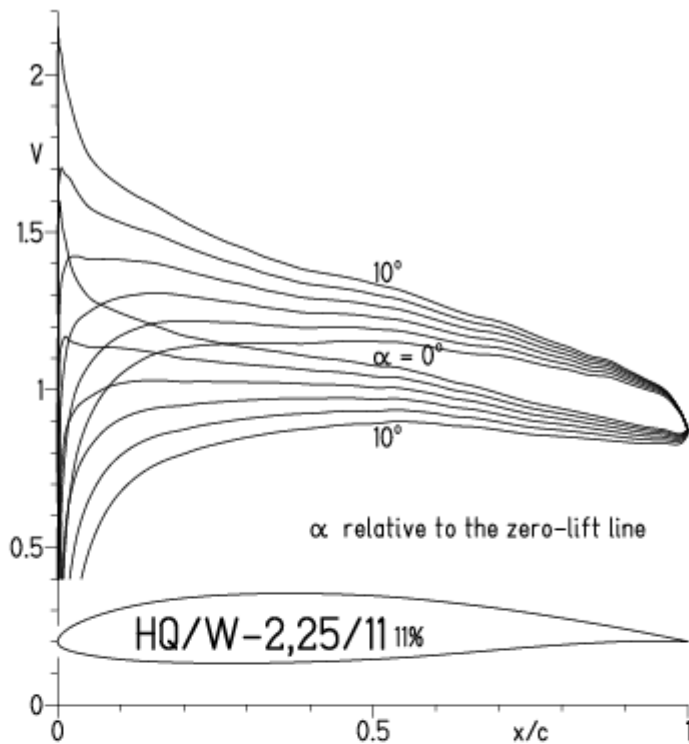


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

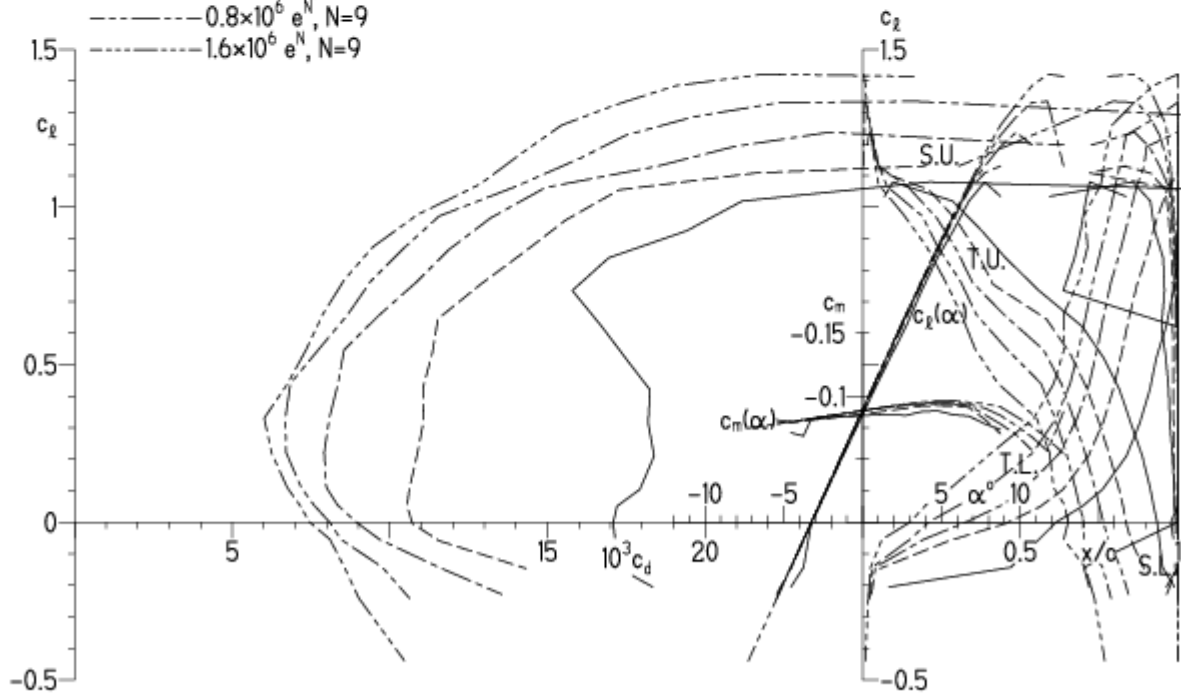
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

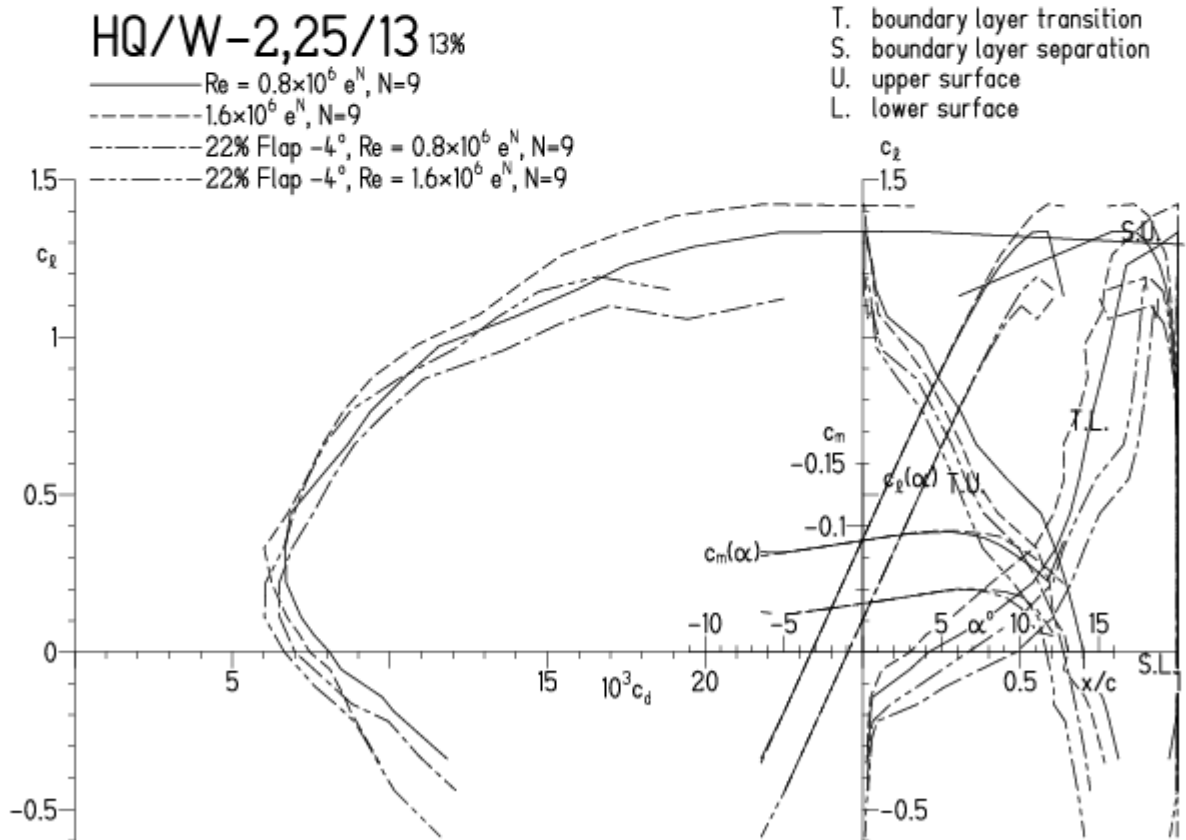


HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

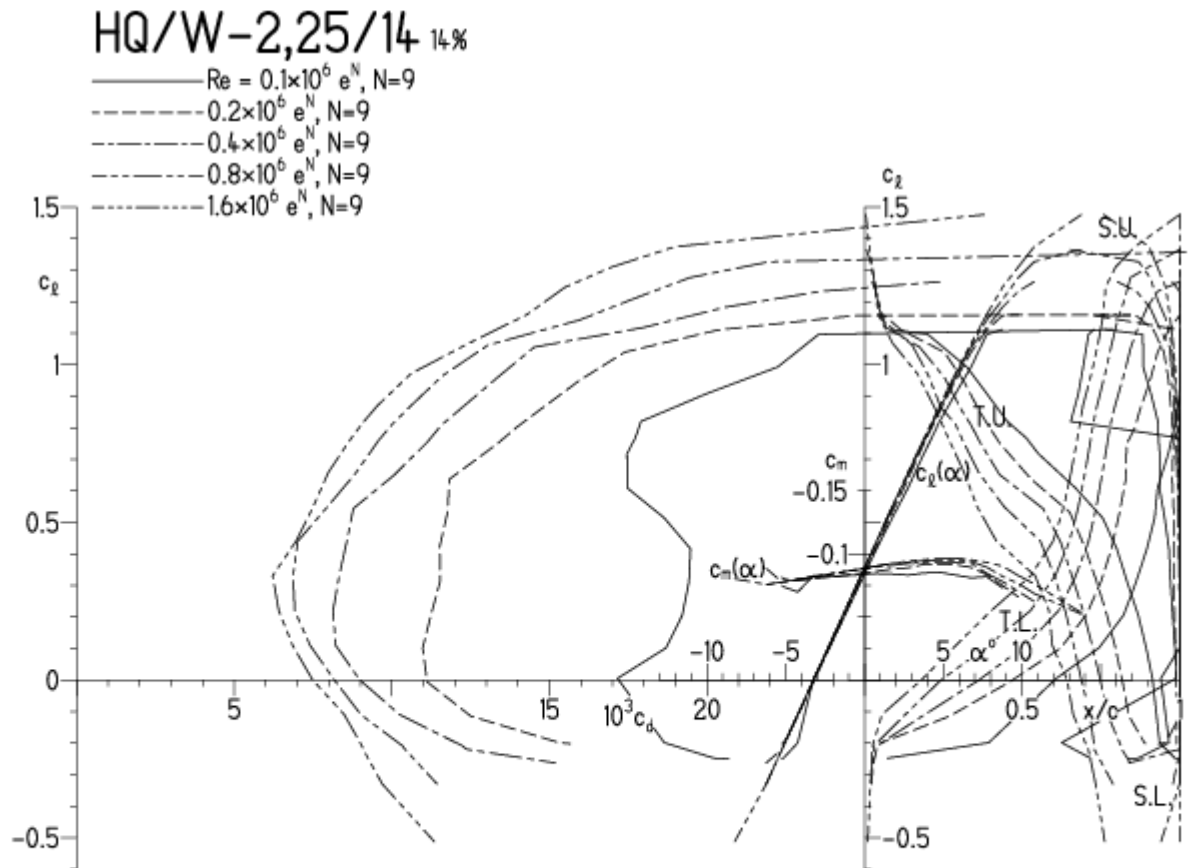


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

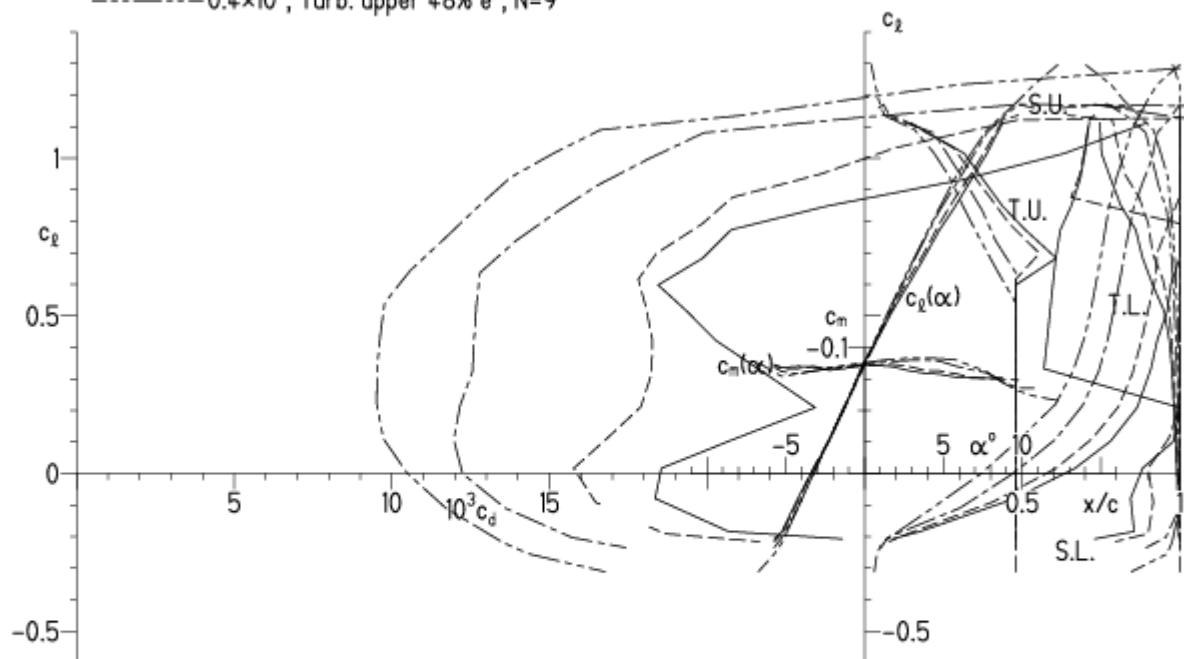
EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

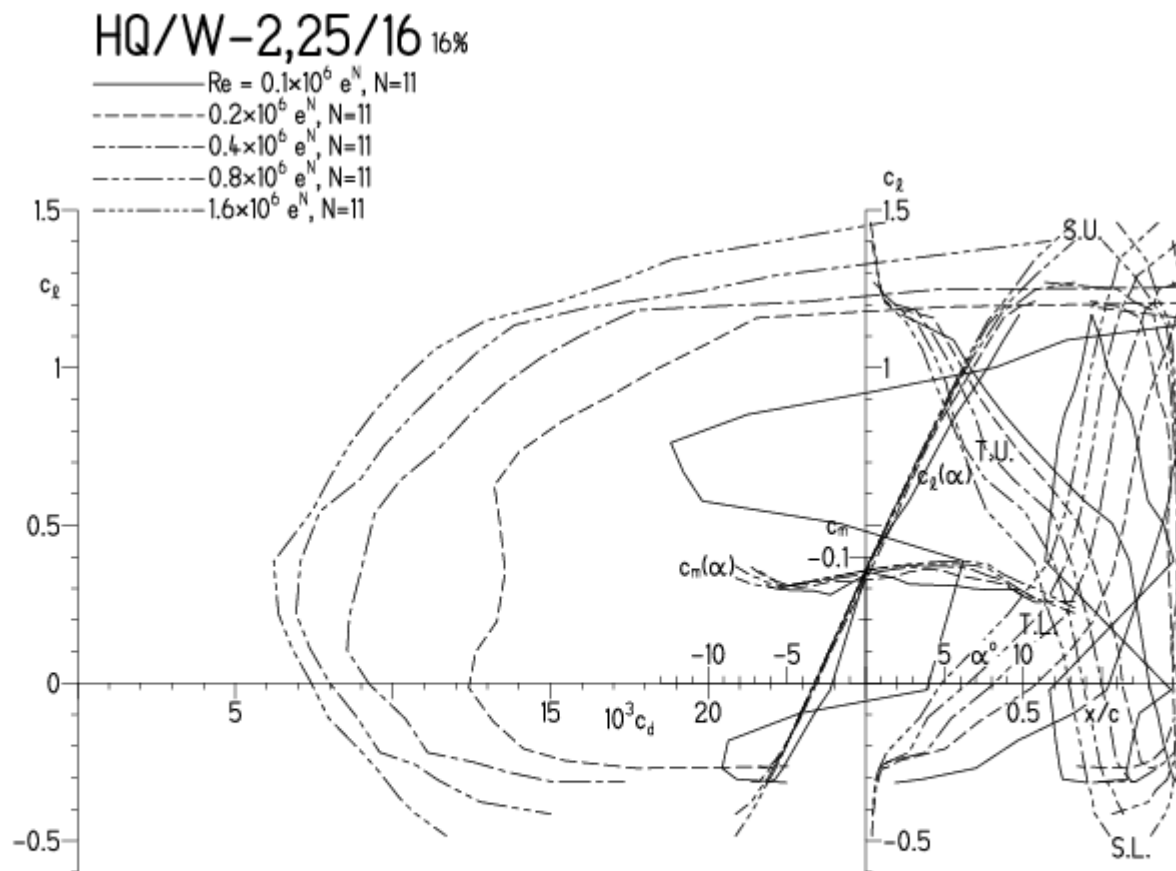


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

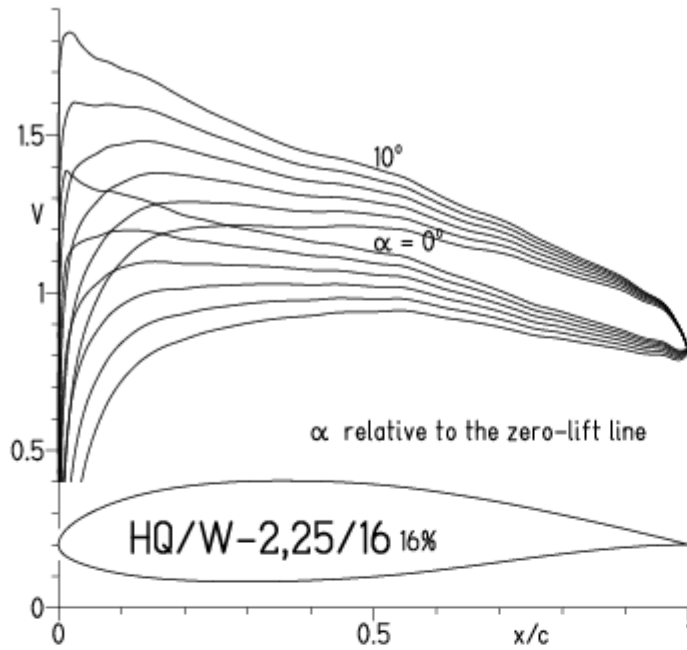
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

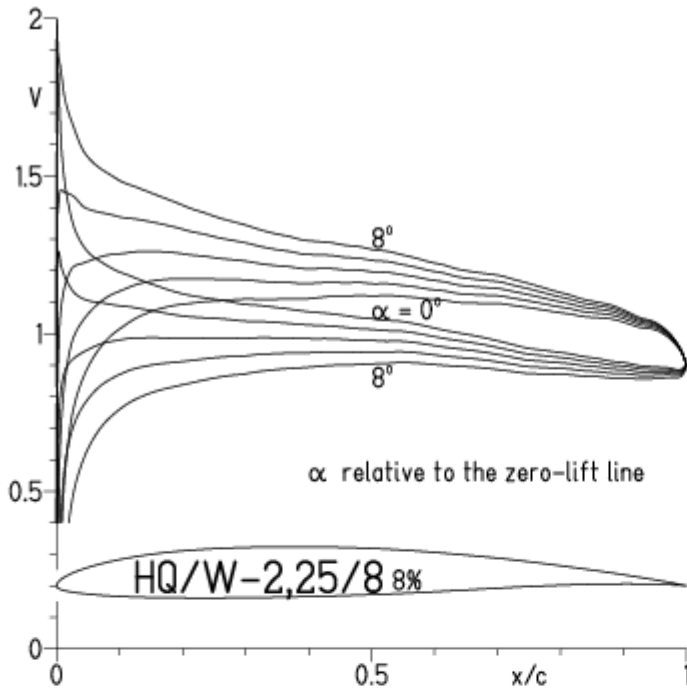
HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - · 22% Flap 4°, Re = 75 000 e^N, N=9
- · - · 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

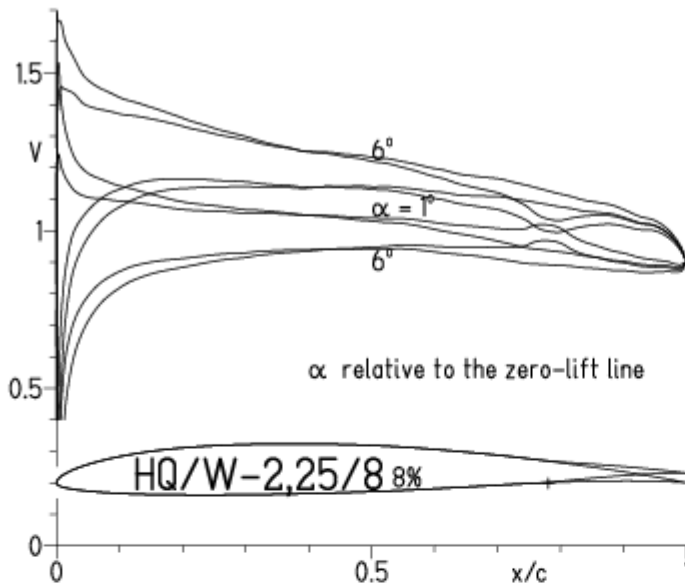
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

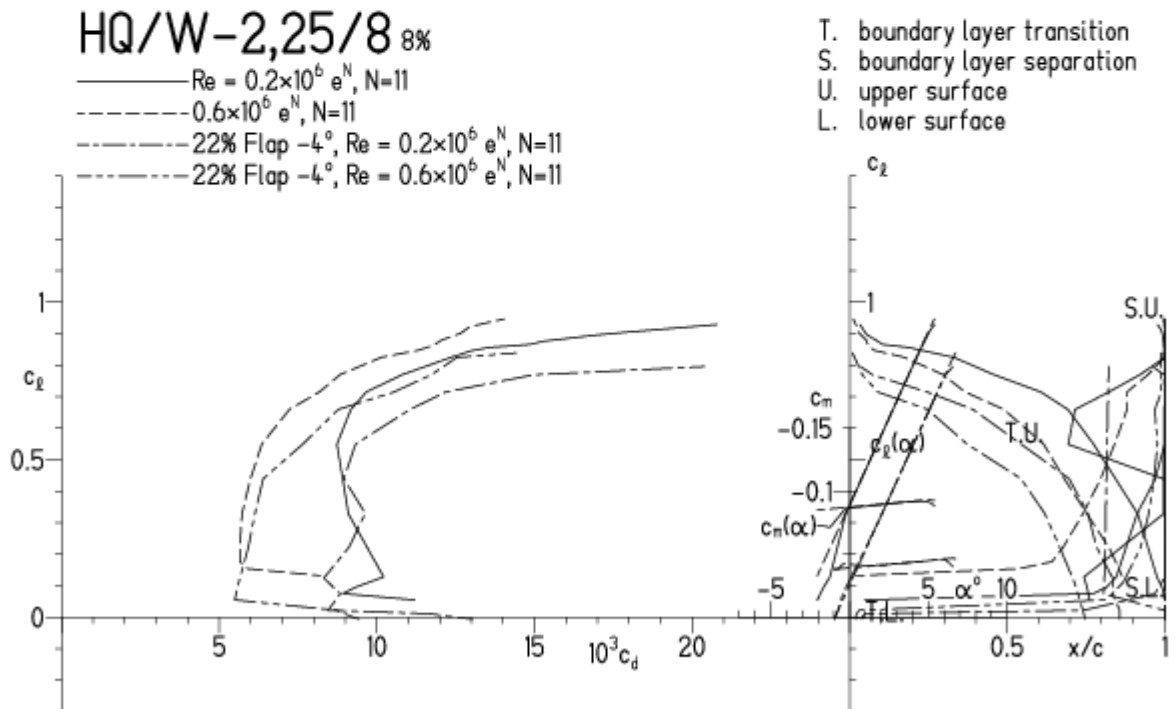


HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23

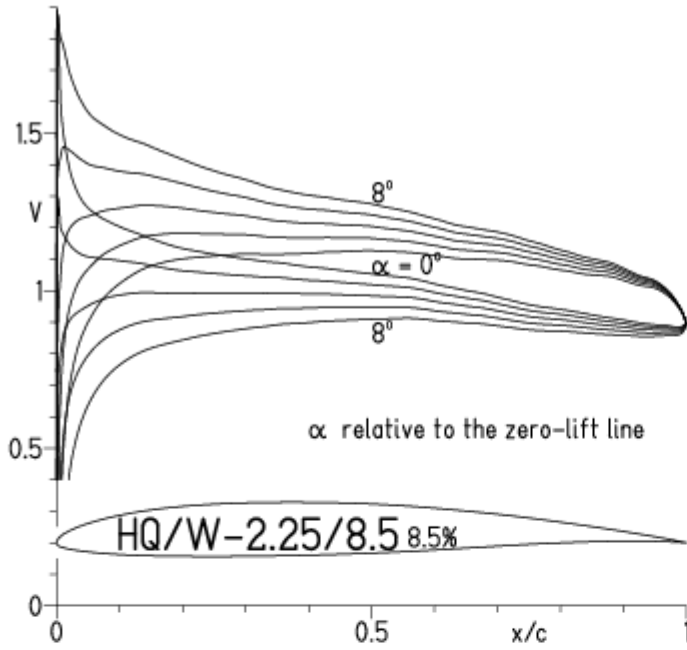


EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

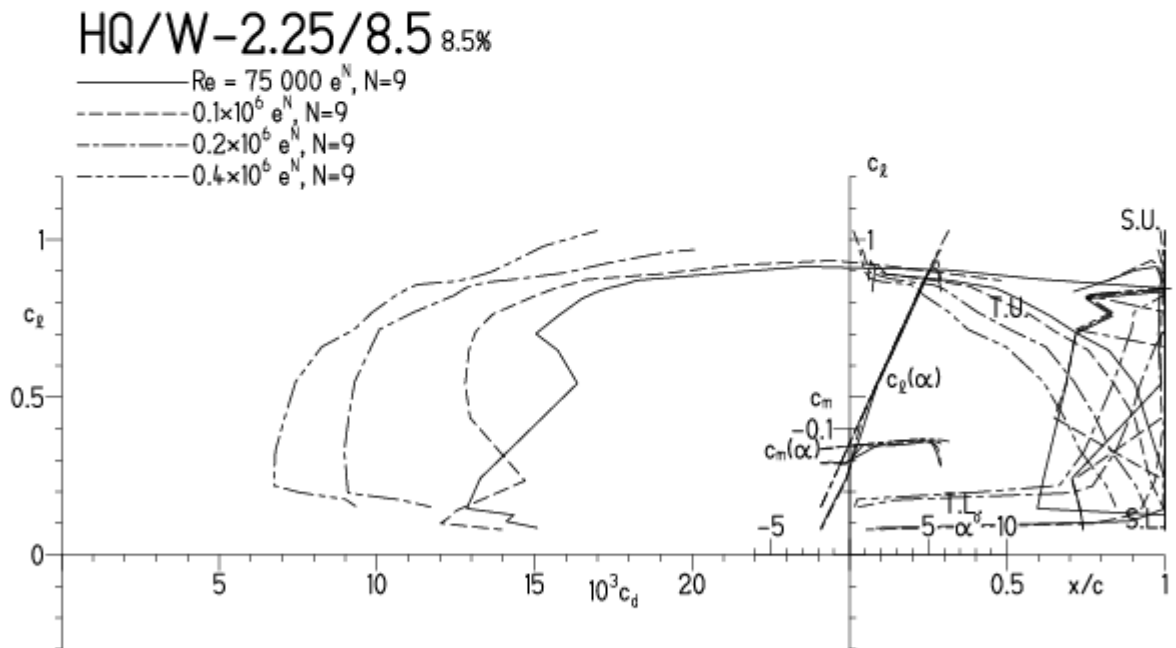


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

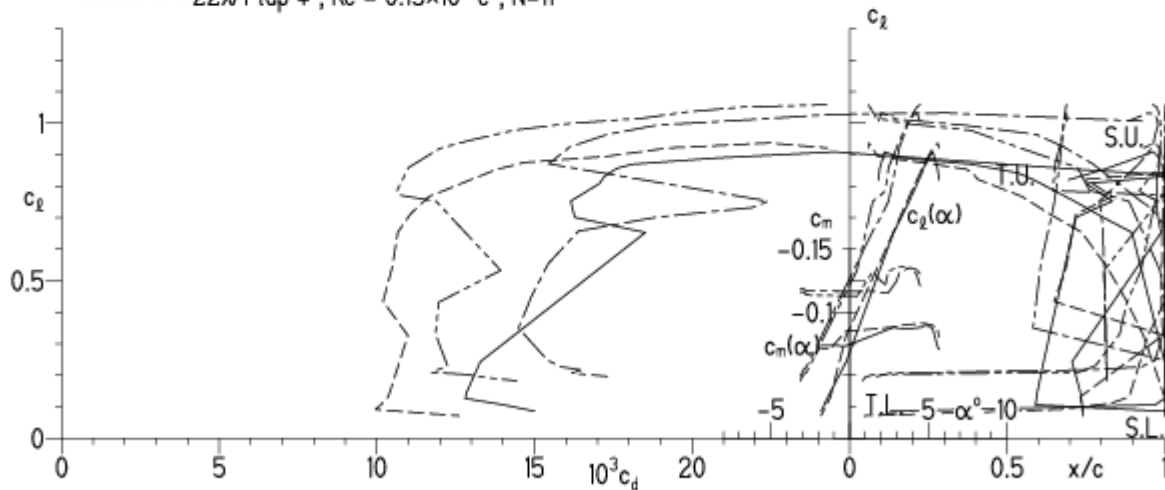


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

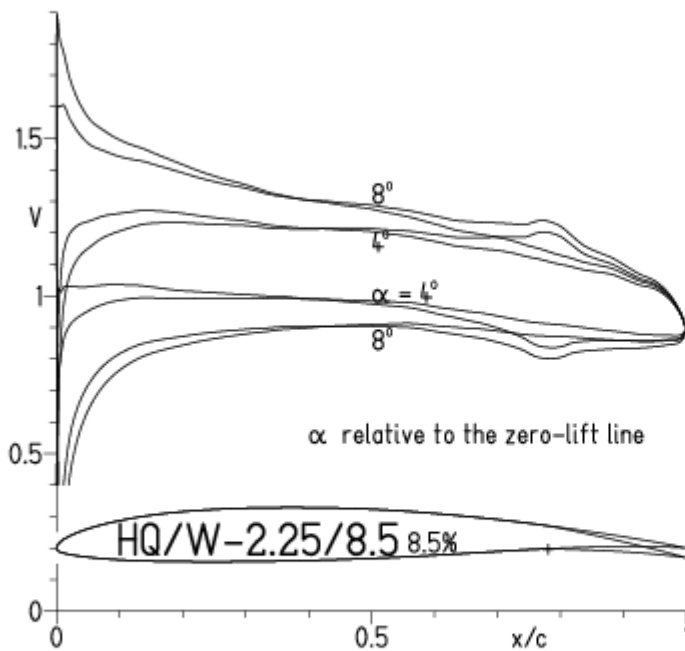
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

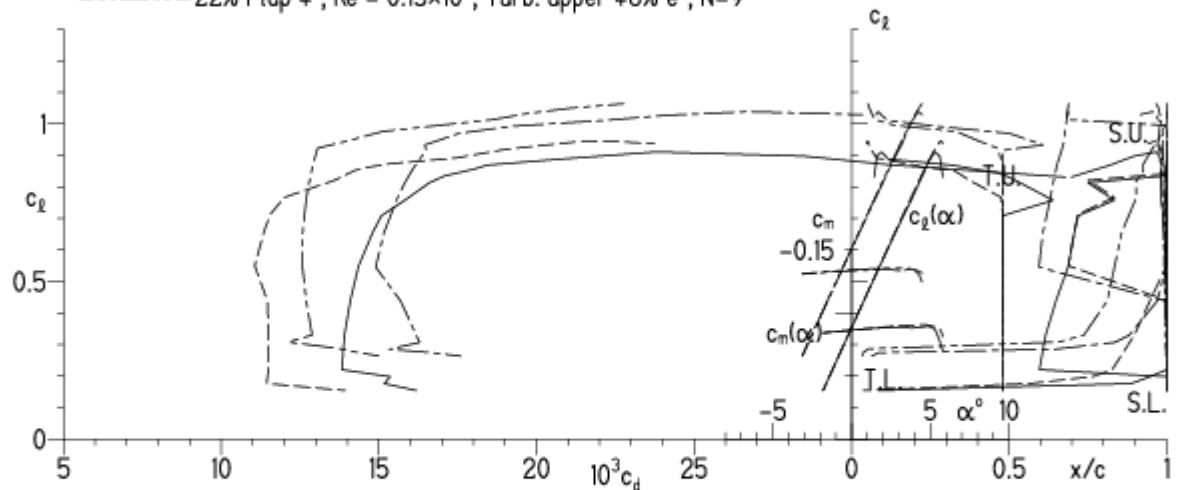


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

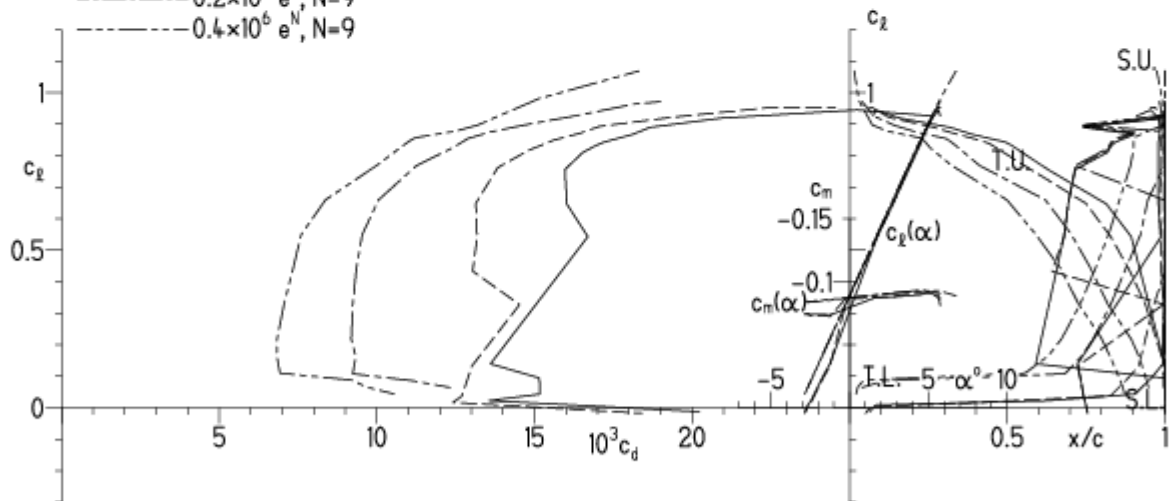
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

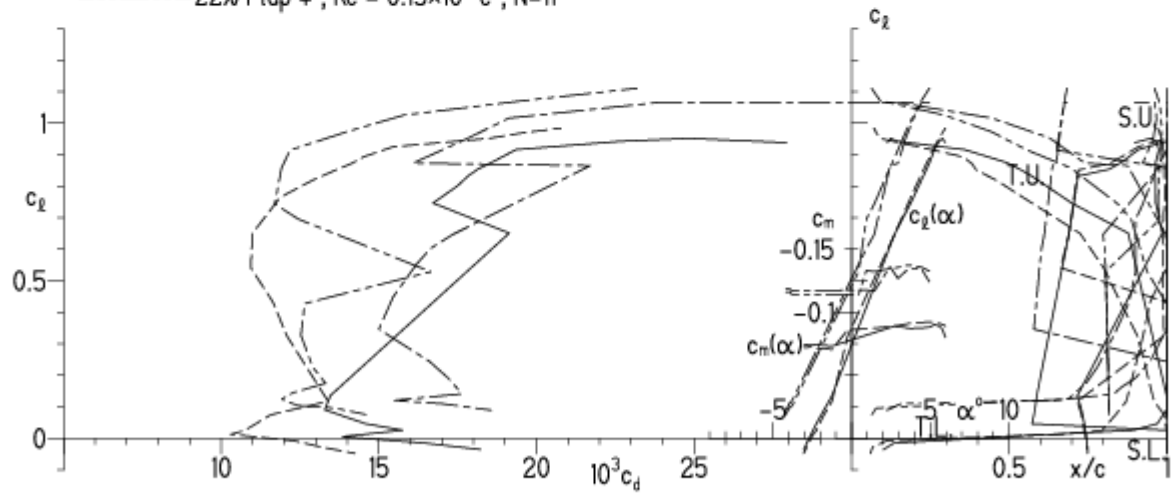


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

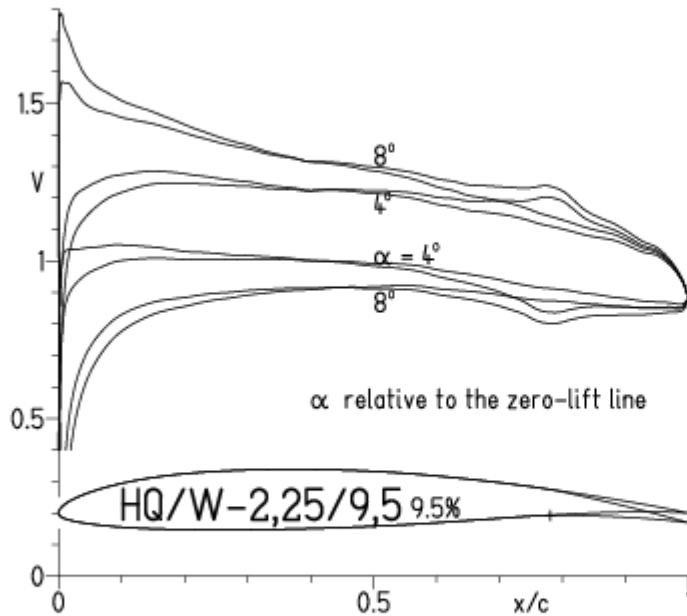
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
(Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

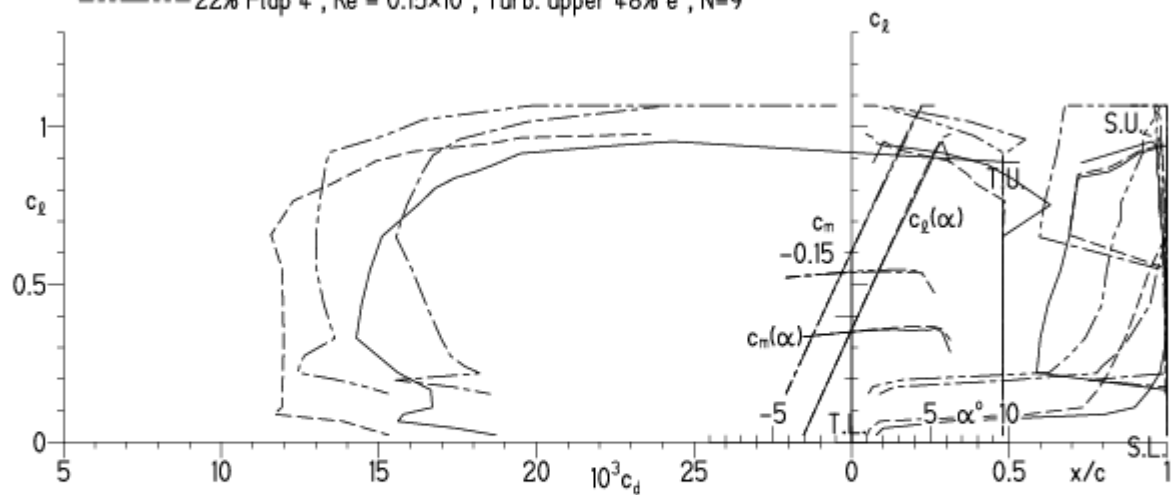


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



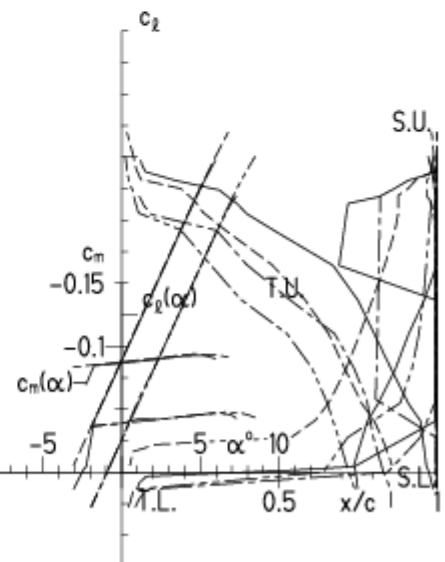
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

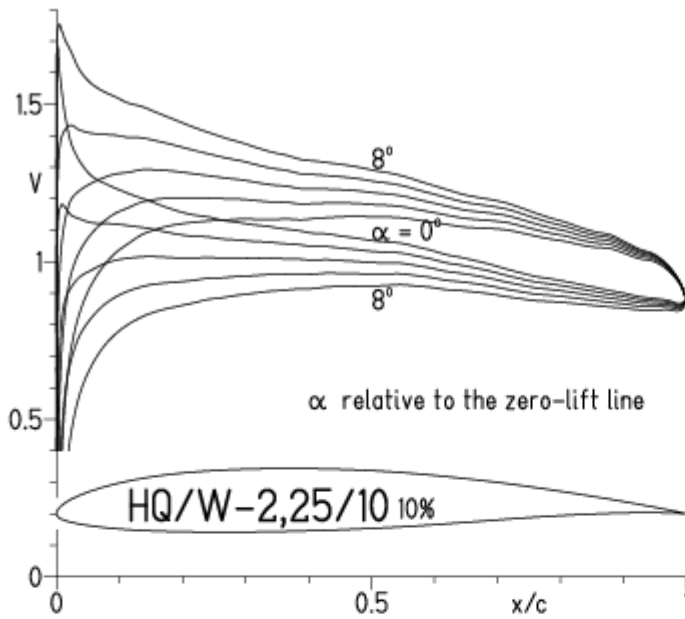


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

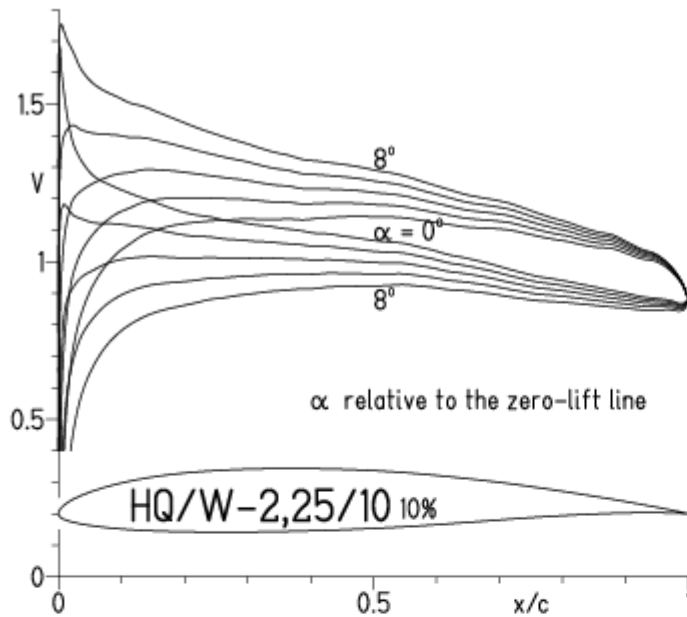


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

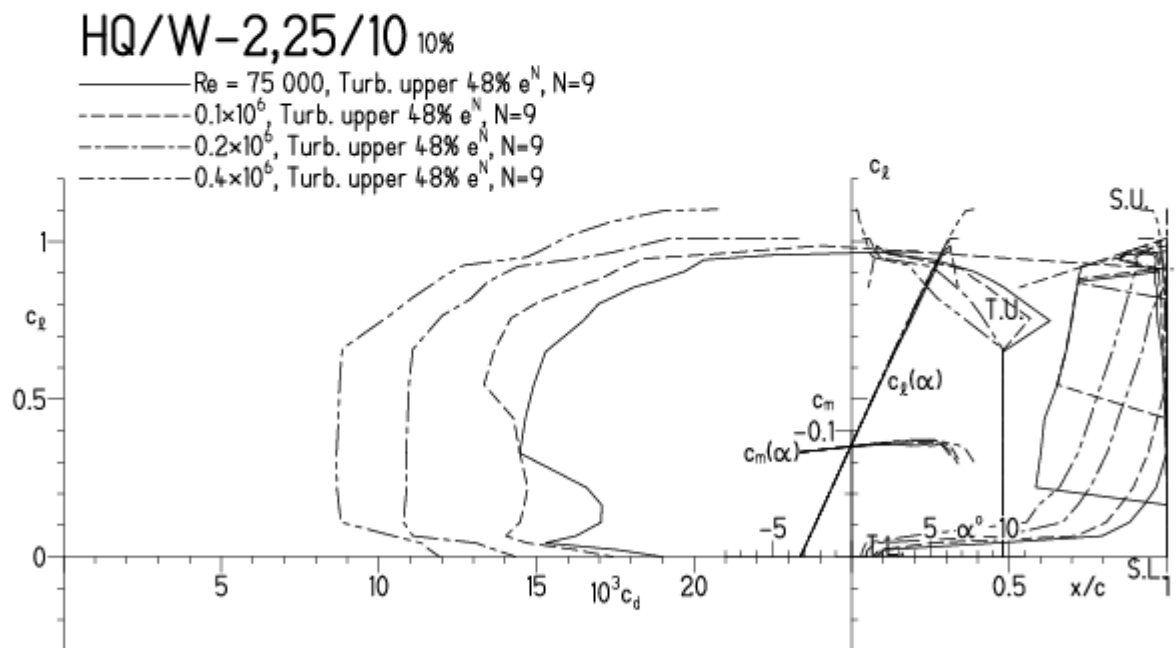


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

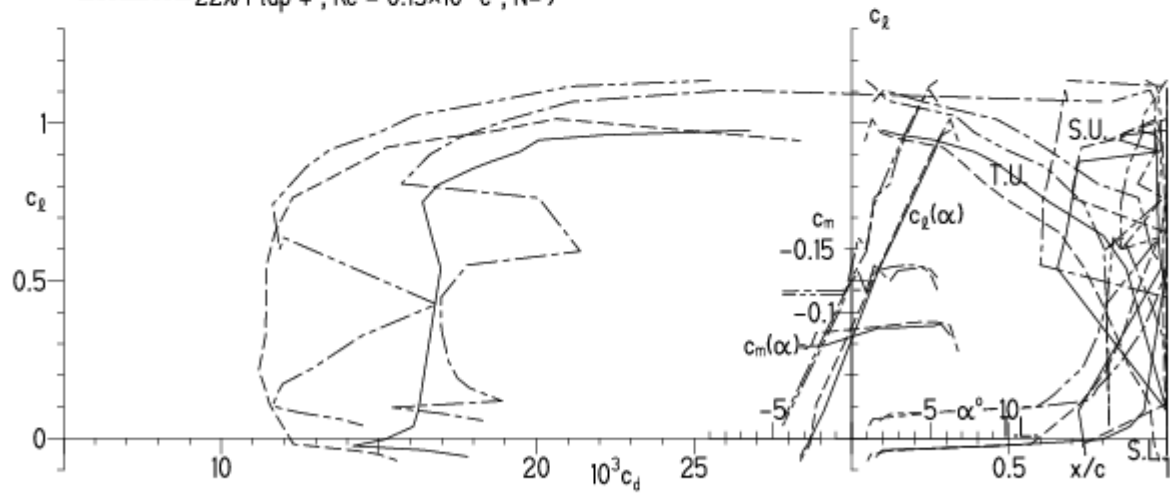


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

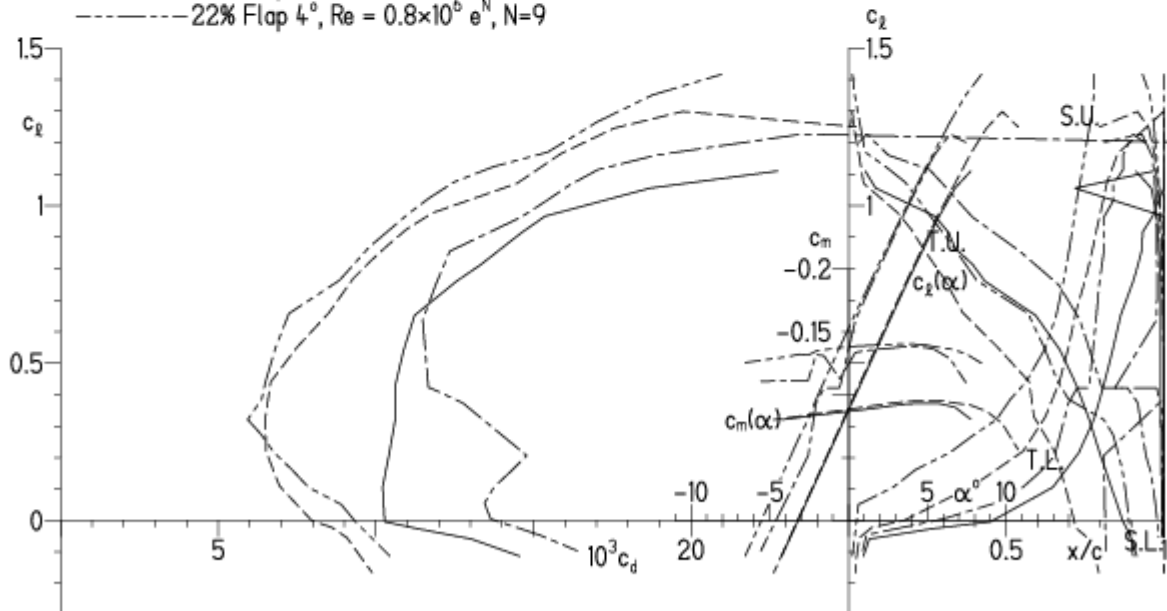


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

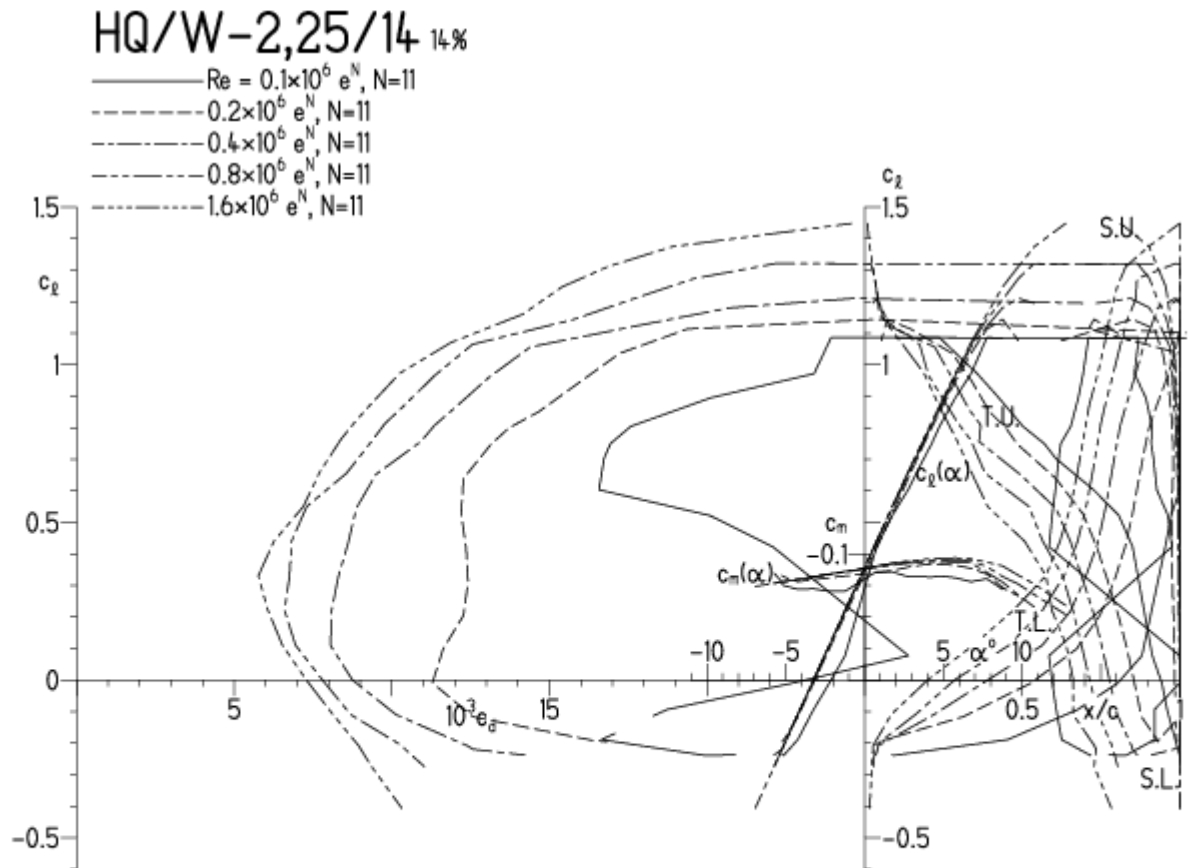


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

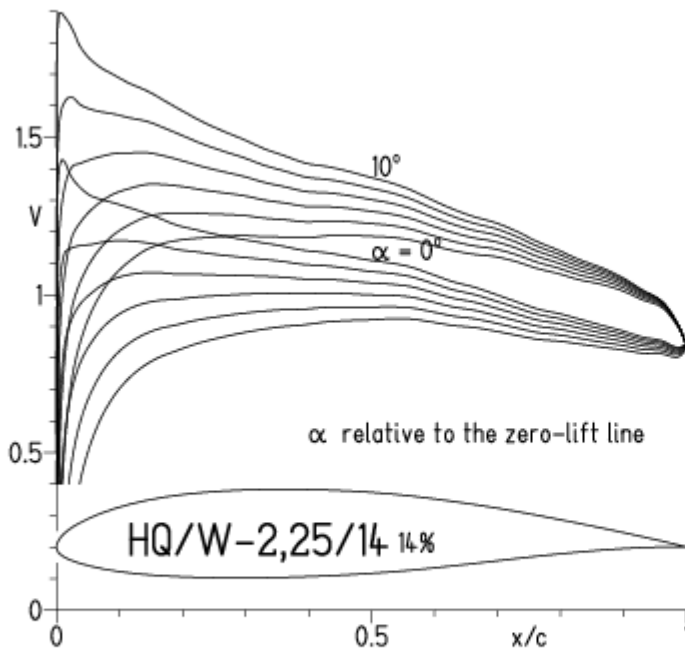


EPPLER 2005 V. 8.

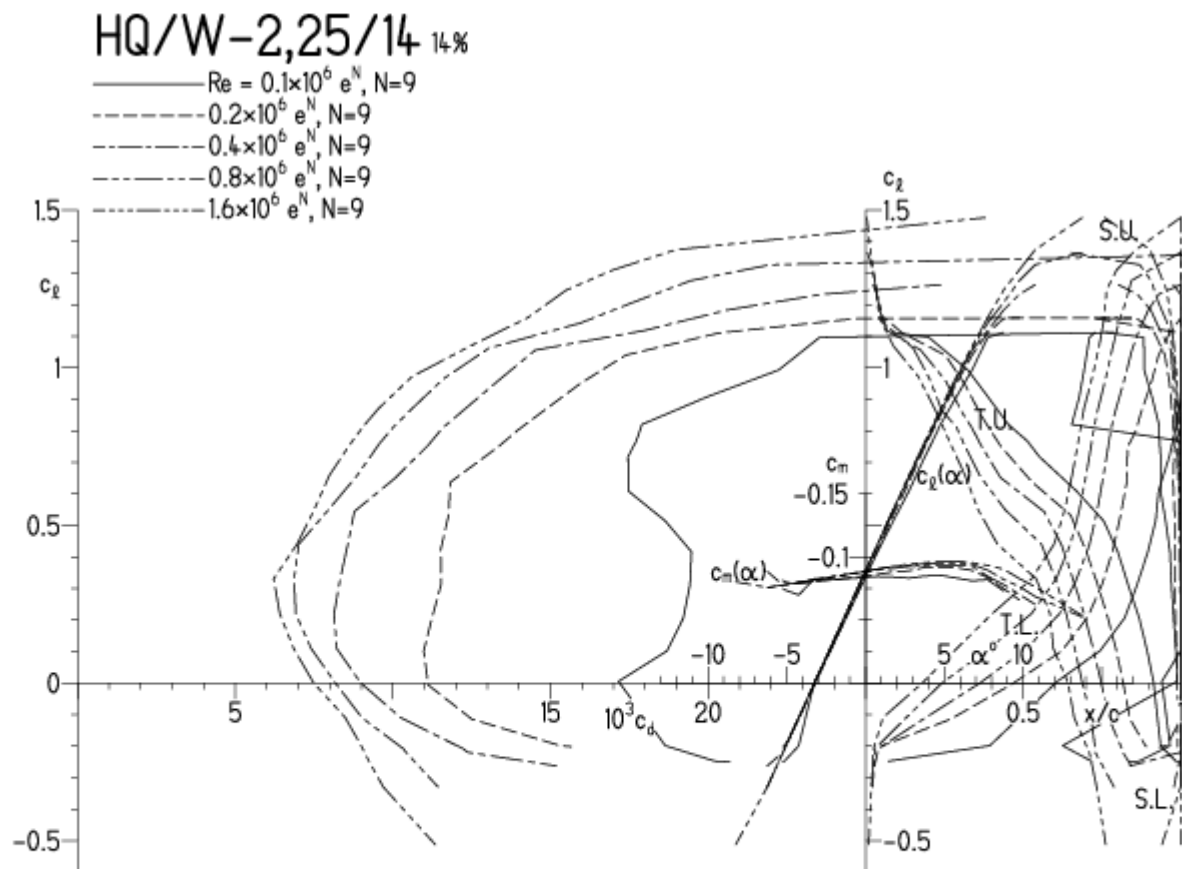


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

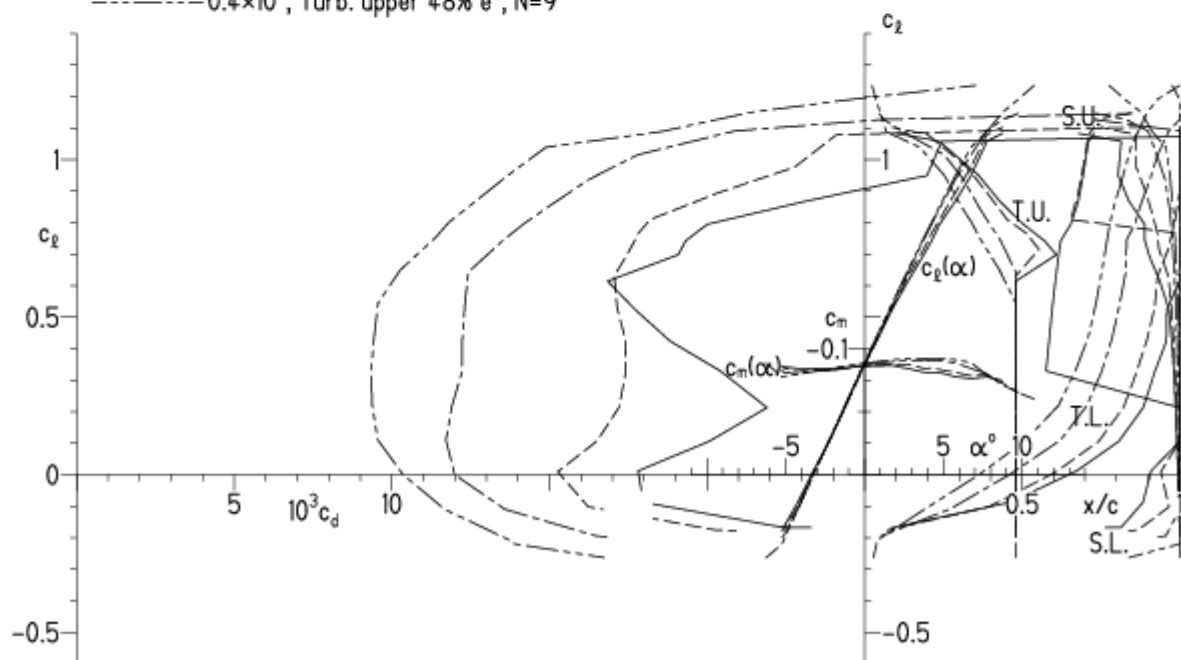
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

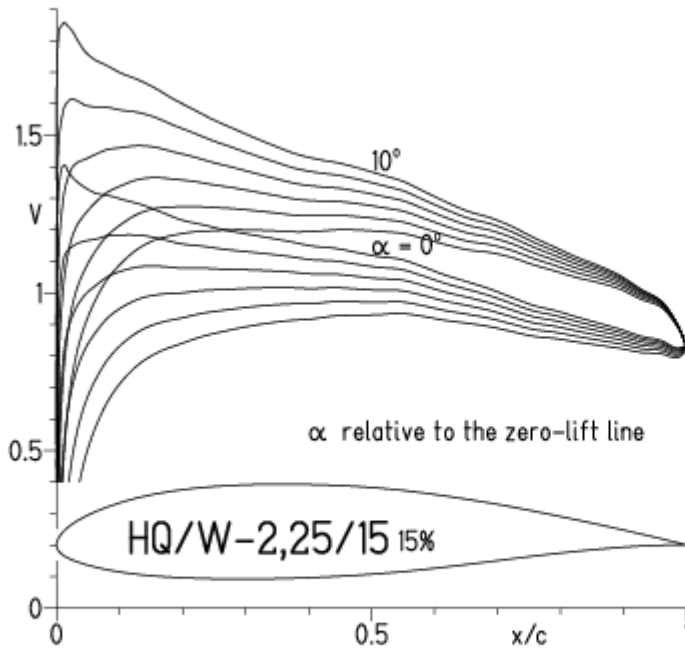


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

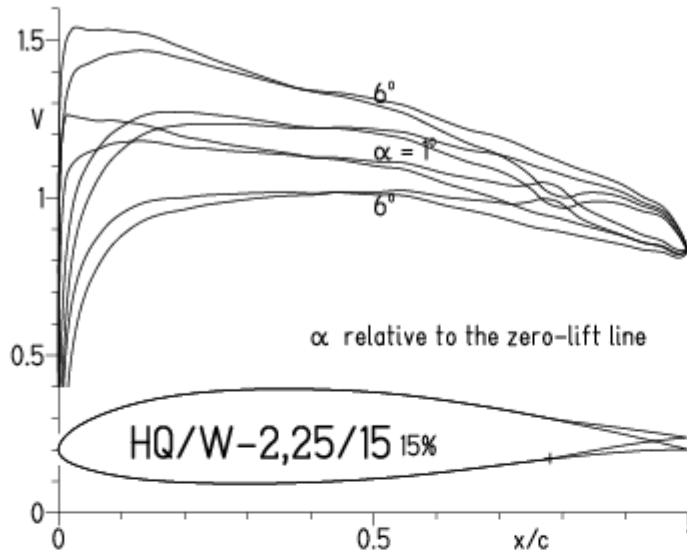


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

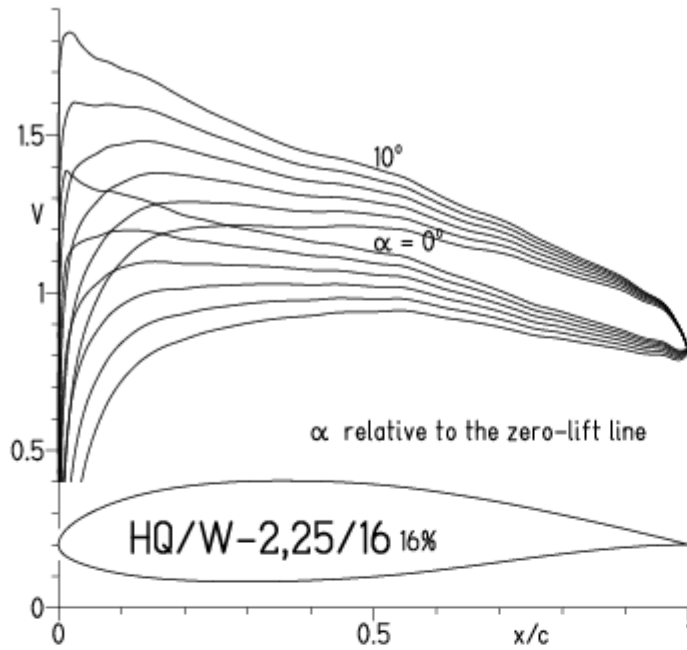
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



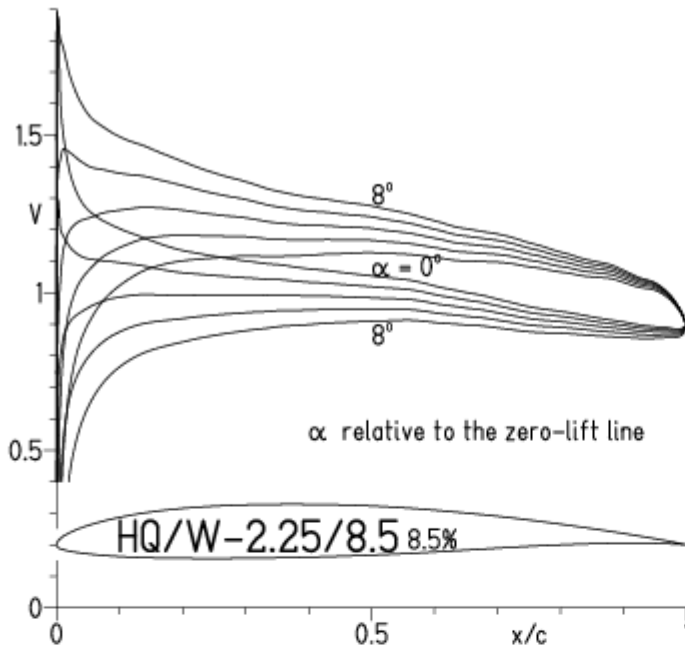
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

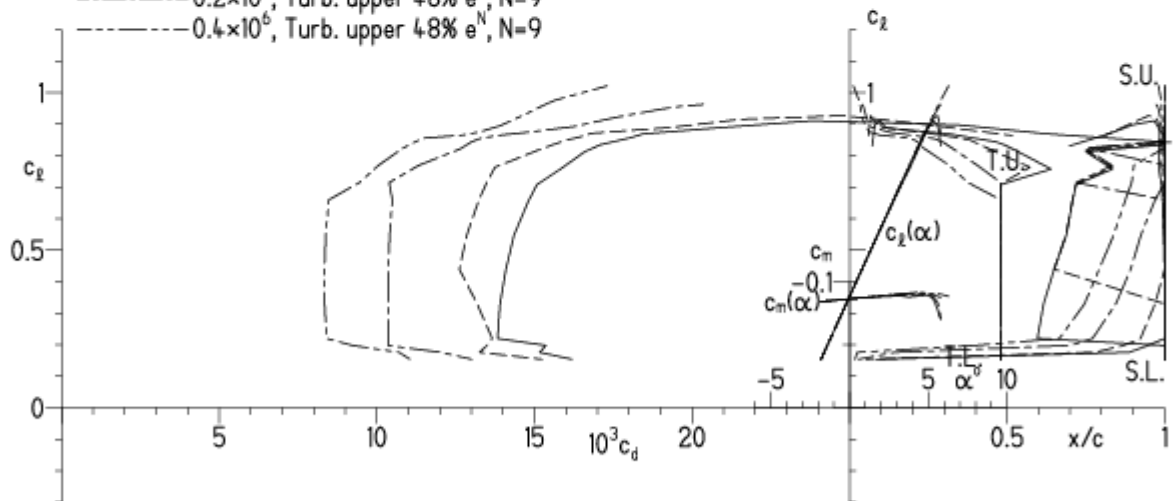
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

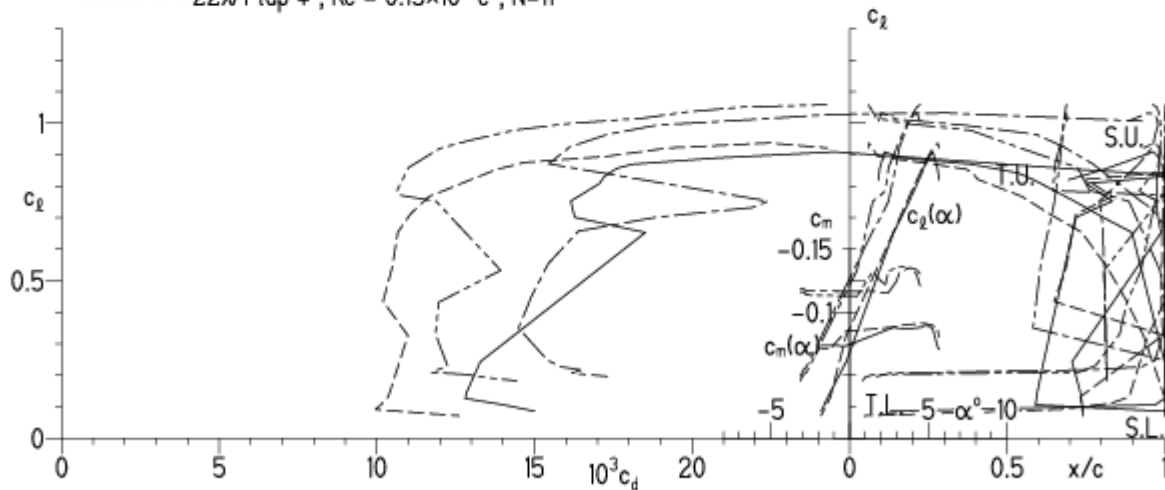


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

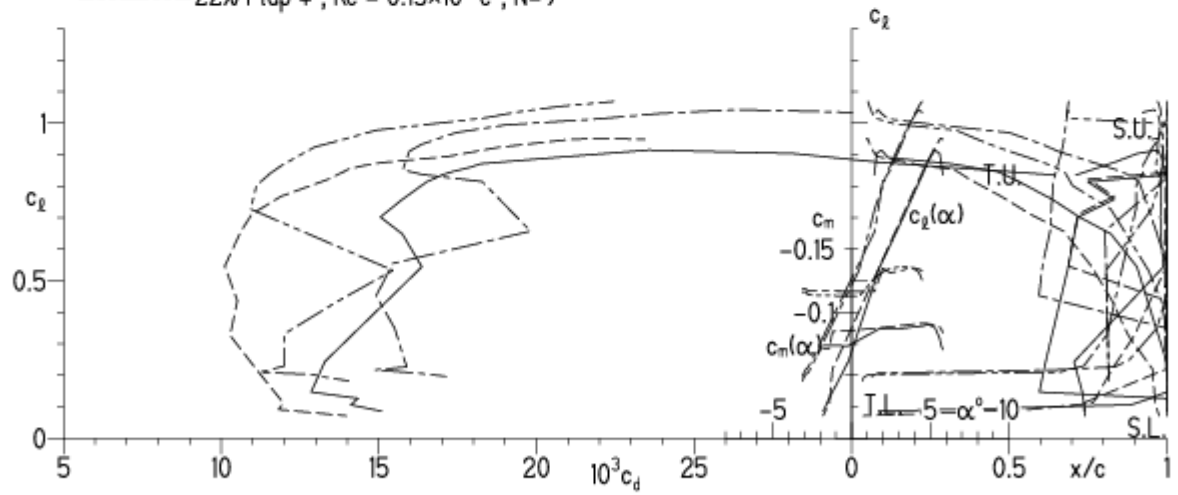


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

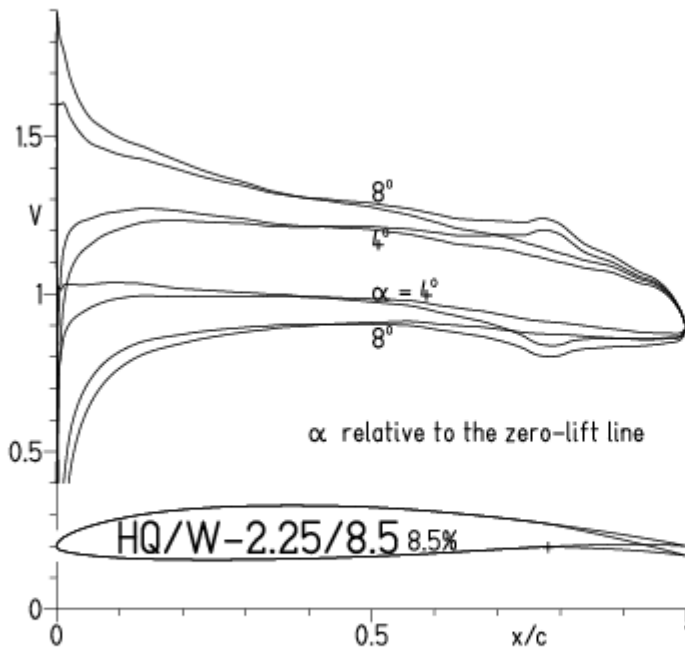
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

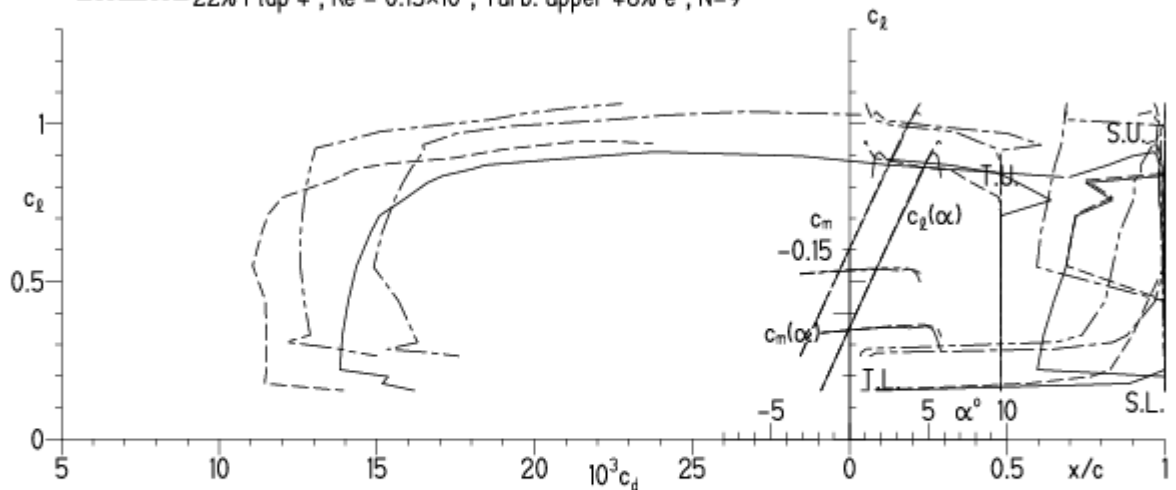


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

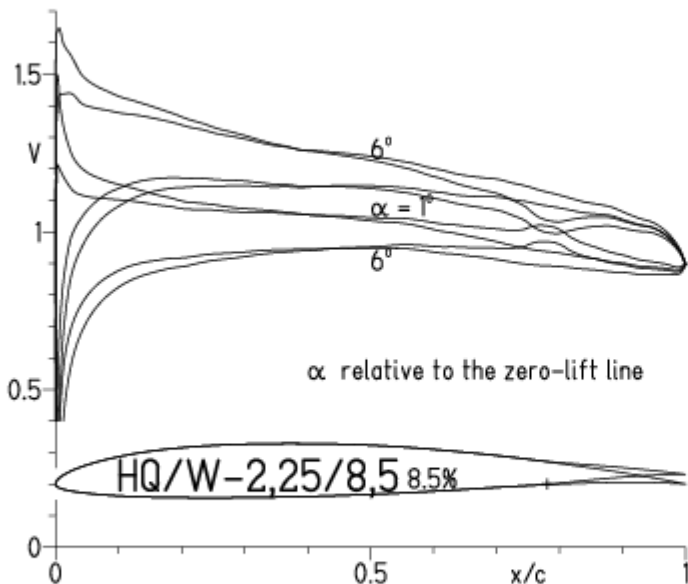
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

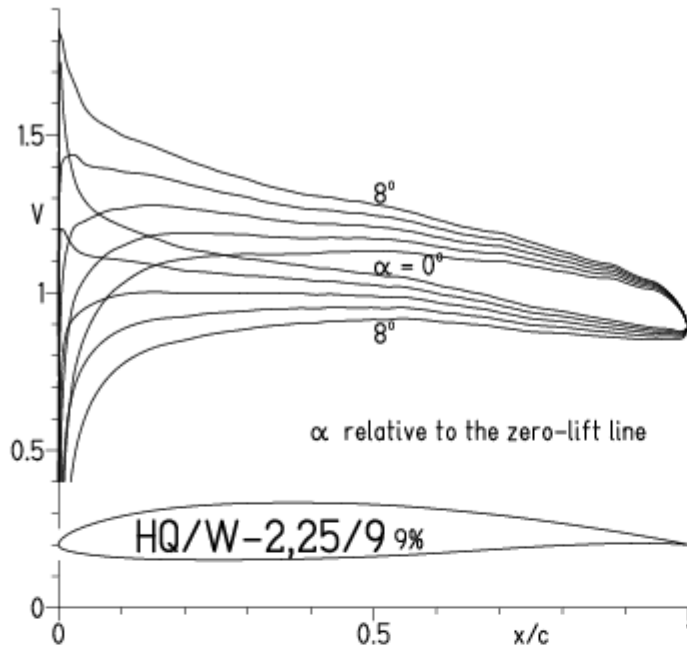


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

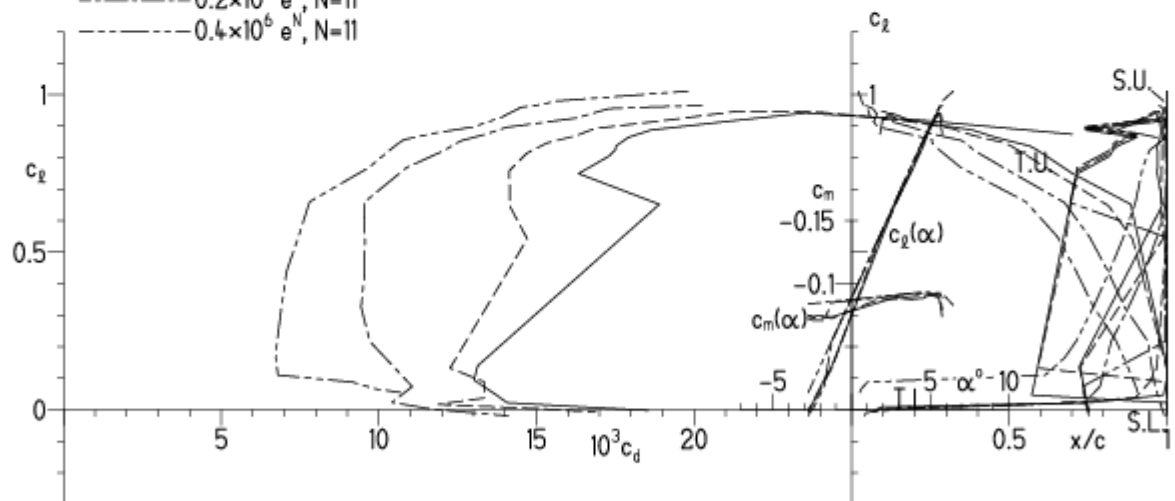
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

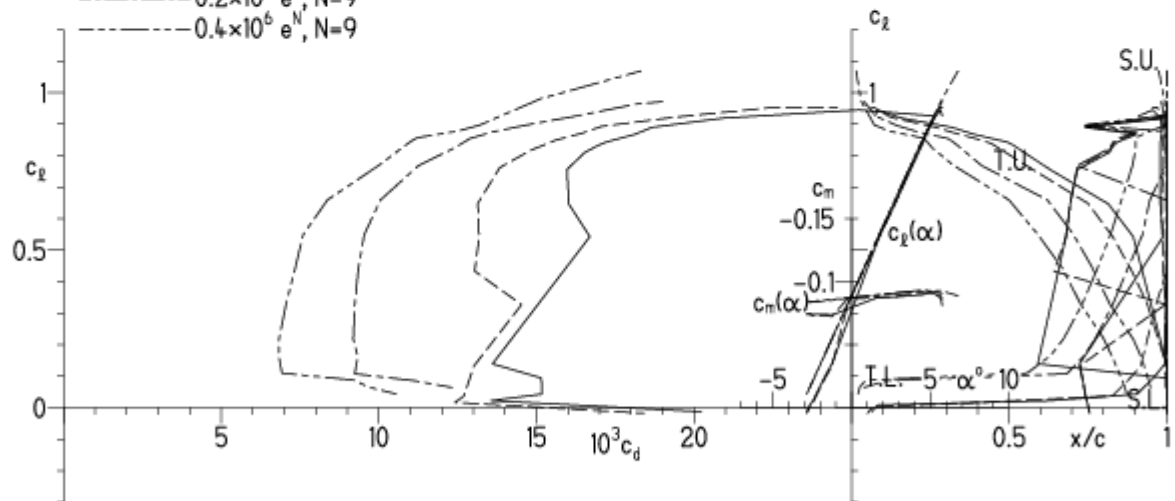
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

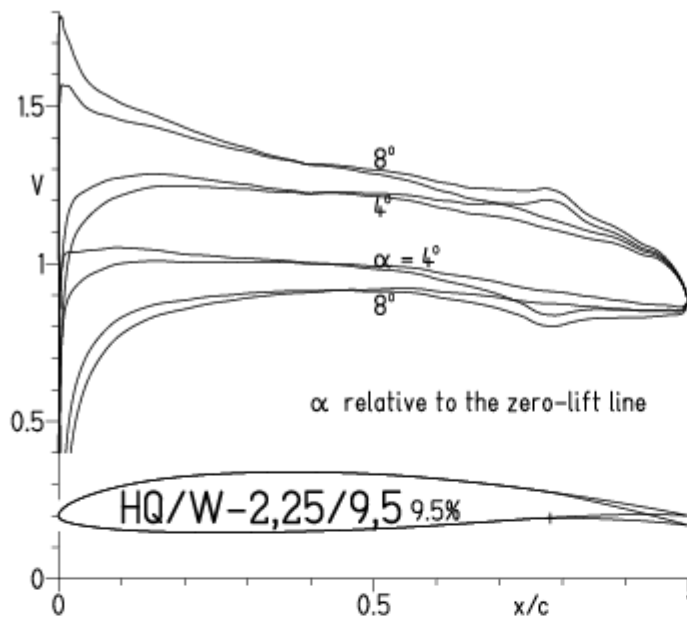
- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

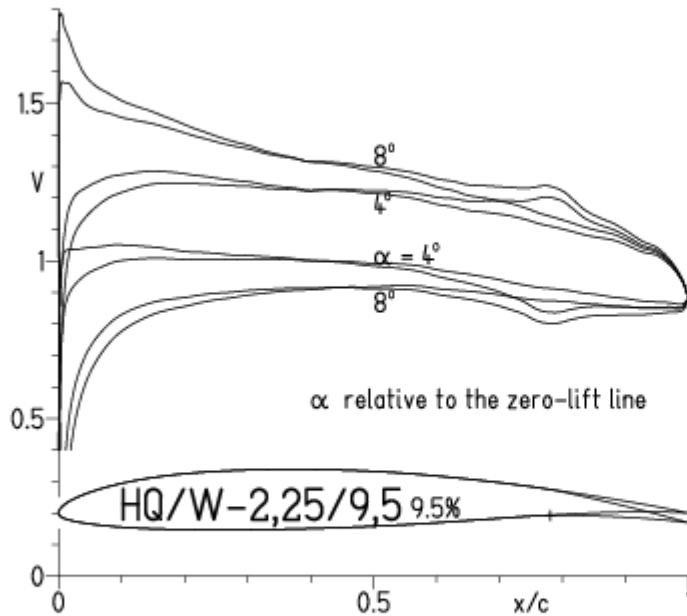
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

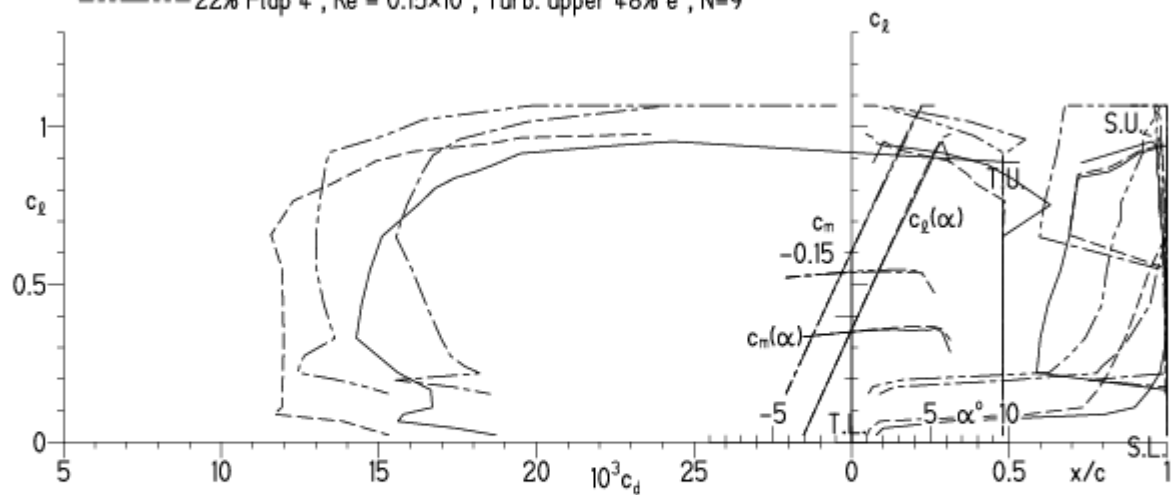


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

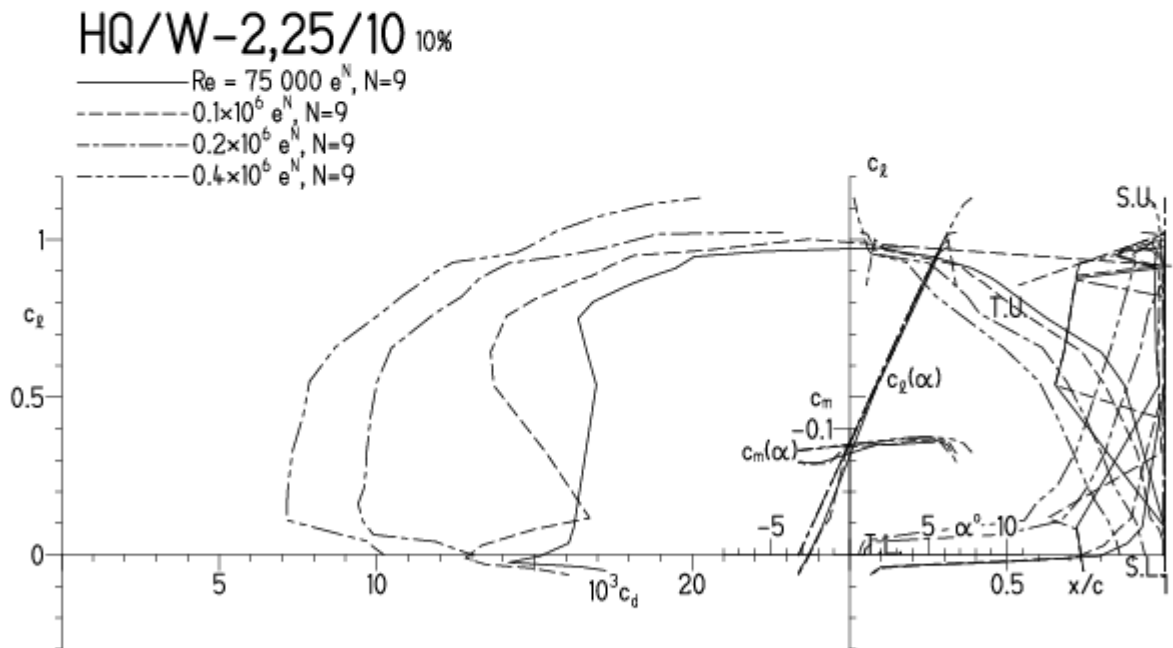


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

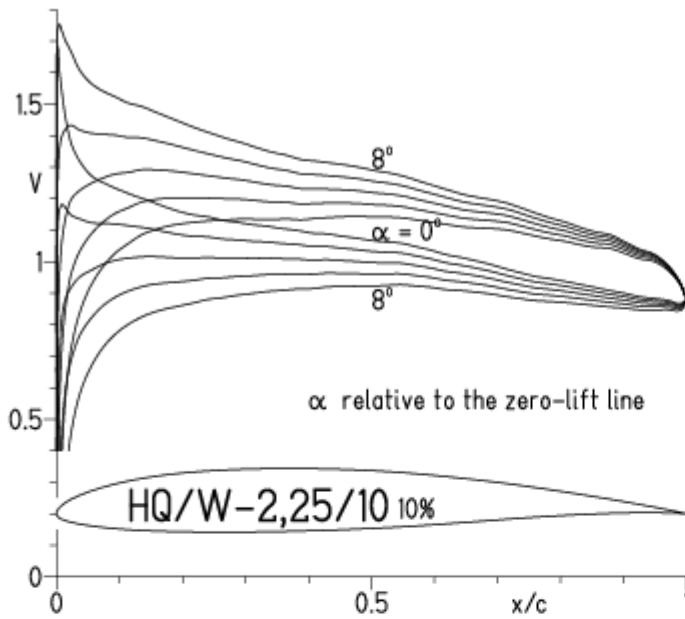


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

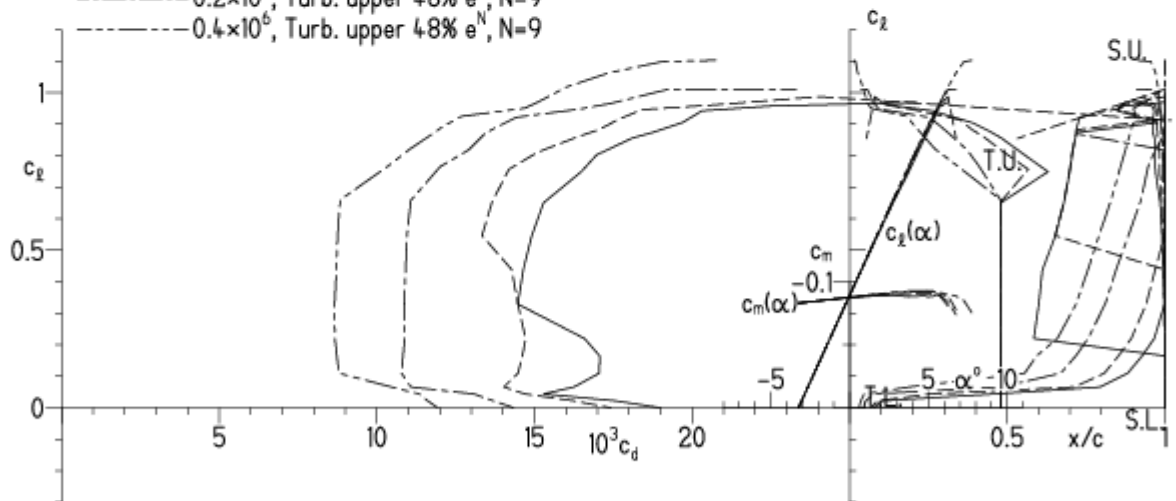
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

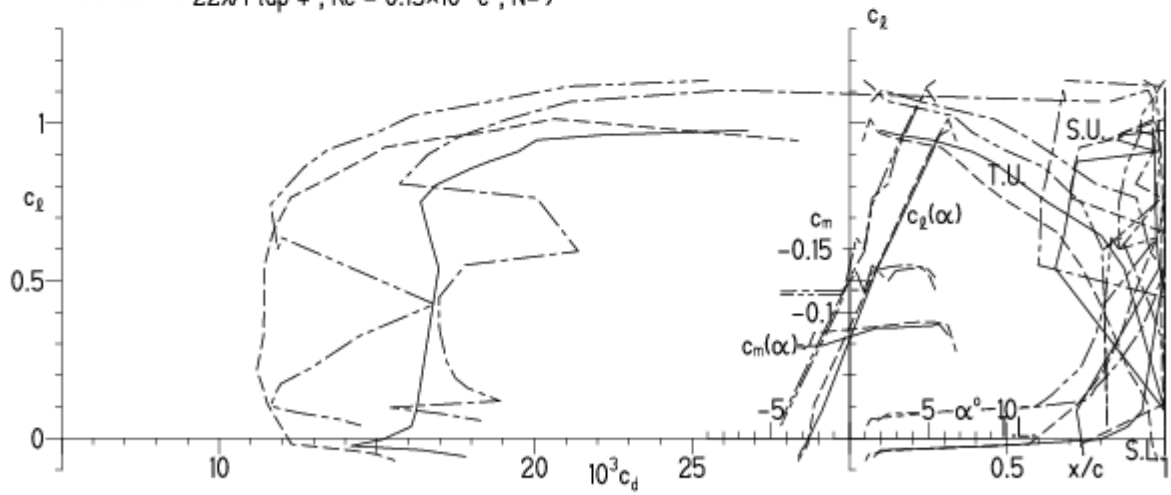


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

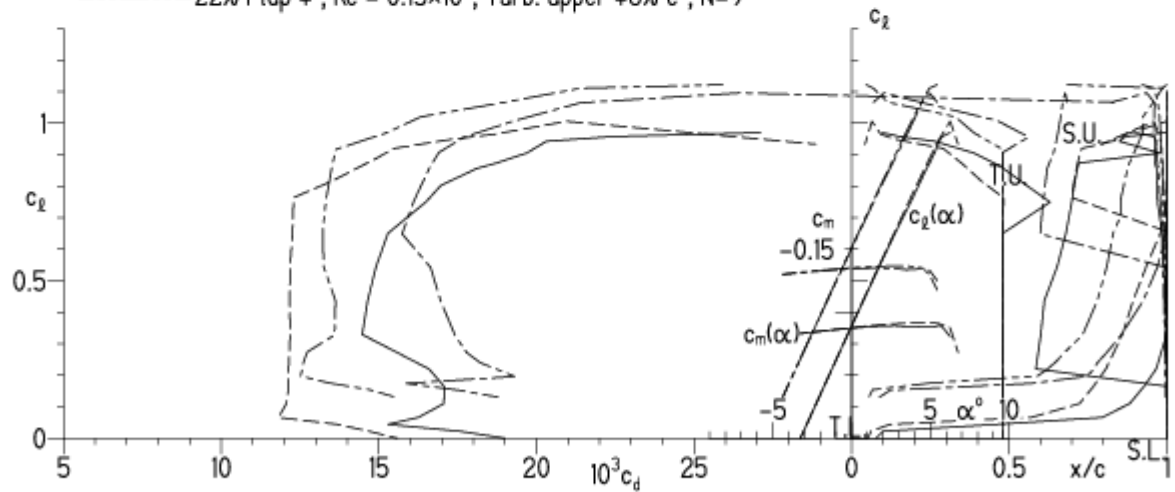


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

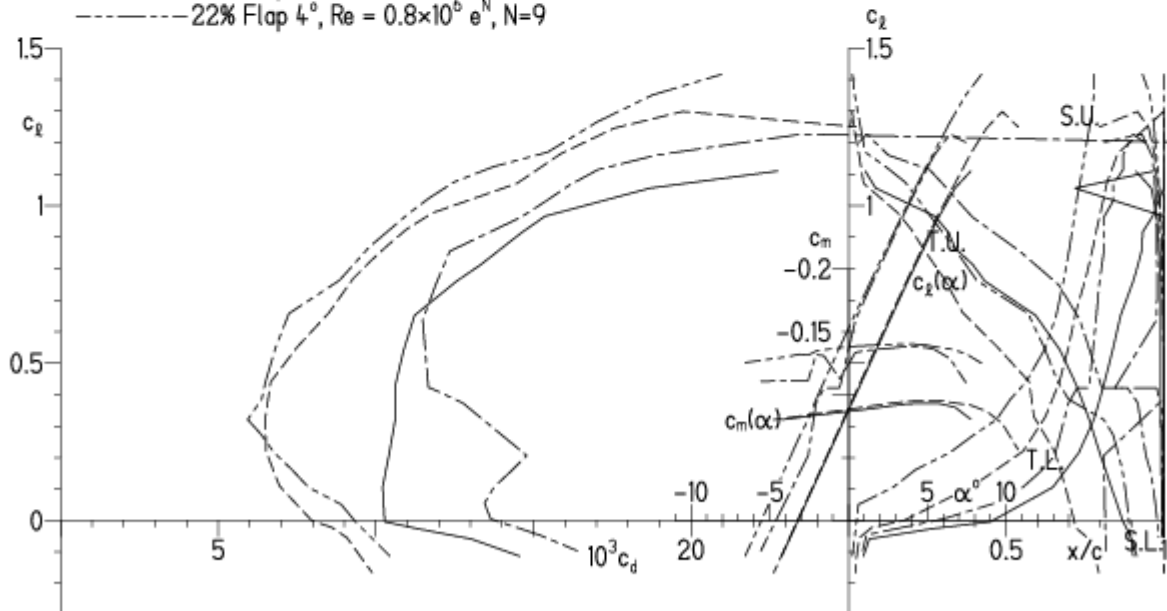


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11

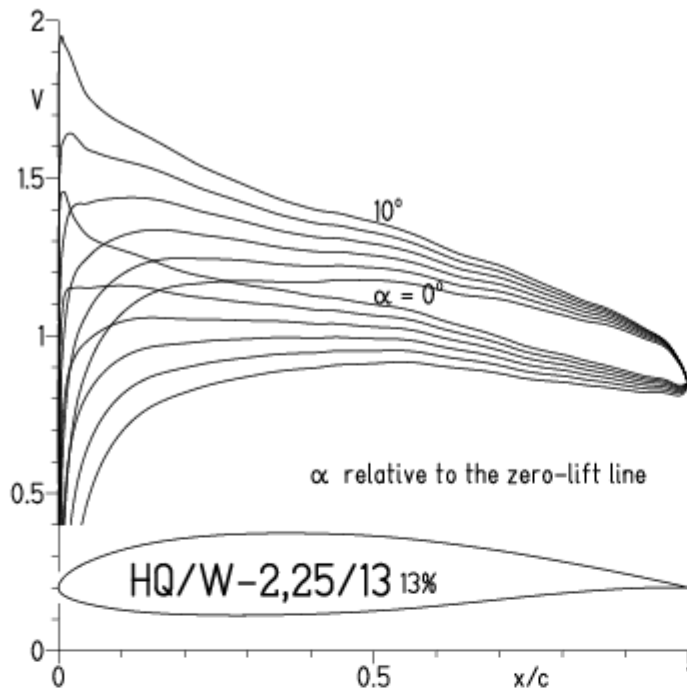


EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

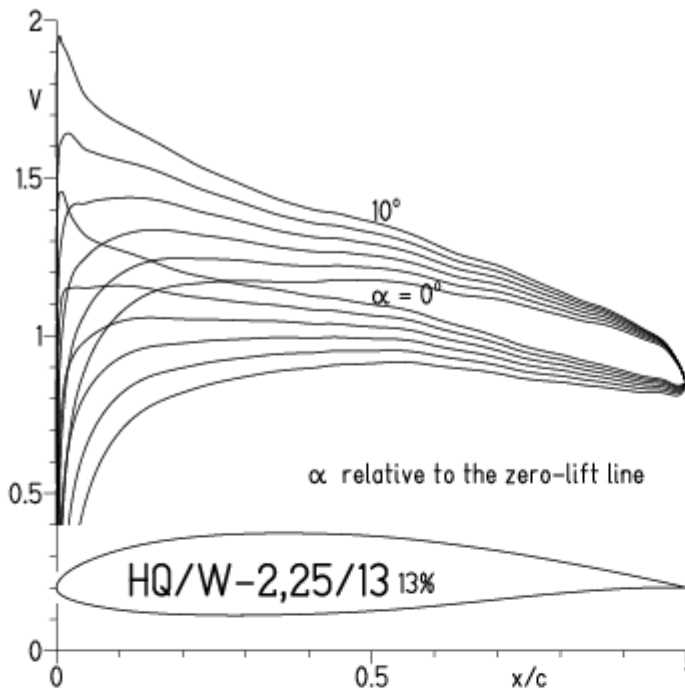
HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

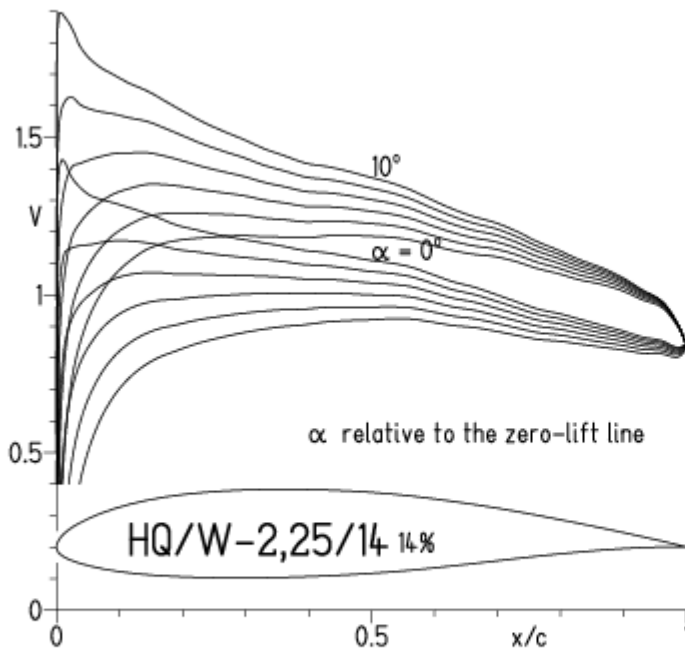


EPPLER 2005 V. 8.

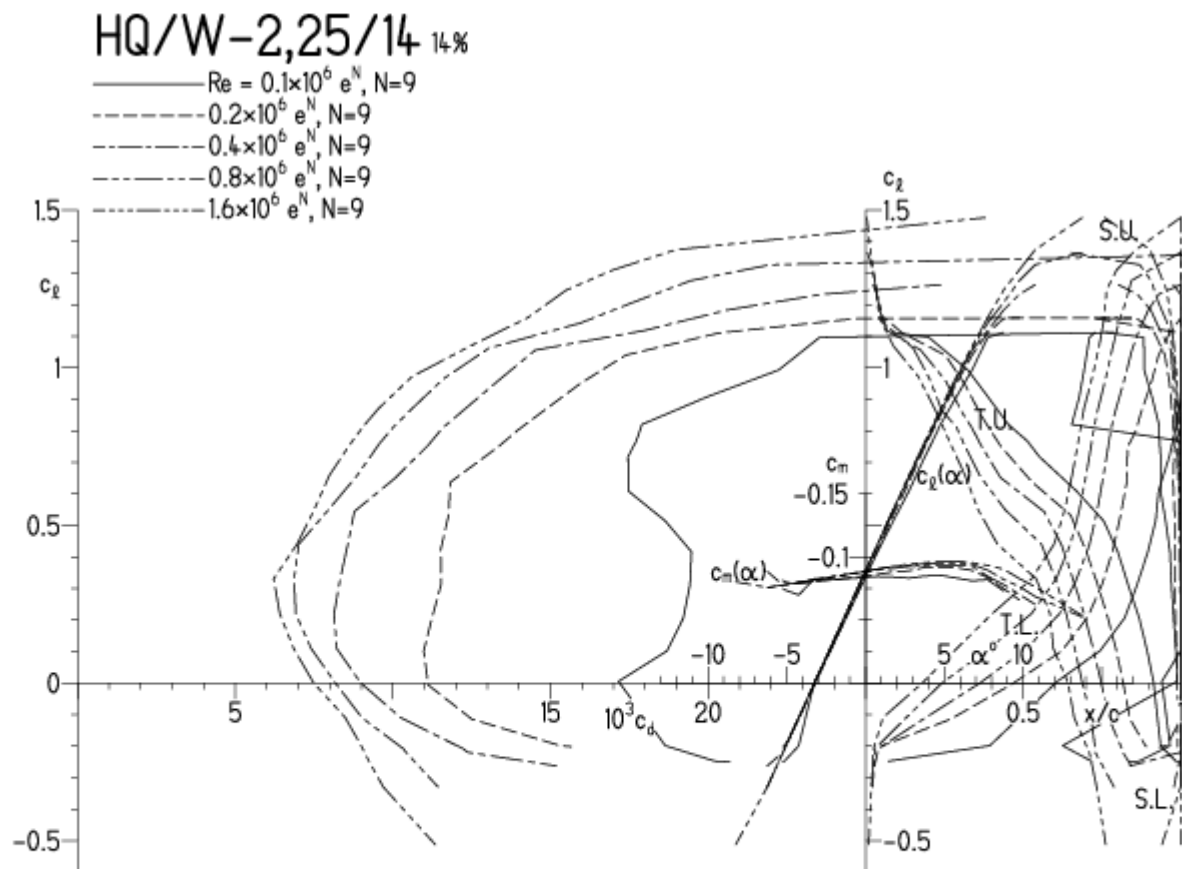


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

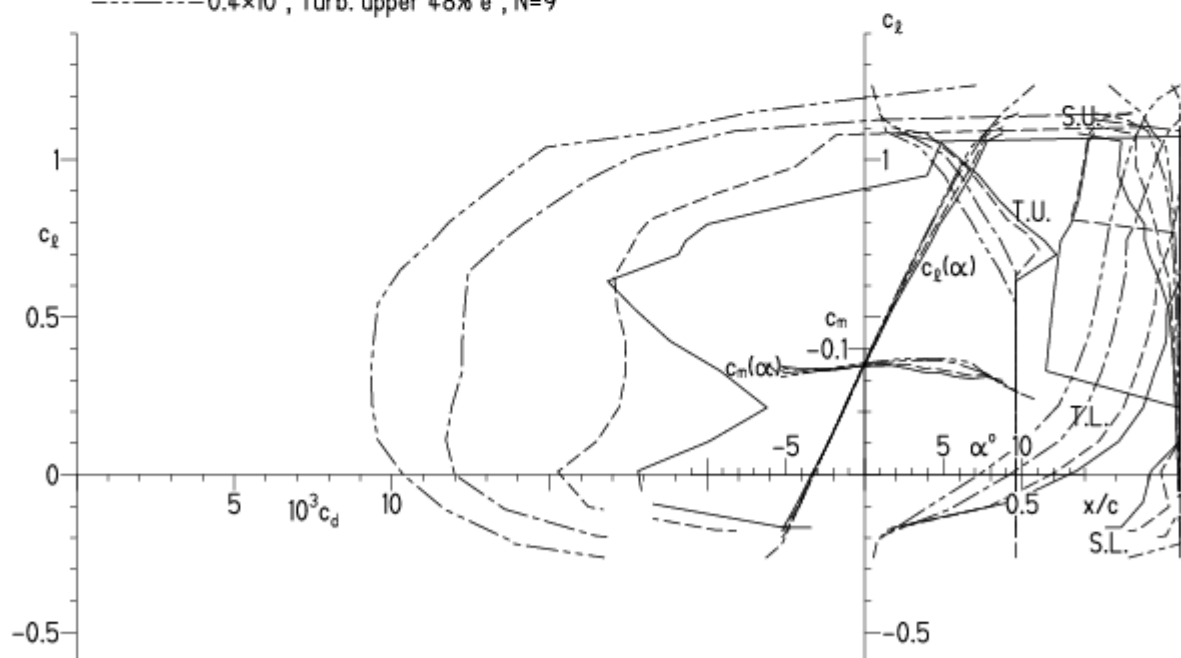
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

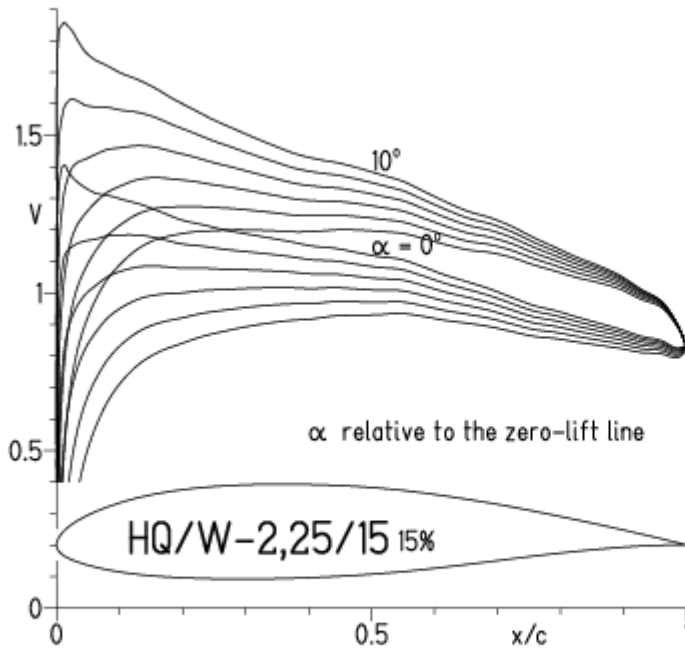


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

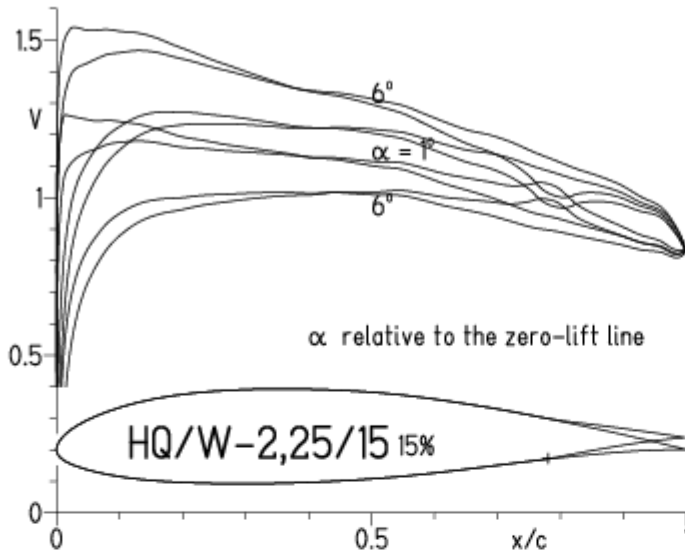


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

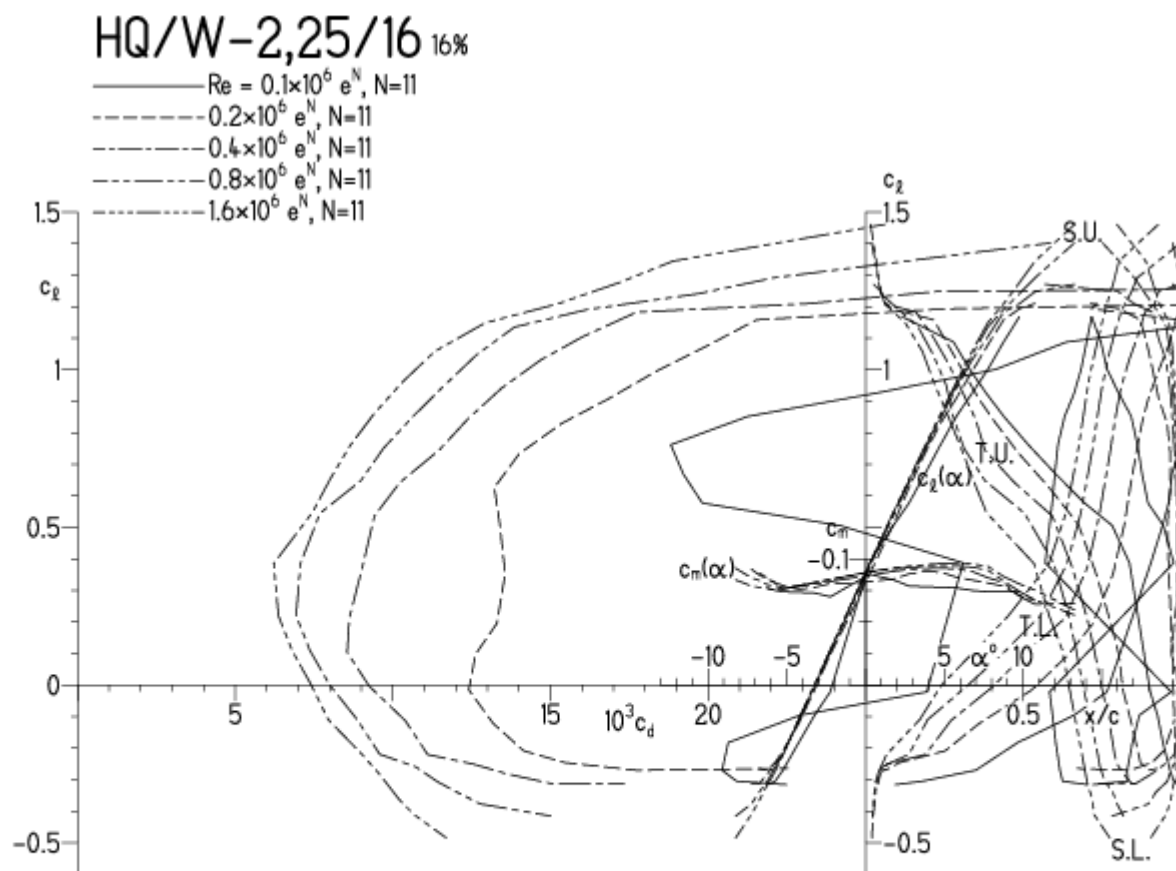


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

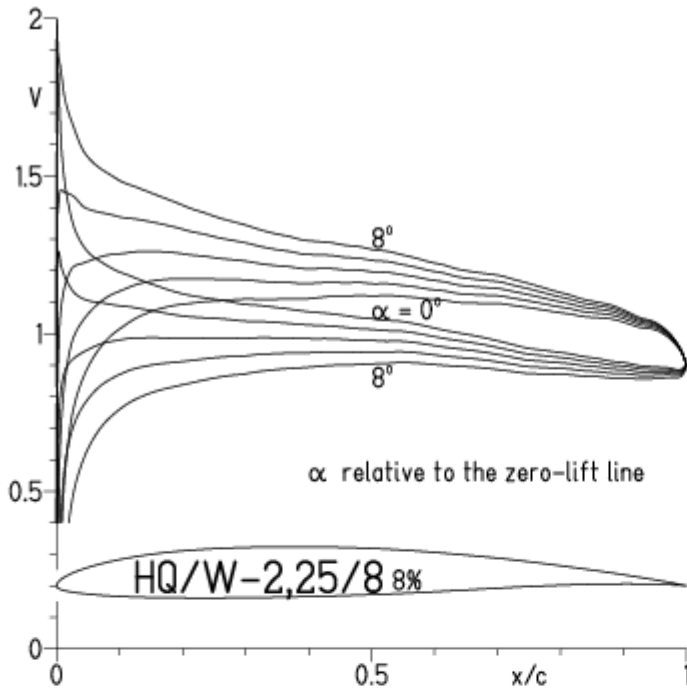
HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. $30 - 35 \text{ m/s}$ Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



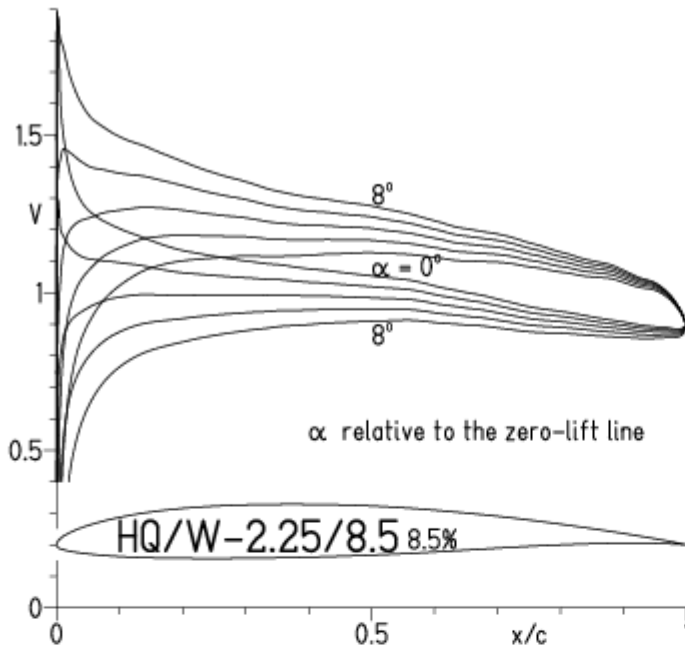
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

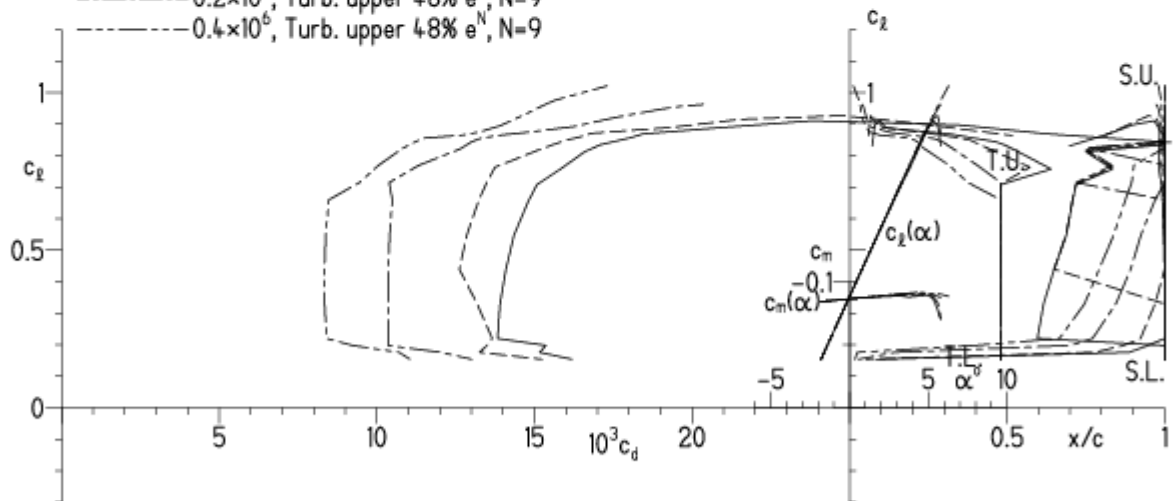
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

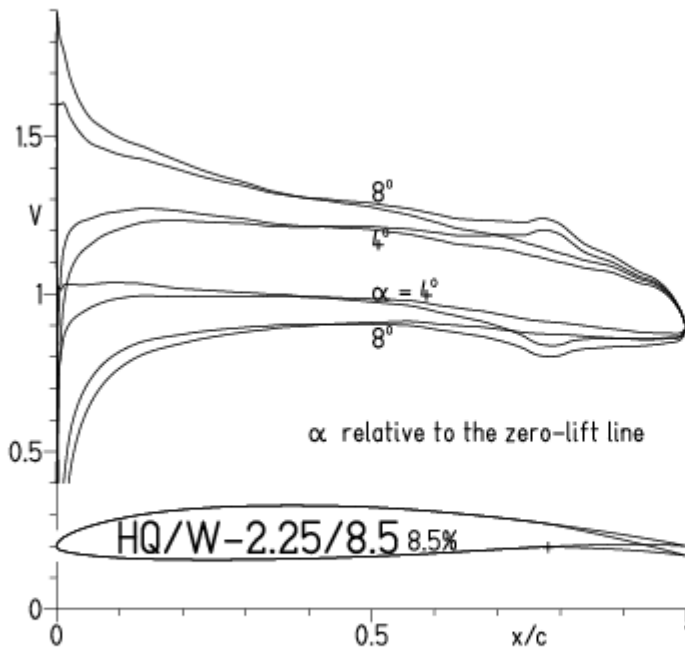
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

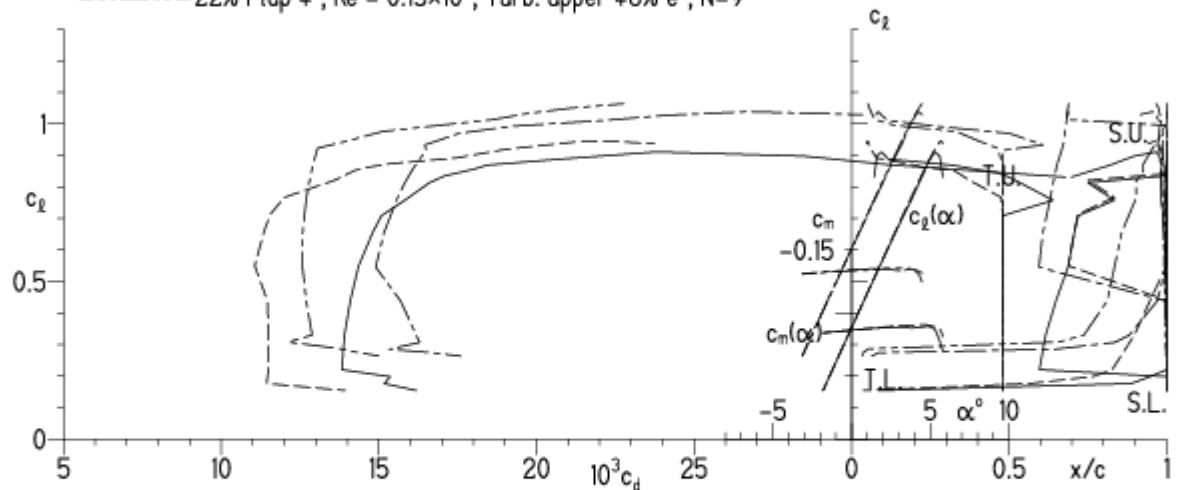


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

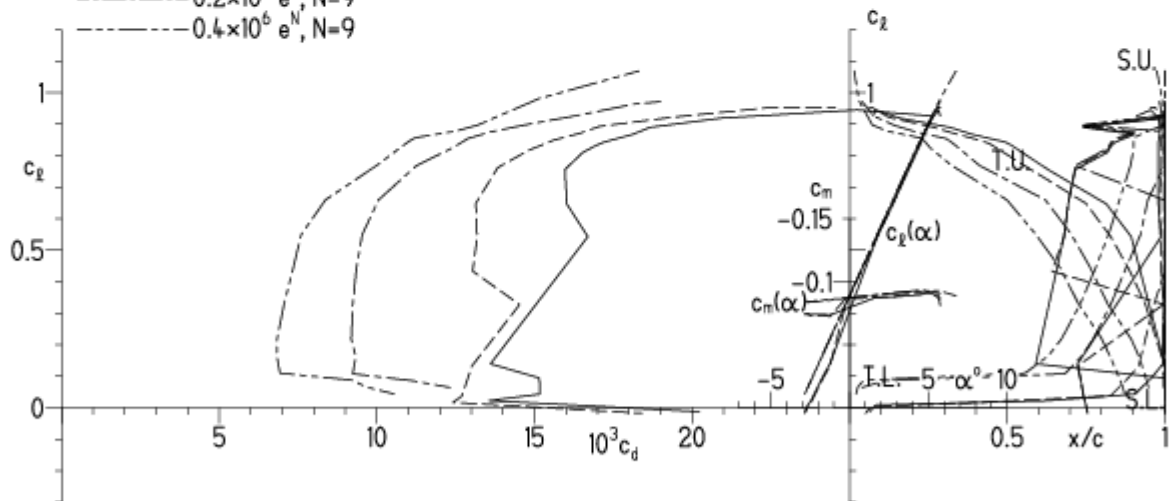
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

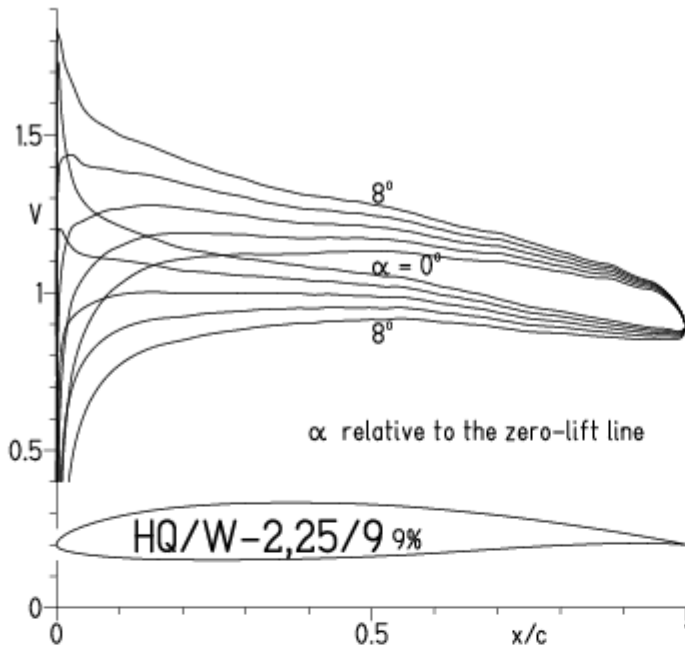
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

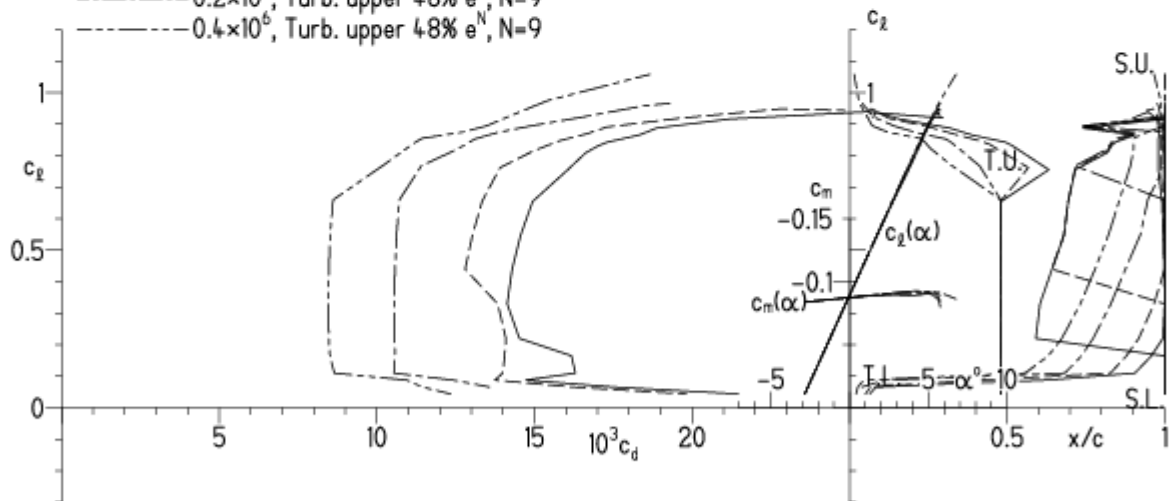
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

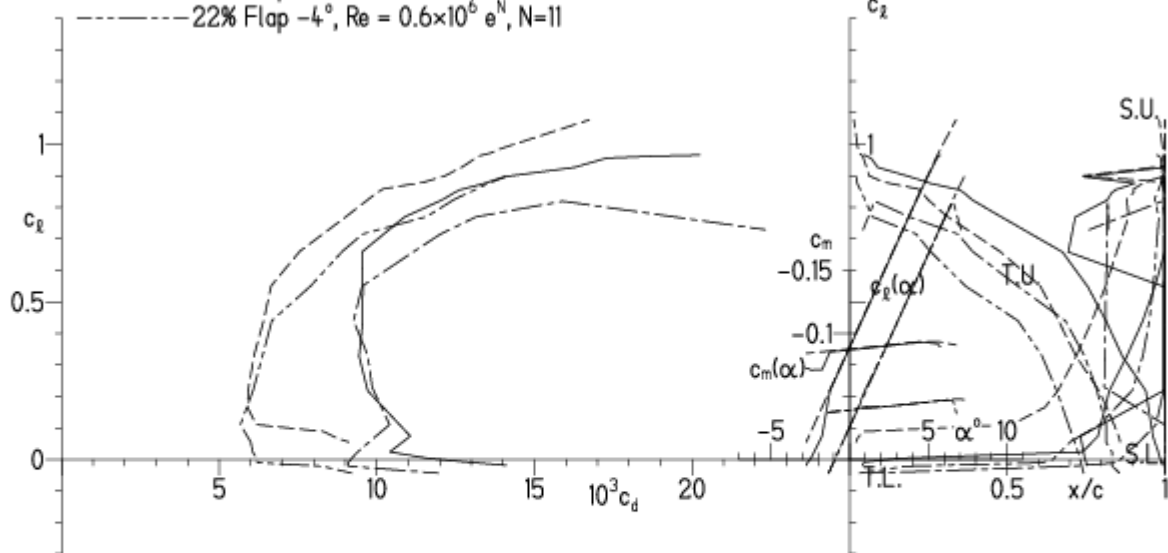
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

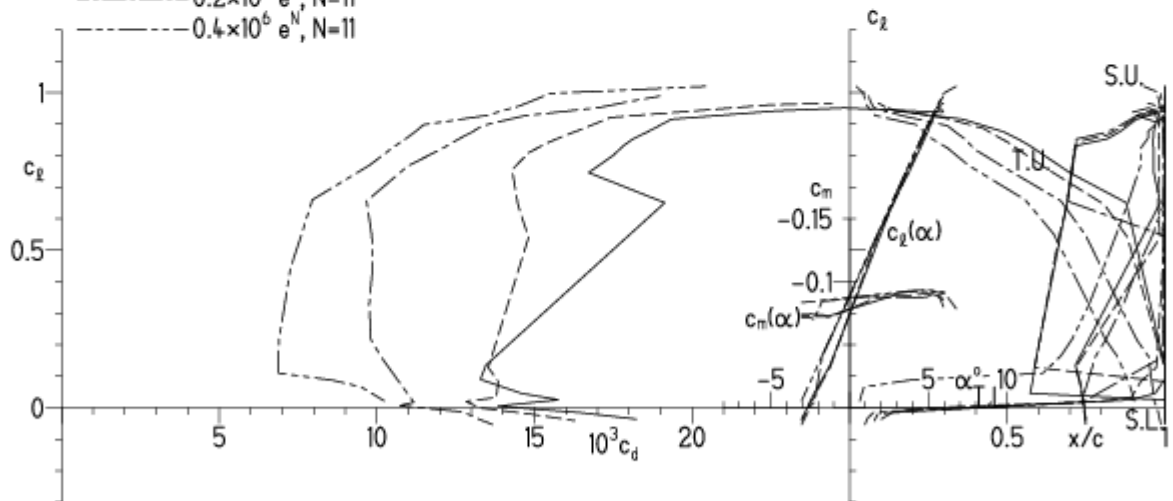
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

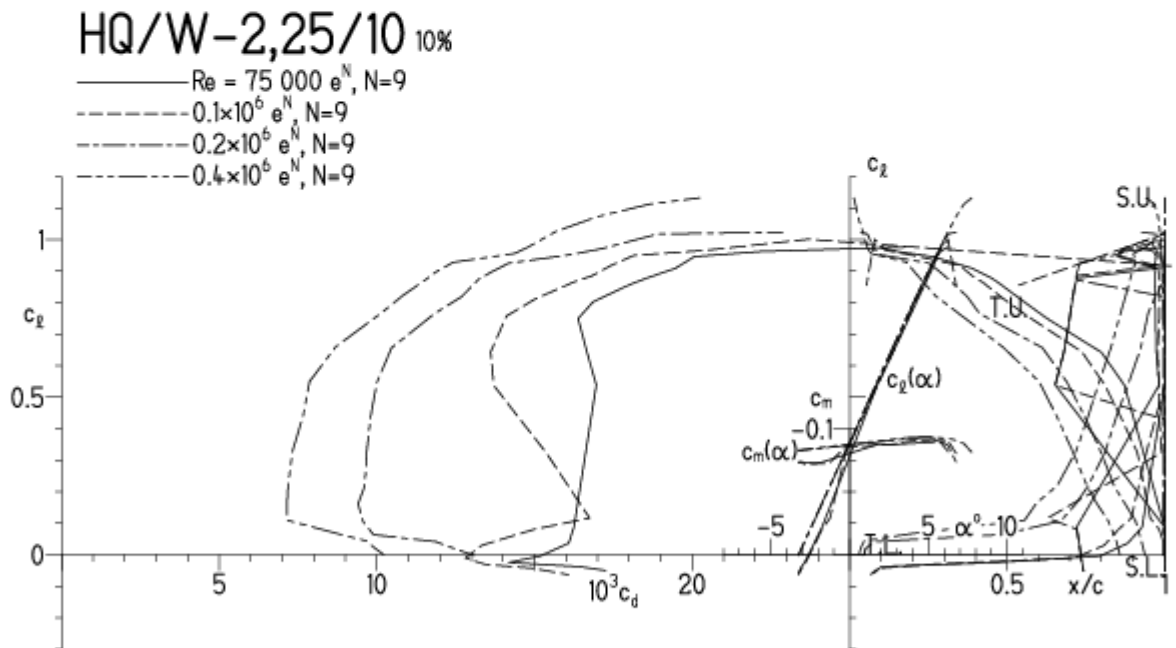


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

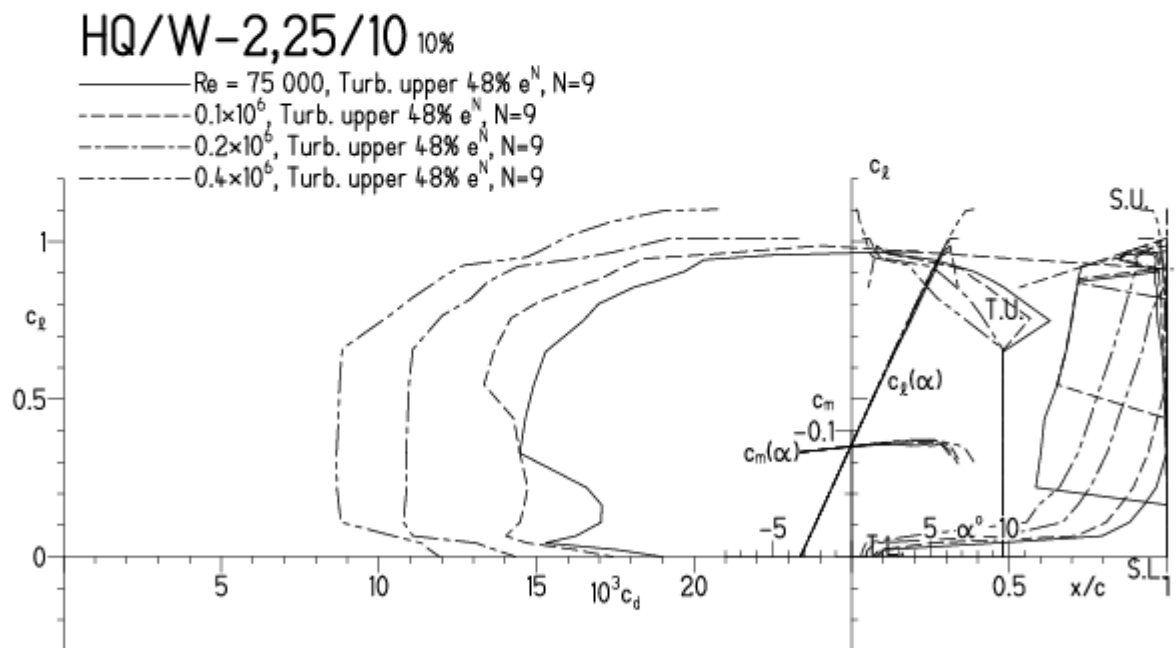


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

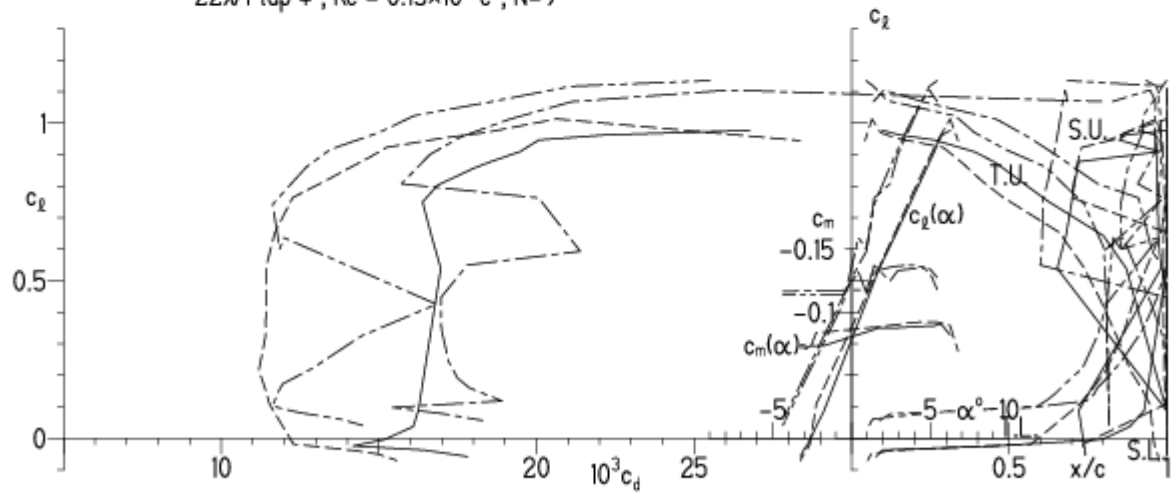


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

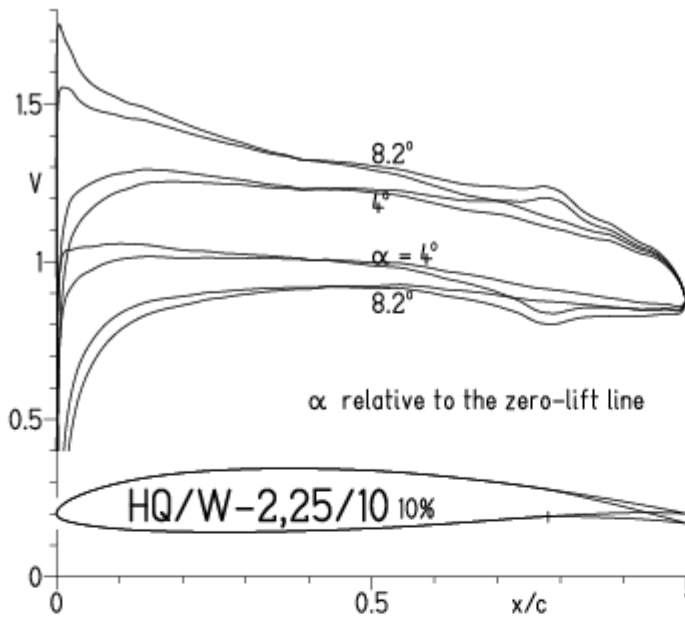
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

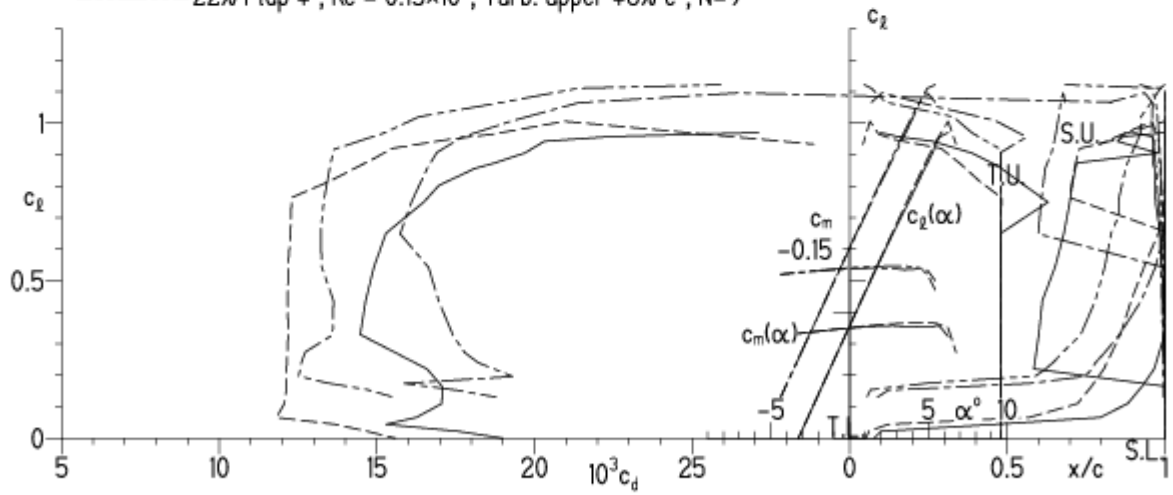


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

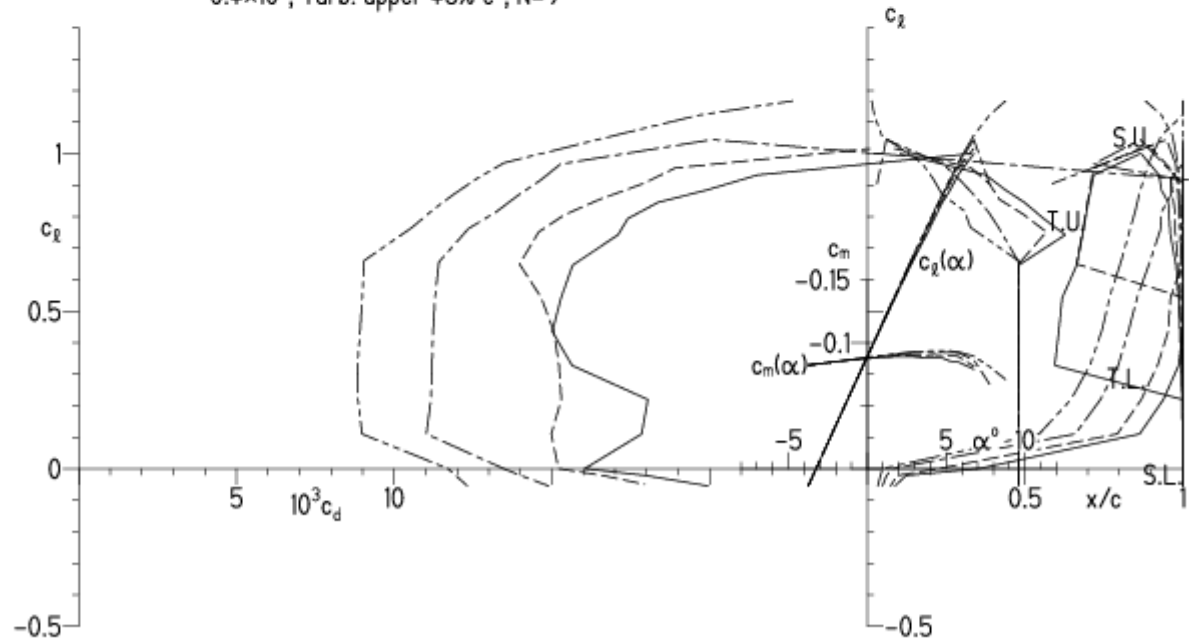
EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

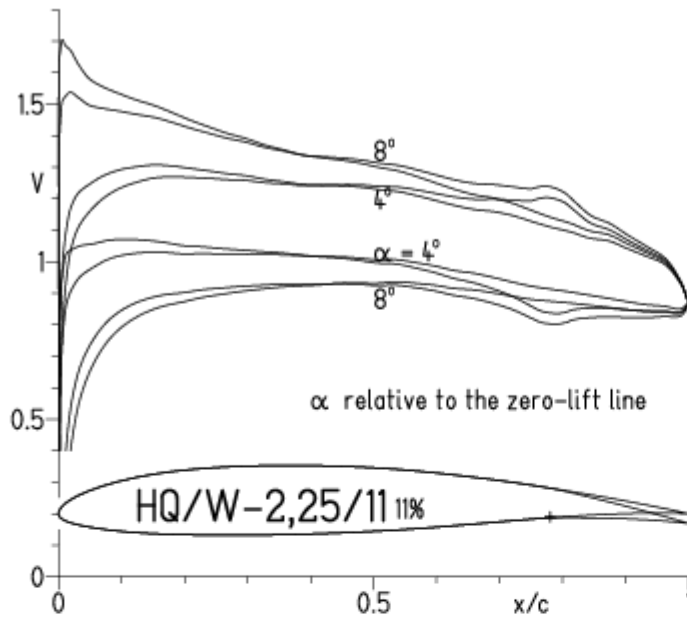
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

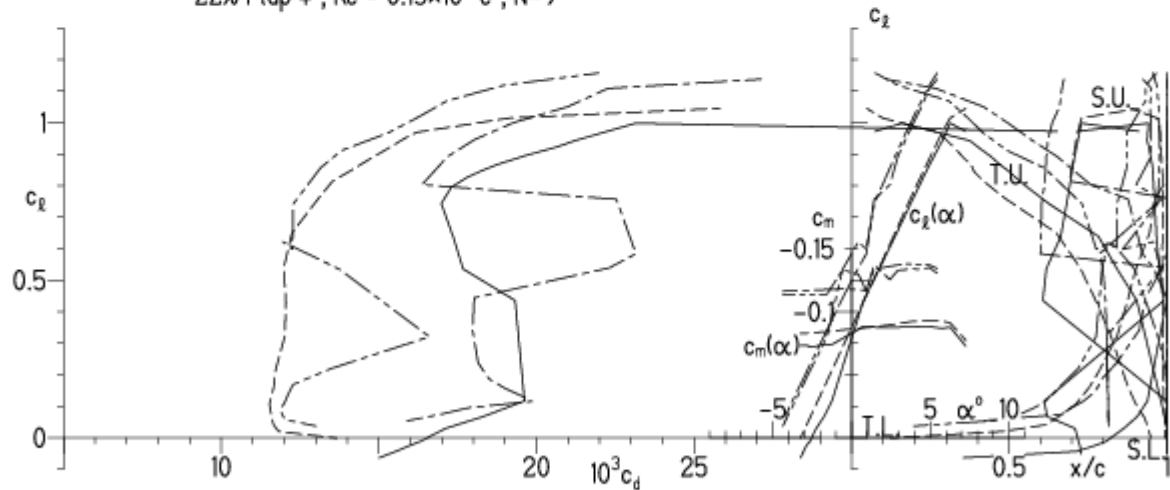


EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

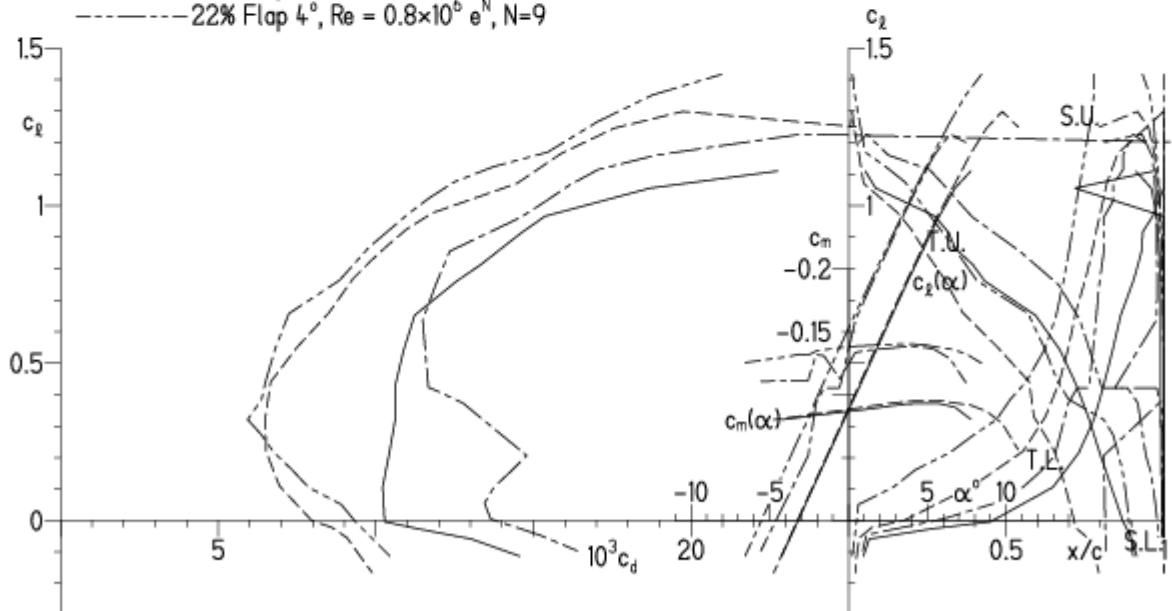


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

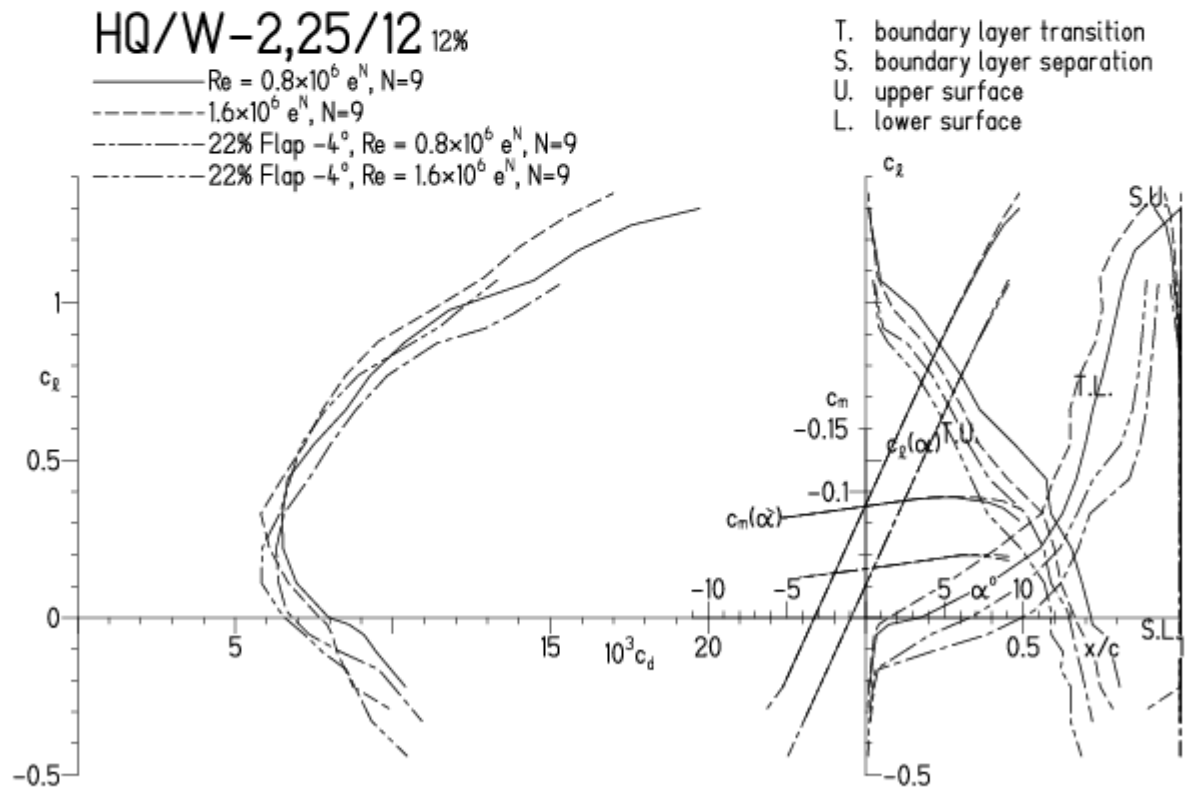


HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

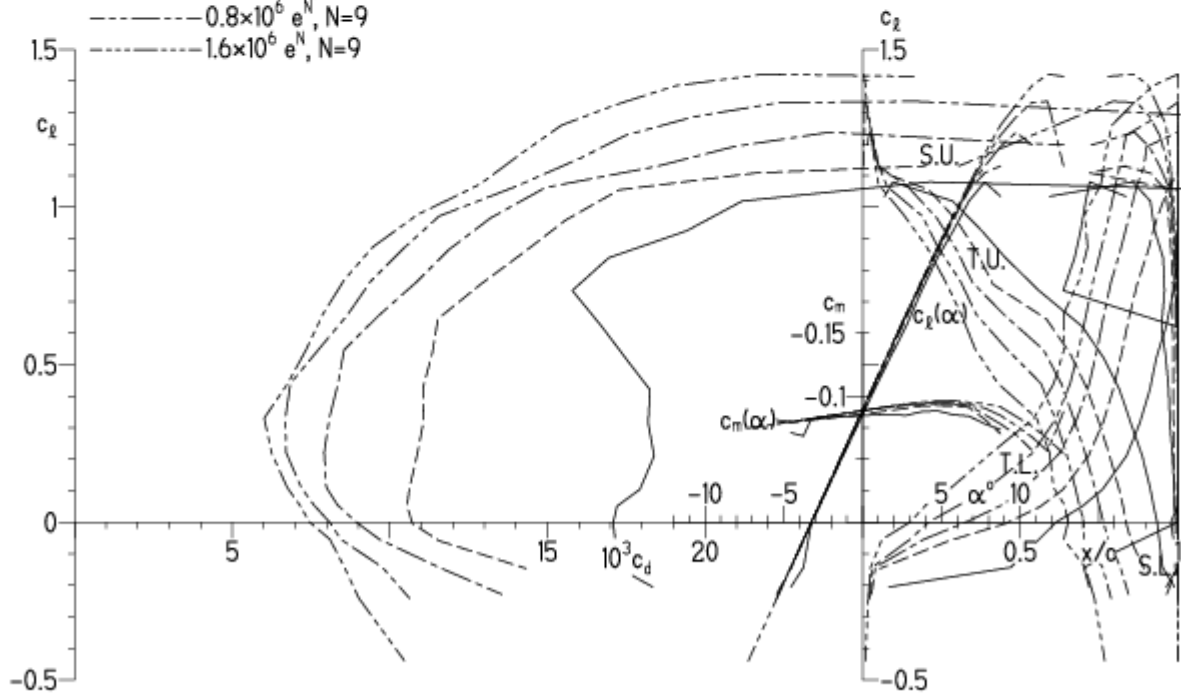
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

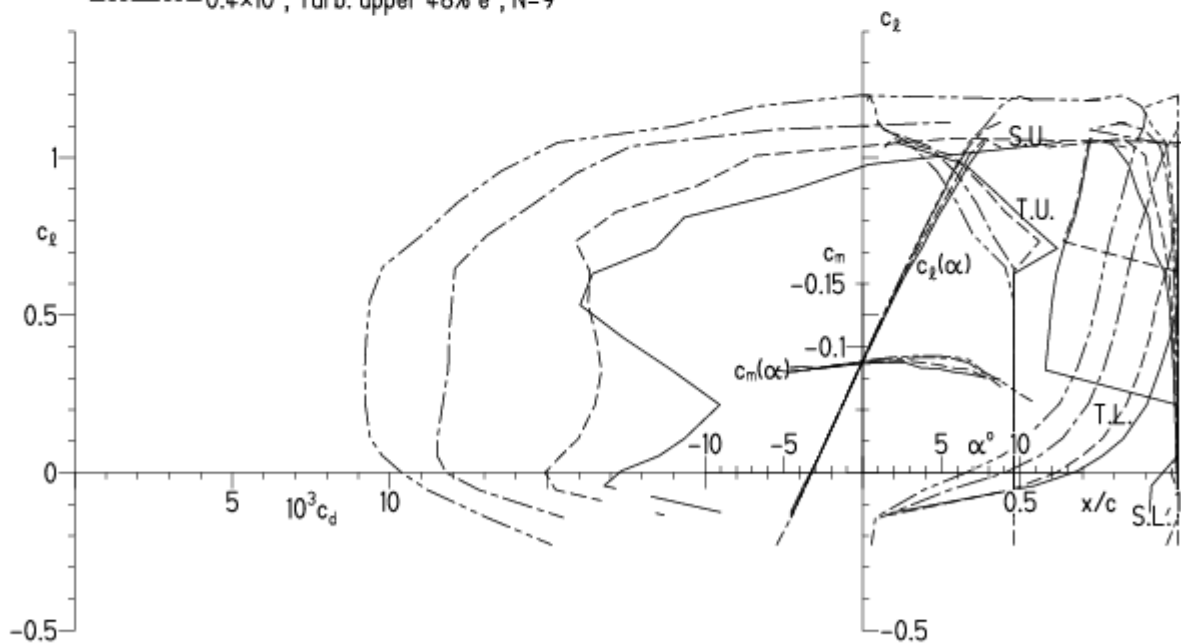
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

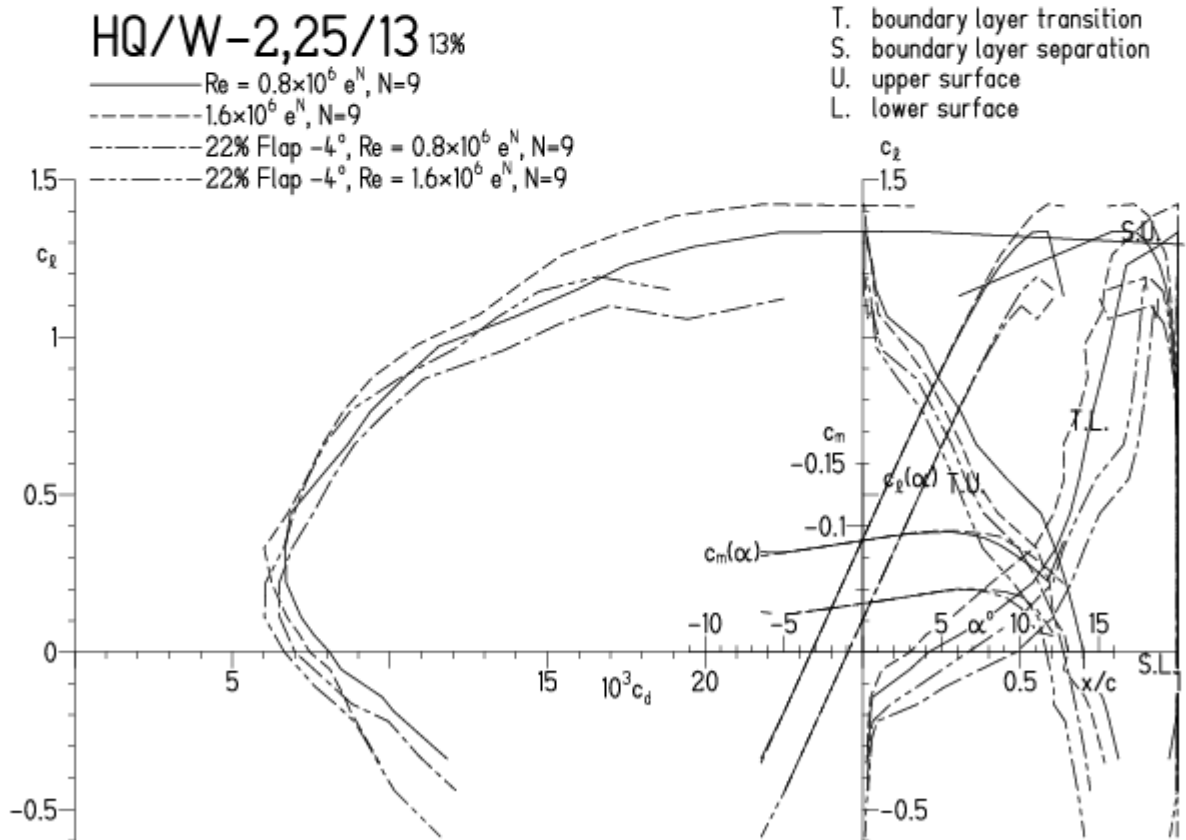


HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

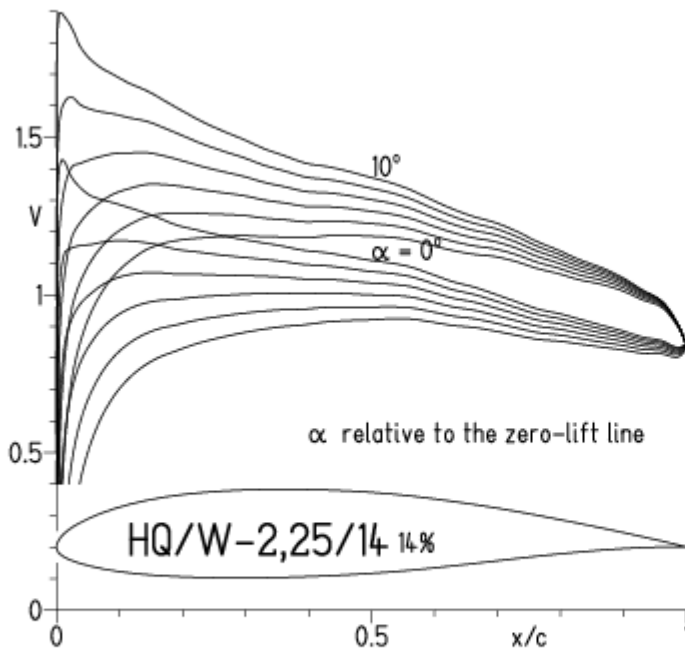


EPPLER 2005 V. 8.

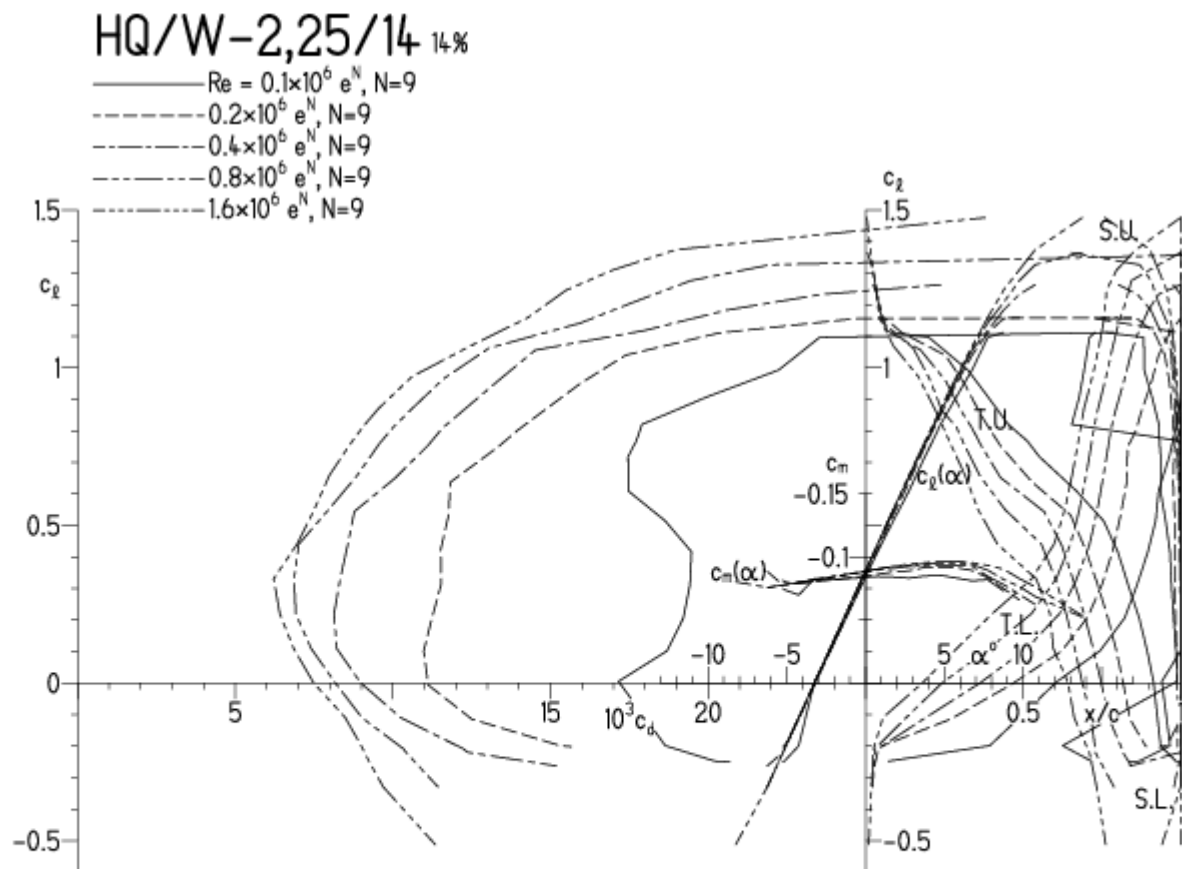


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

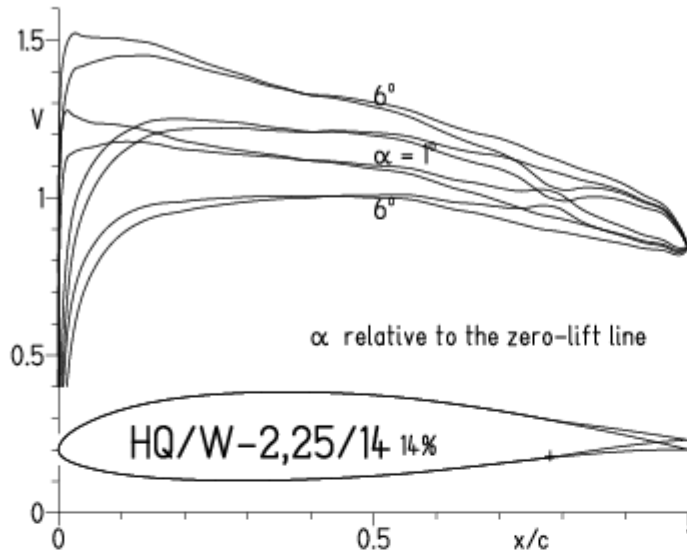
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

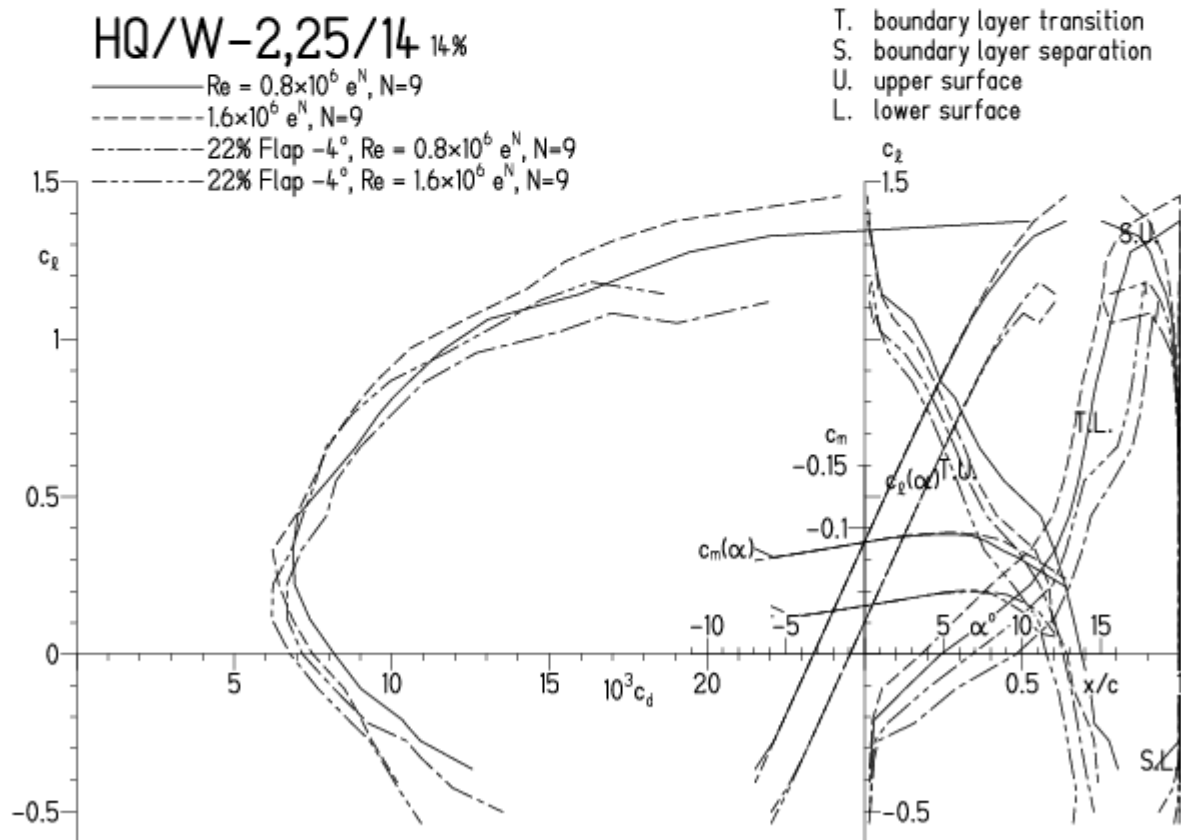


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

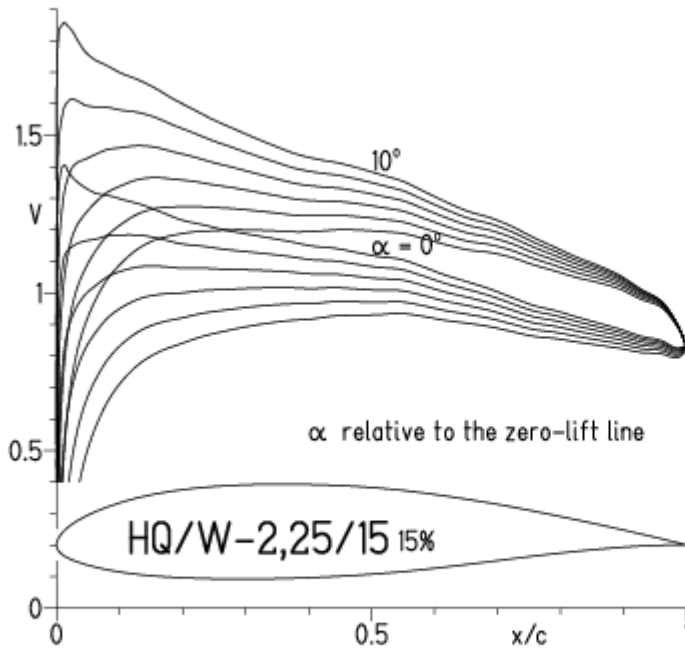


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

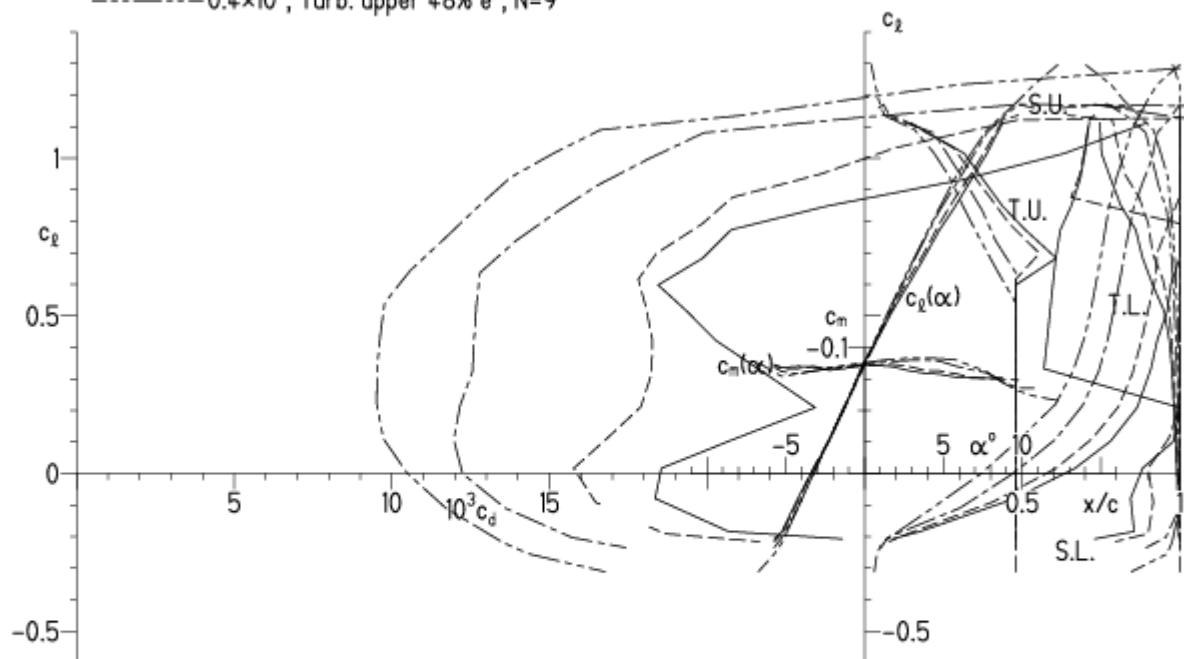
EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

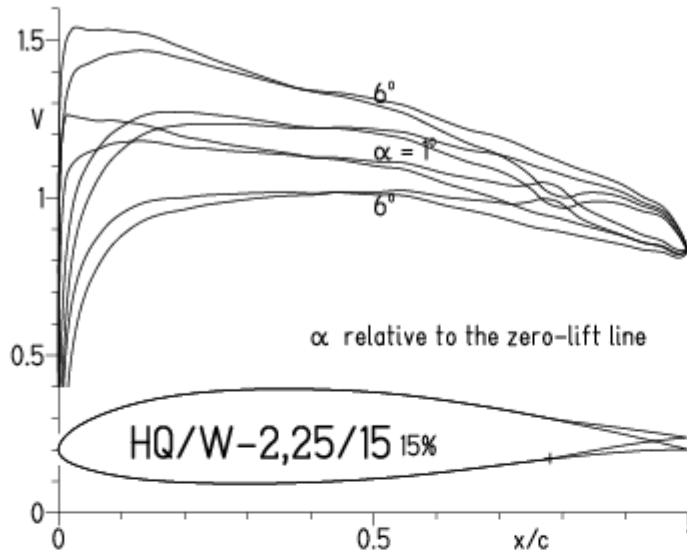


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

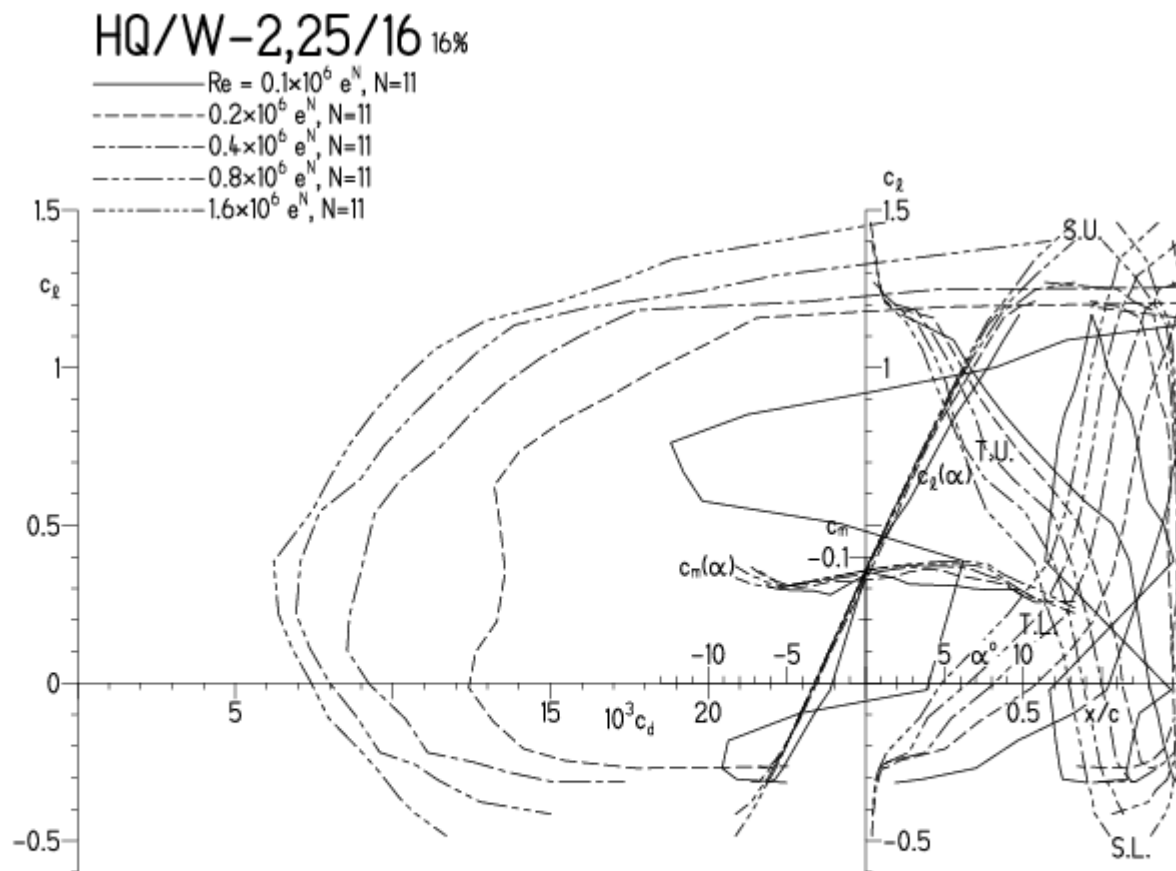


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. $30 - 35 \text{ m/s}$ Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

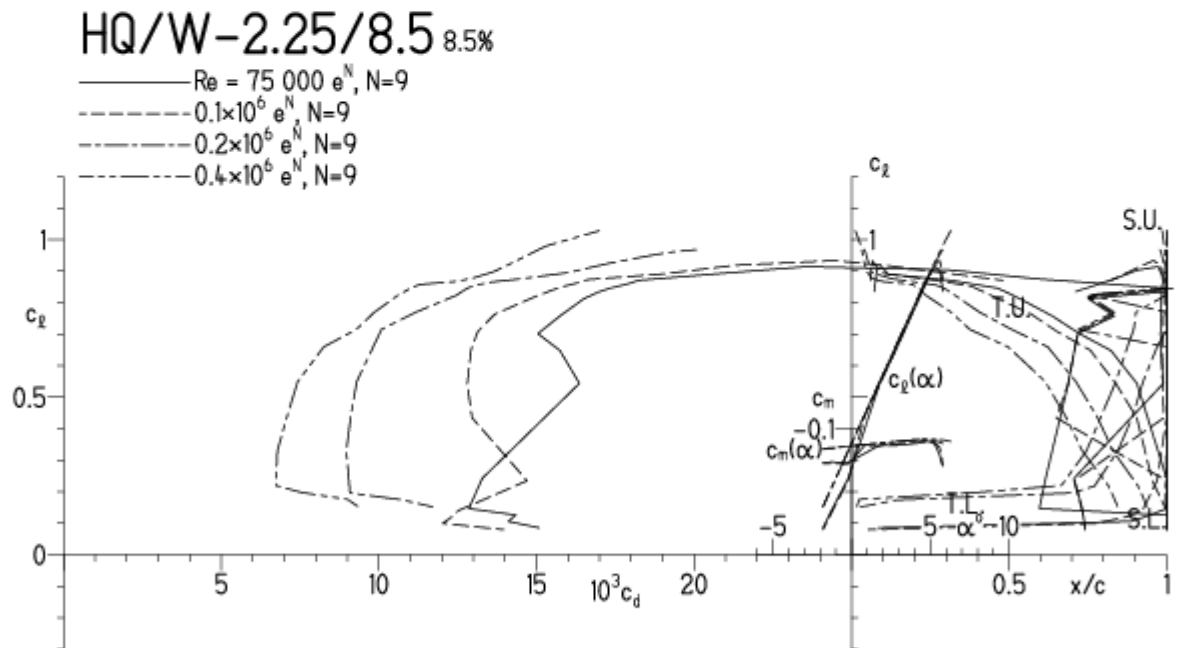


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

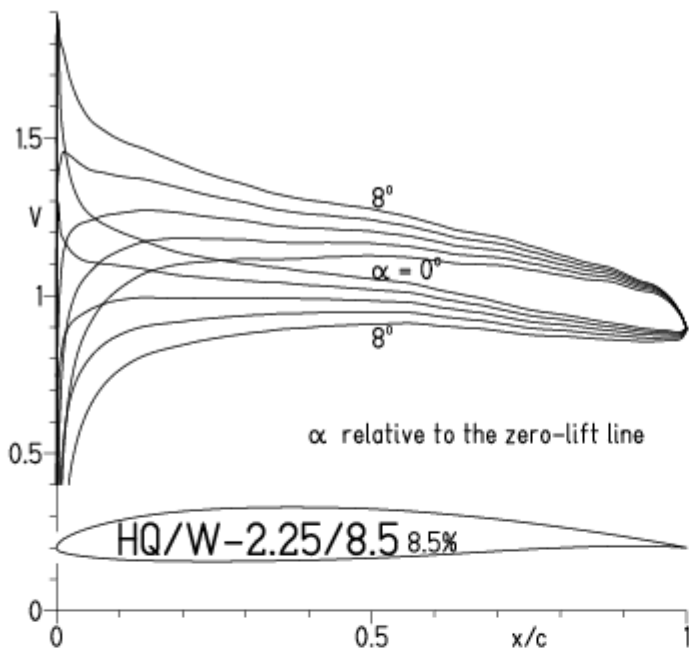


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

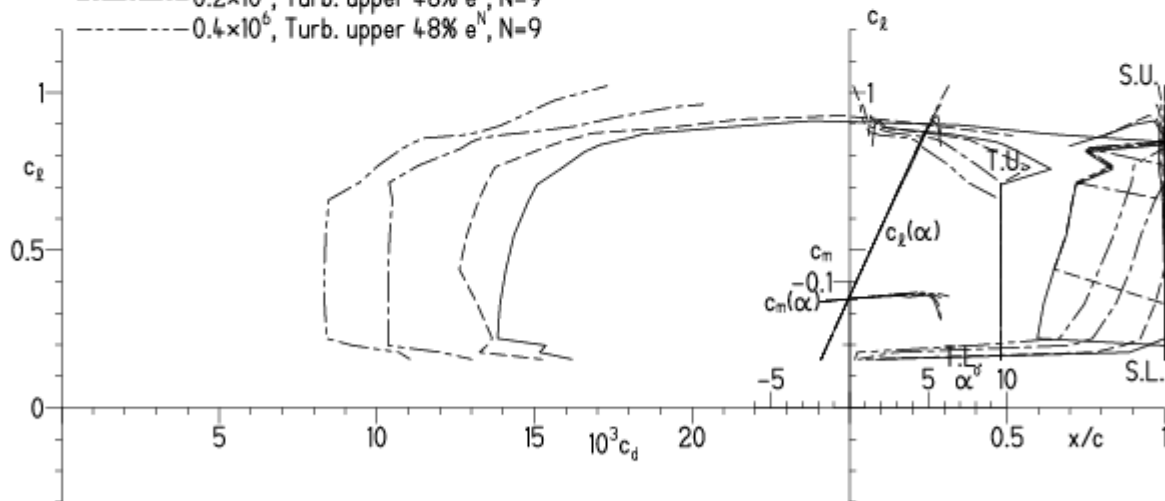
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

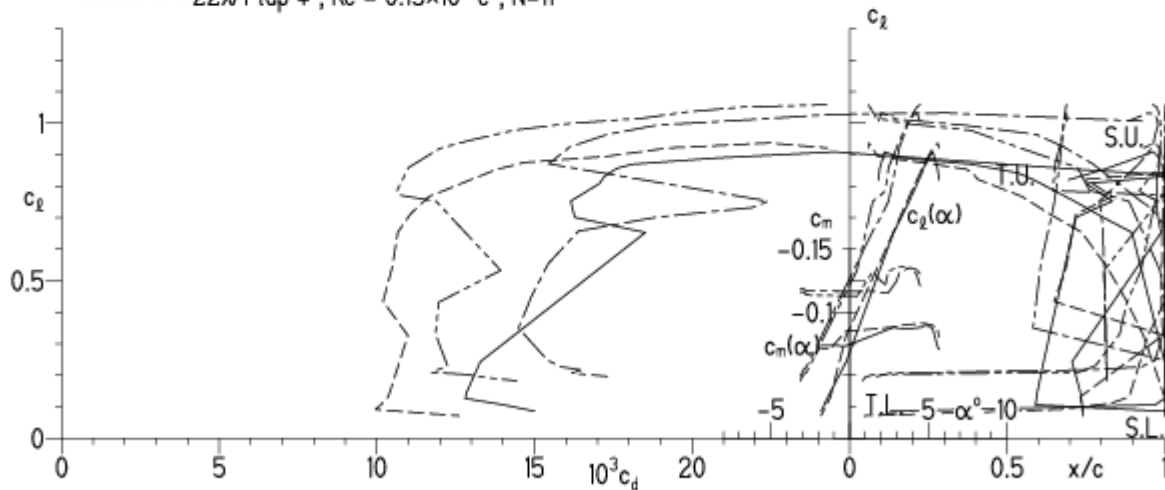


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$

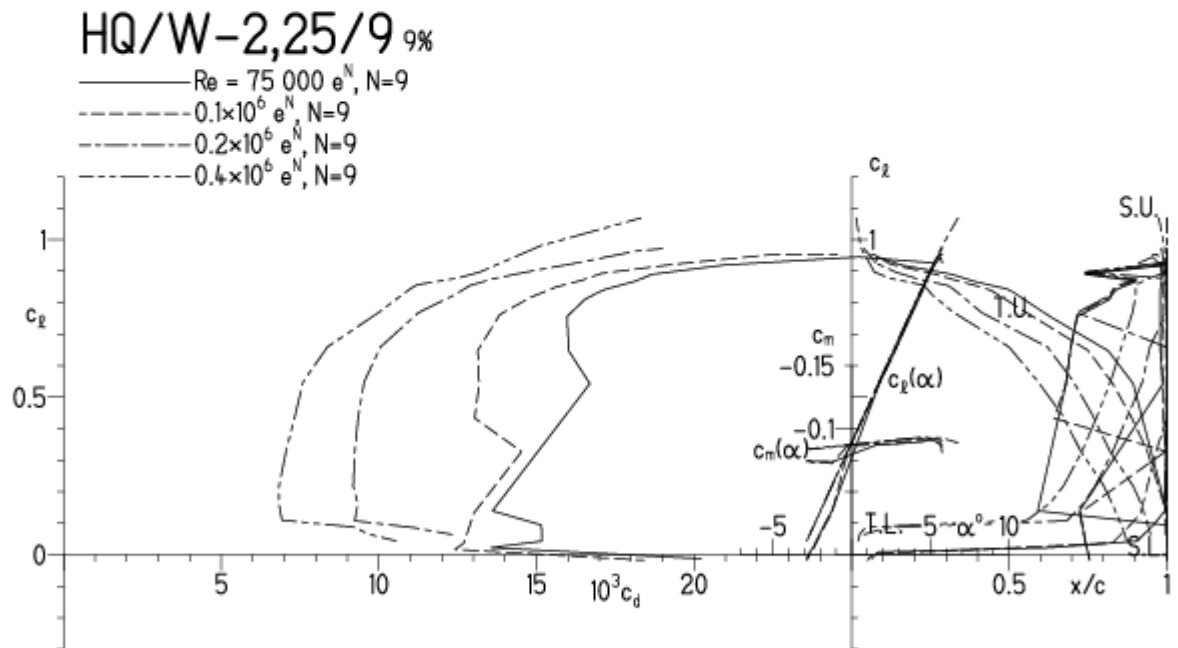


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

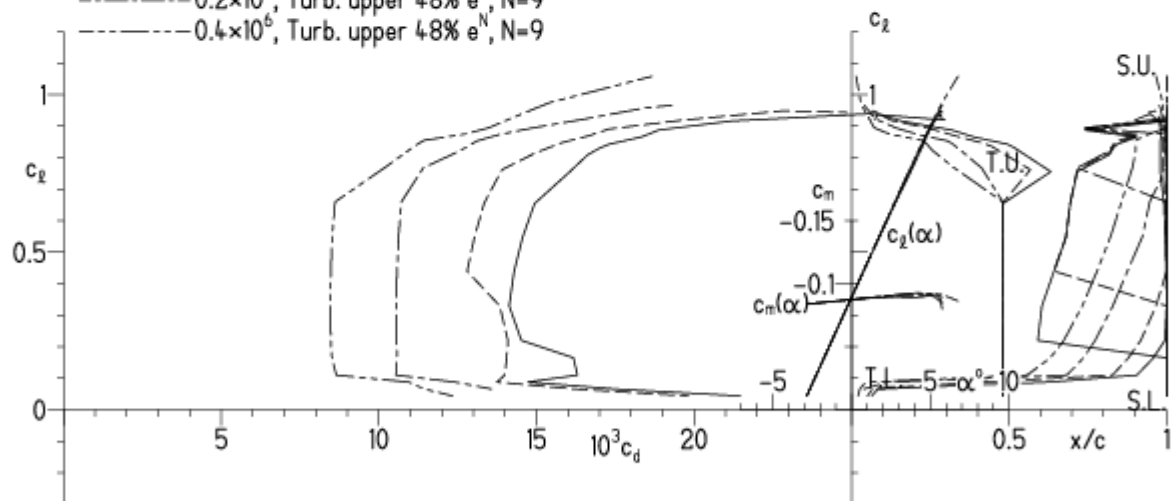
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38

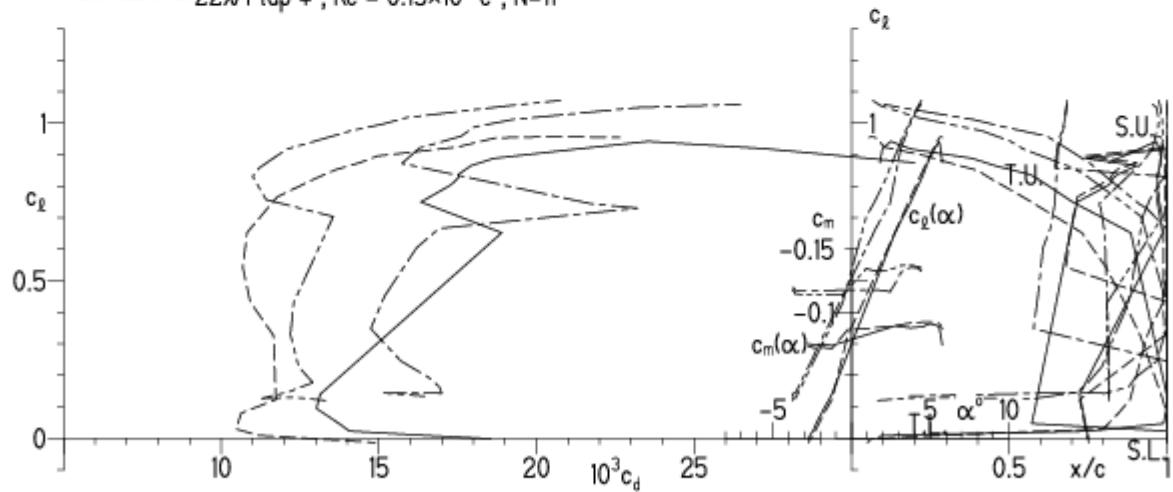


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48

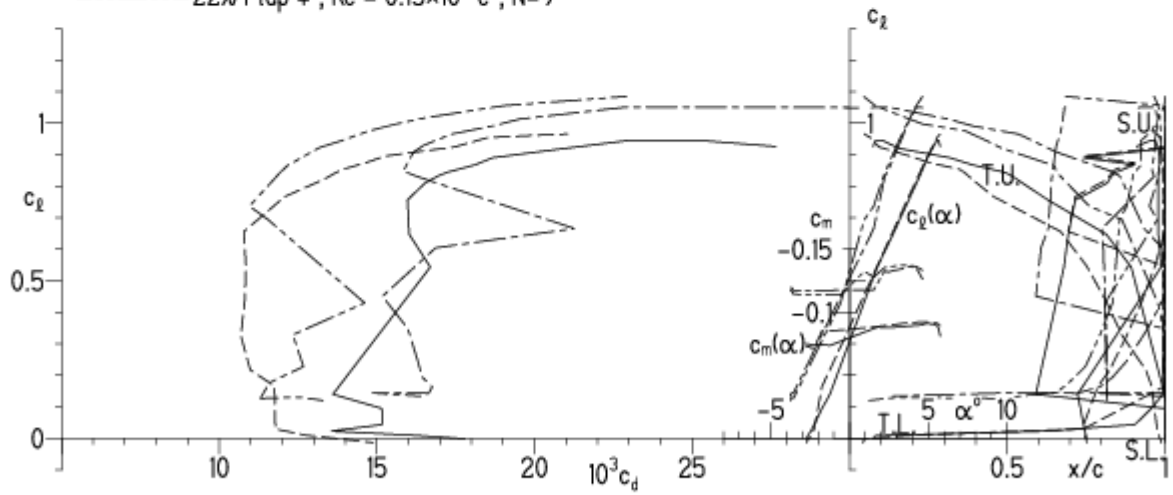


EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17

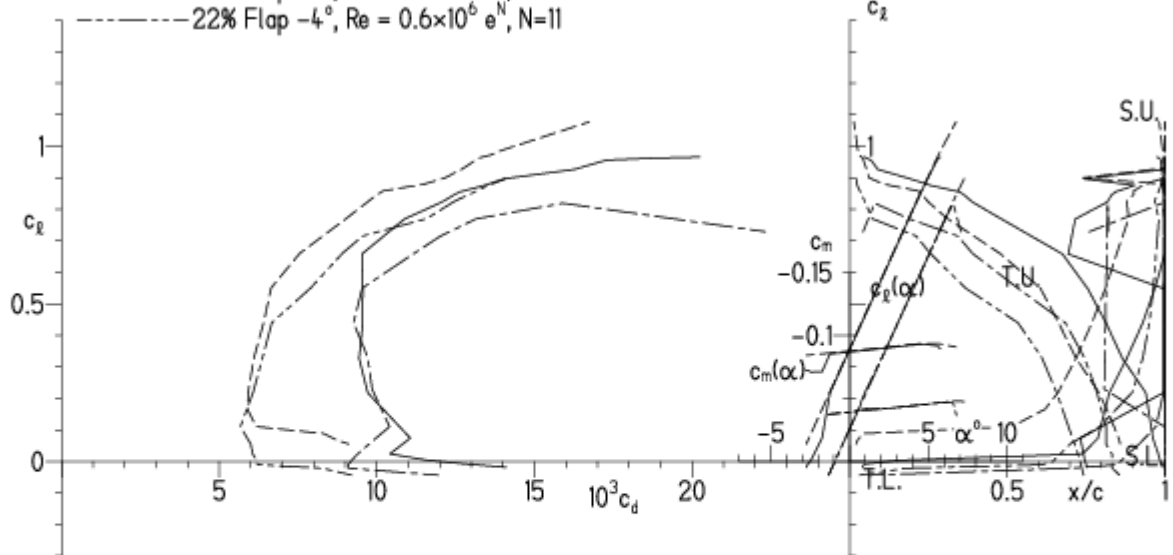


EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11

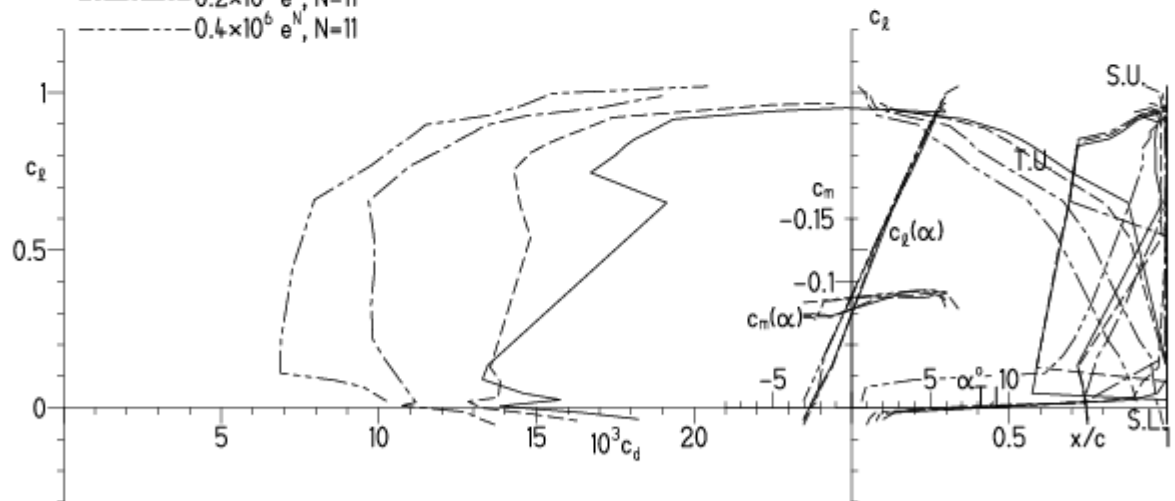
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



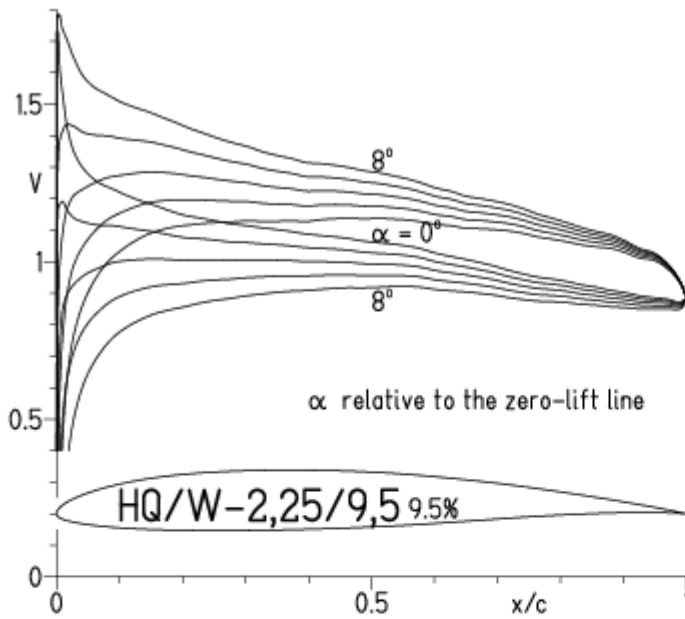
EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

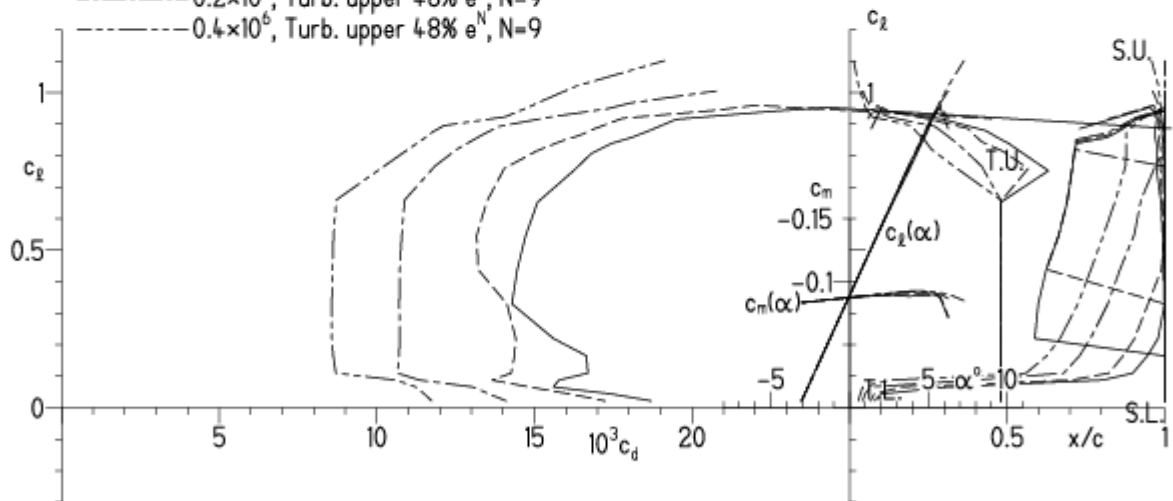
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

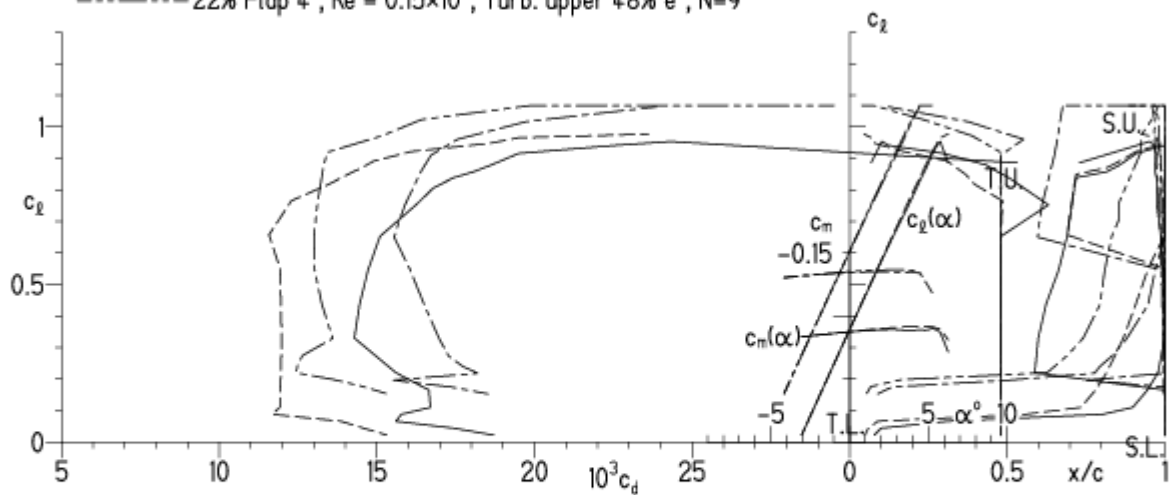


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



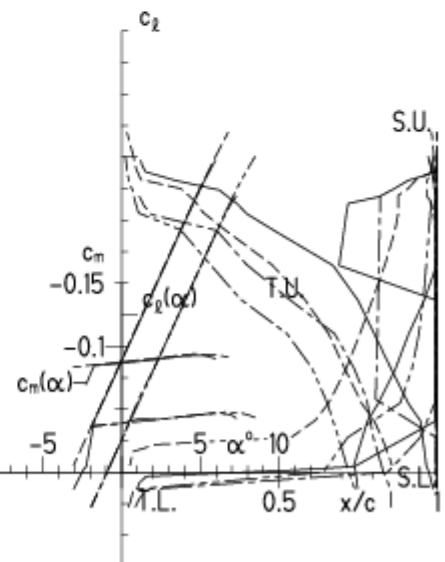
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

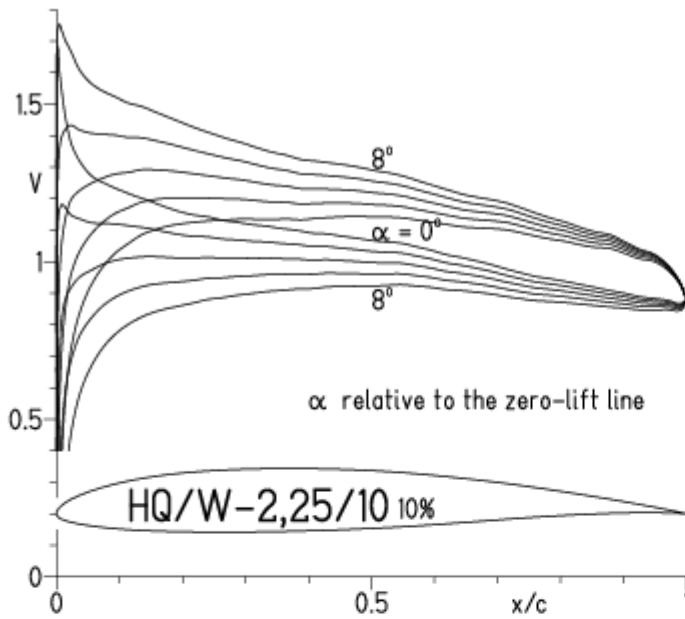


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

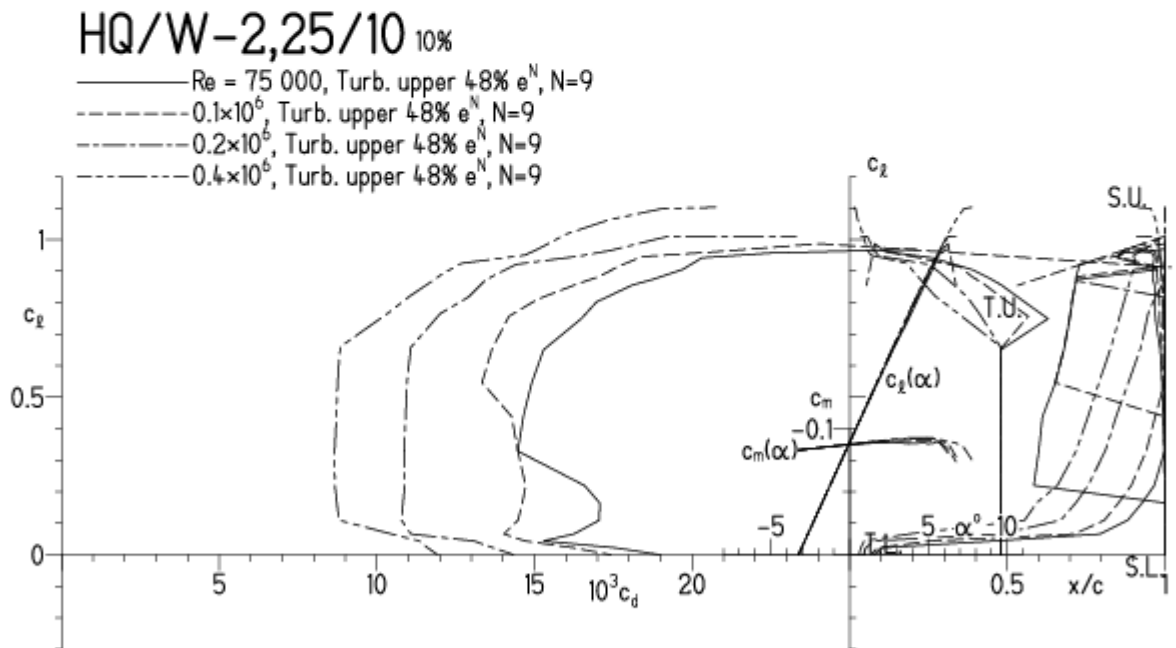


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

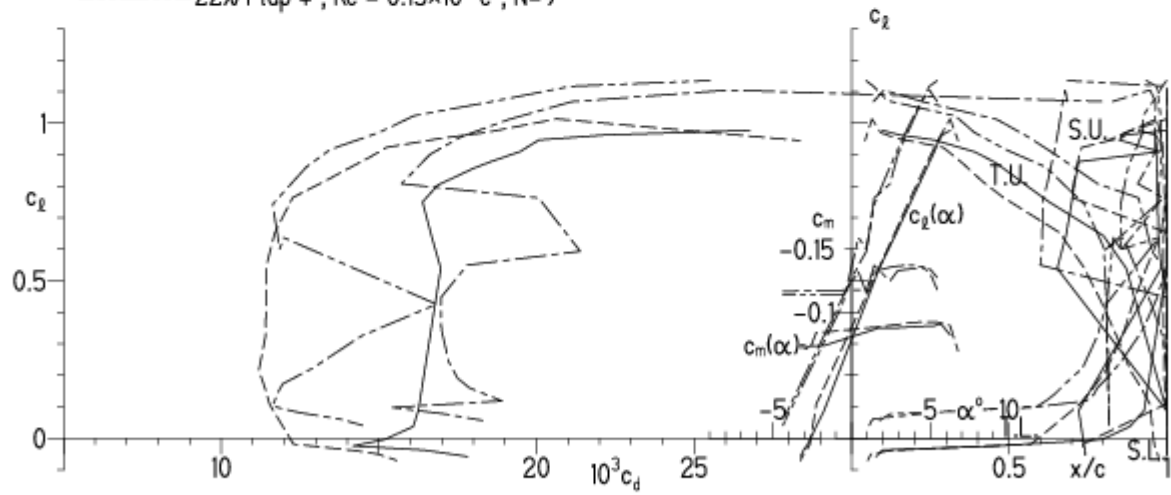


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

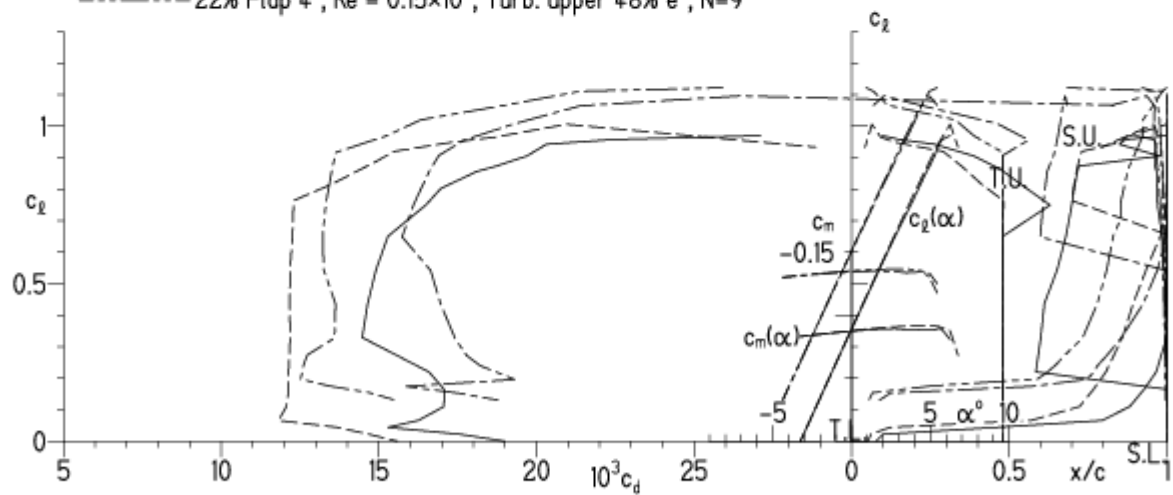


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · - 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

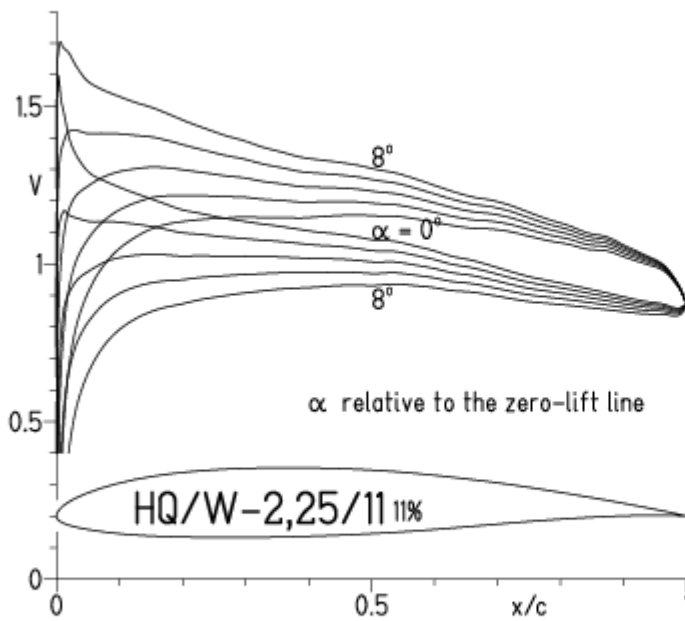


EPPLER 2005 V. 8.5.07 RUN

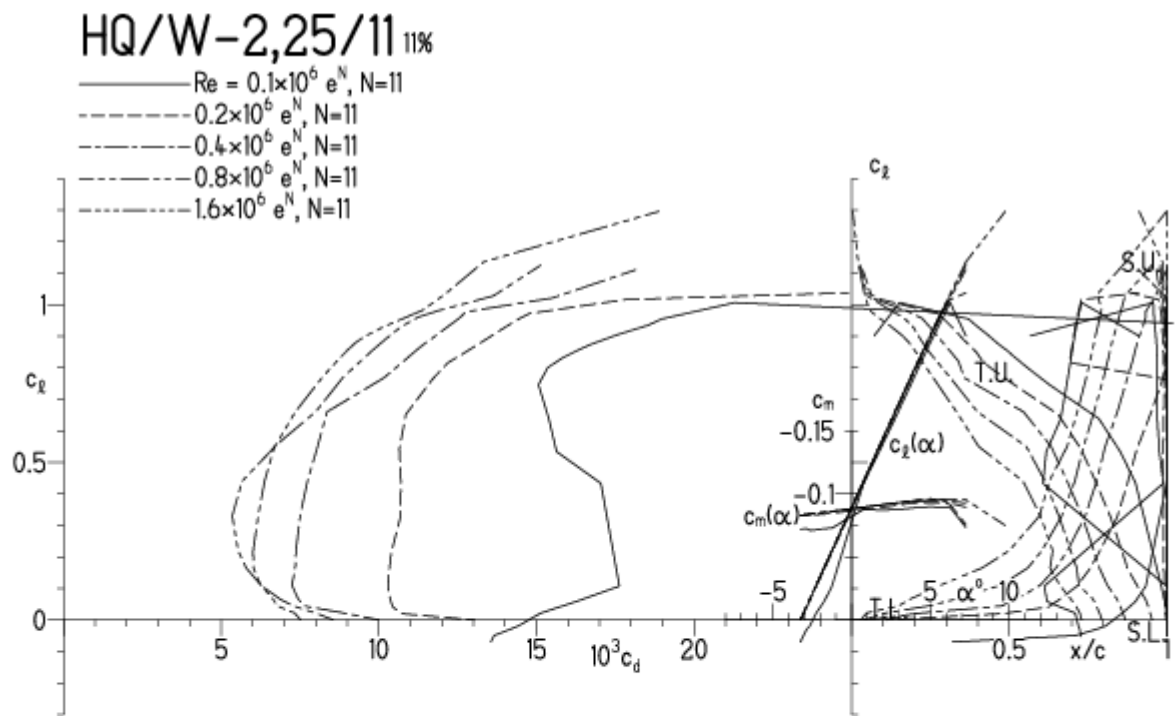


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

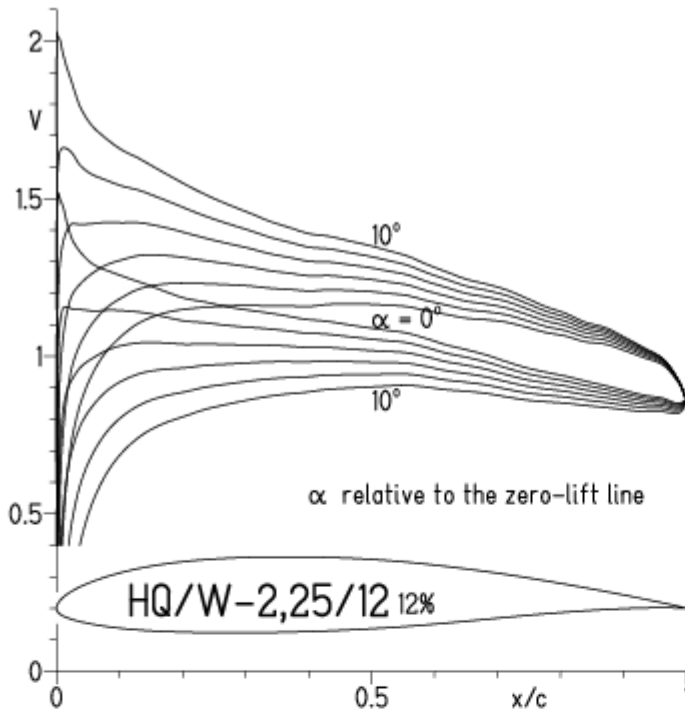
HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

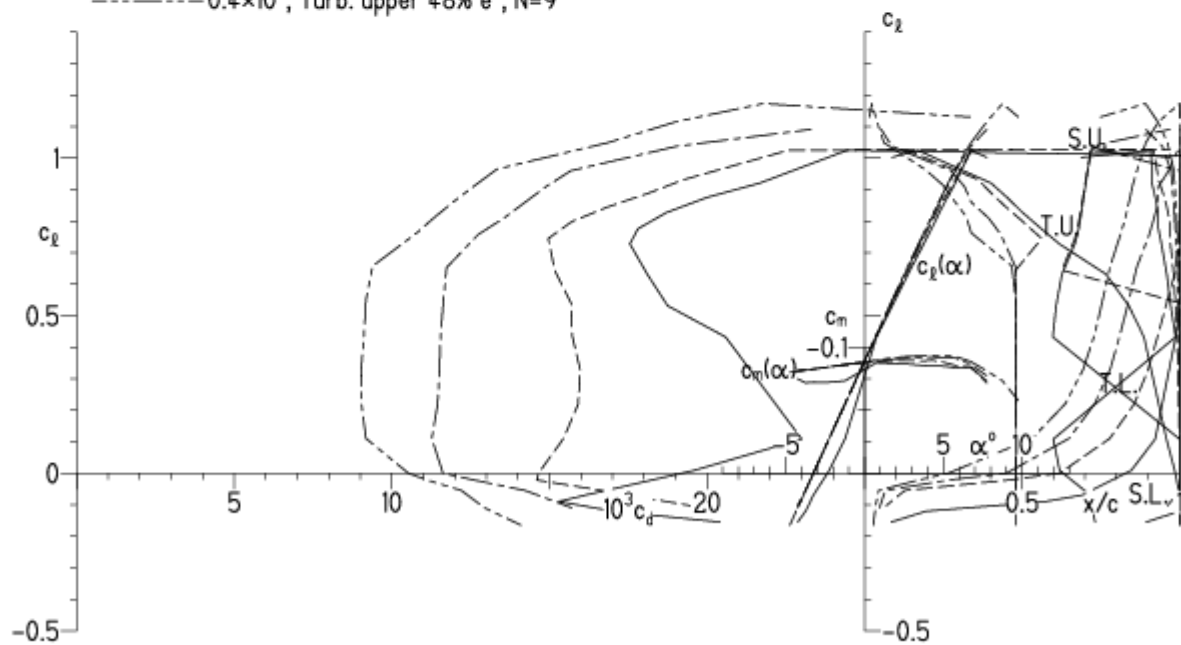
EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - $0.8 \times 10^6 e^N, N=9$
- · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

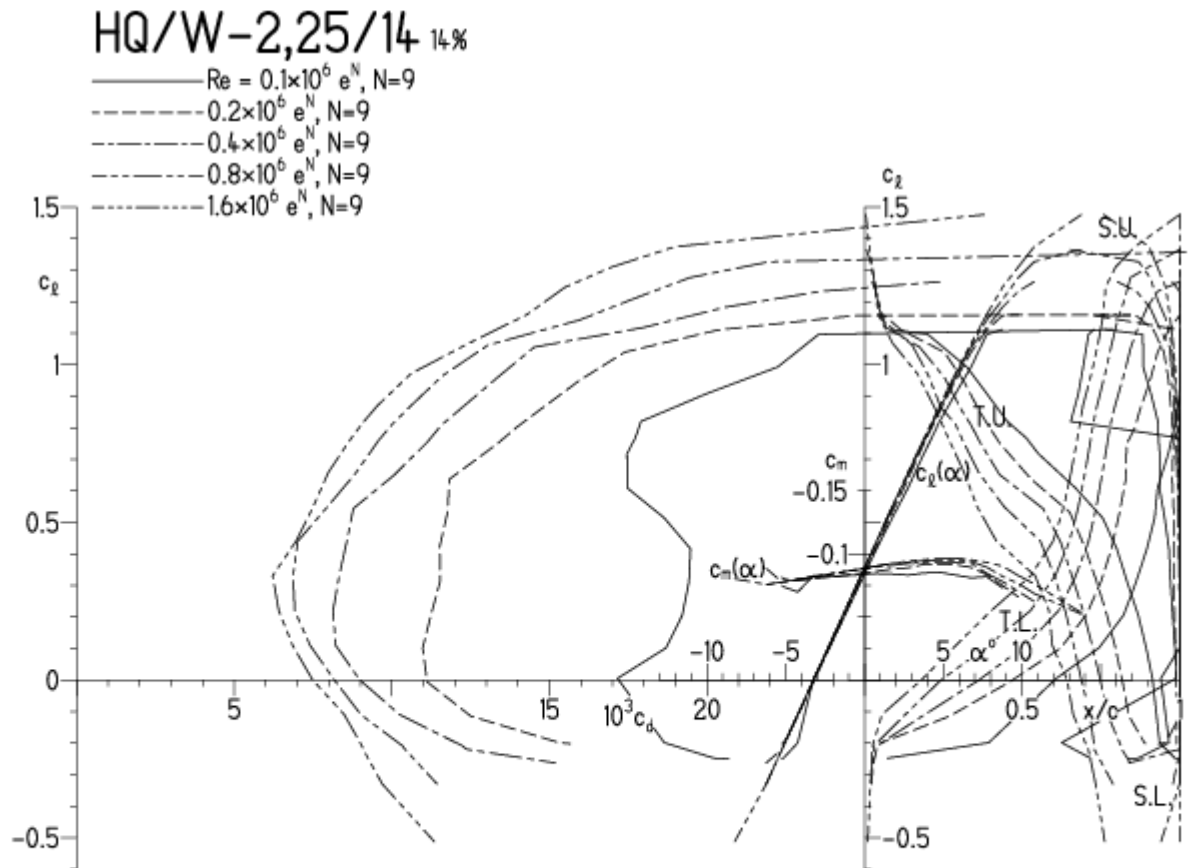


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

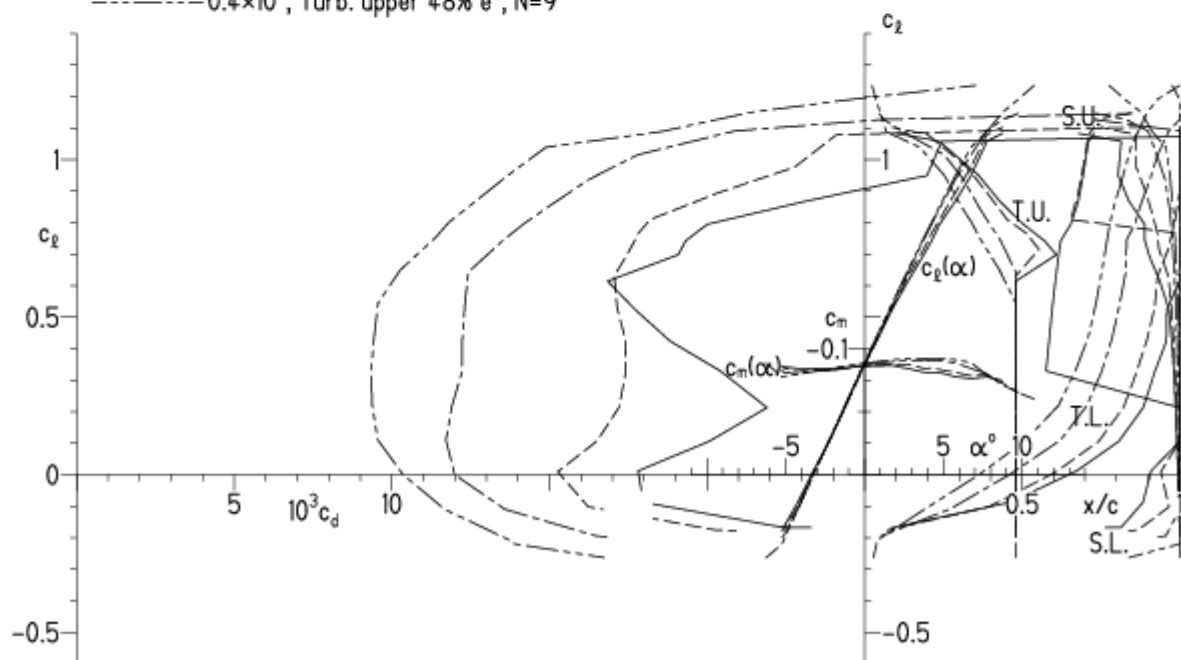
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

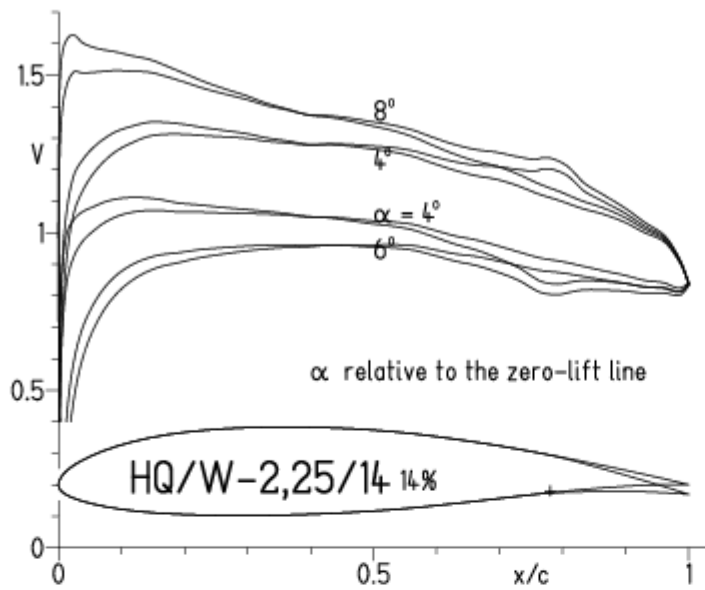
HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

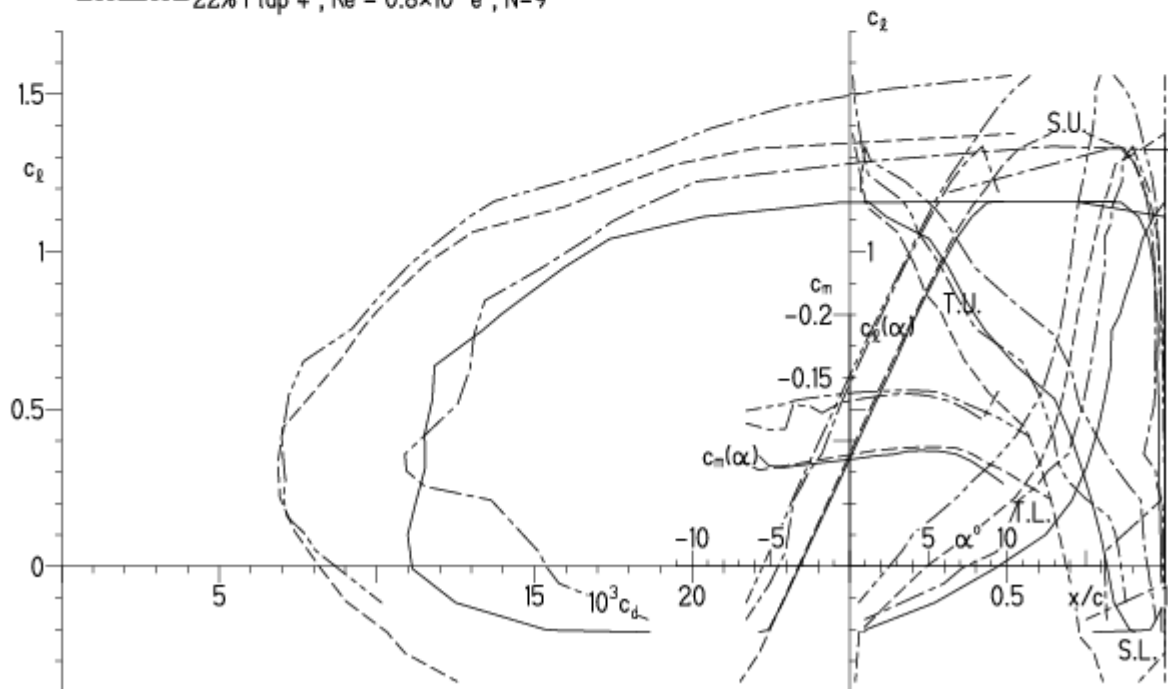


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

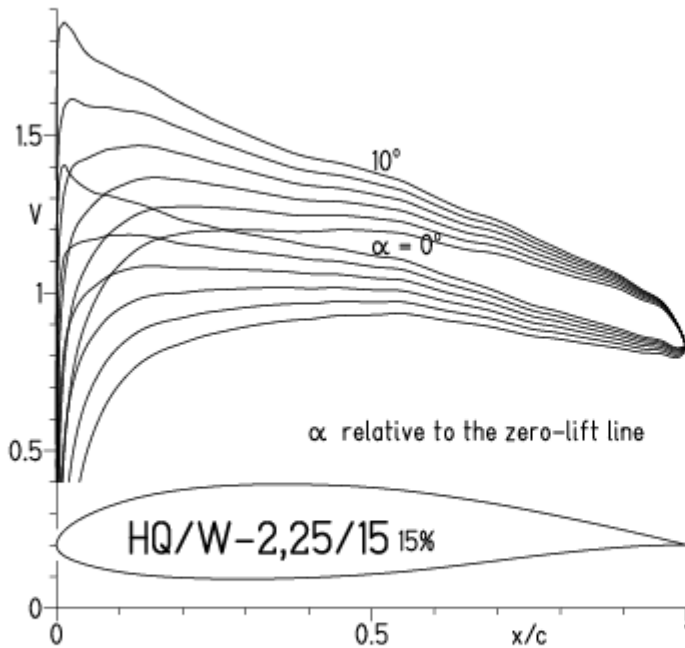


EPPLER 2005 V. 8.5.07

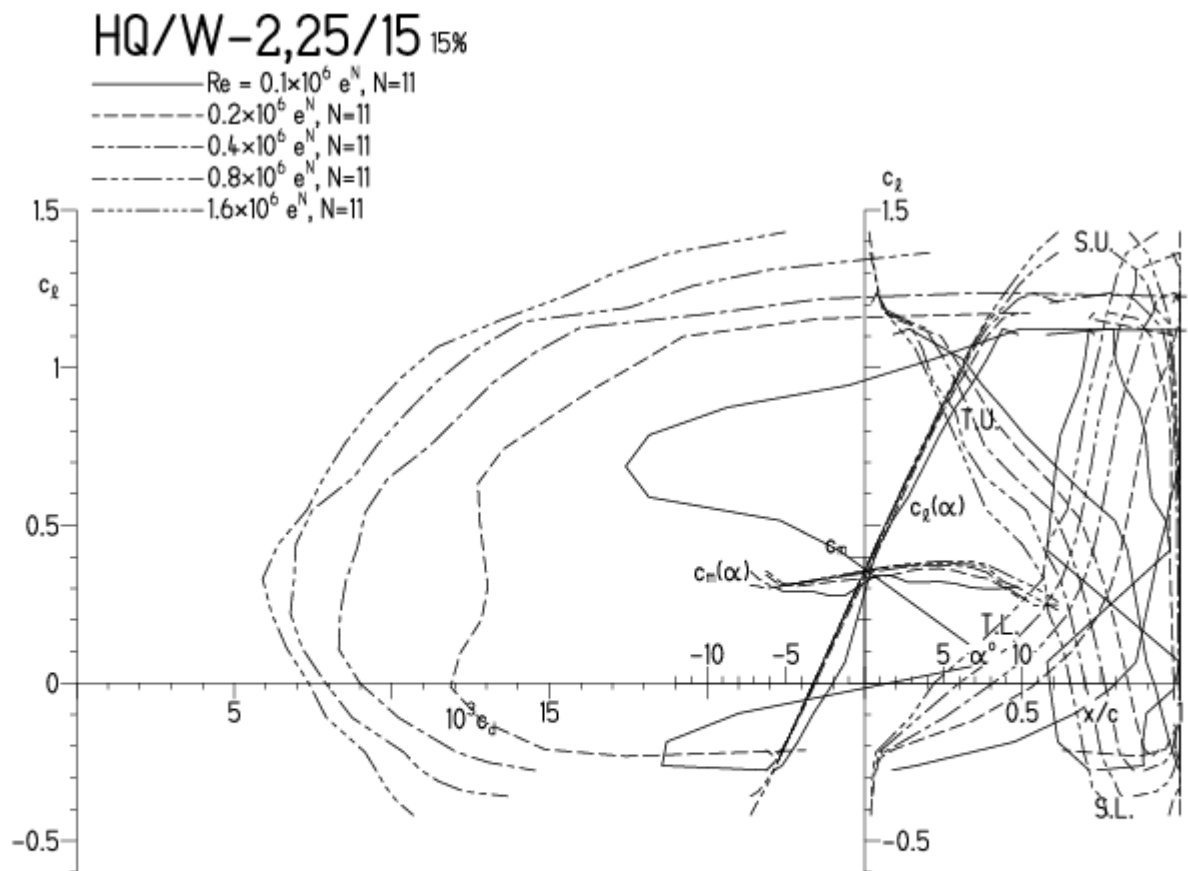


HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

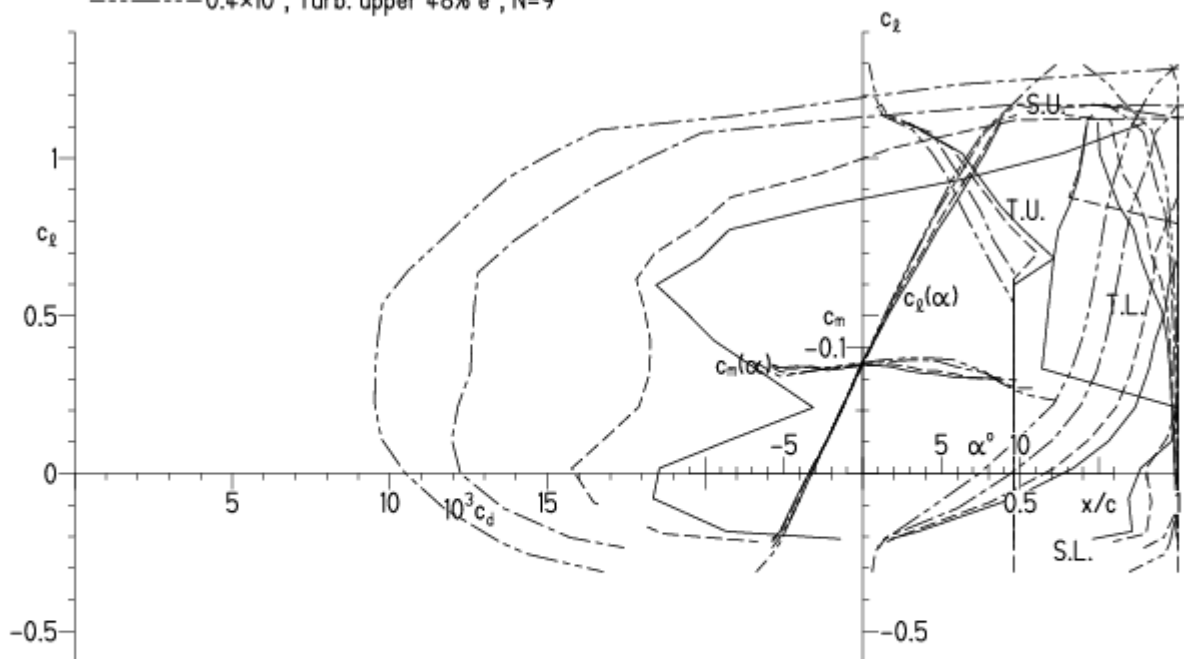
EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



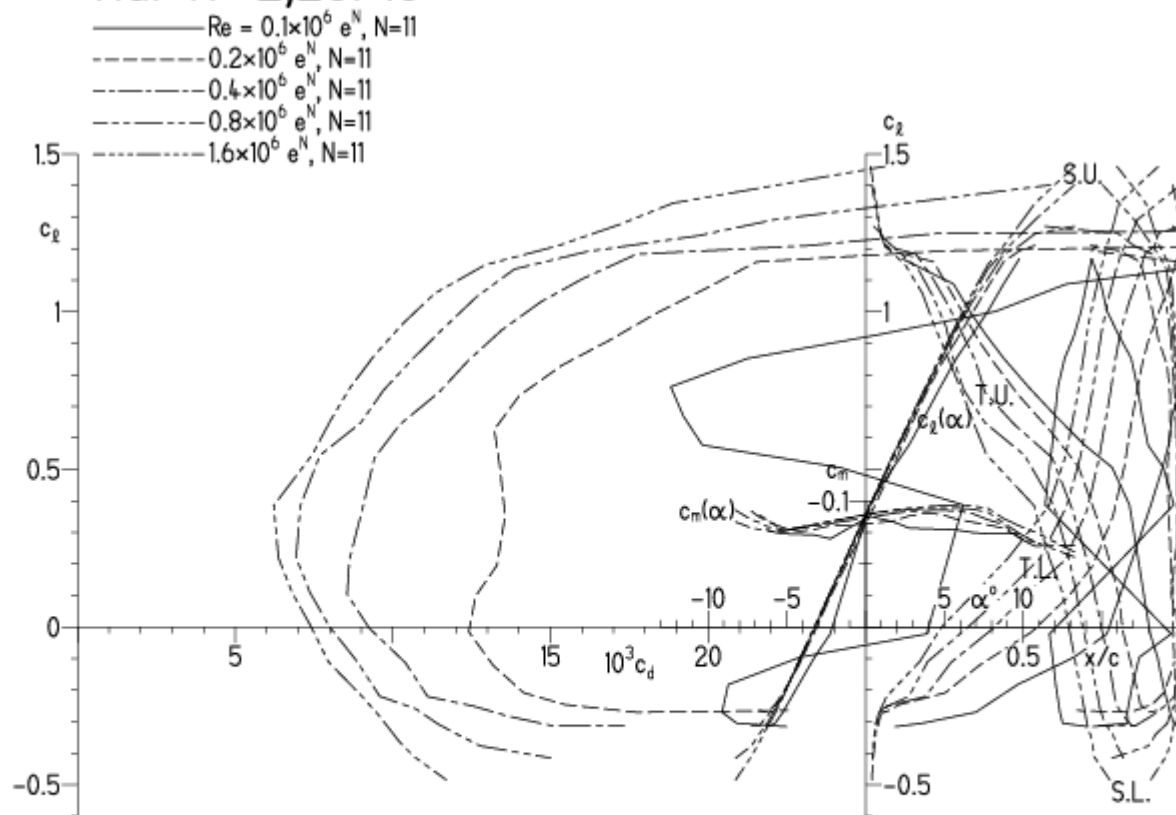
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

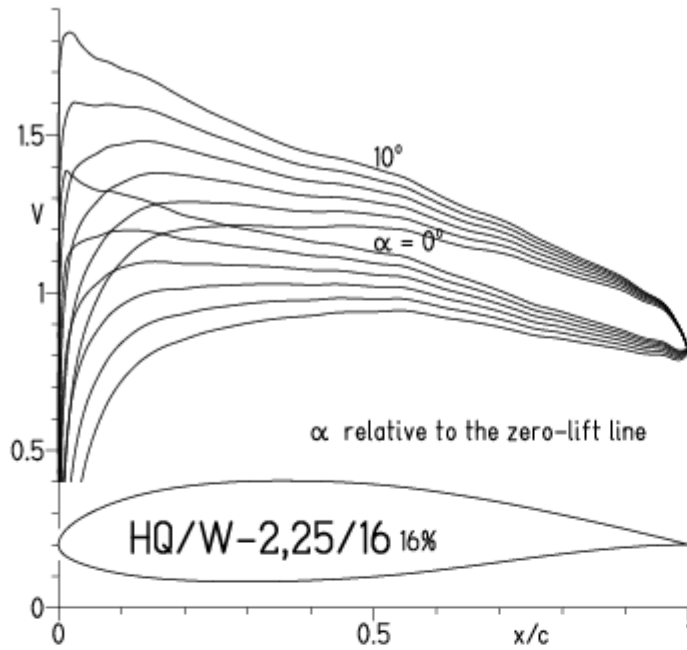
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

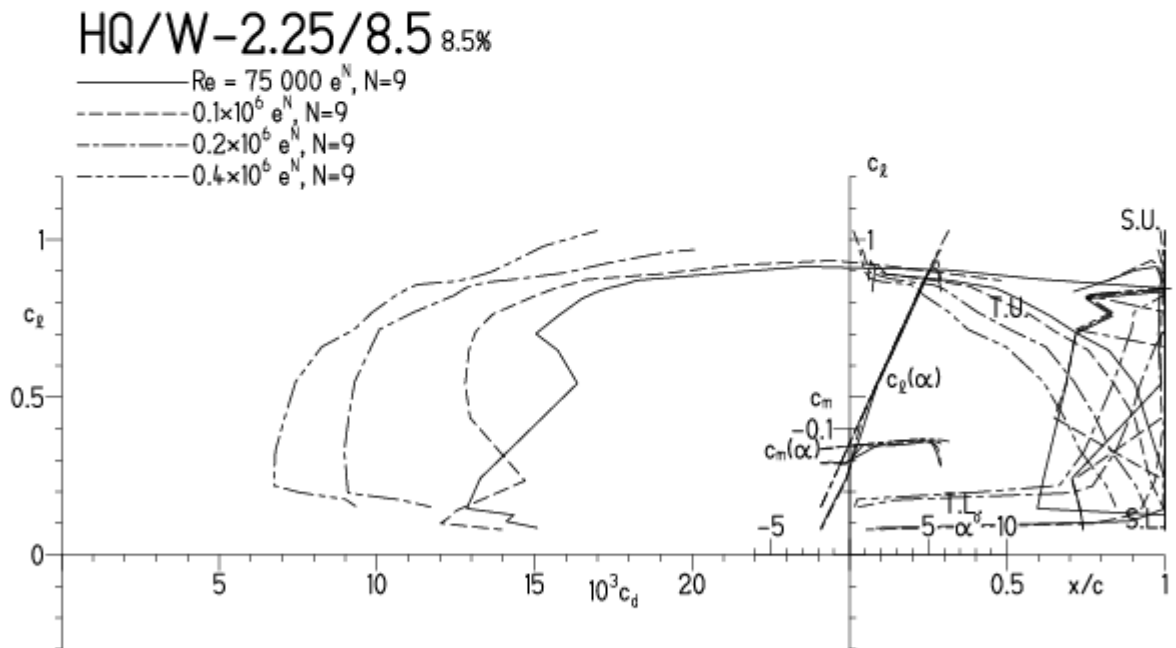


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

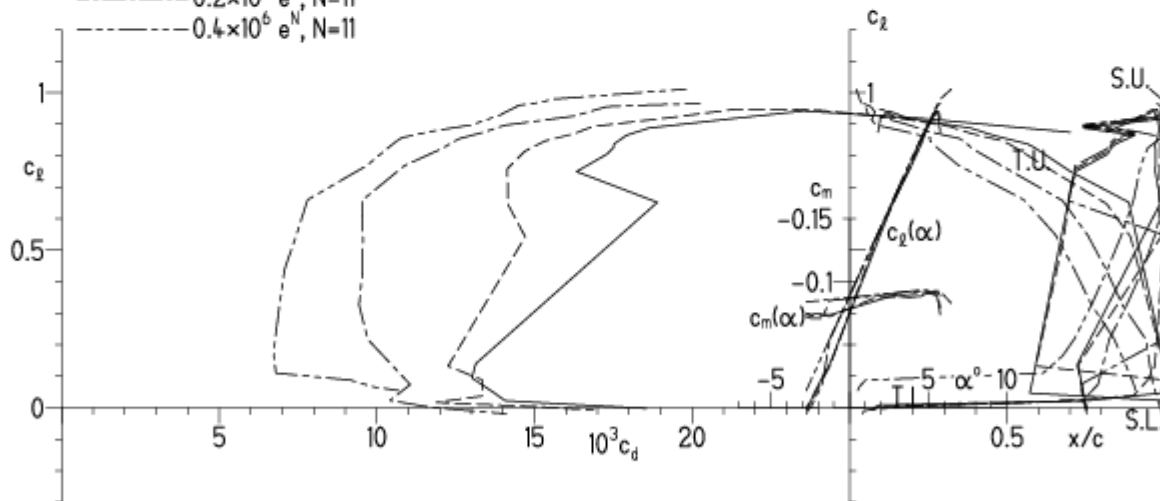
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$

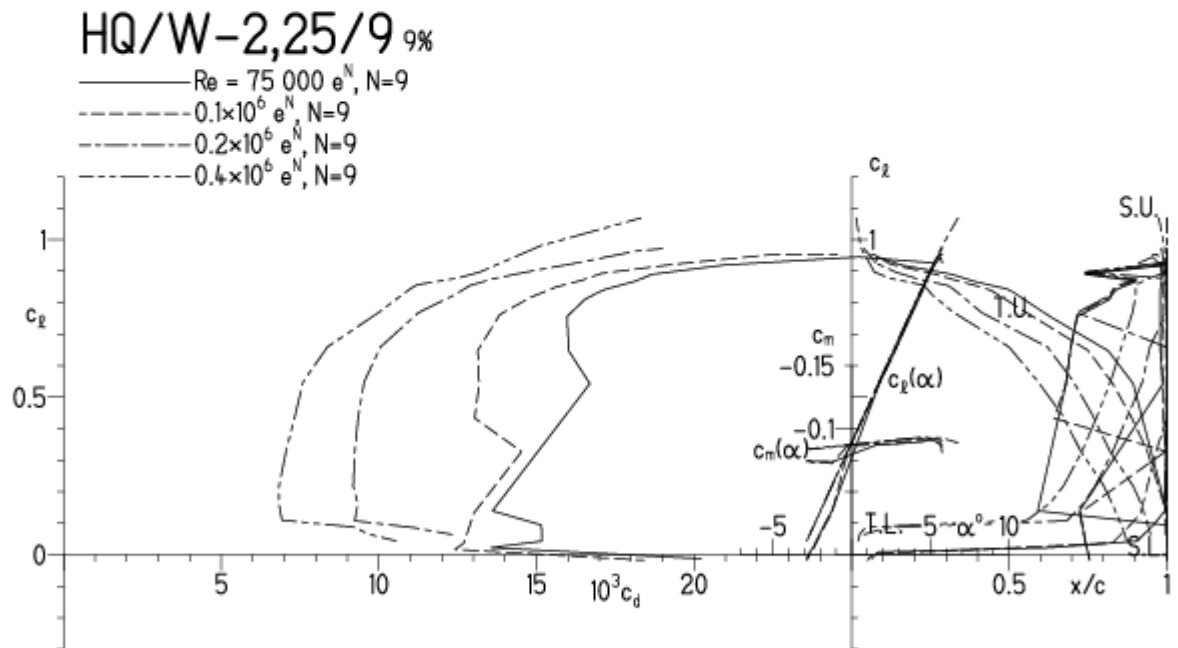


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

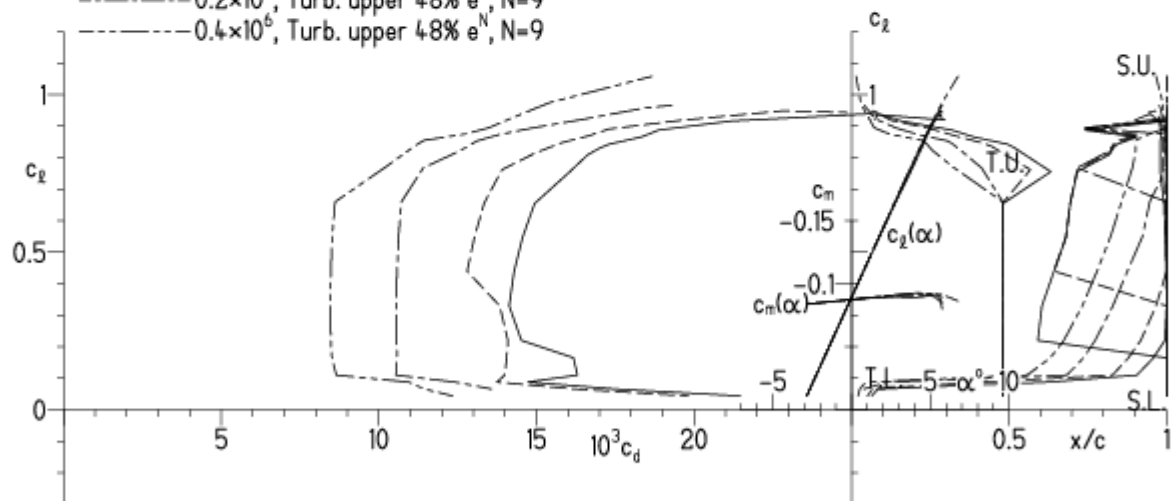
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38

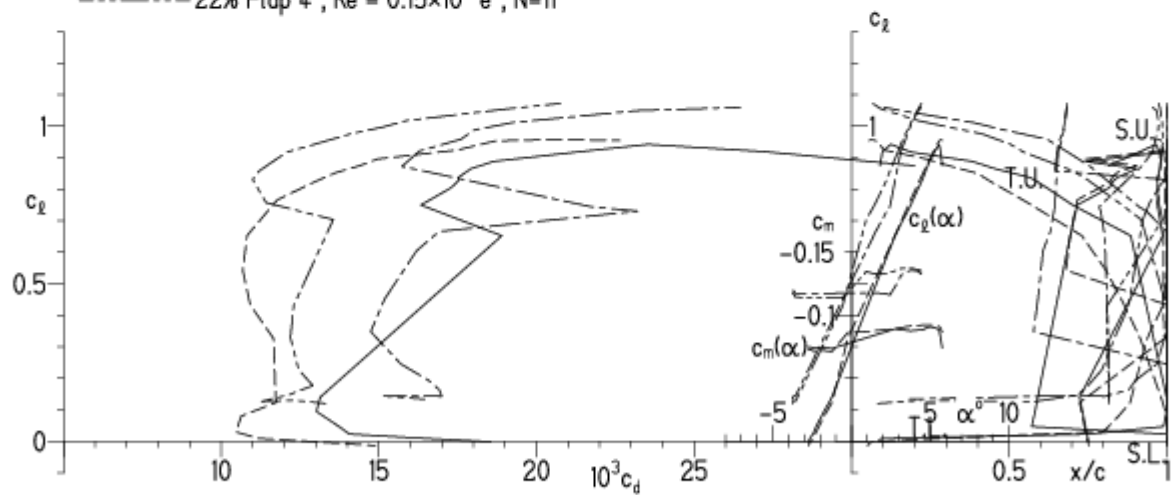


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

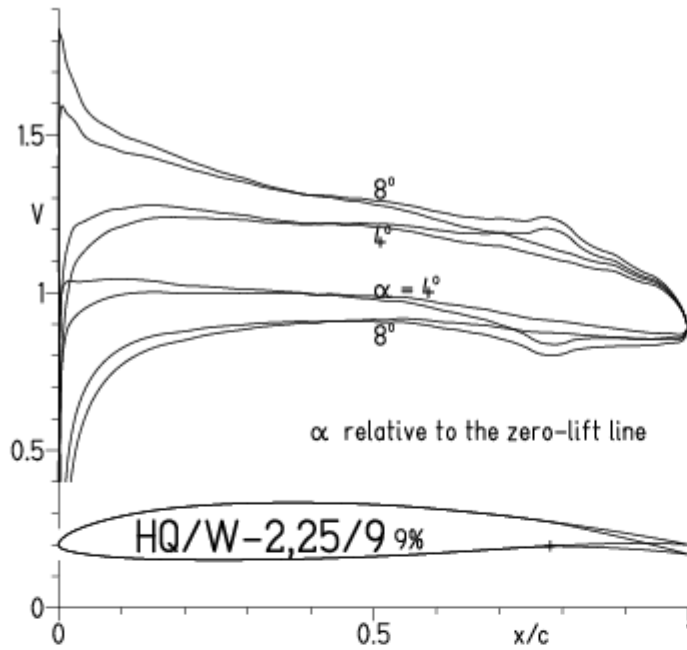
- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48

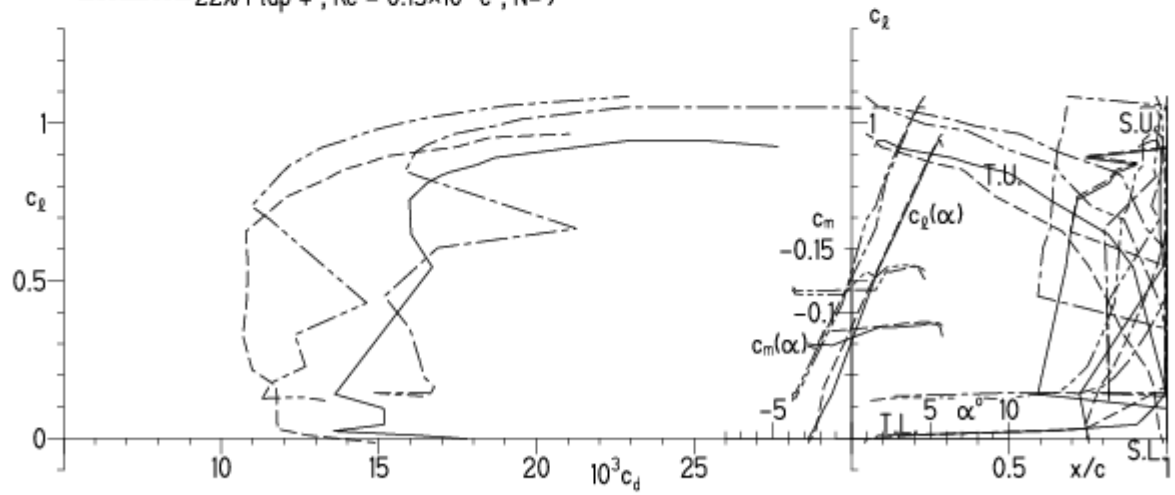


EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

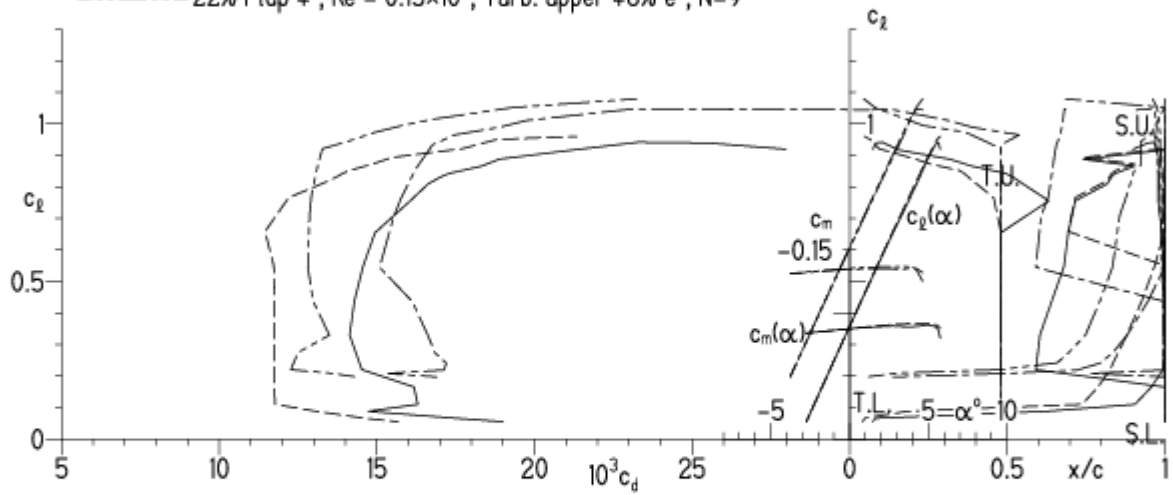


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

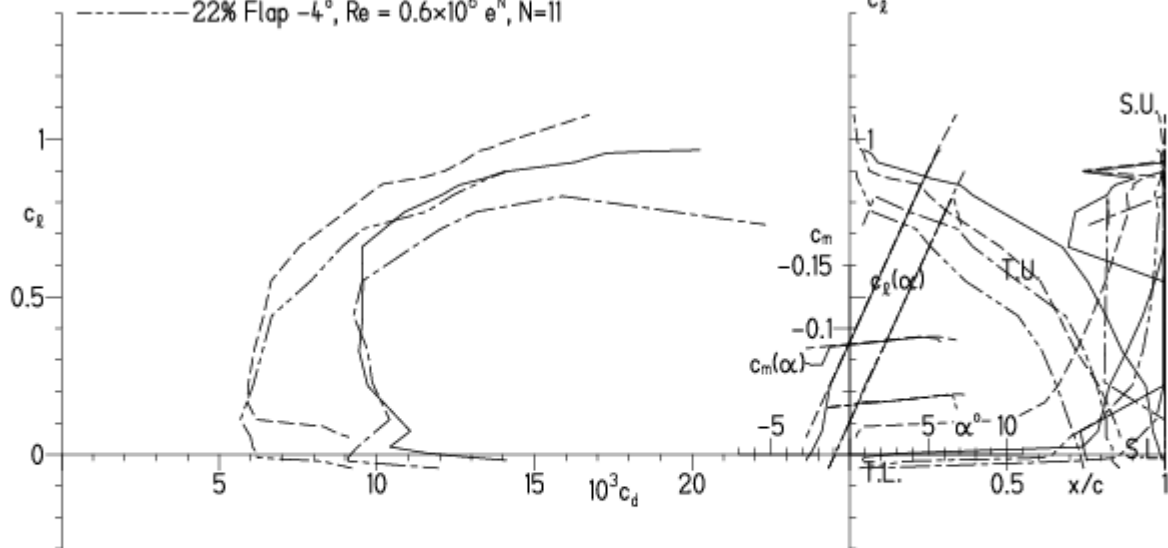
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

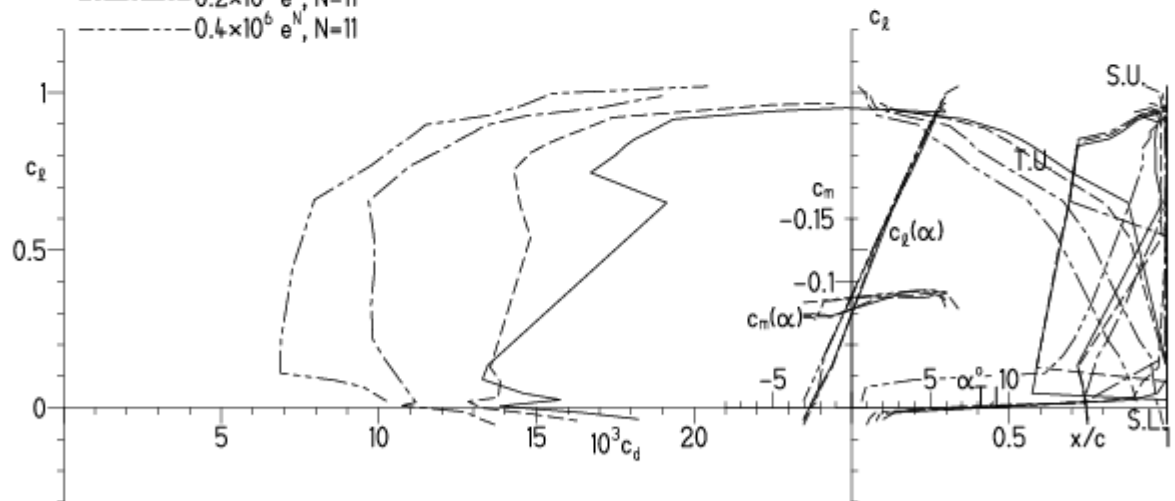
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

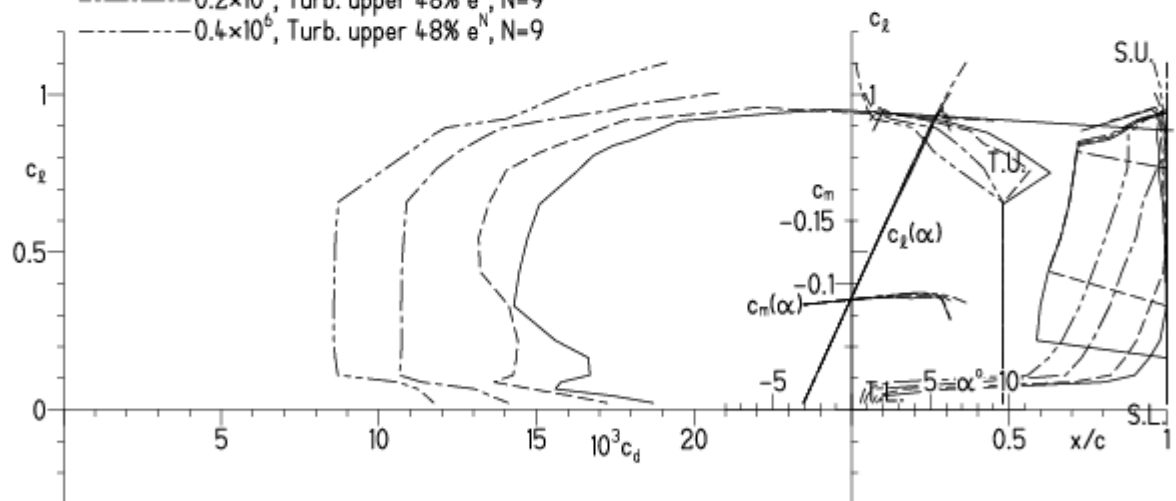
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N$, $N=11$
- - - $0.6 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 0.2 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N$, $N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

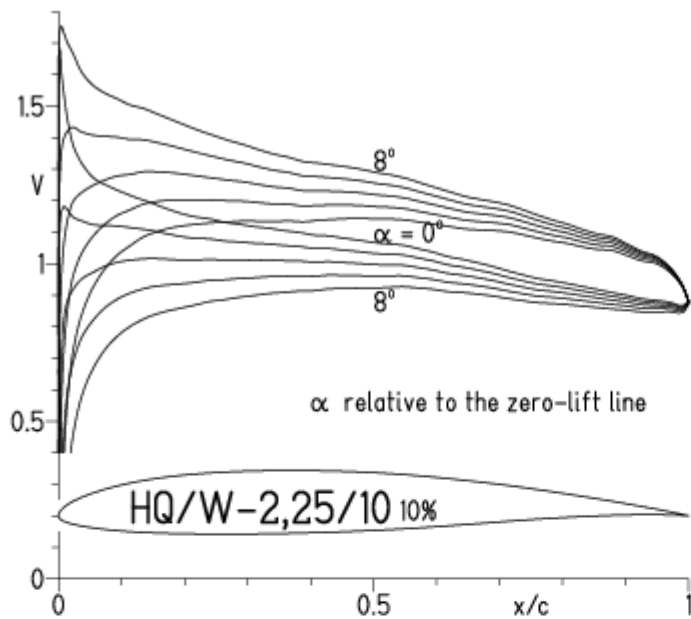


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

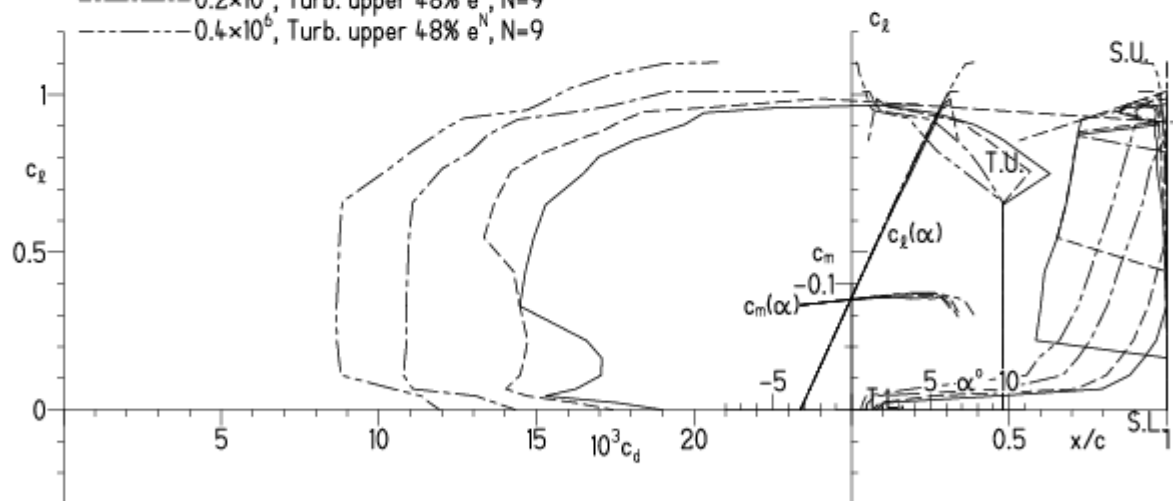
HQ/W-2,25/10 10%

— Re = 75 000, Turb. upper 48% e^N, N=9

- - - 0.1 × 10⁶, Turb. upper 48% e^N, N=9

- · - 0.2 × 10⁶, Turb. upper 48% e^N, N=9

- - - 0.4 × 10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

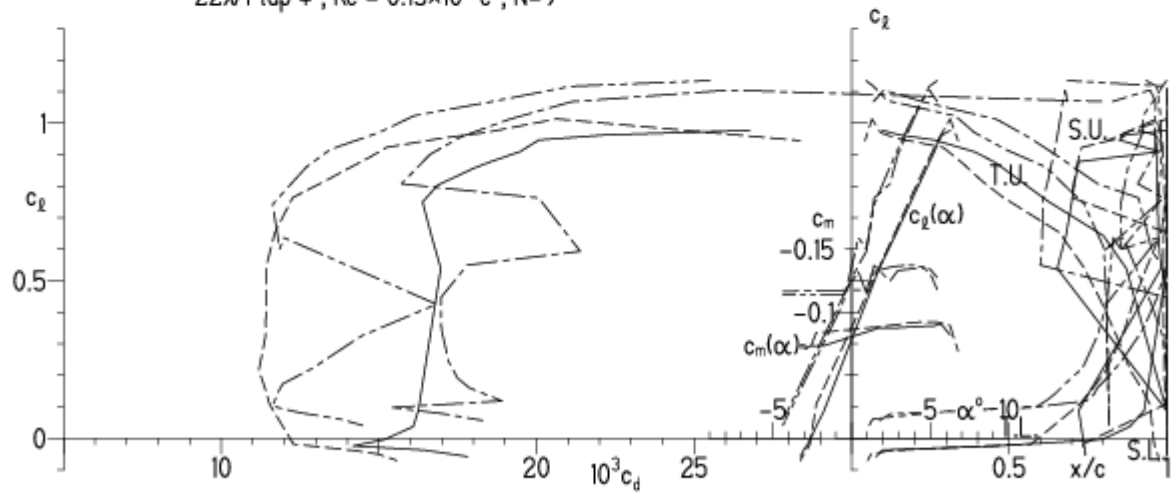


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

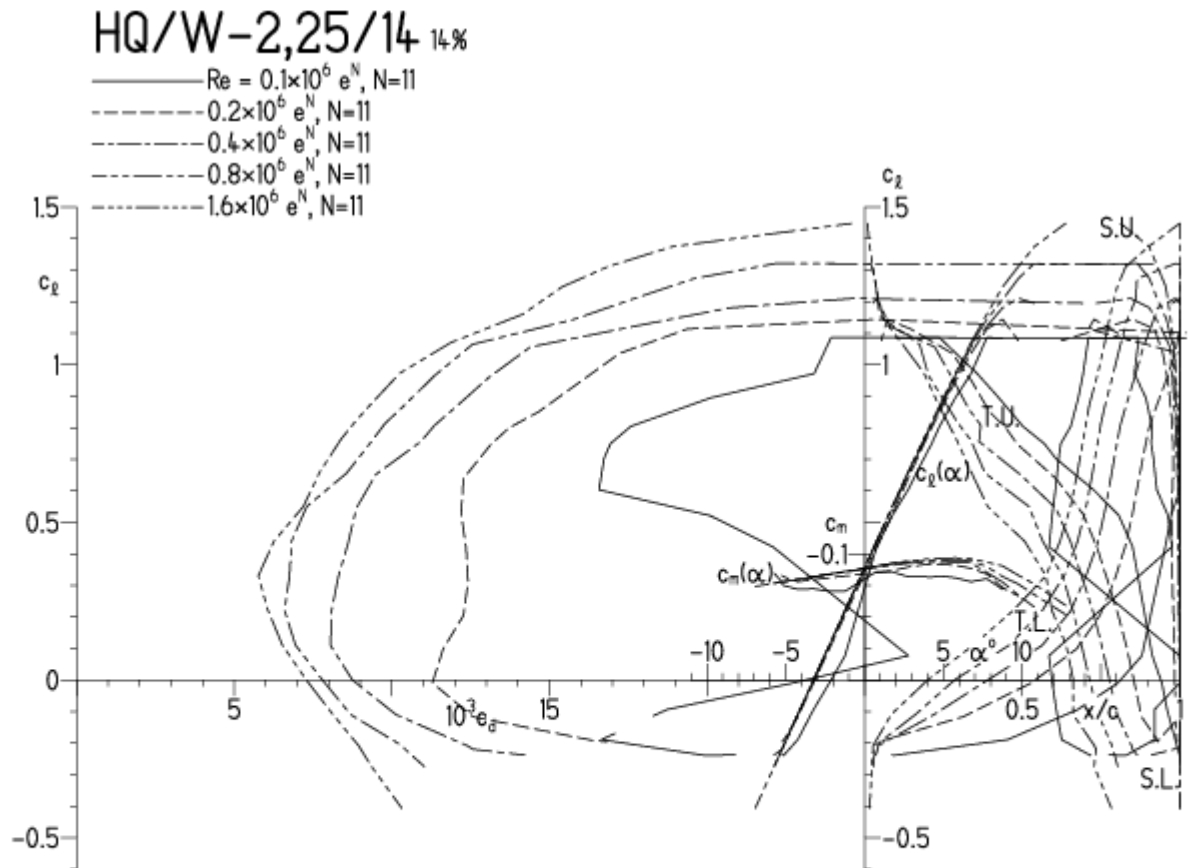


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

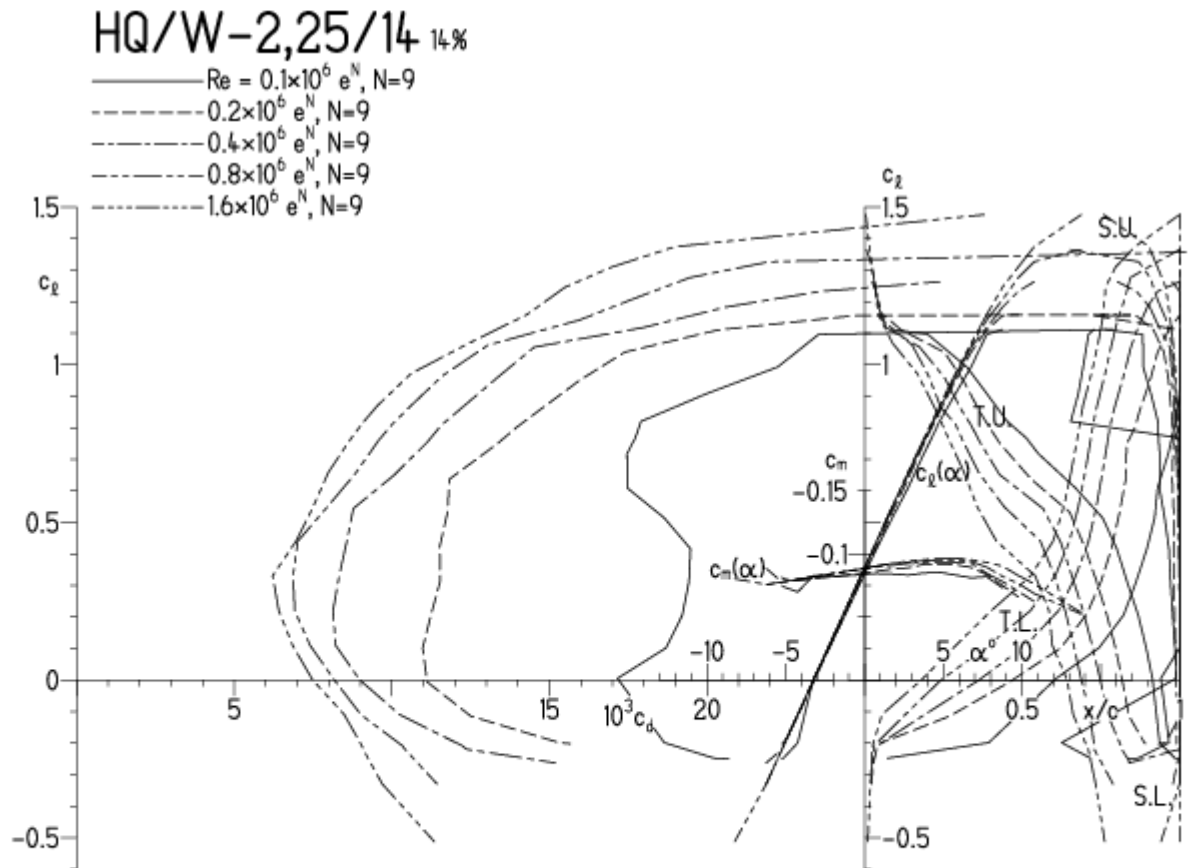


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

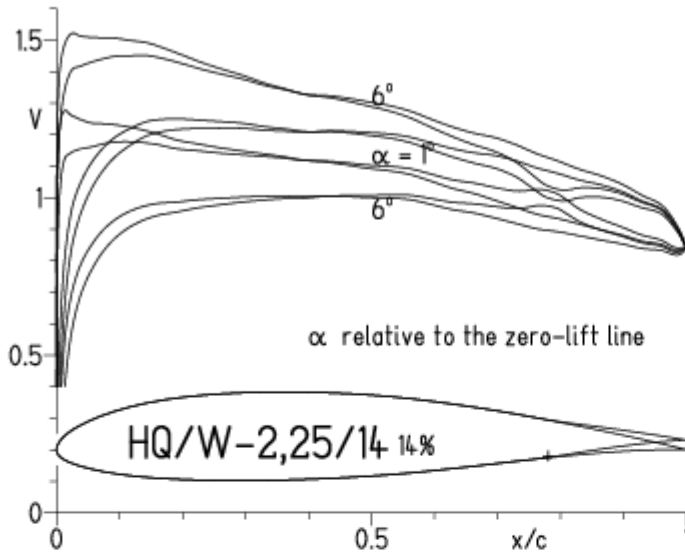
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

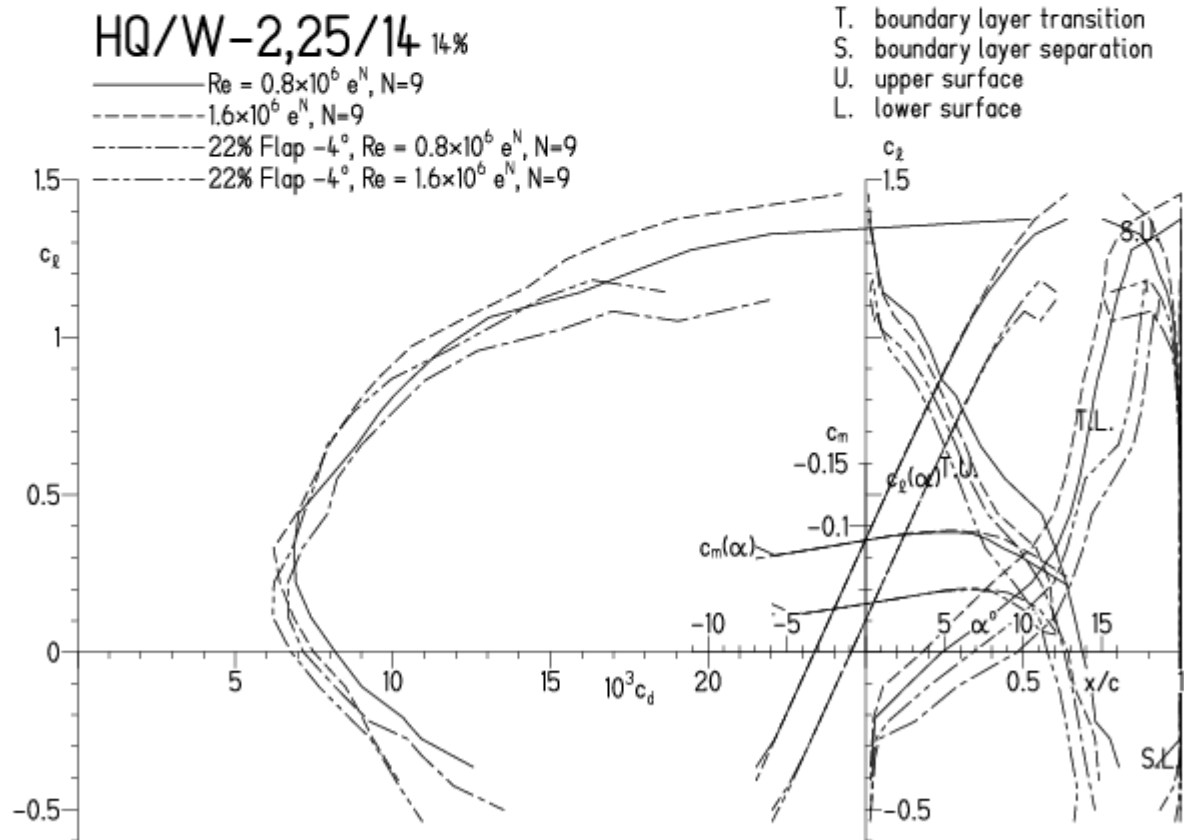


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

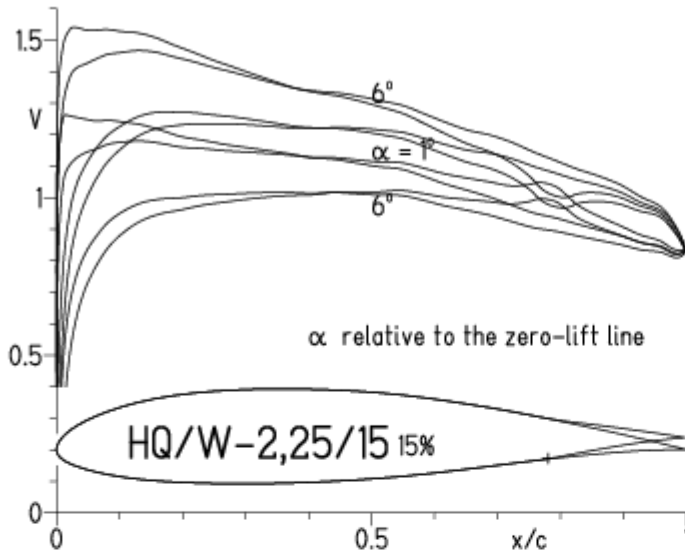


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

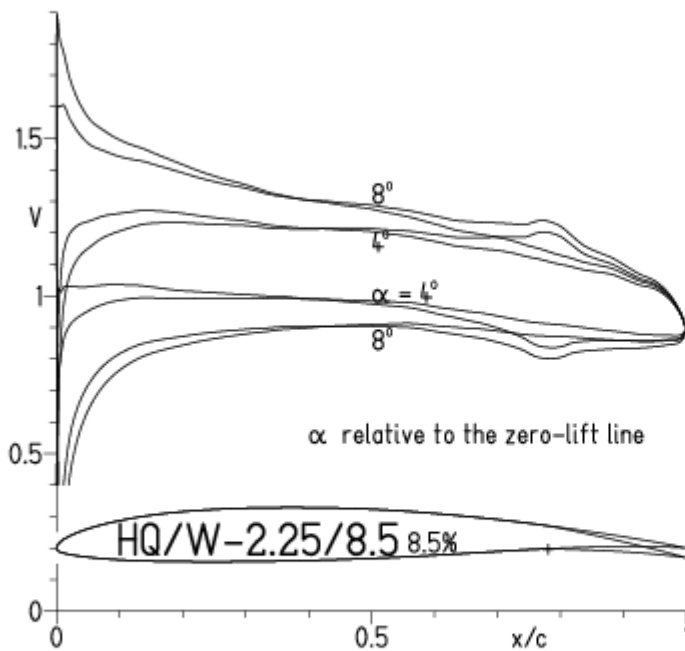
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

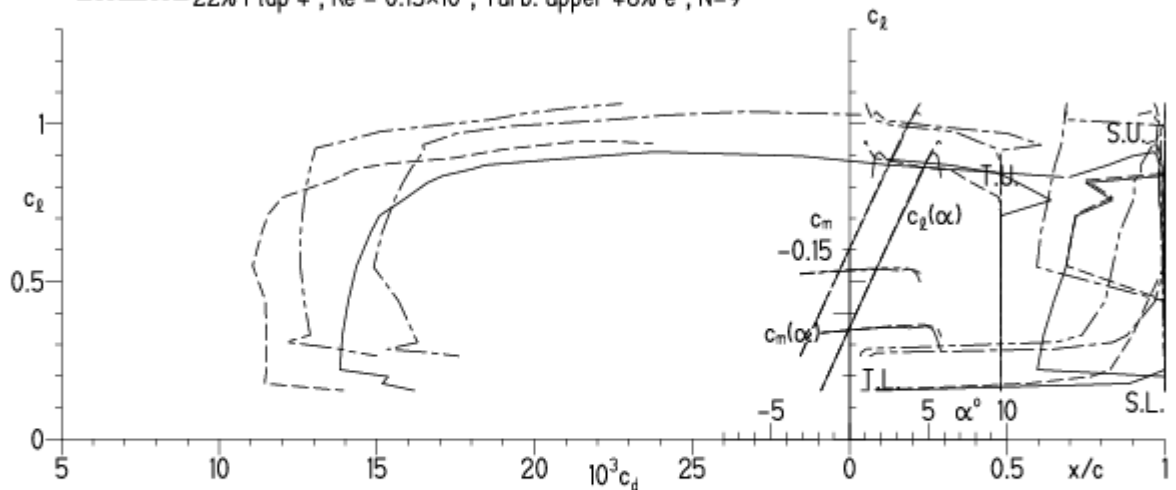


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

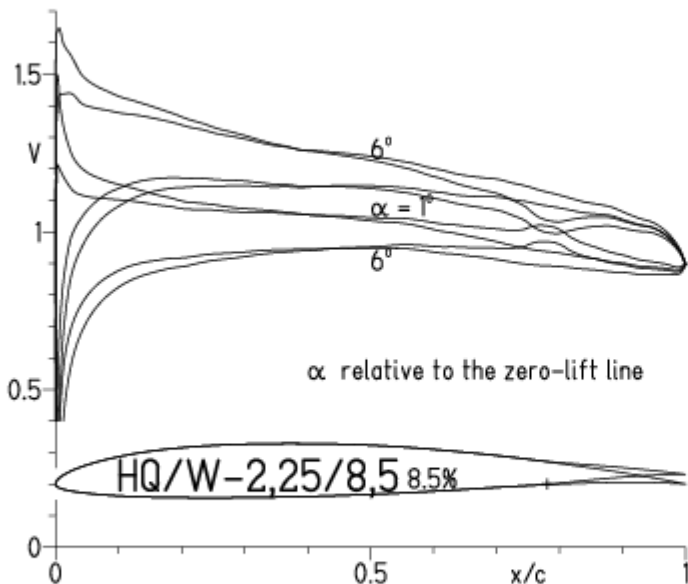
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



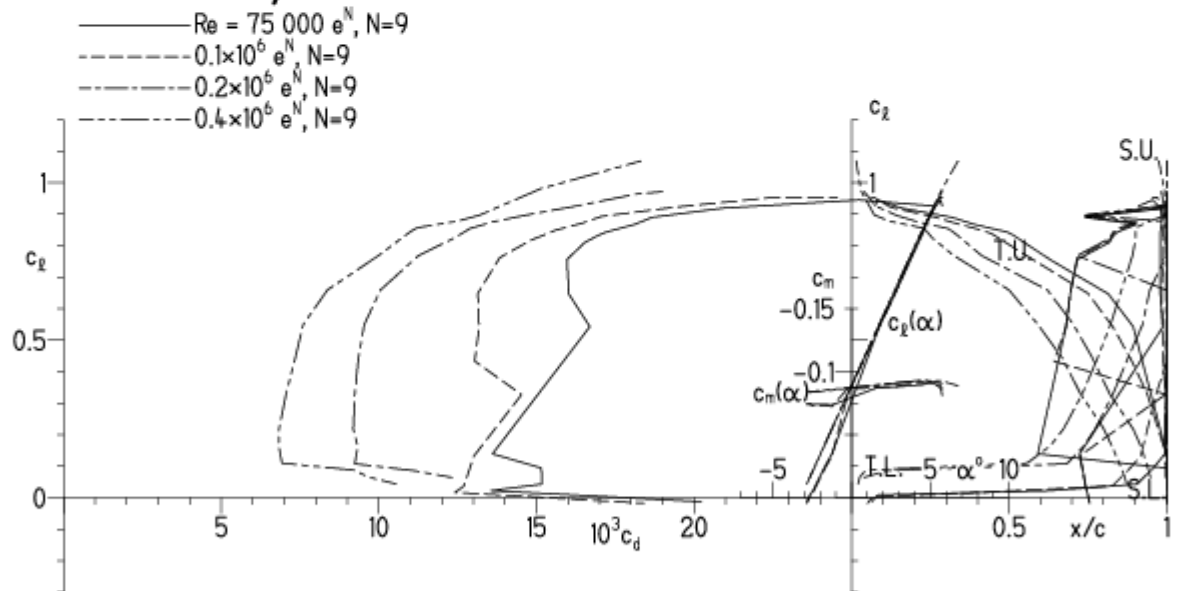
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

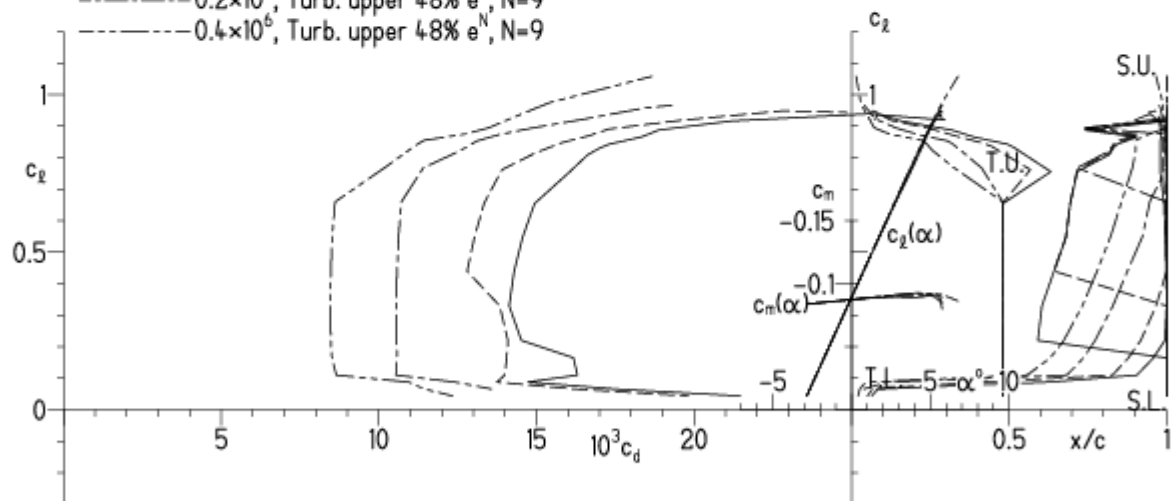
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48

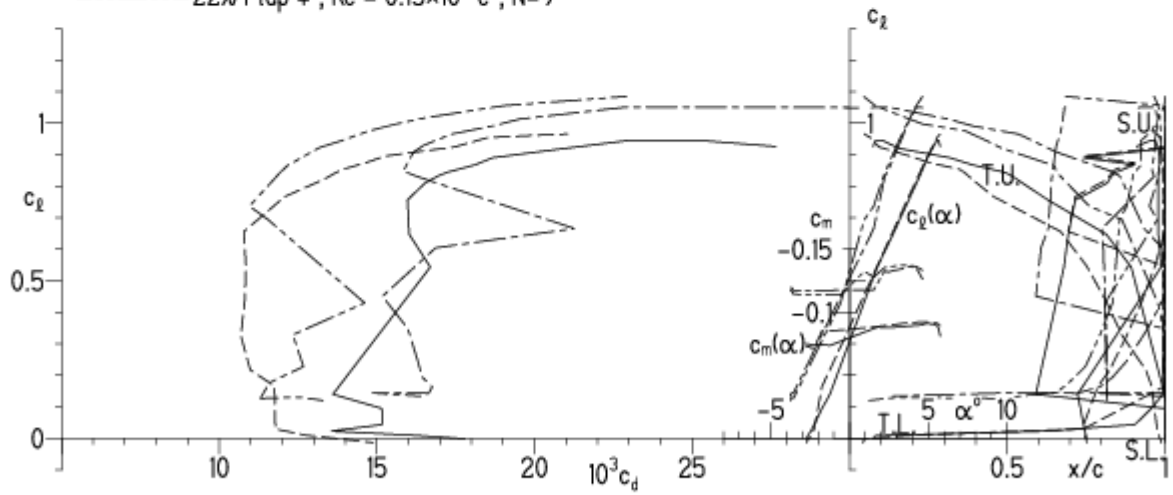


EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

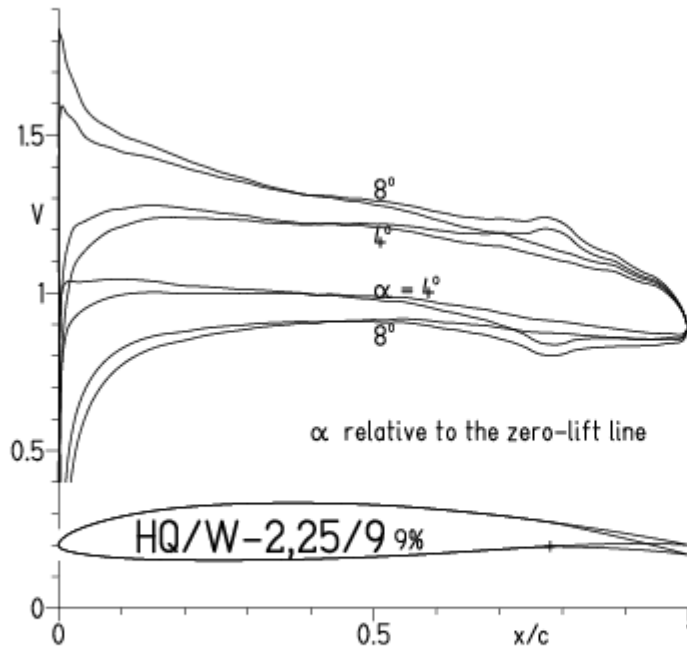
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

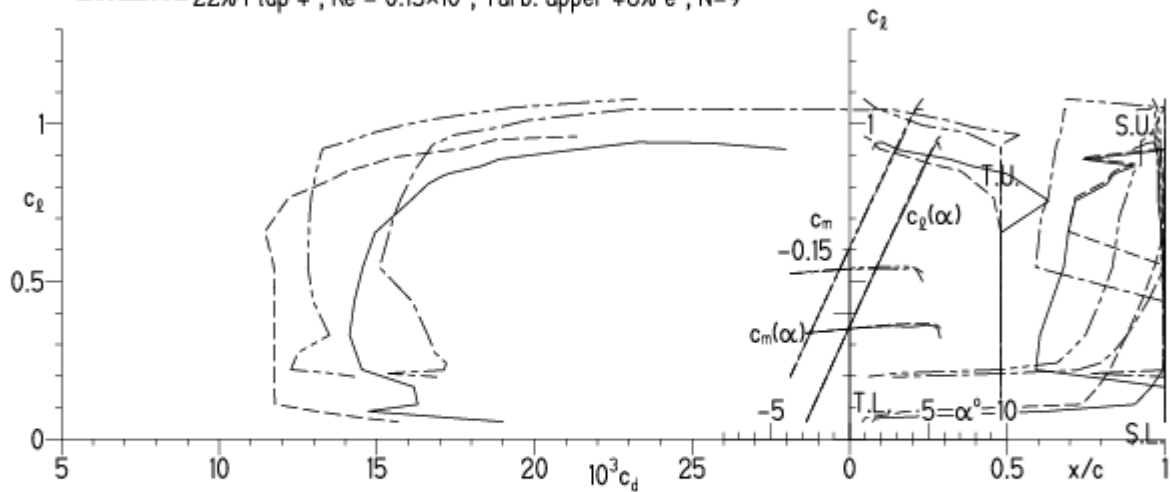


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

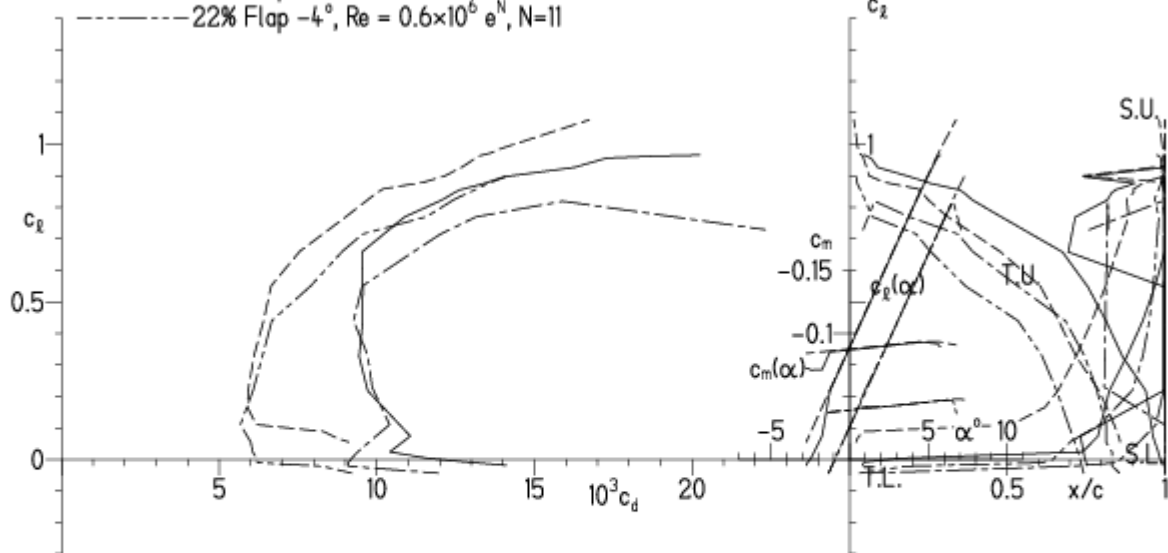
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



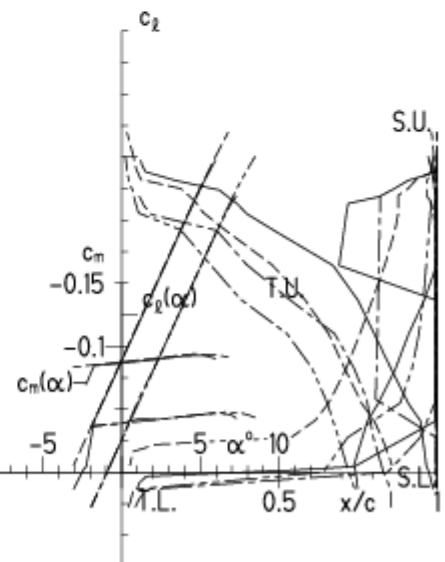
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

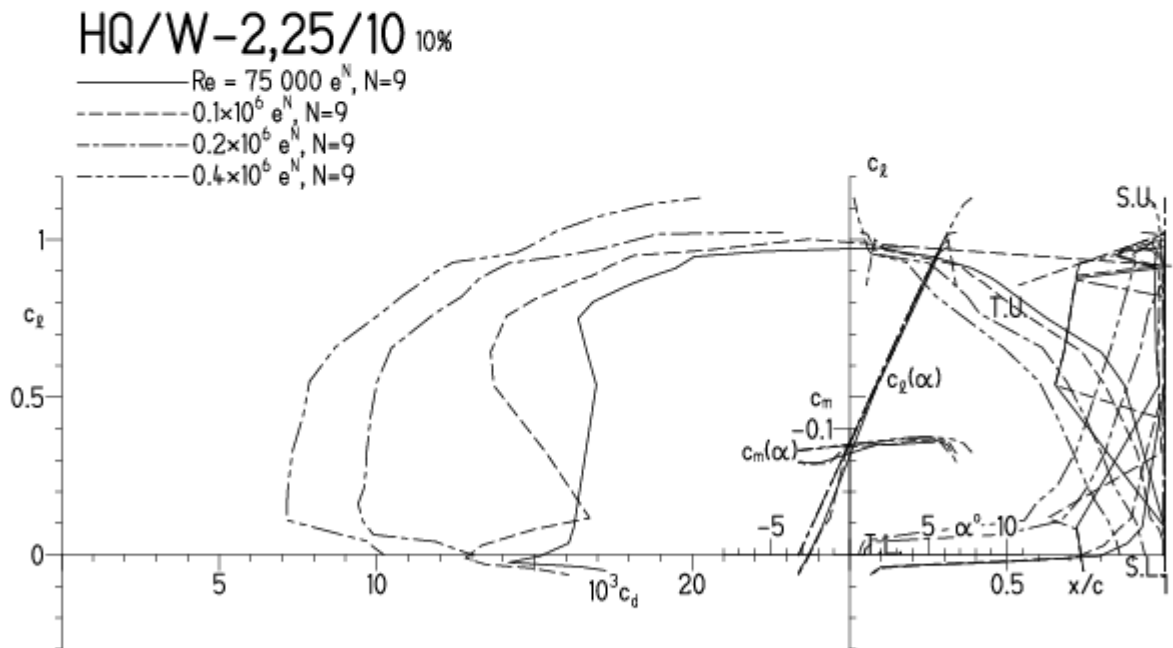


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

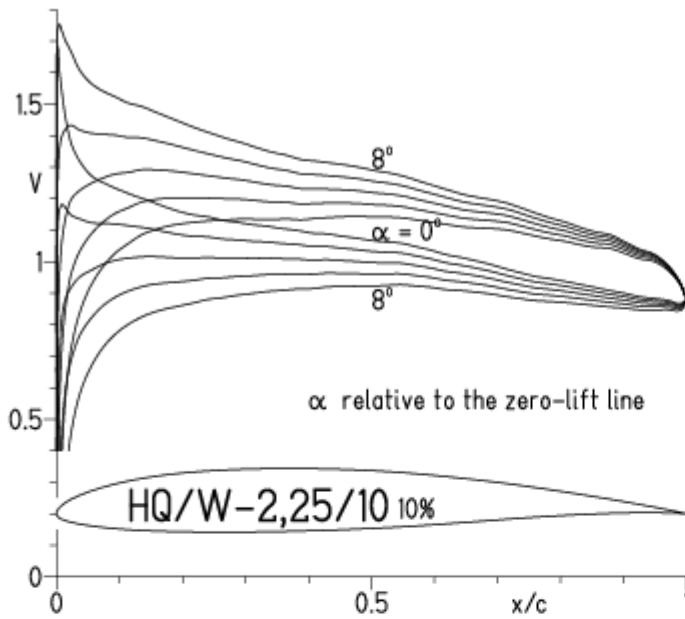


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

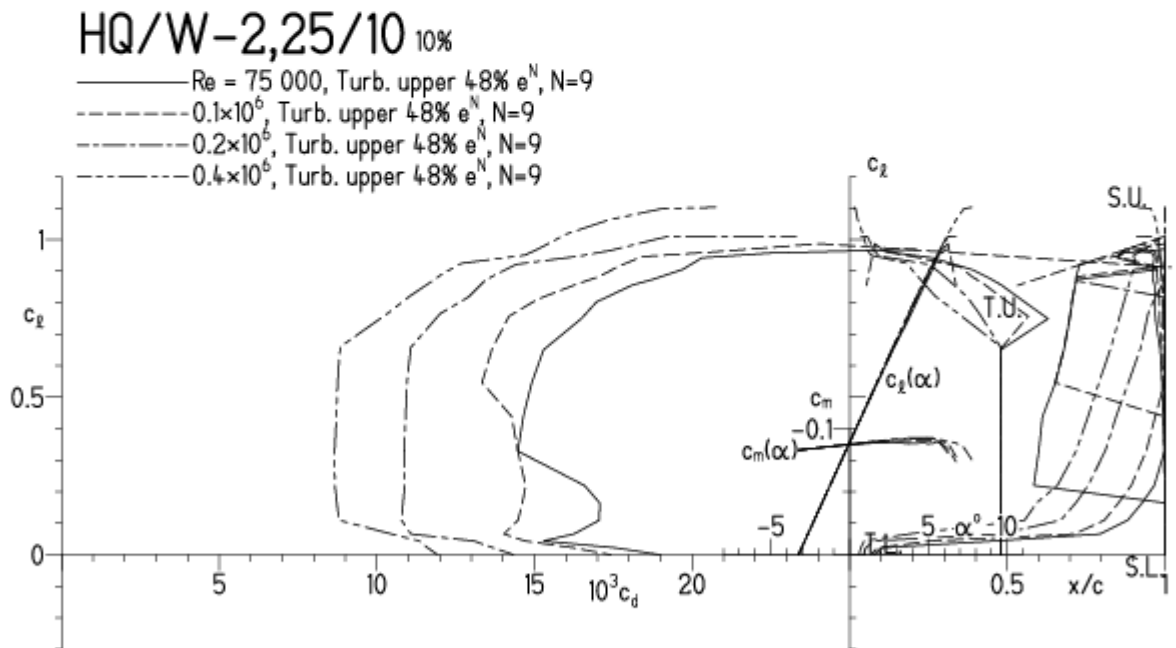


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

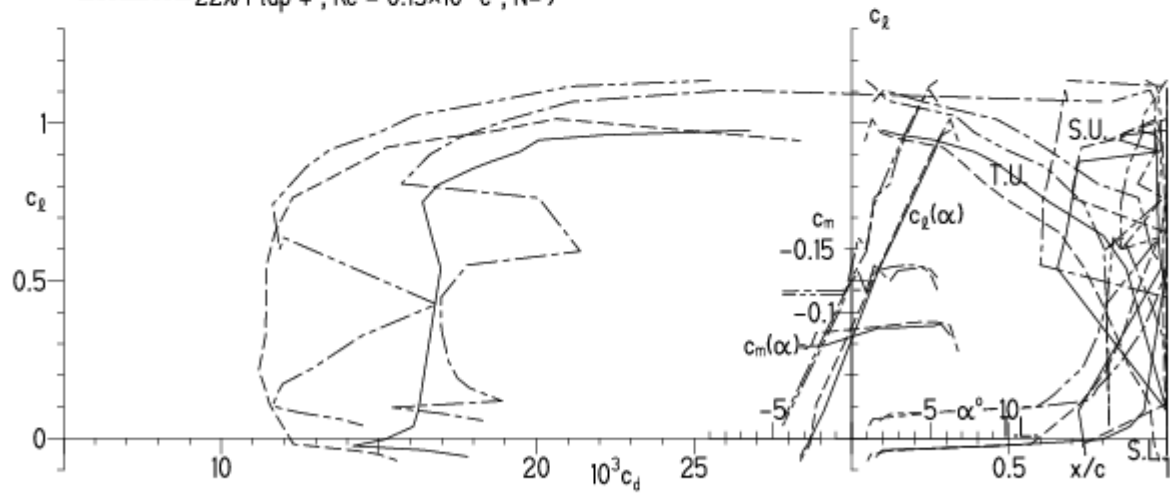


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

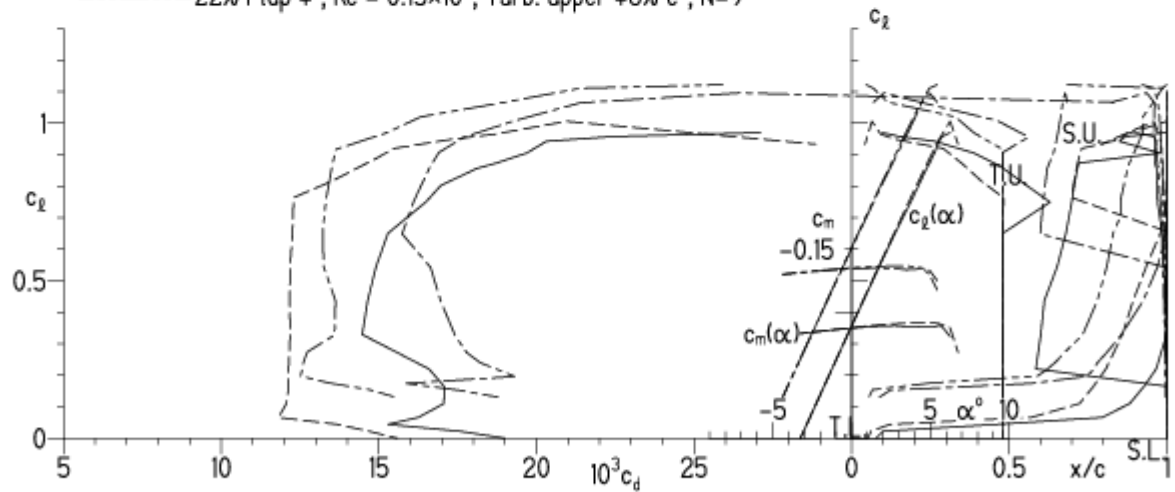


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

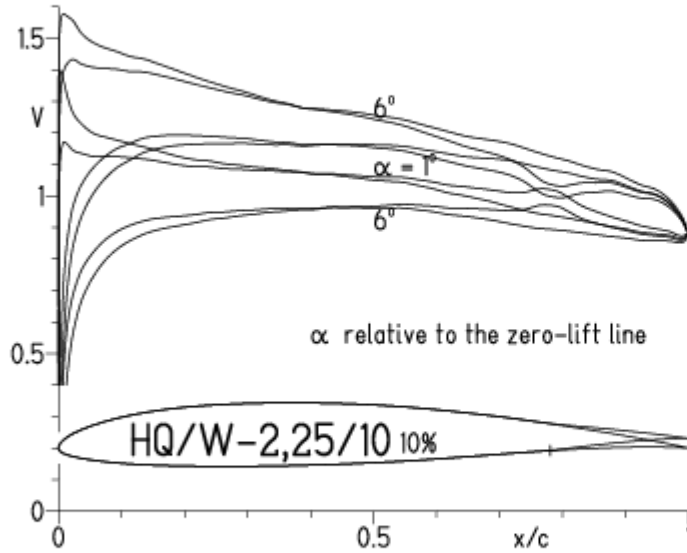
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

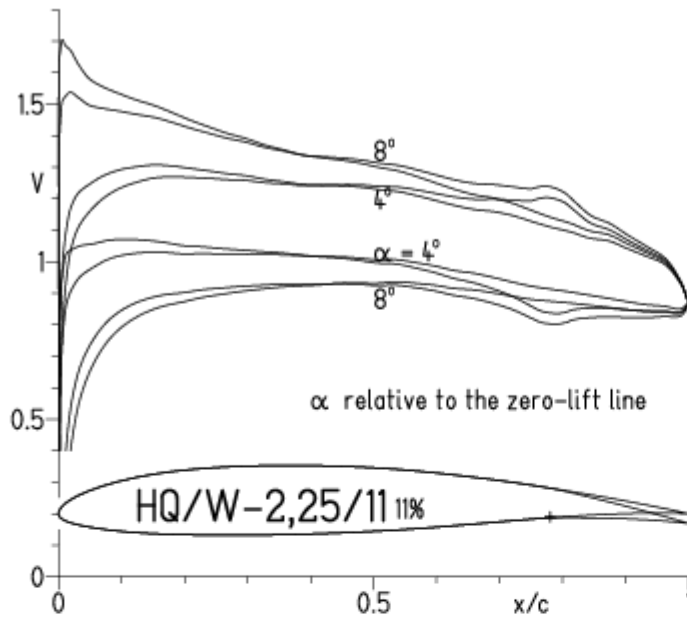
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

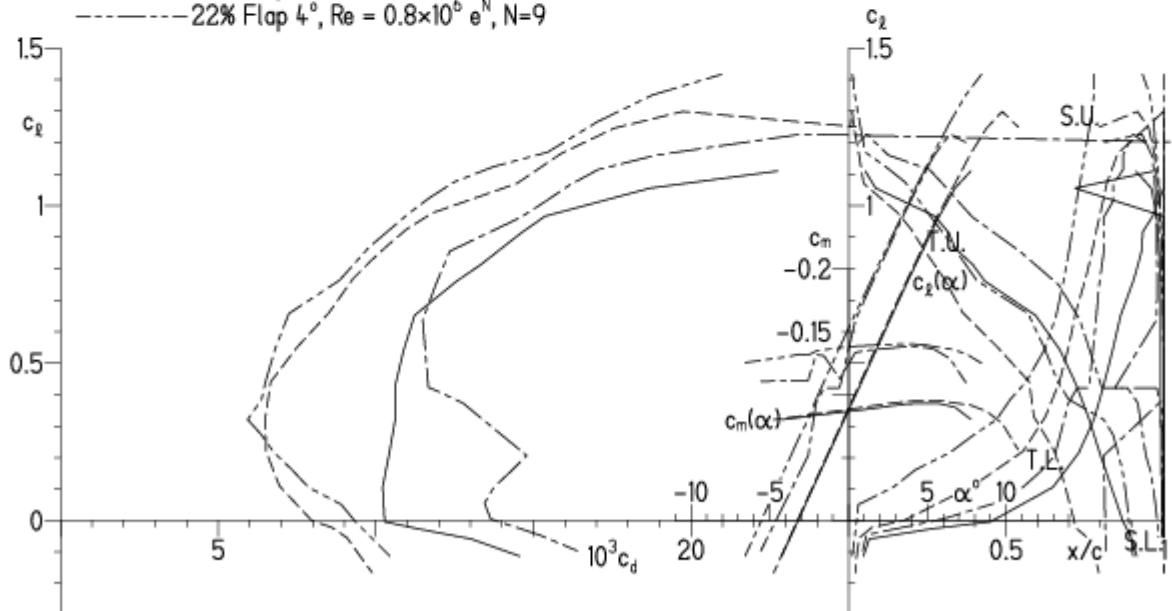


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

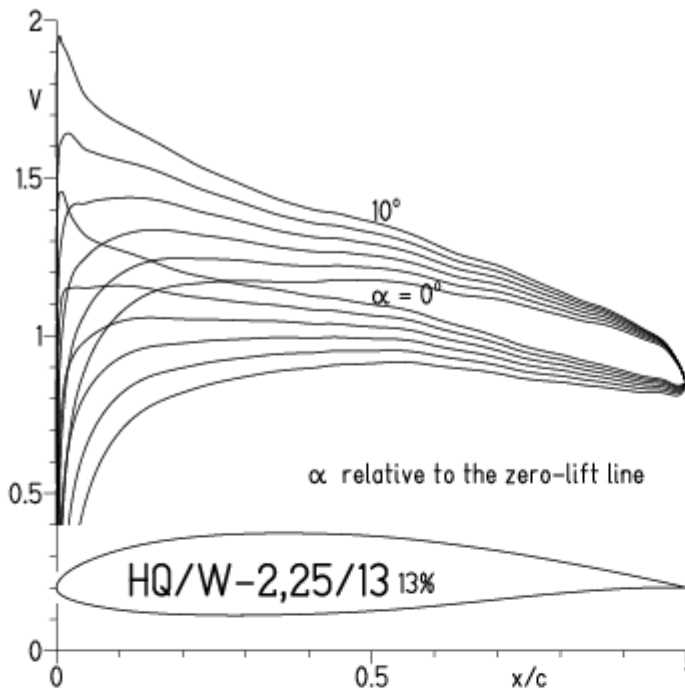
HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

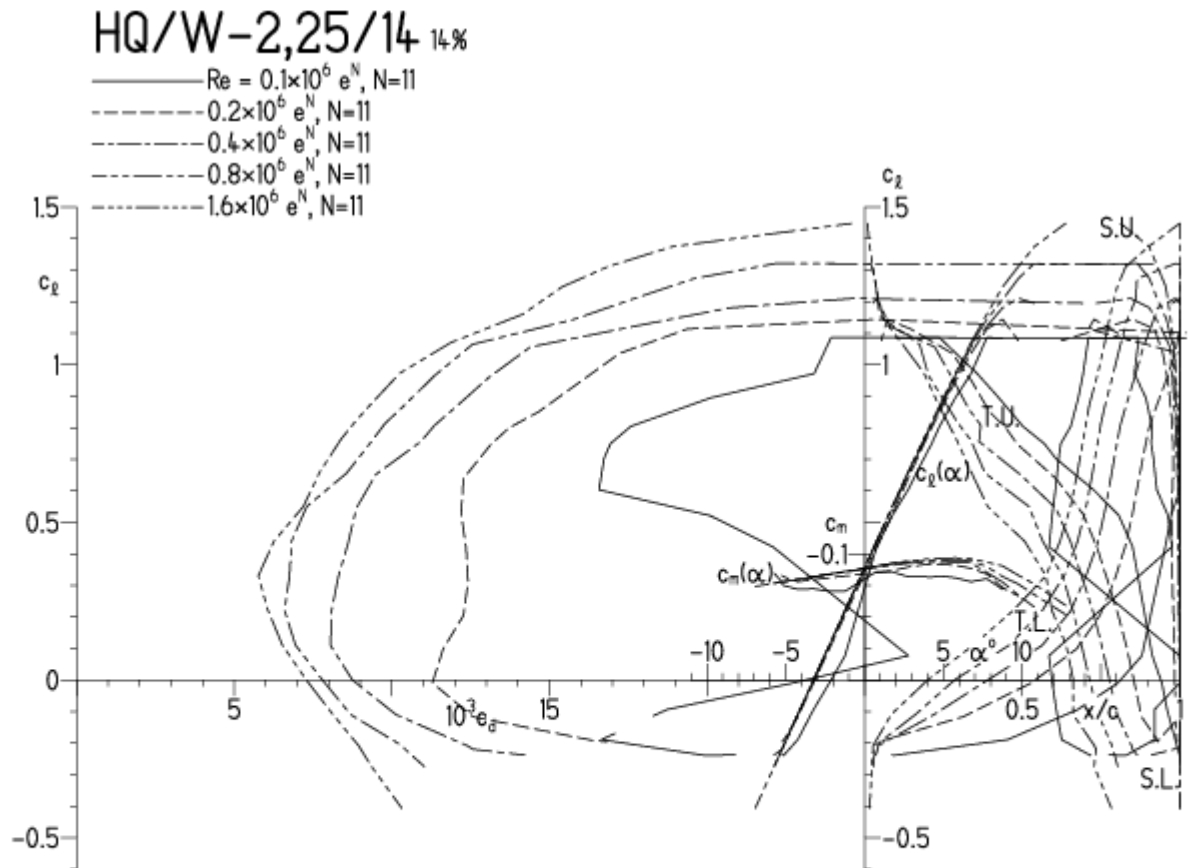


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

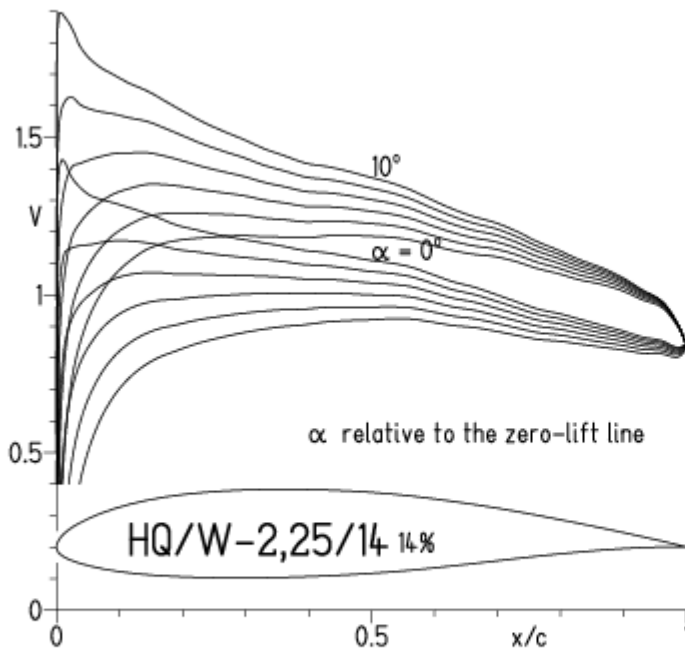


EPPLER 2005 V. 8.

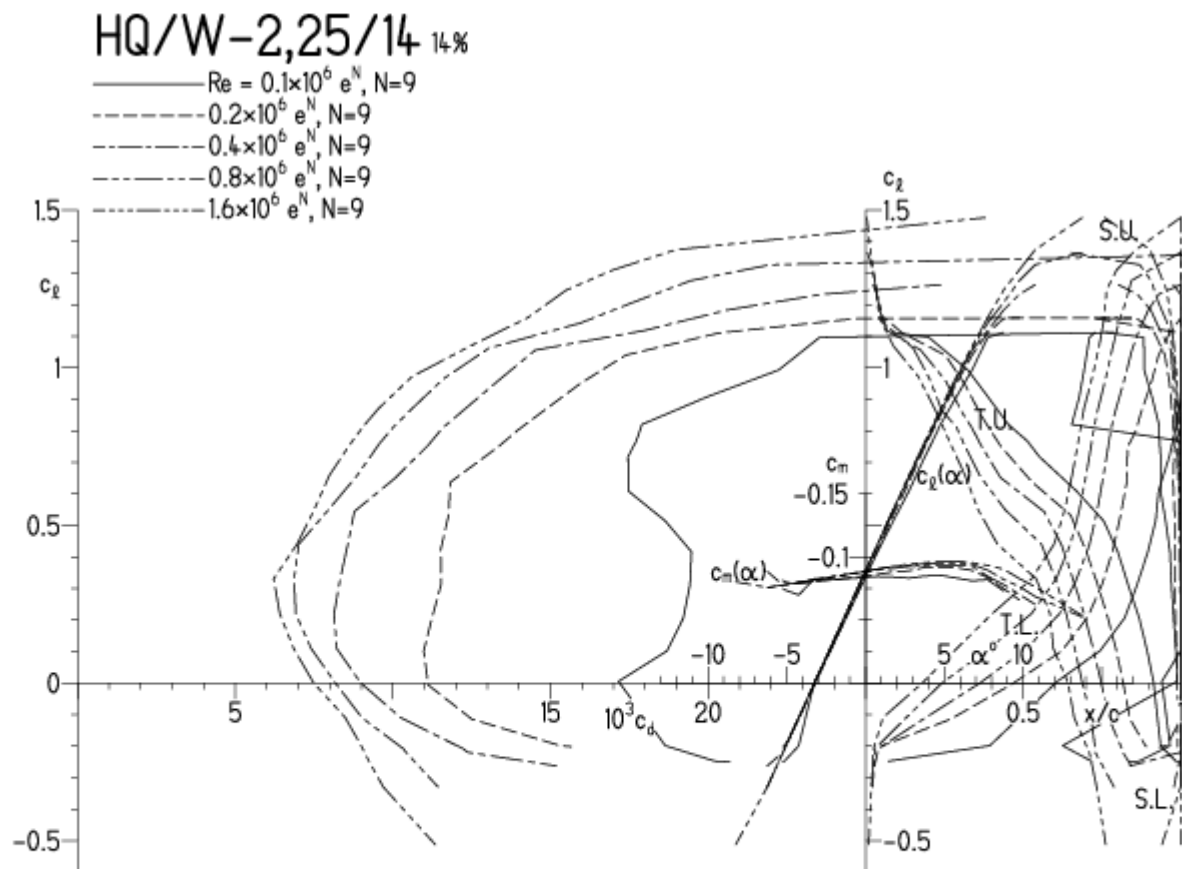


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

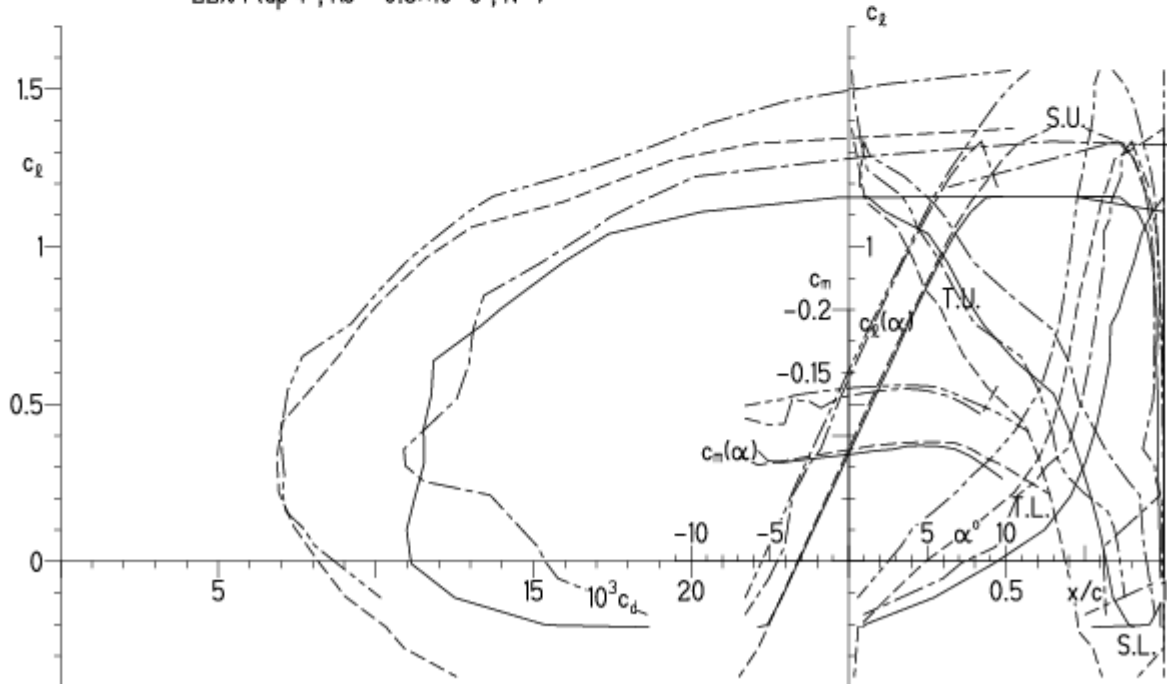


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

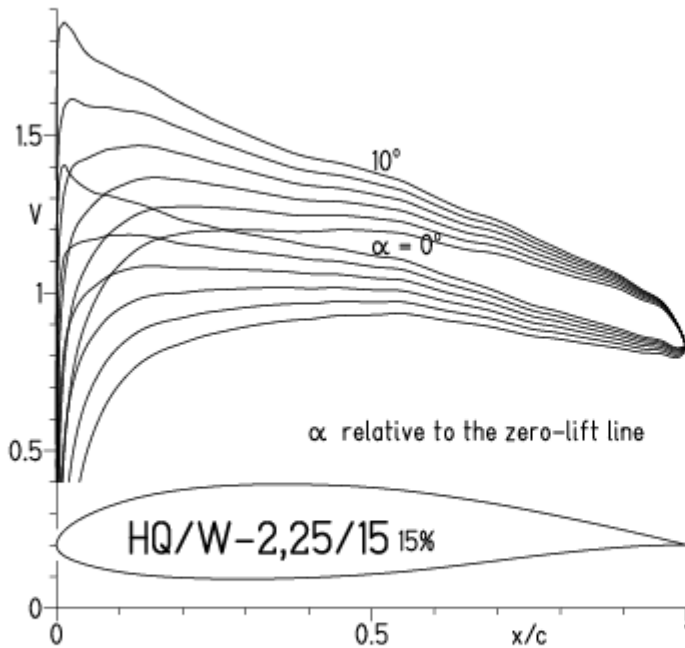


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

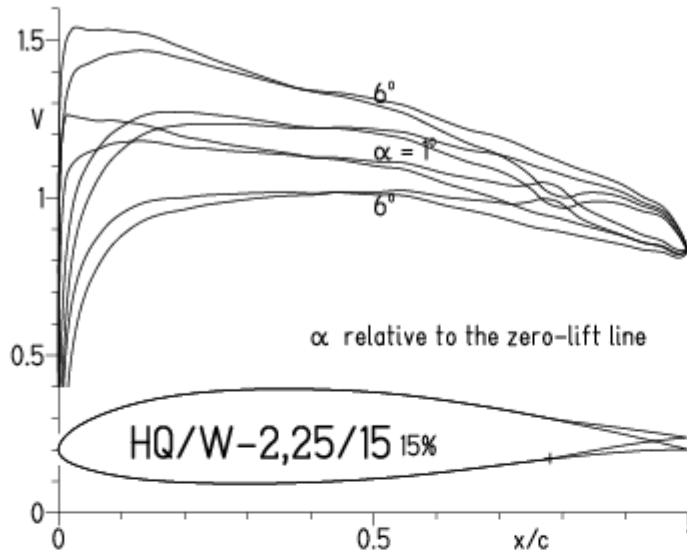


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



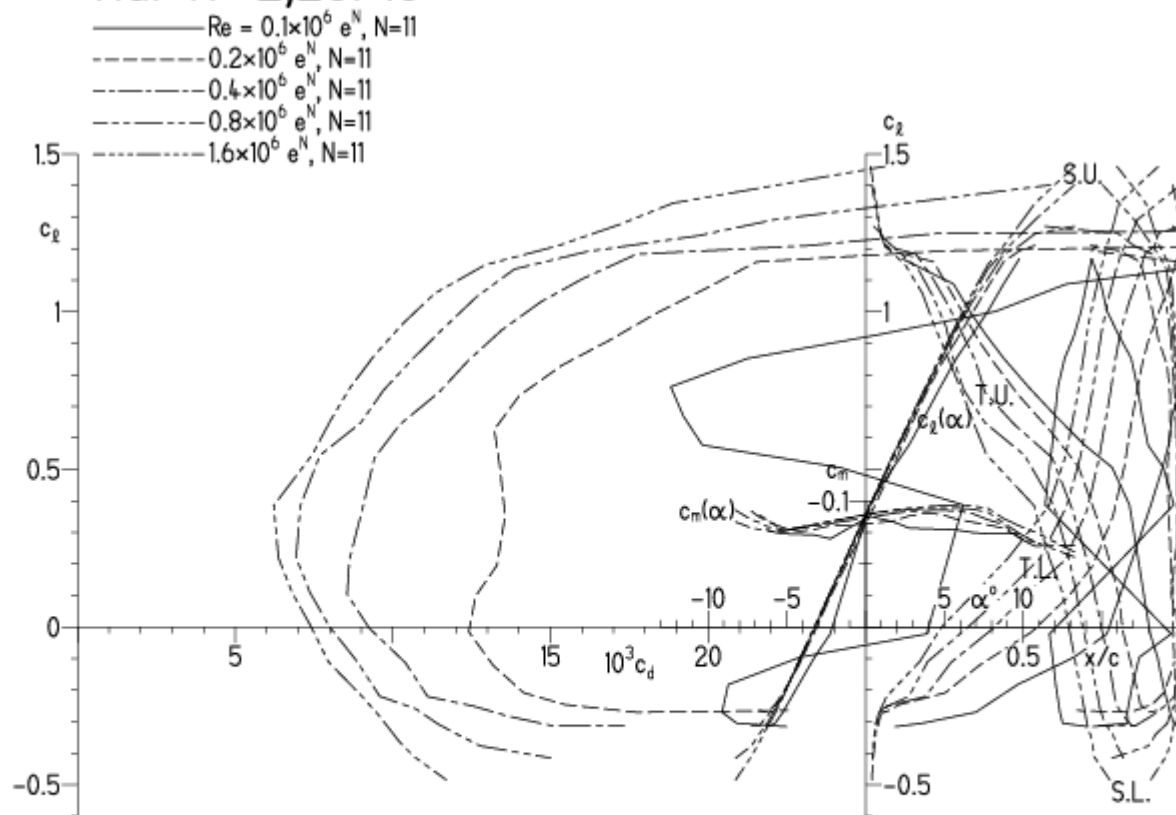
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

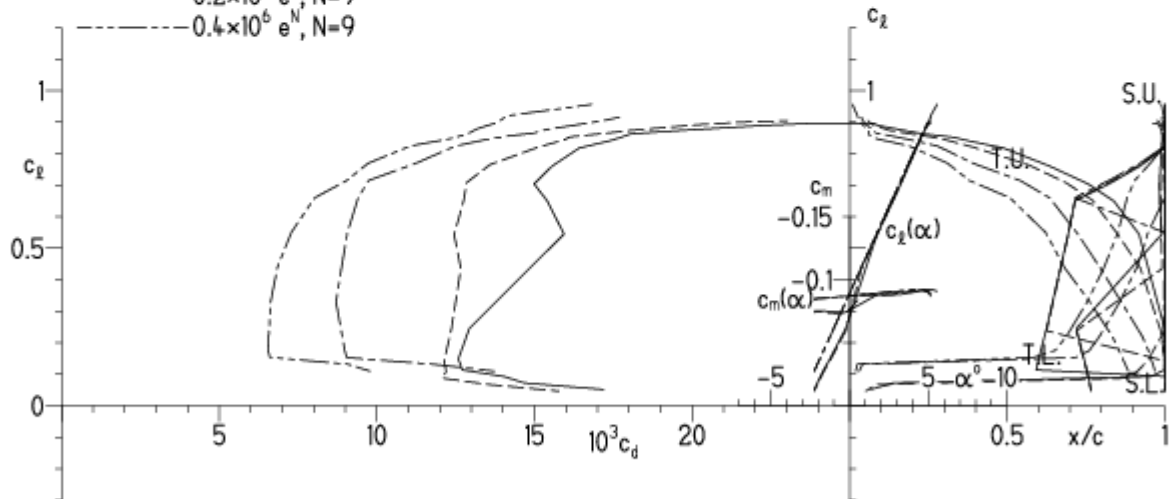
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

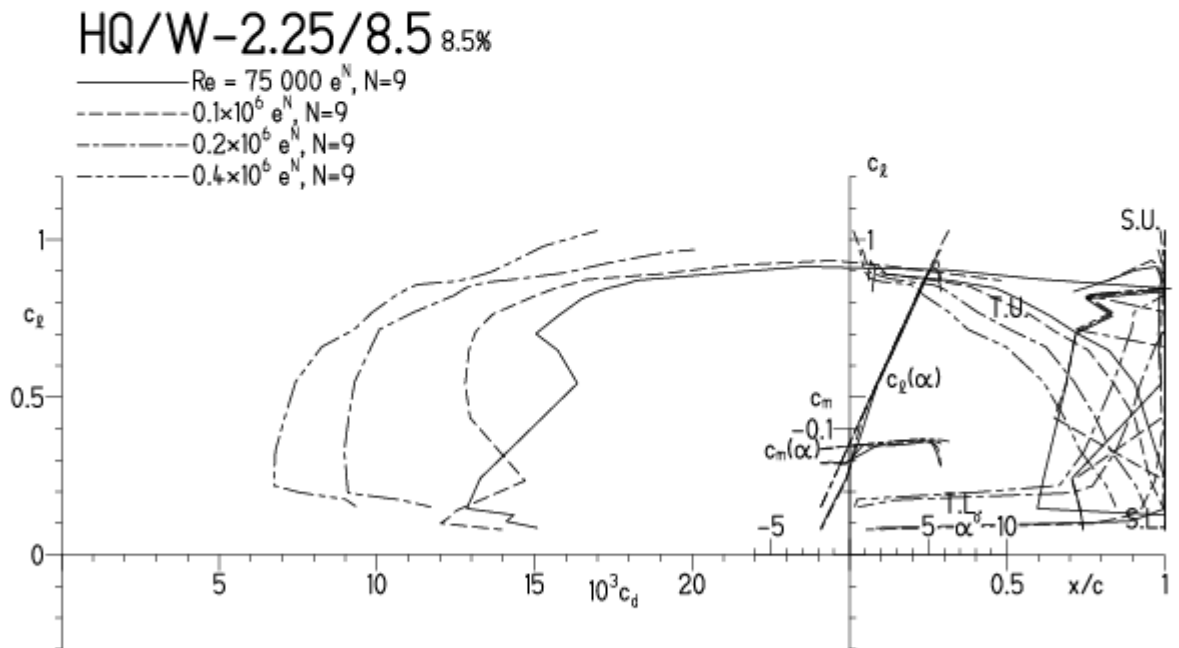


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

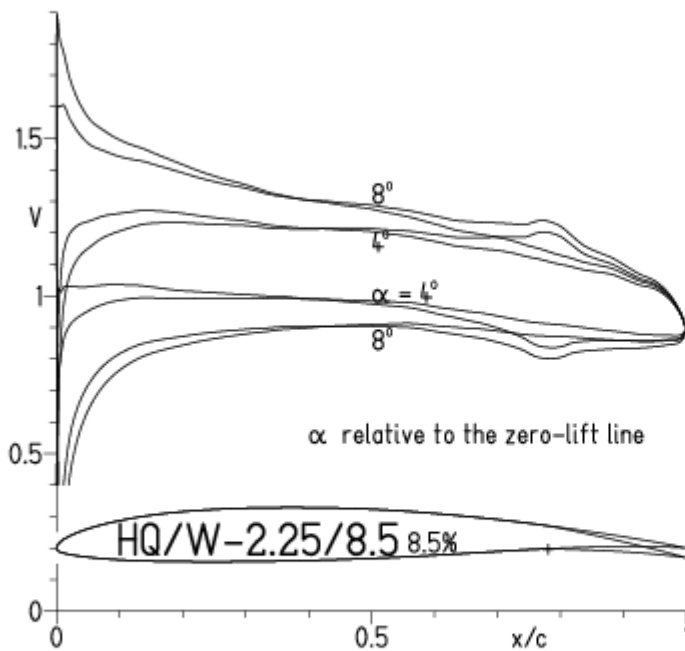
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

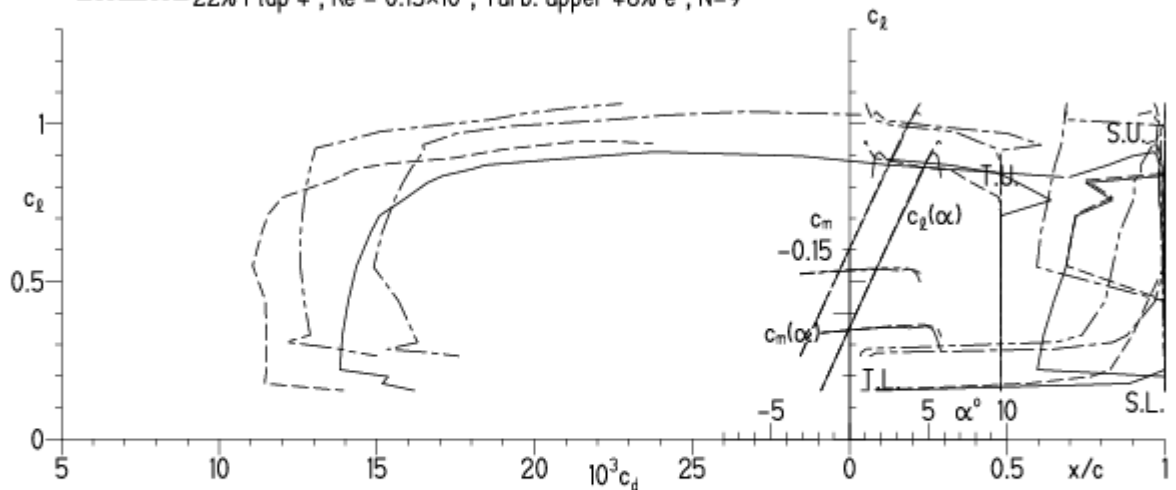


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

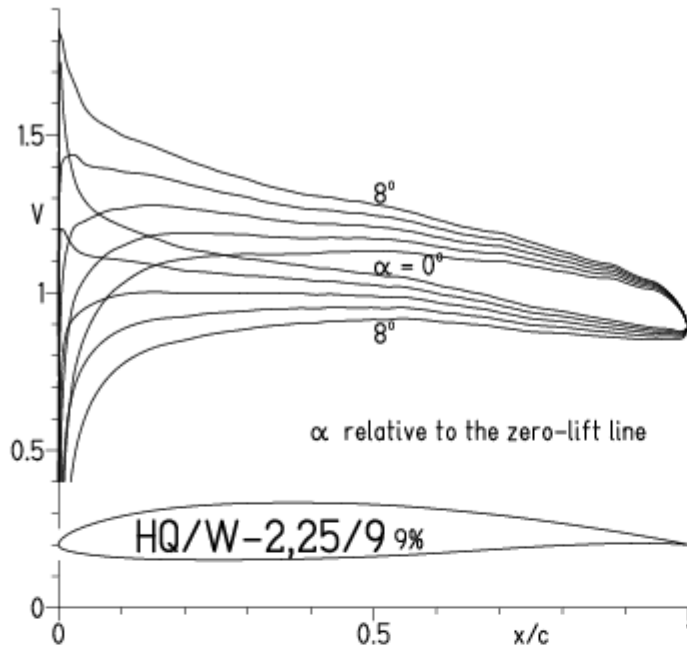


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

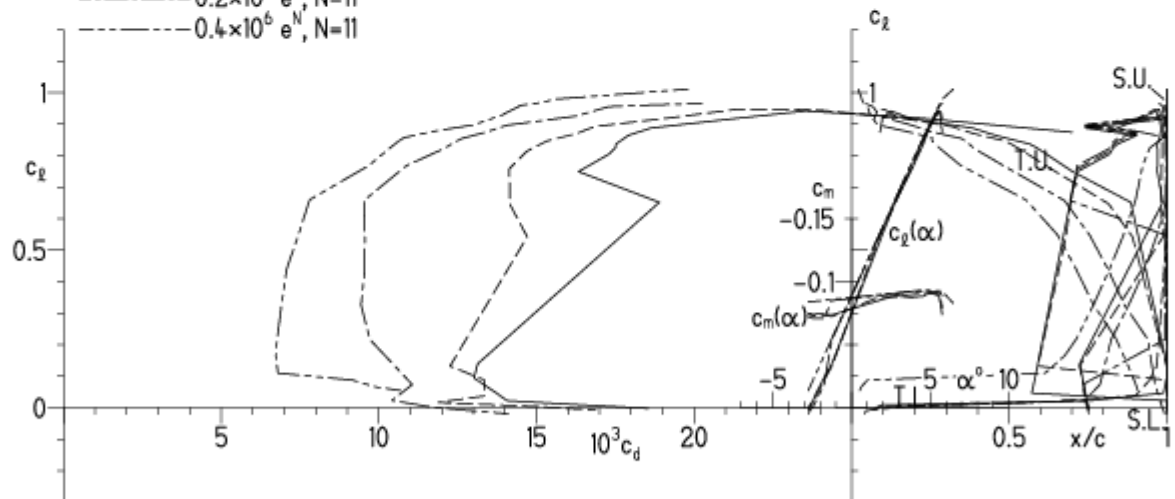
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

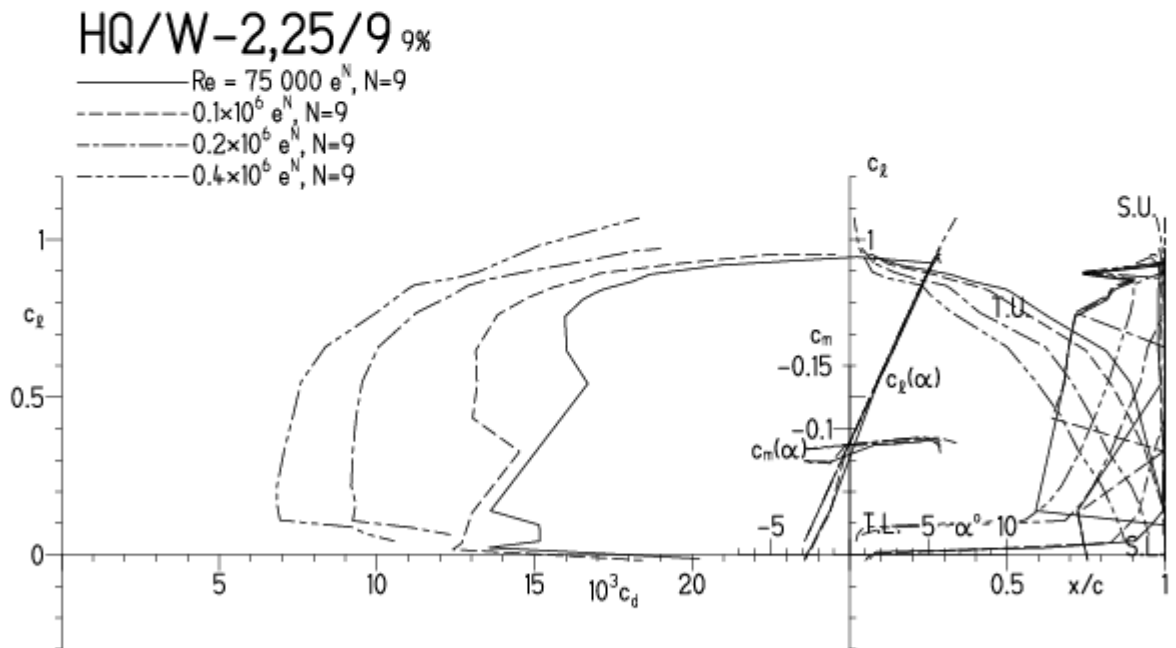


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

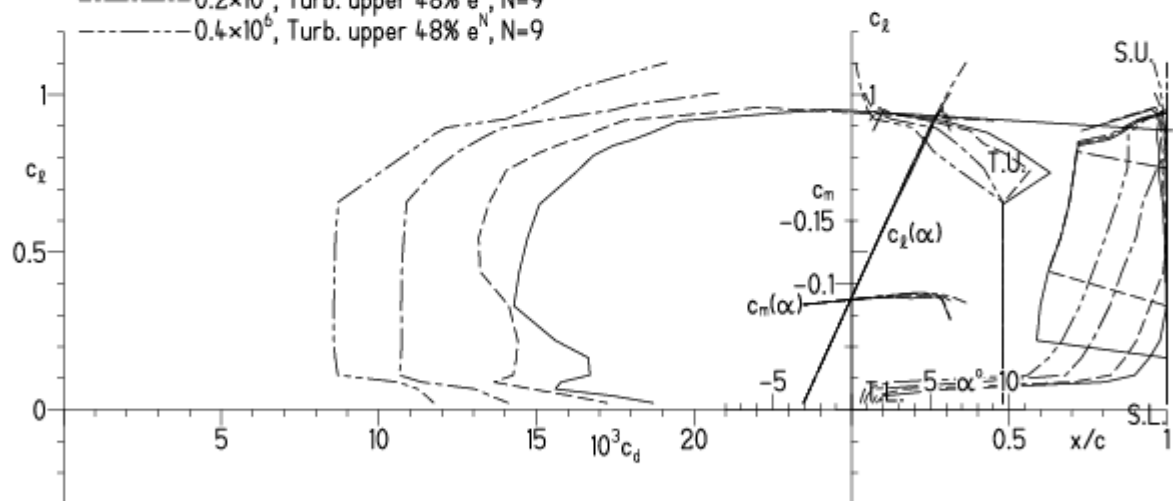
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

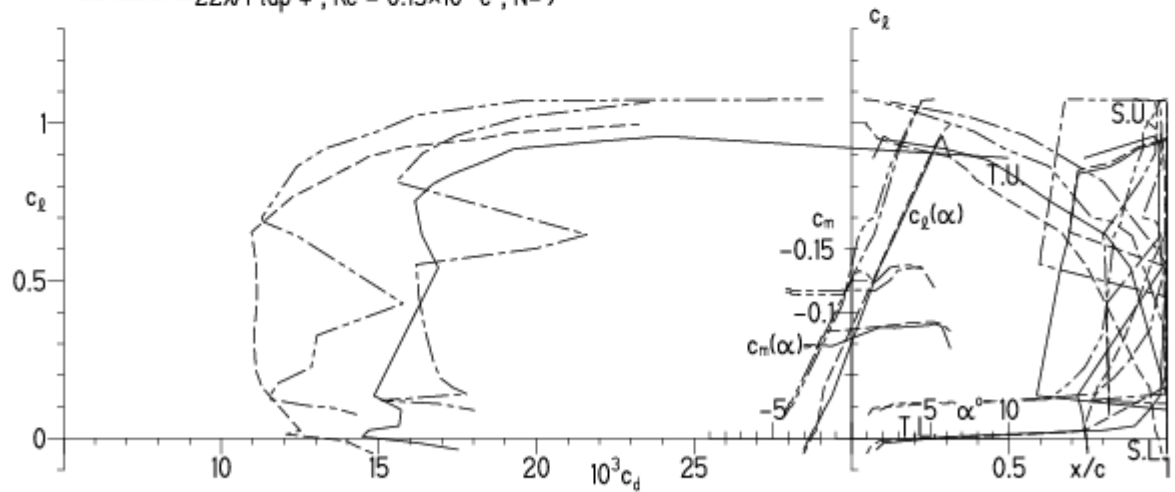


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

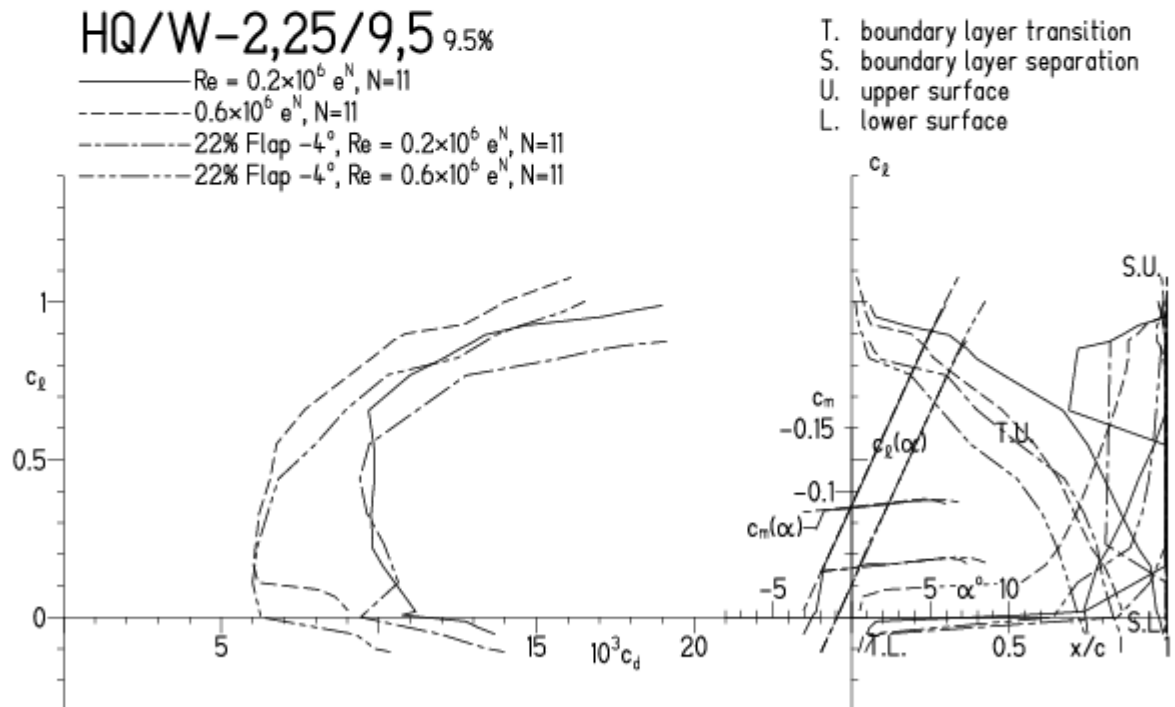


HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

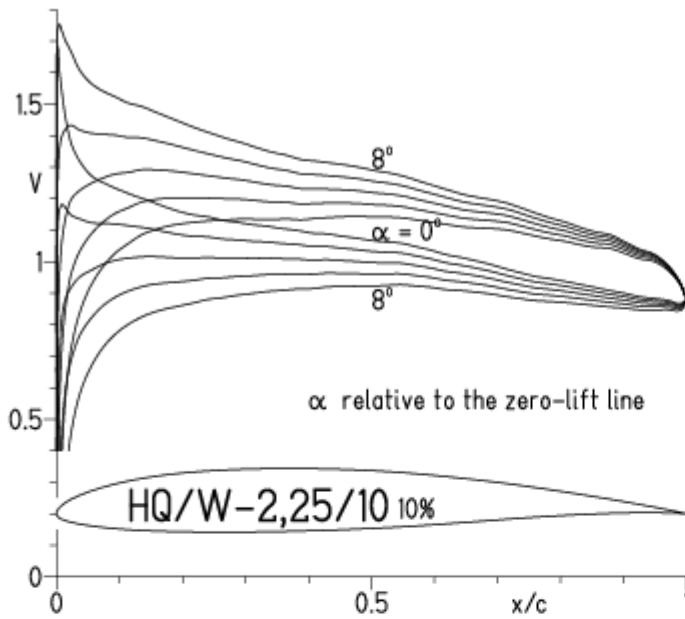


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

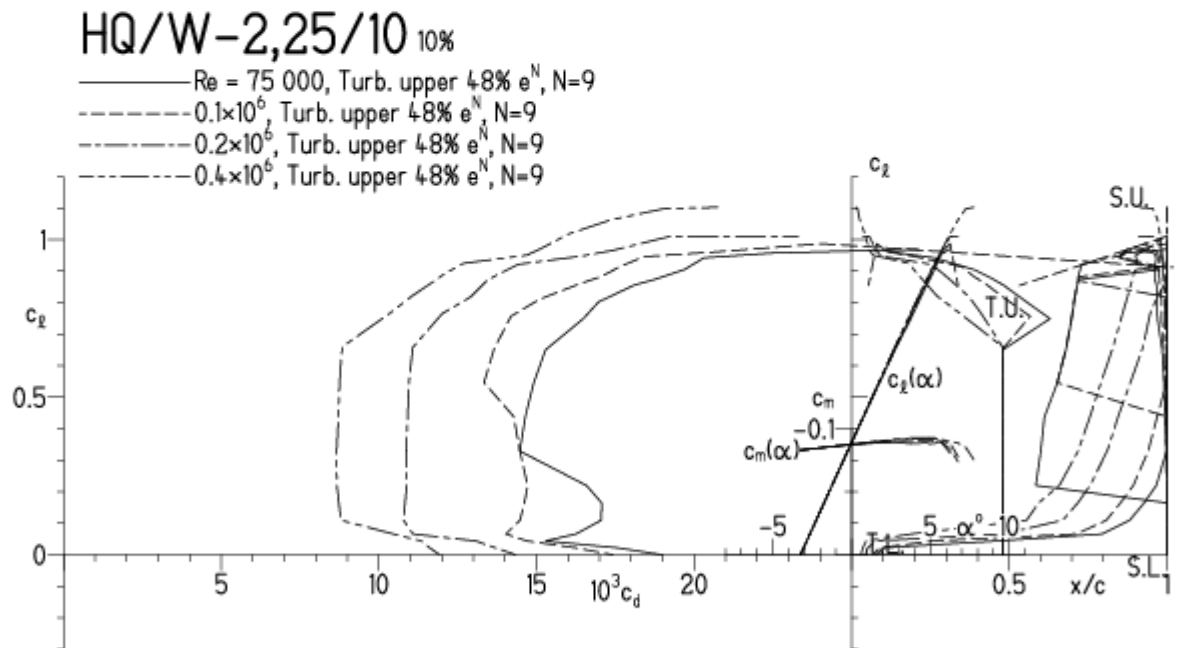


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

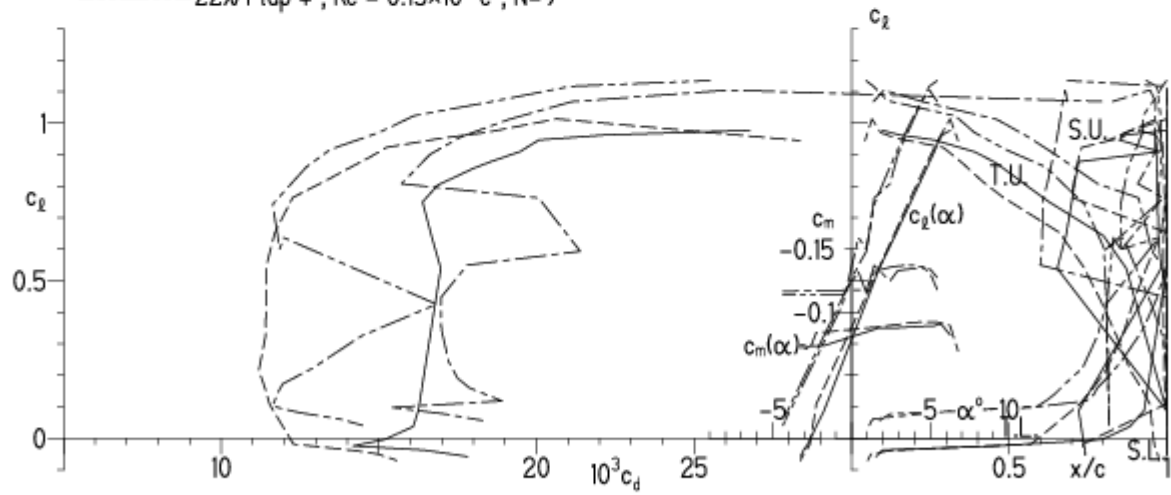


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

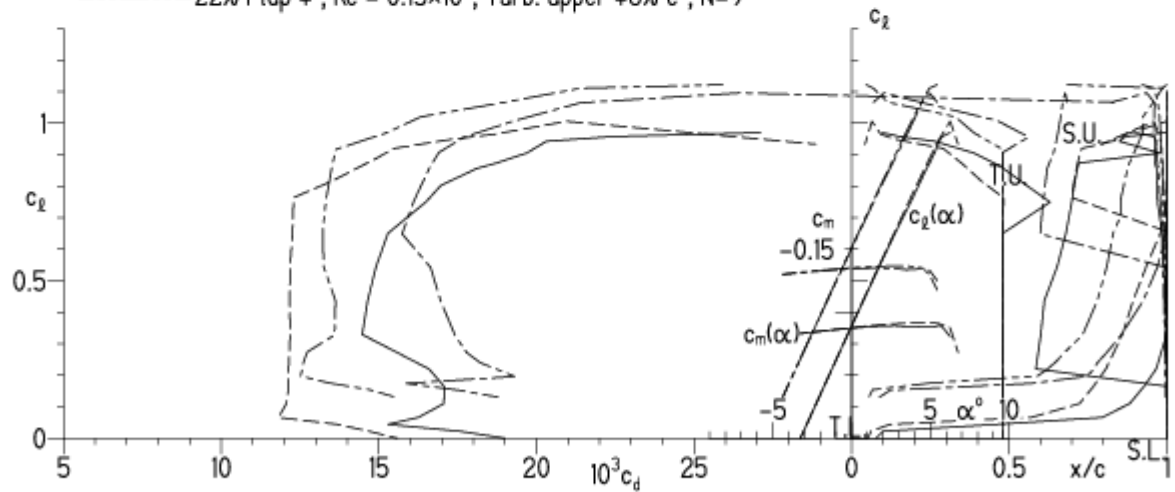


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

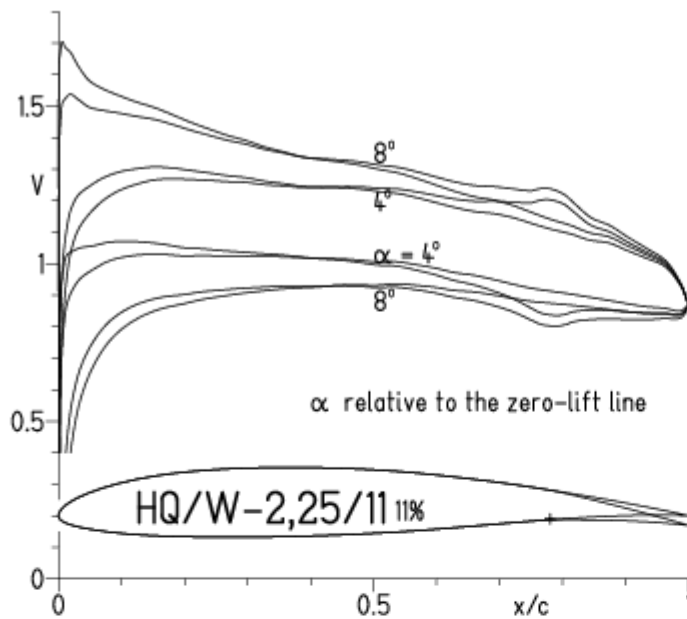
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

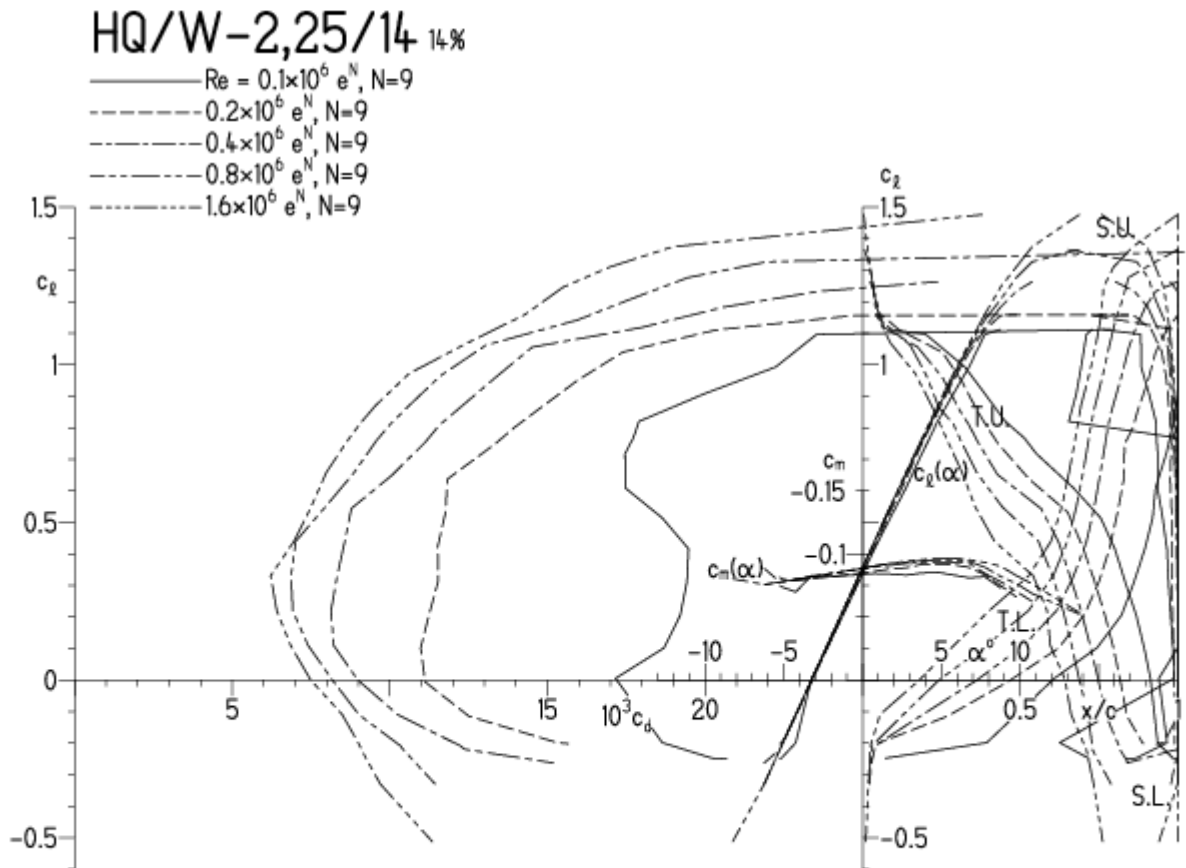


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

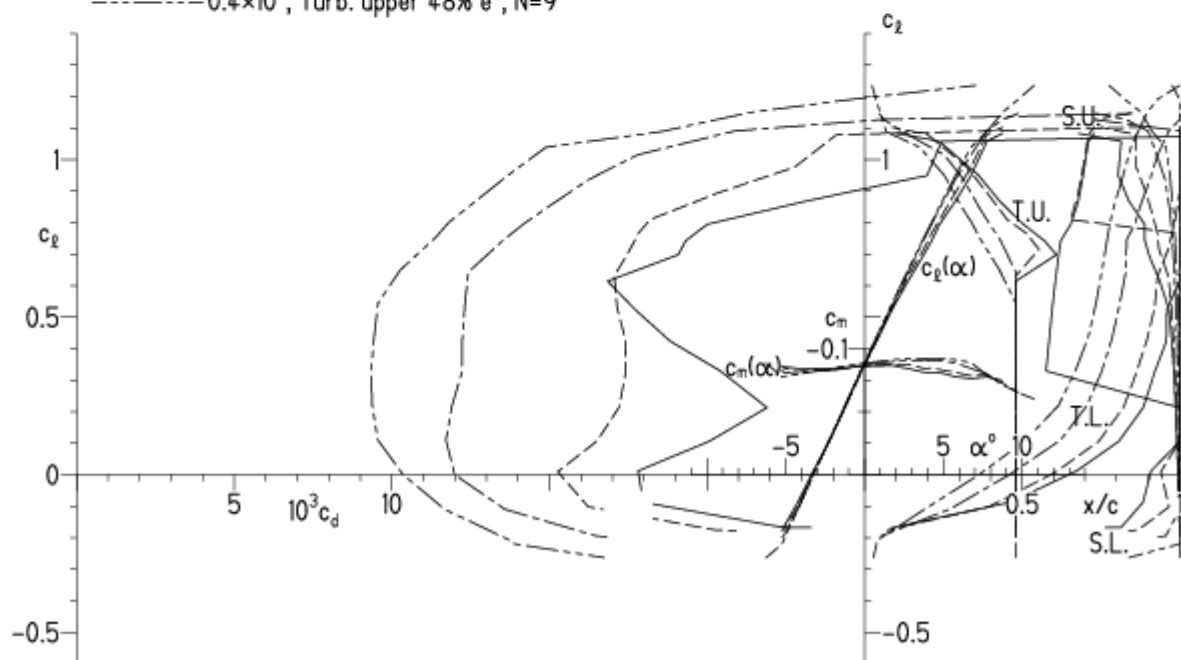
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

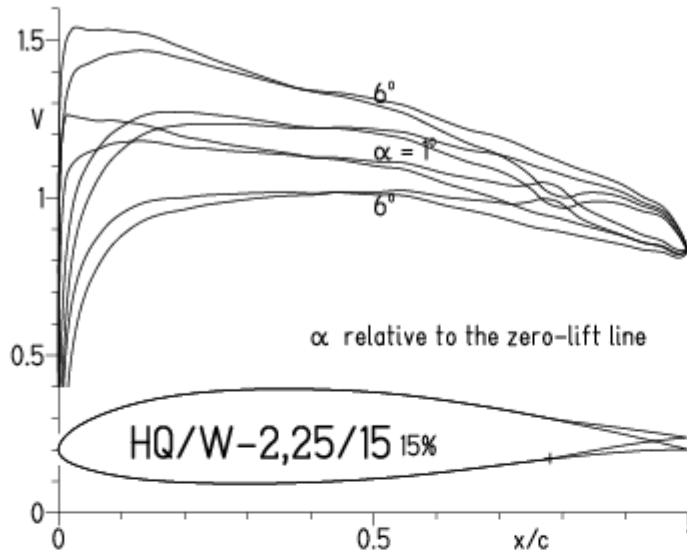


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



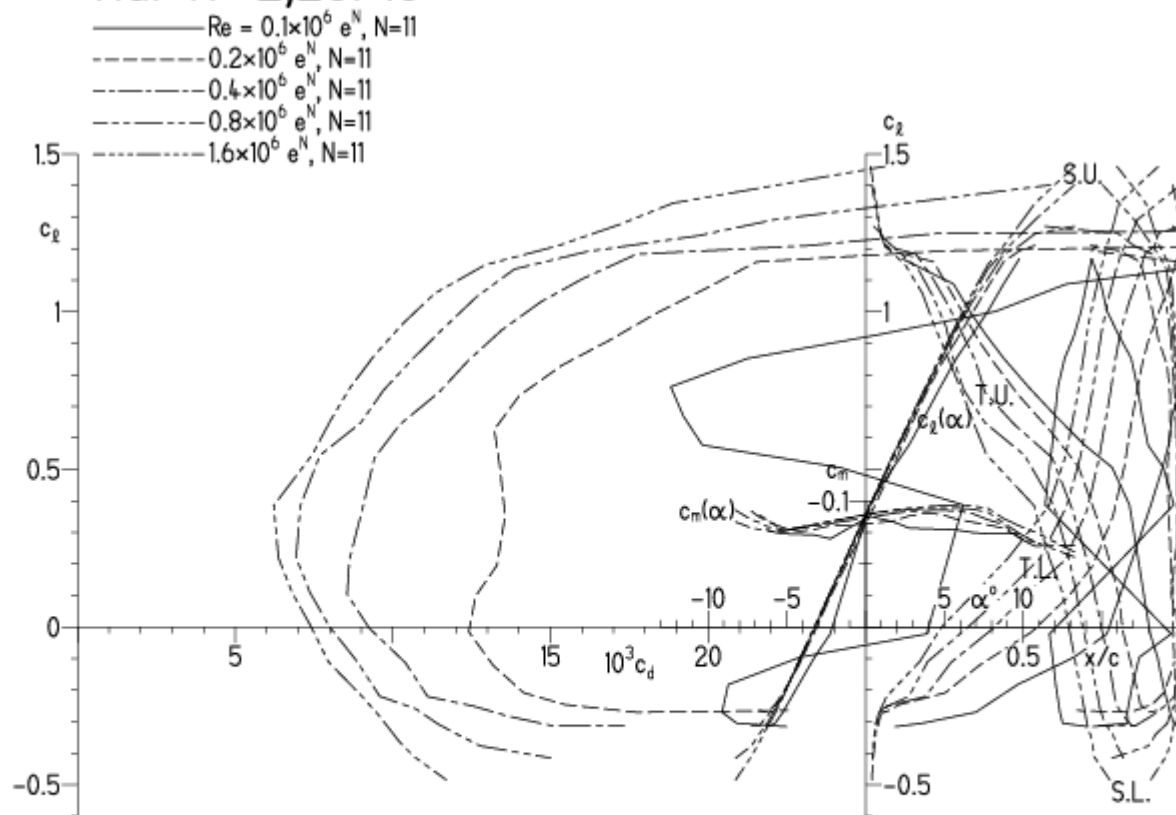
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

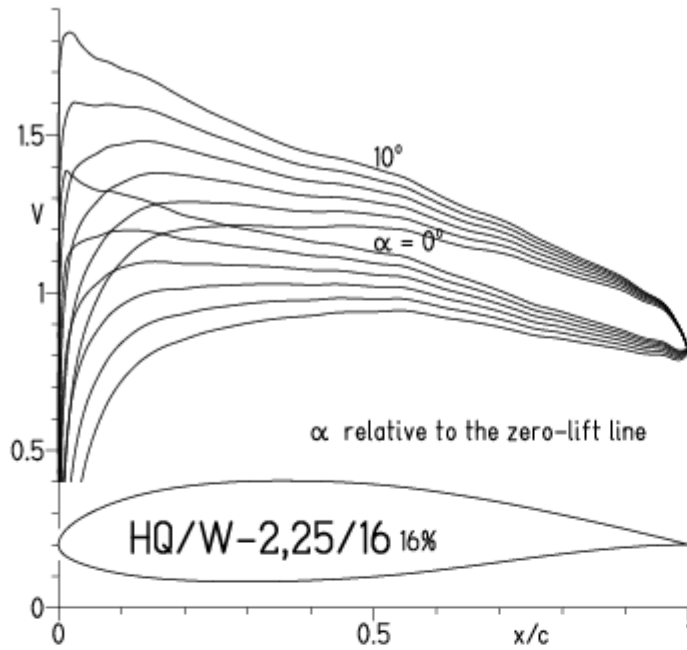
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

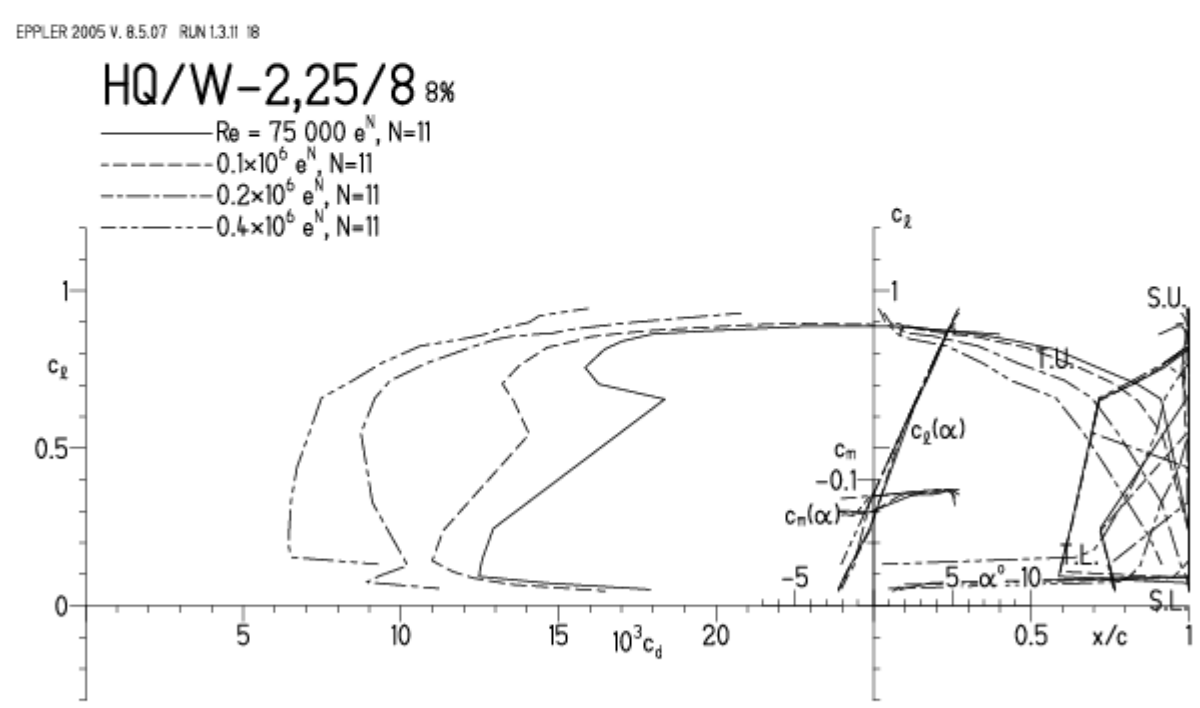
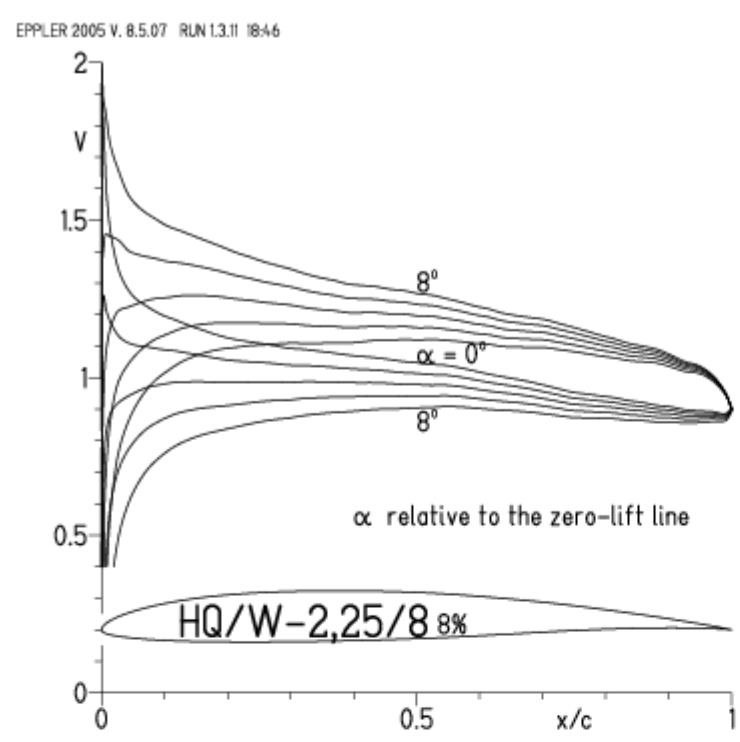
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - · 22% Flap 4°, Re = 75 000 e^N, N=11
- · - · 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

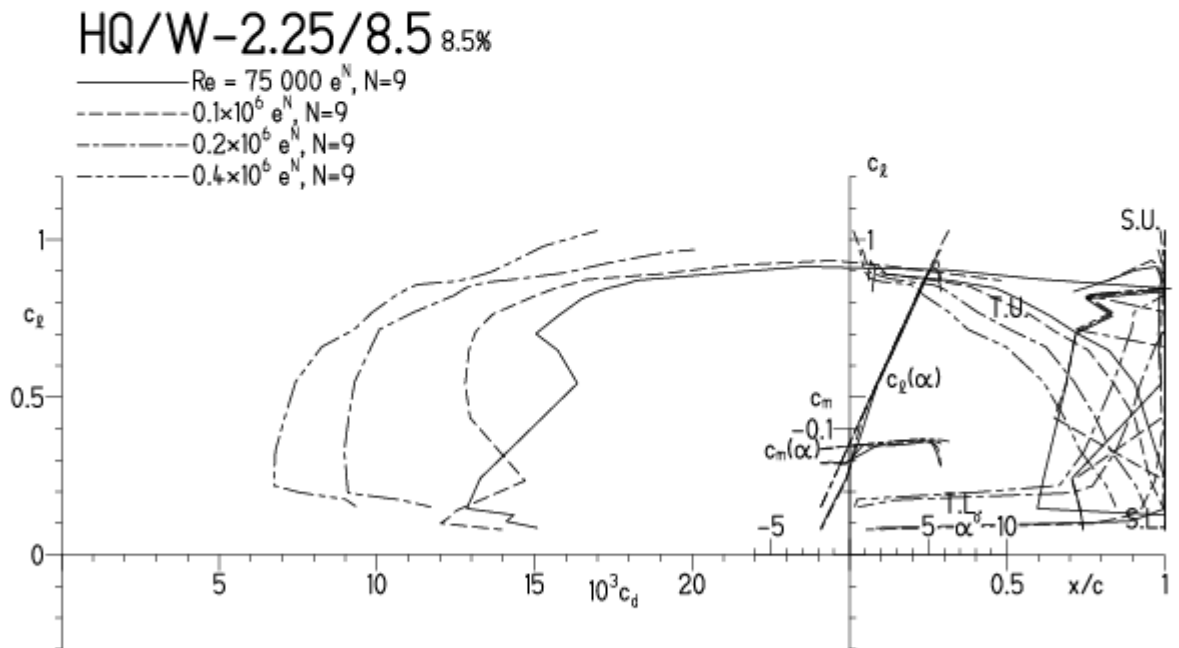


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

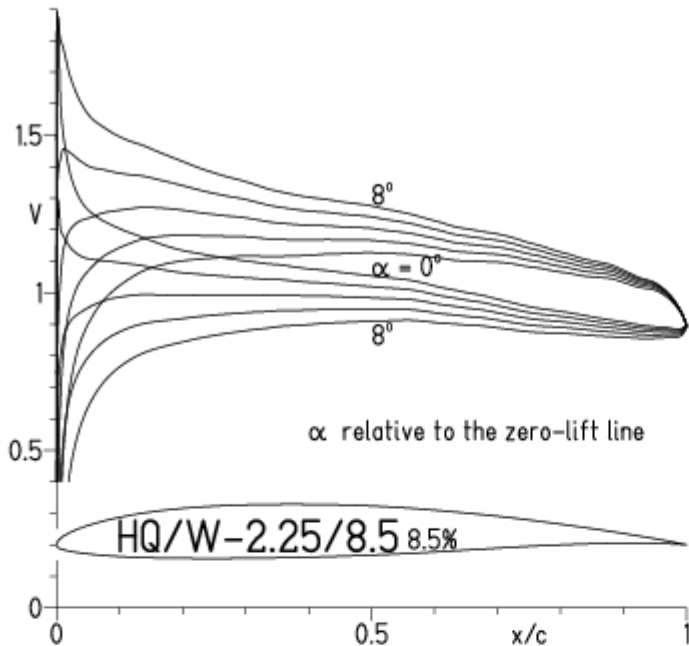


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

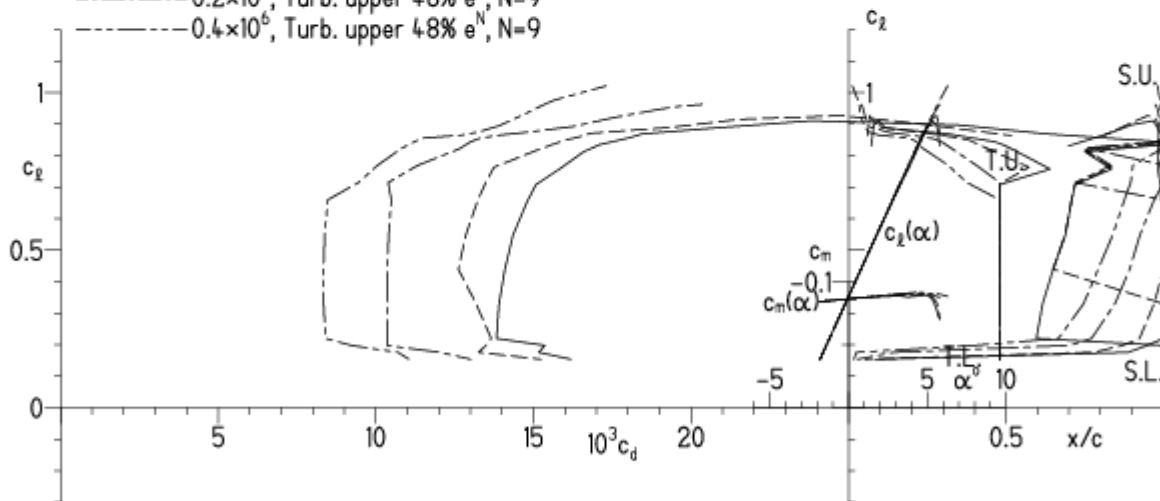
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4°, $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

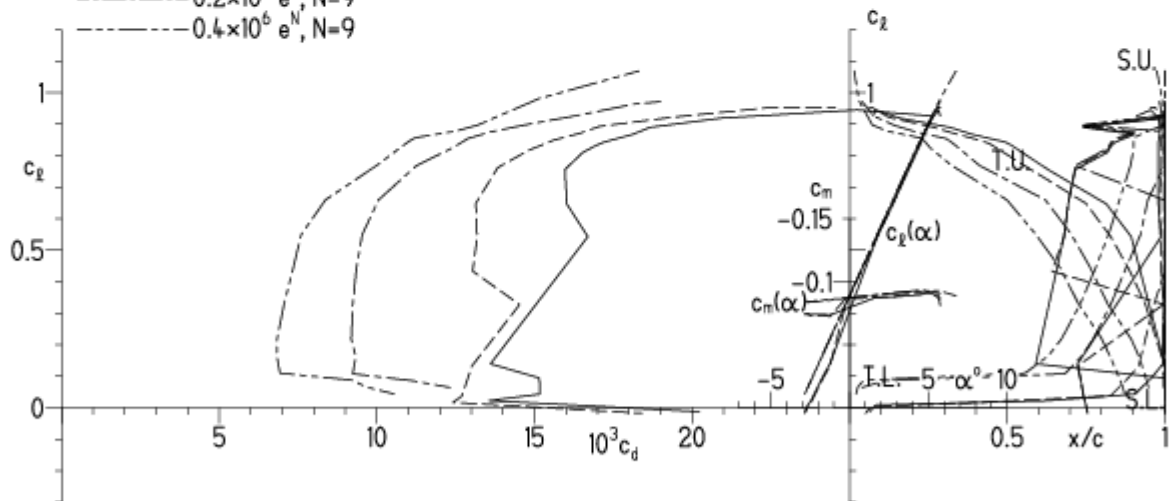
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

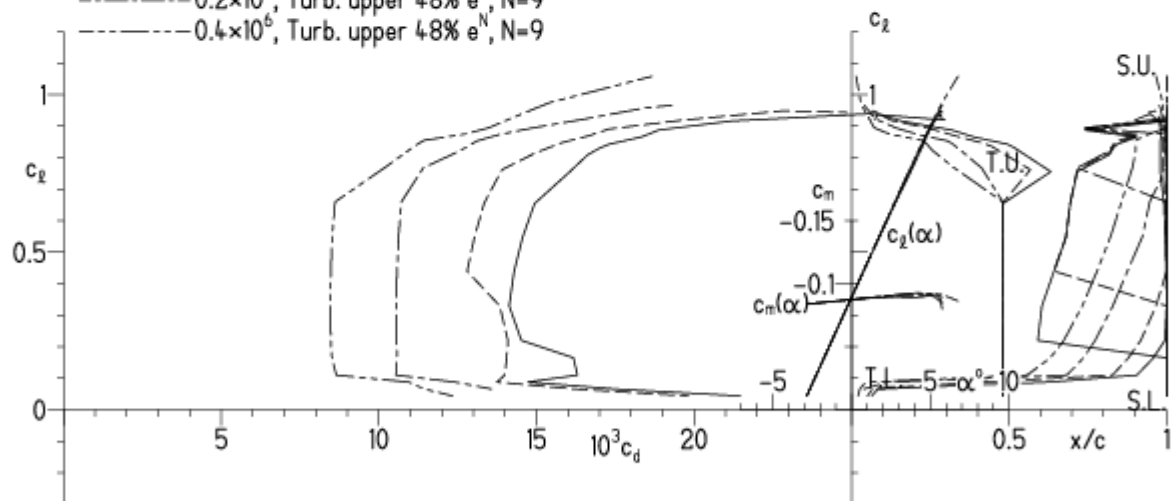
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

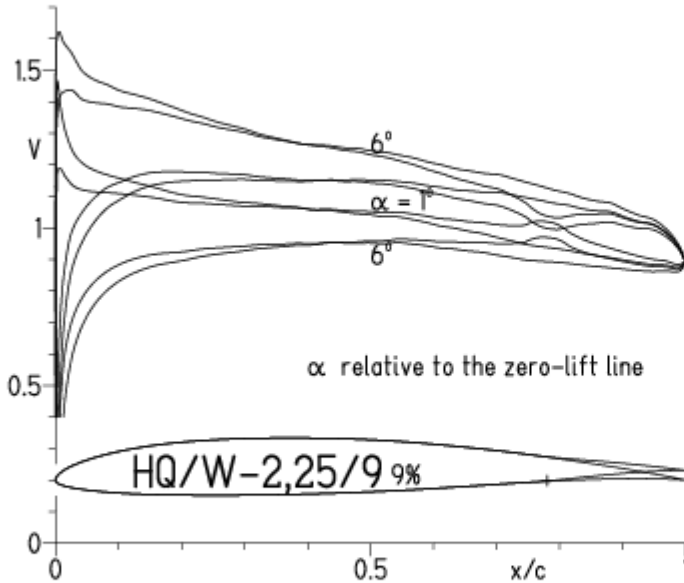
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

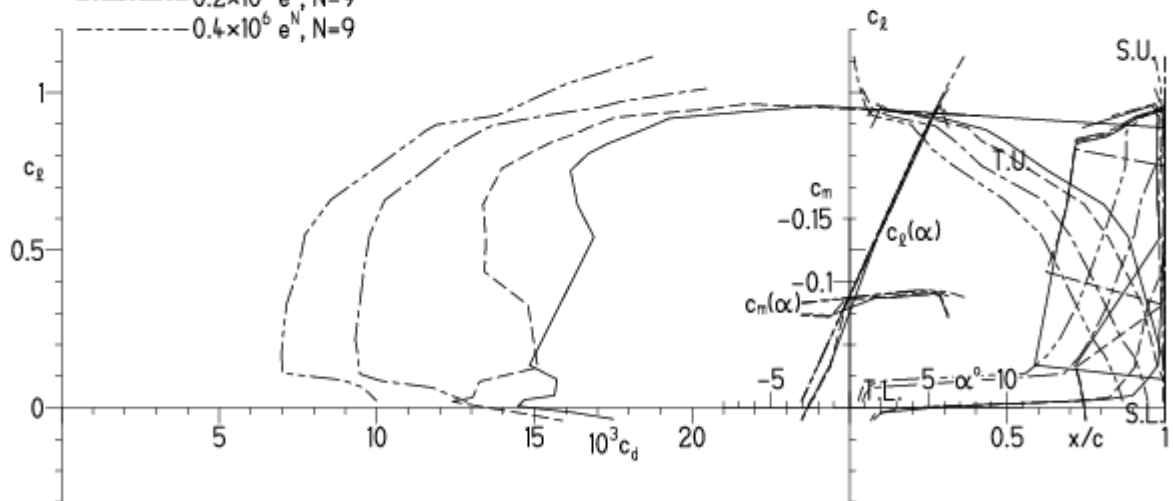
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

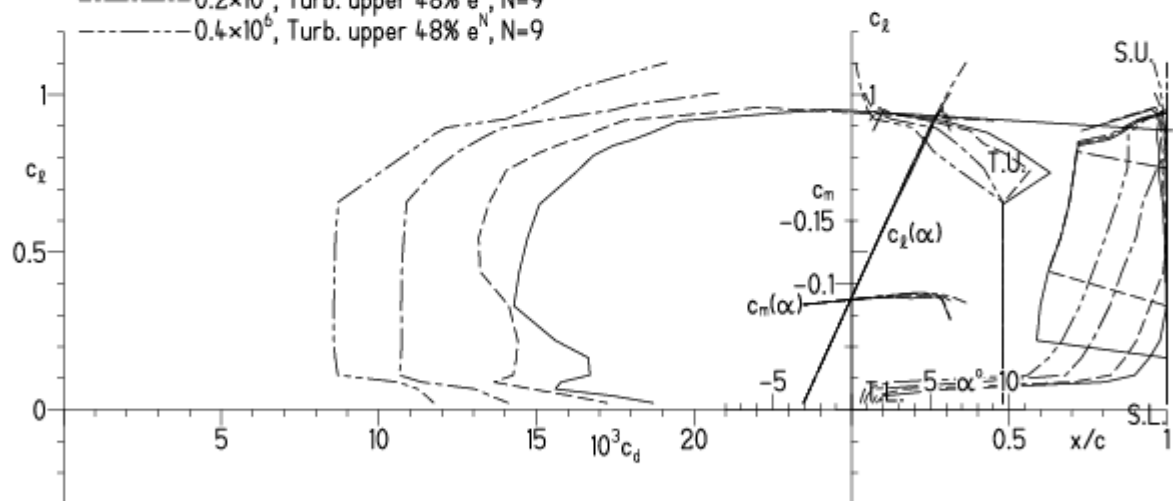
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

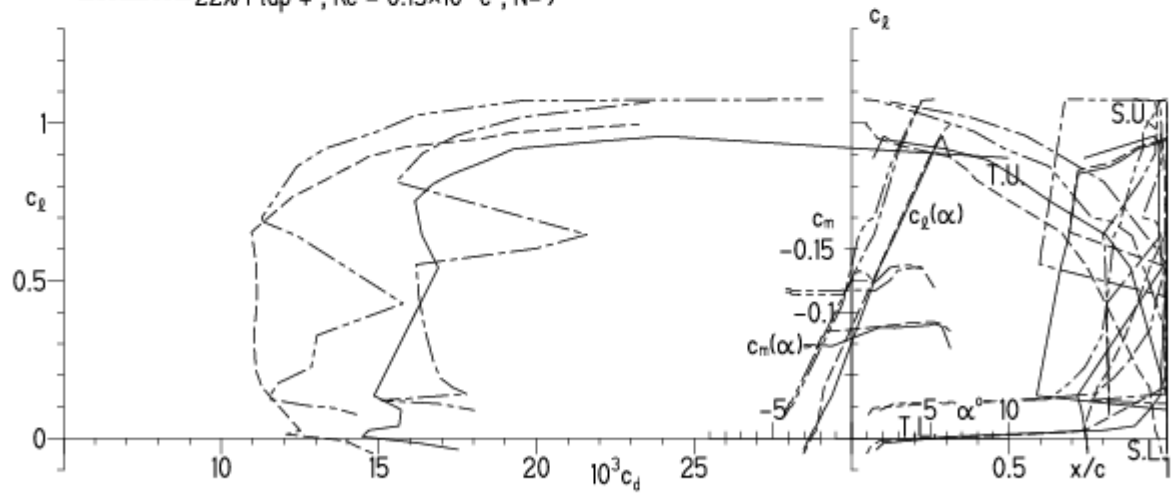


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

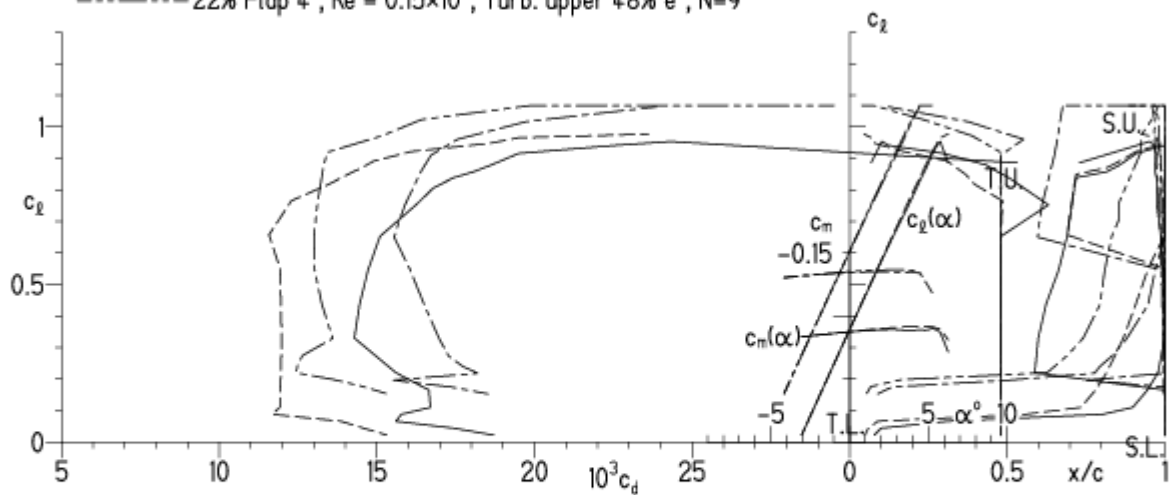


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

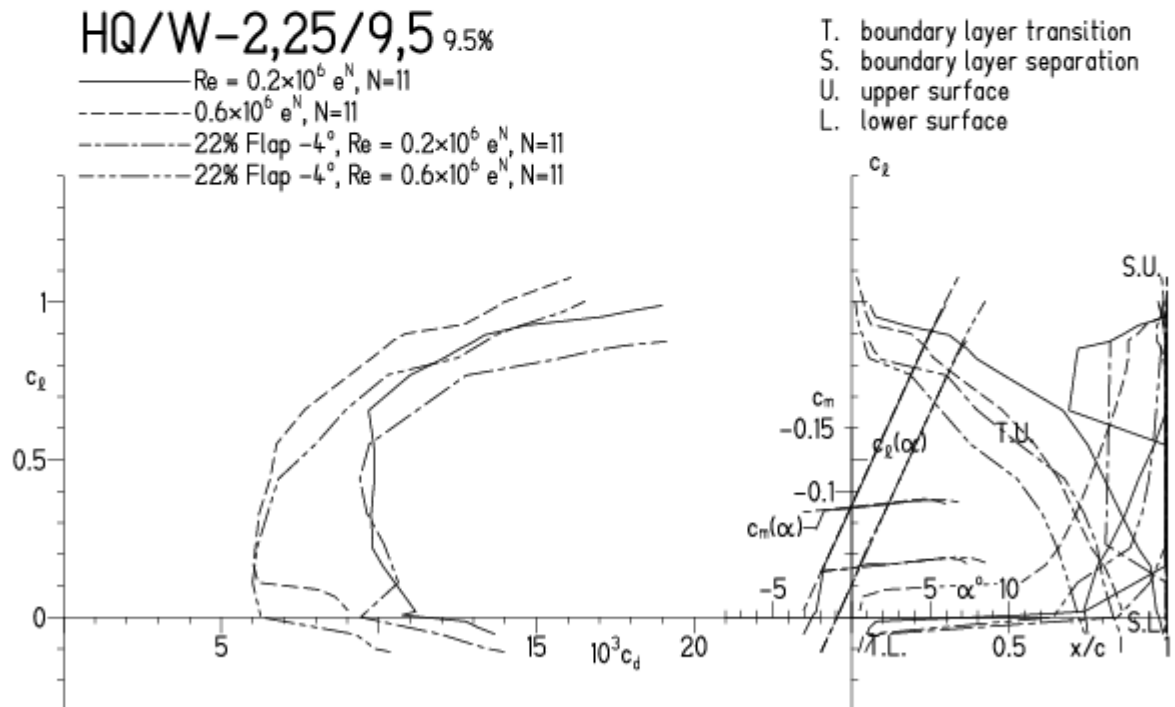


HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

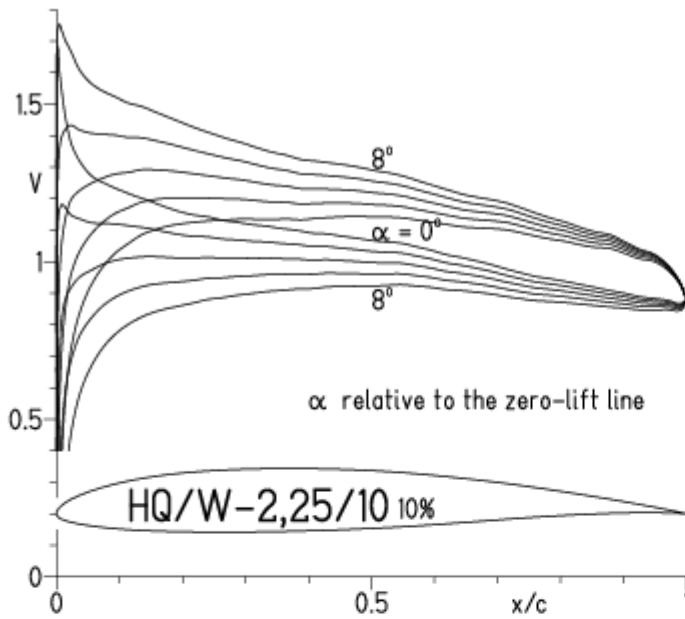


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

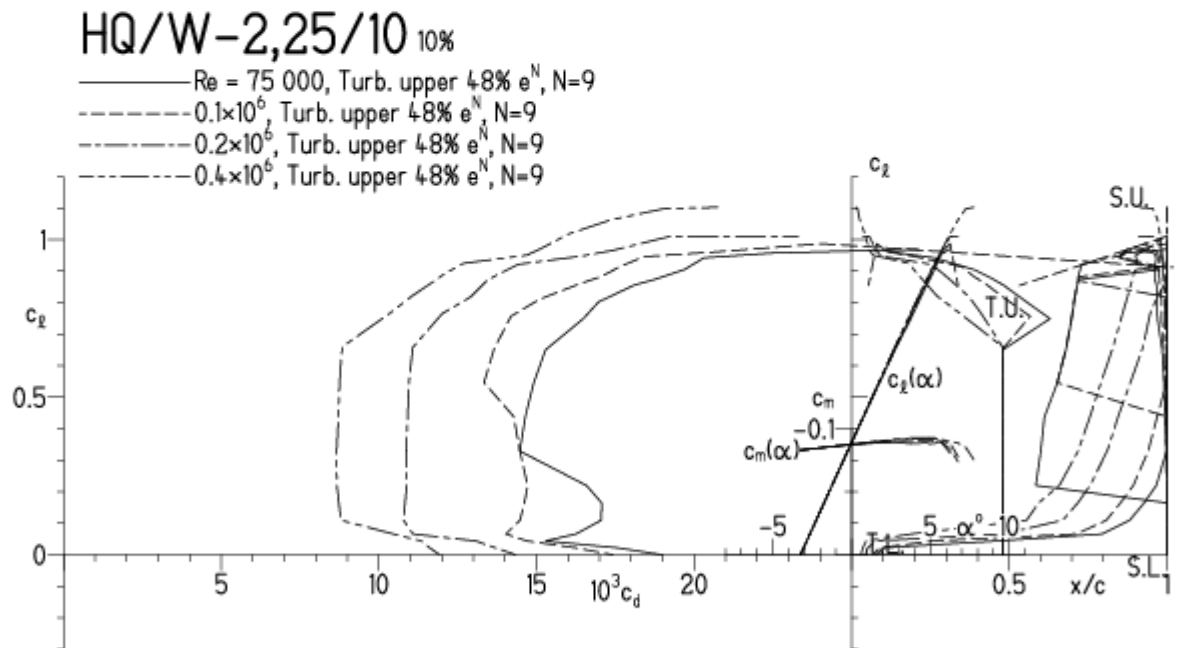


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

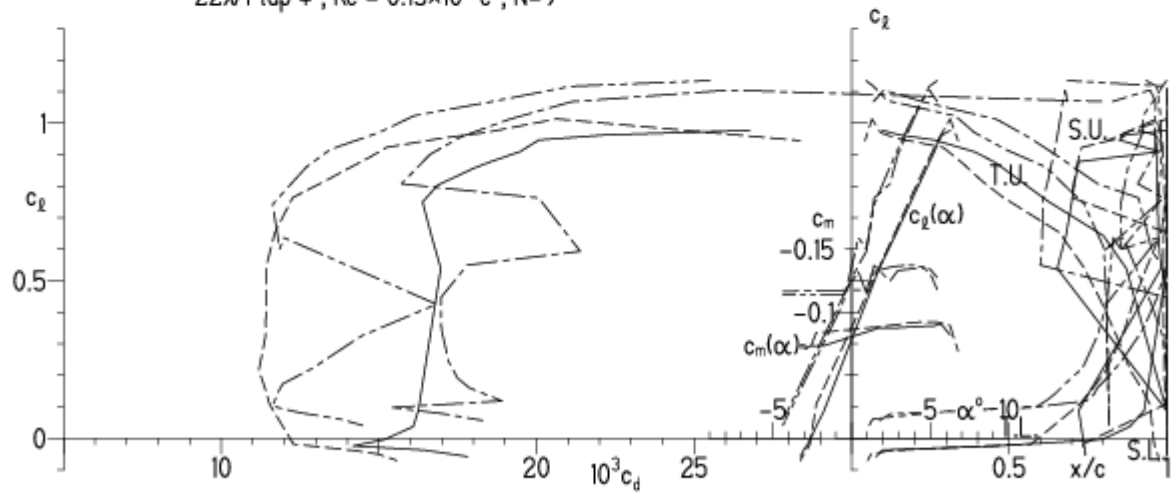


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

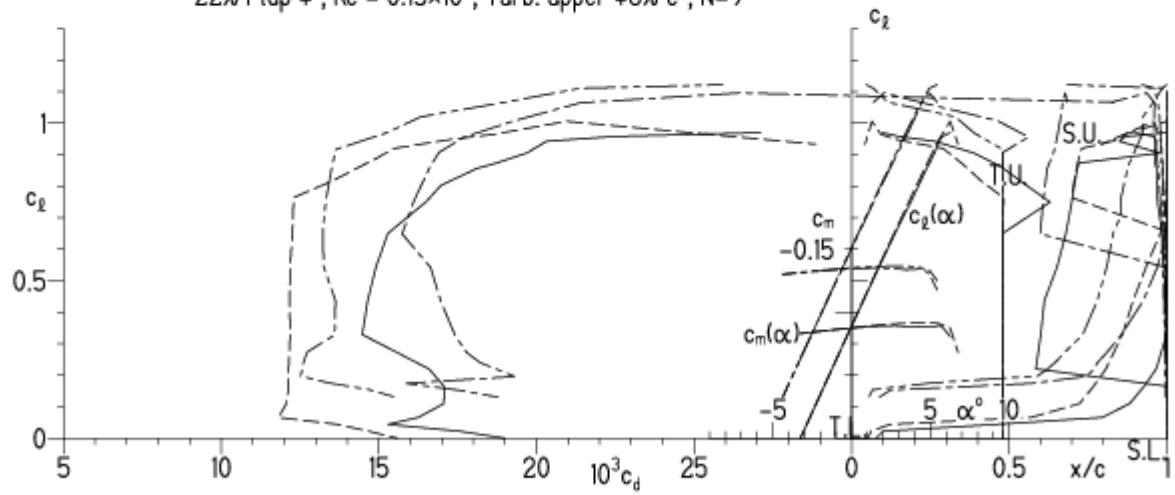


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

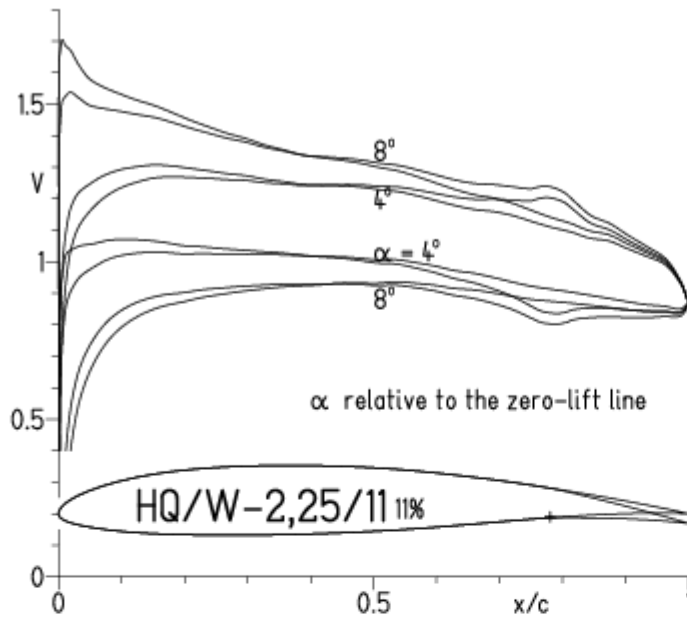
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52

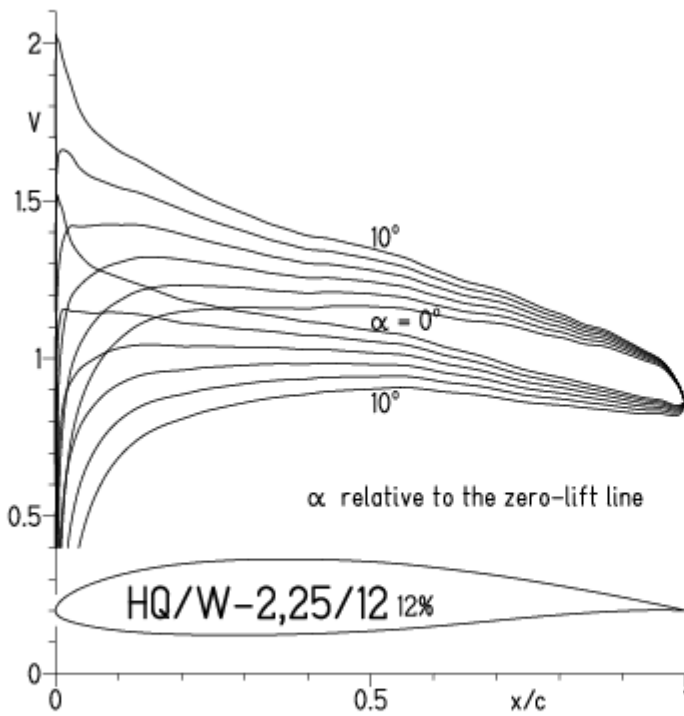


EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

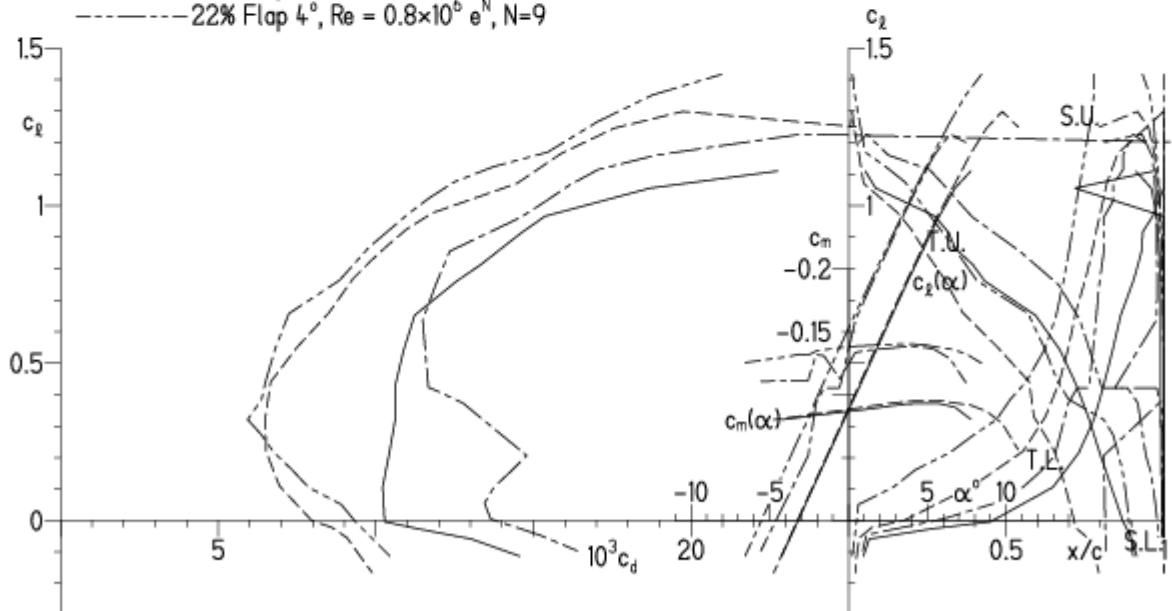


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

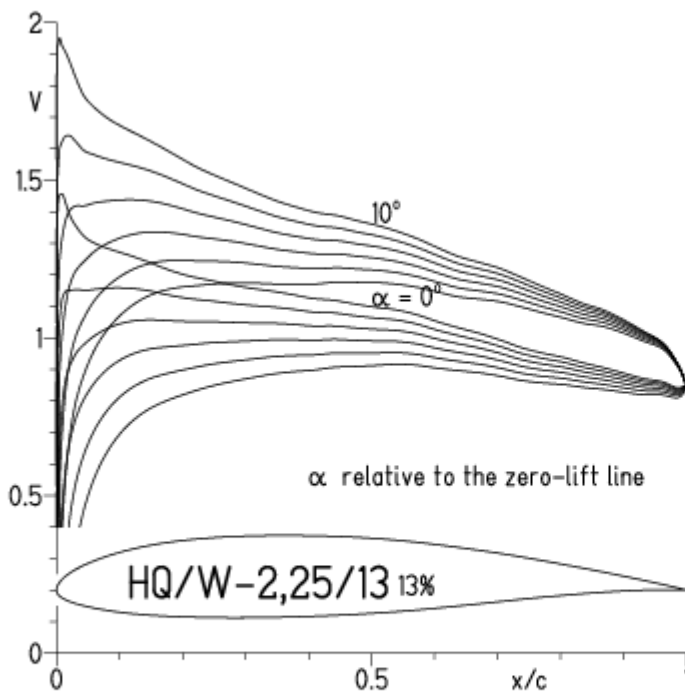


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

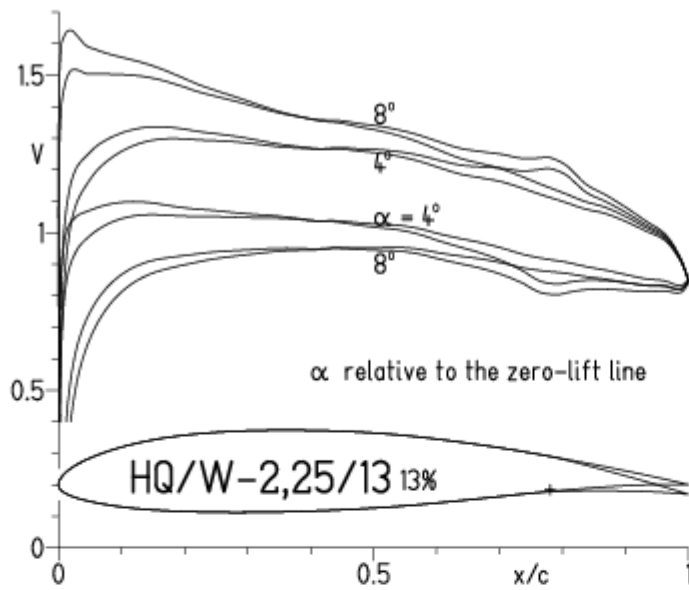
HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

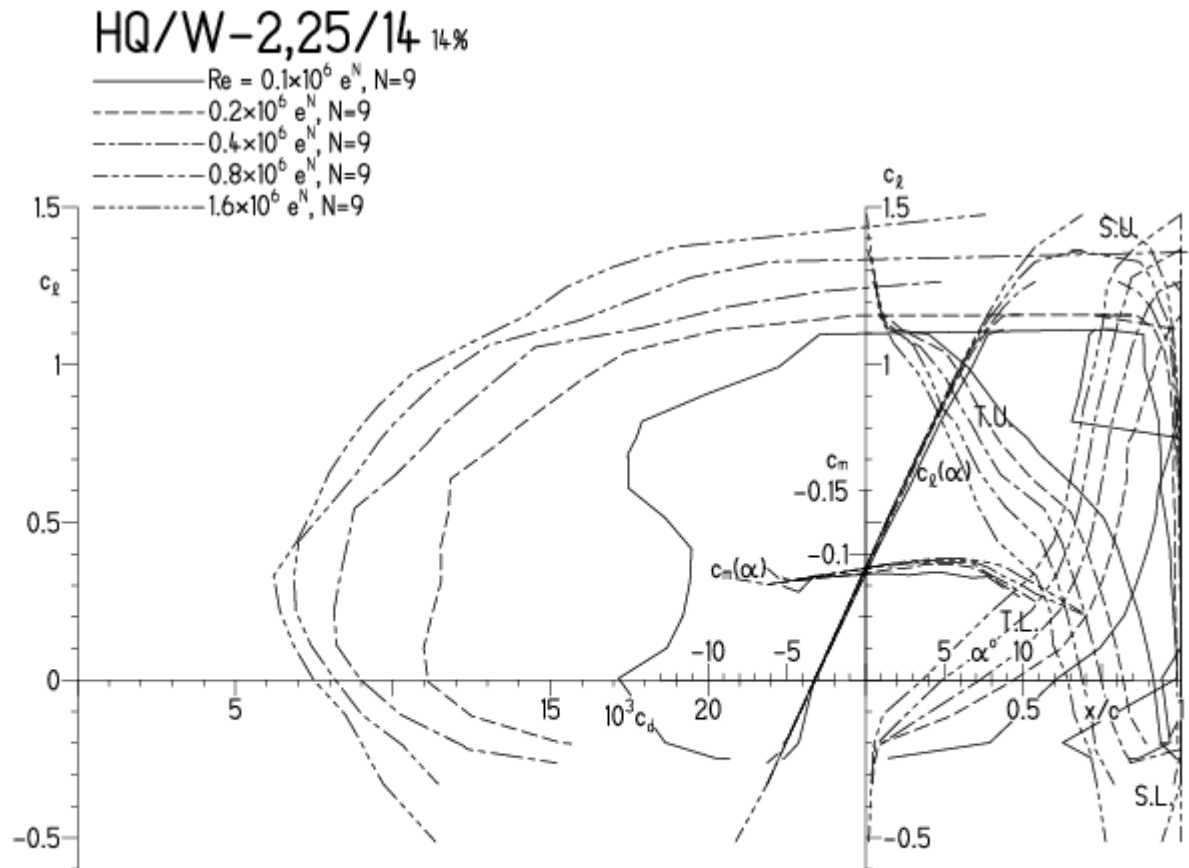


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

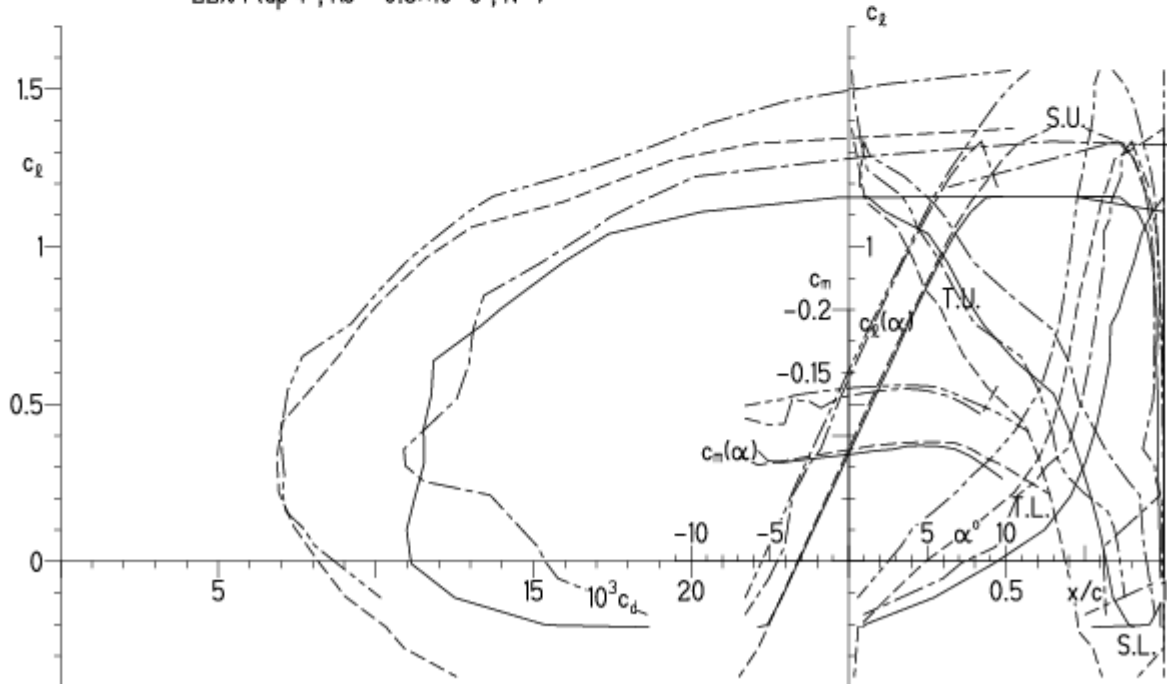


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

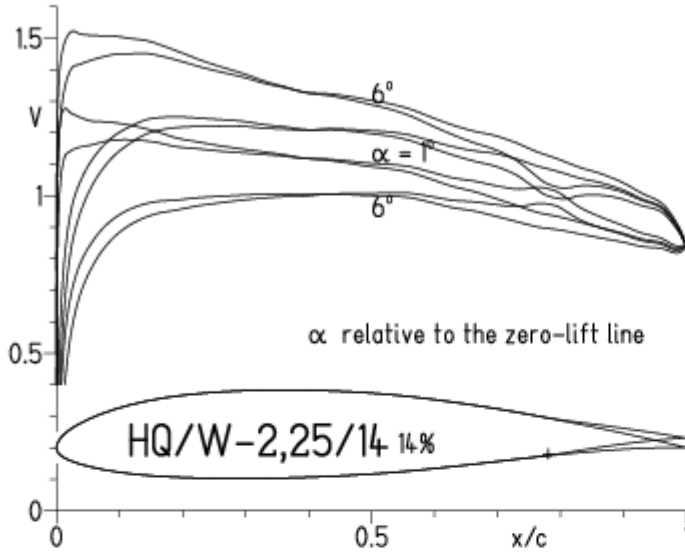
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

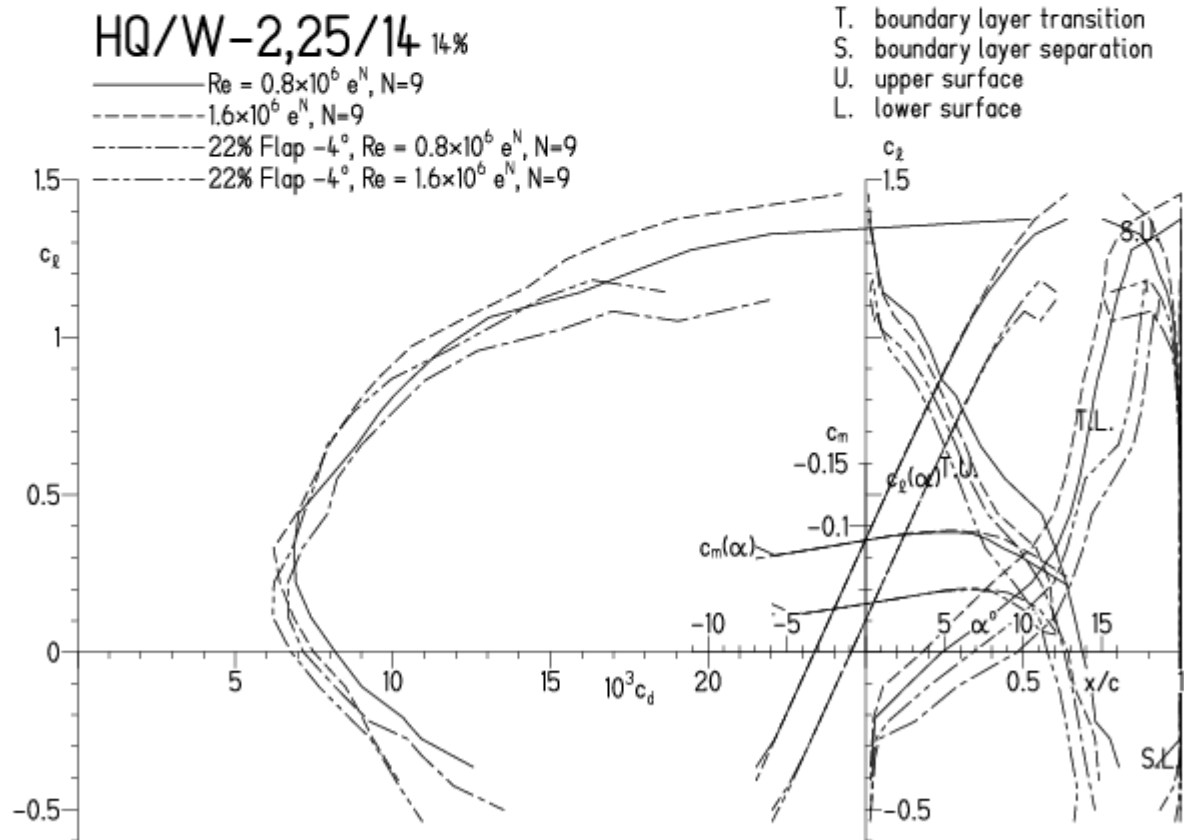


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

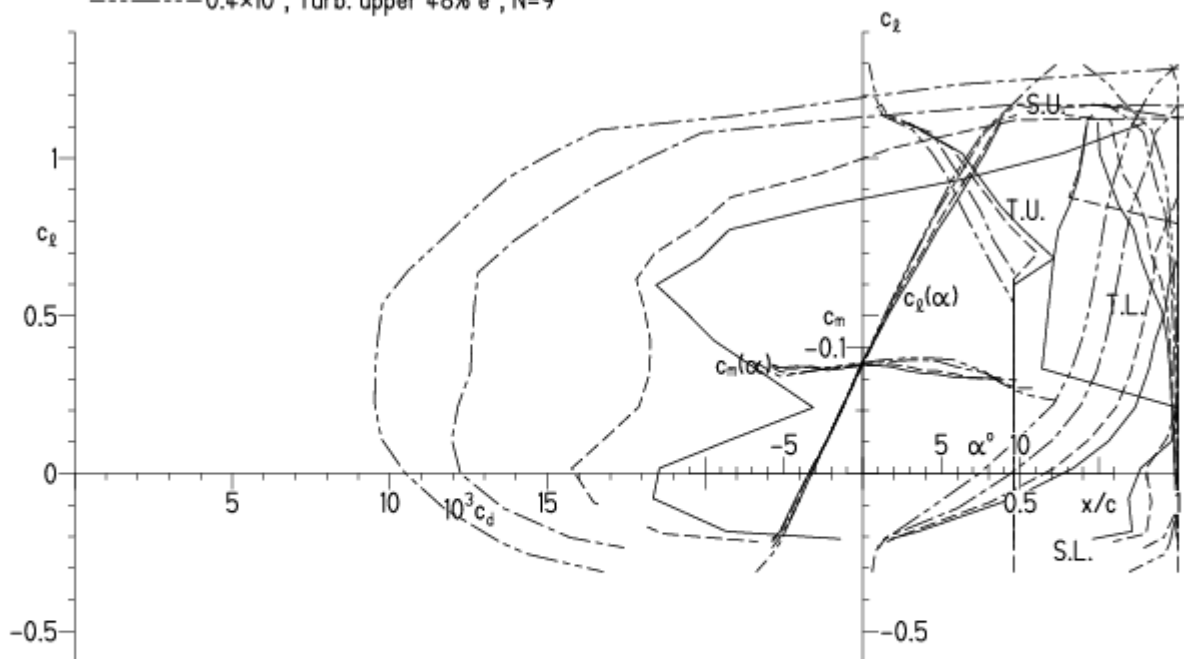
EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

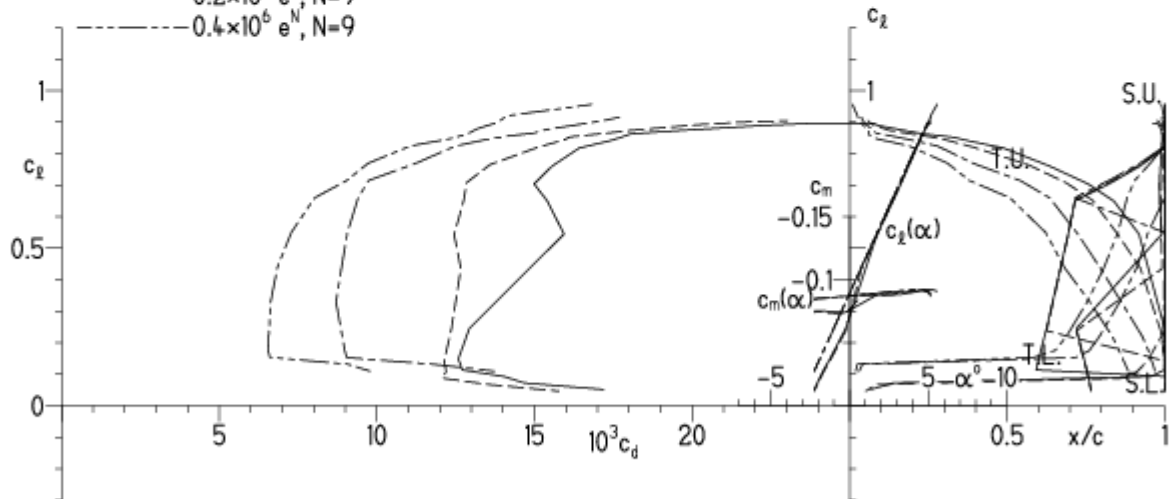
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



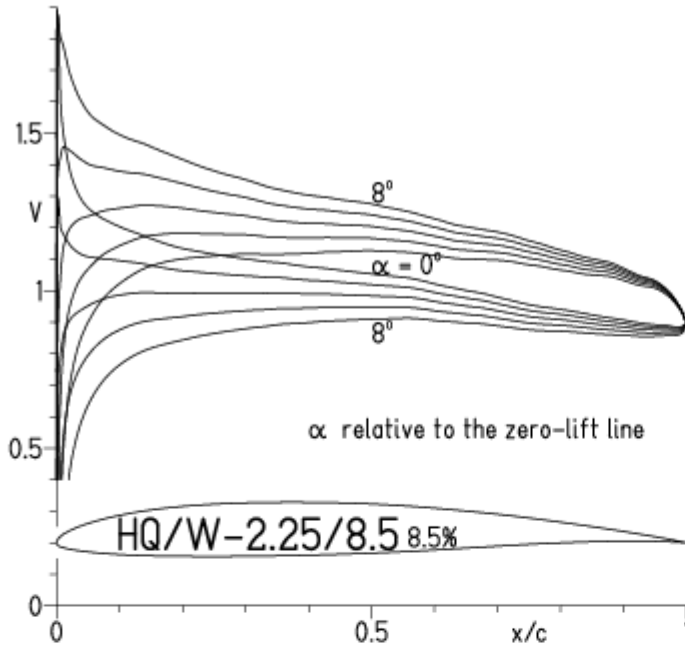
EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

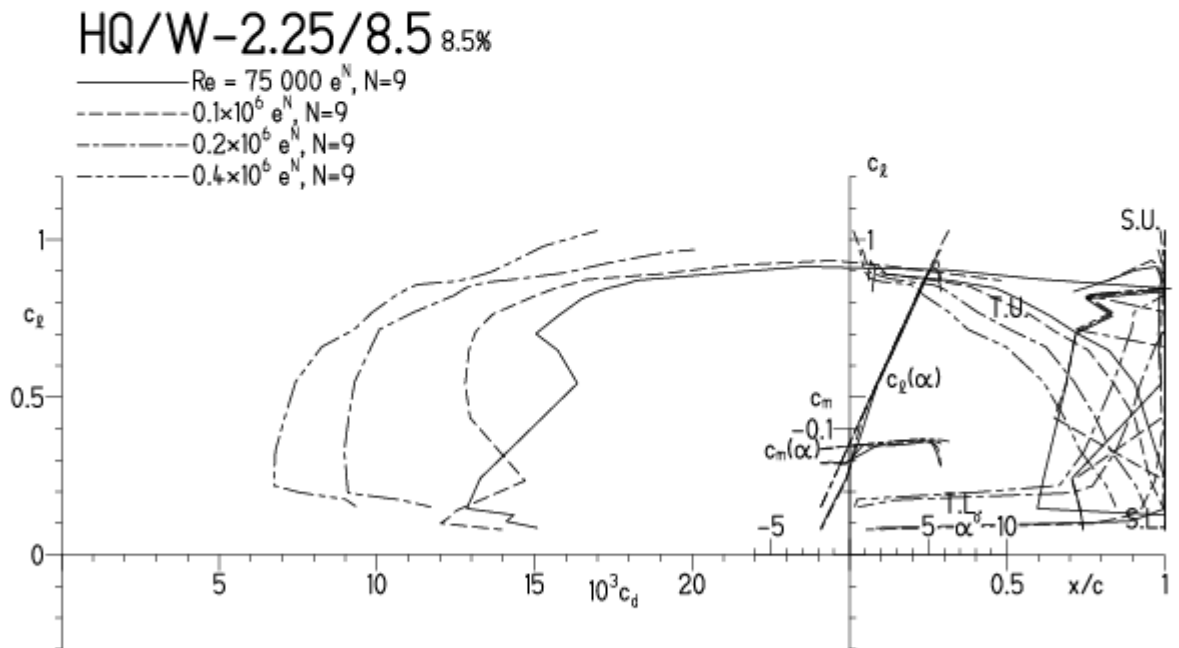


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

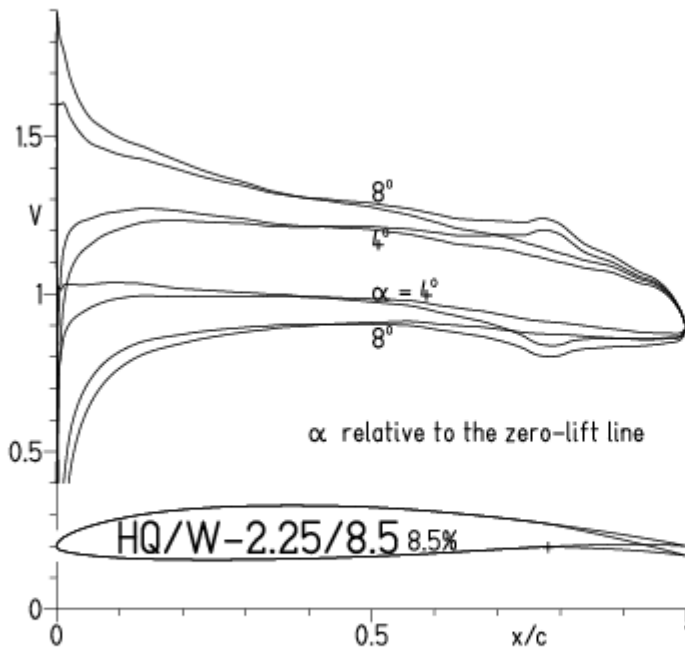
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

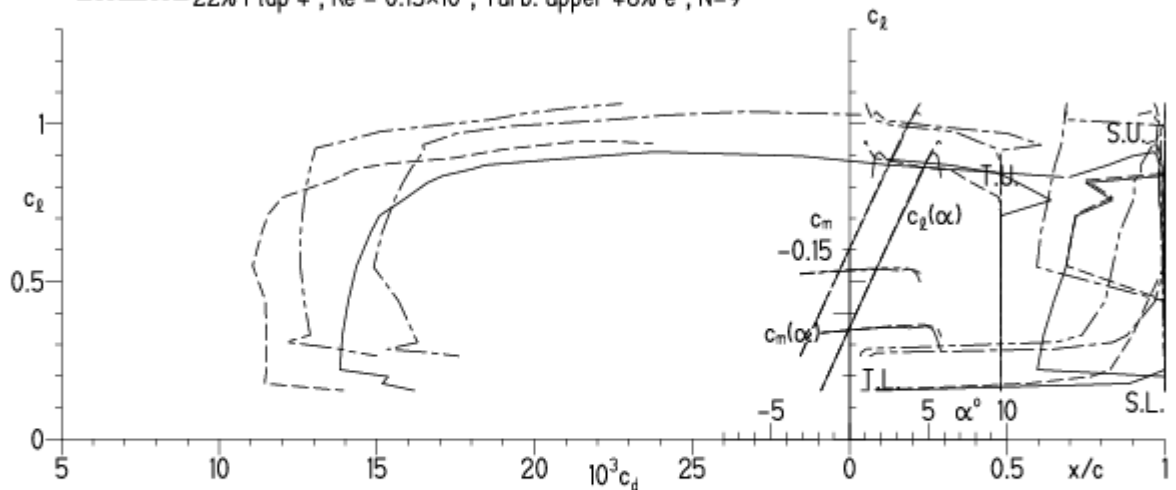


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

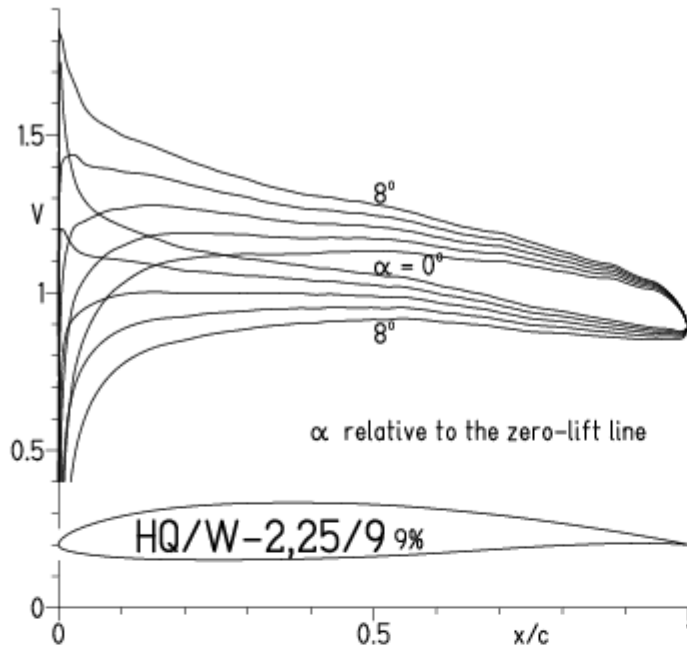


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

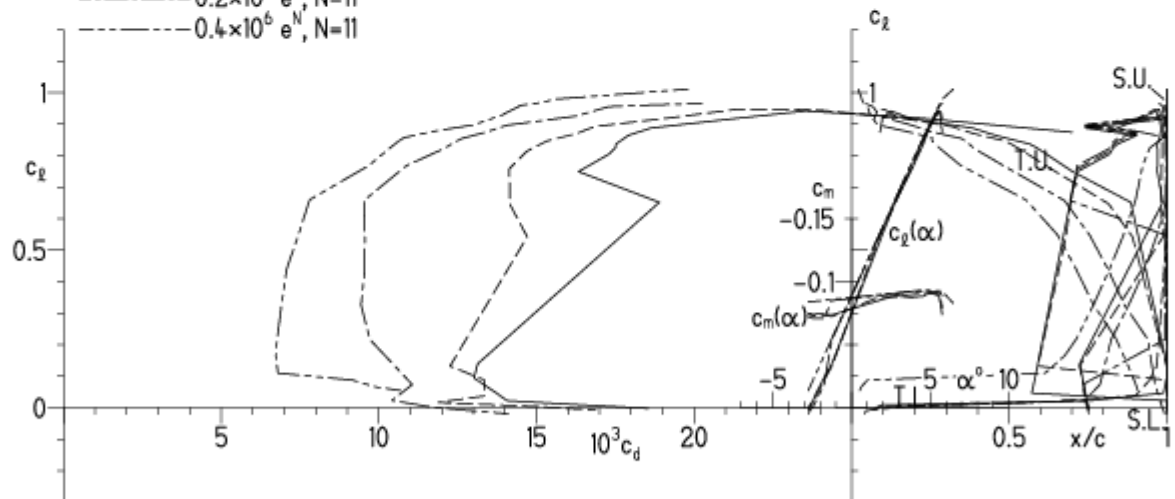
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

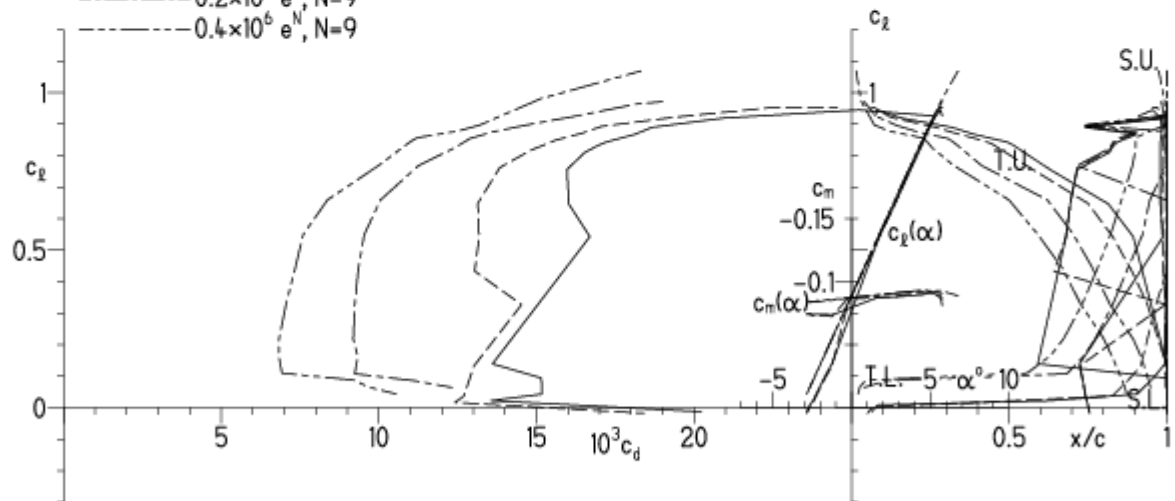
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

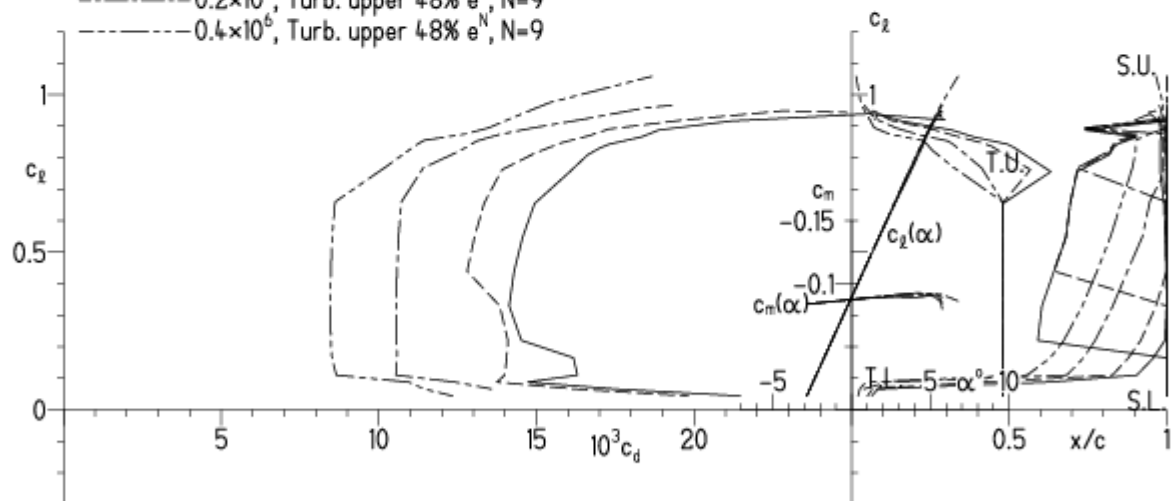
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

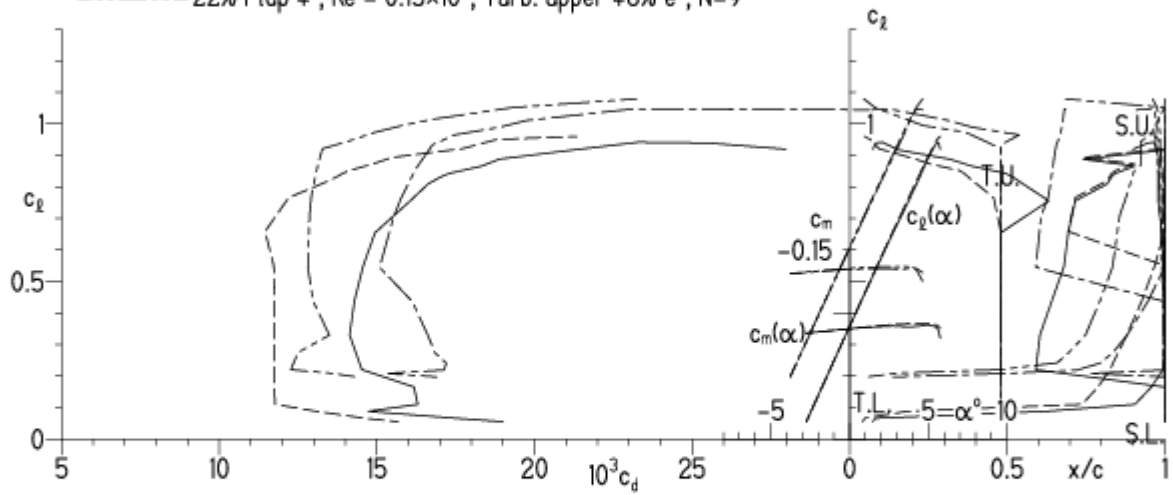


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9 9%

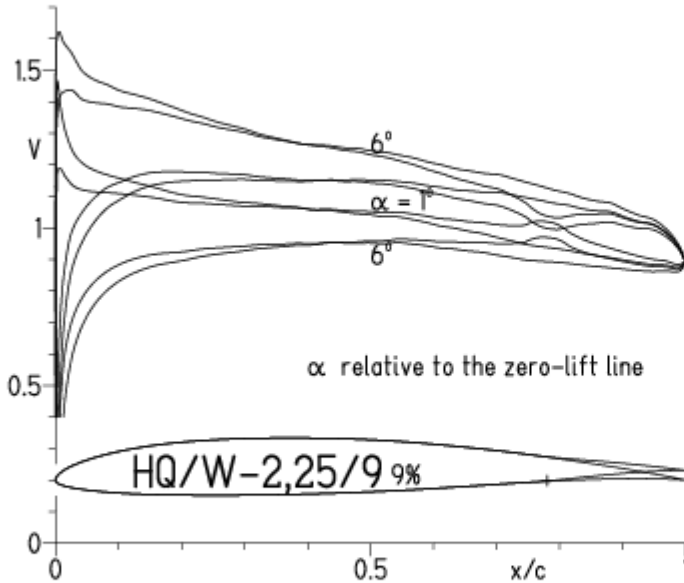
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

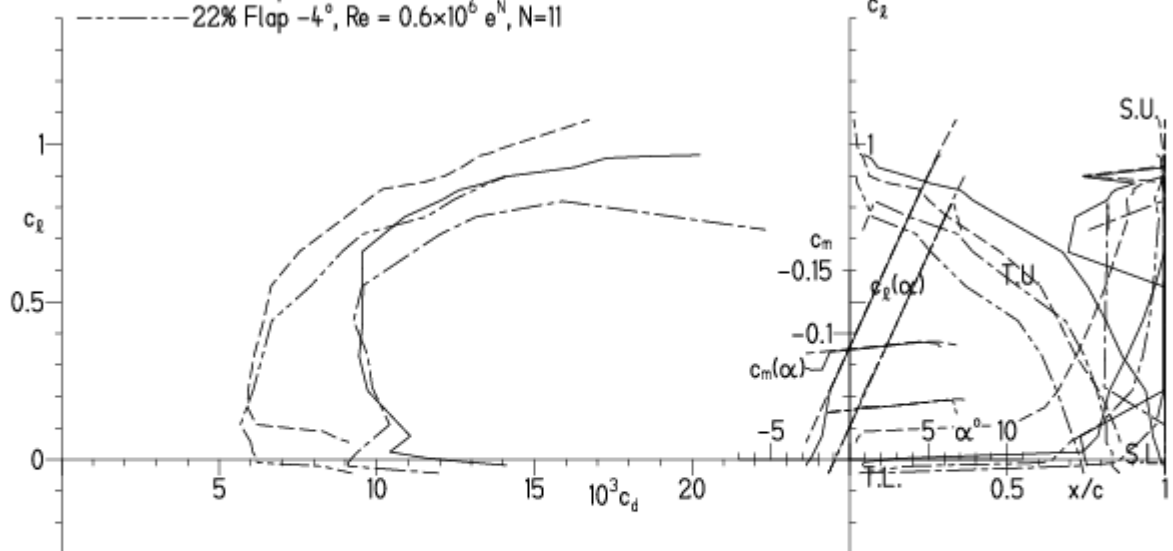
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

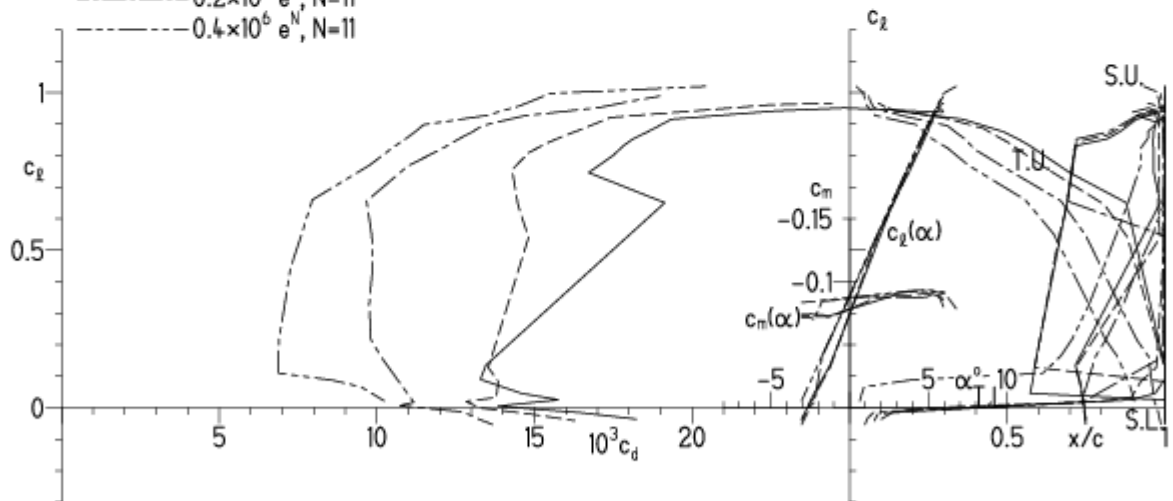
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

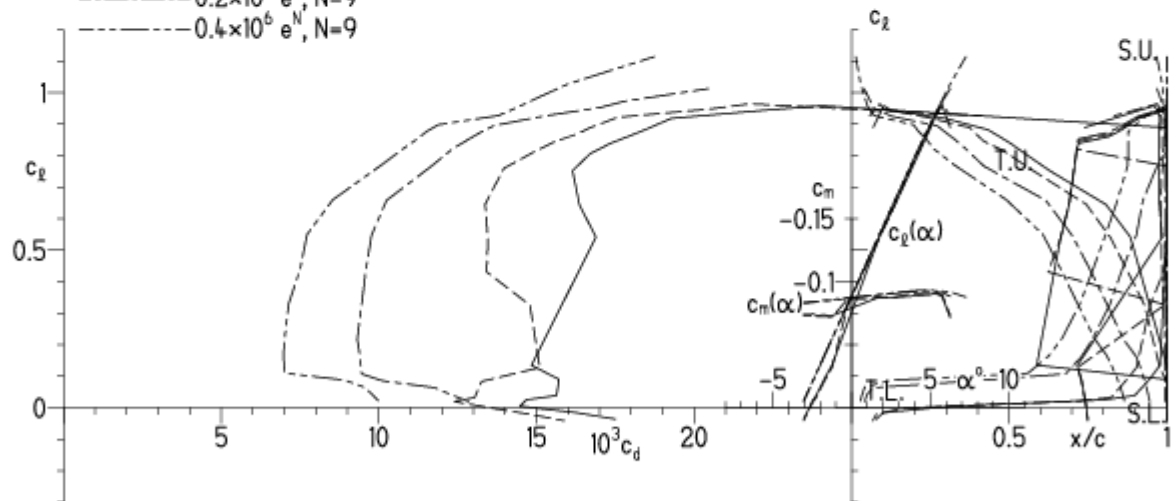
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

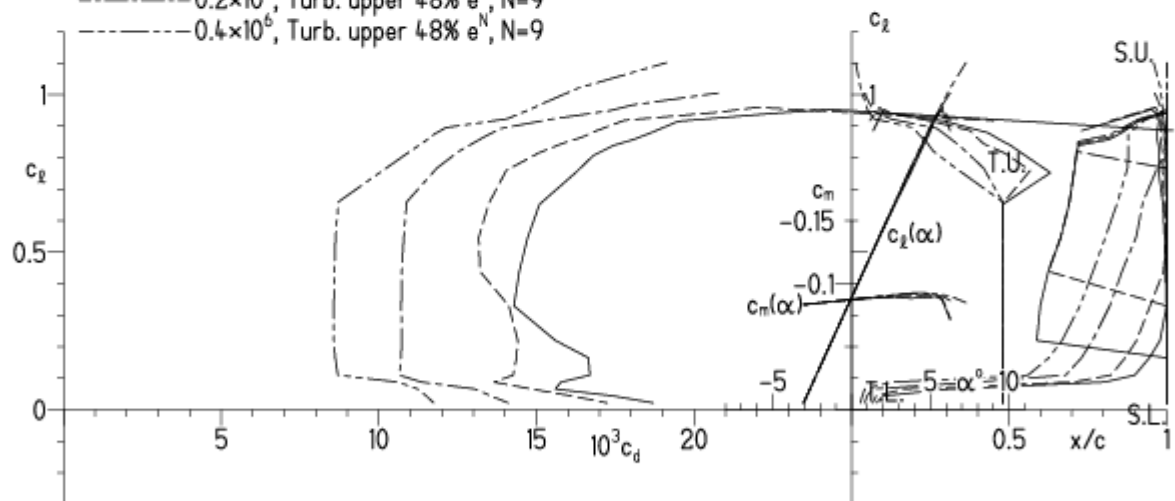
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N$, $N=11$
- - - $0.6 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 0.2 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N$, $N=11$

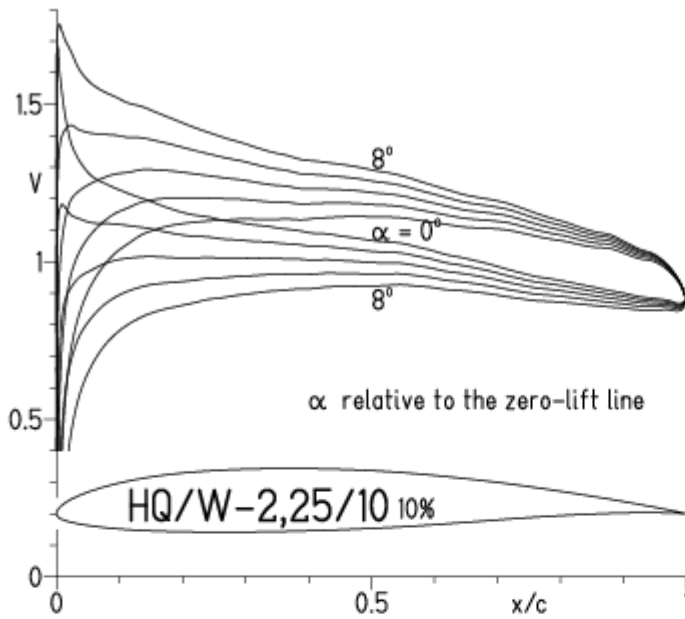


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

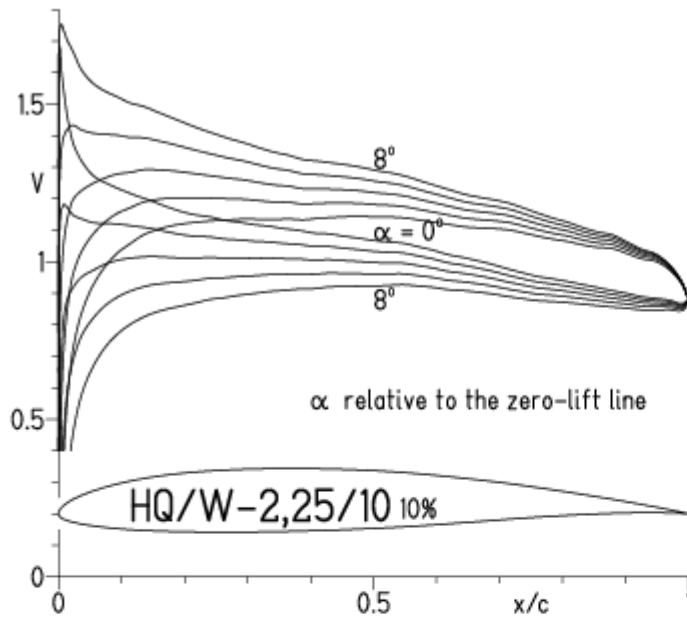


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

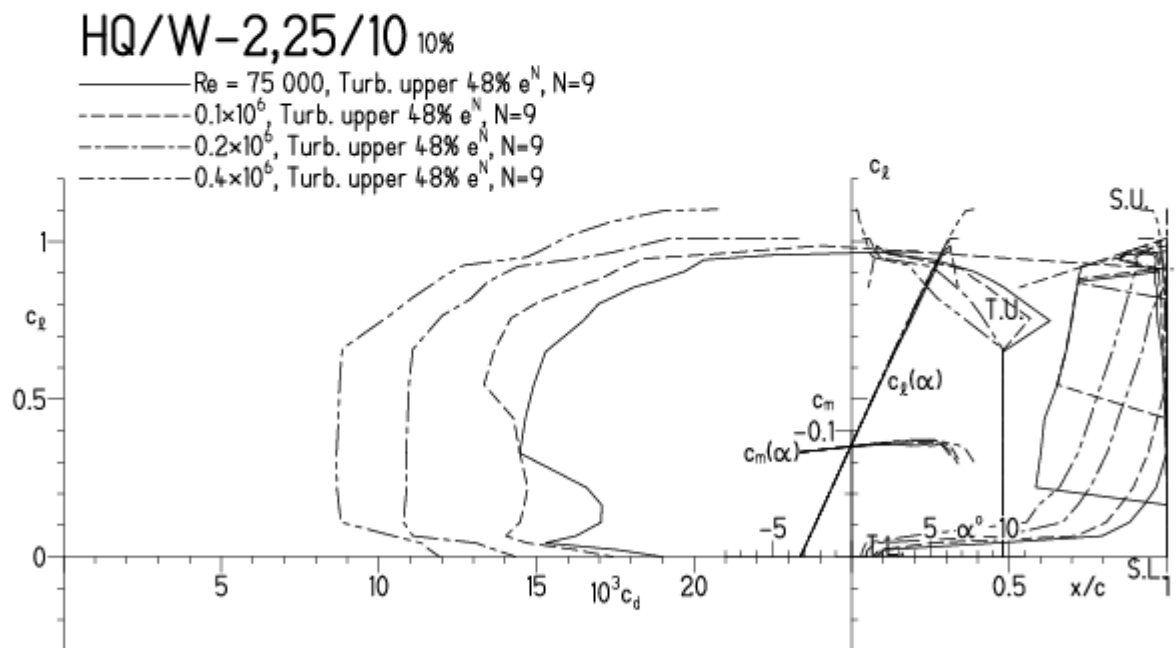


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

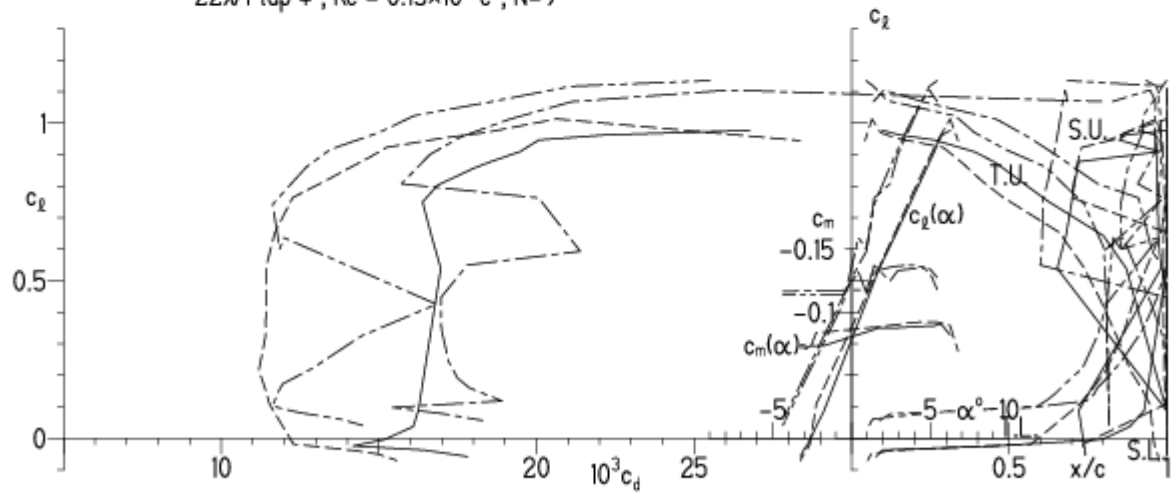


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

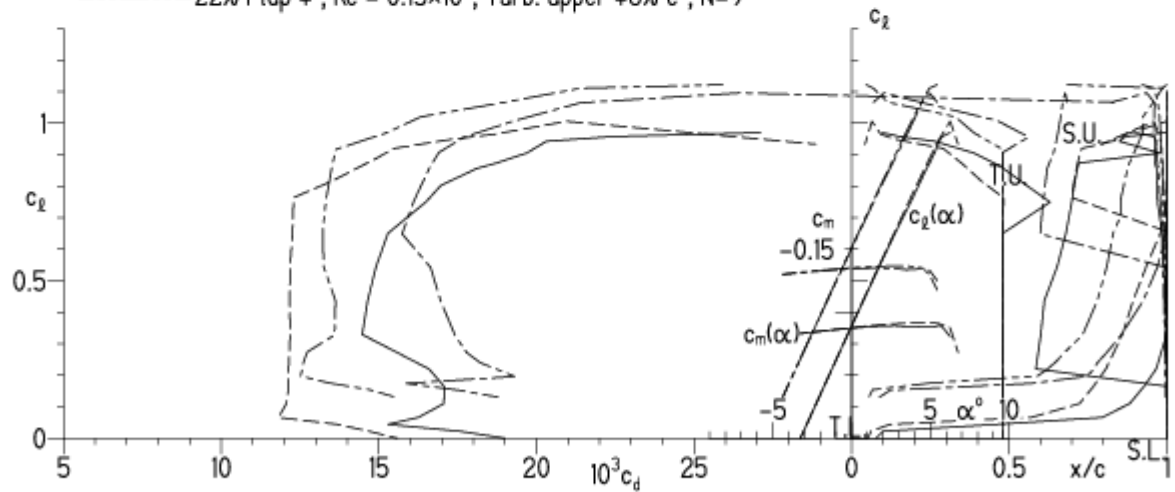


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

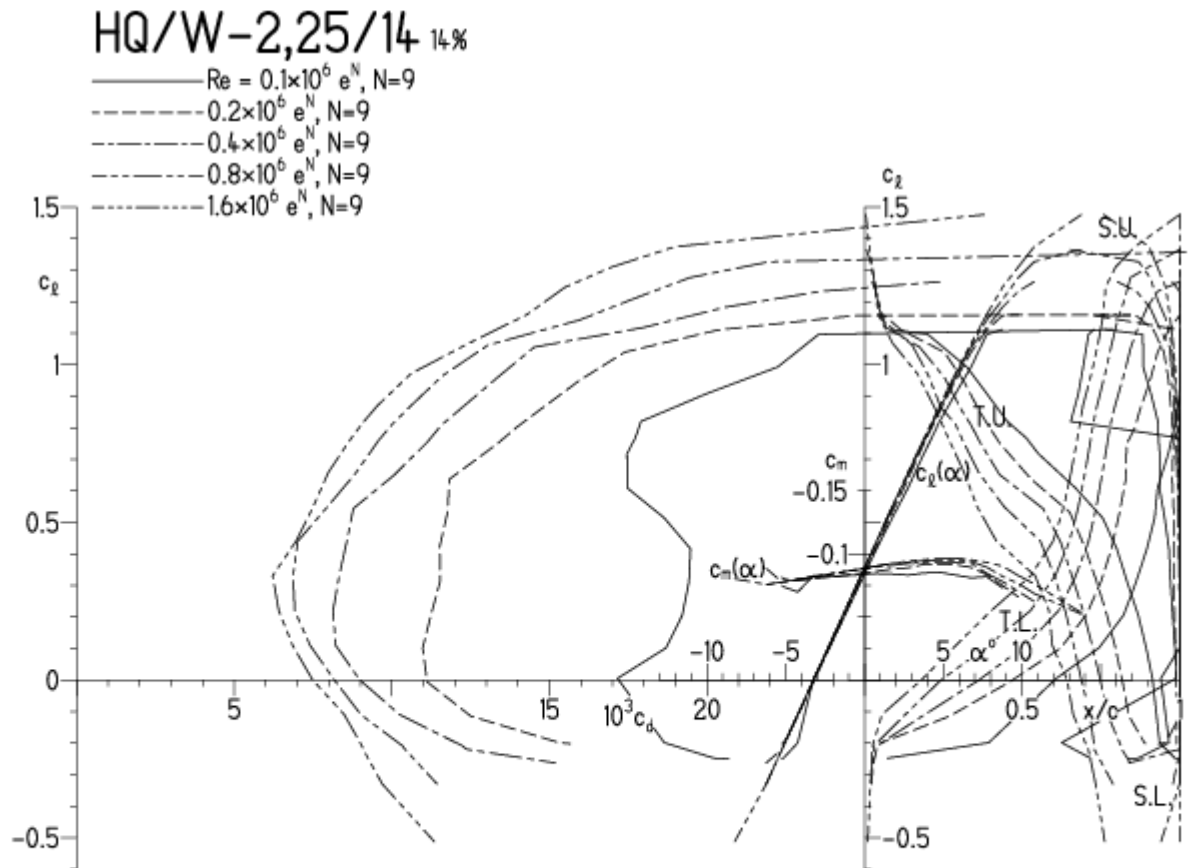


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

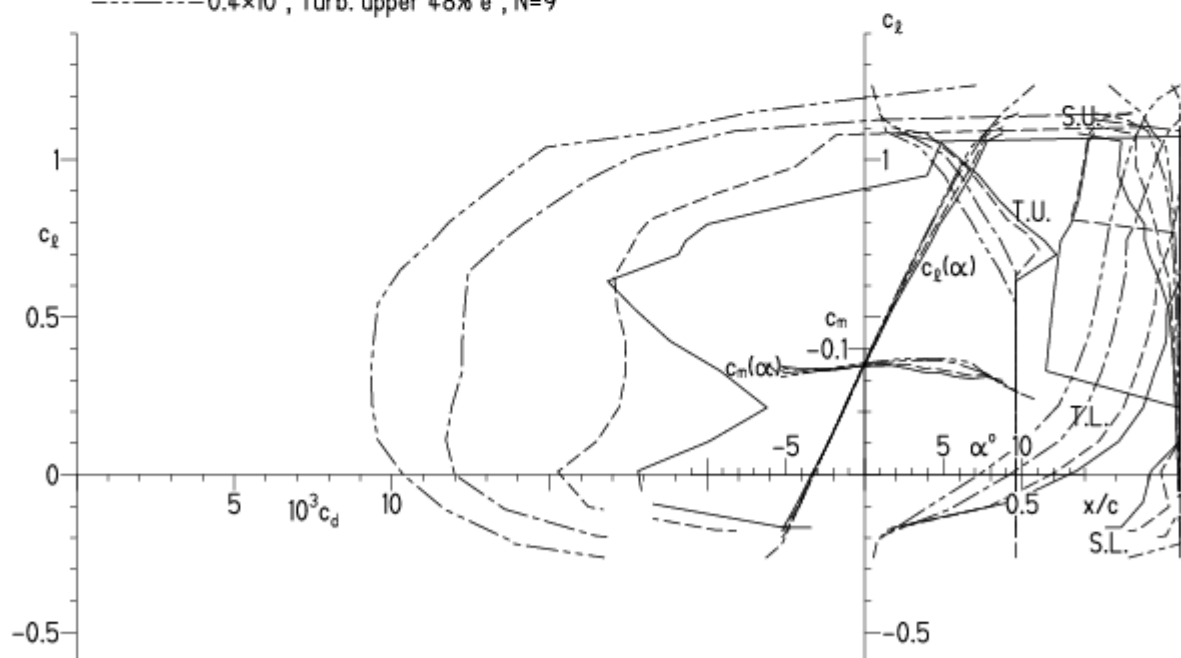
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

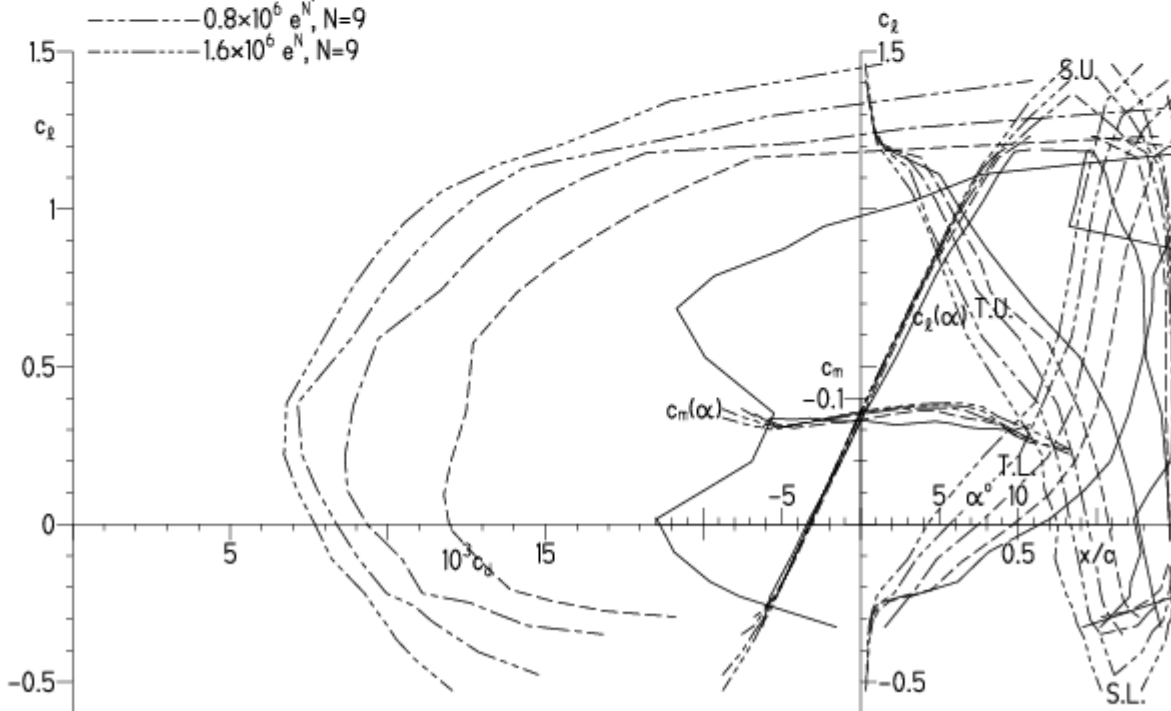
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

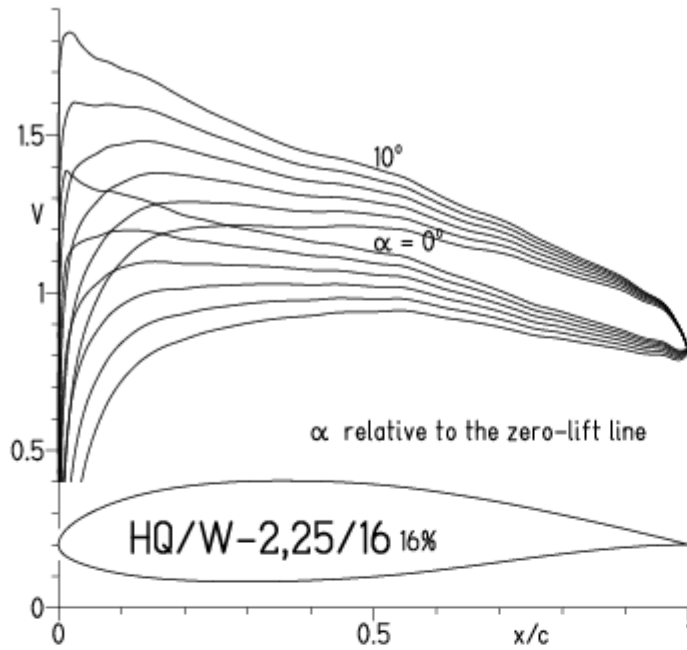
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

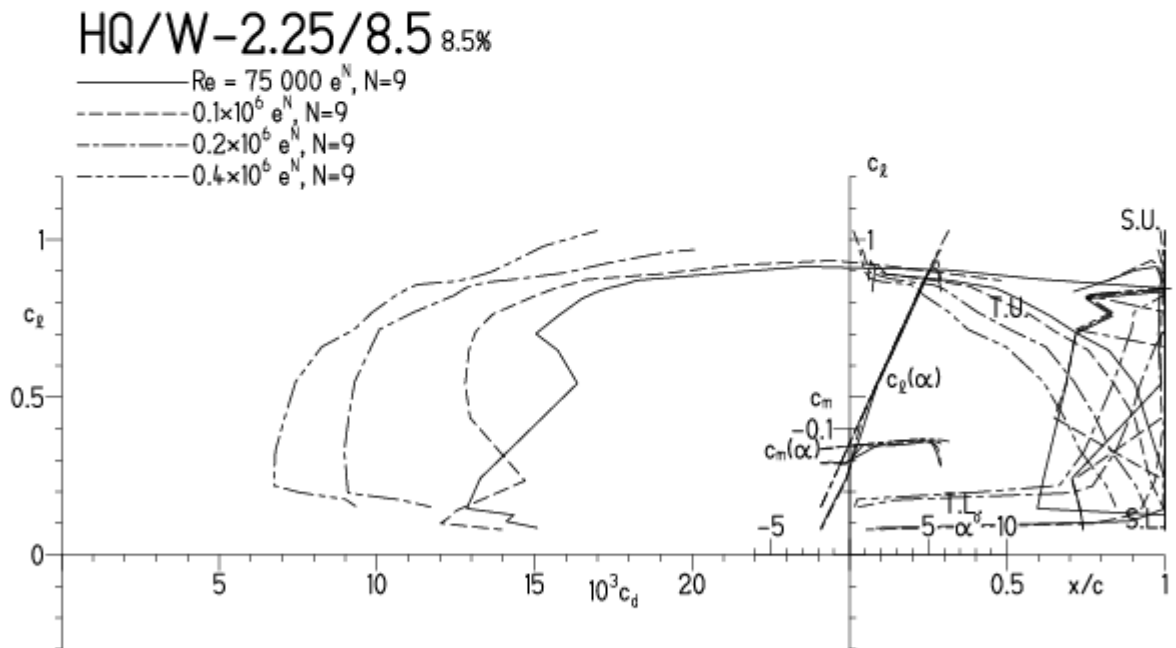


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

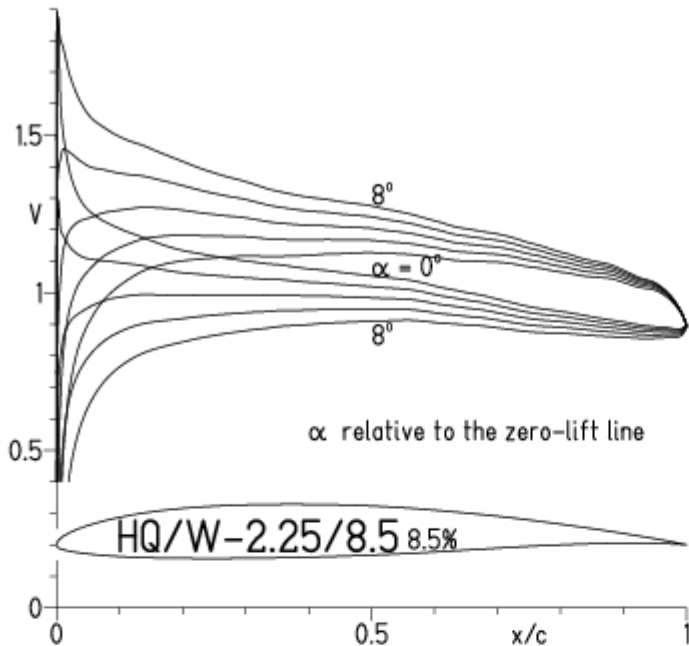


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

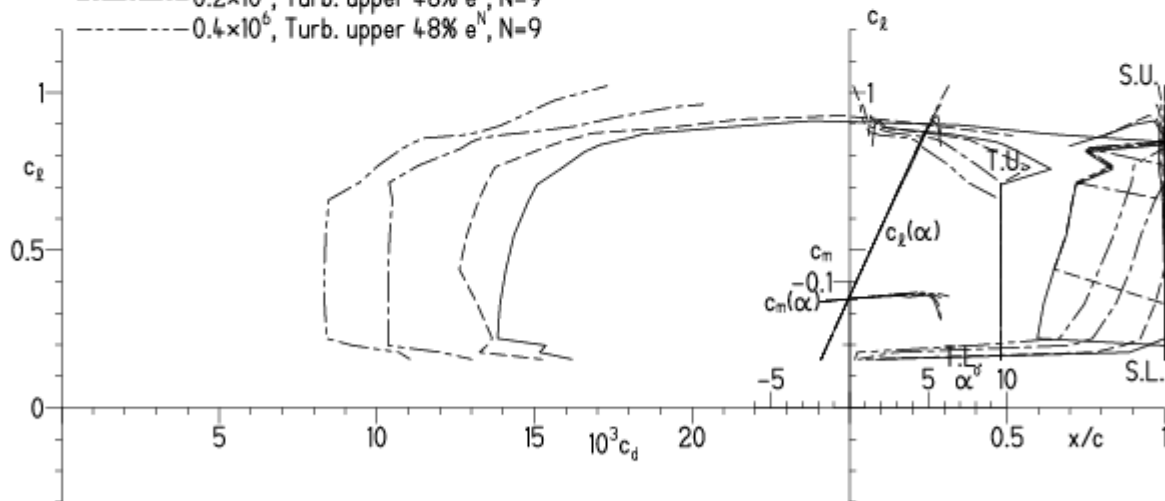
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

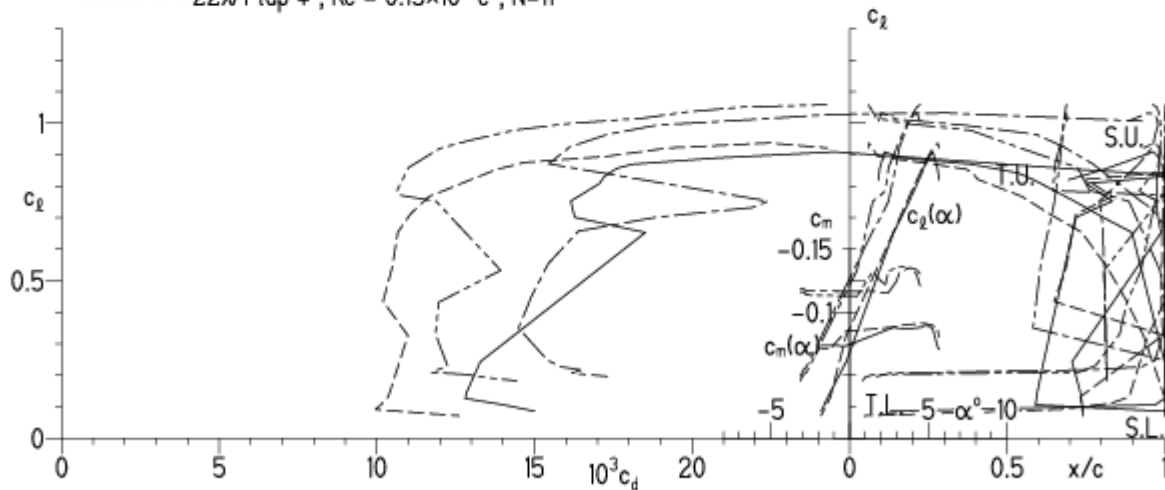


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



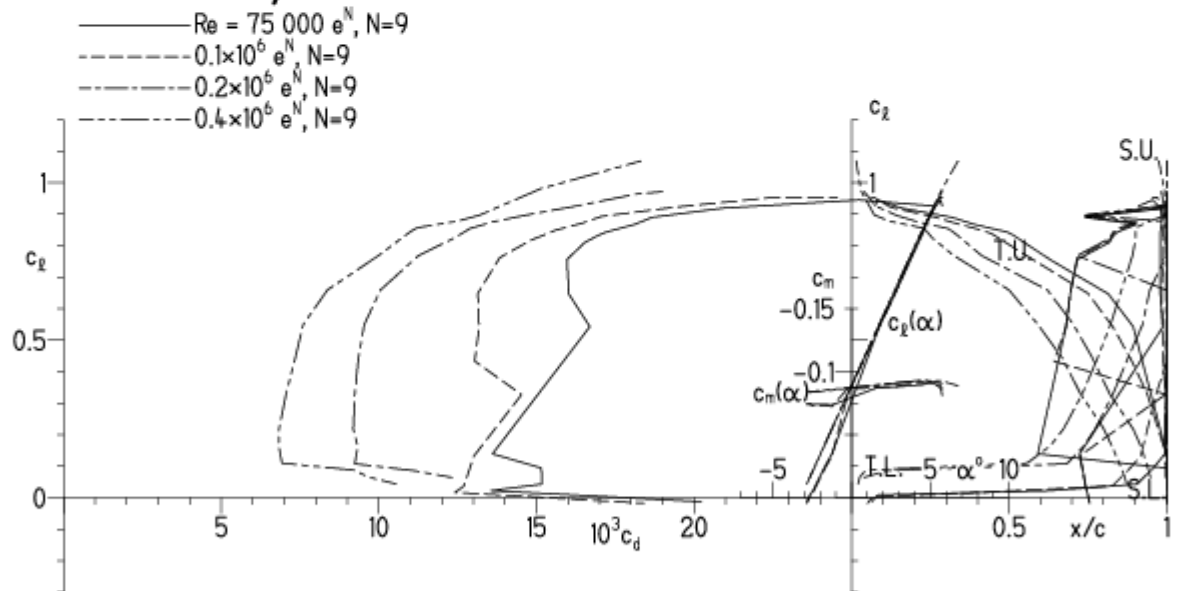
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38

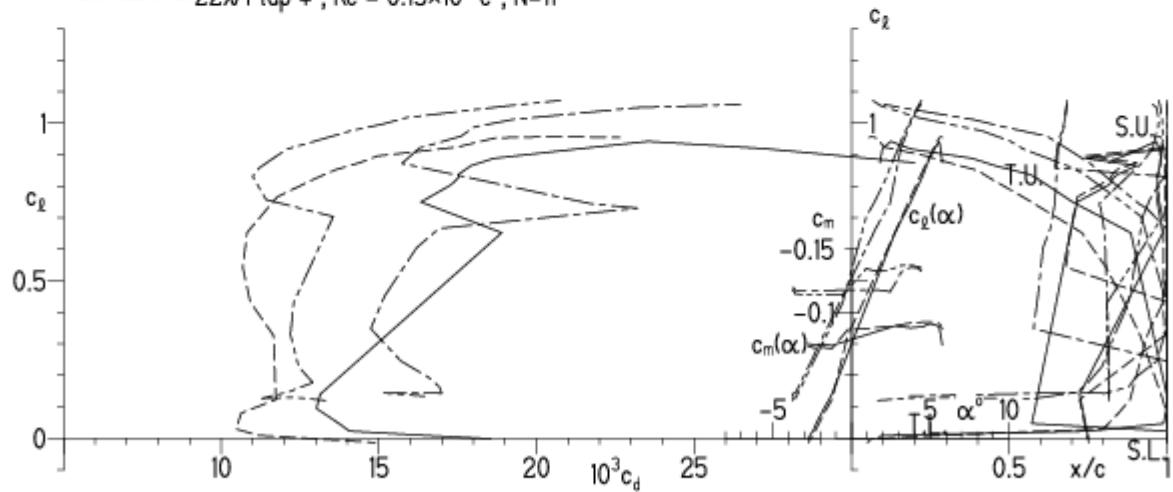


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2 × 10⁶ e^N, N=11
- - - 0.6 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.2 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.6 × 10⁶ e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

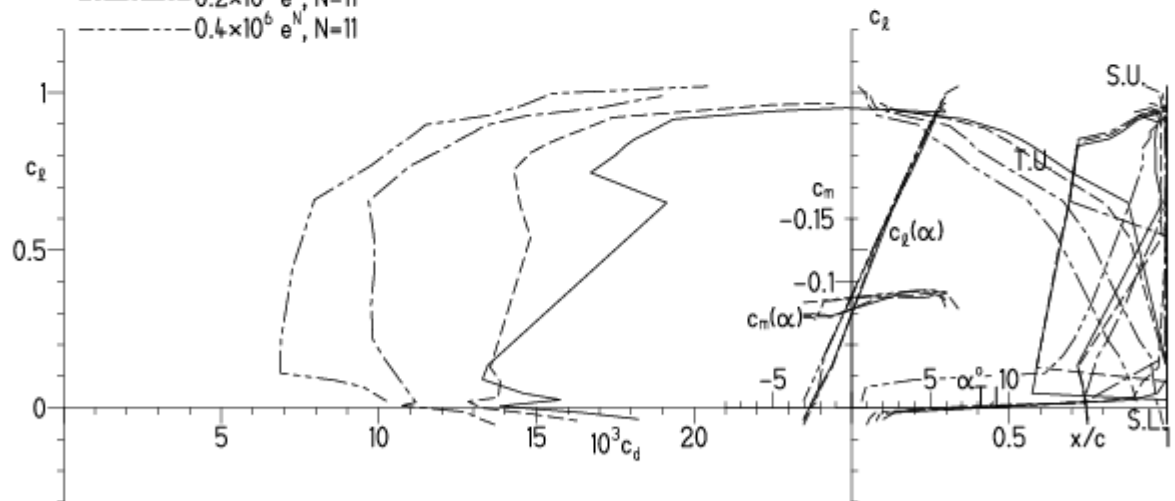
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



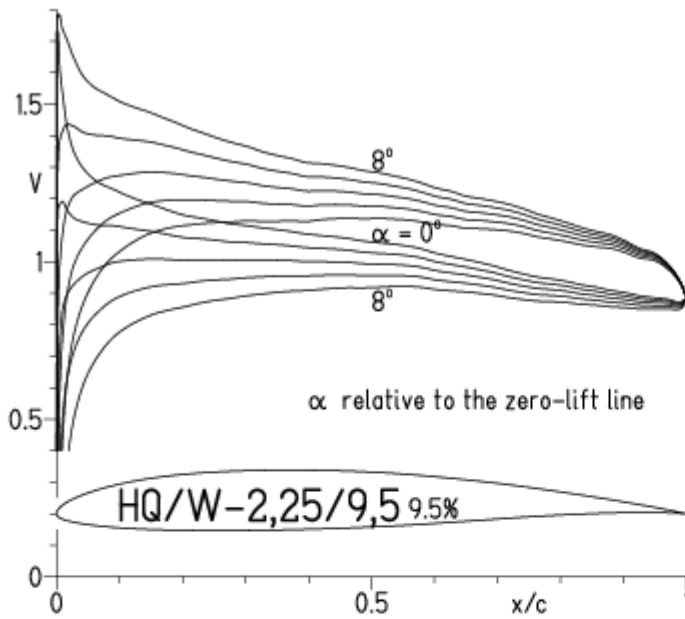
EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%

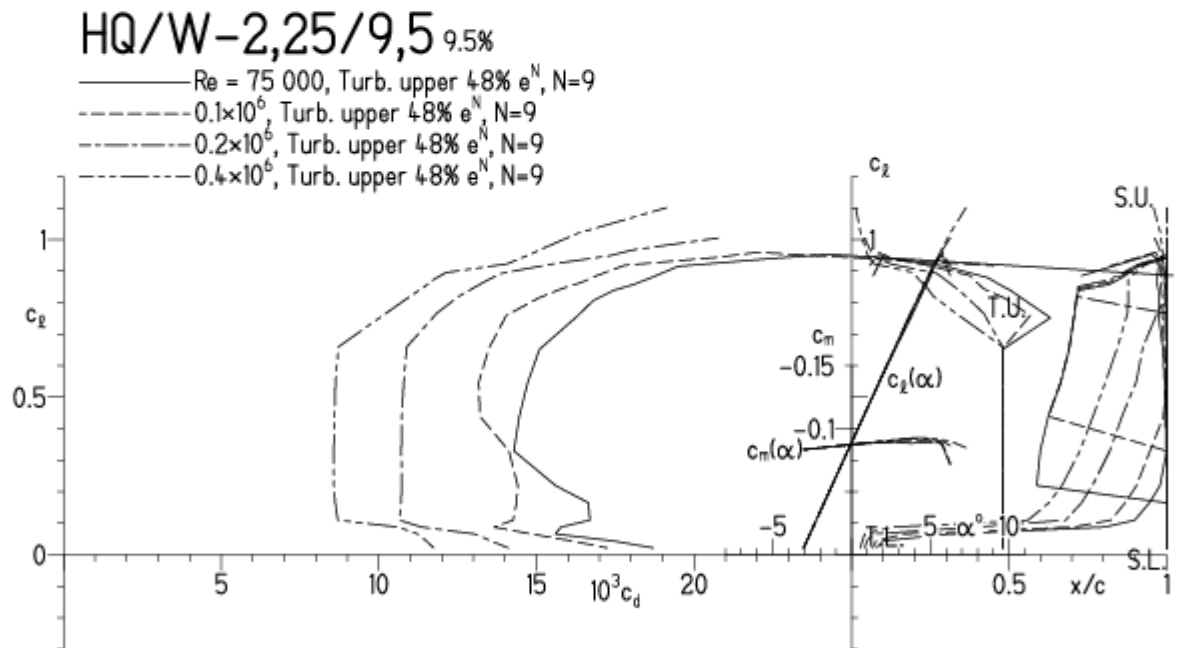


HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

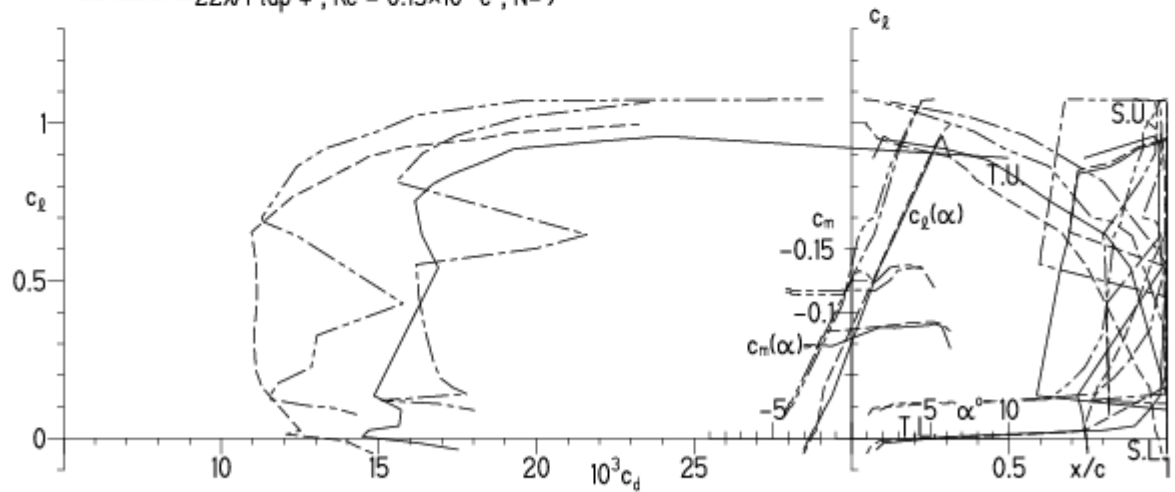


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



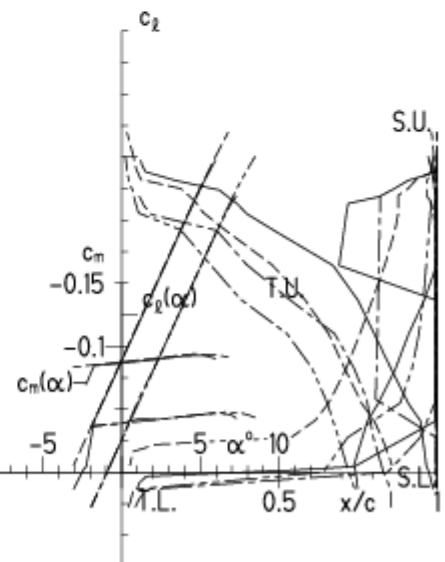
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

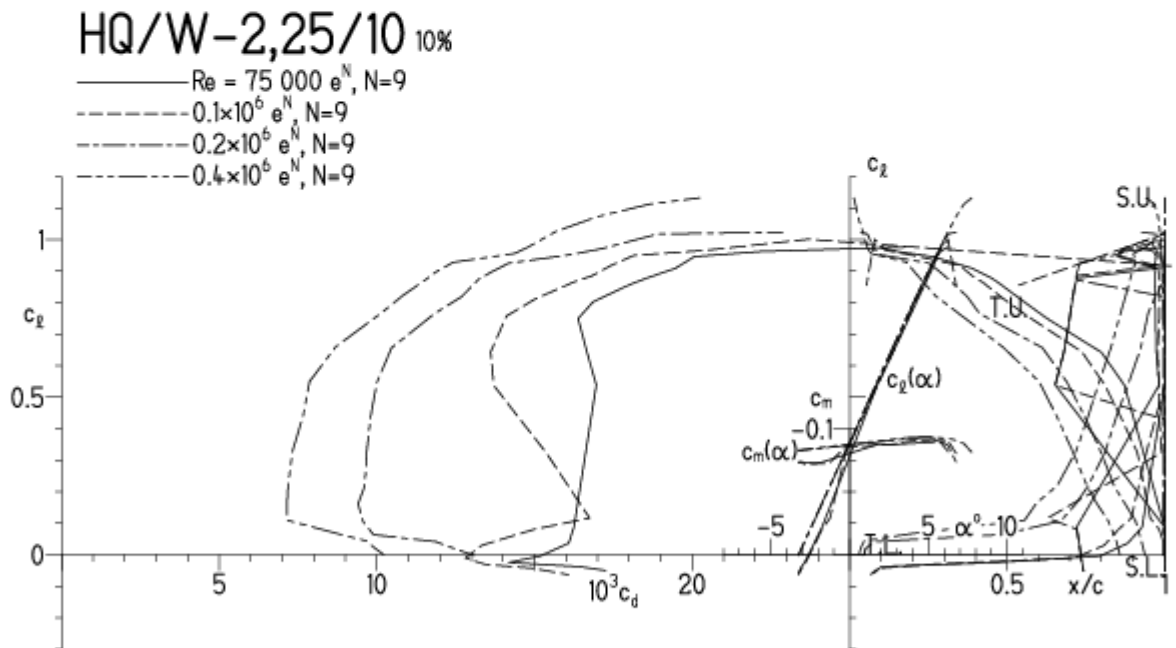


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

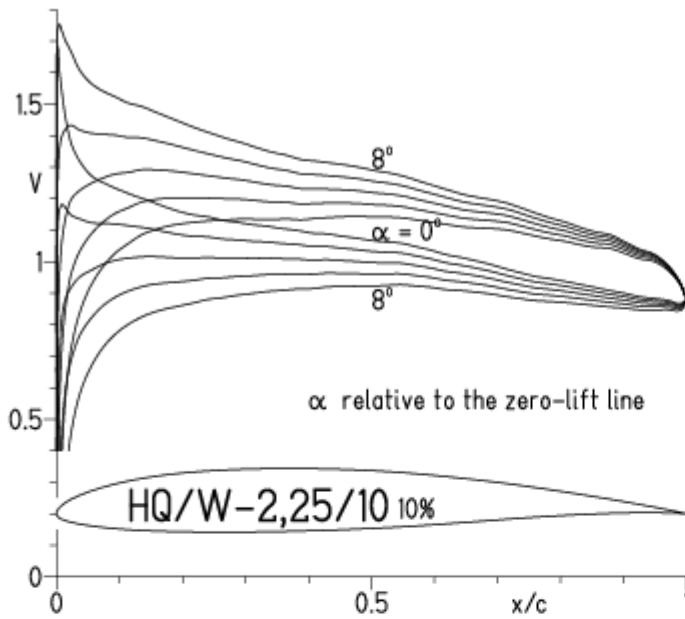


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

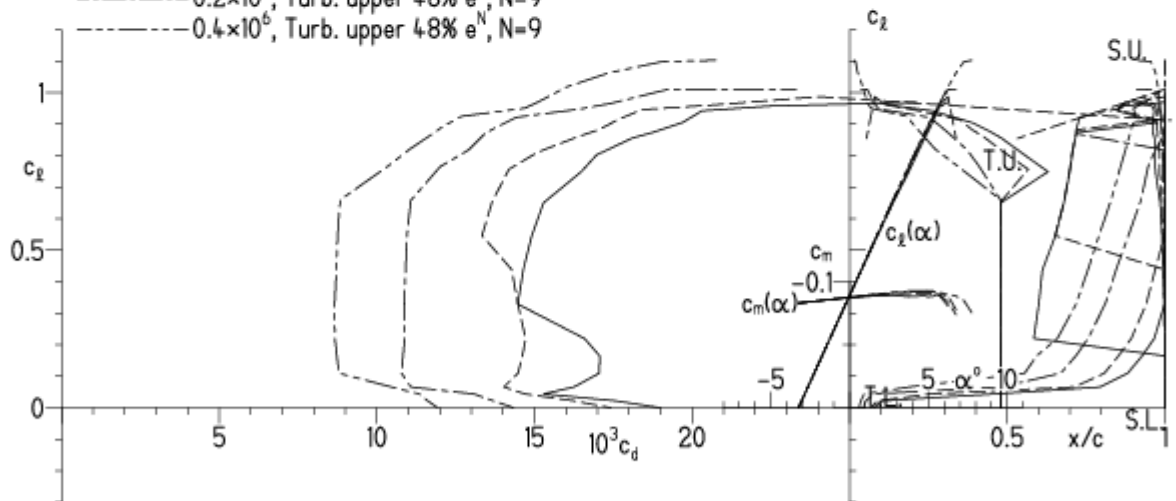
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

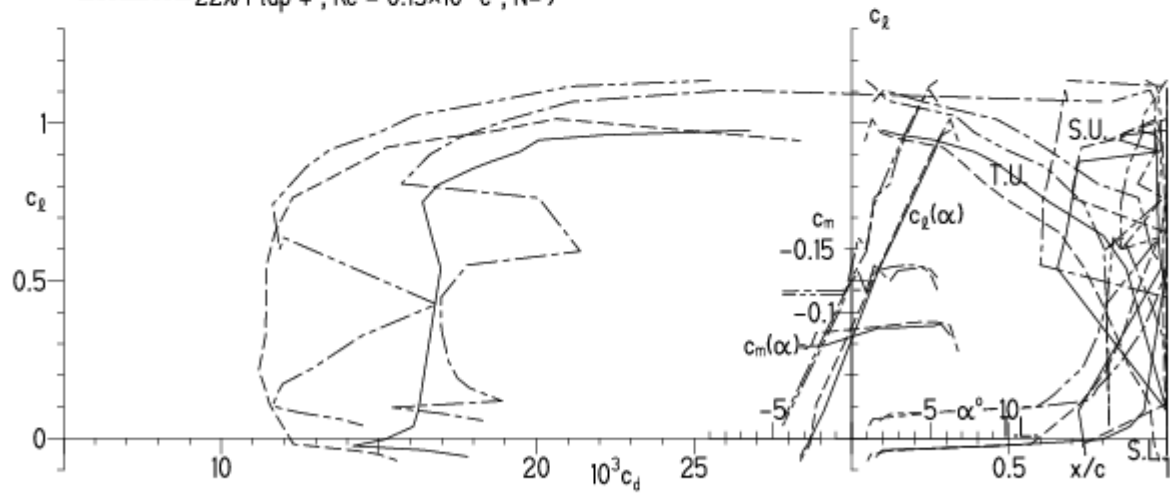


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

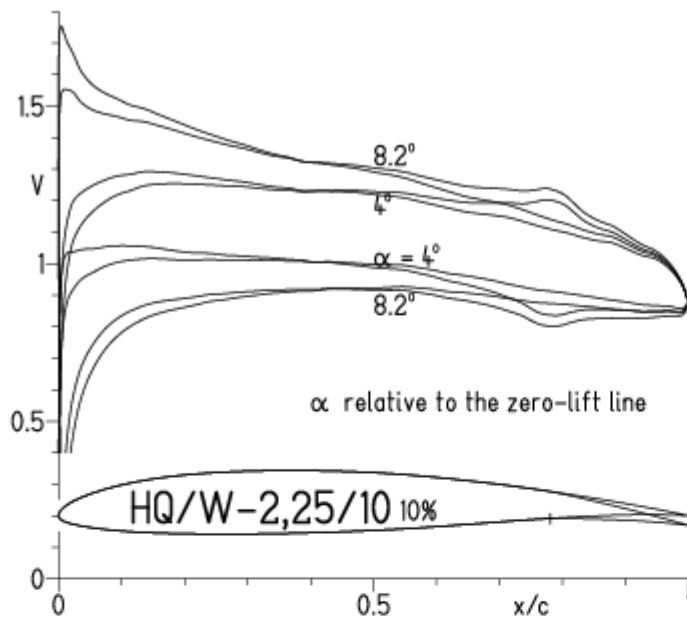
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

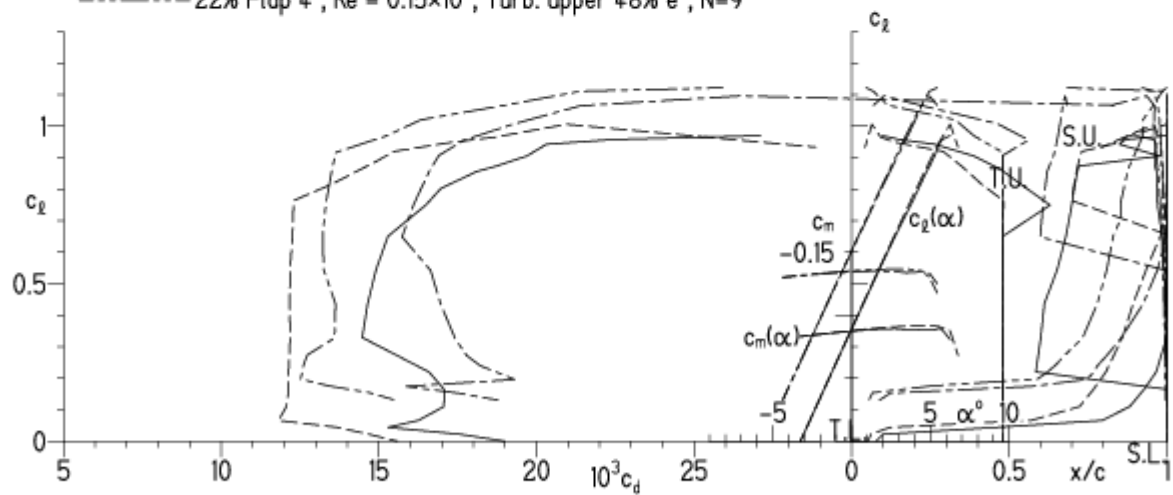


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

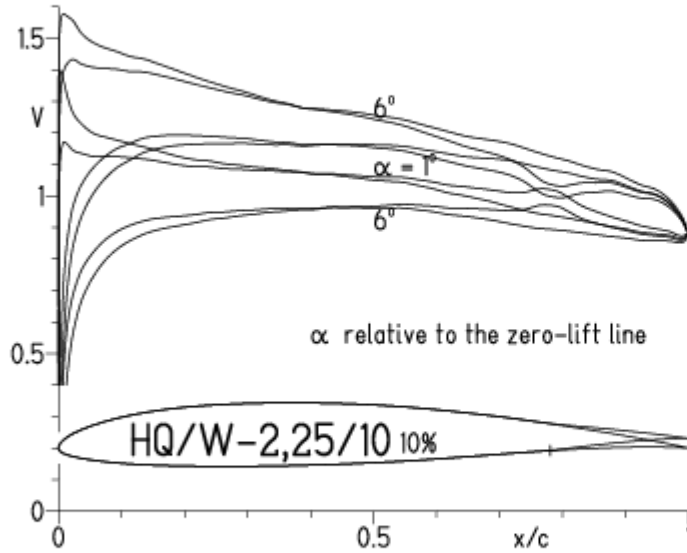
- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

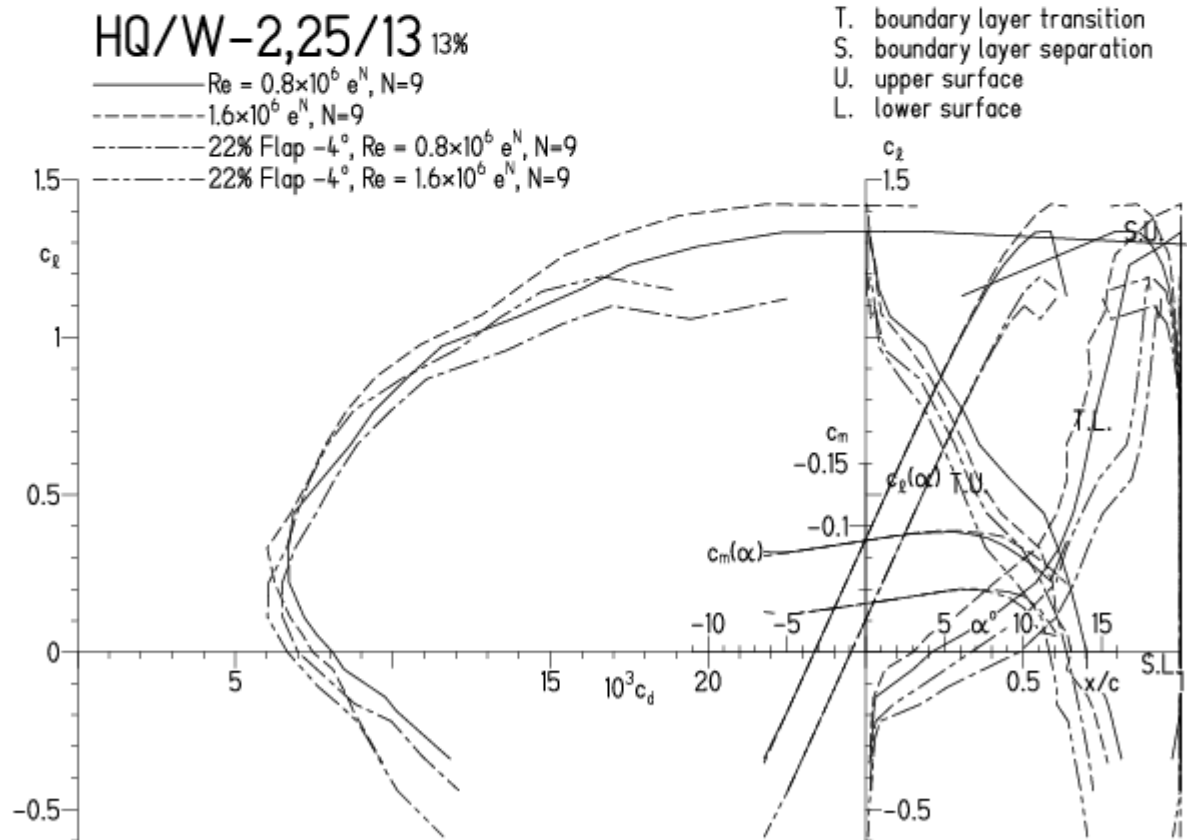


HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

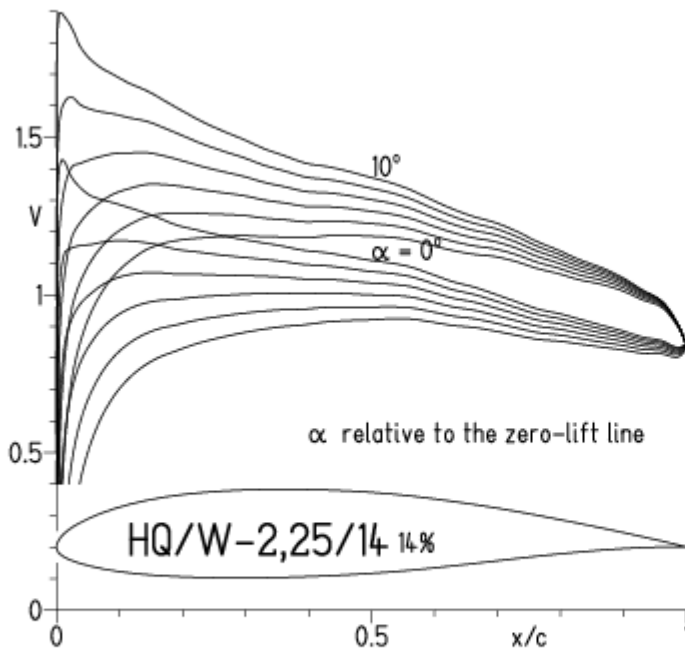


EPPLER 2005 V. 8.

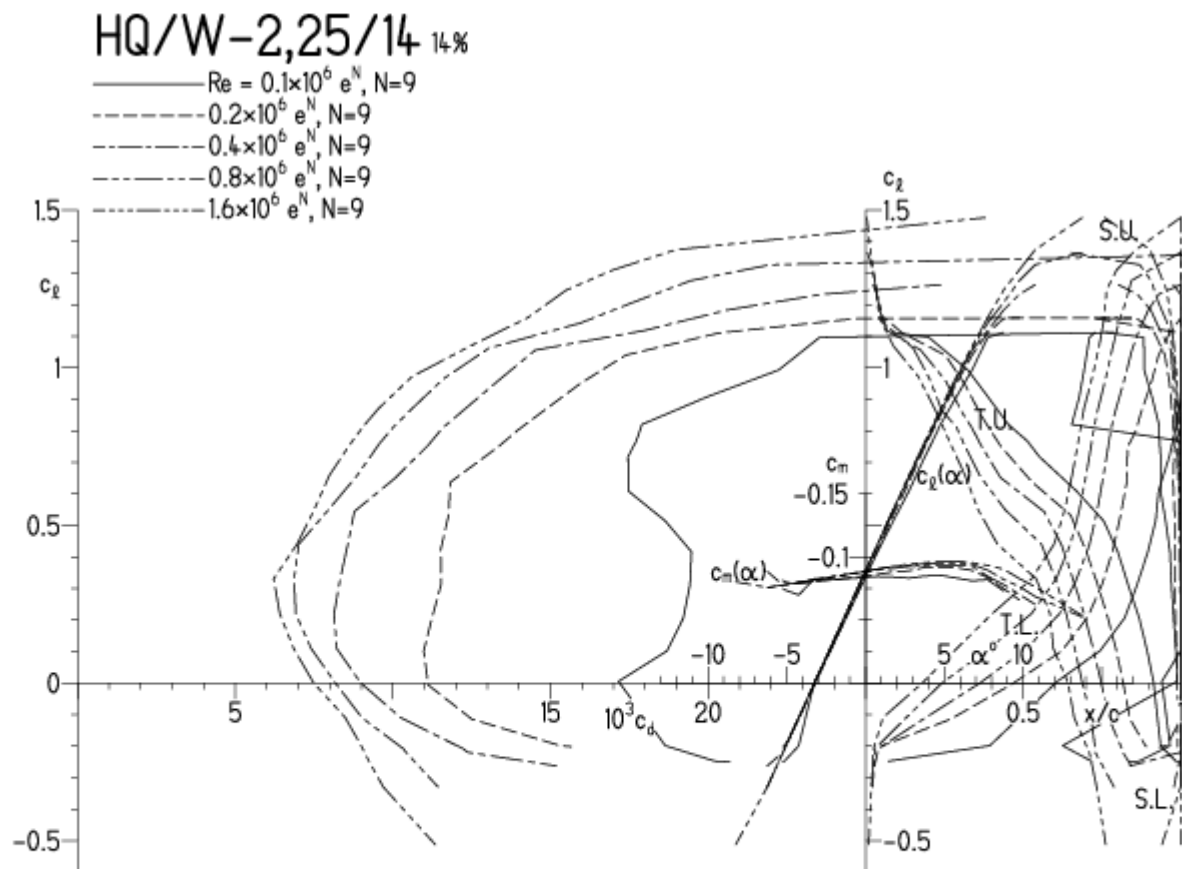


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

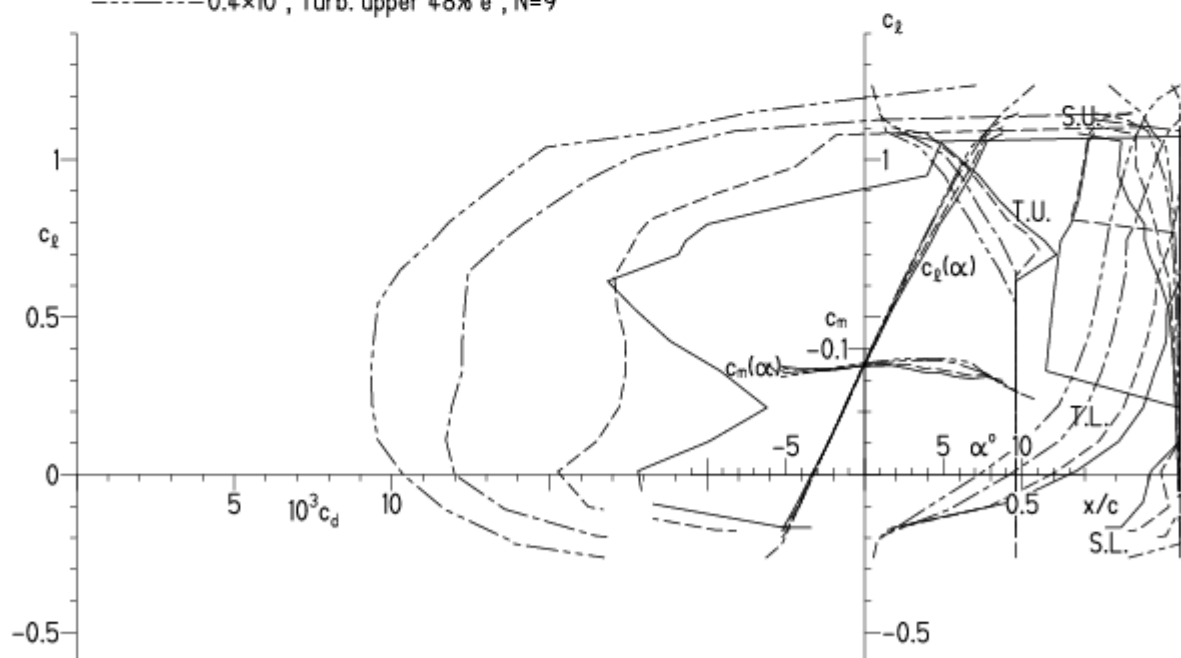
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

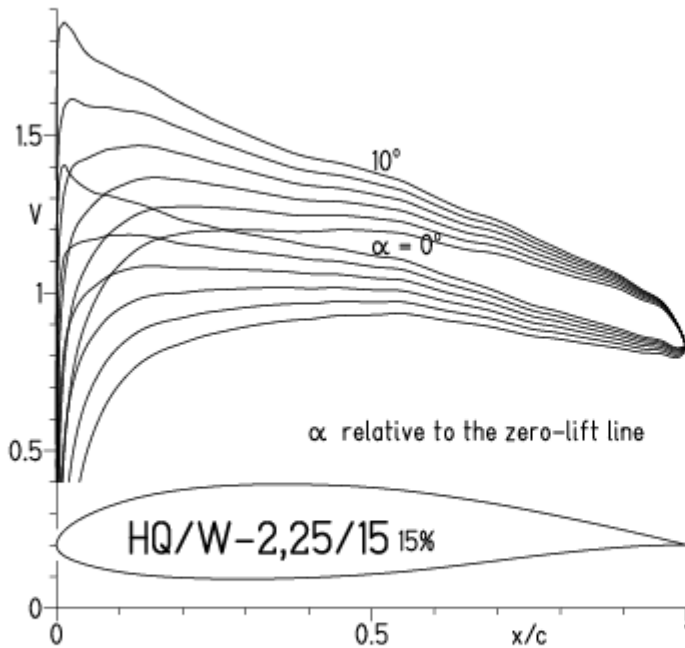


EPPLER 2005 V. 8.5.07

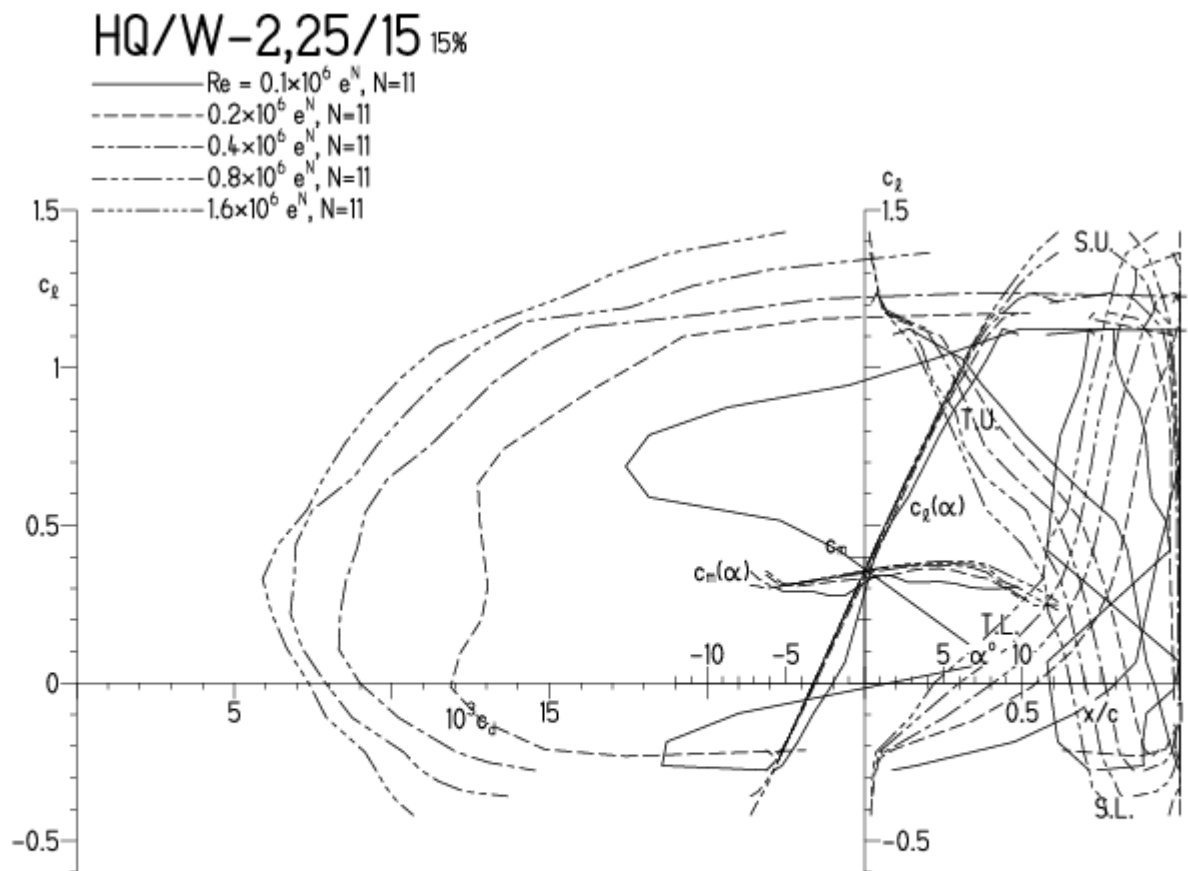


HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

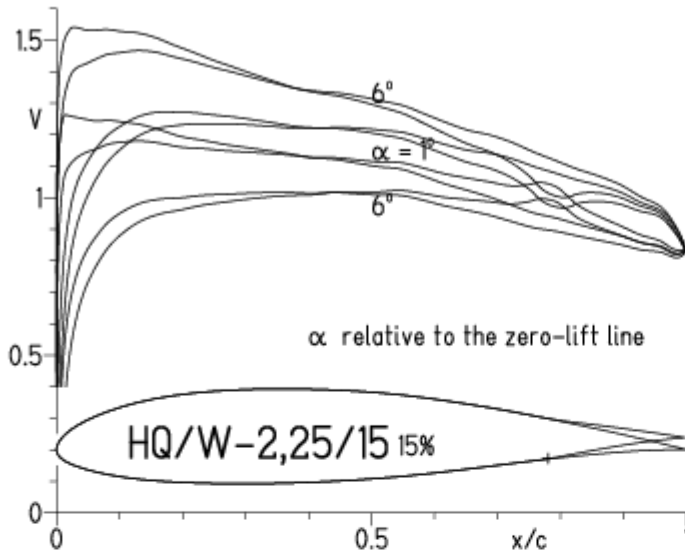


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

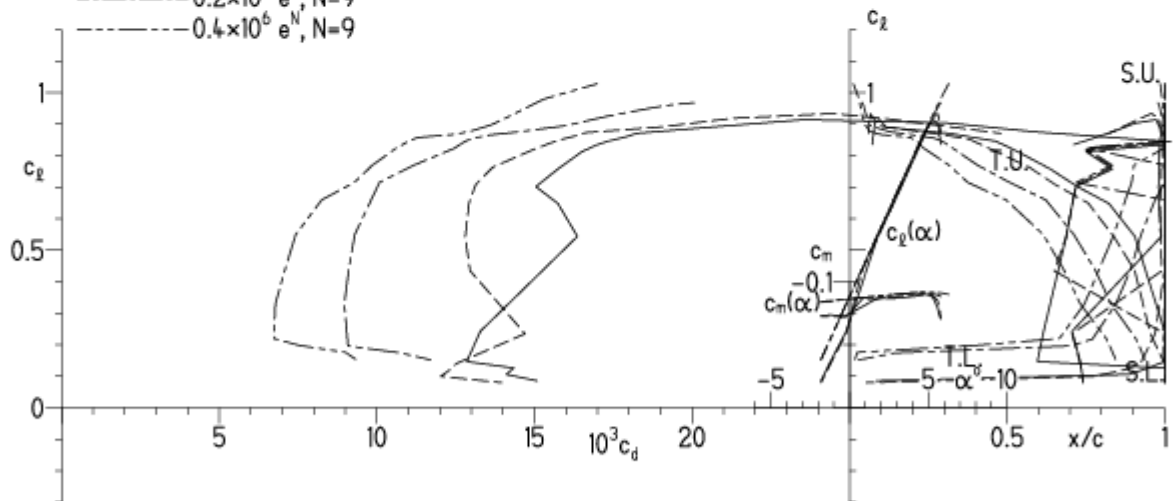
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

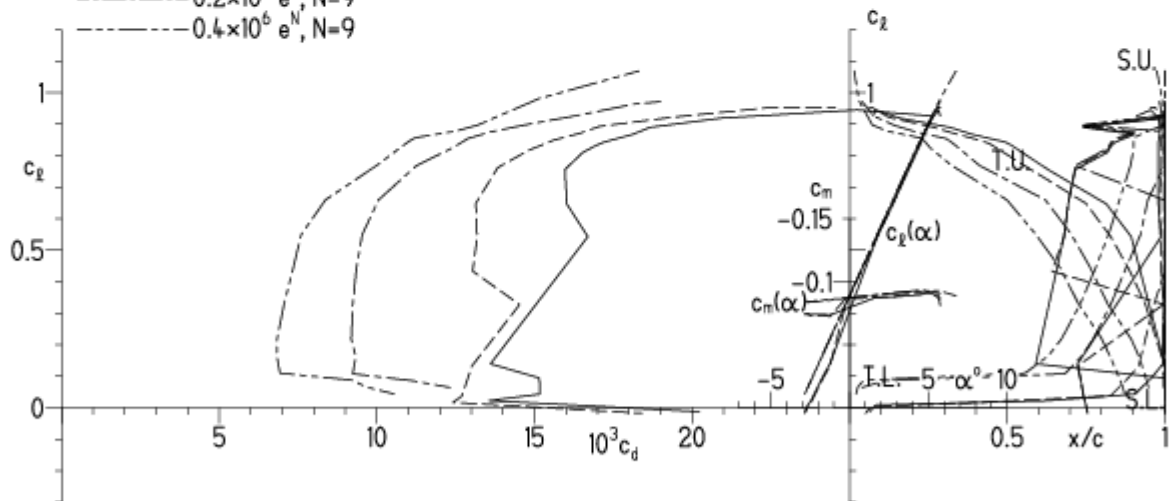
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

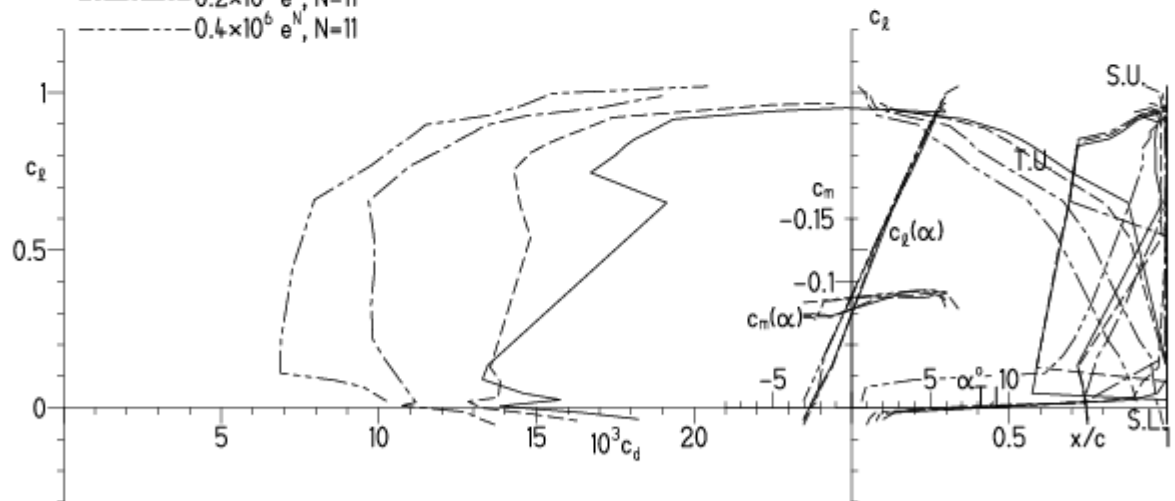
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

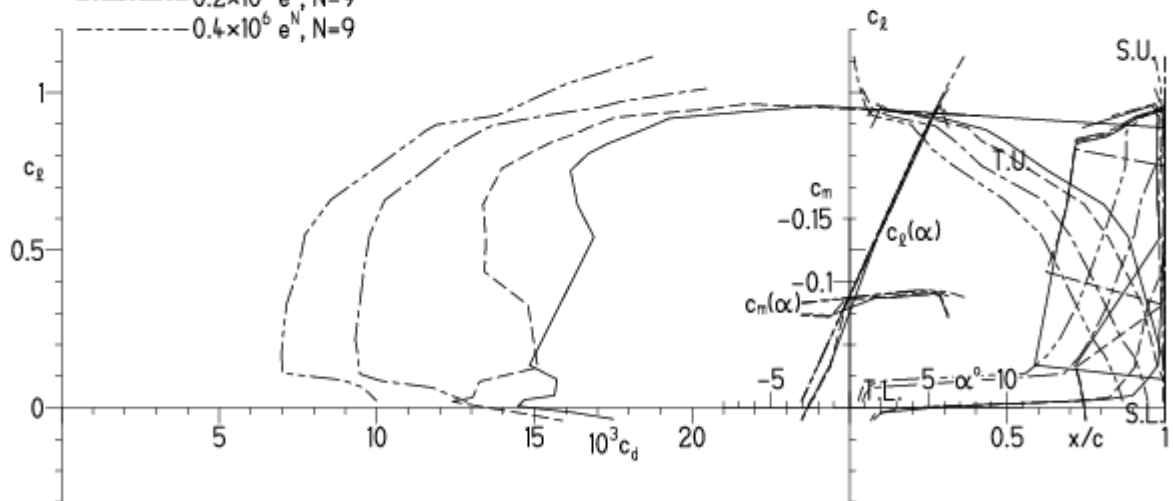
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

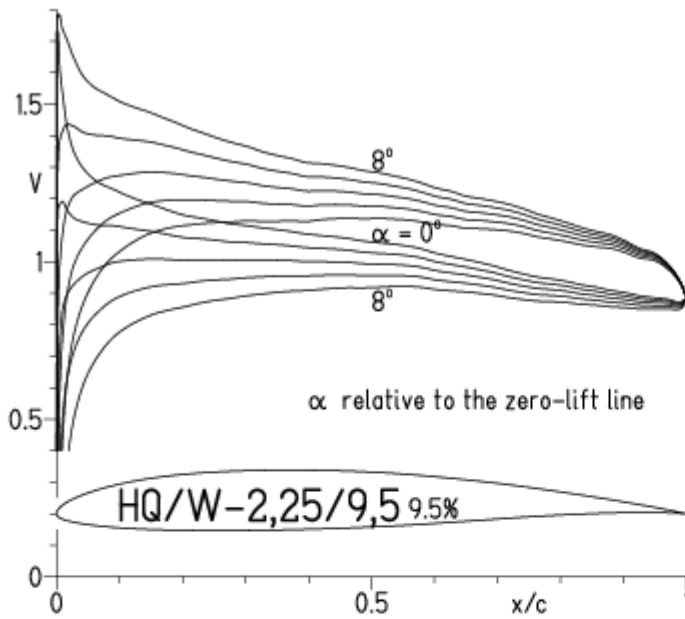
HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

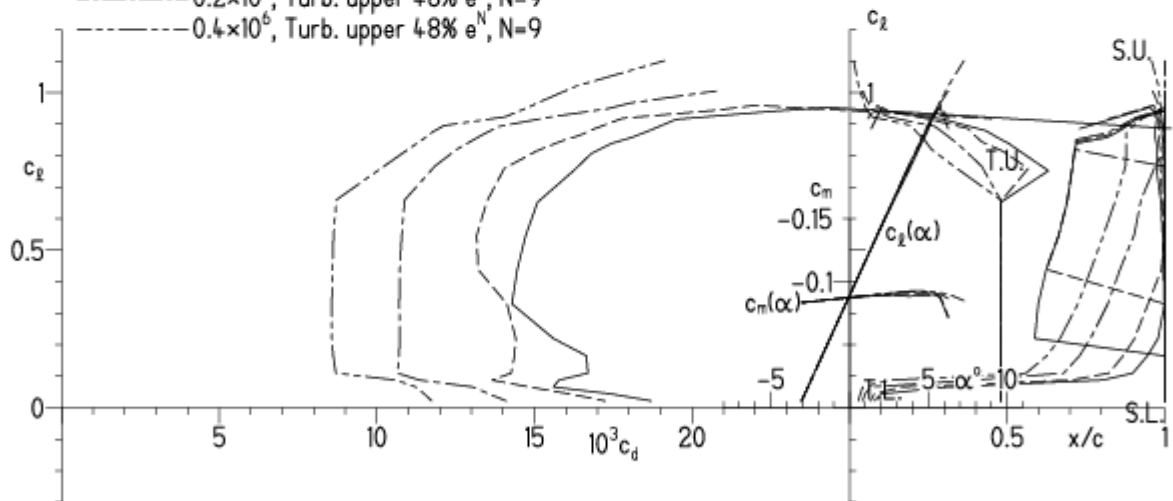
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

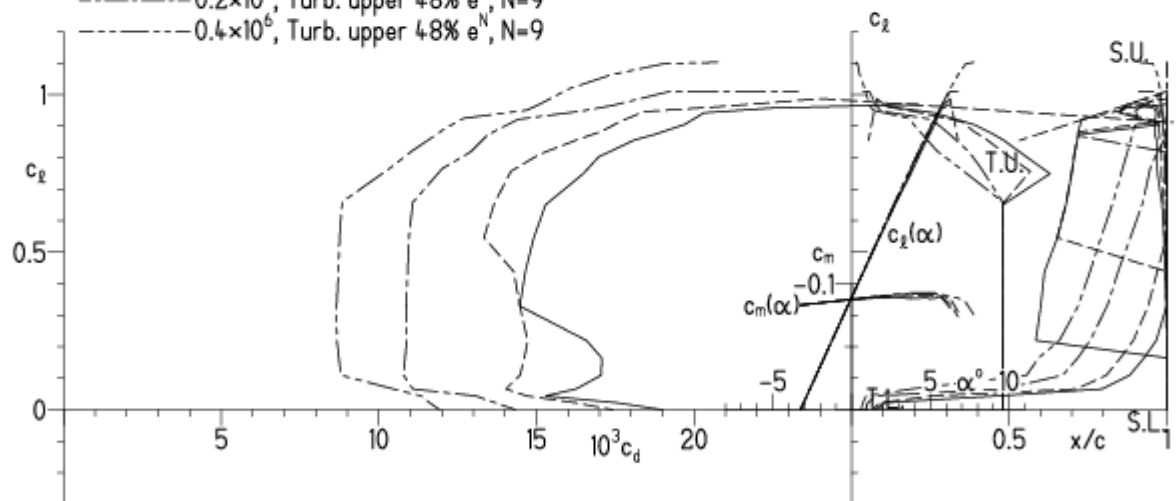
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

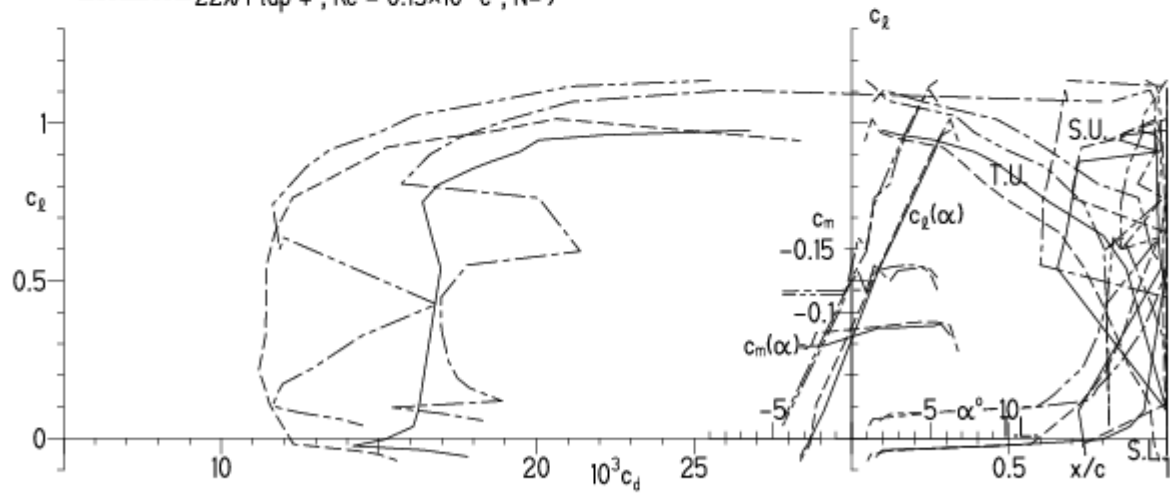


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

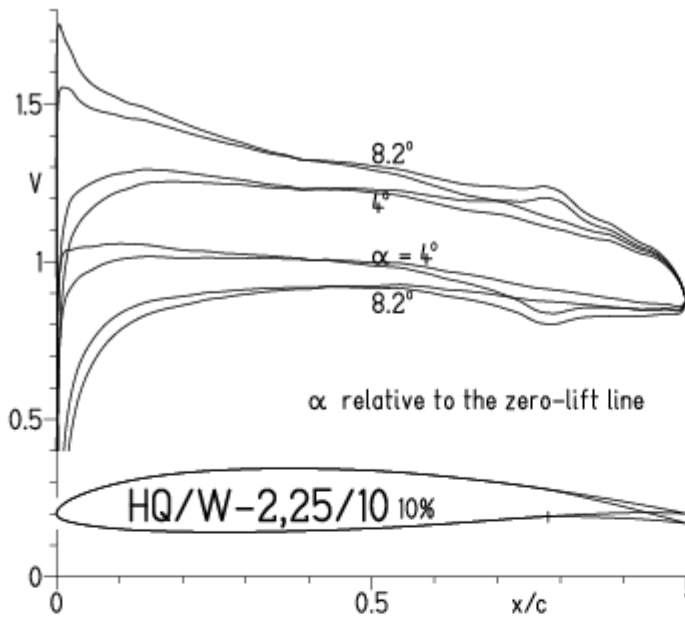
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

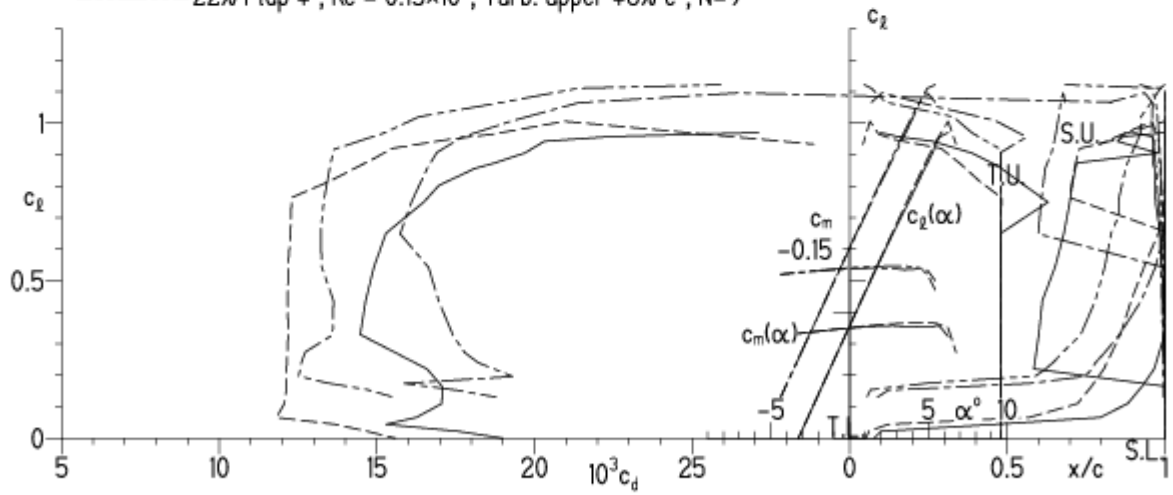


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

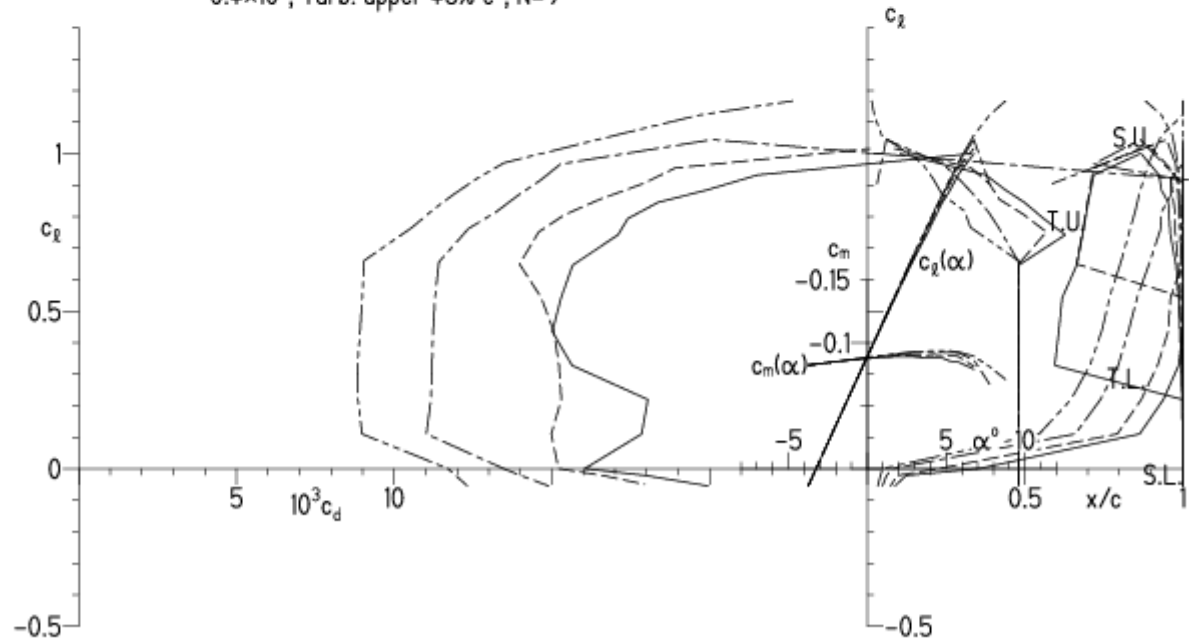
EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

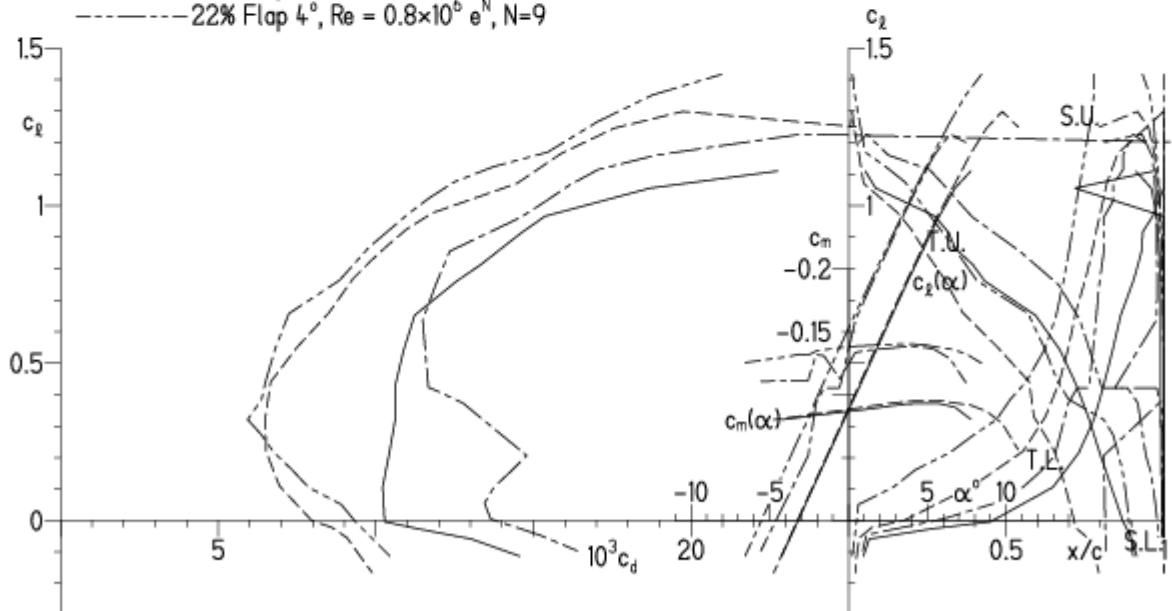


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

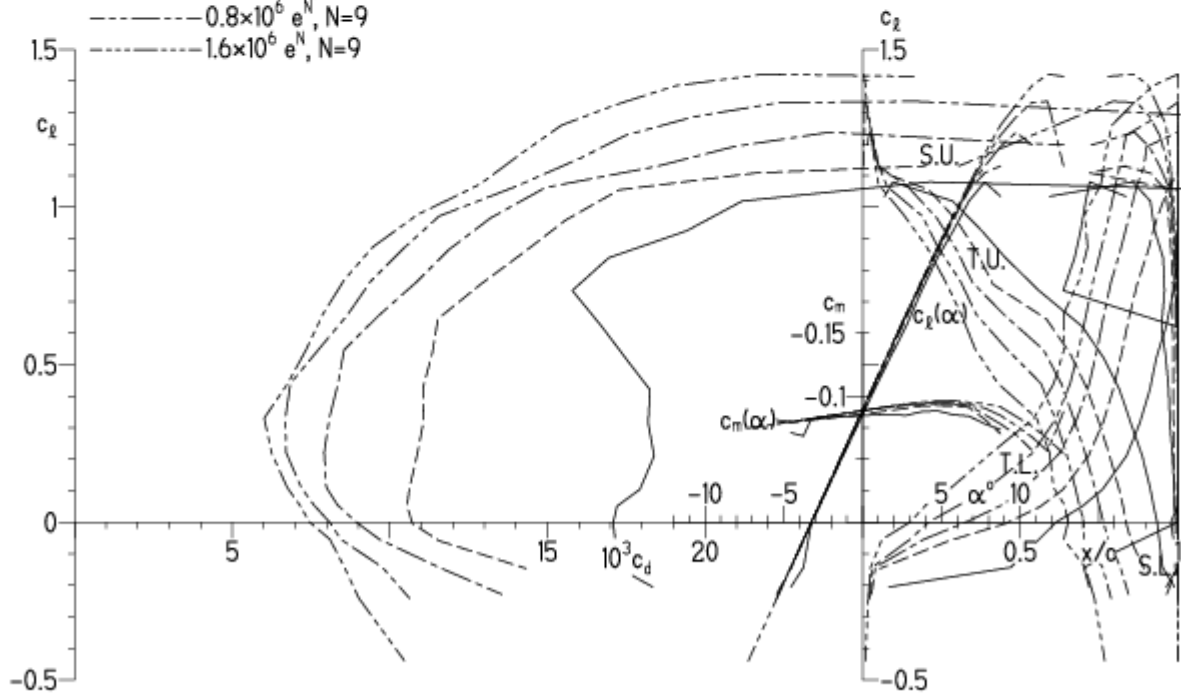
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

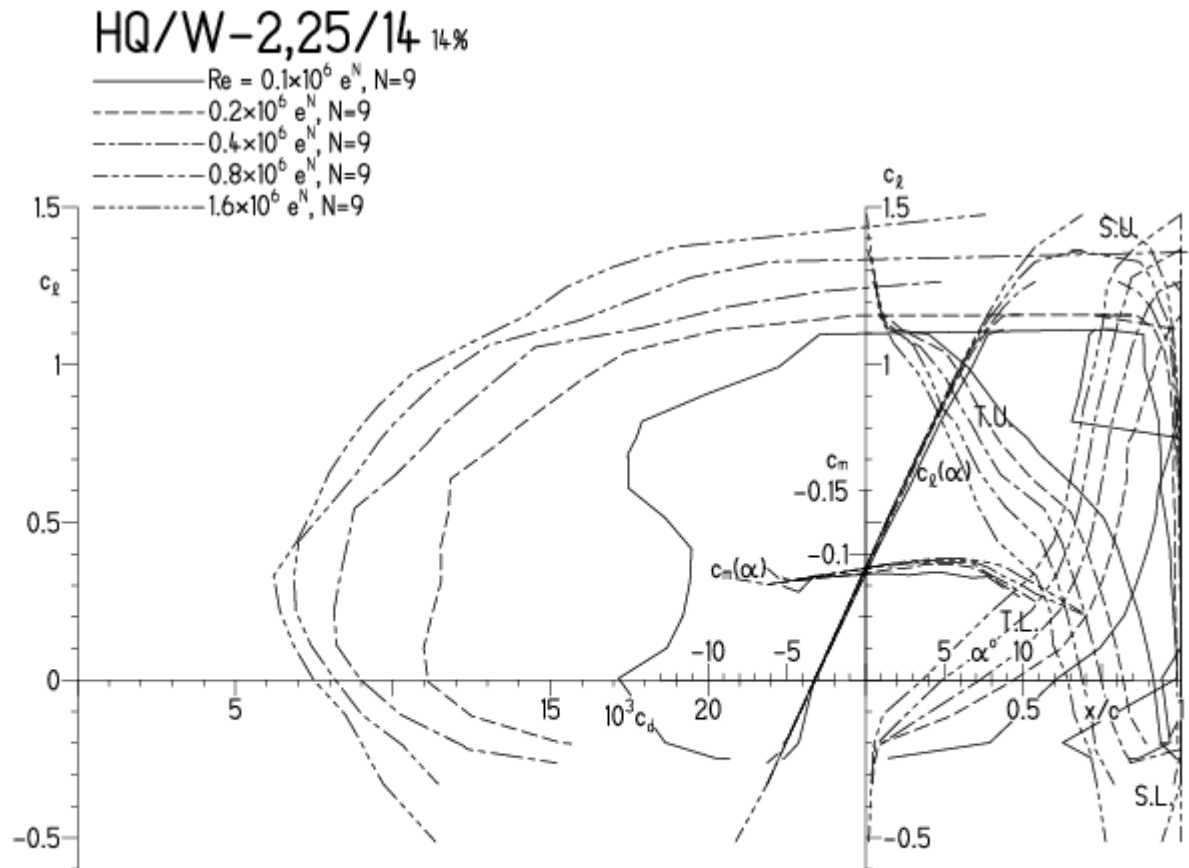


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

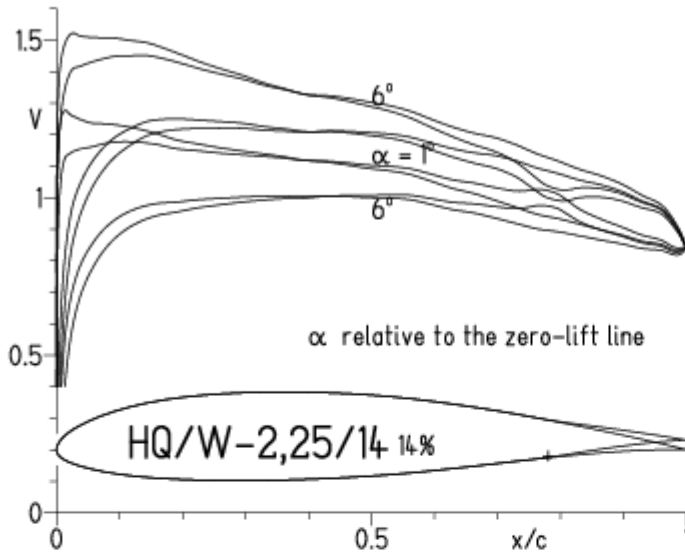
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

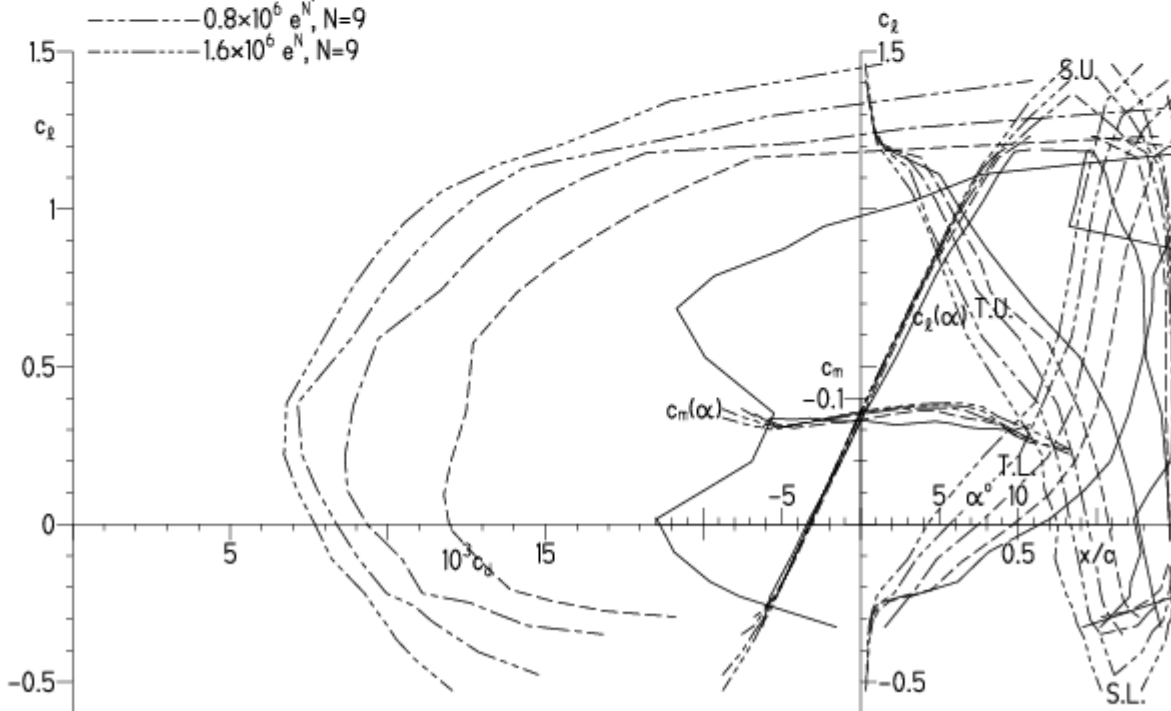
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

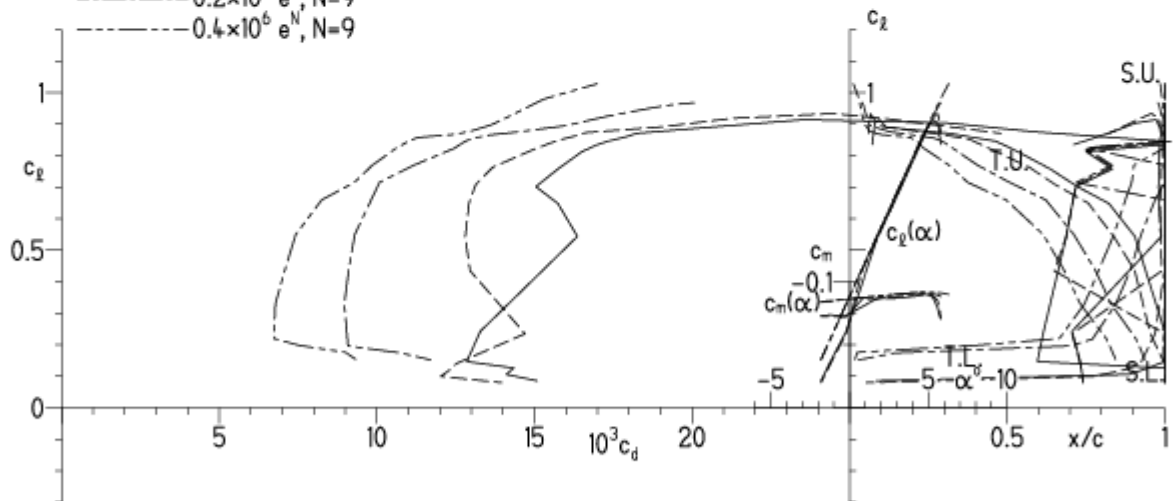
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

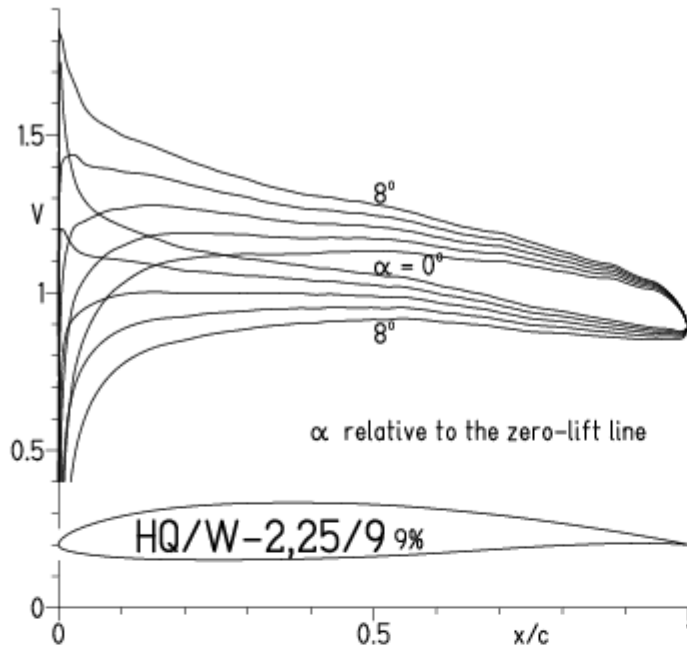


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

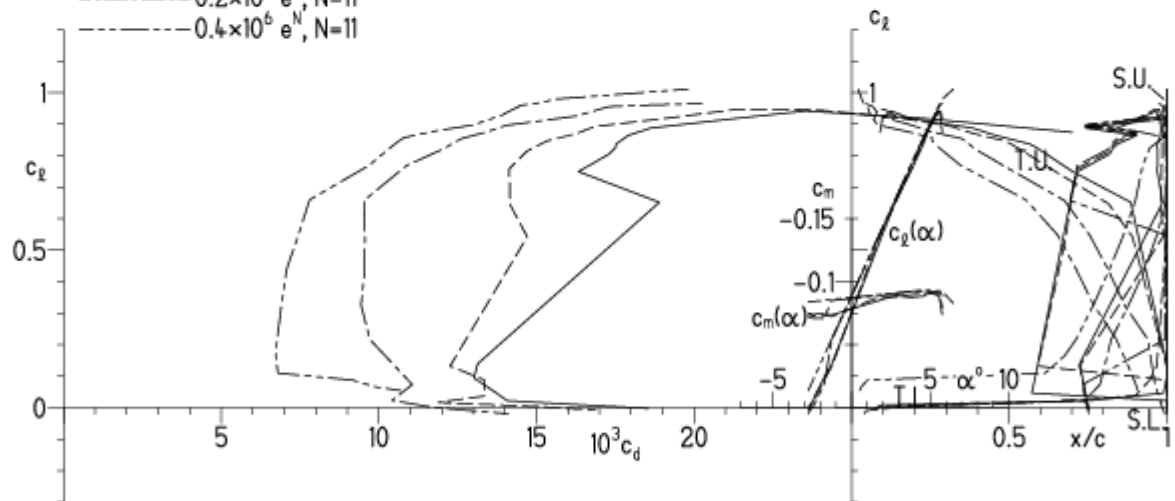
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



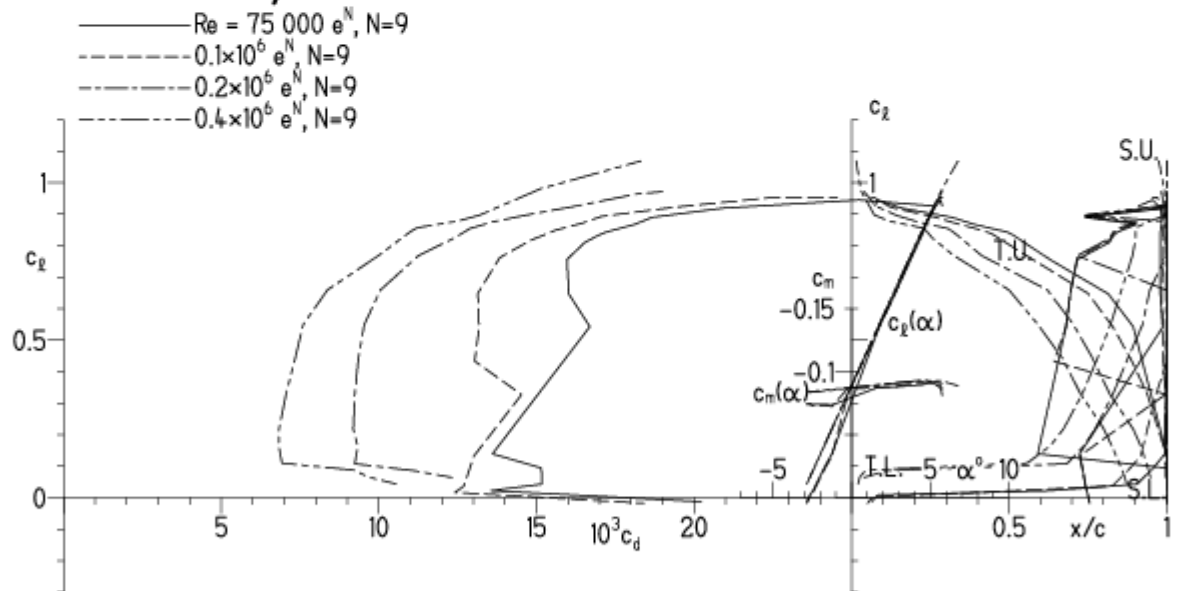
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

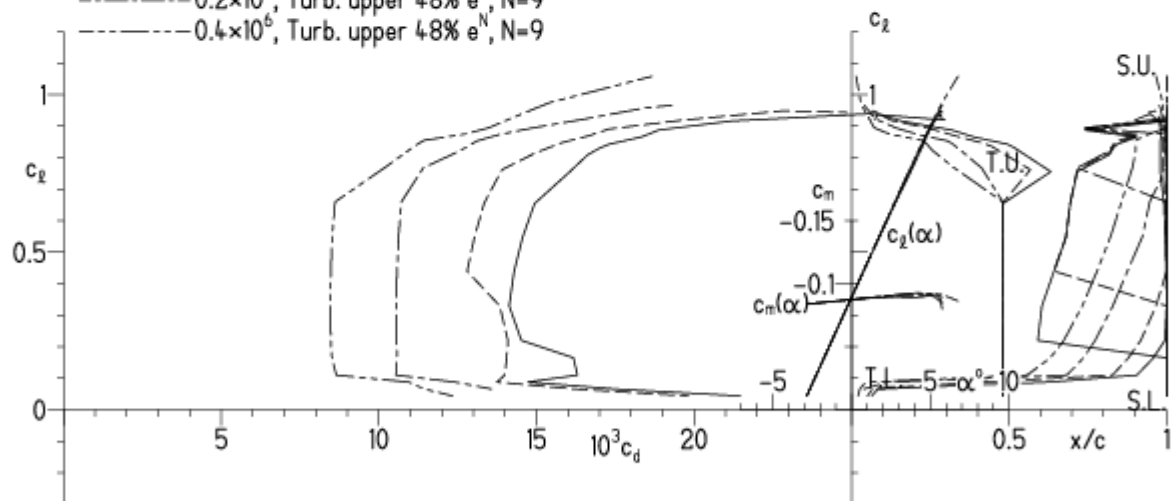
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38

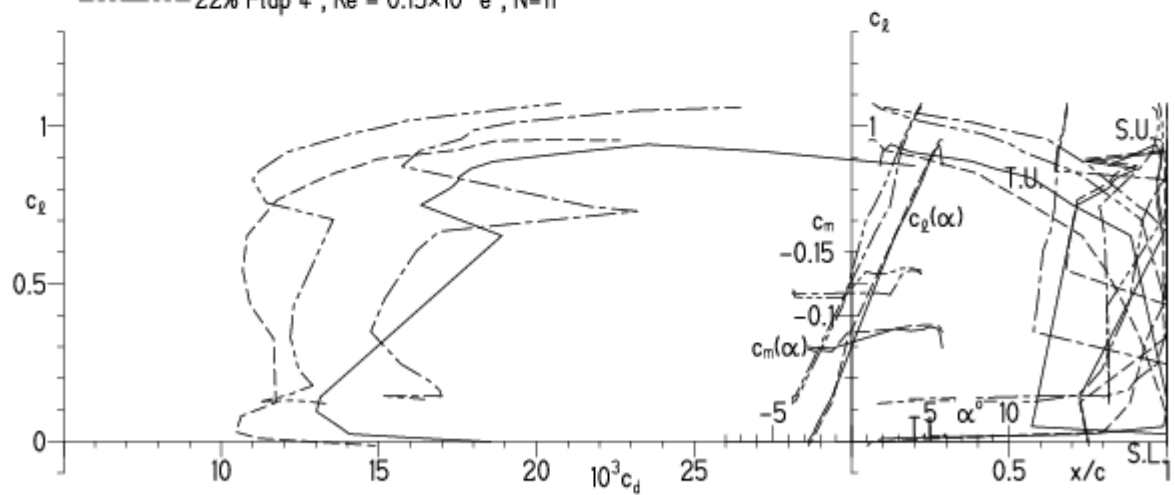


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

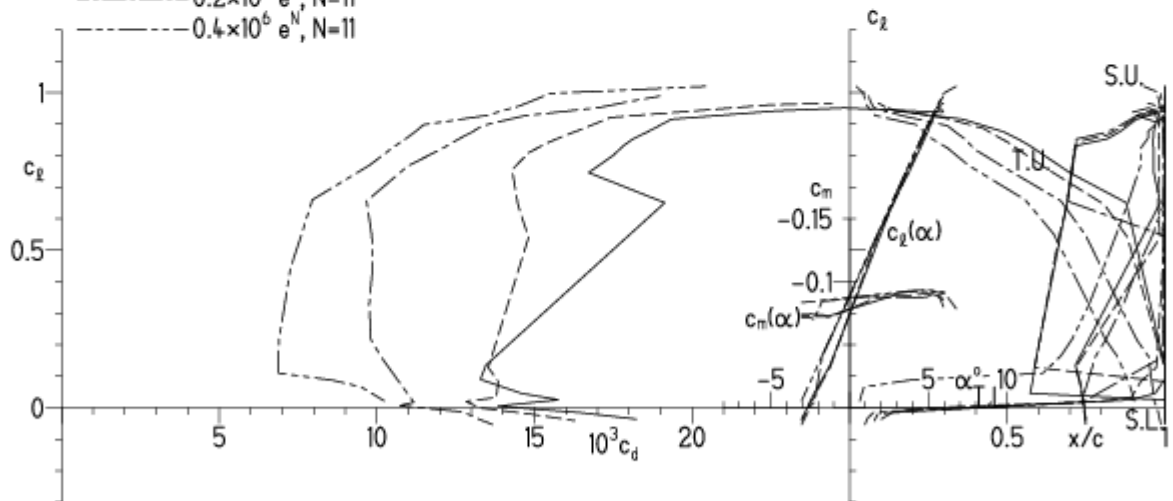
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

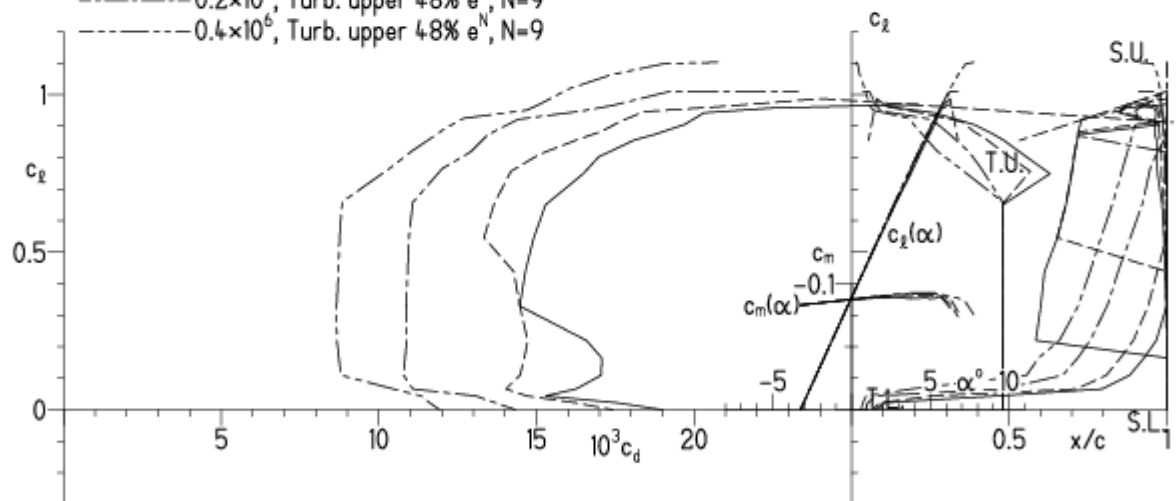
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

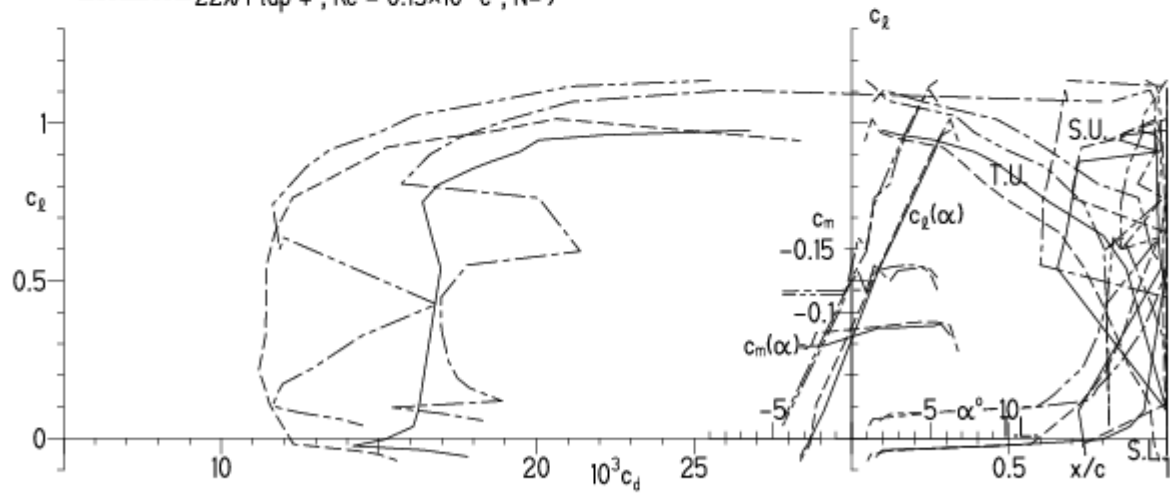


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

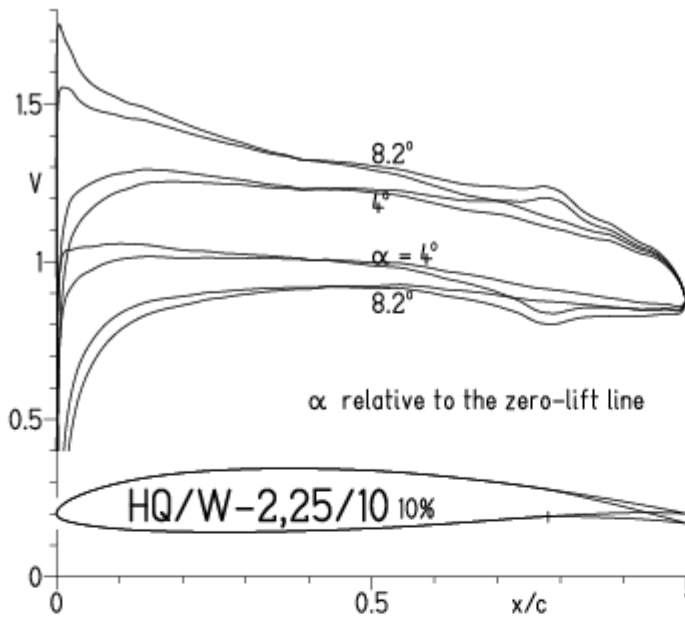
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

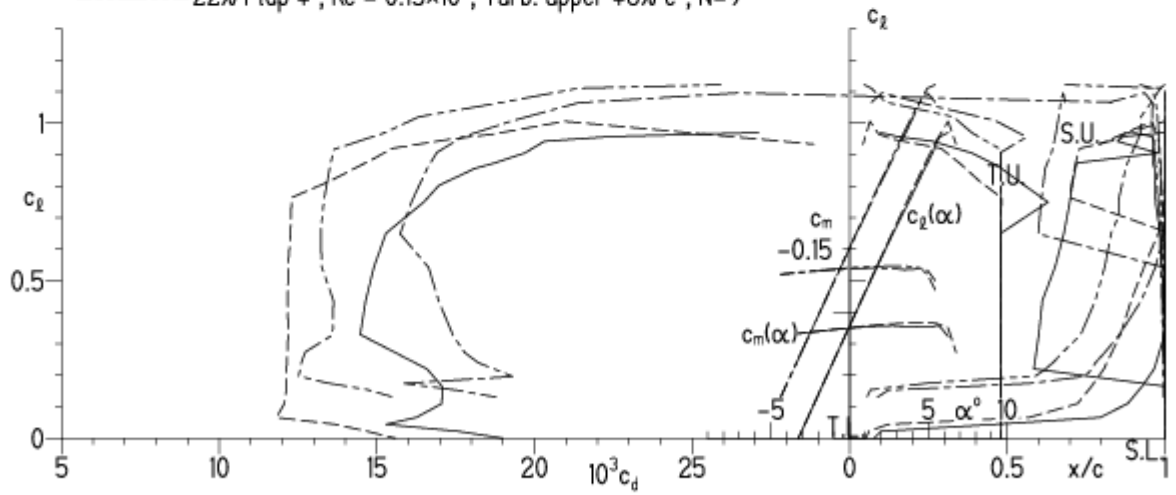


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

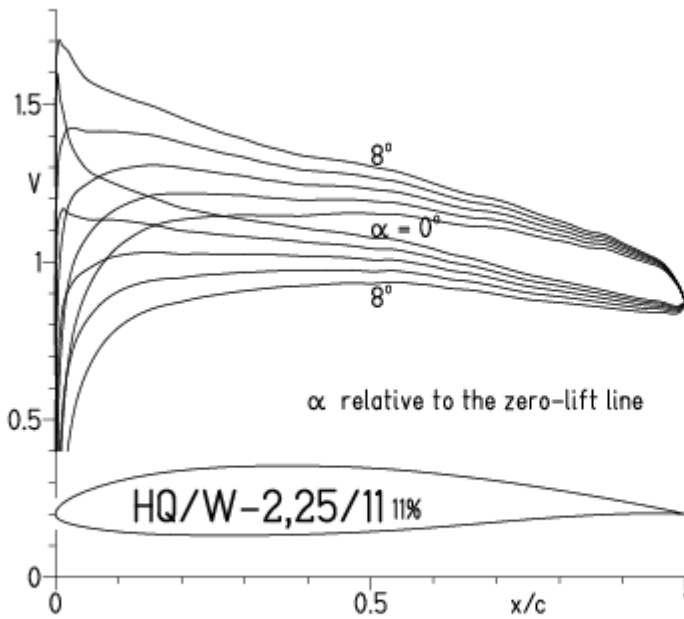


EPPLER 2005 V. 8.5.07 RUN

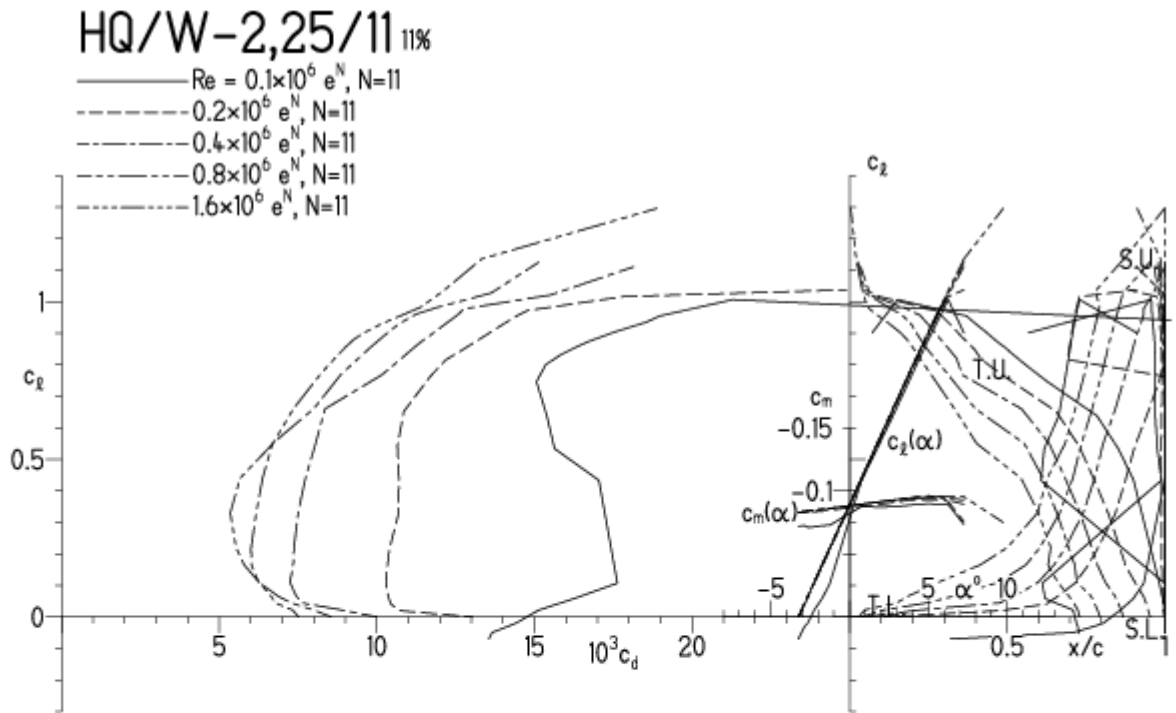


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6$, e^N , $N=9$
- - - 0.2×10^6 , e^N , $N=9$
- · - 0.4×10^6 , e^N , $N=9$
- · - · 0.8×10^6 , e^N , $N=9$
- · - · - 1.6×10^6 , e^N , $N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

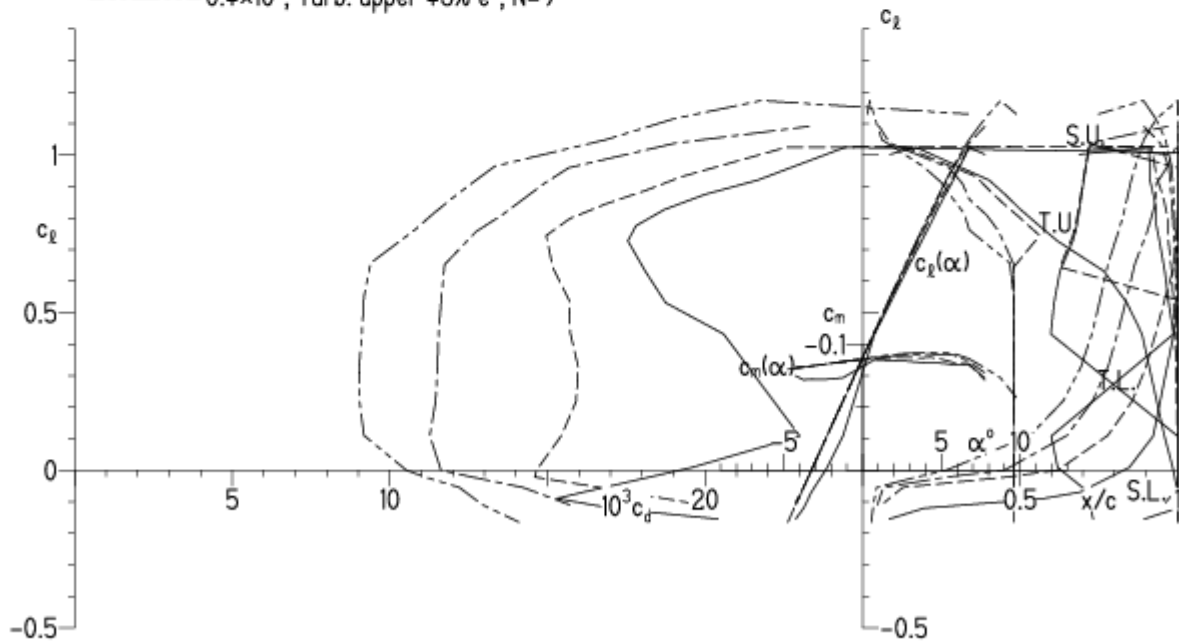
EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

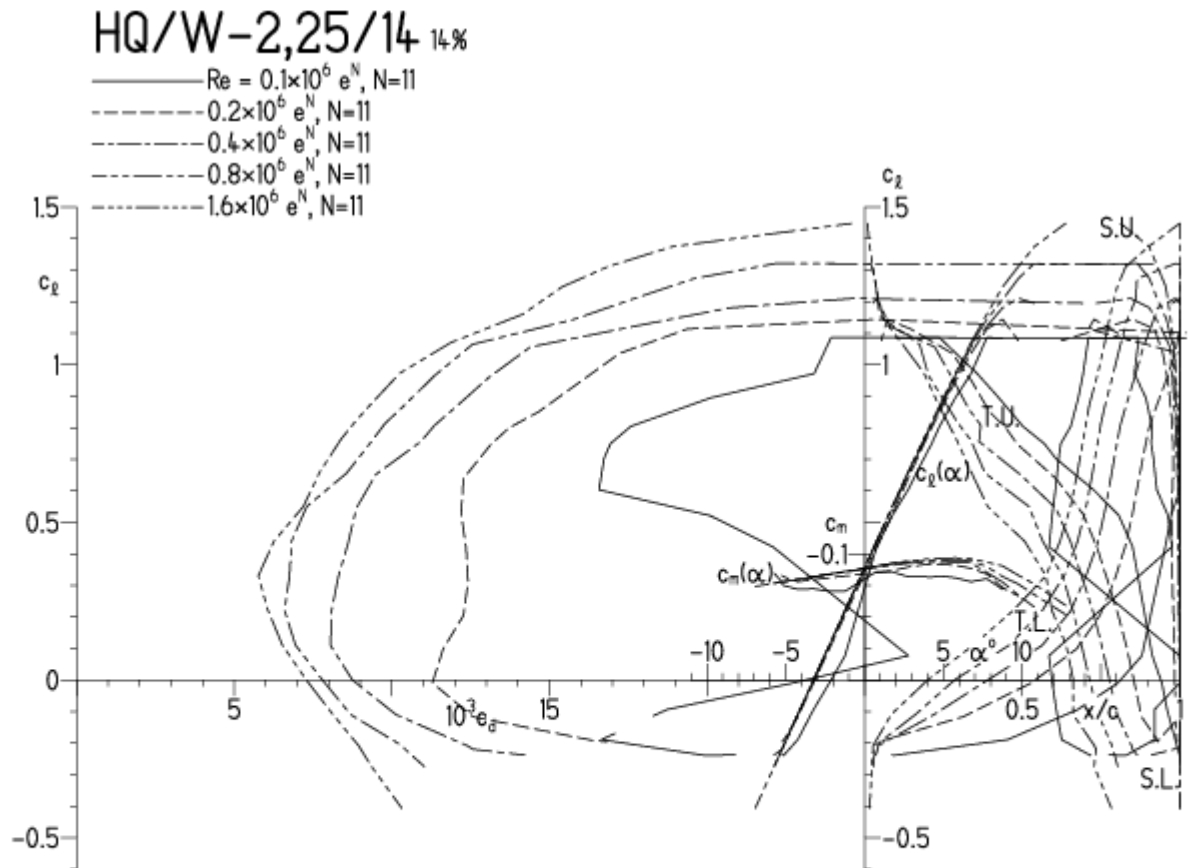


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

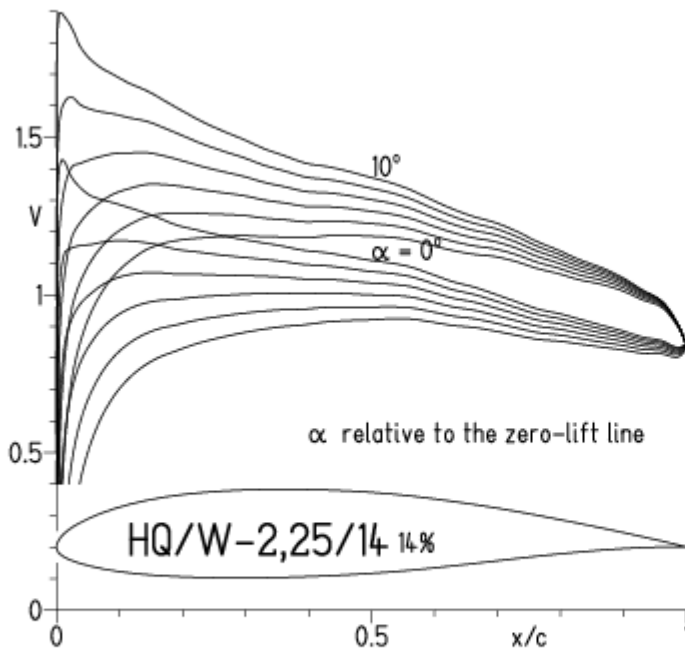


EPPLER 2005 V. 8.

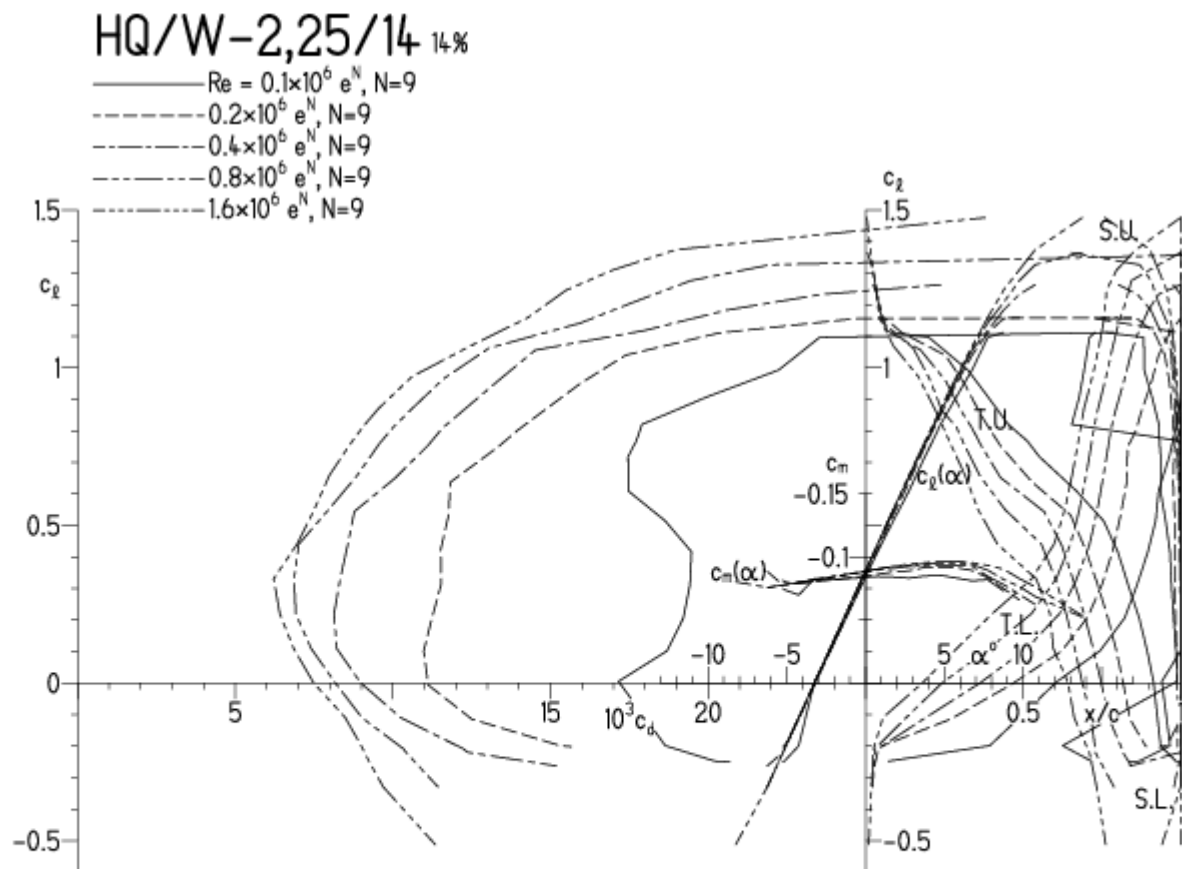


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

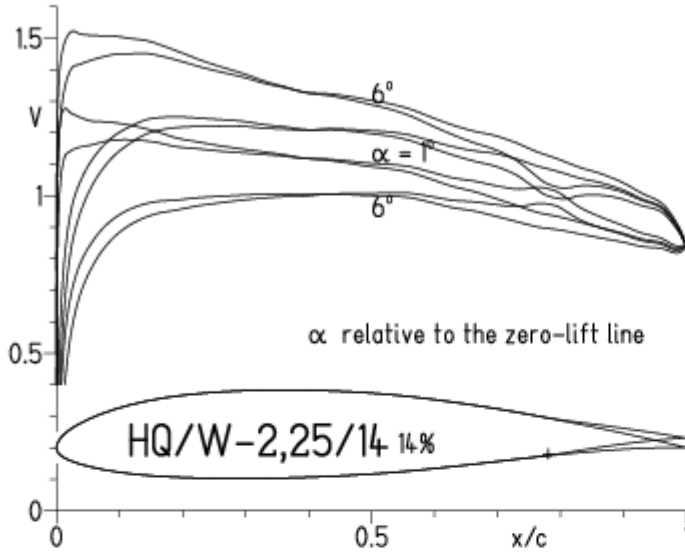
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

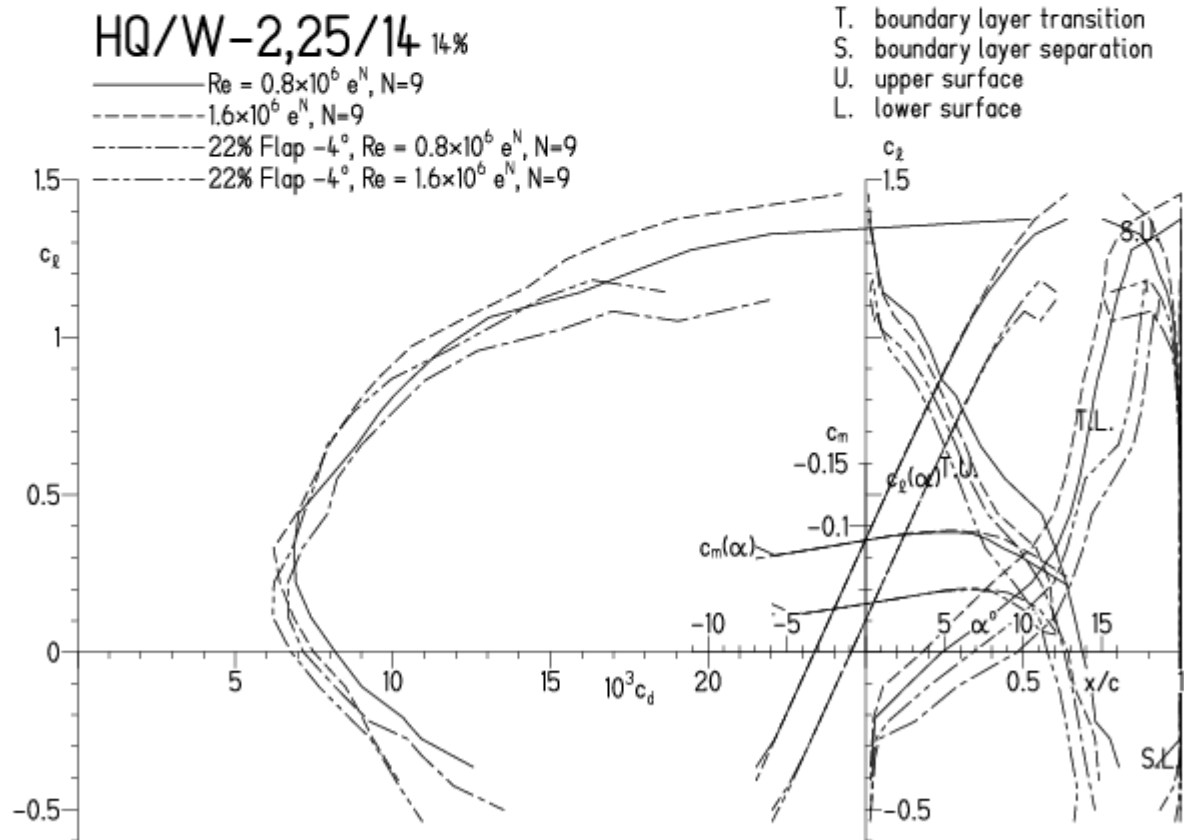


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07

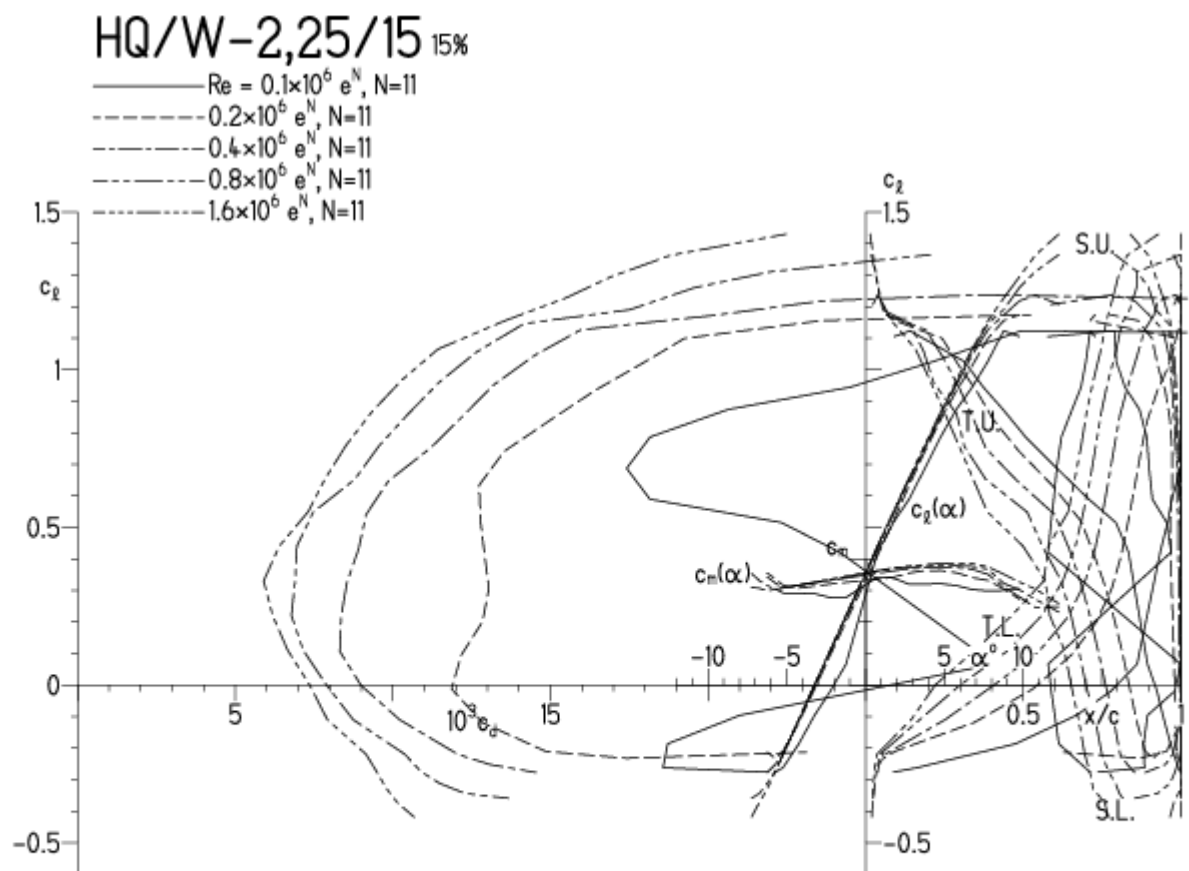


HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

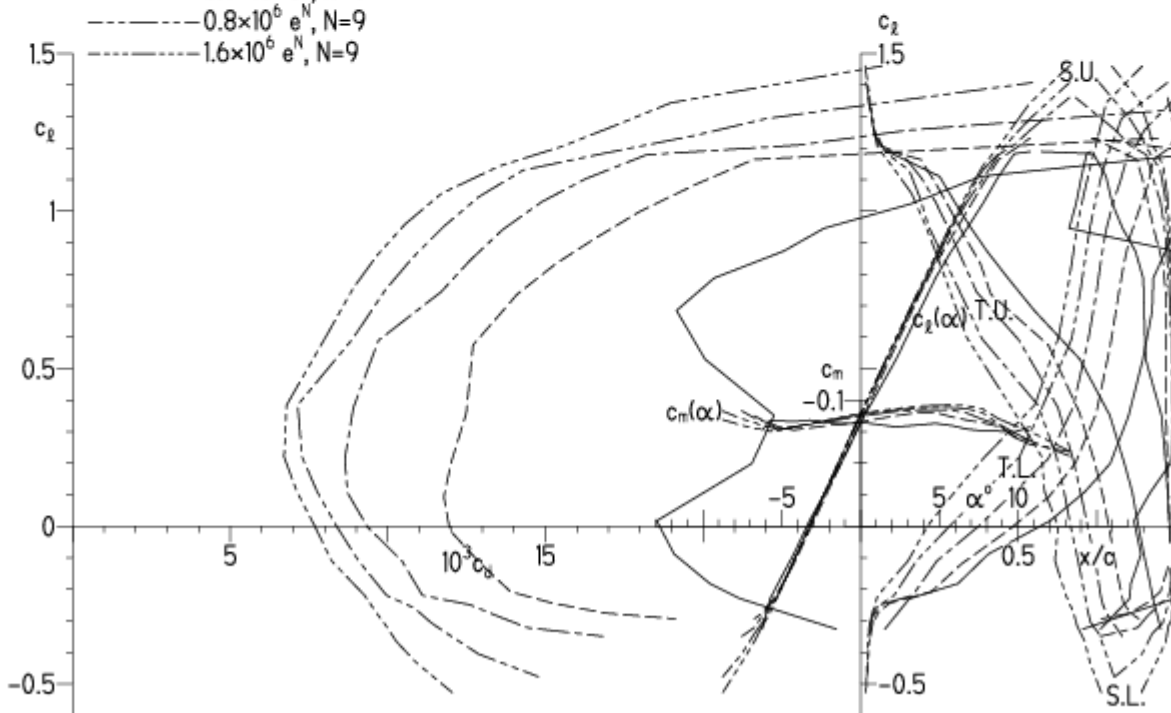
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

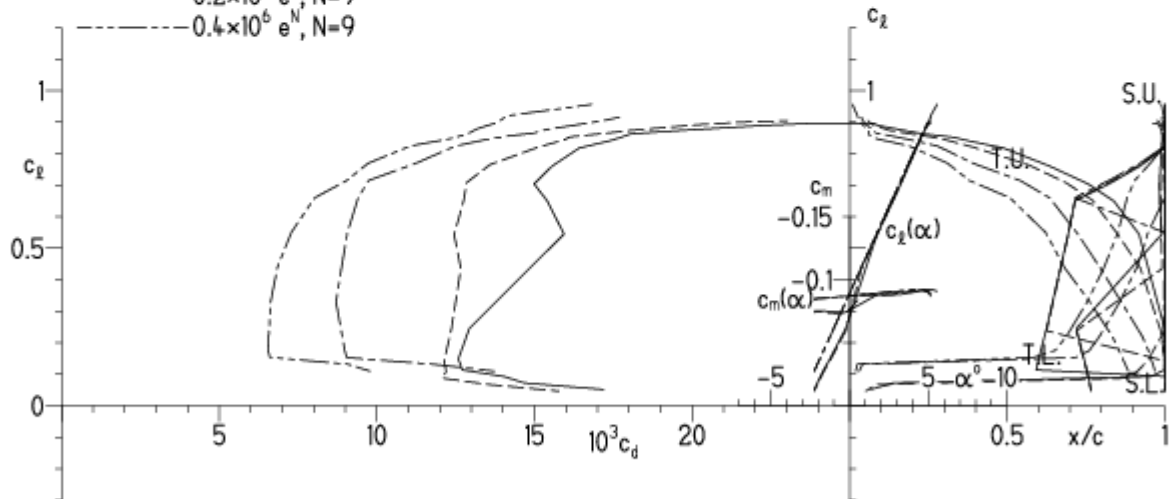
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

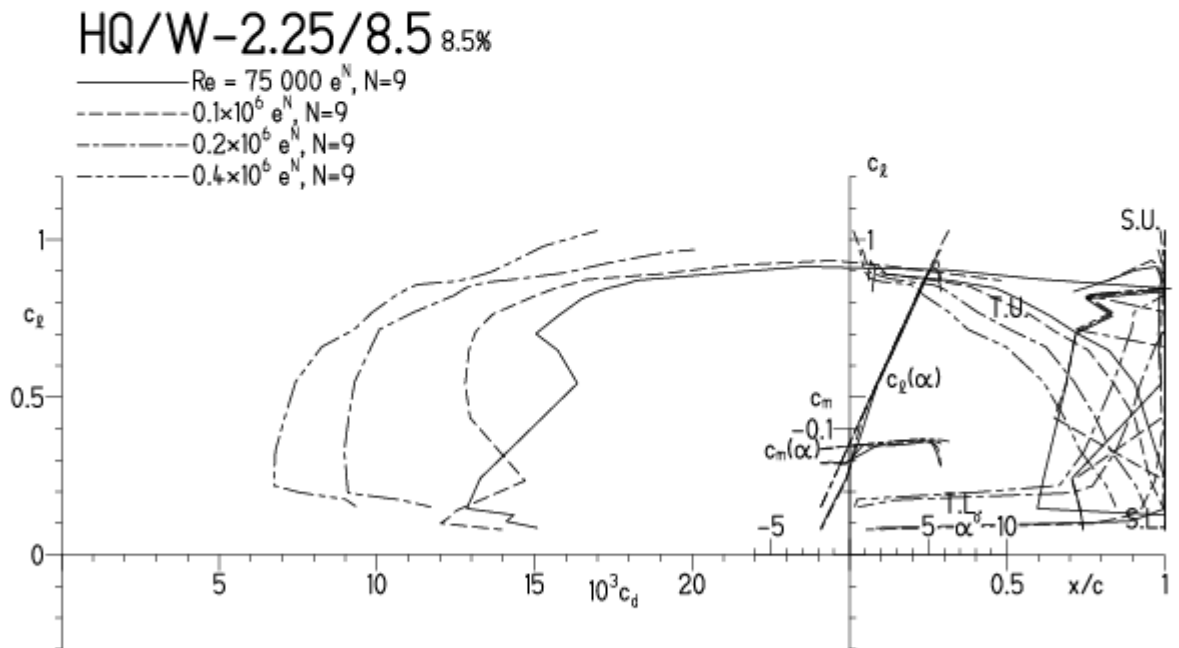


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

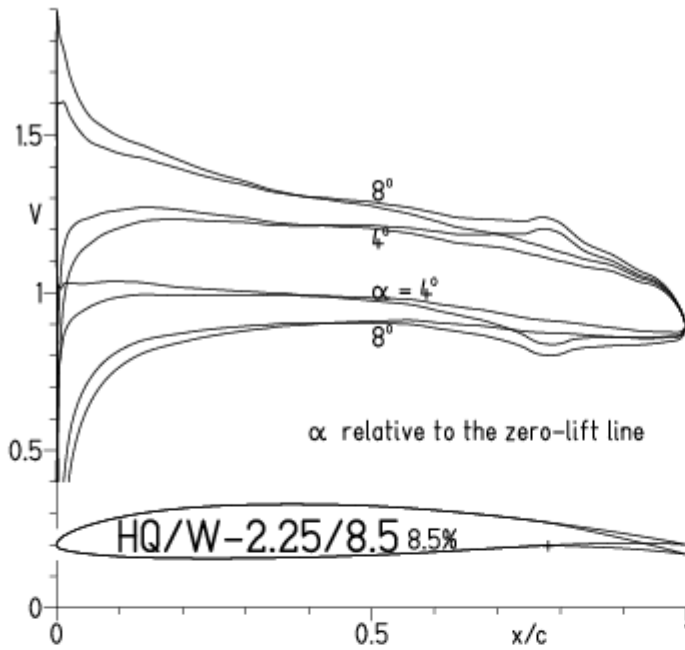
HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

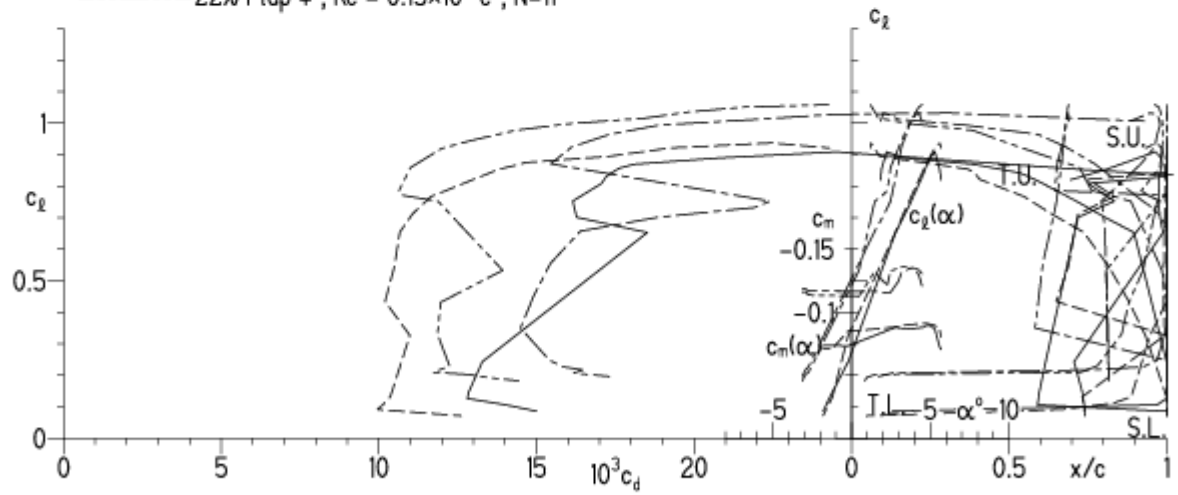


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

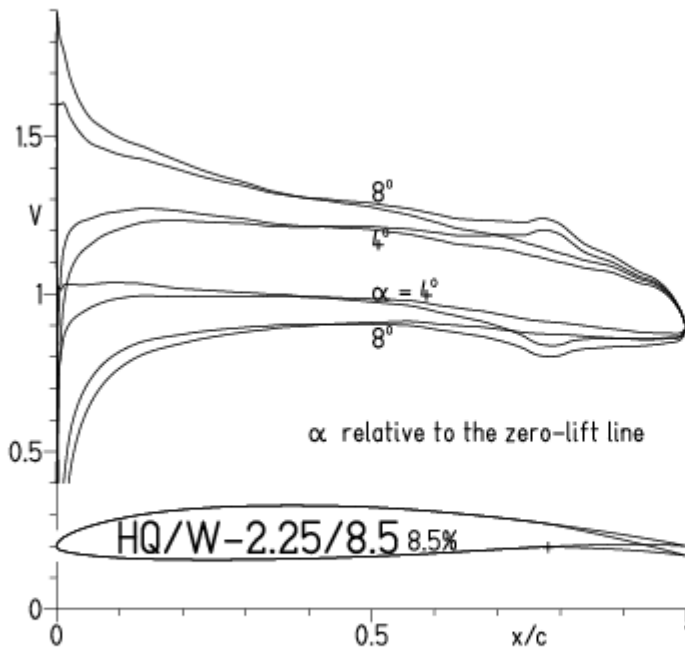
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

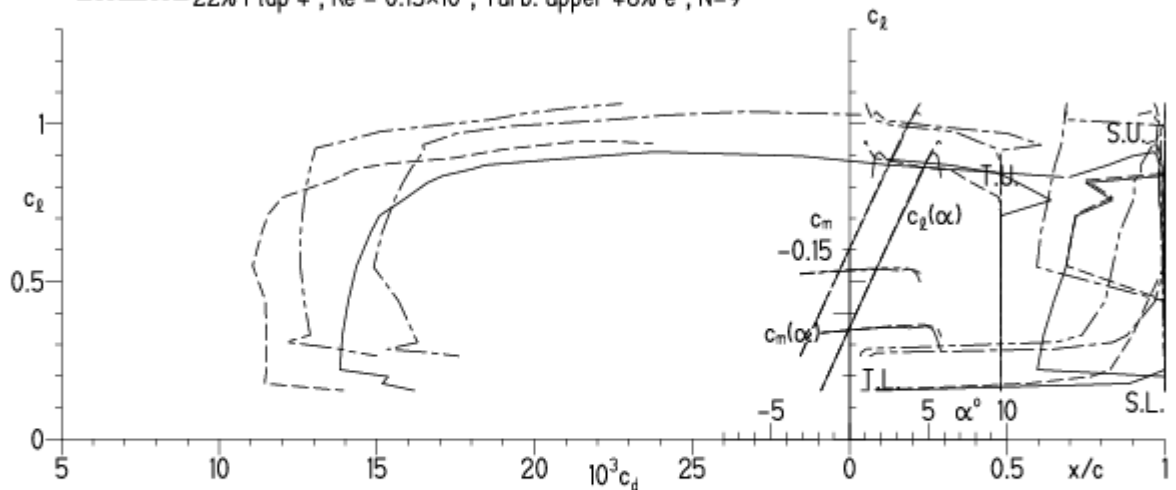


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

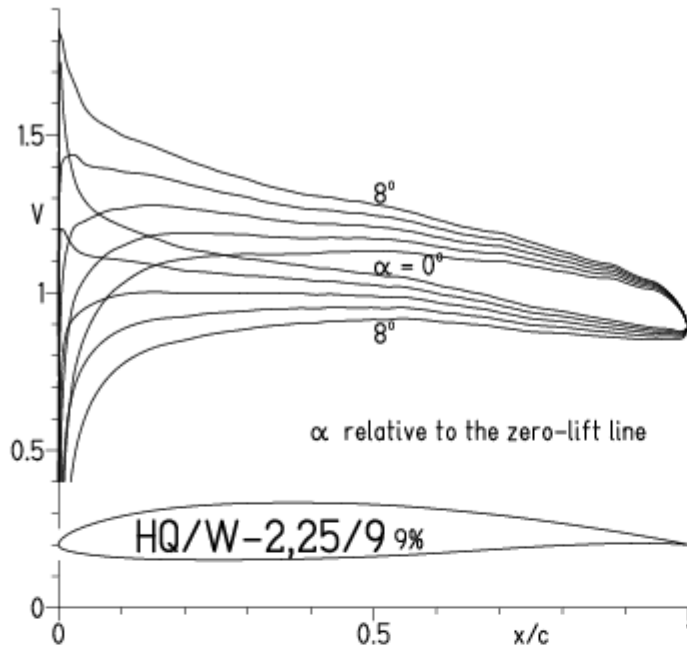


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

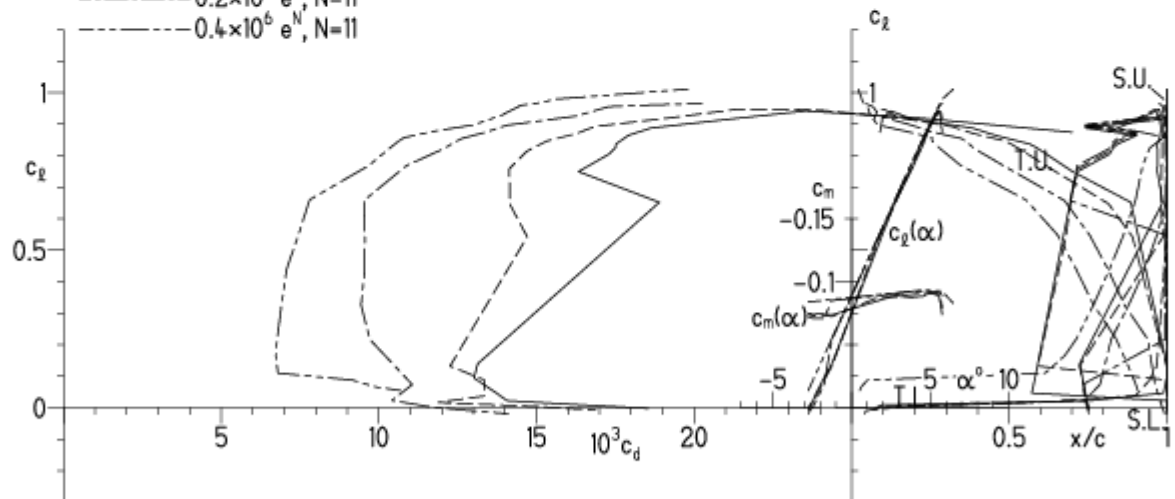
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

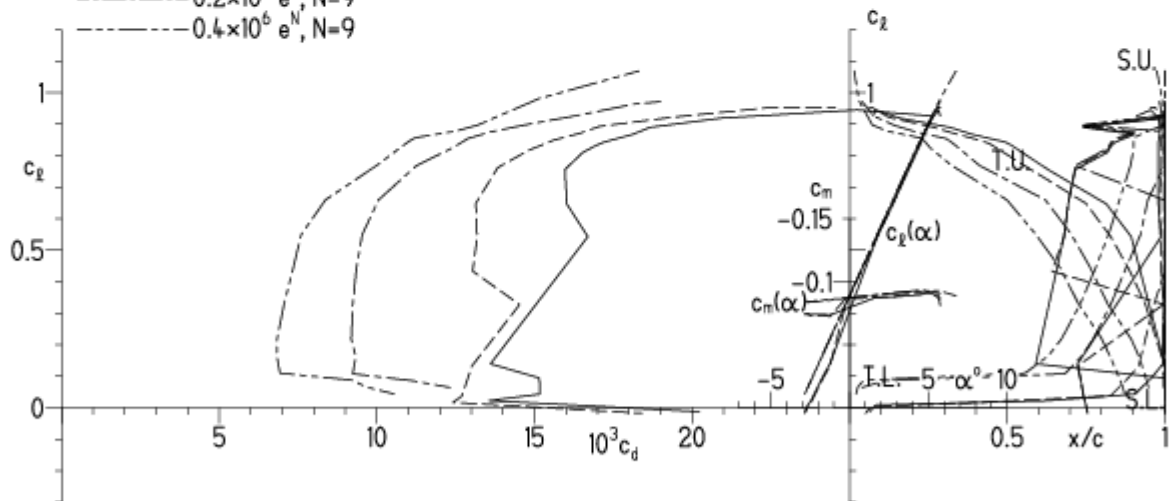
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

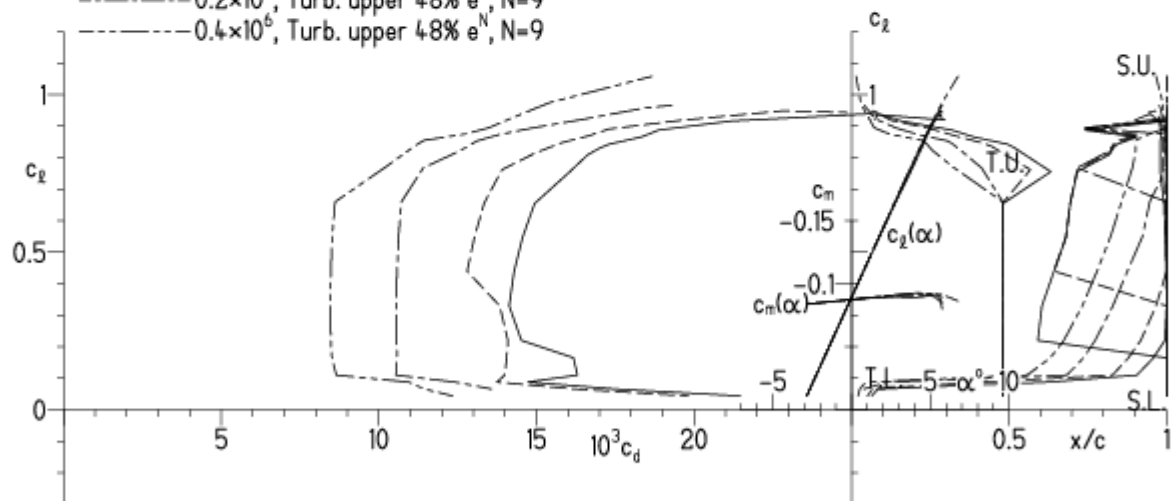
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

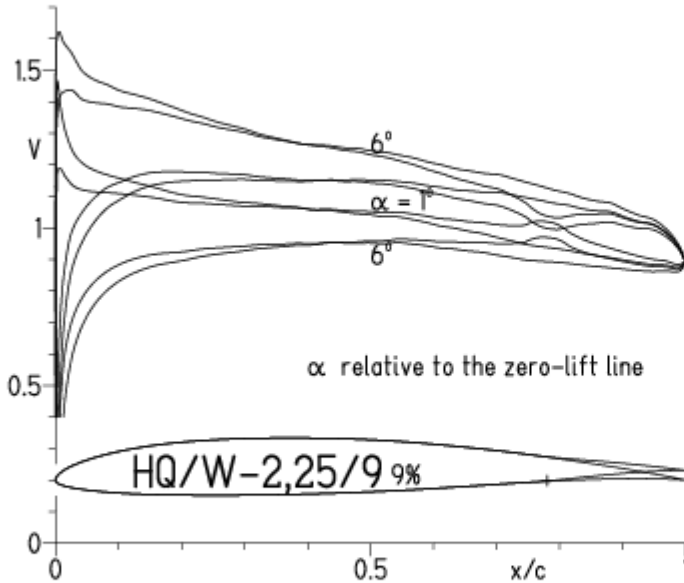
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$

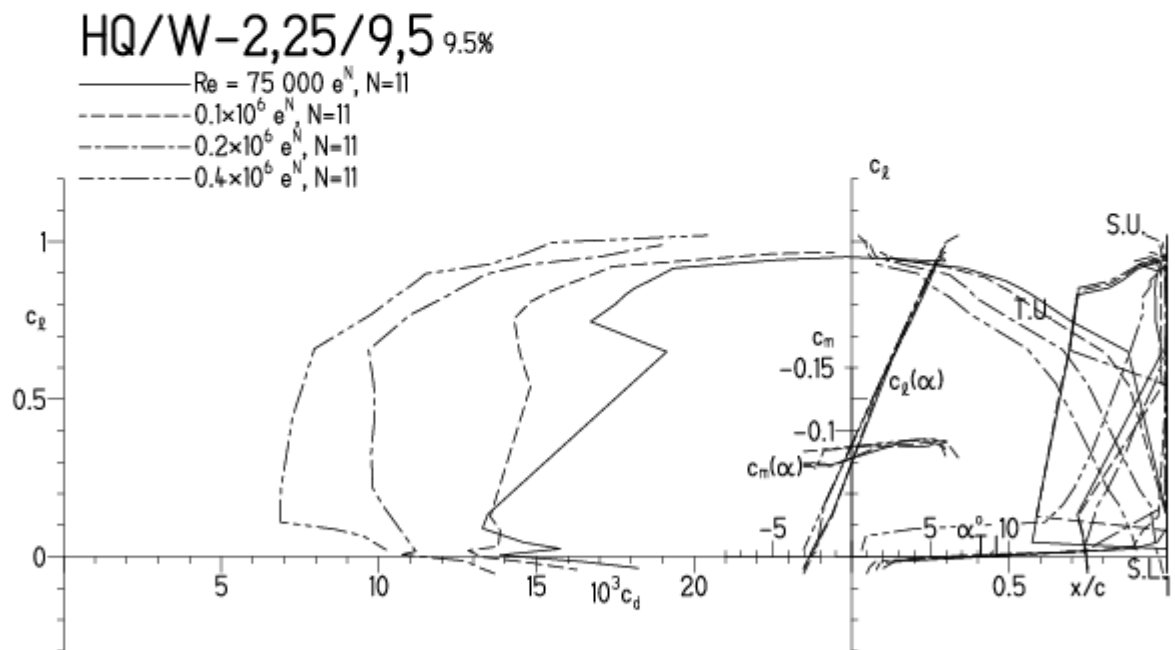


HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

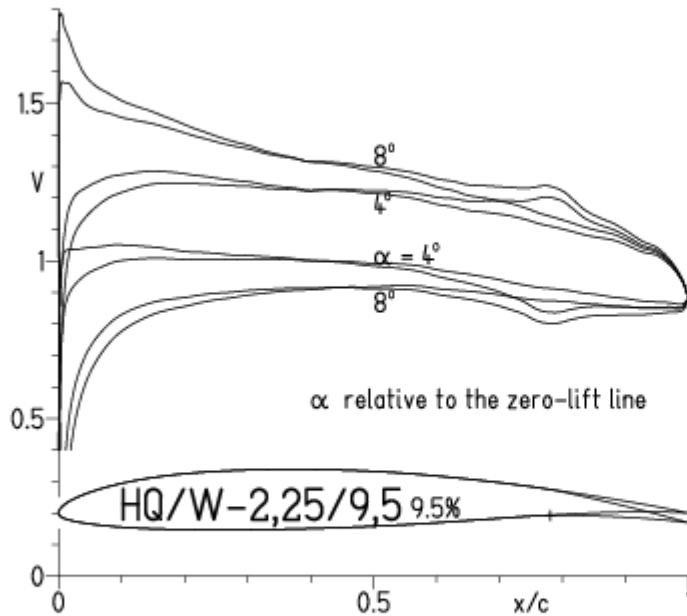
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

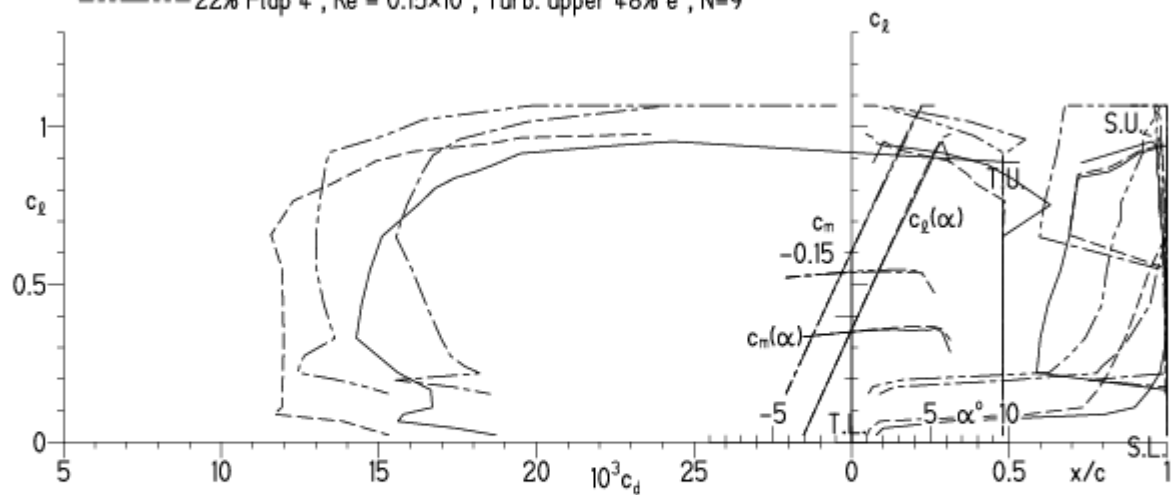


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

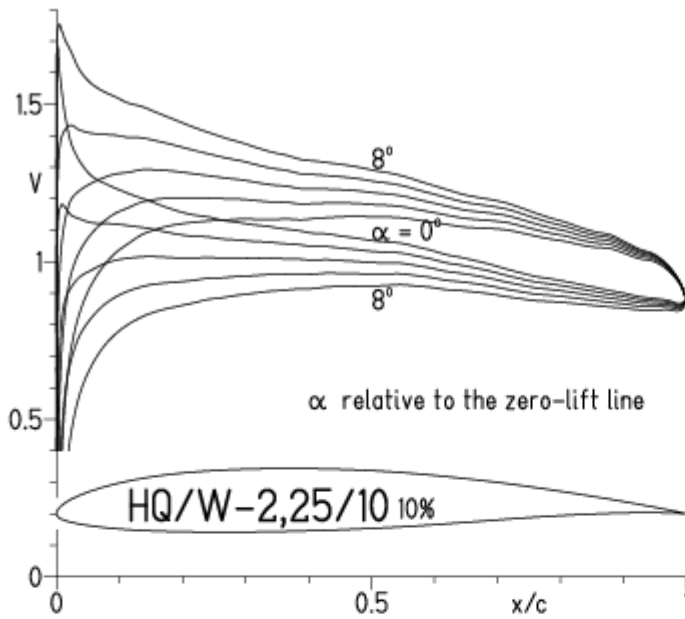


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

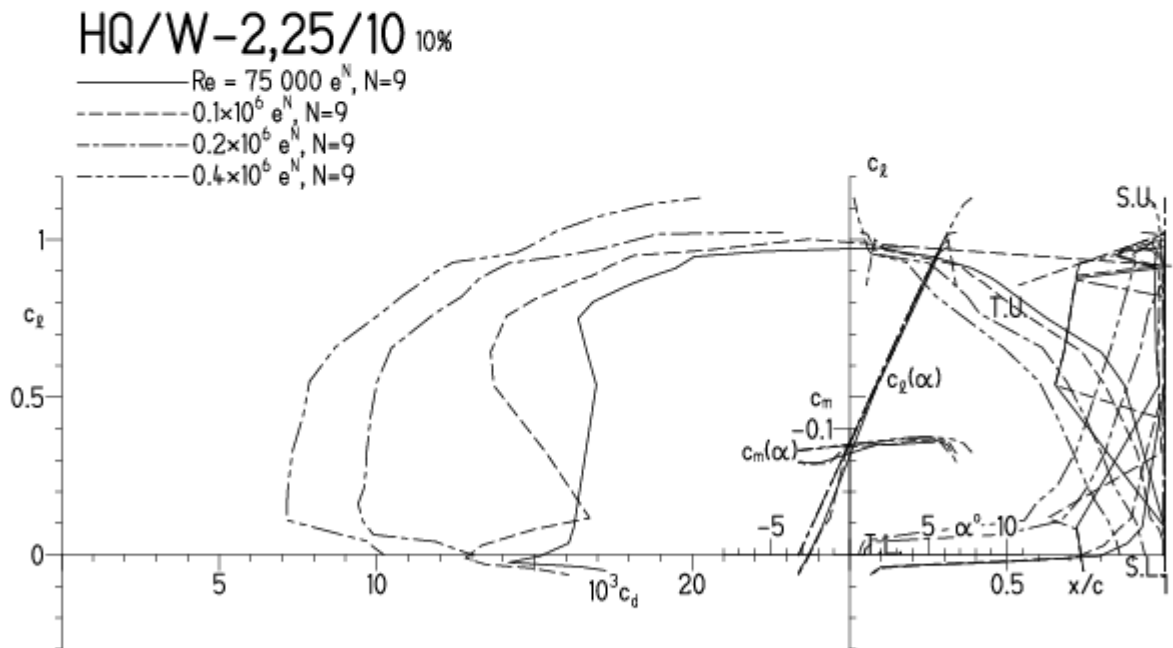


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

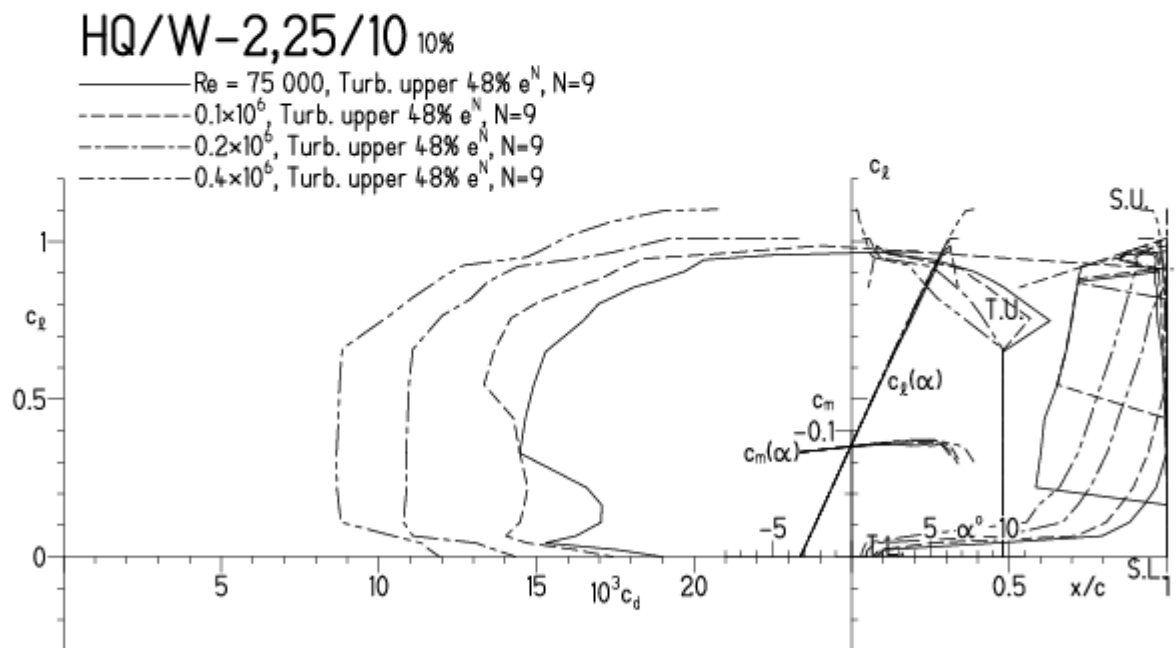


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

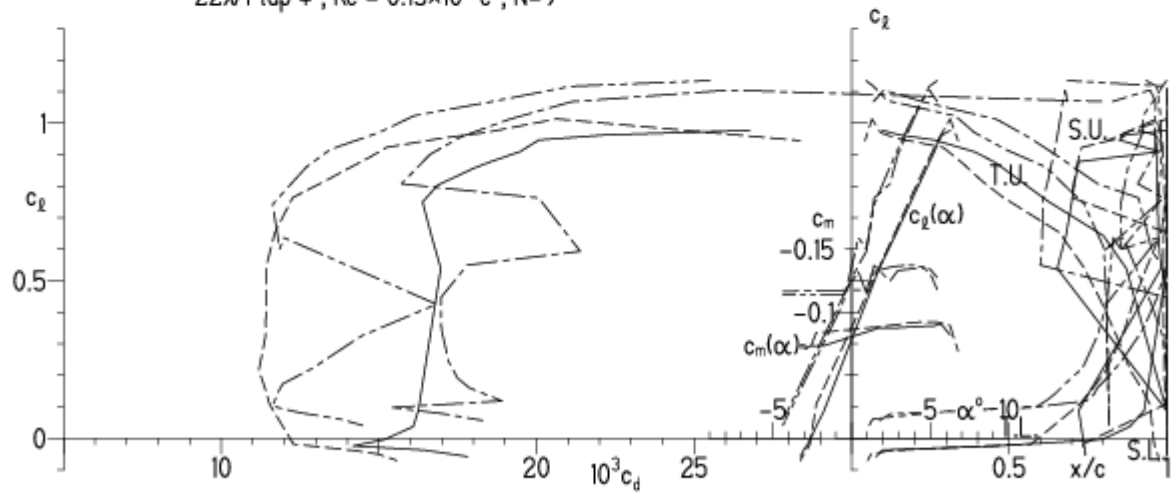


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

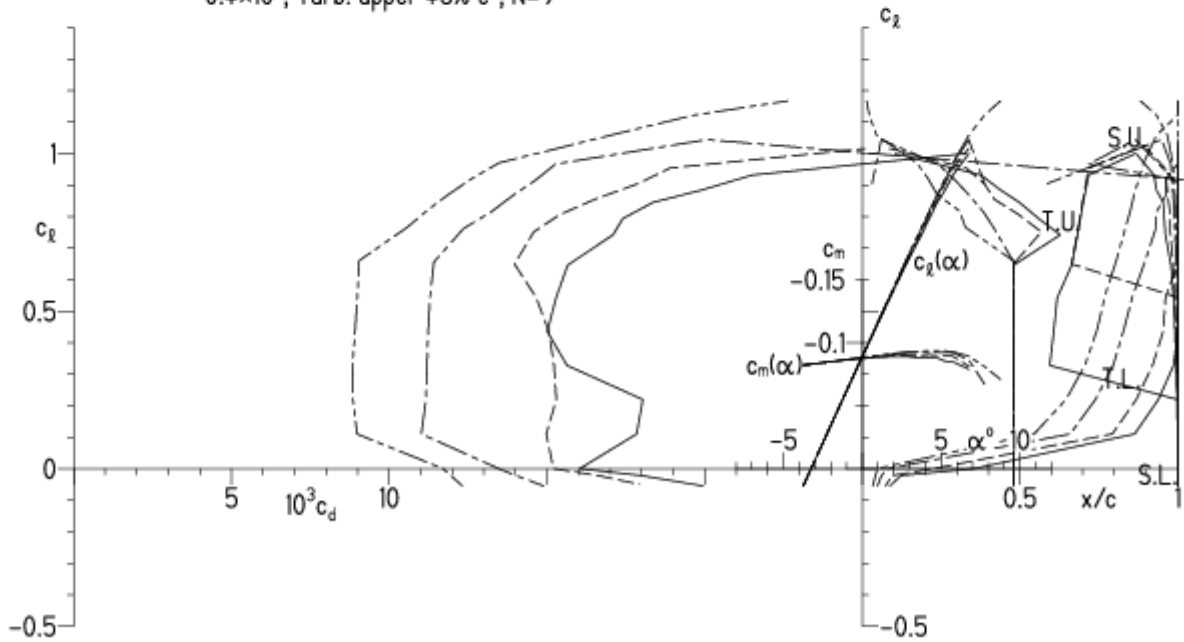
EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

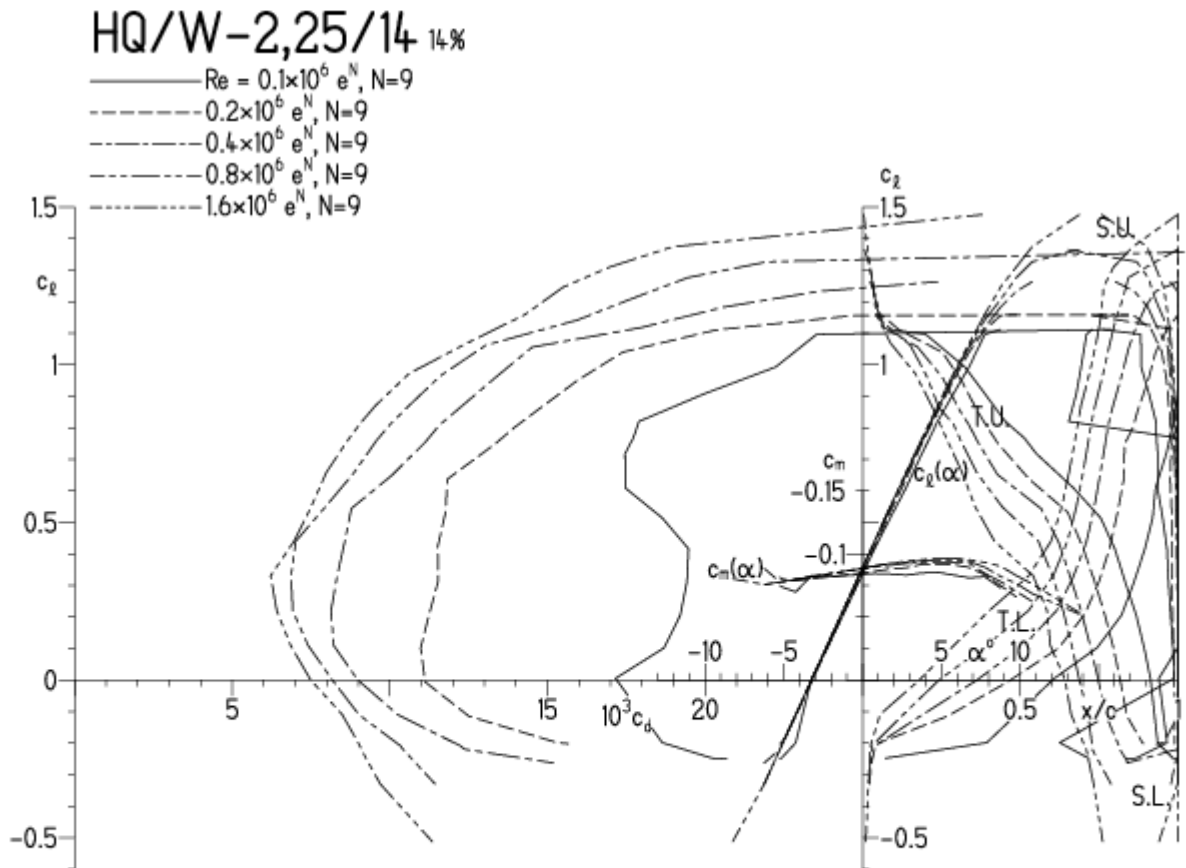


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

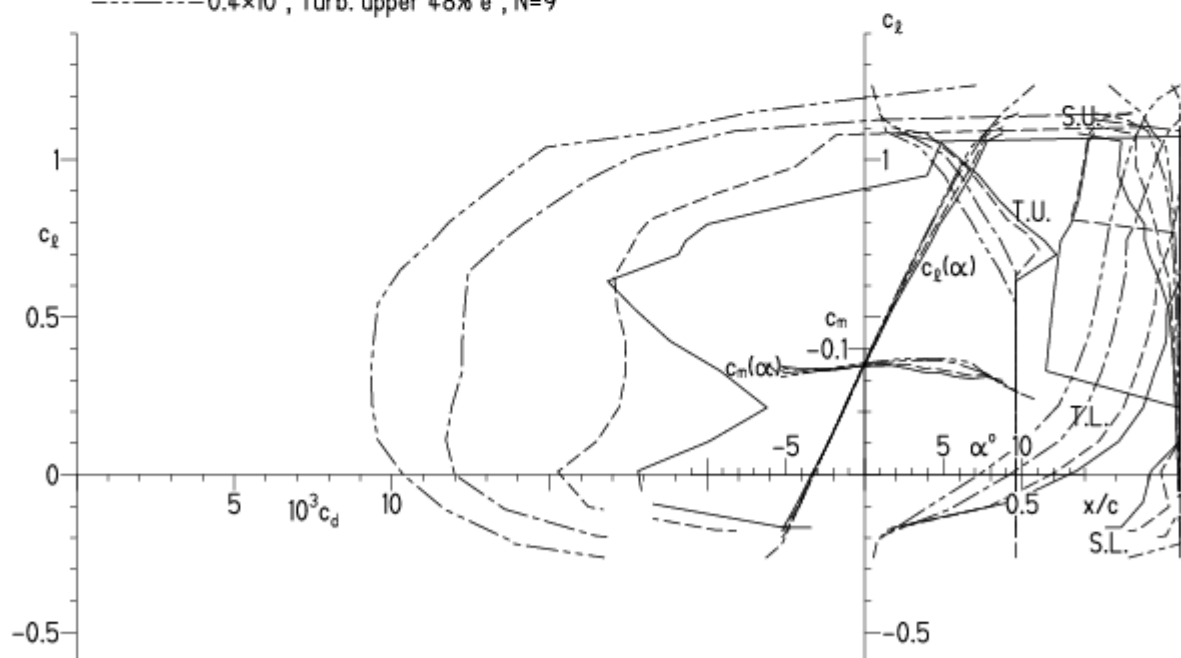
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

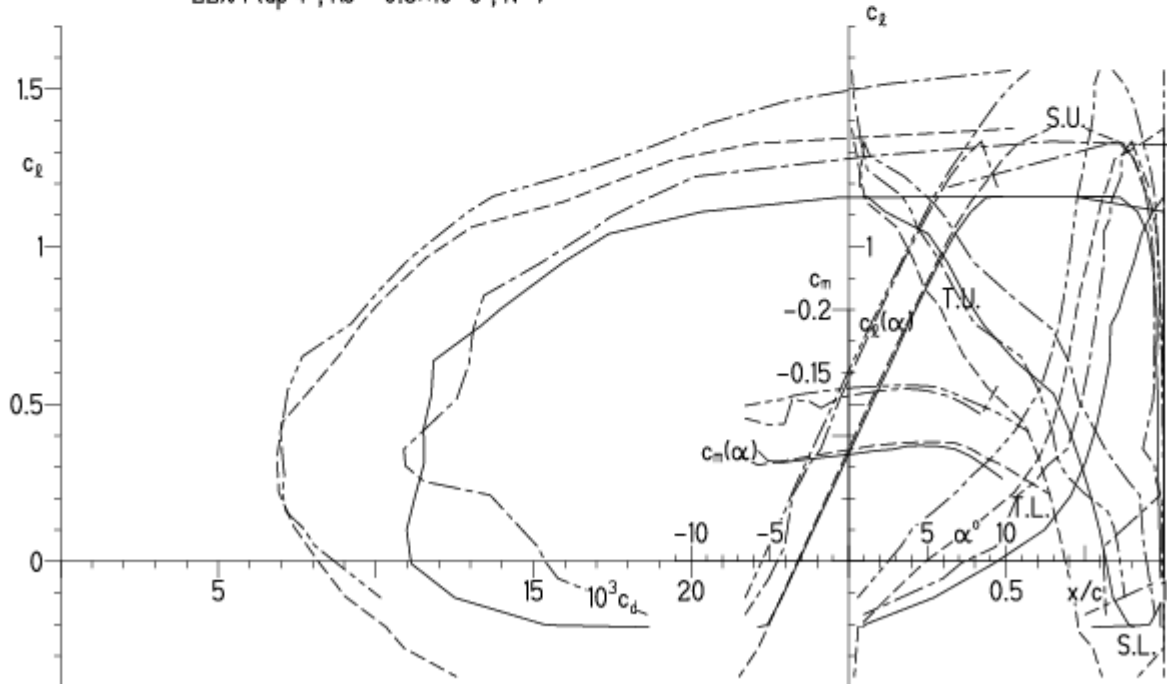


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

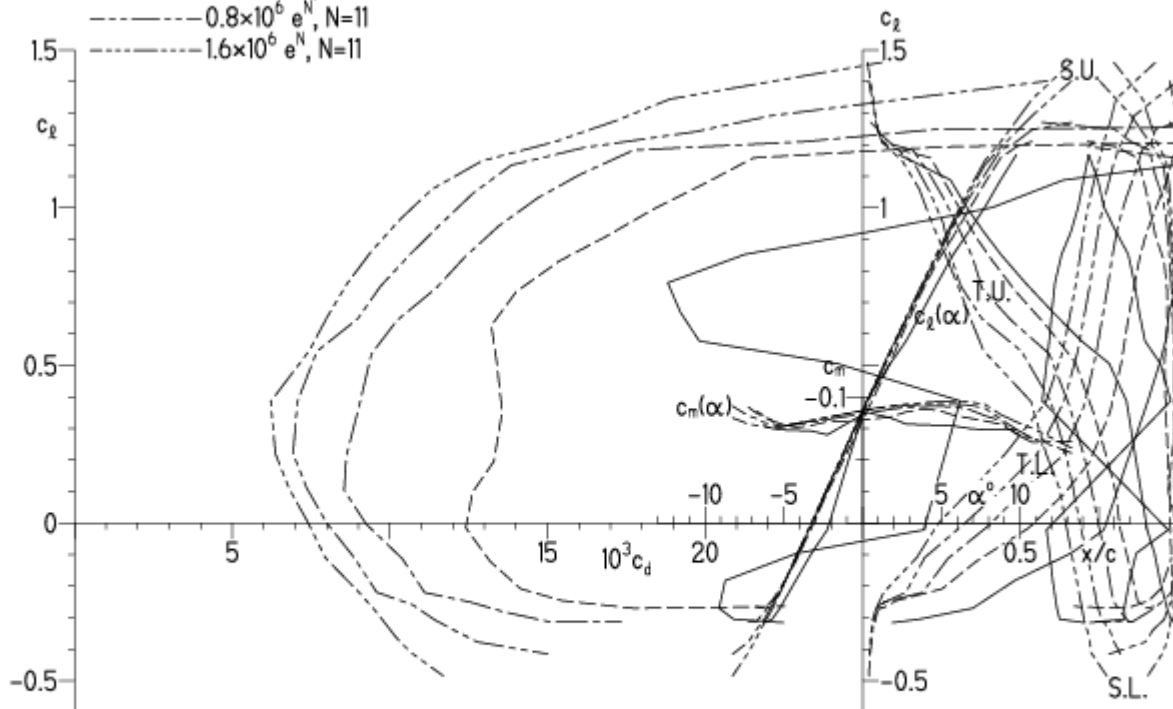
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/16, N=9

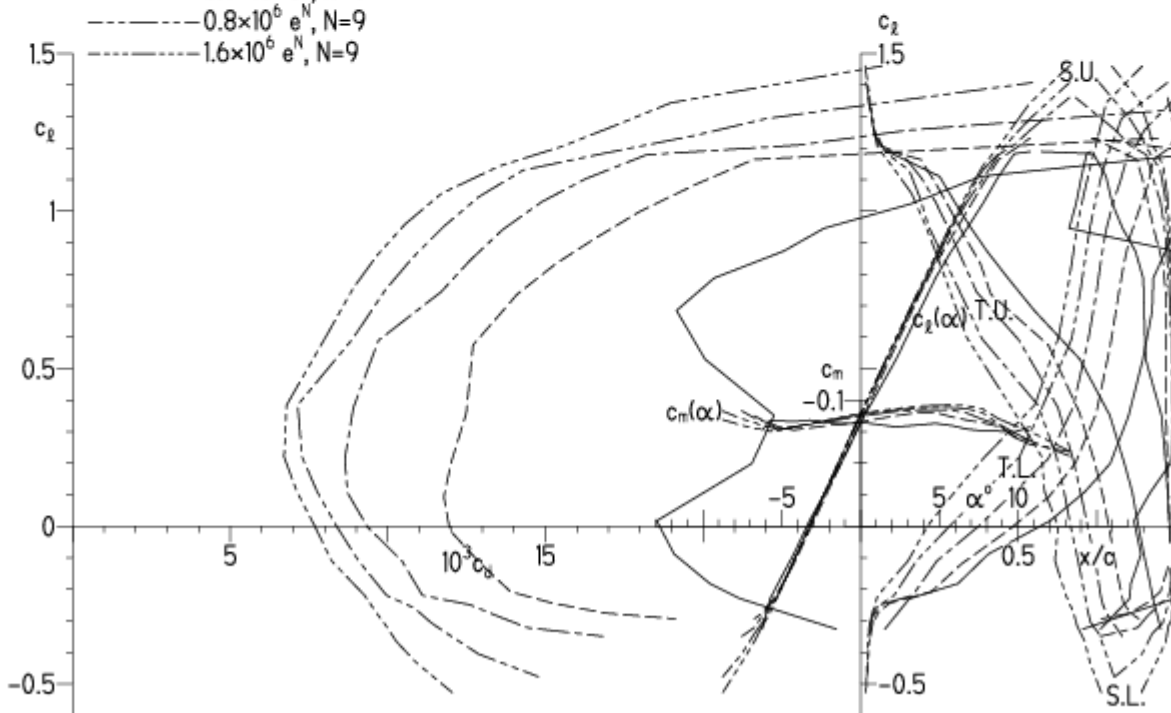
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - · 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2,25/8,5 8.5%

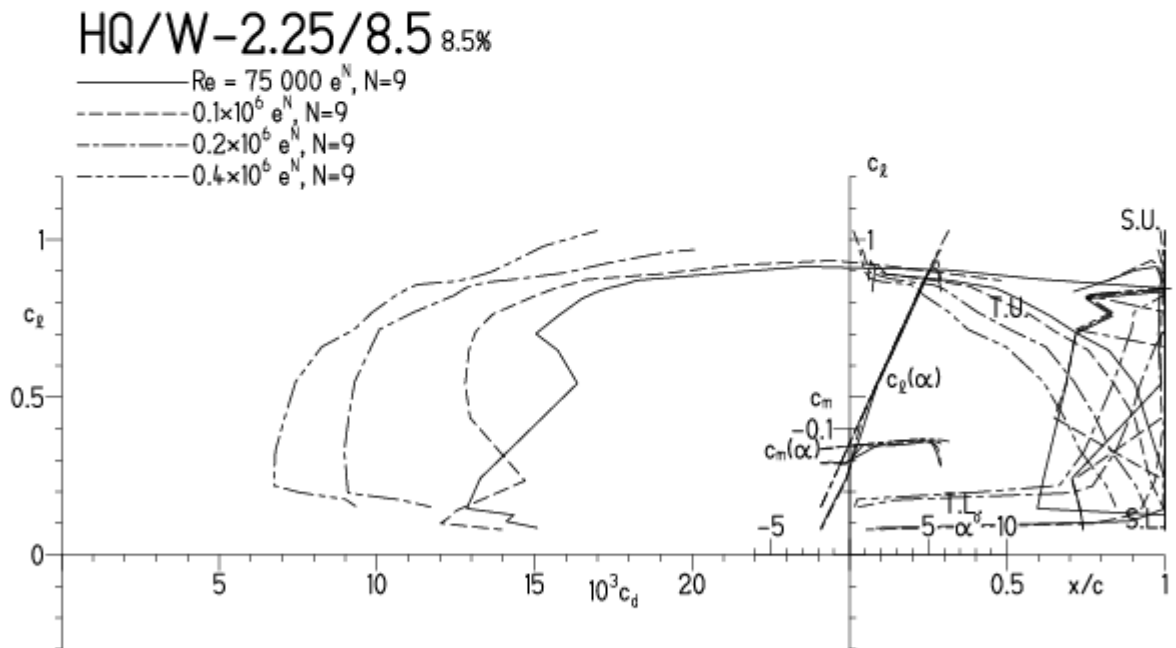


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

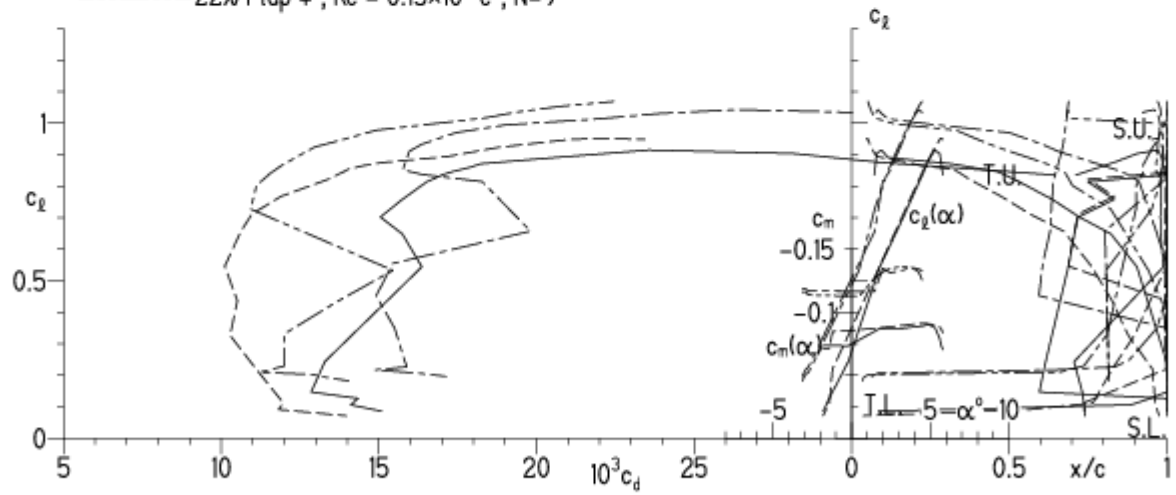


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

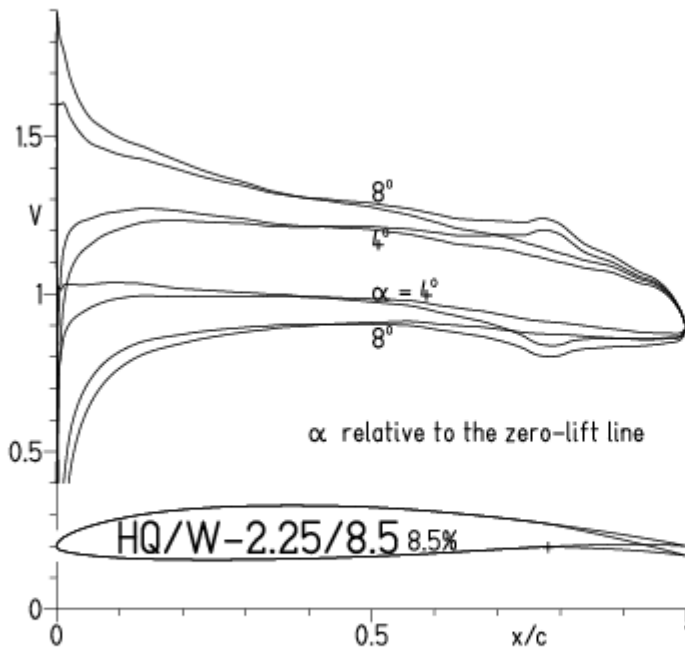
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

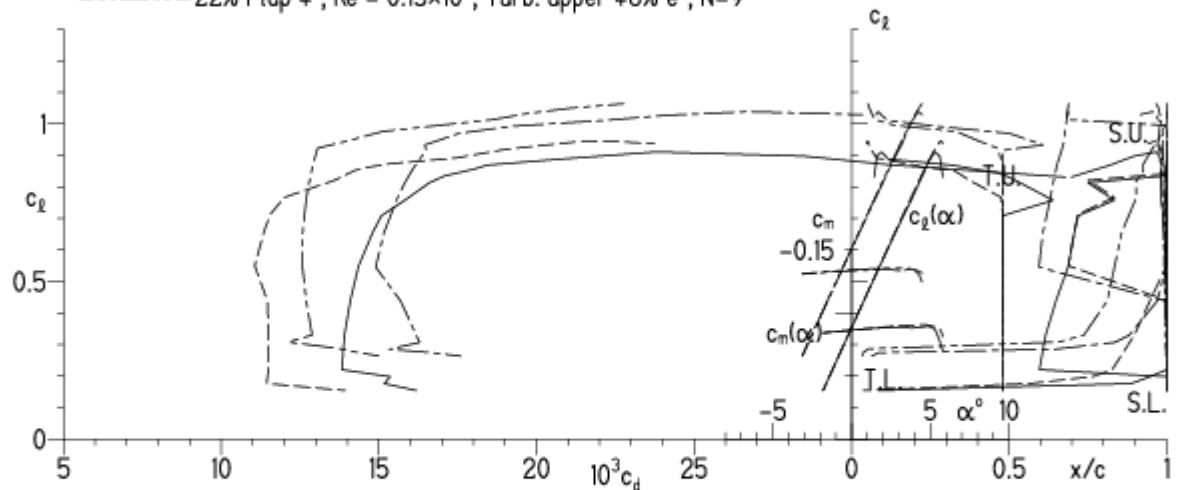


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

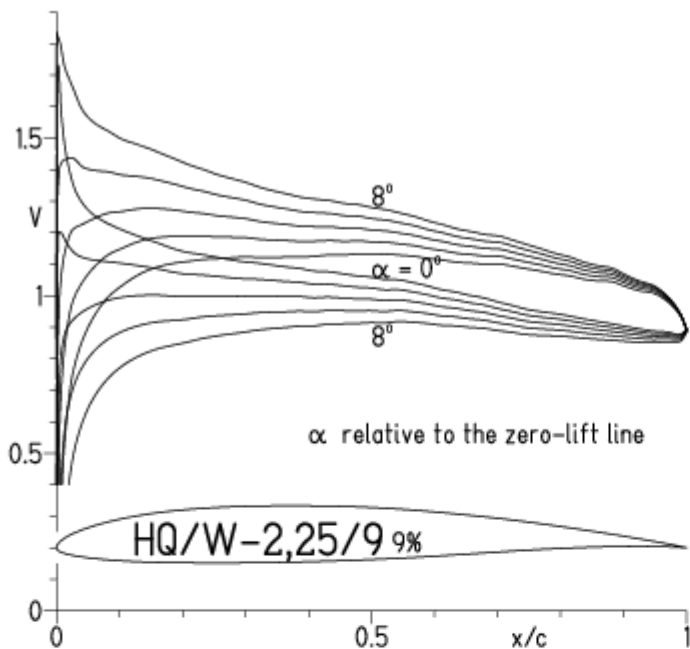


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

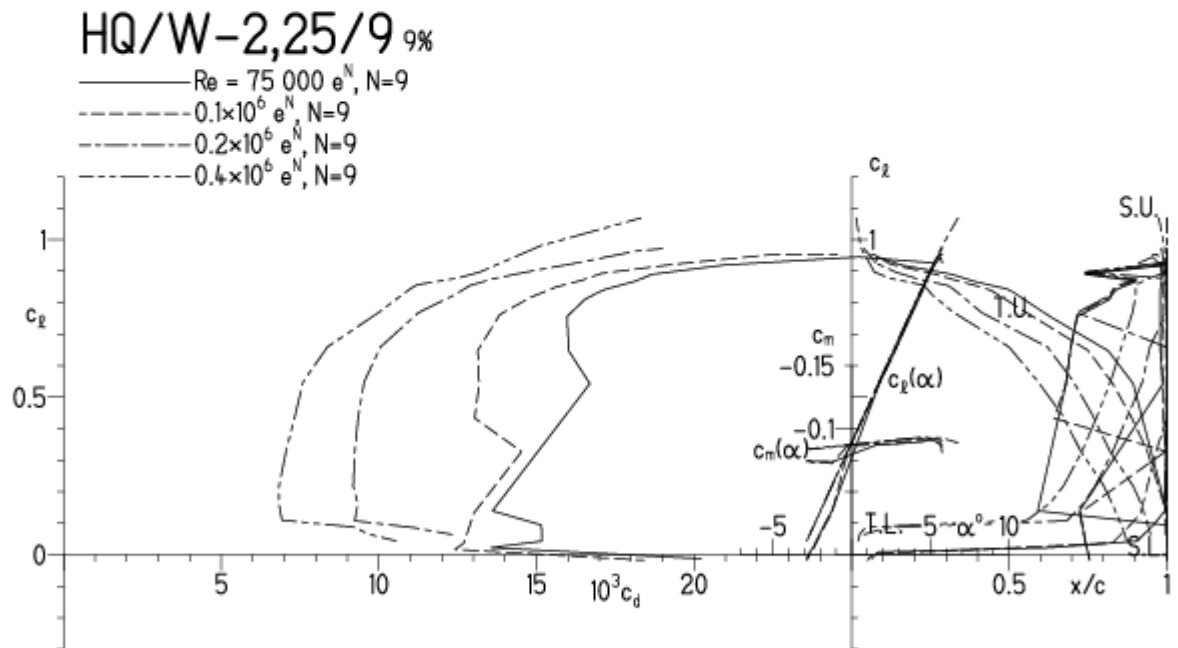


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17

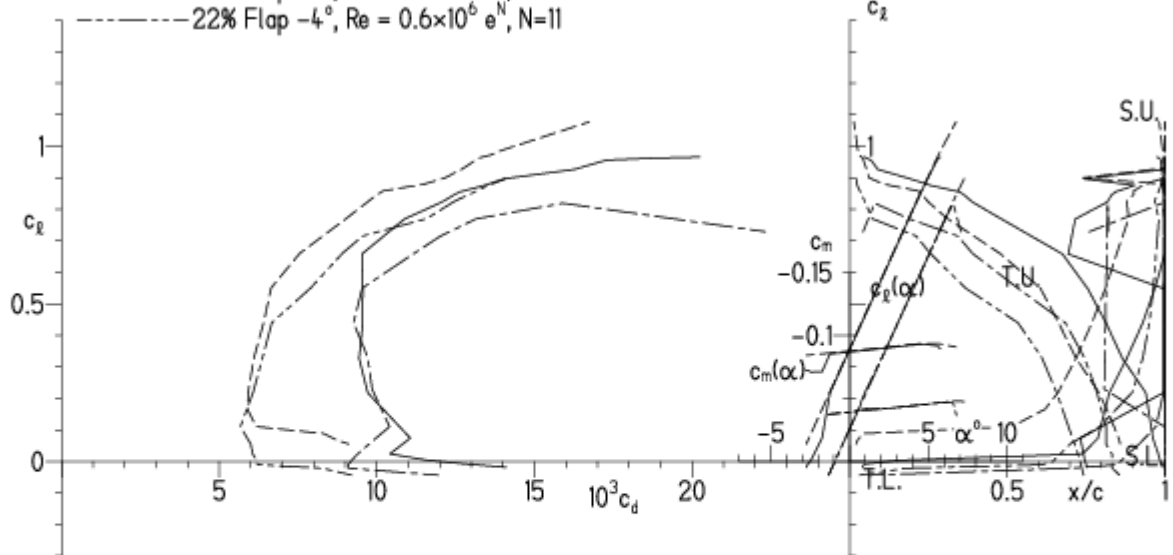


EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

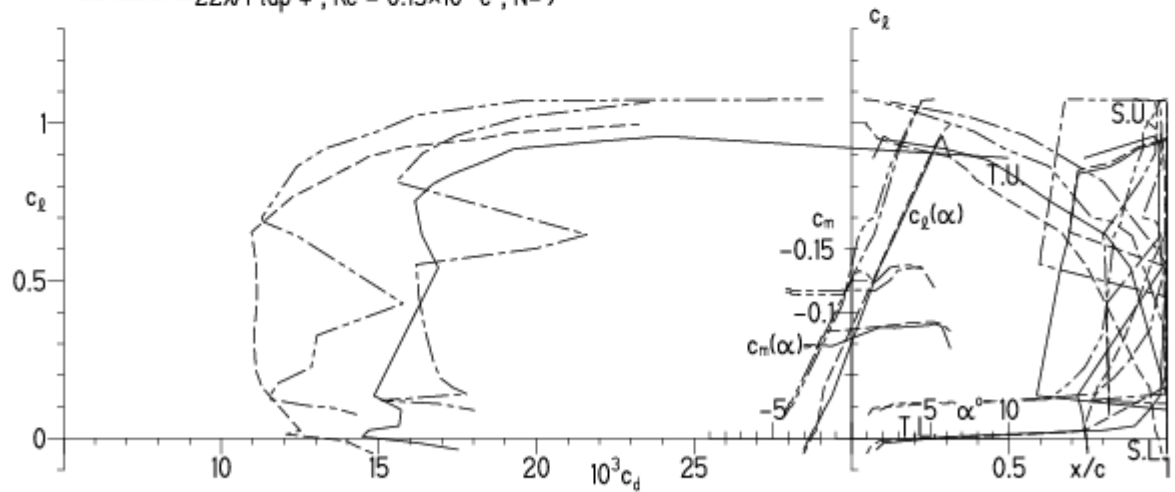


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

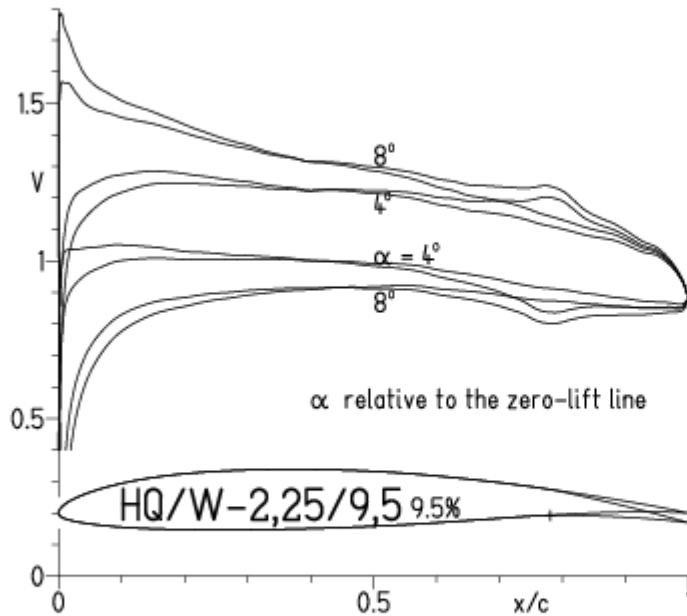
- Re = 75 000 e^N, N=9
- - - 0.15x10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

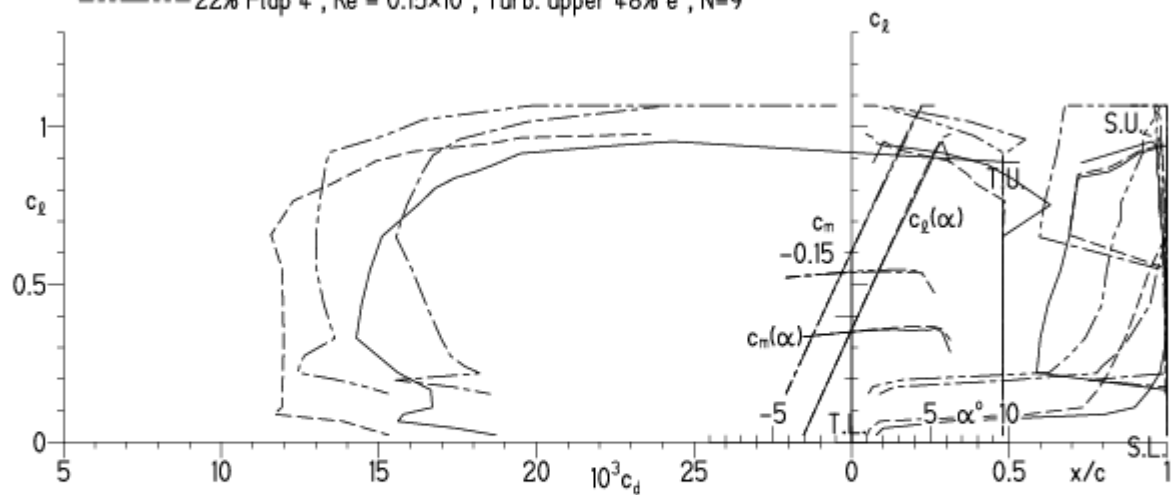


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



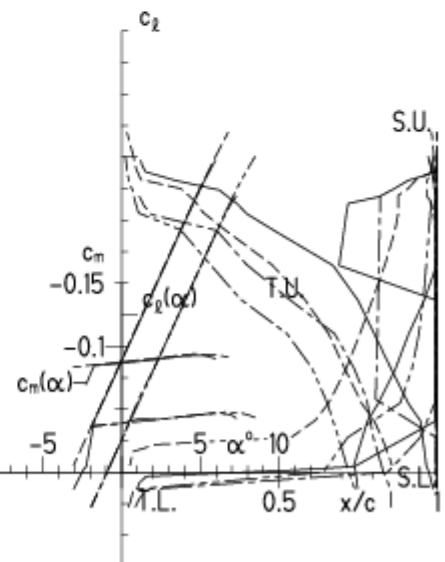
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

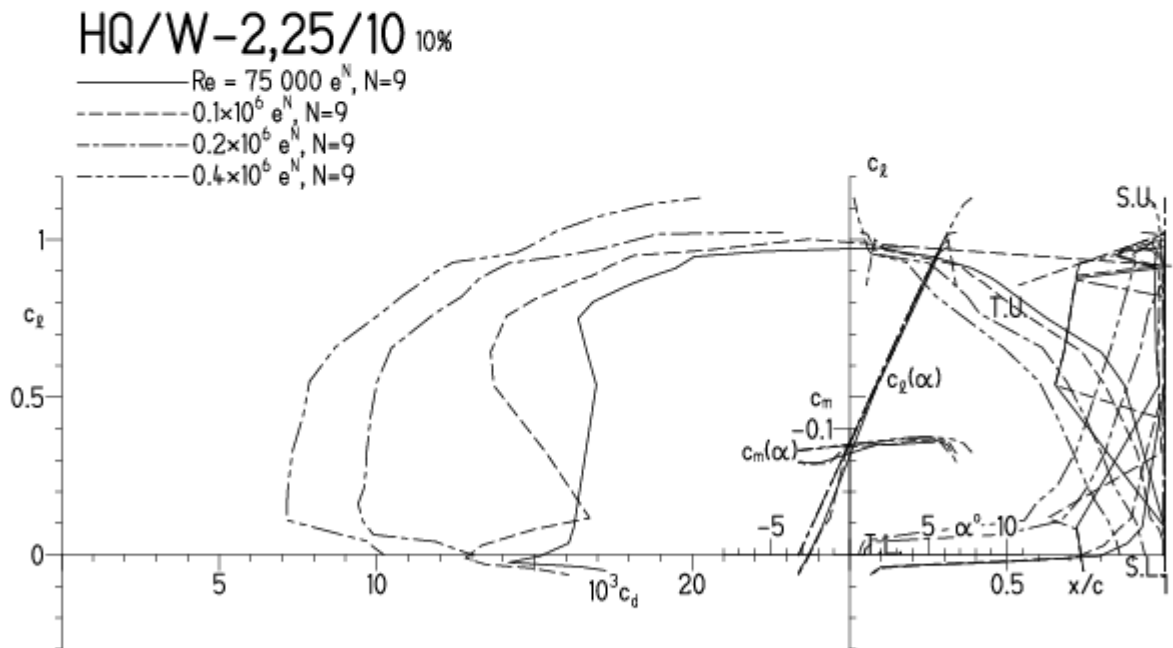


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

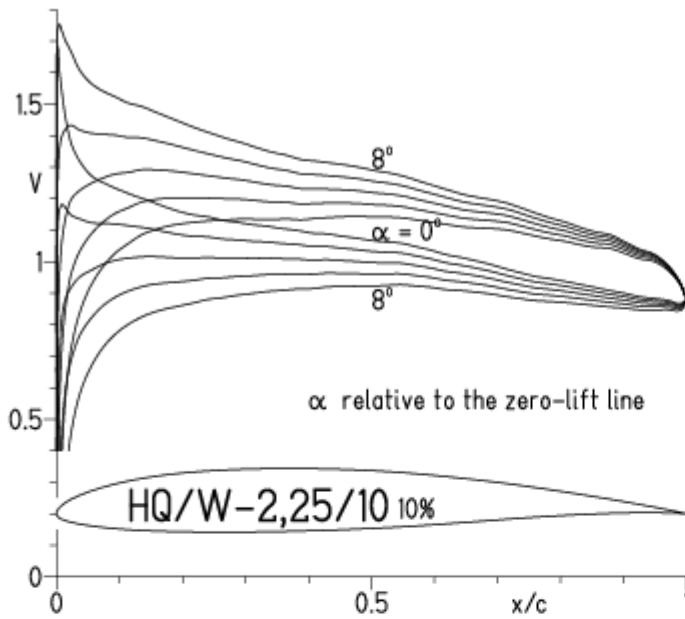


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

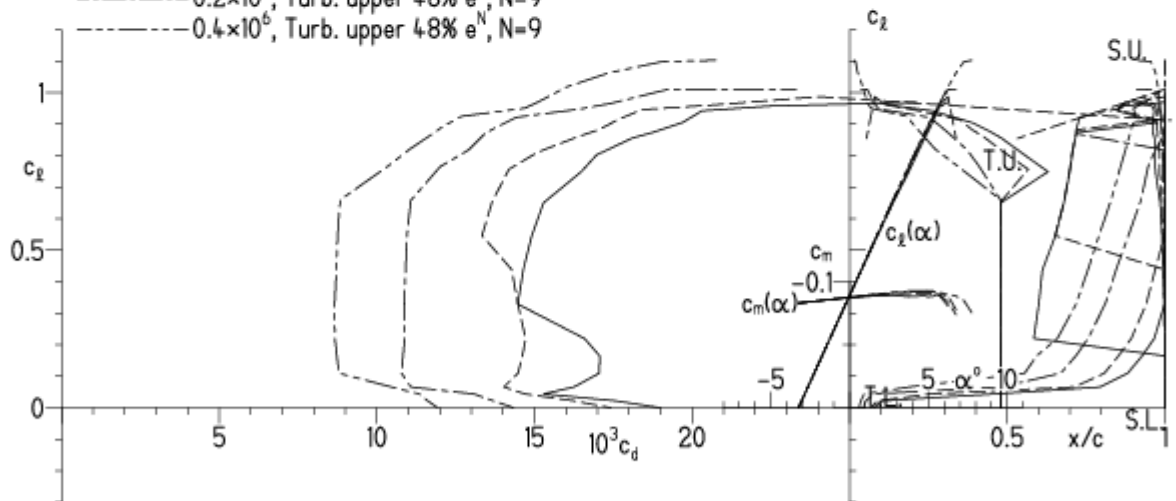
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

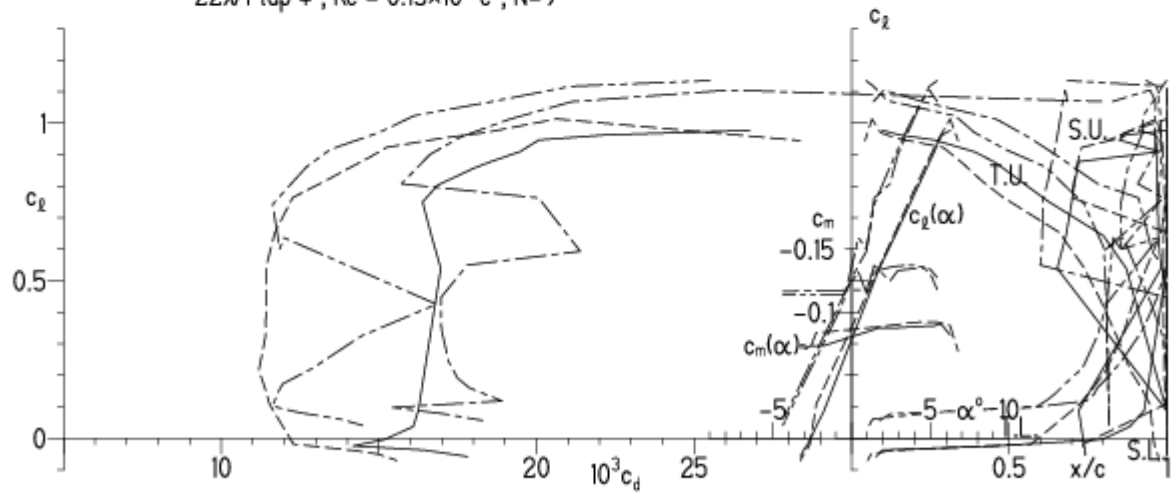


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

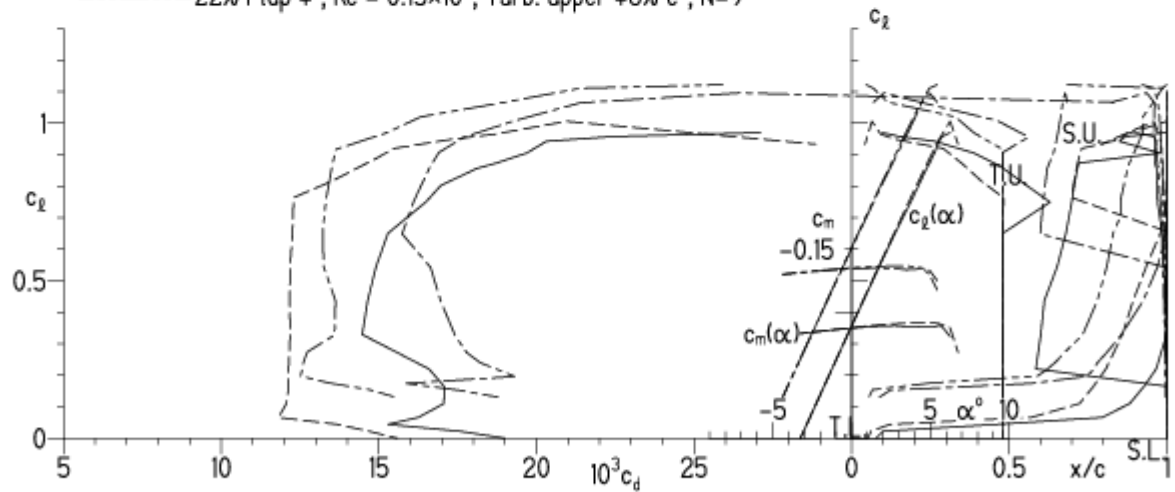


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

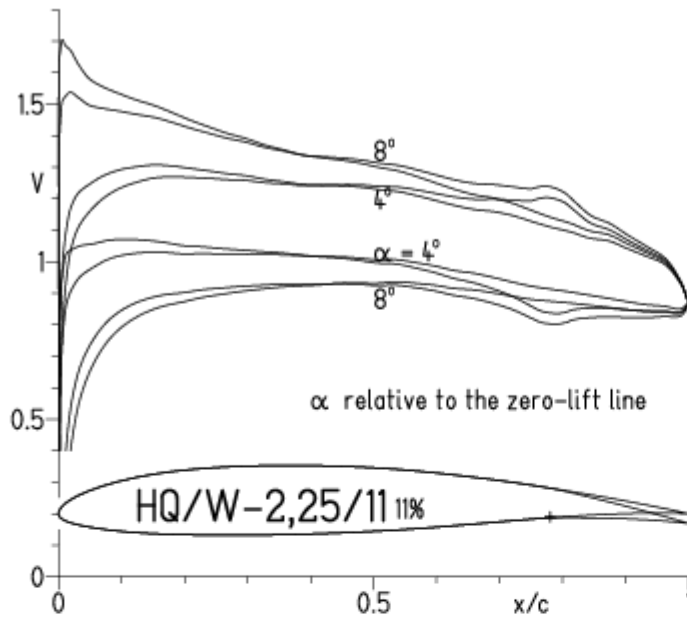
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

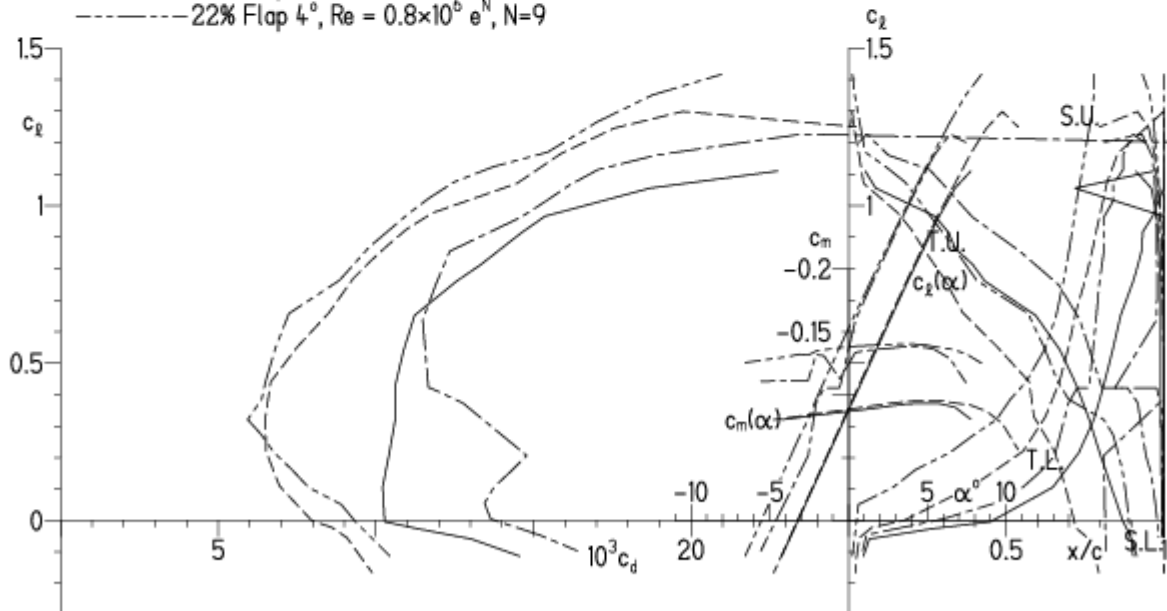


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11

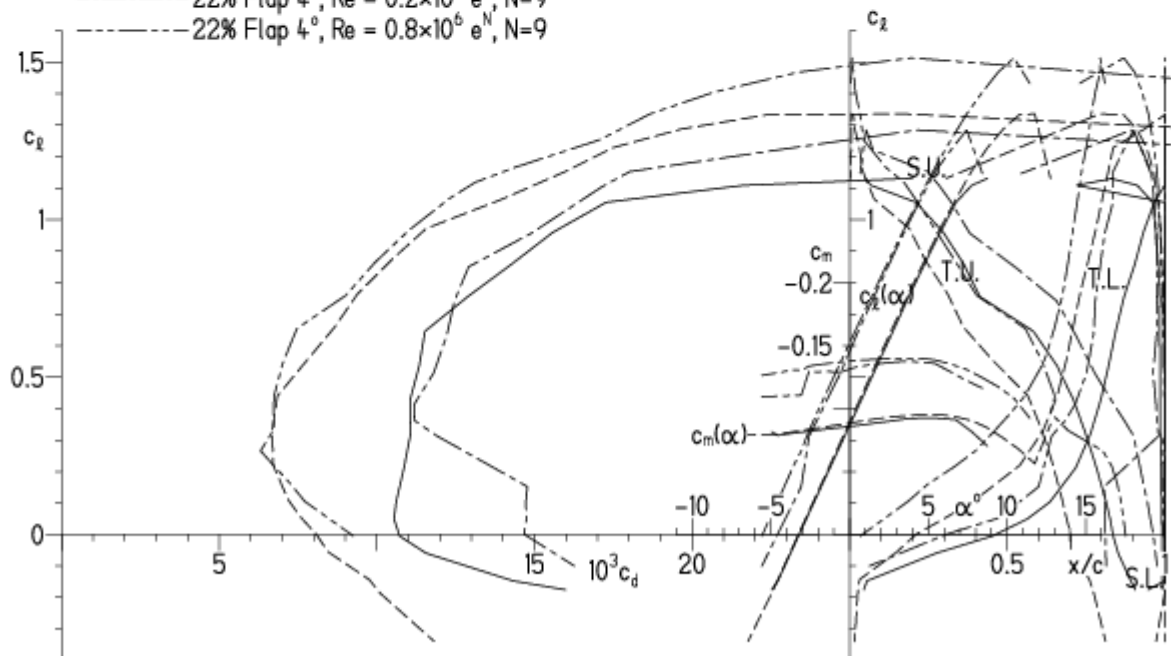


EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

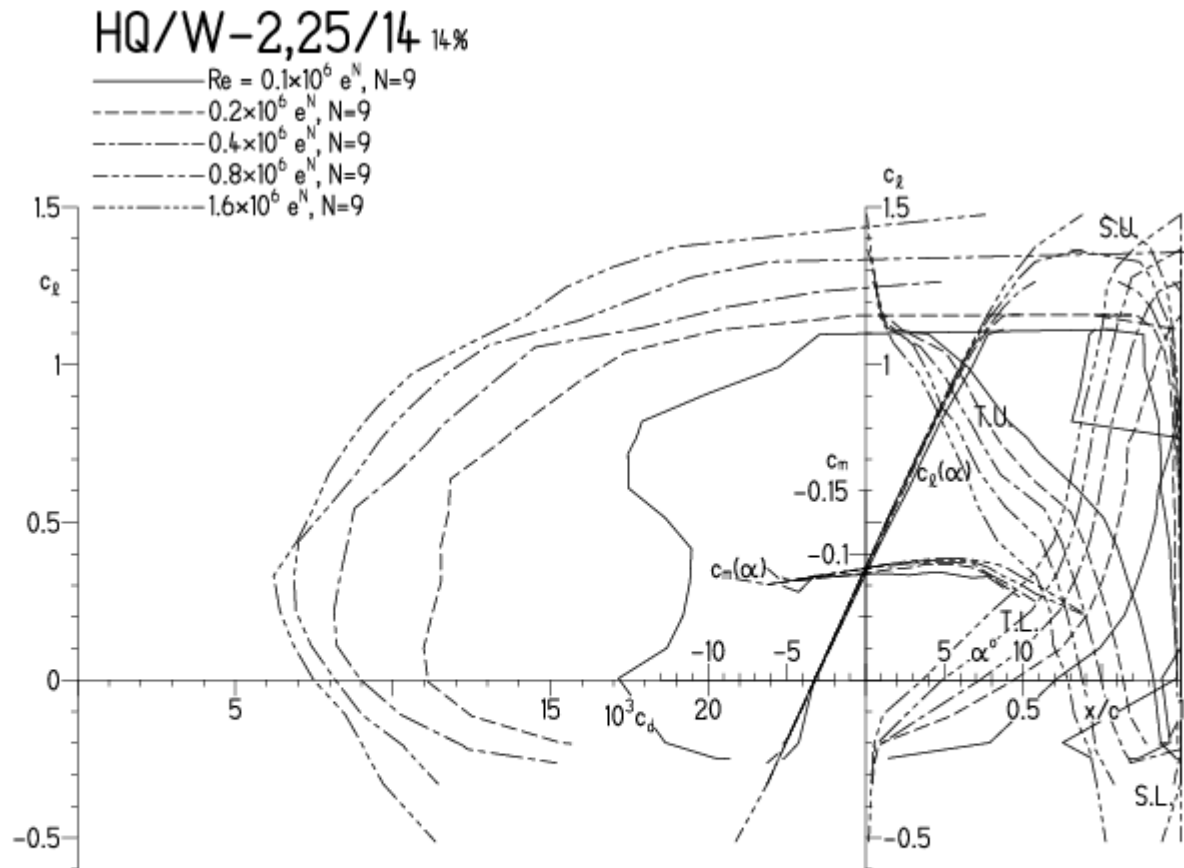


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

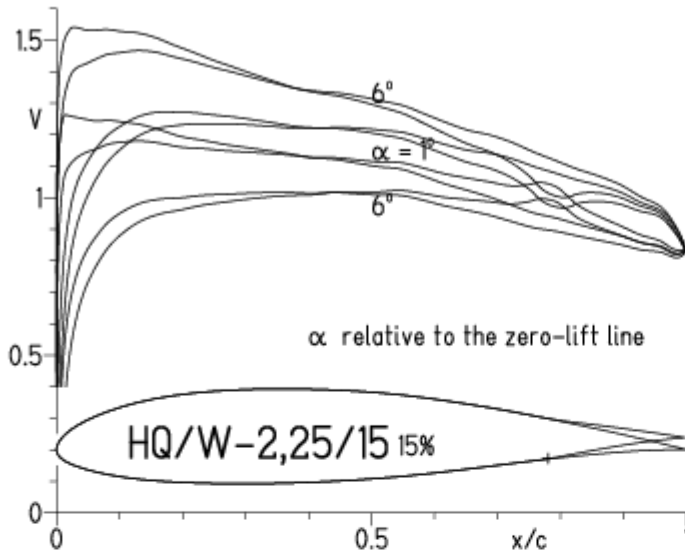


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

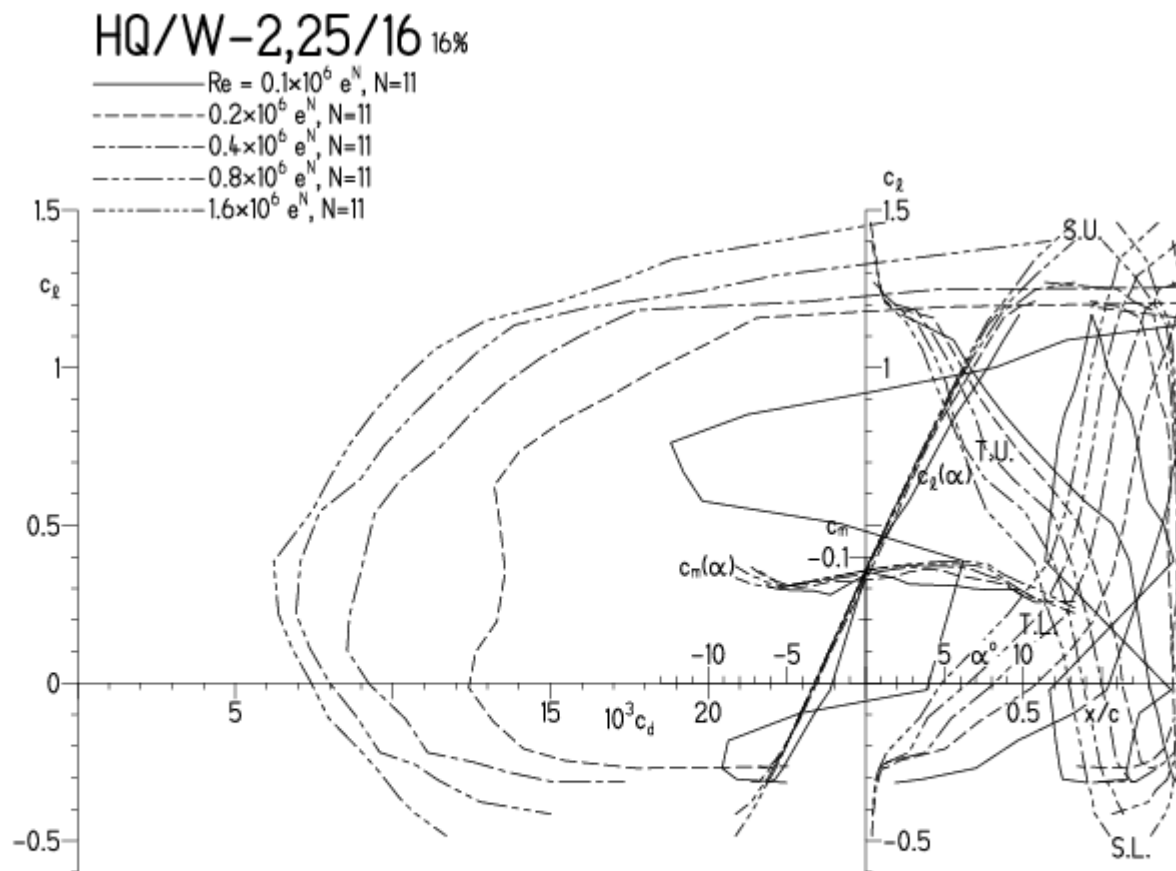


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

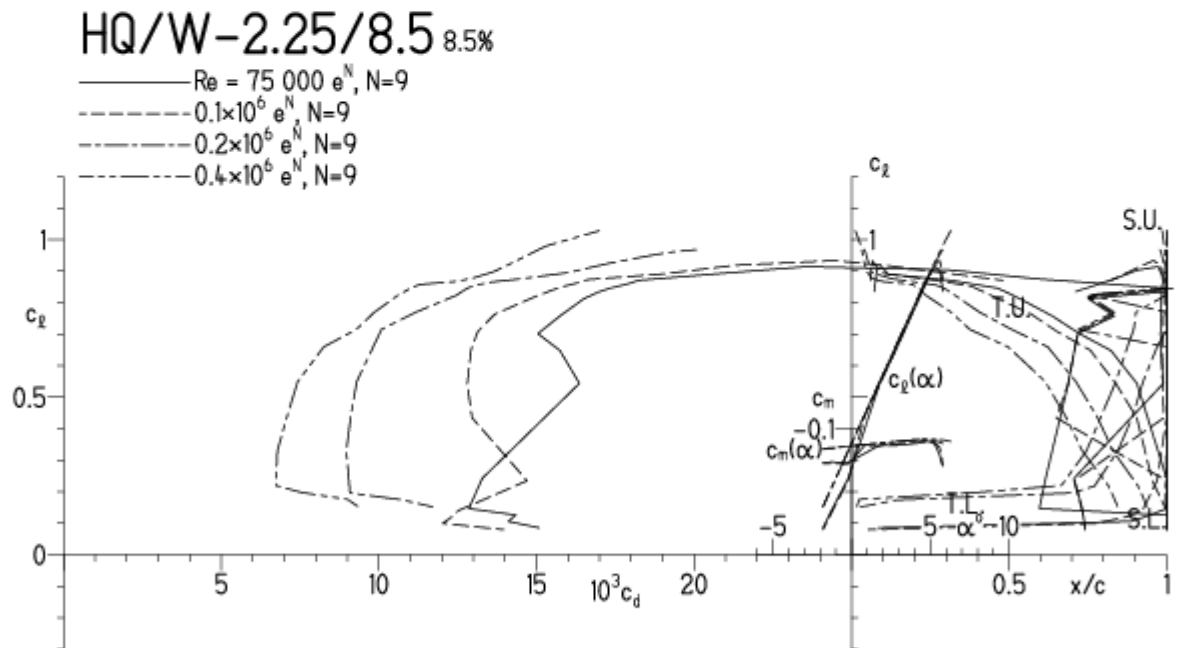


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

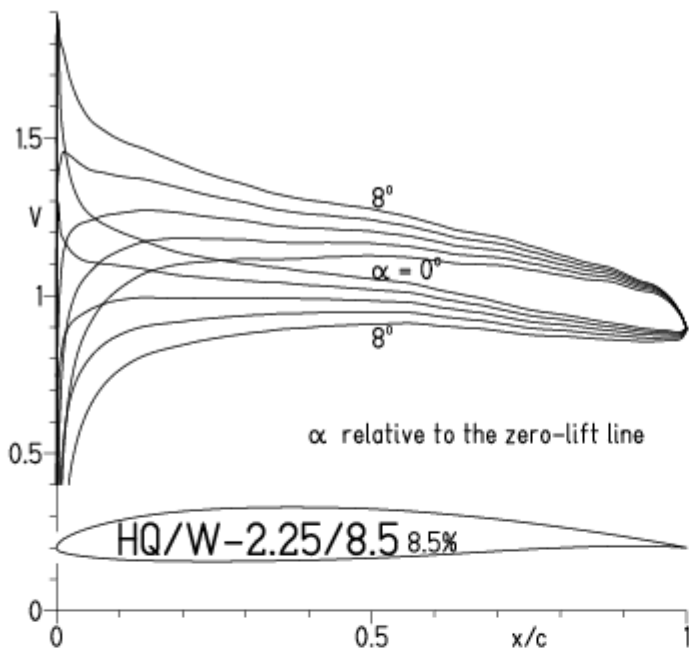


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

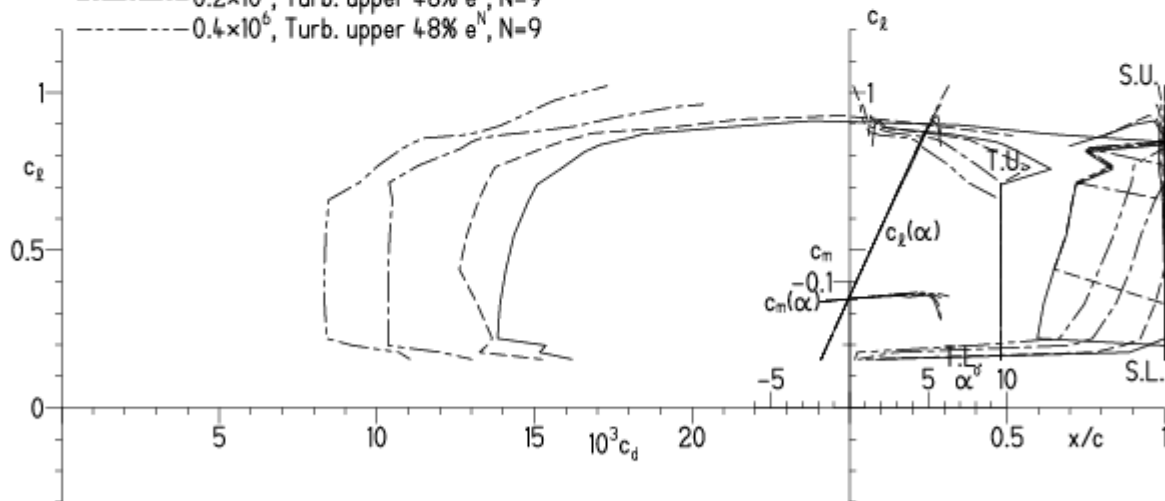
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

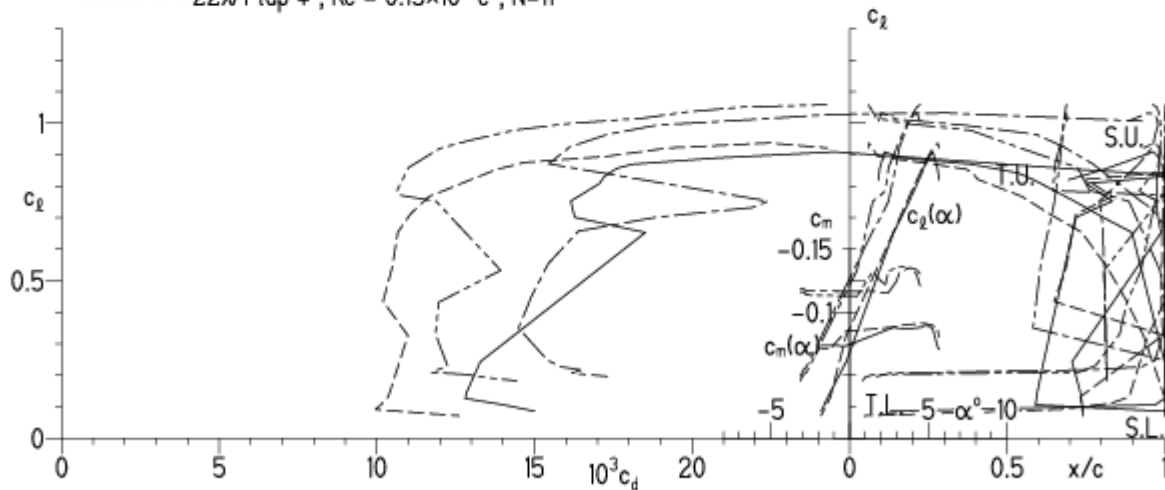


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

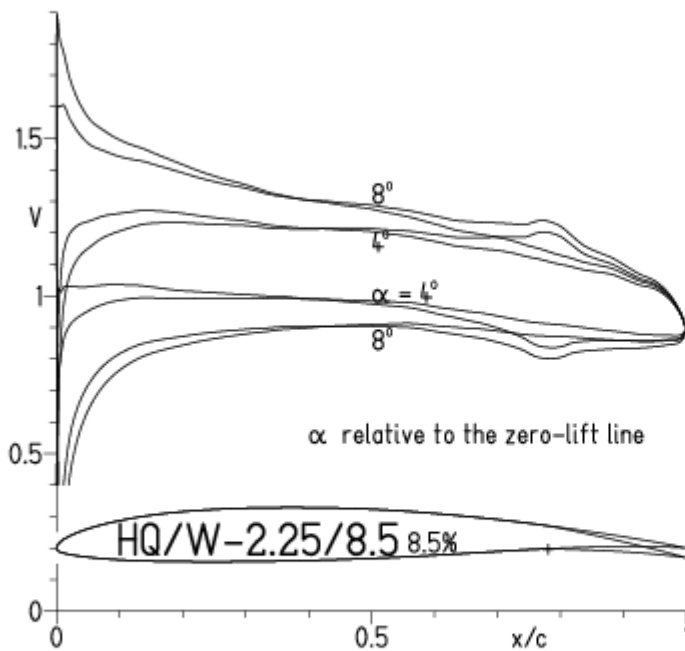
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

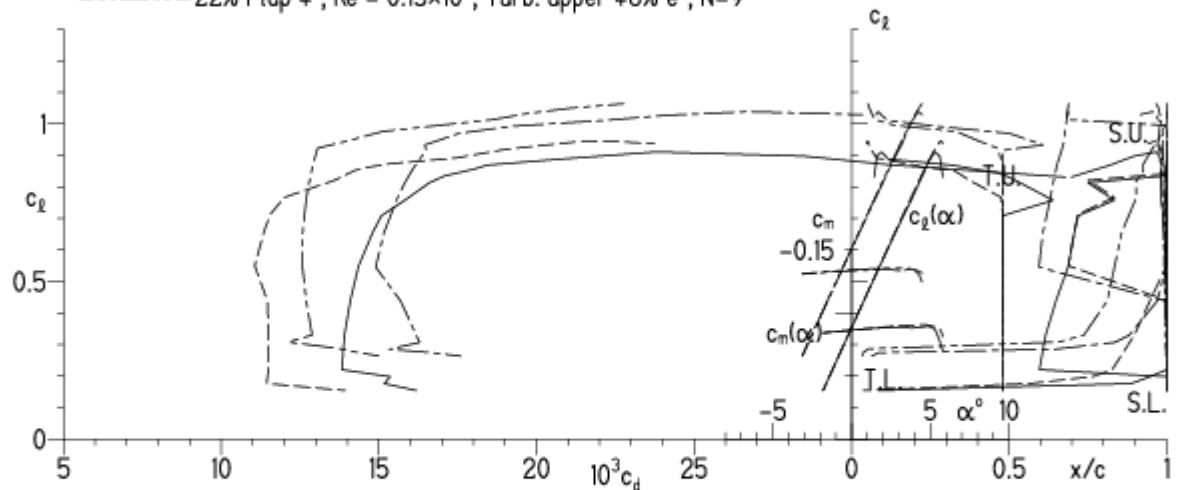


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

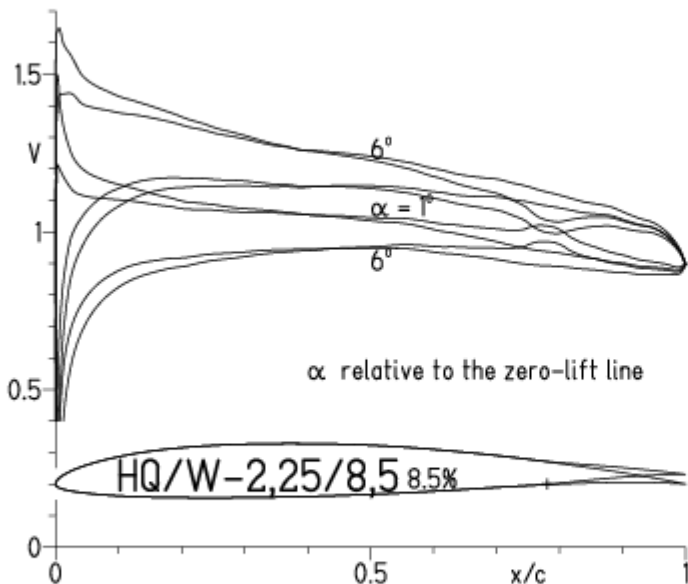
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

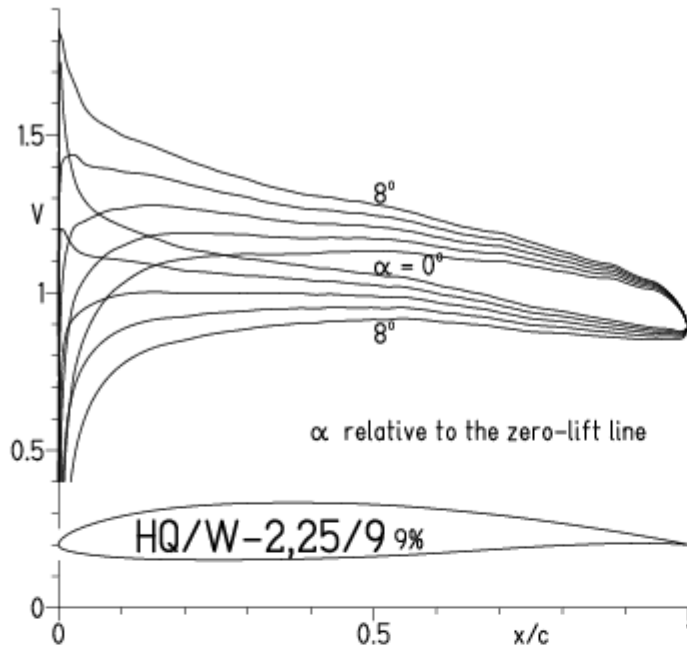


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

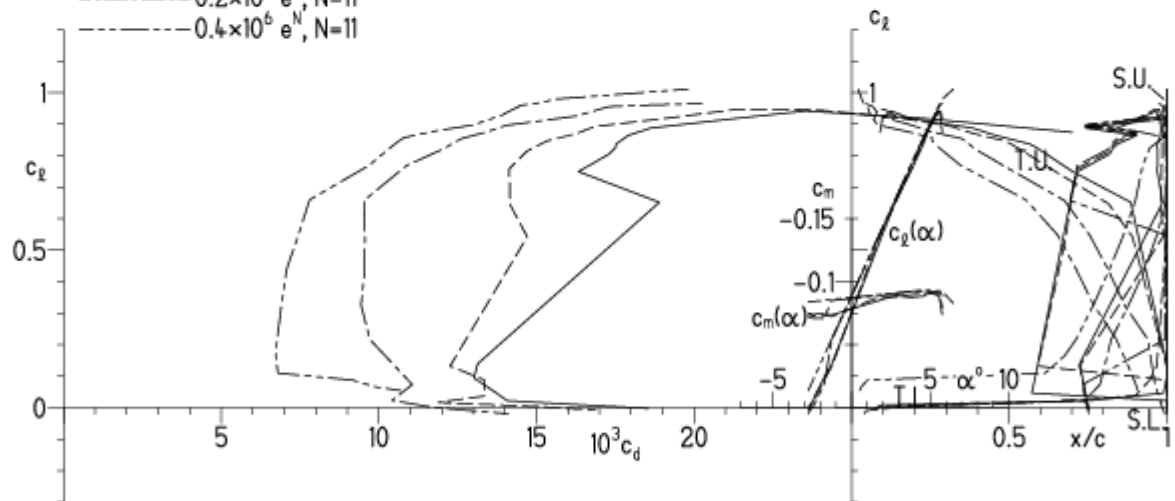
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

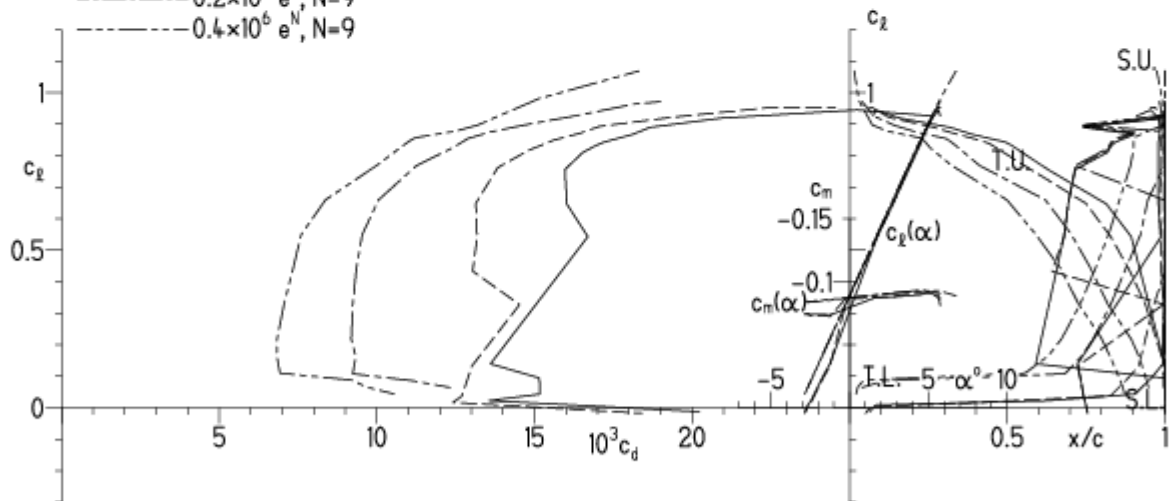
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

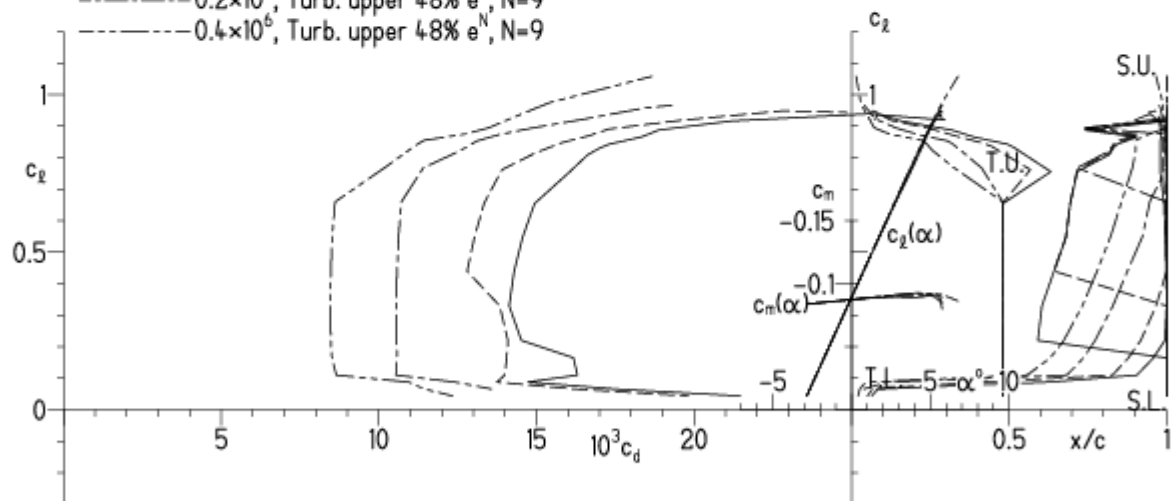
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48

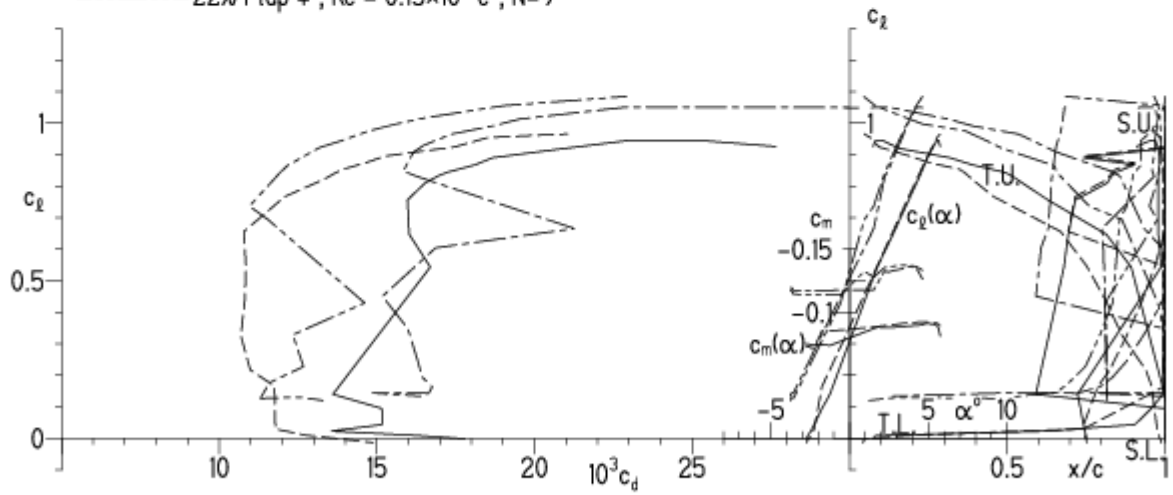


EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

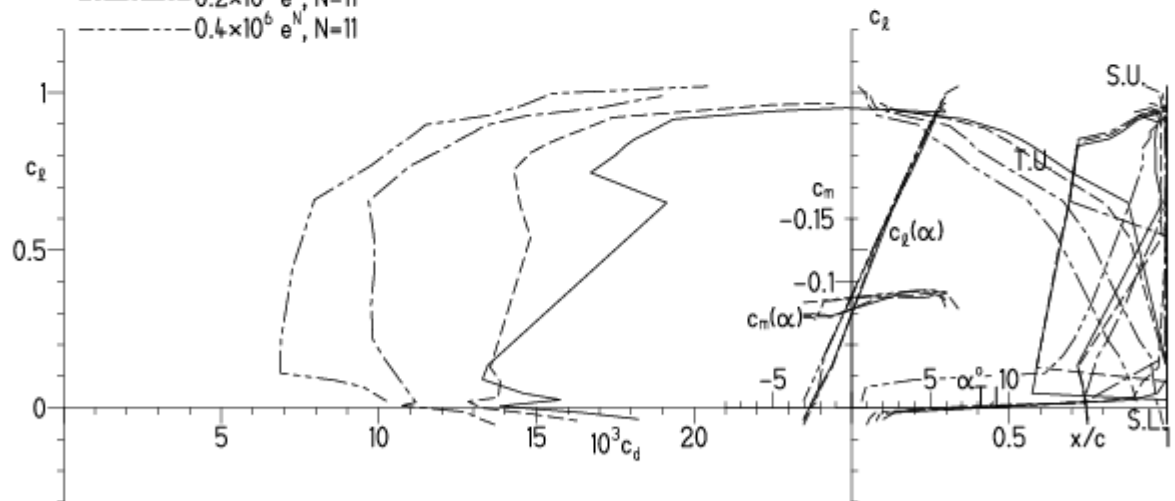
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

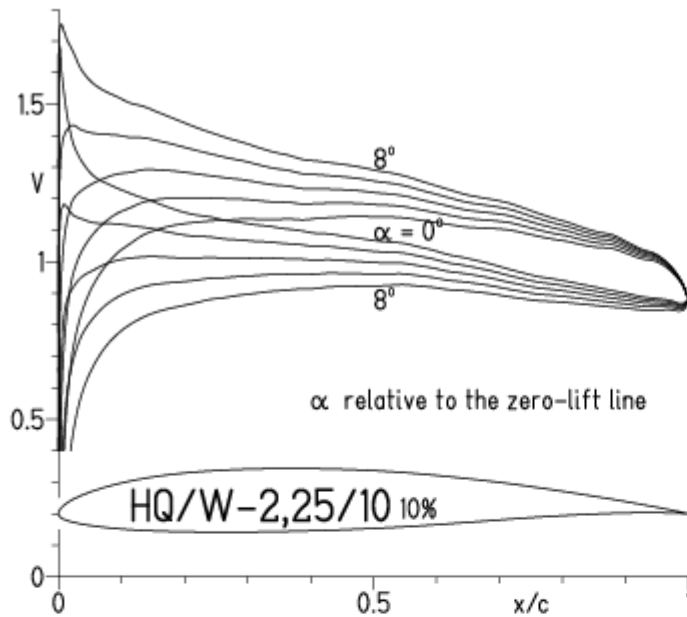


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

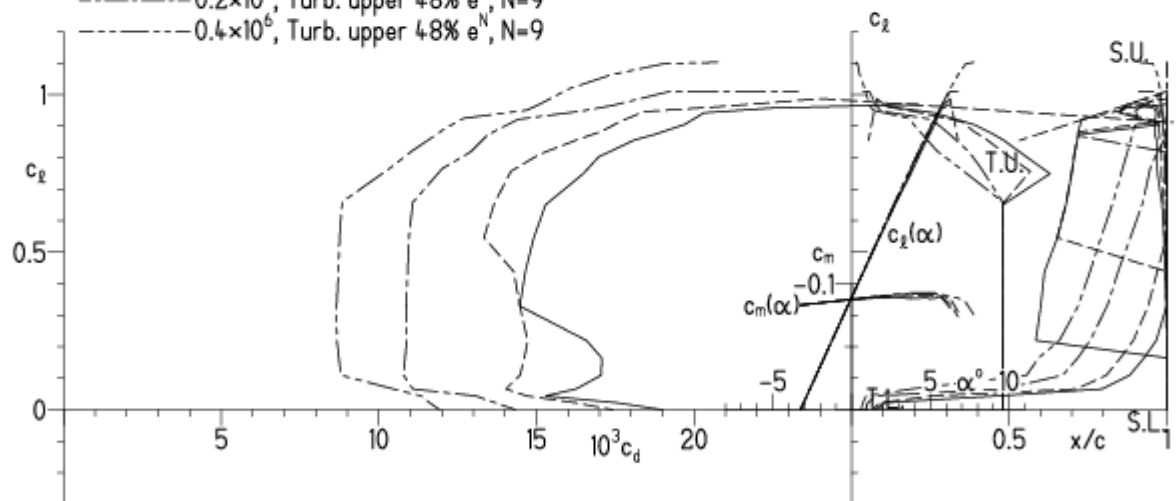
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

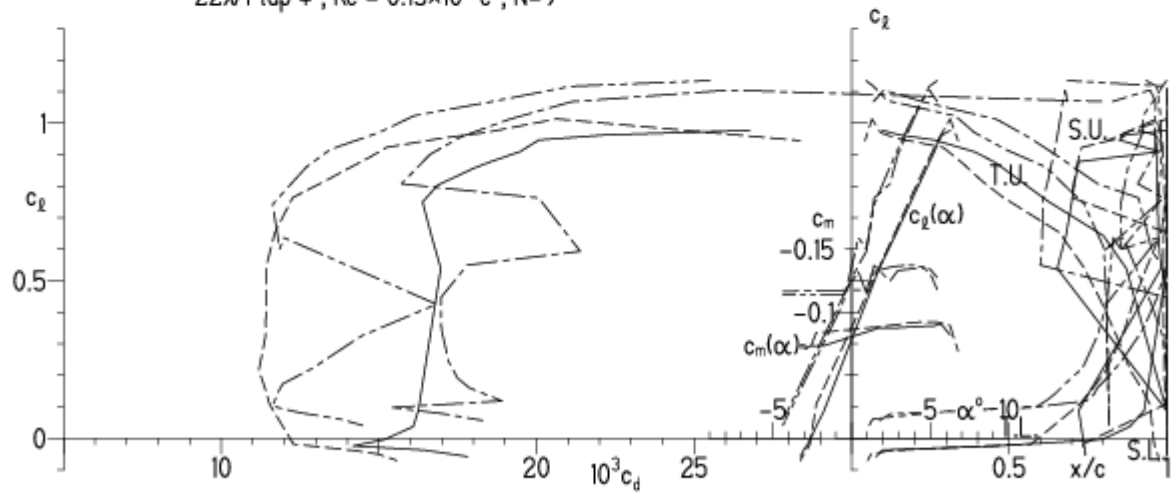


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

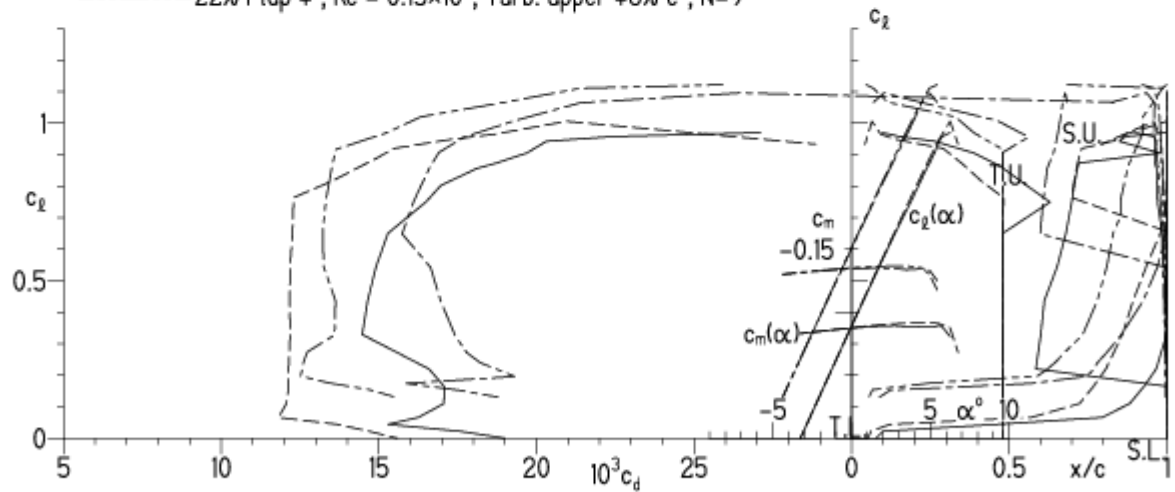


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

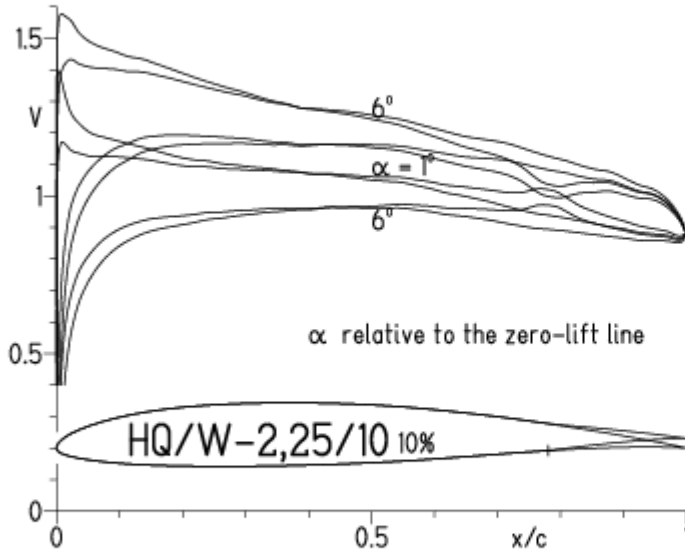
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

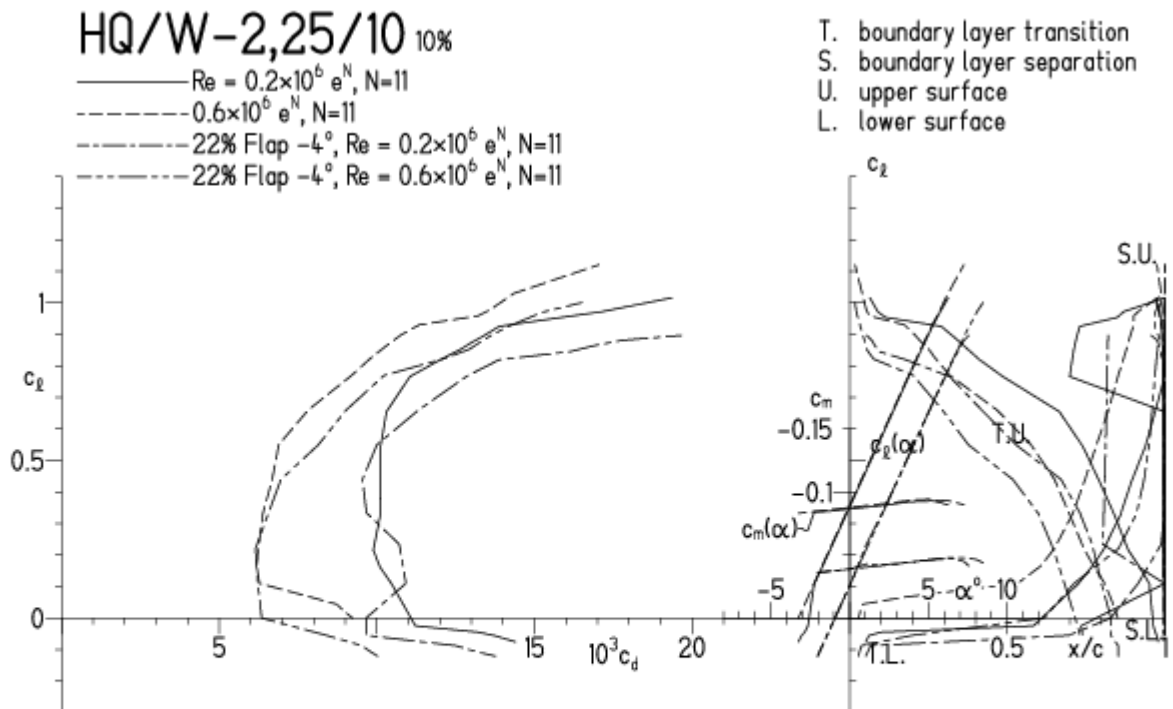


HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

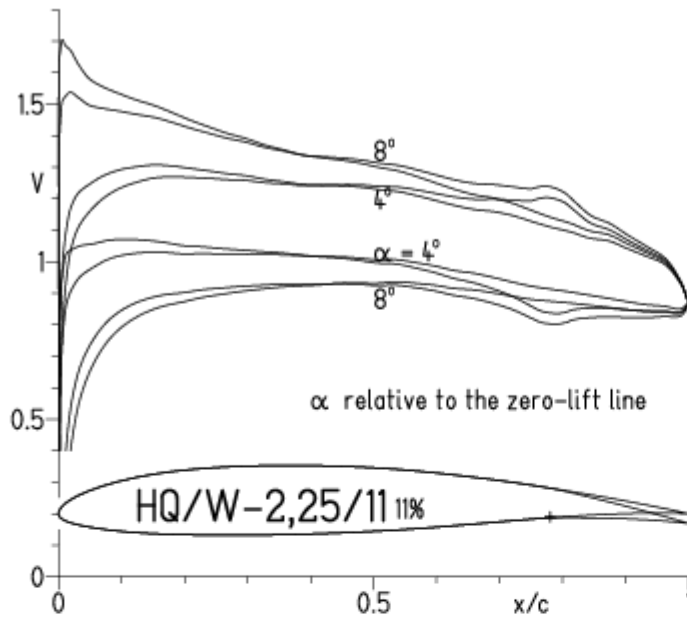
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

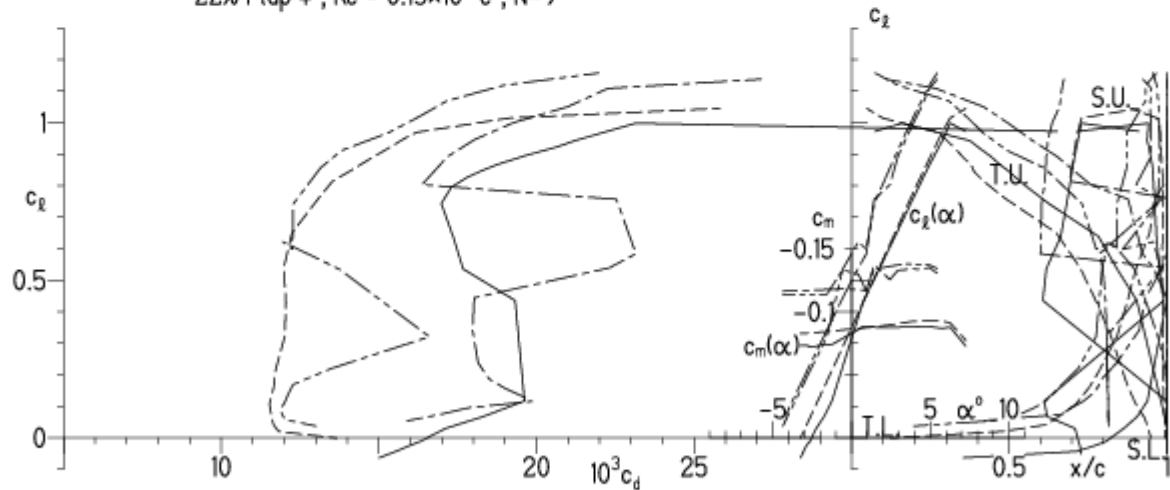


EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- Re = 0.2×10^6 e^N, N=9
- - - 0.8×10^6 e^N, N=9
- · - · 22% Flap 4°, Re = 0.2×10^6 e^N, N=9
- · - · 22% Flap 4°, Re = 0.8×10^6 e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

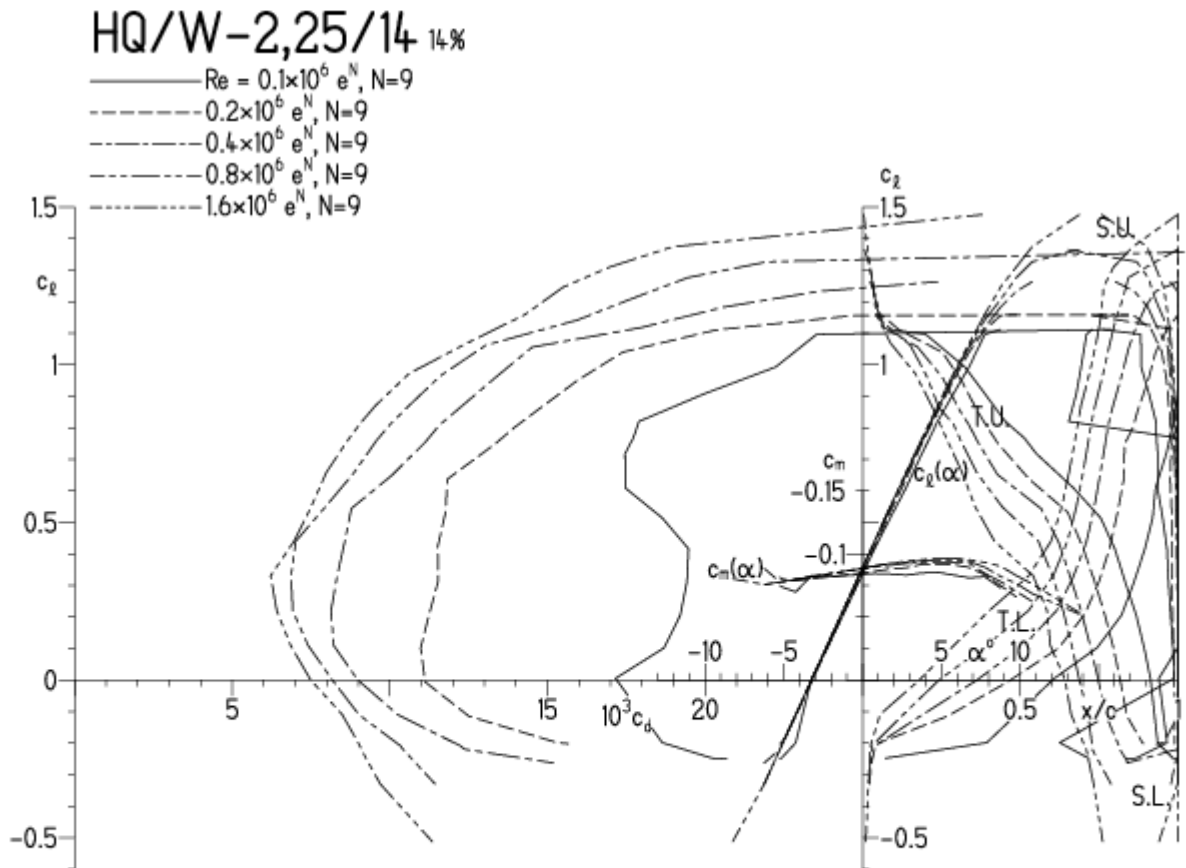


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

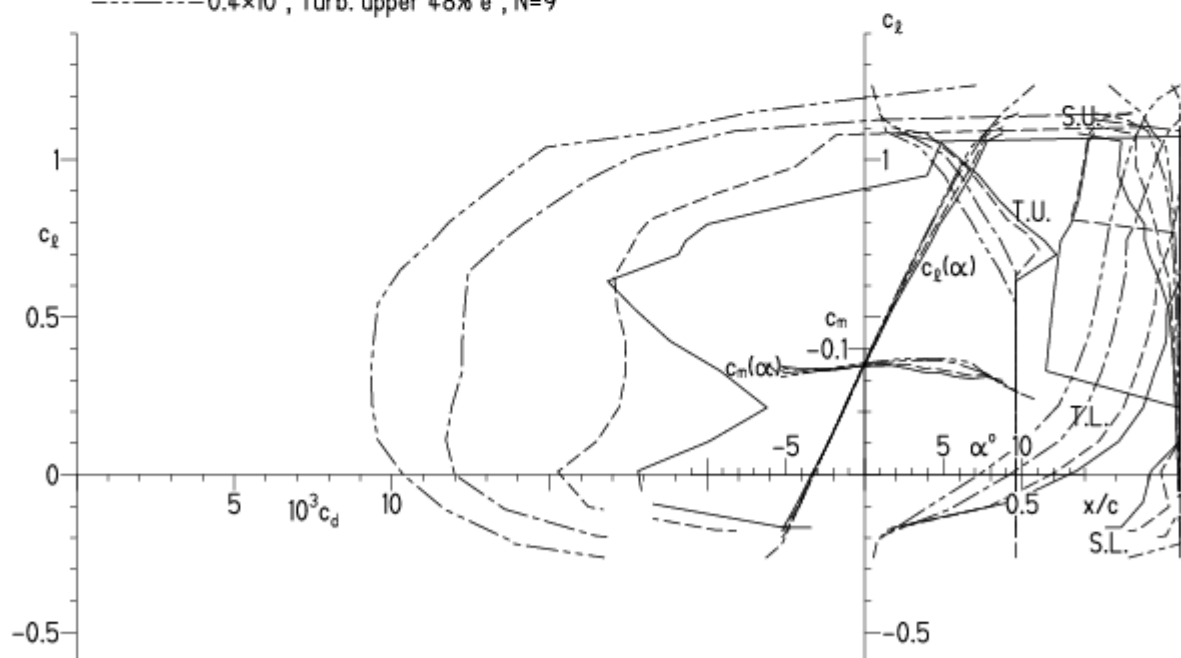
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

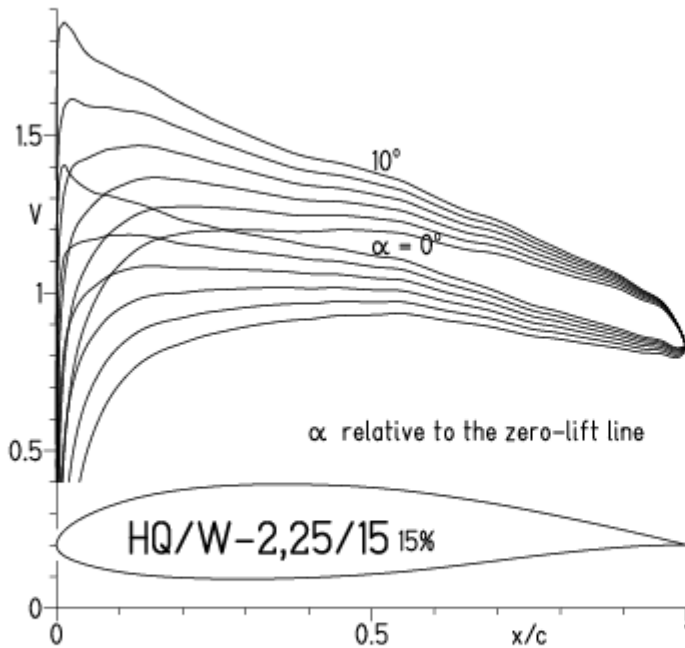


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31

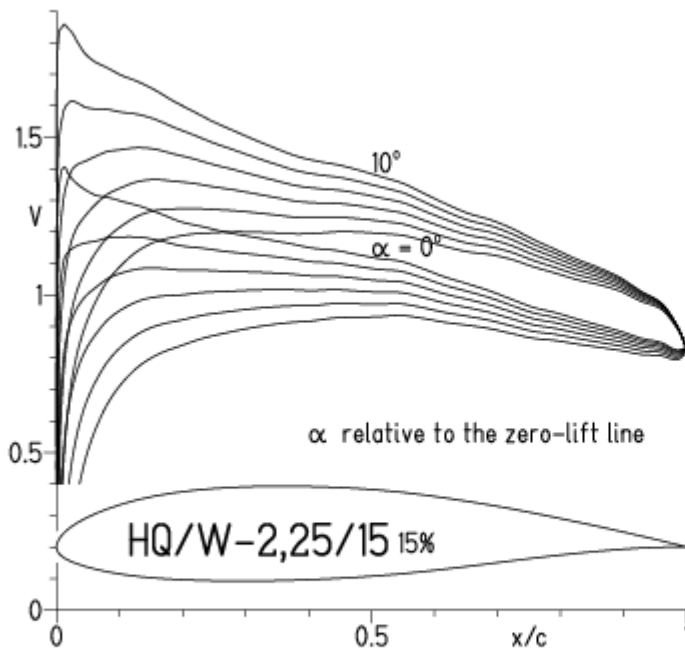


EPPLER 20

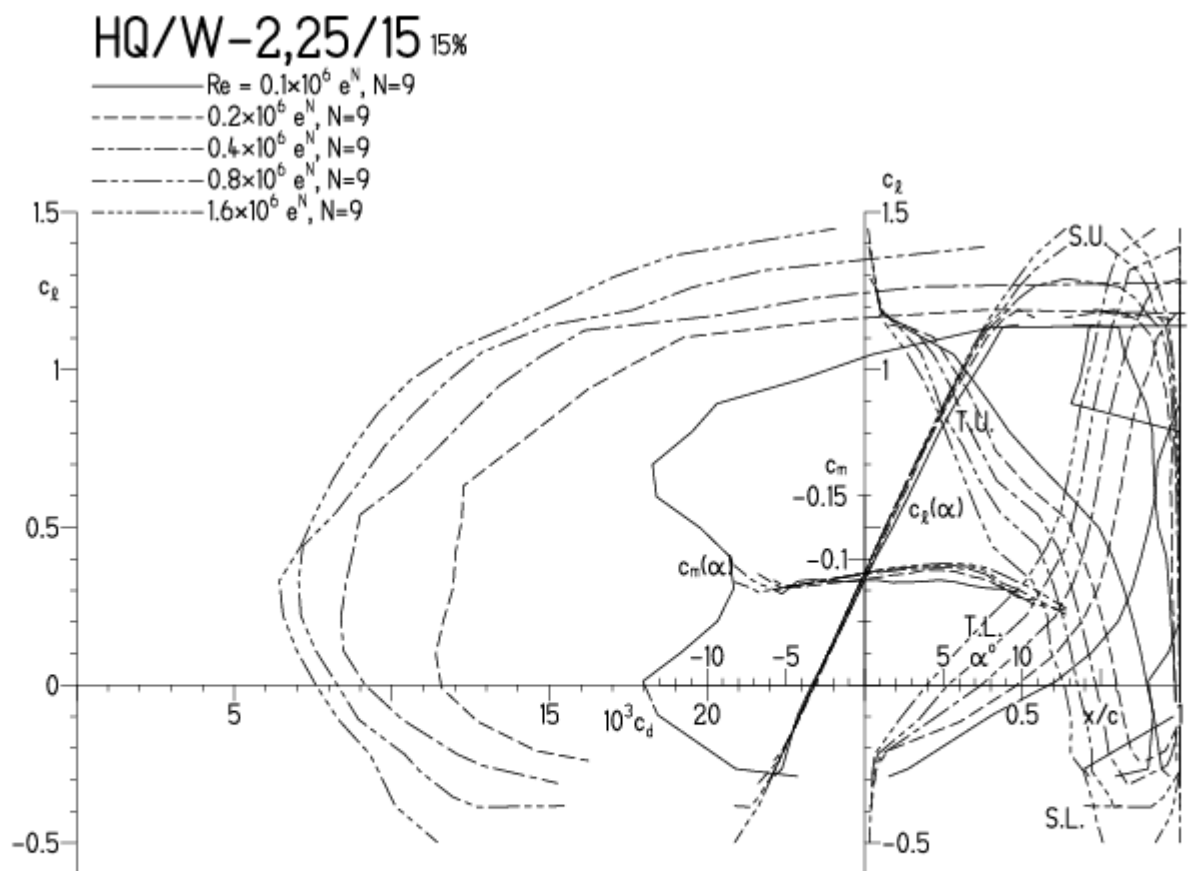


HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

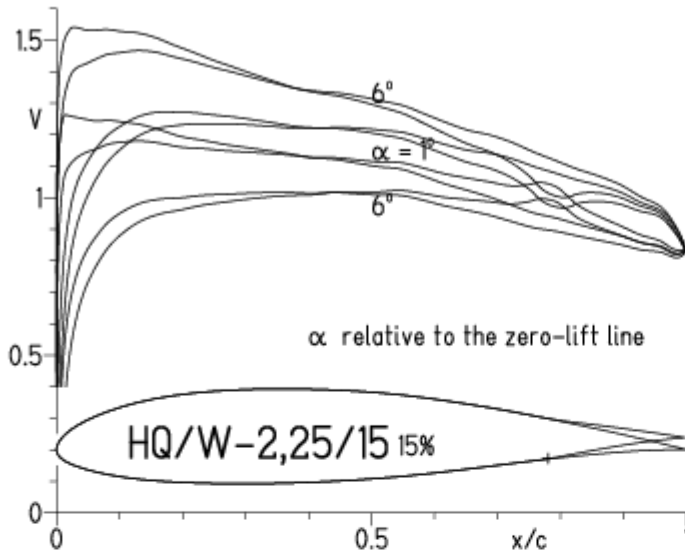


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

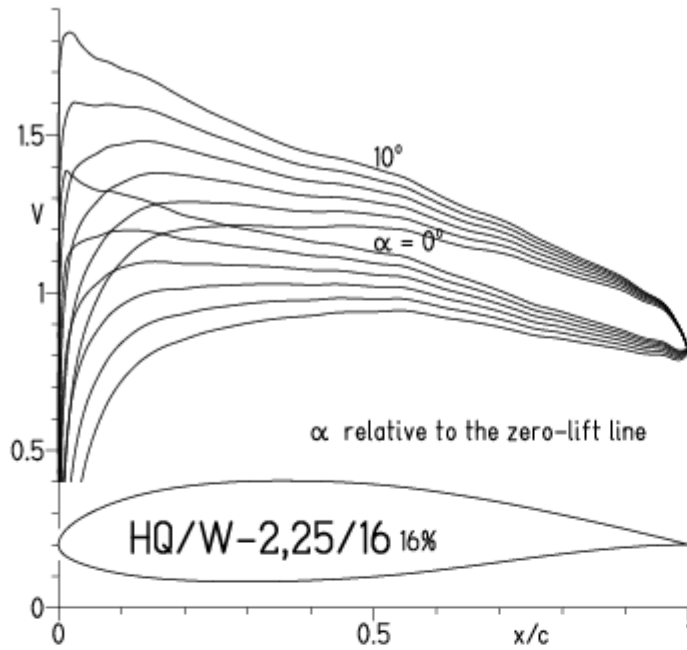
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

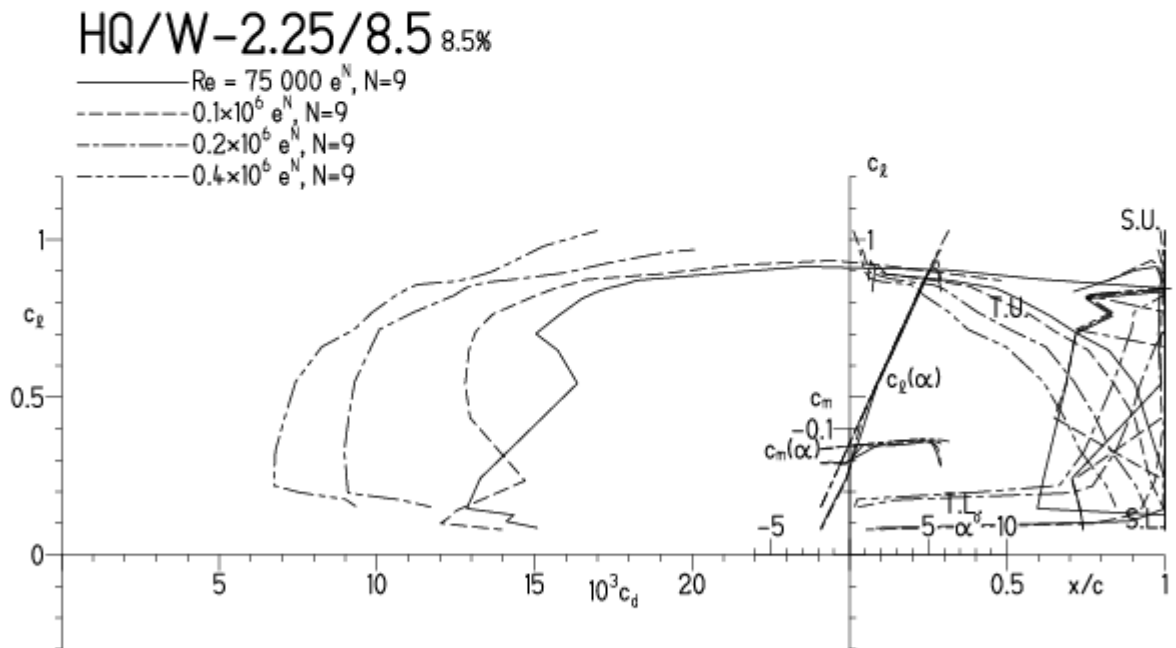


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

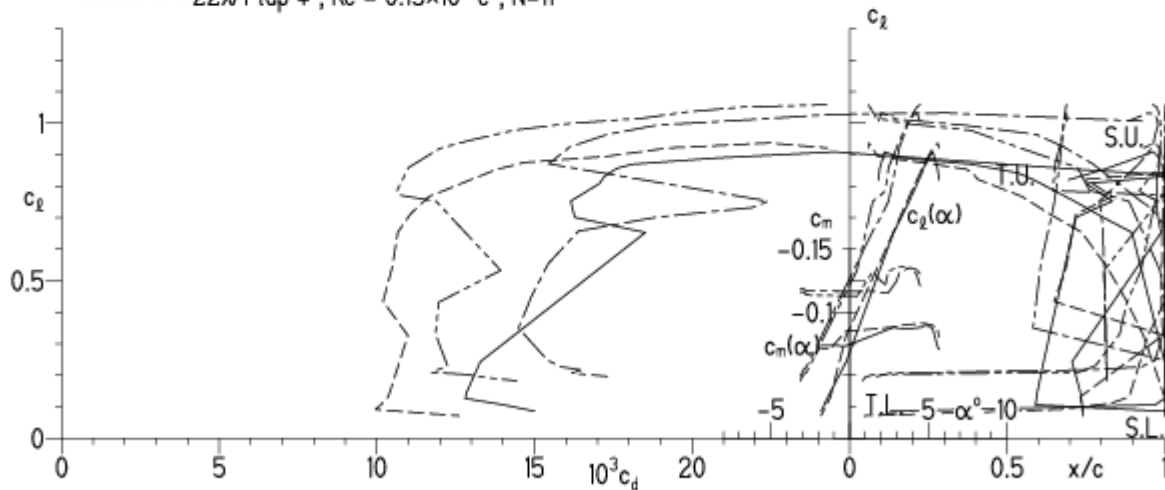


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

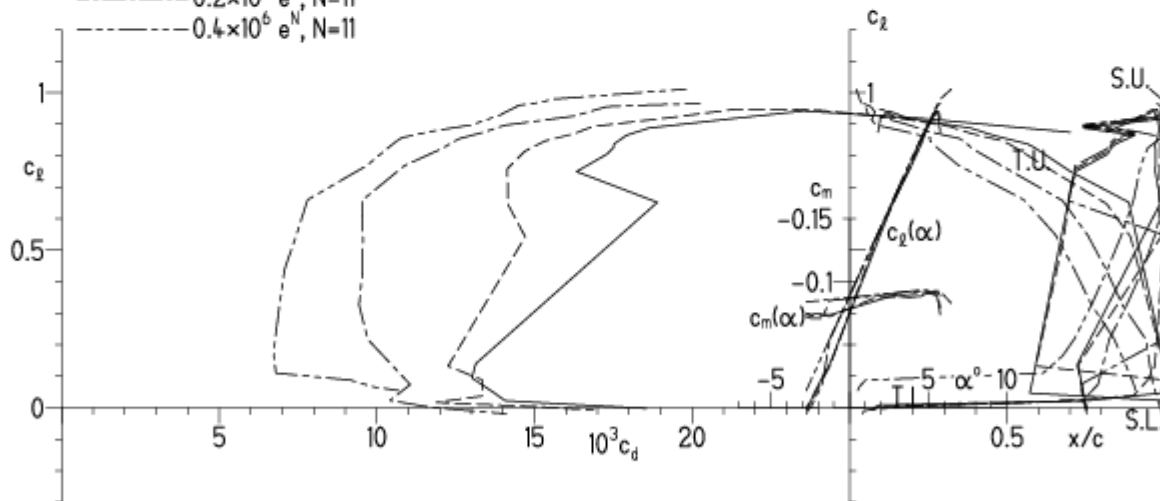
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



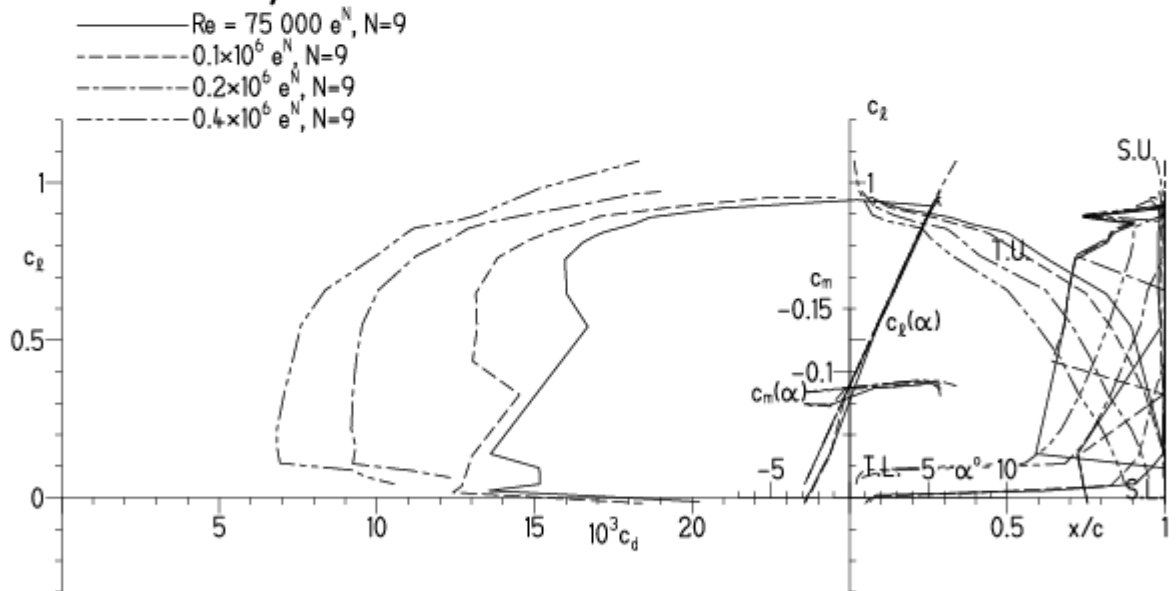
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

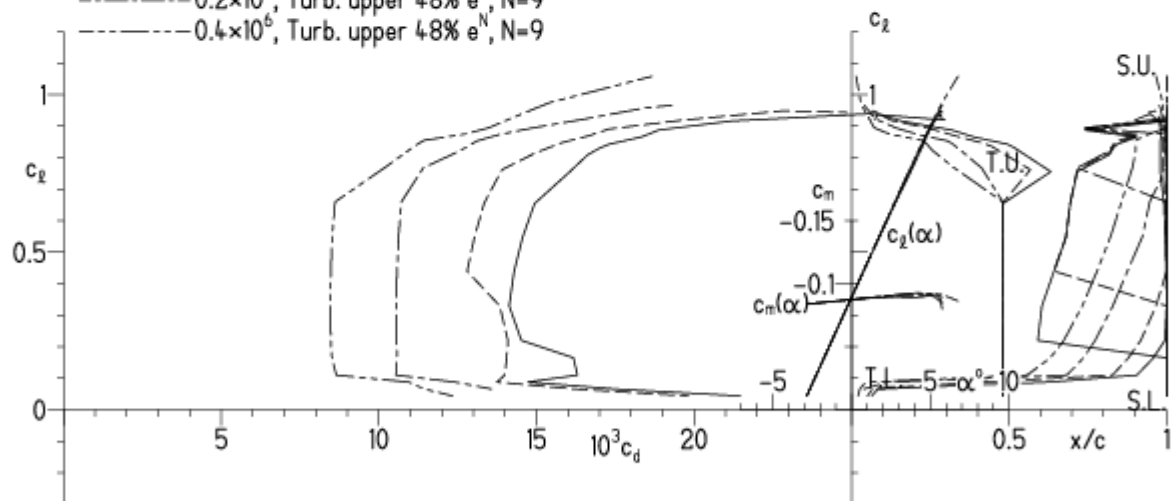
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



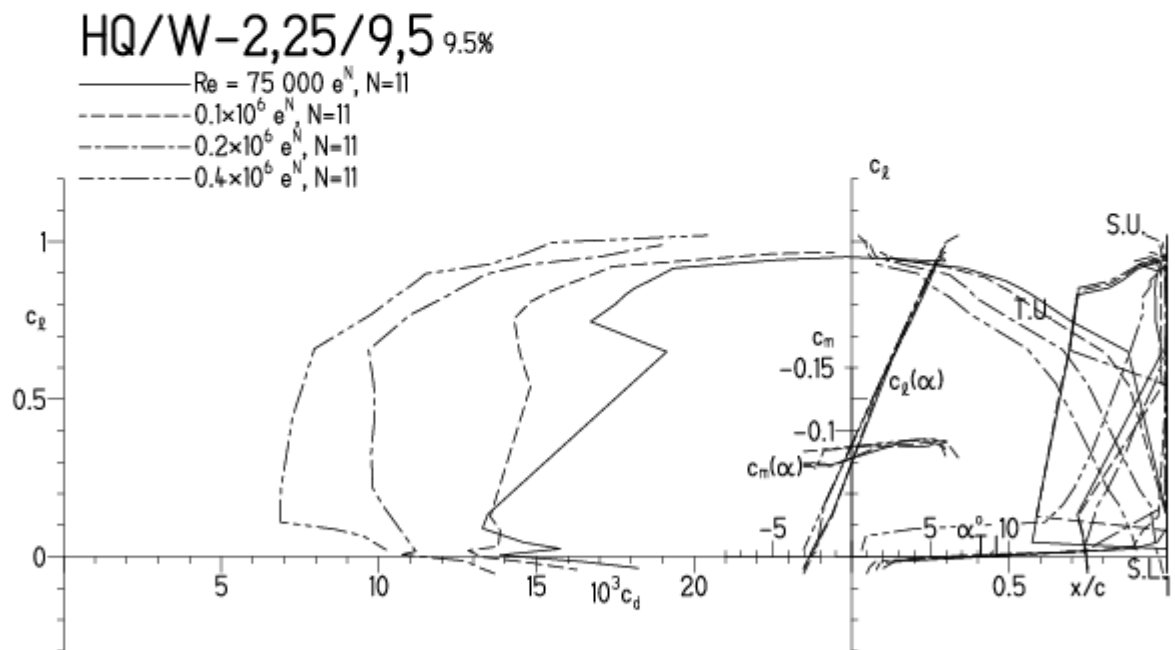
- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

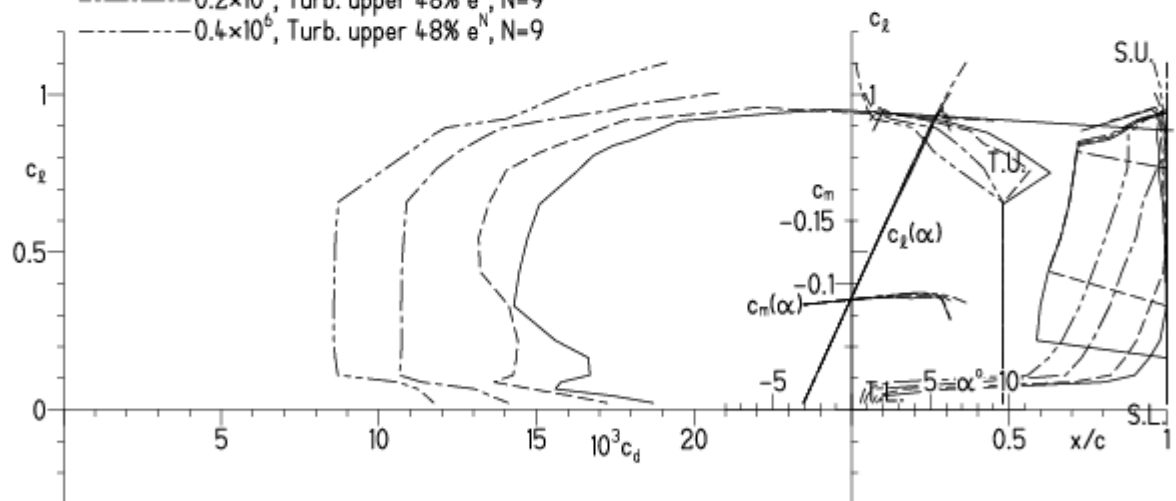
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

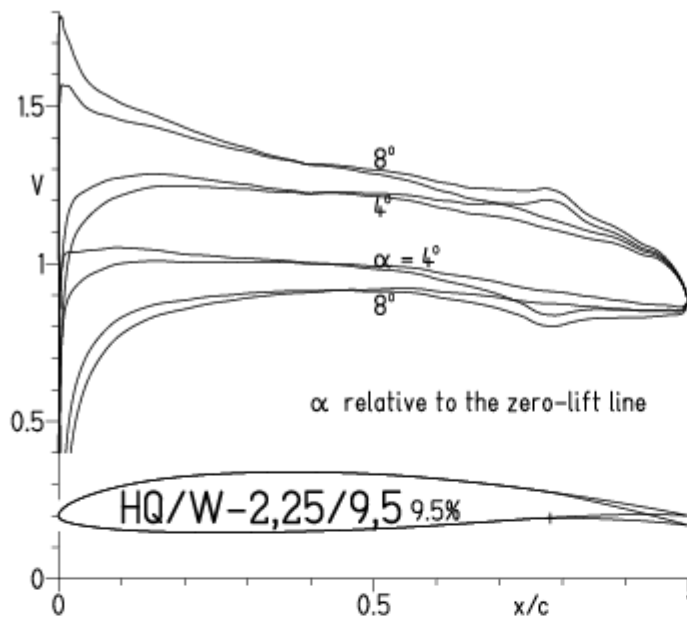
- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

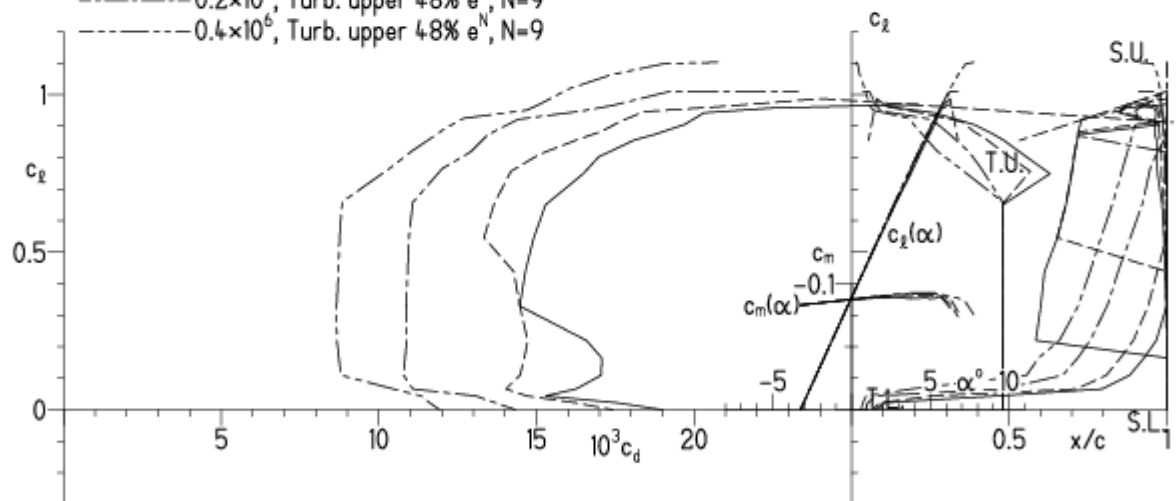
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

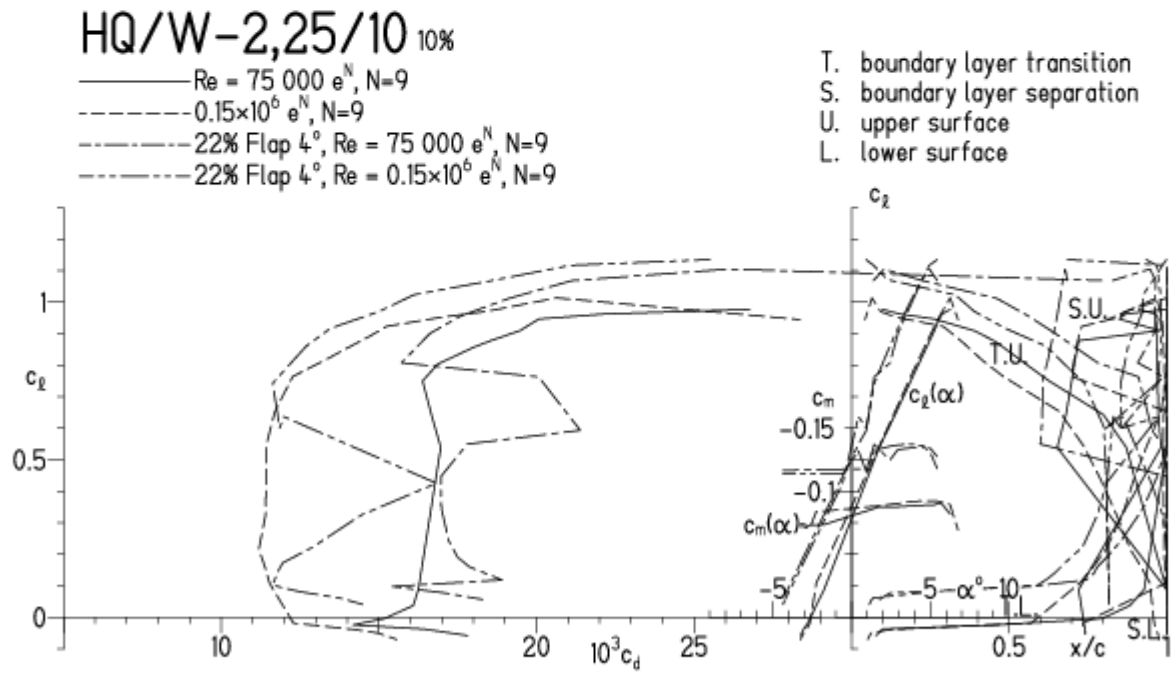


HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

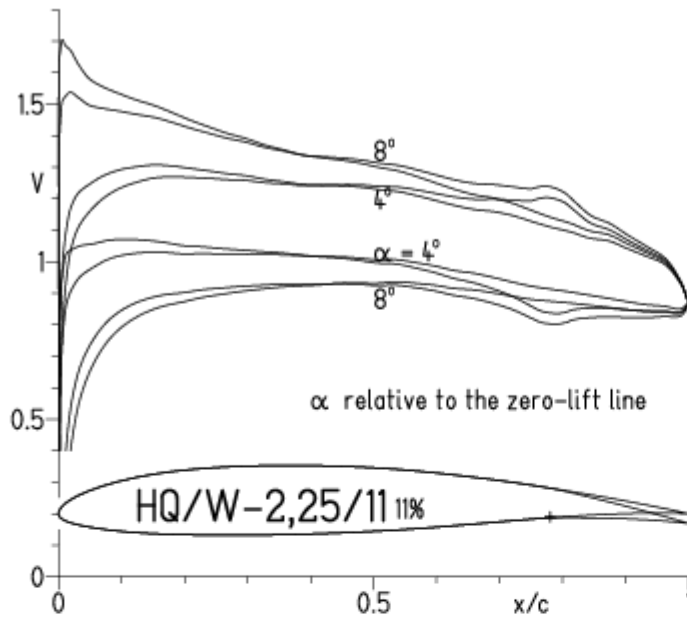
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

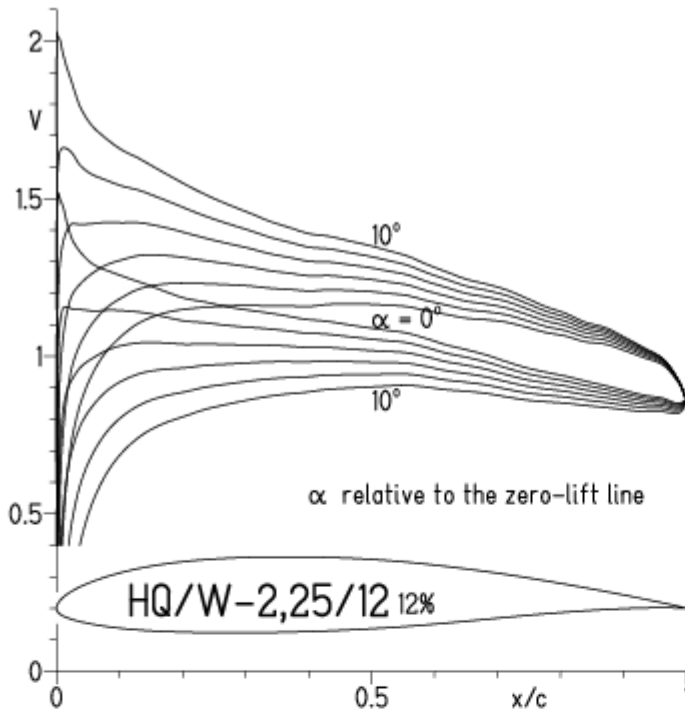
HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

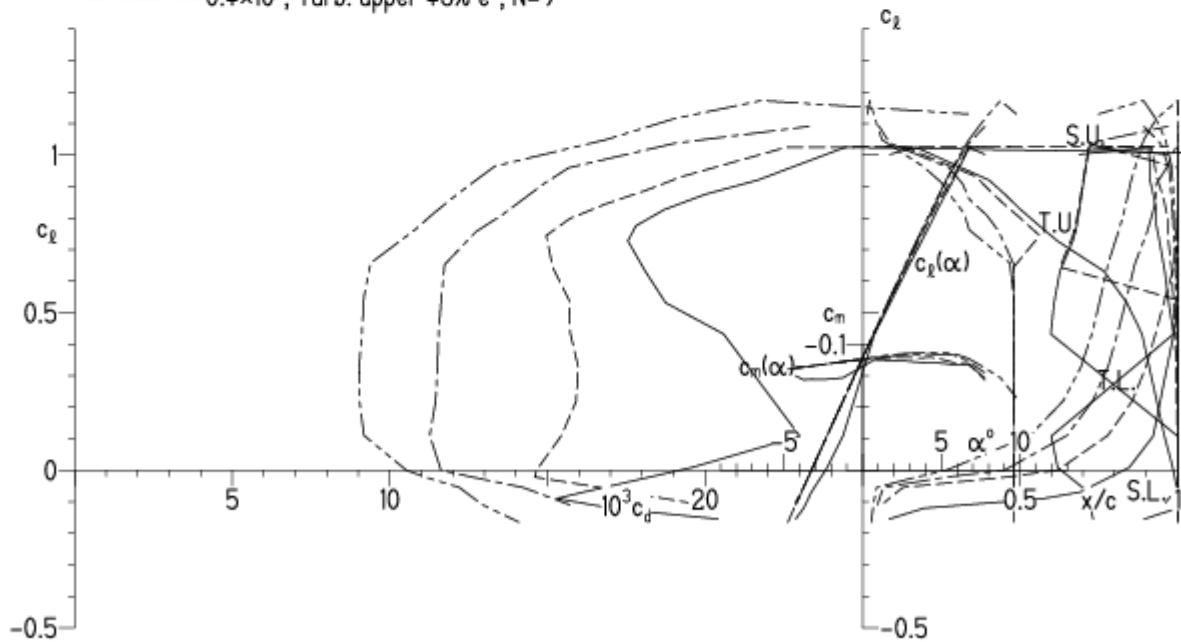
EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

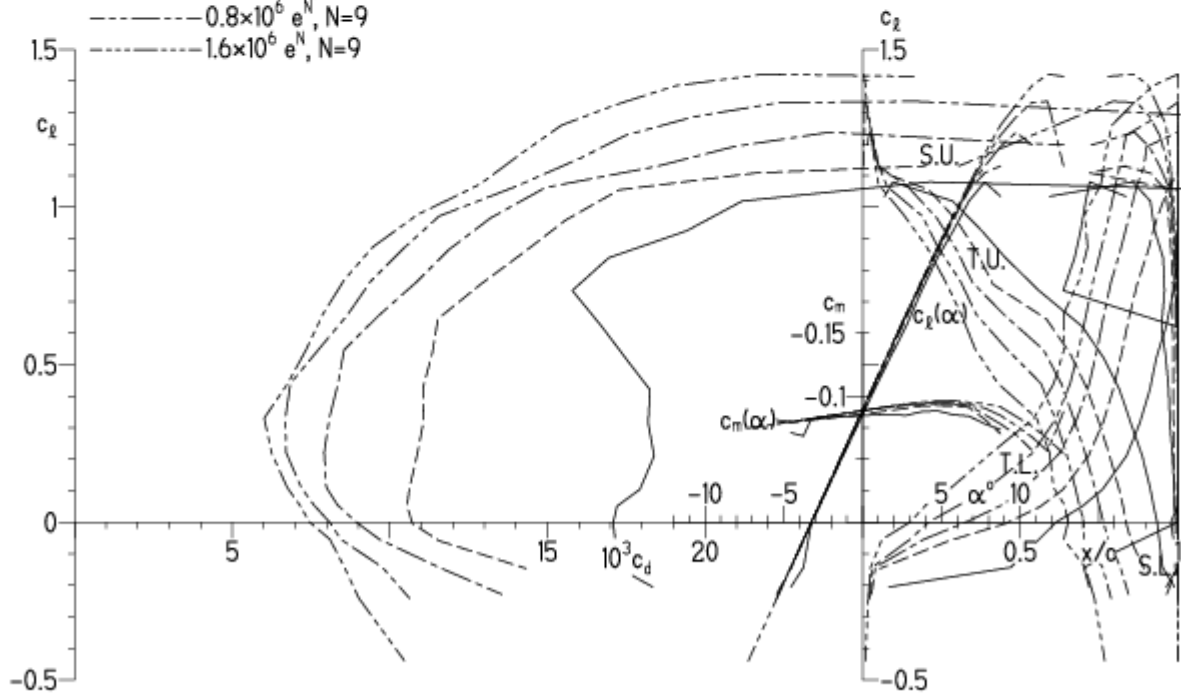
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

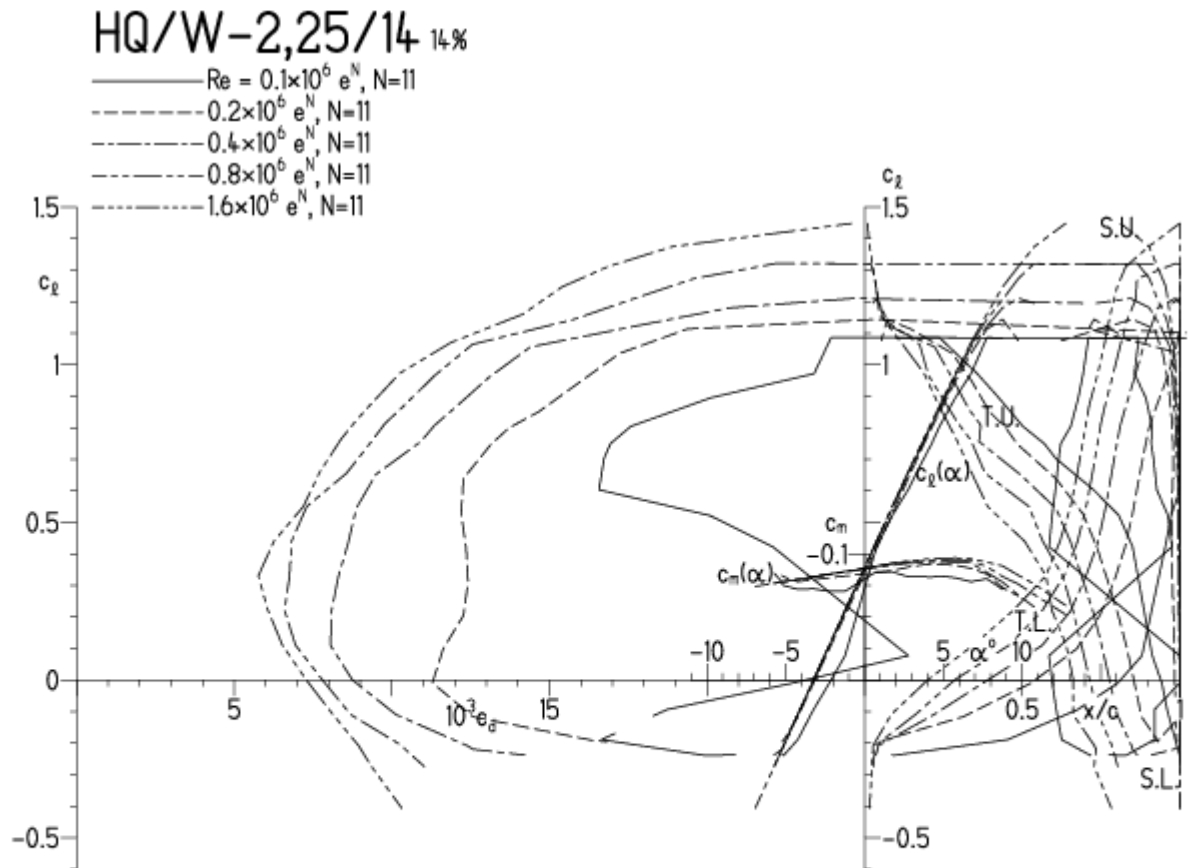


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

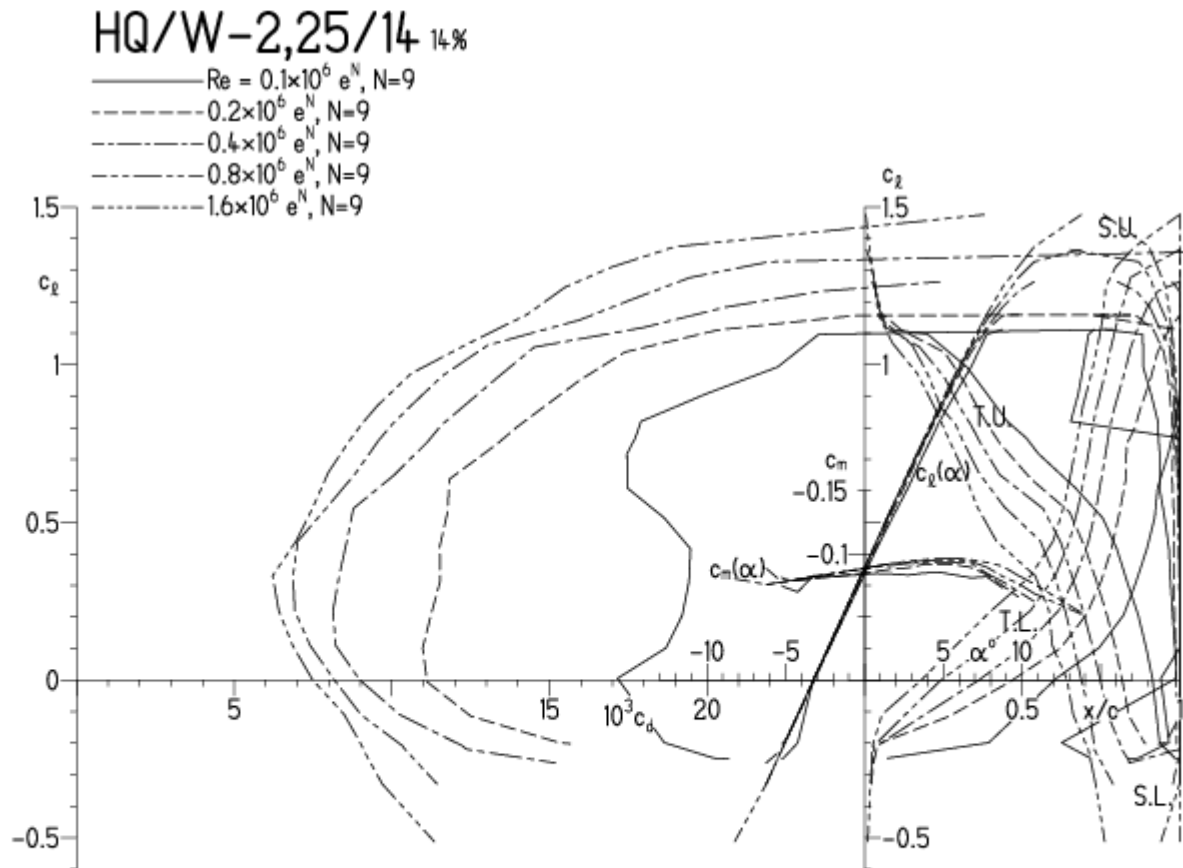


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

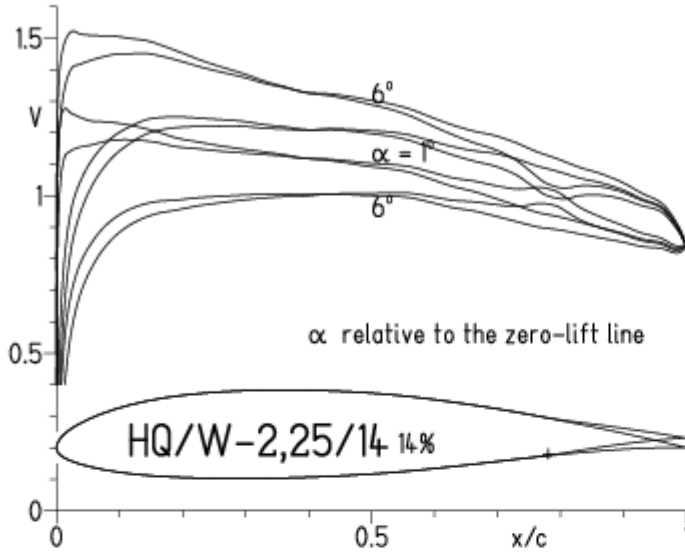
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

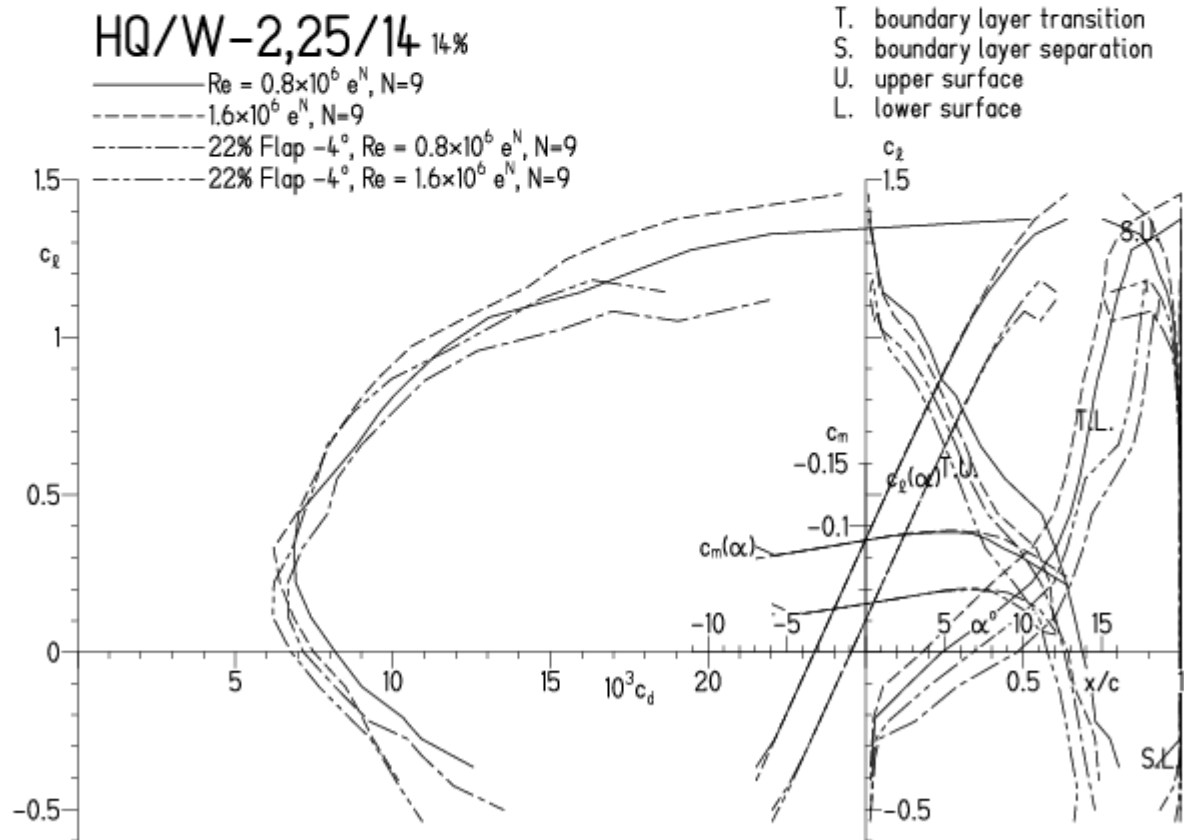


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

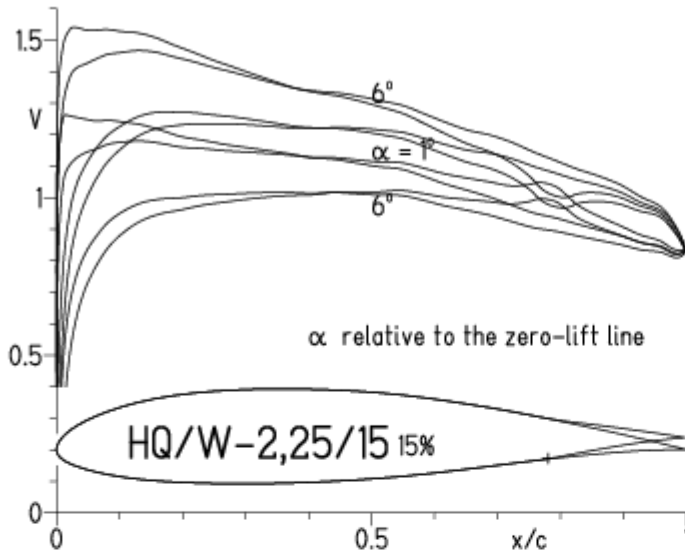


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

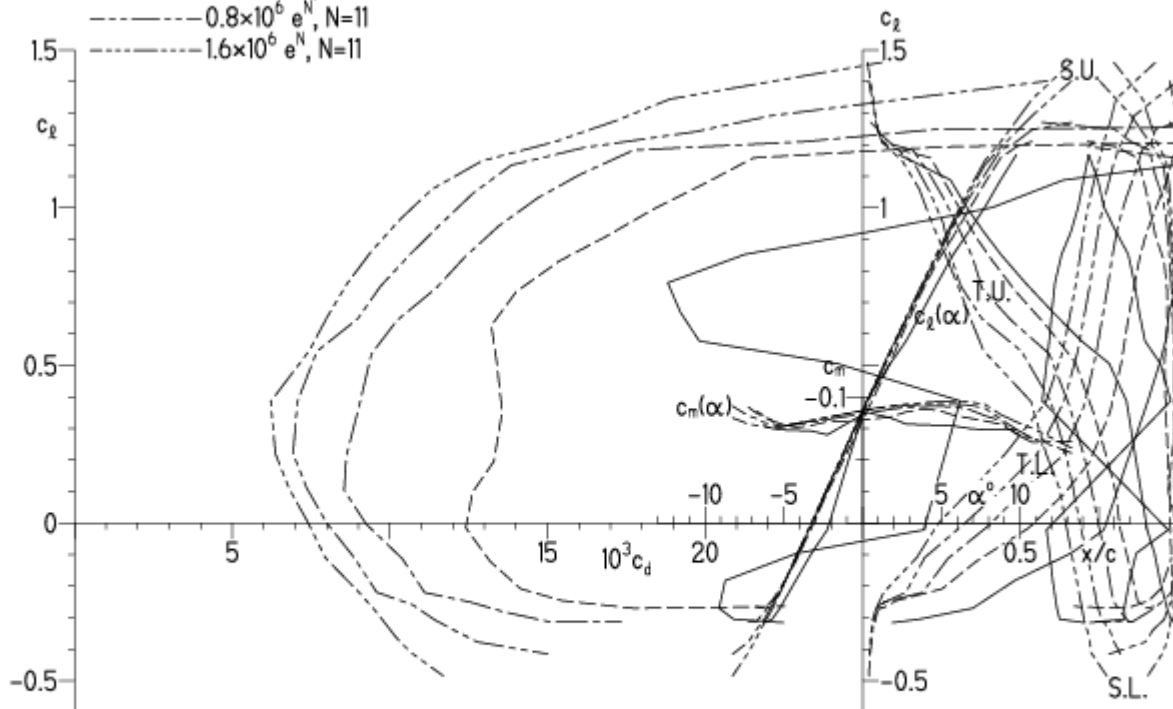
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41

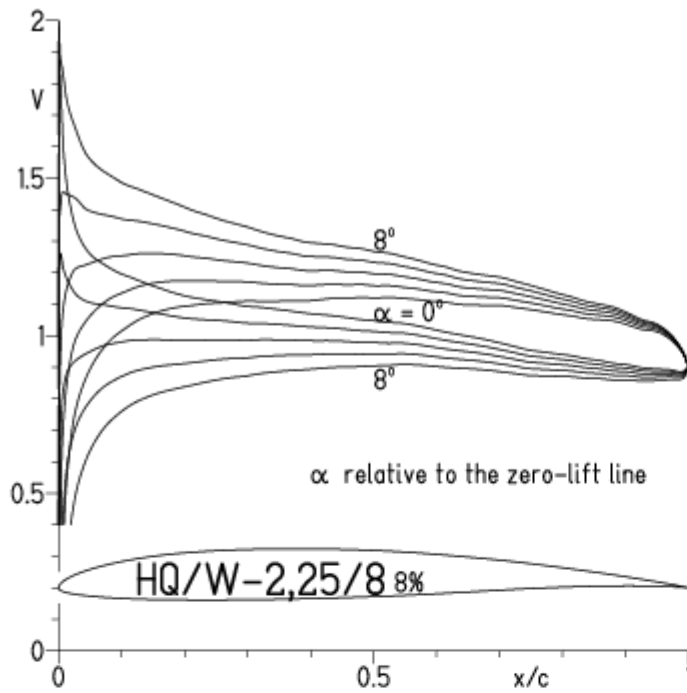


EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

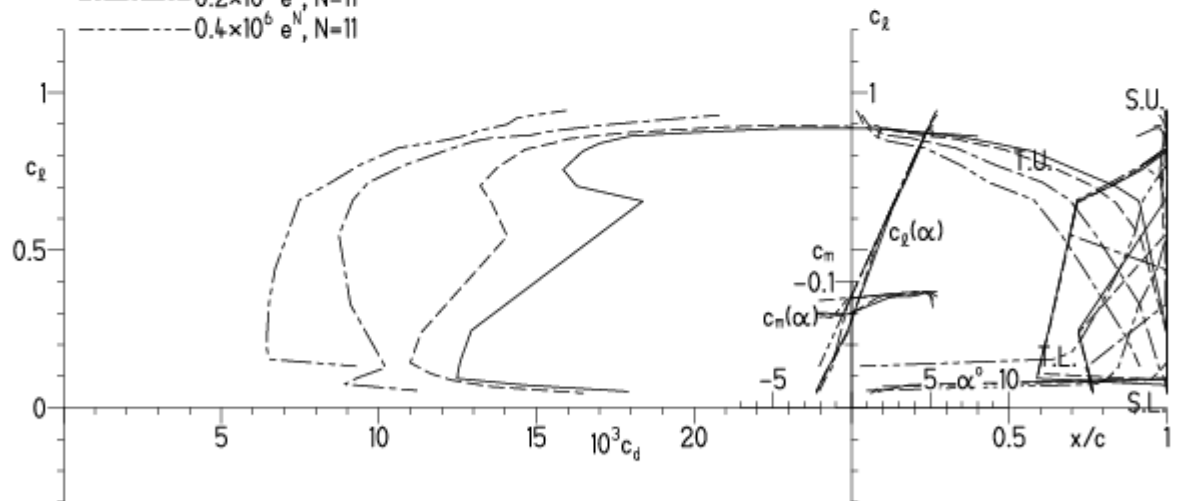
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

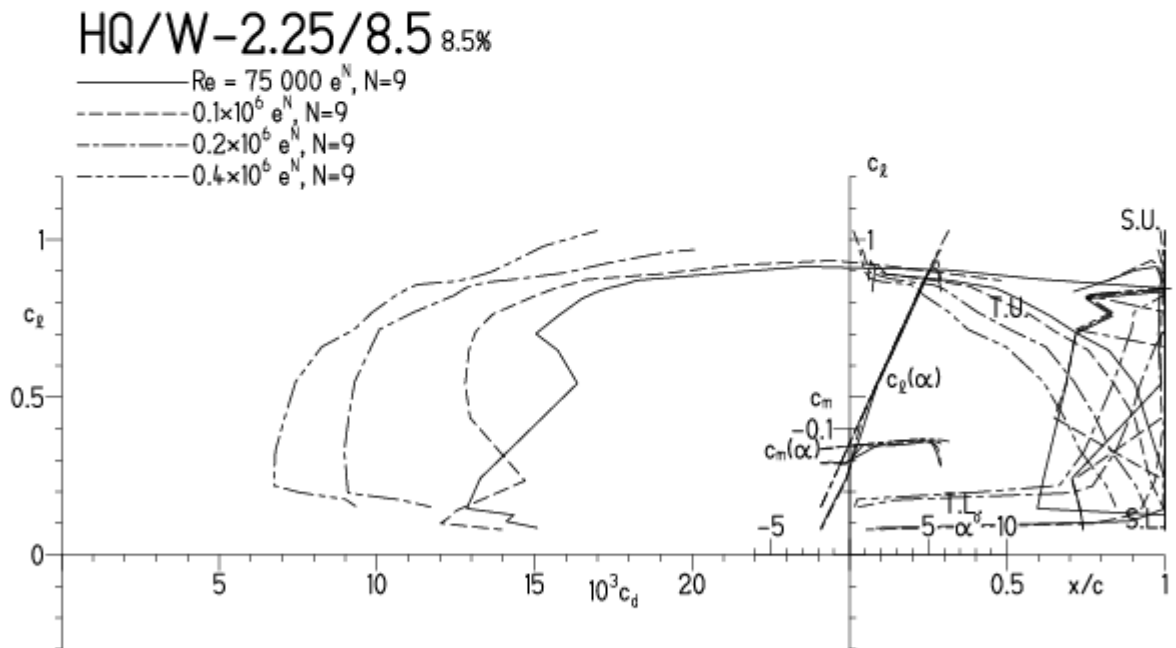


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

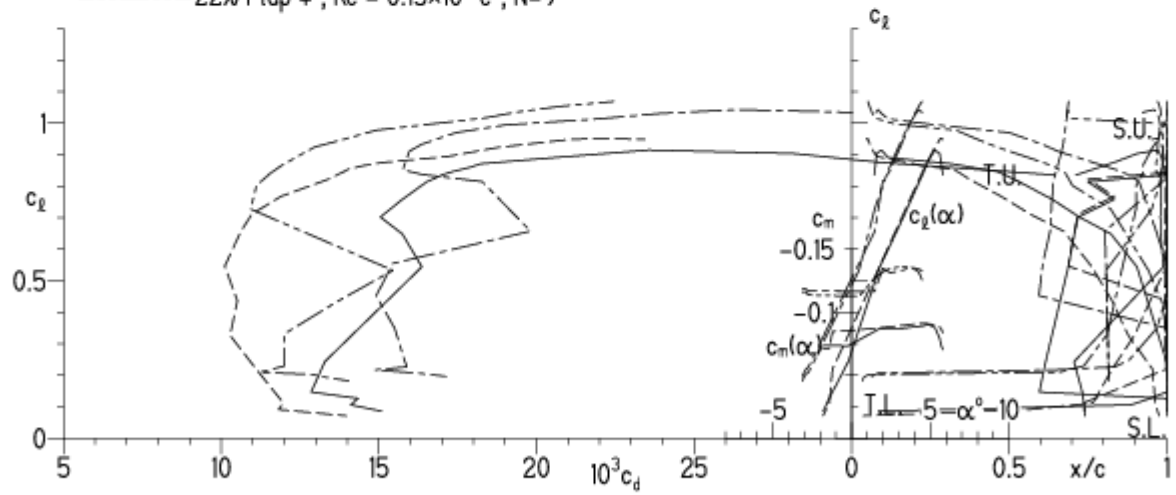


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

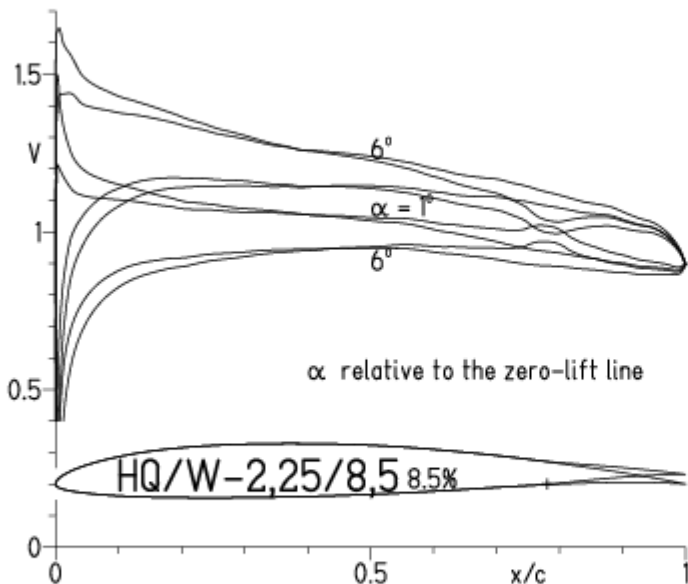
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



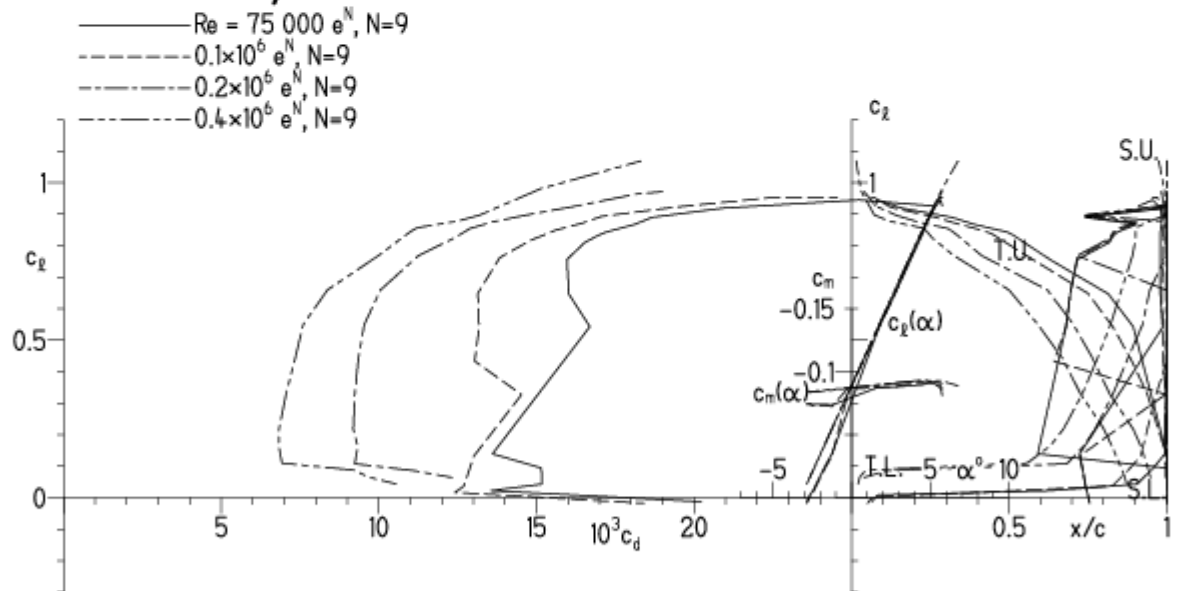
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

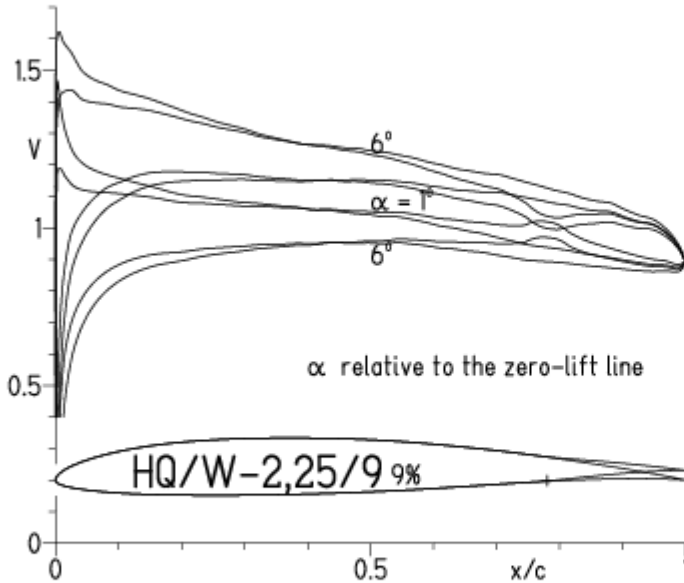
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



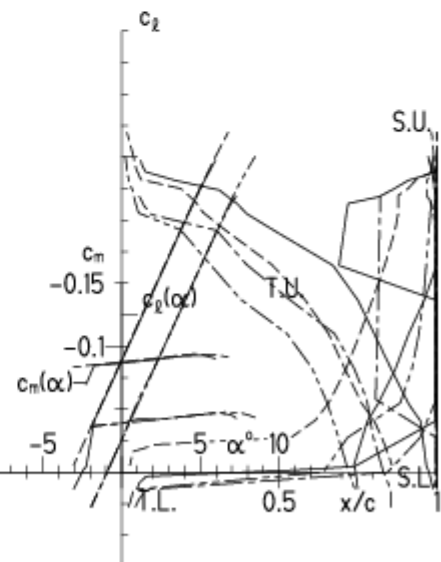
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

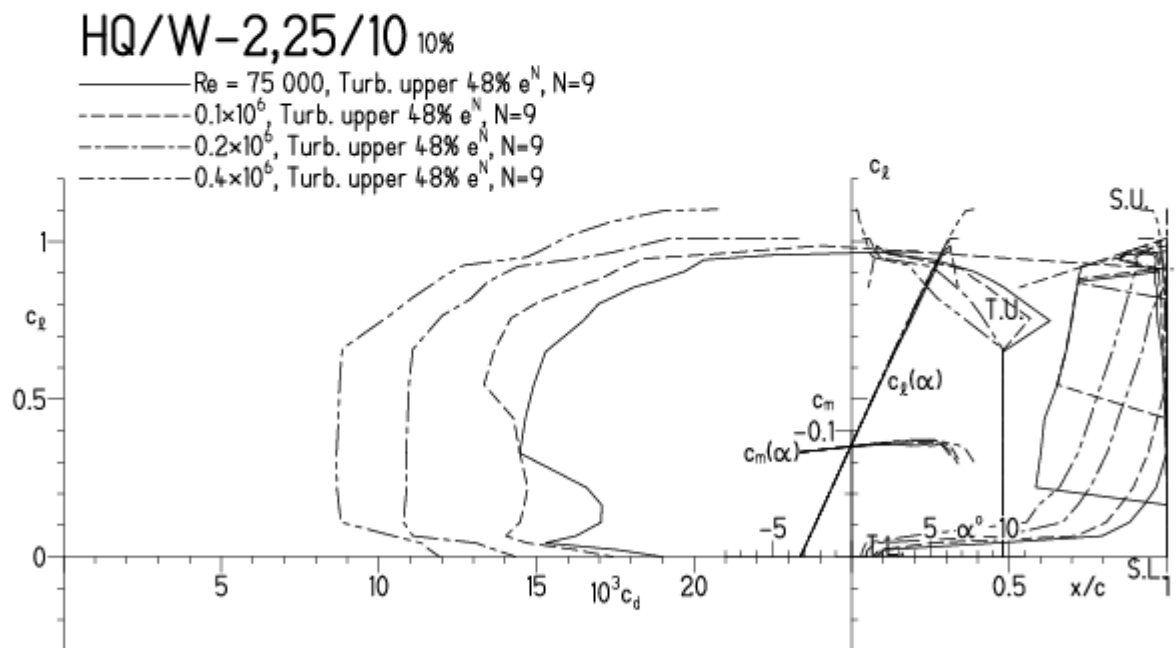


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

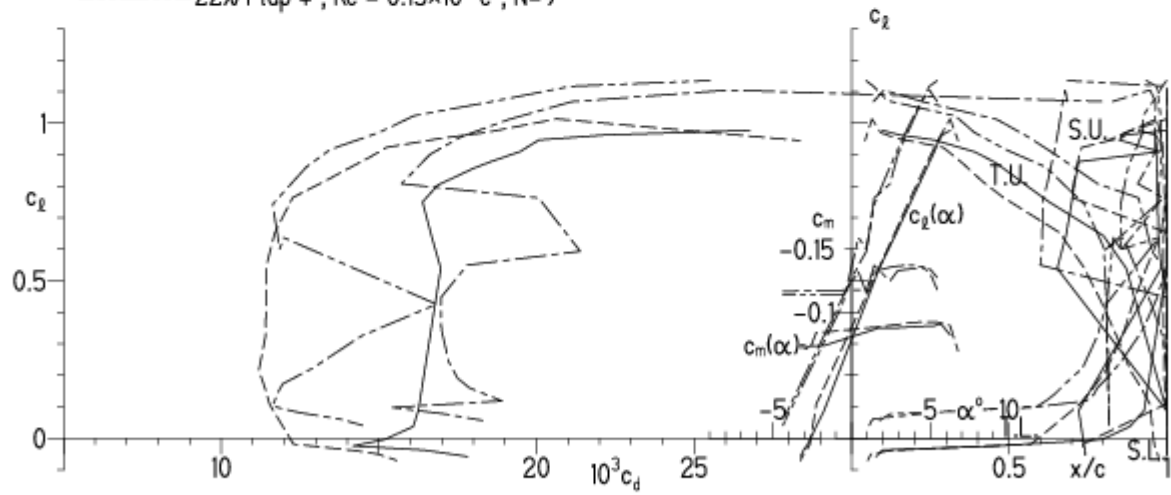


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - $0.8 \times 10^6 e^N, N=9$
- · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

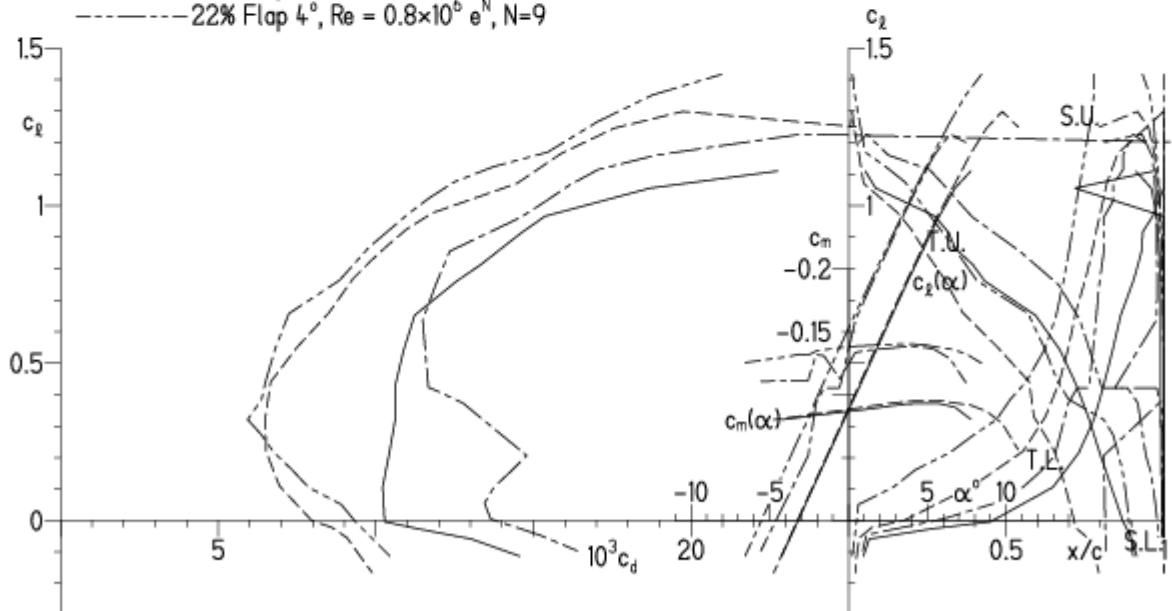


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

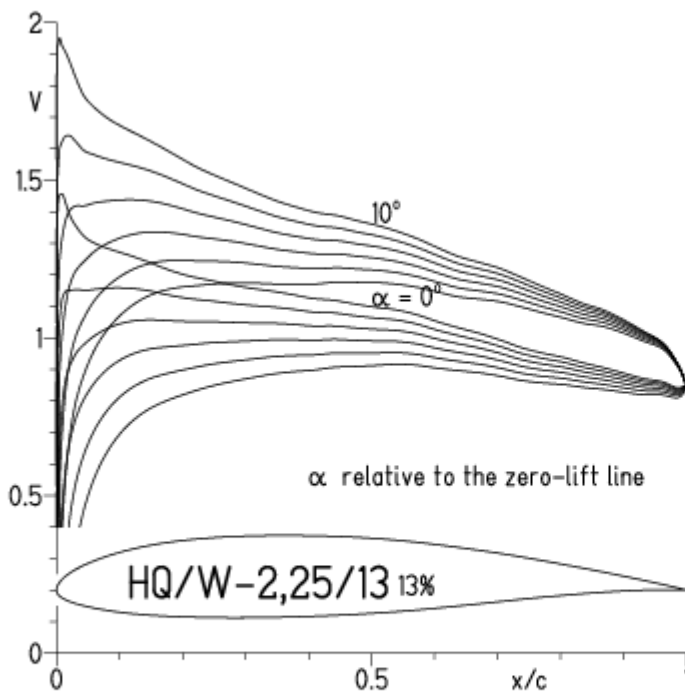


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

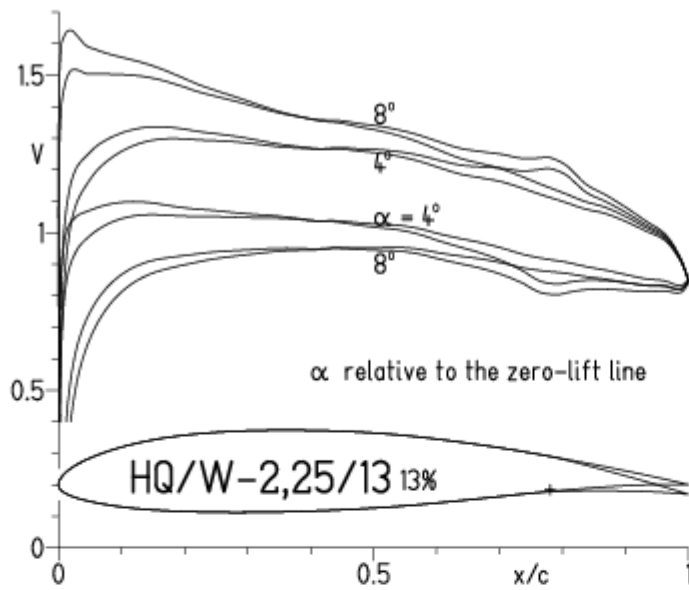
HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

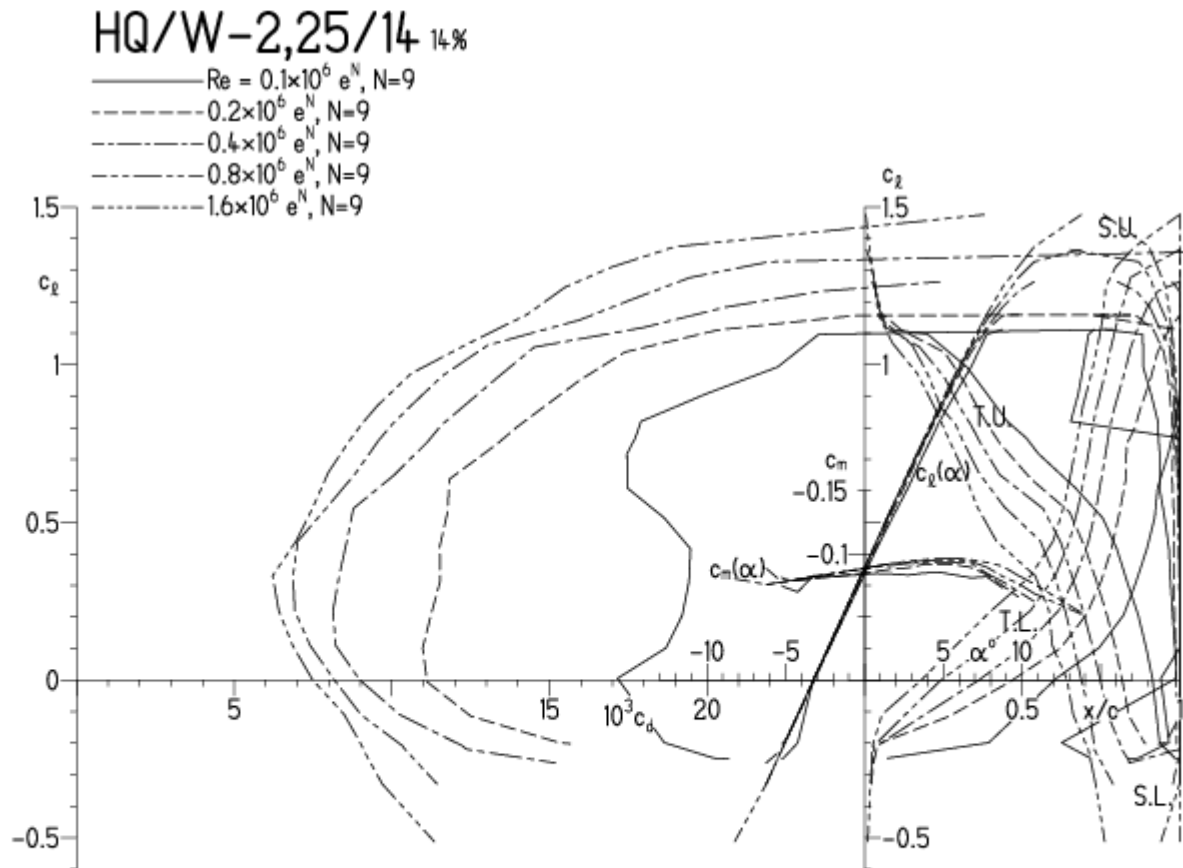


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

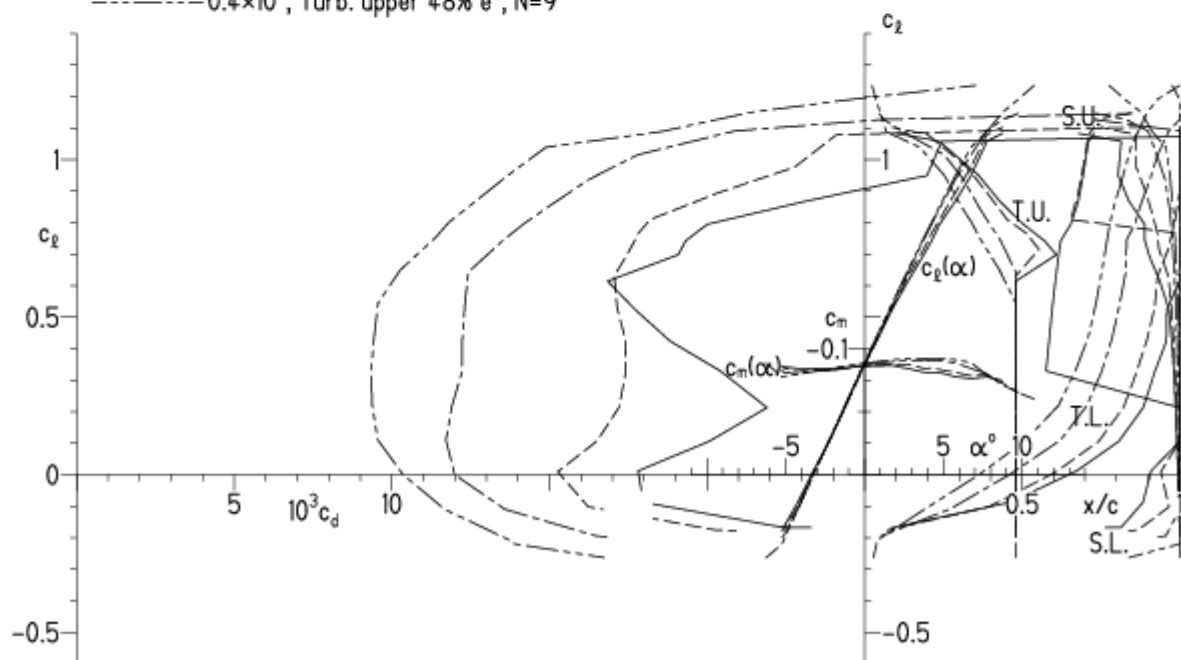
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

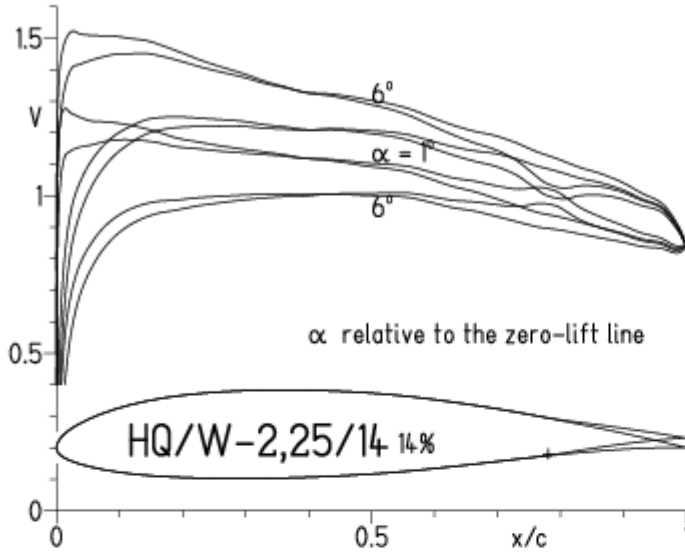
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

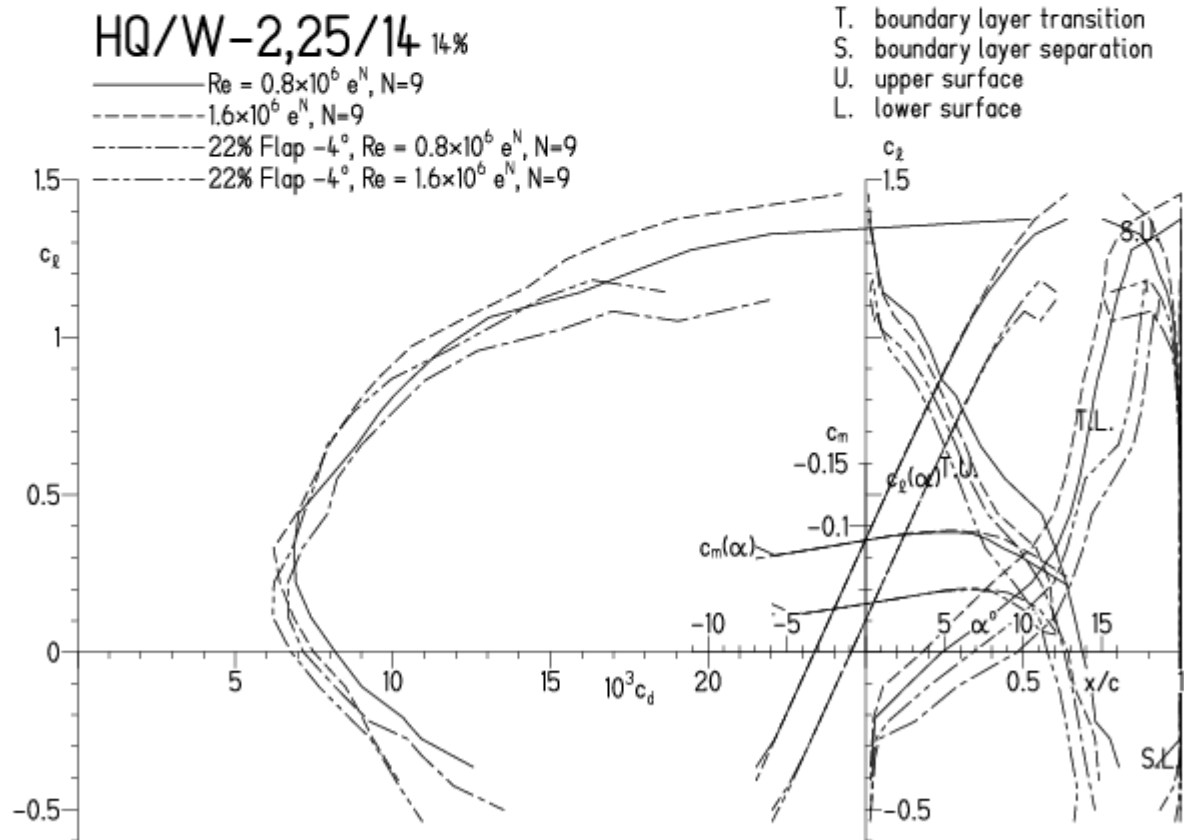


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31

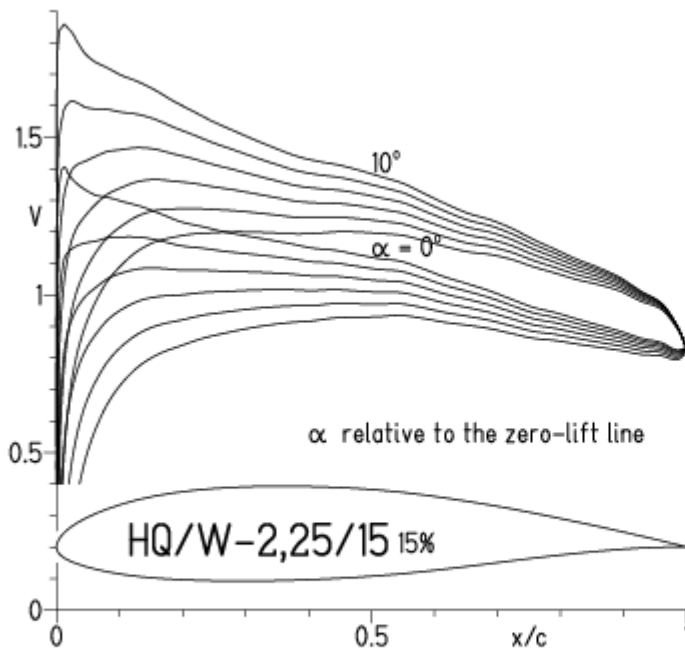


EPPLER 20

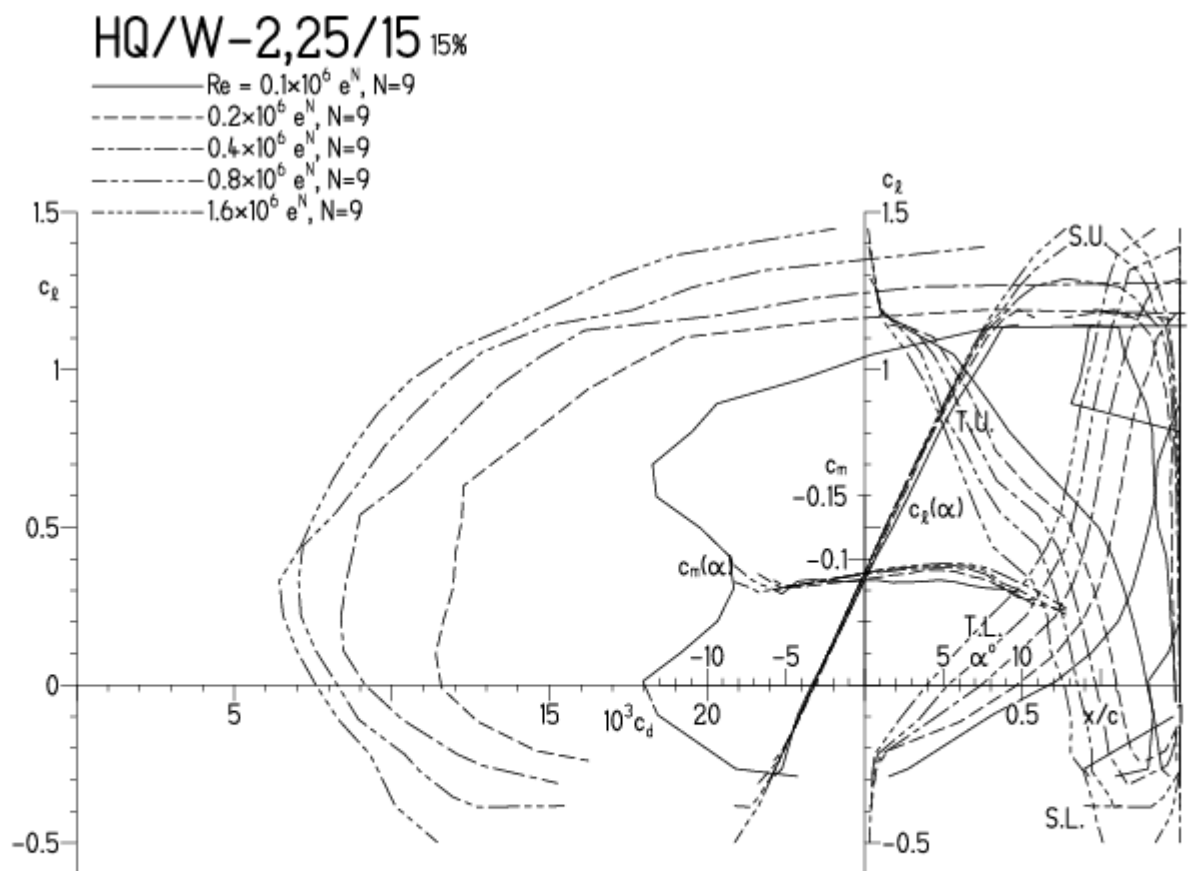


HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

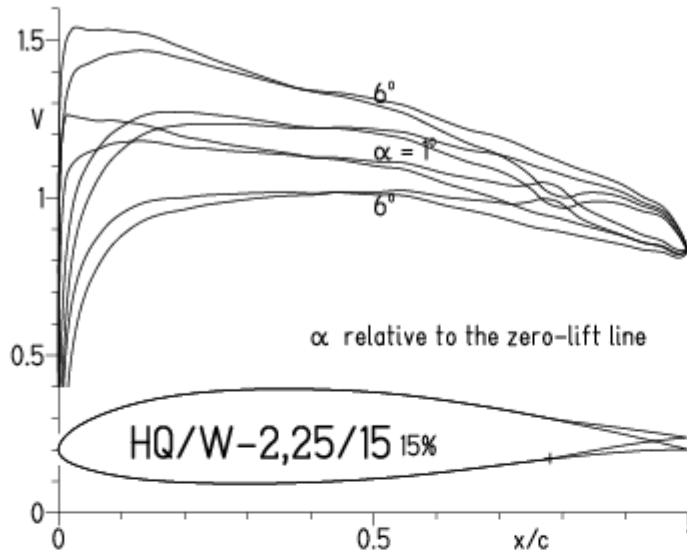


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



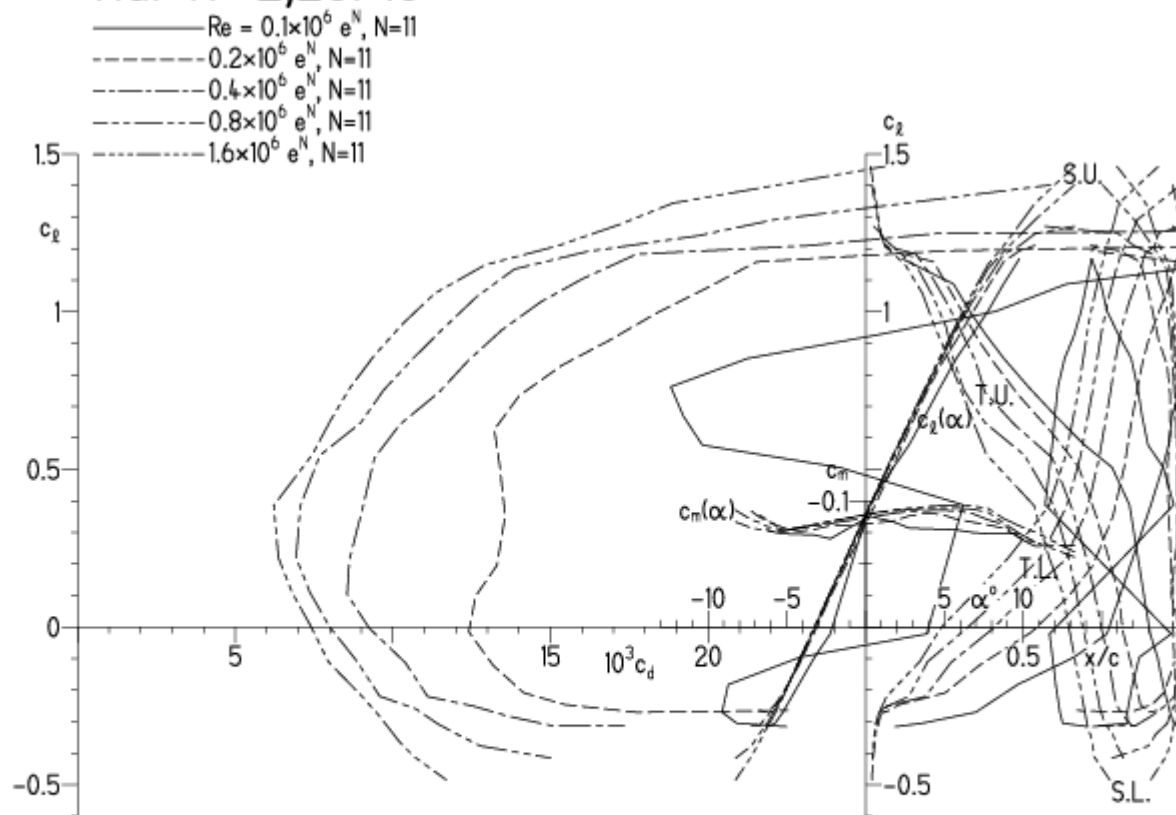
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

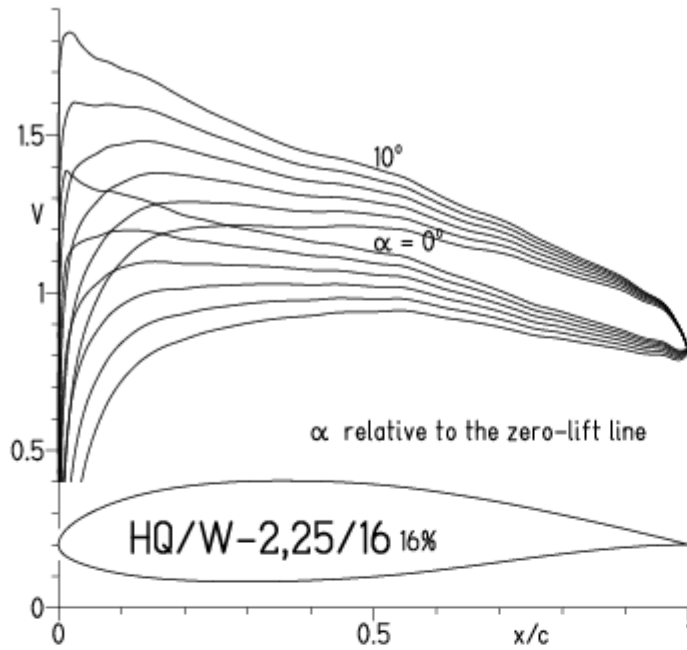
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41

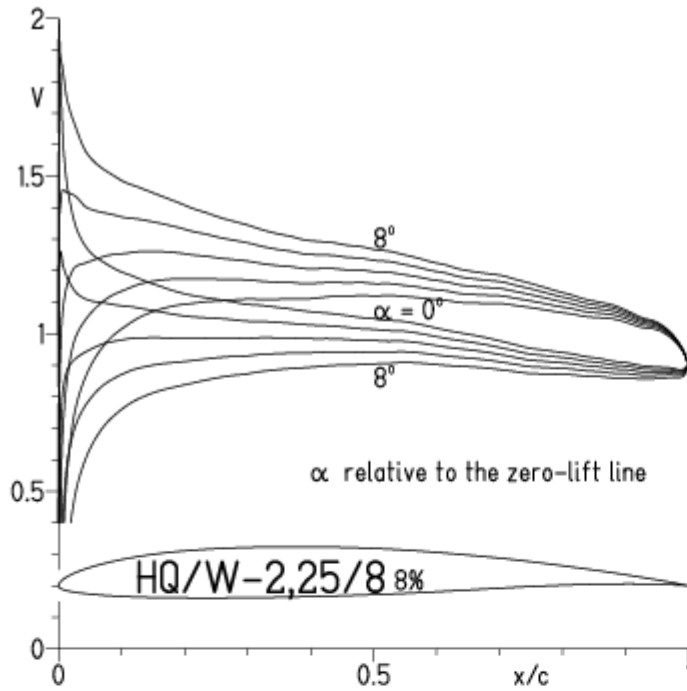


EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



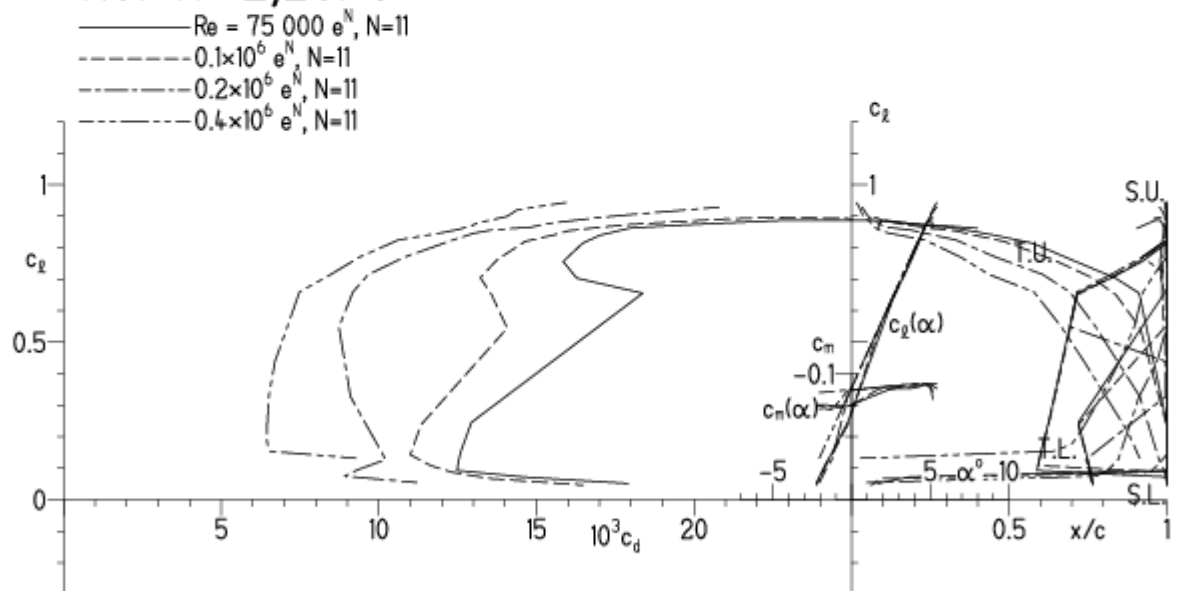
HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. $30 - 35 \text{ m/s}$ Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

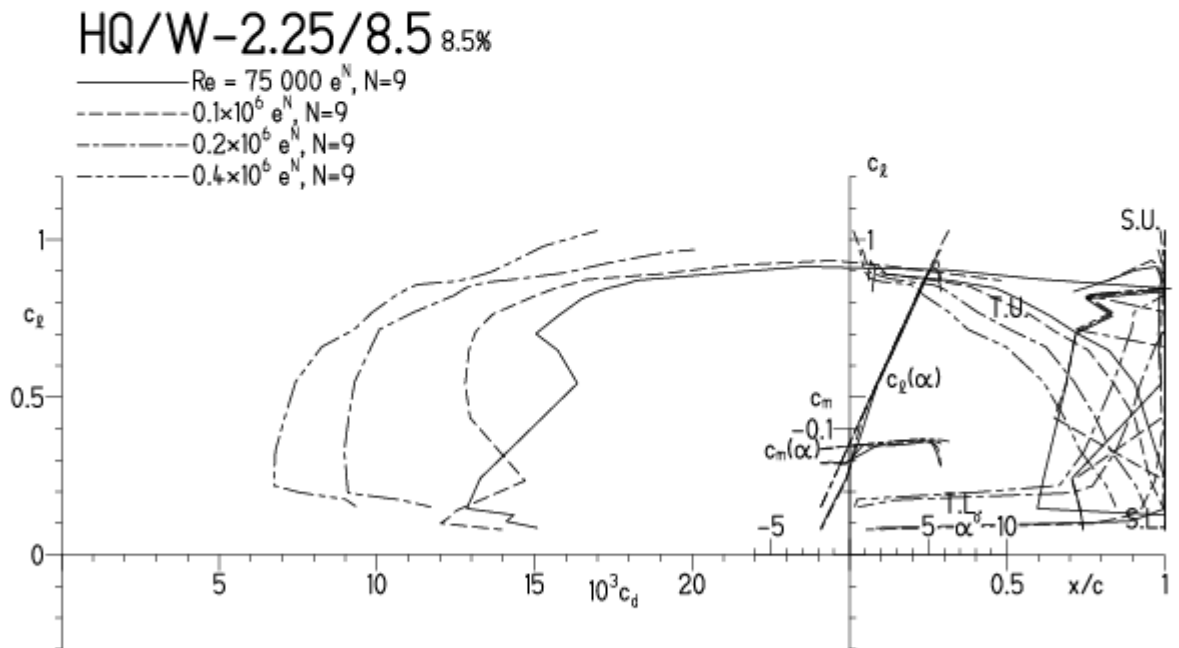


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

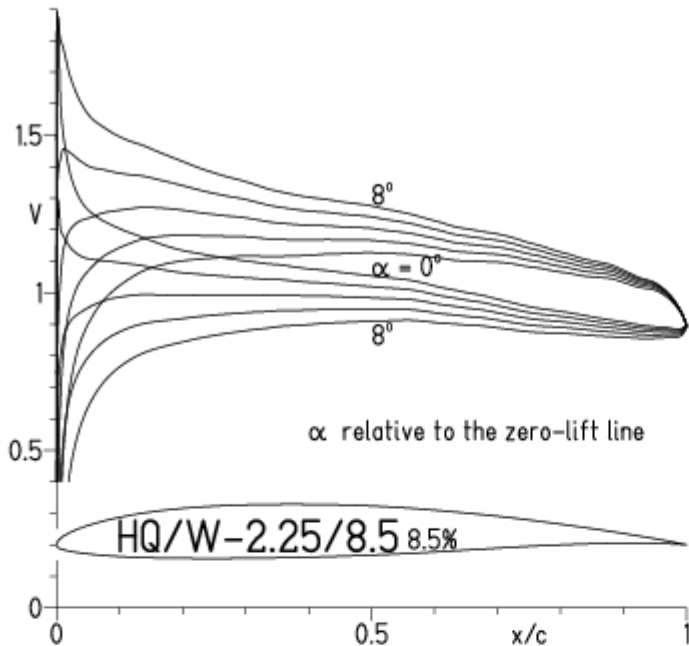


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

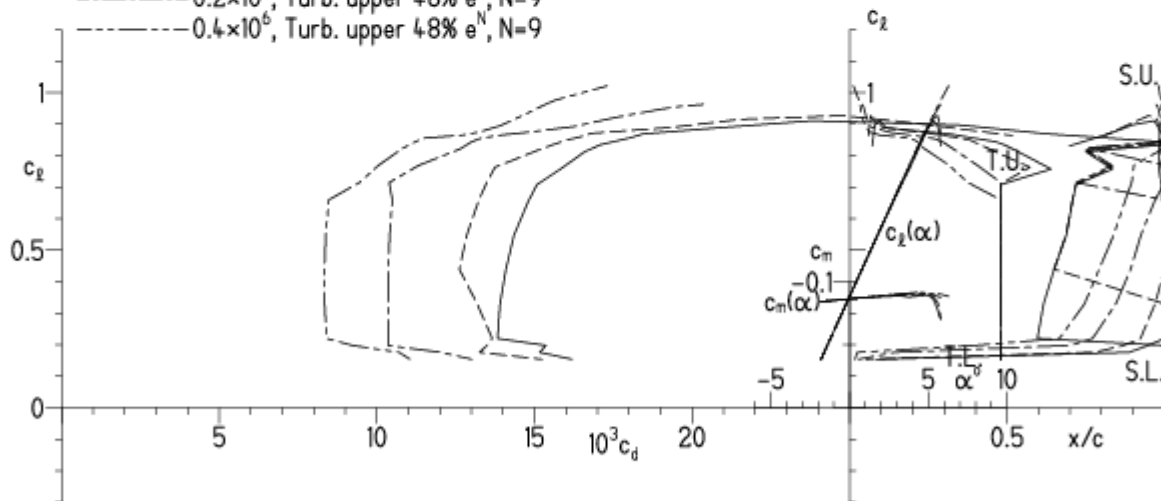
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

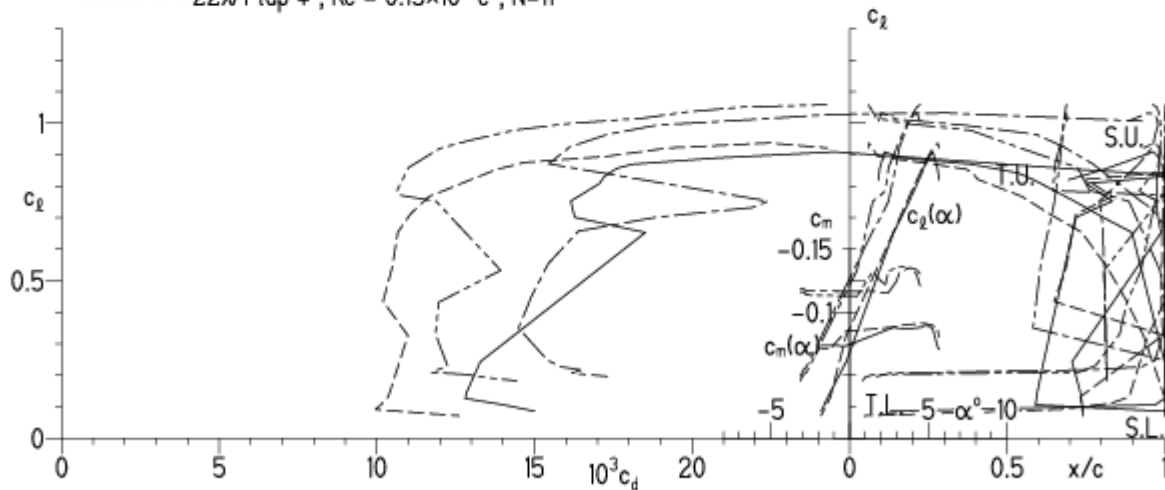


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

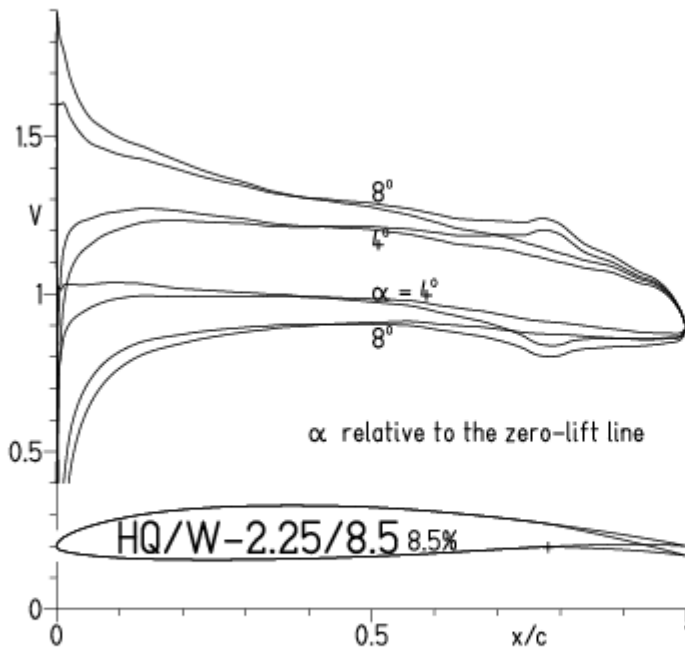
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

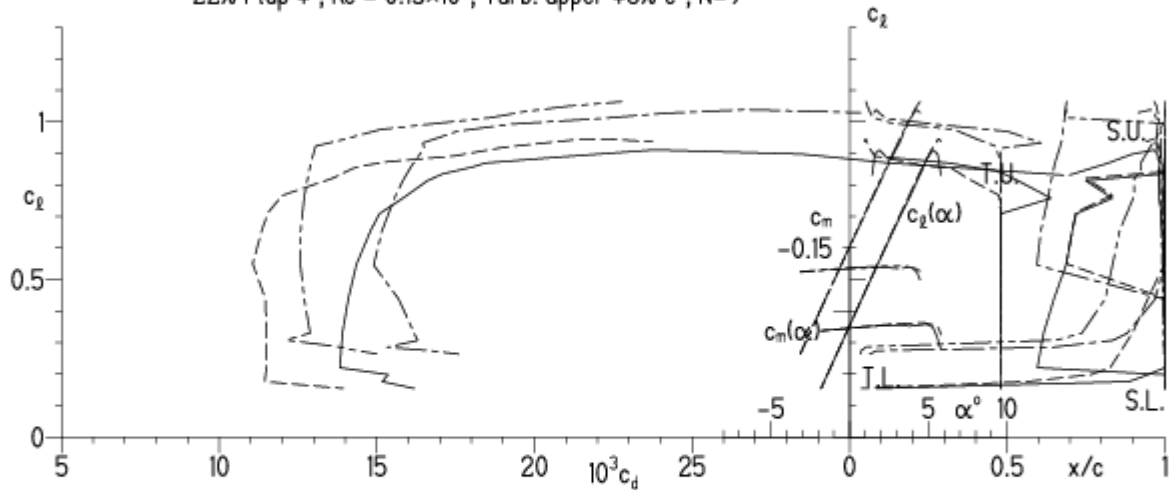


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

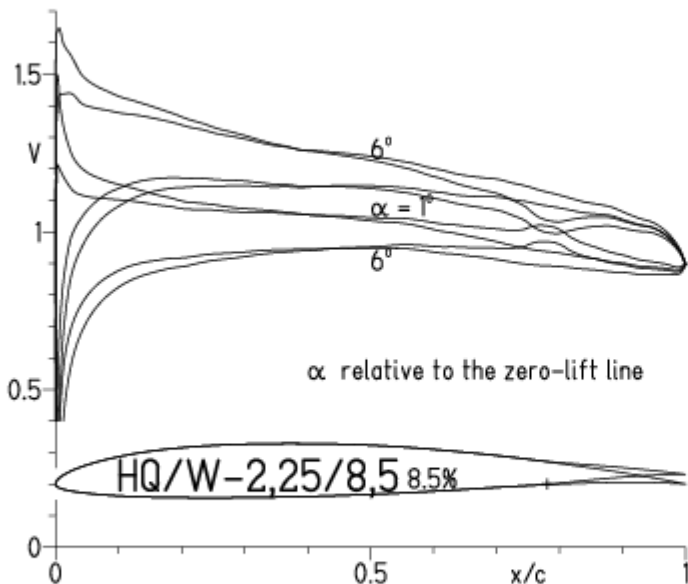
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

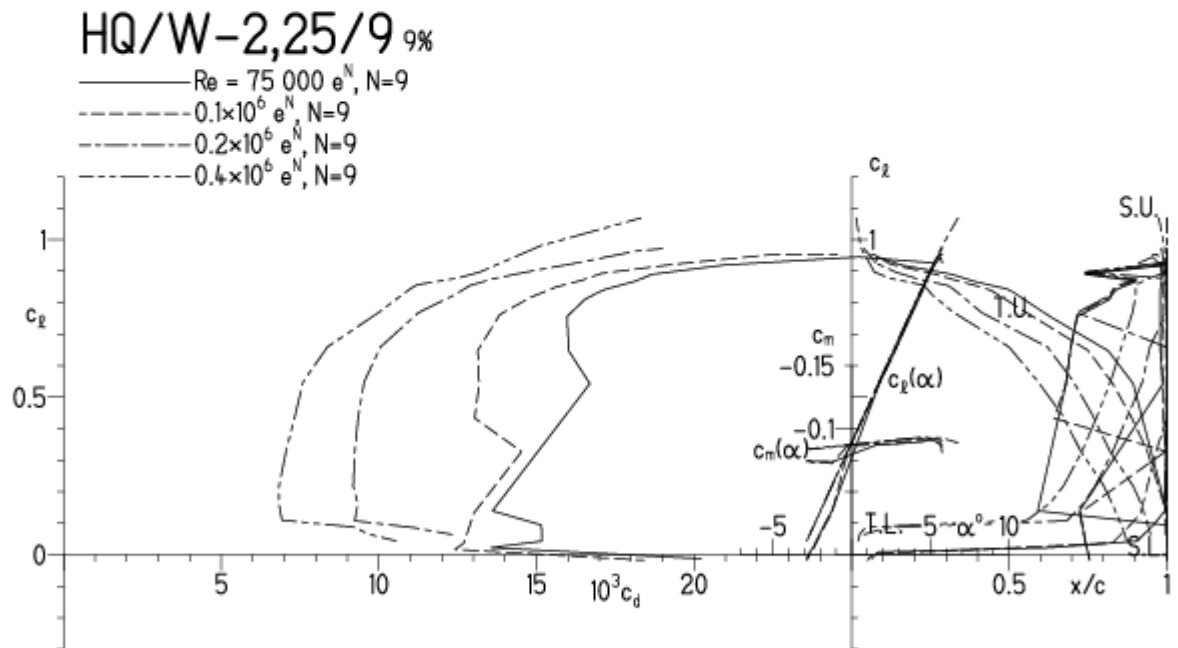


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

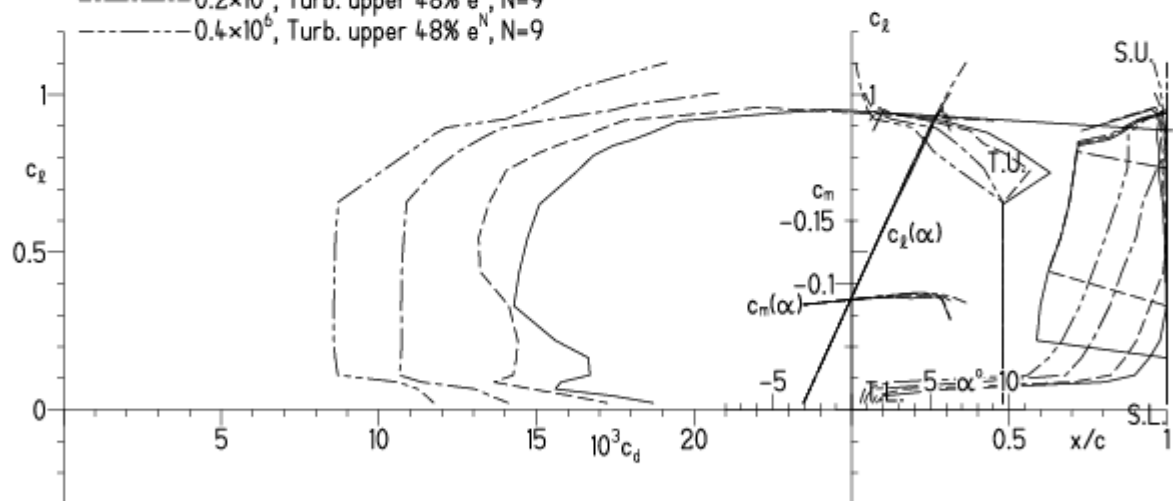
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

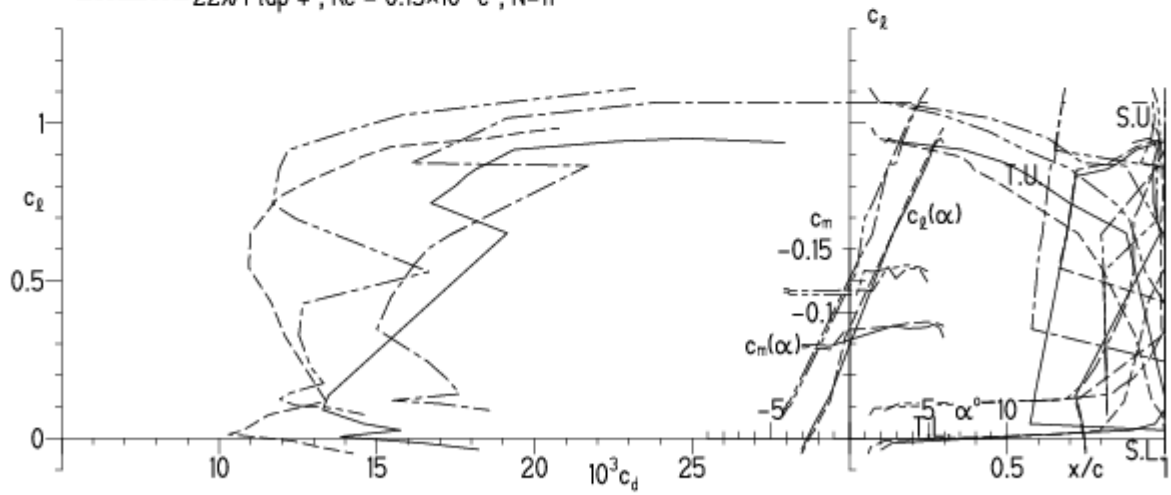


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

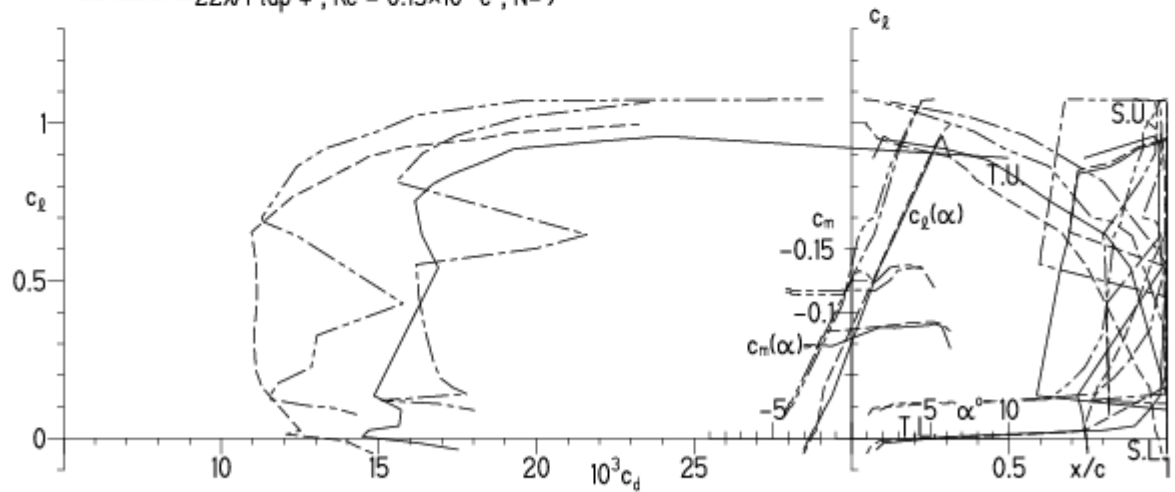


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



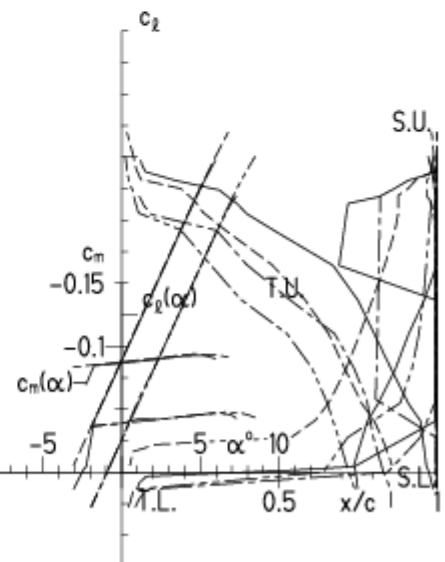
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

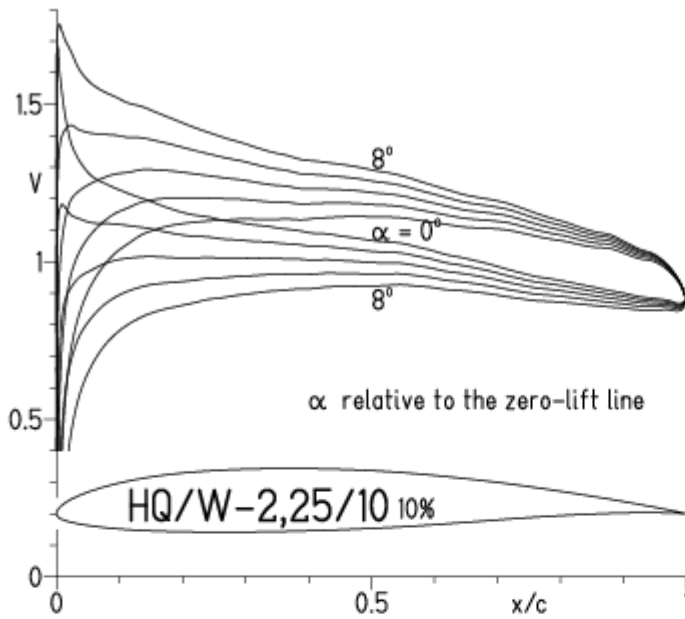


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

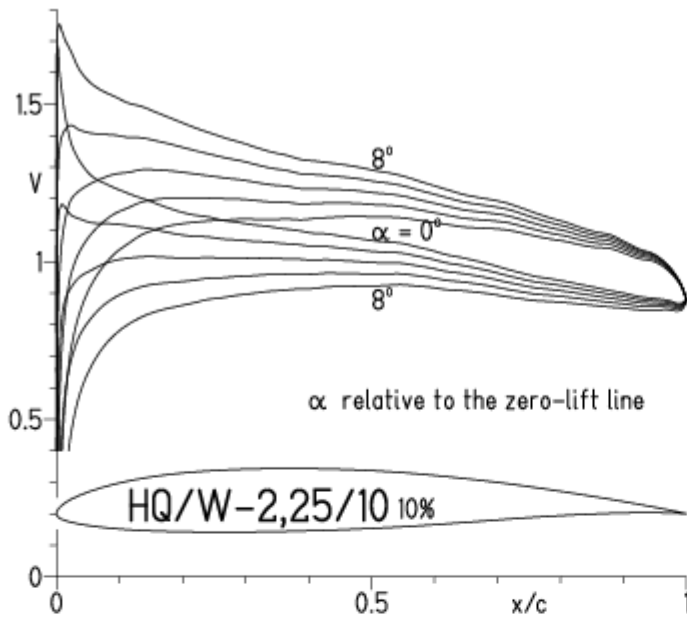


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

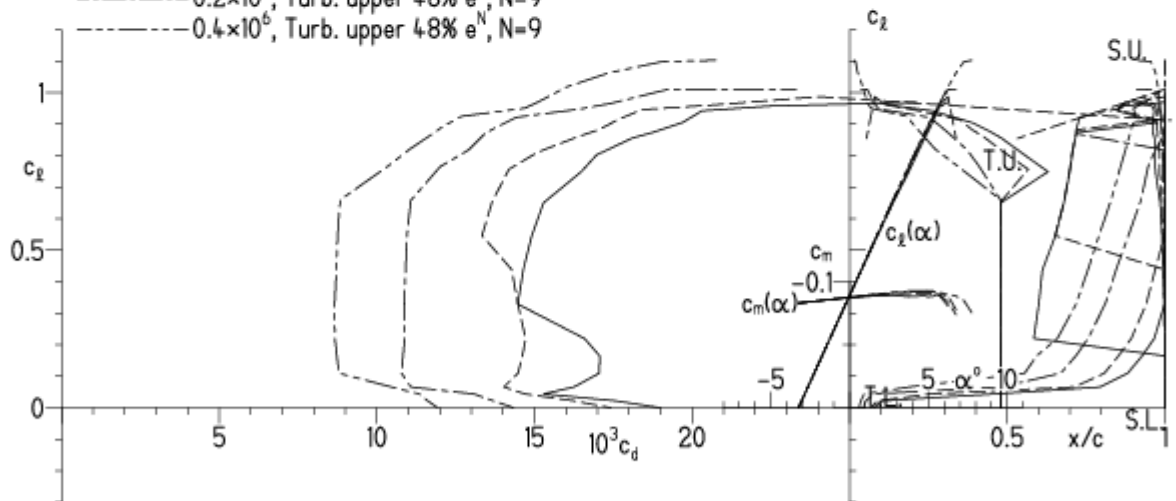
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

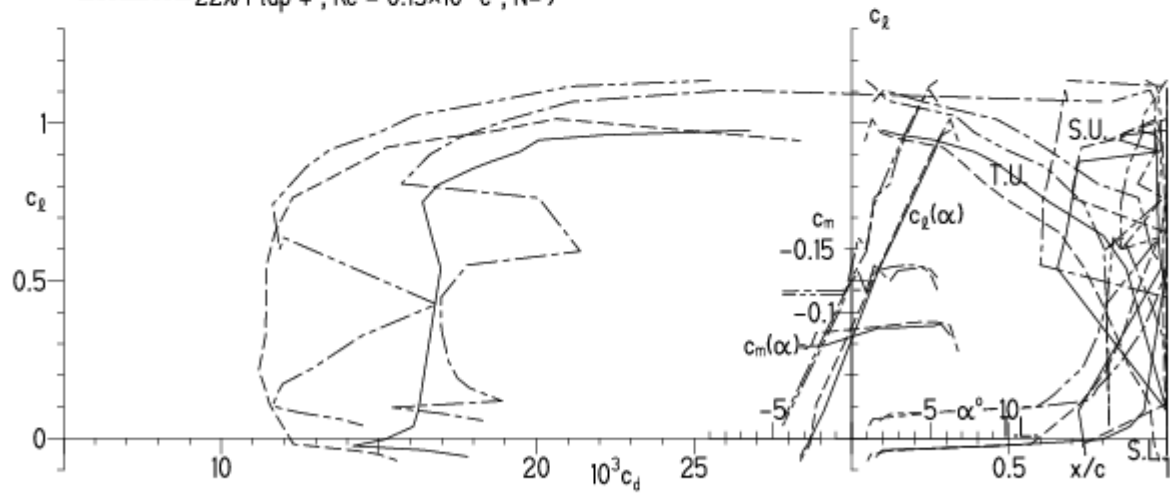


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

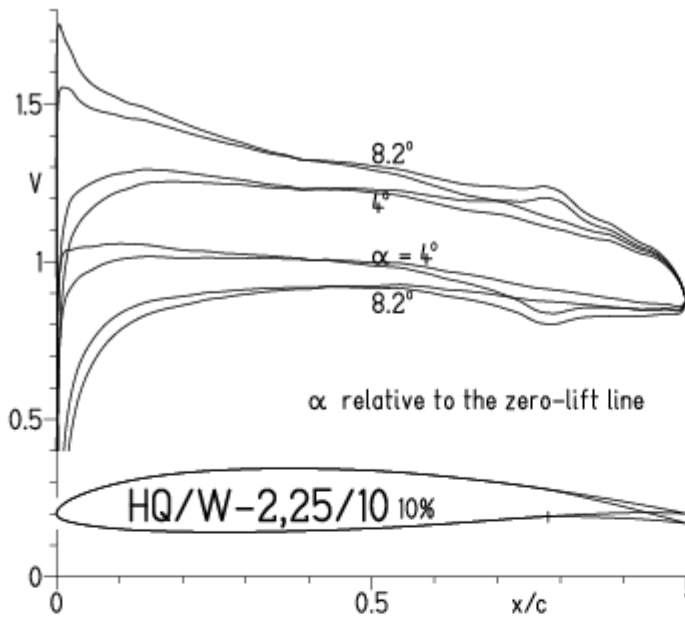
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

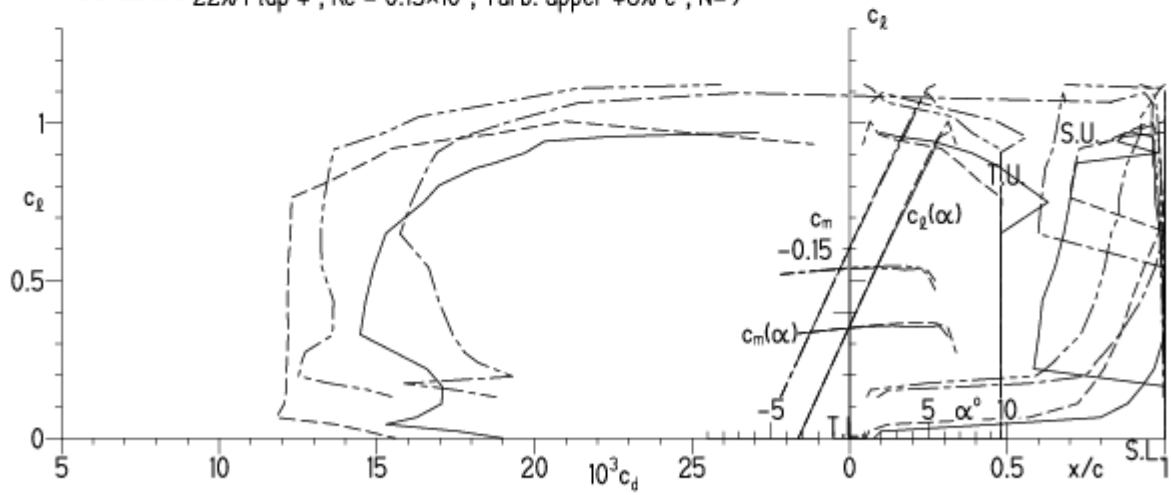


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- Re = 0.2×10^6 e^N, N=9
- - - Re = 0.8×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.2×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.8×10^6 e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - $0.8 \times 10^6 e^N, N=9$
- · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

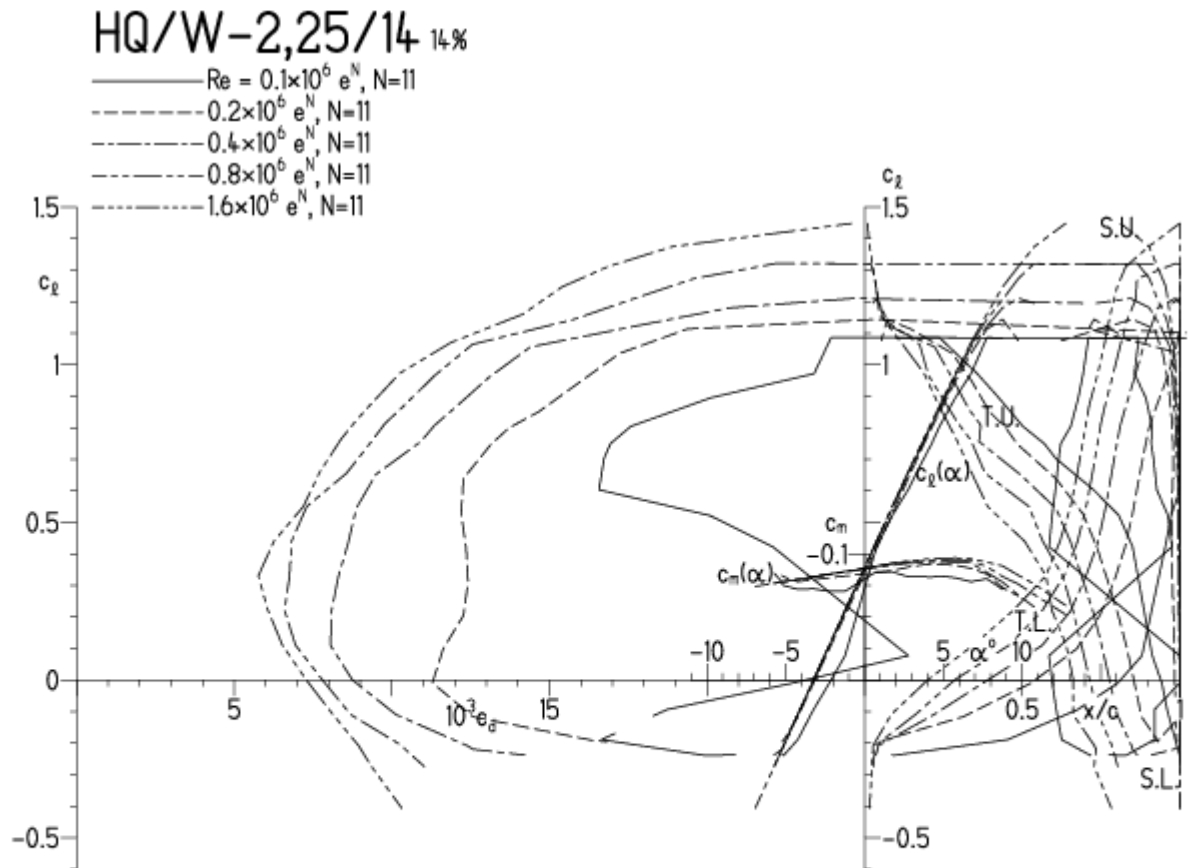


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

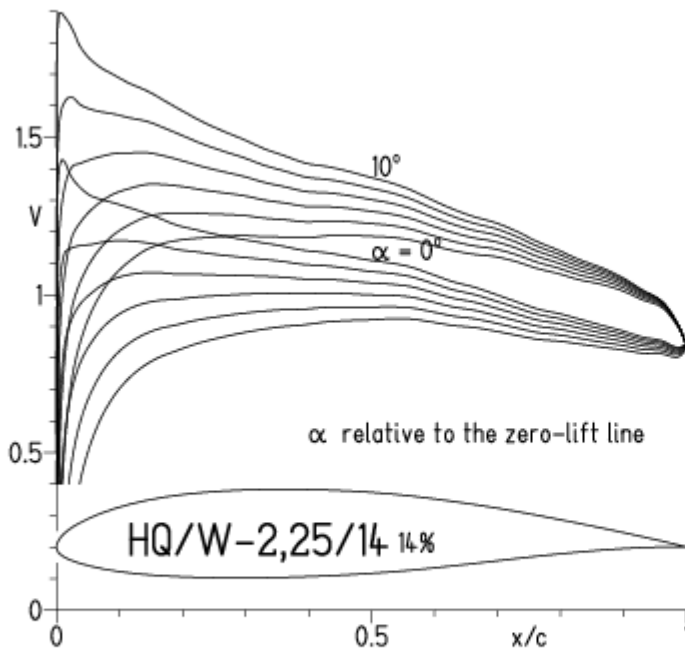


EPPLER 2005 V. 8.

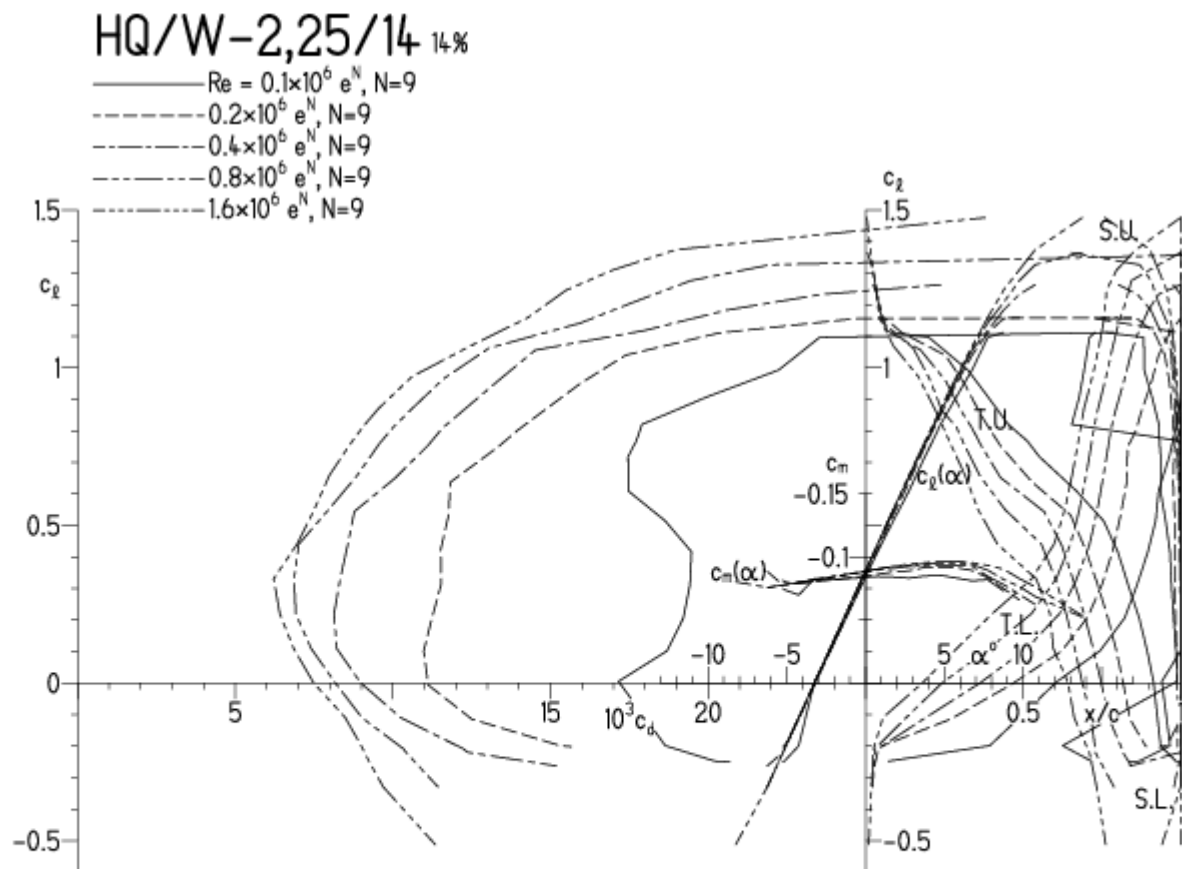


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

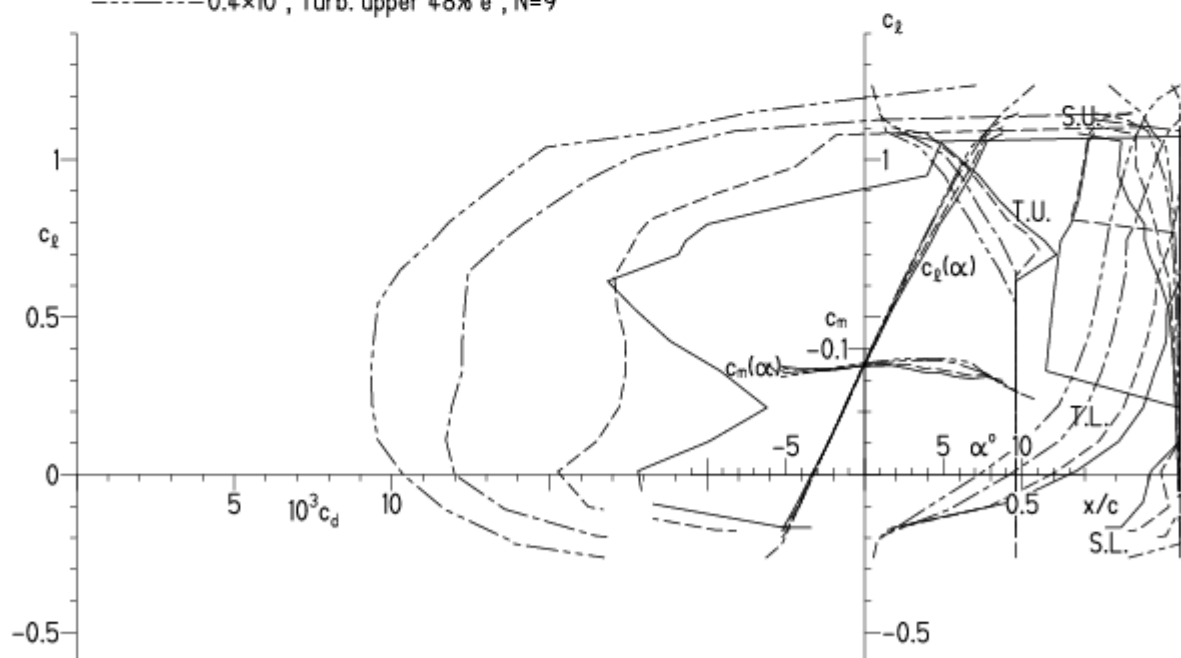
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

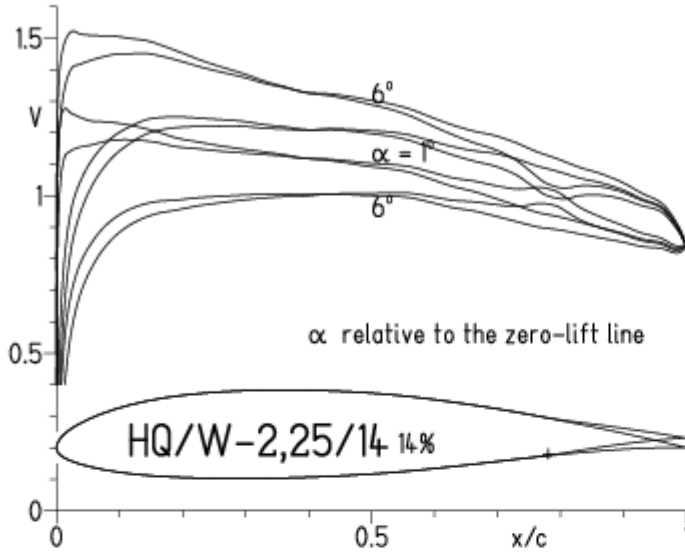
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

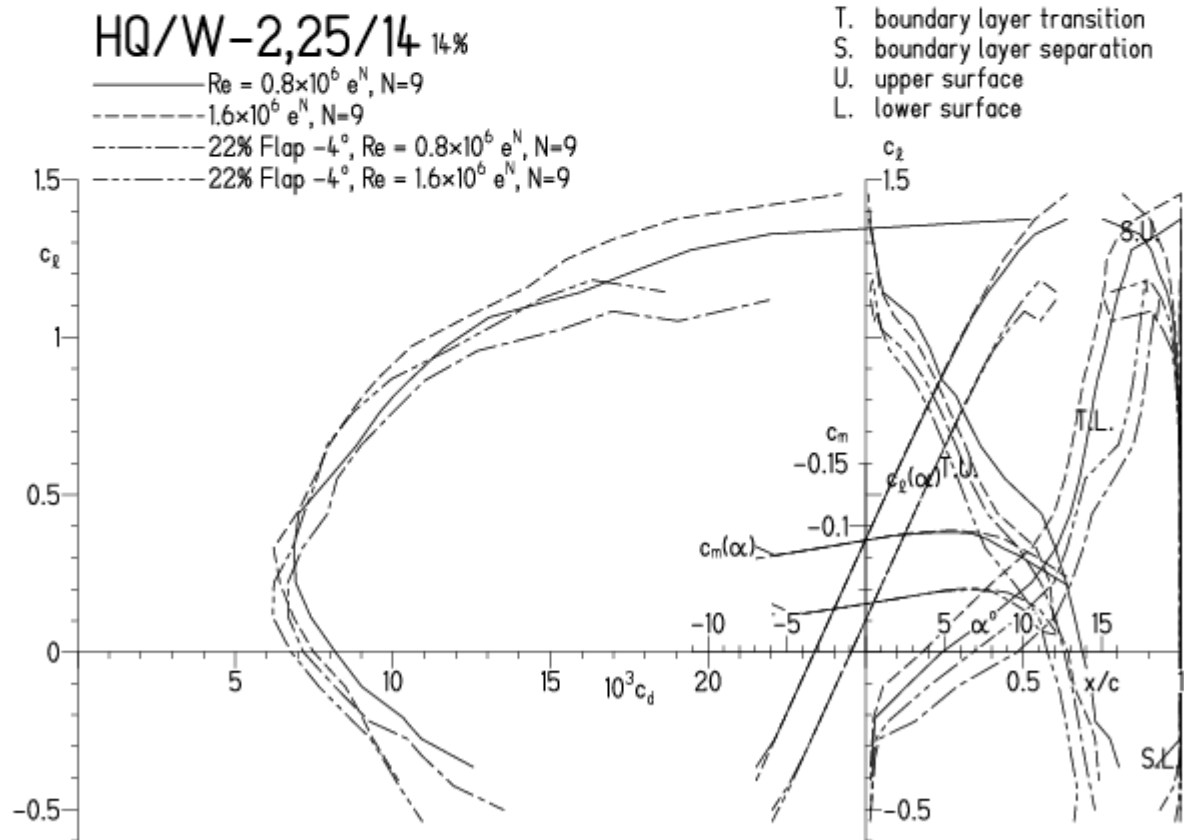


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

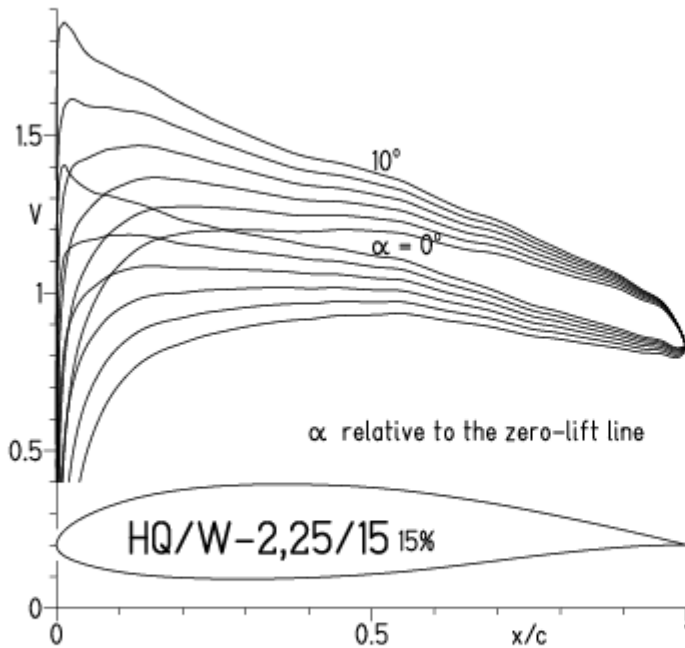


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20

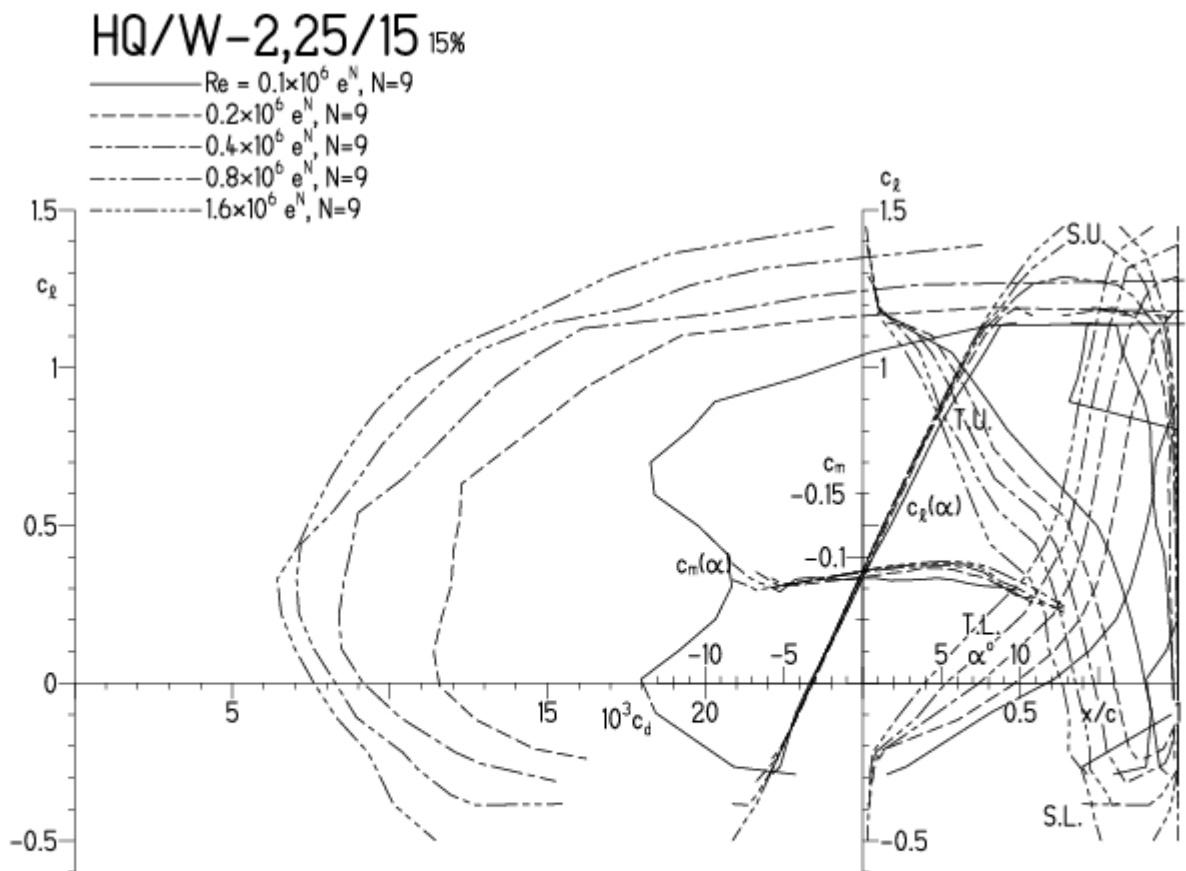


HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



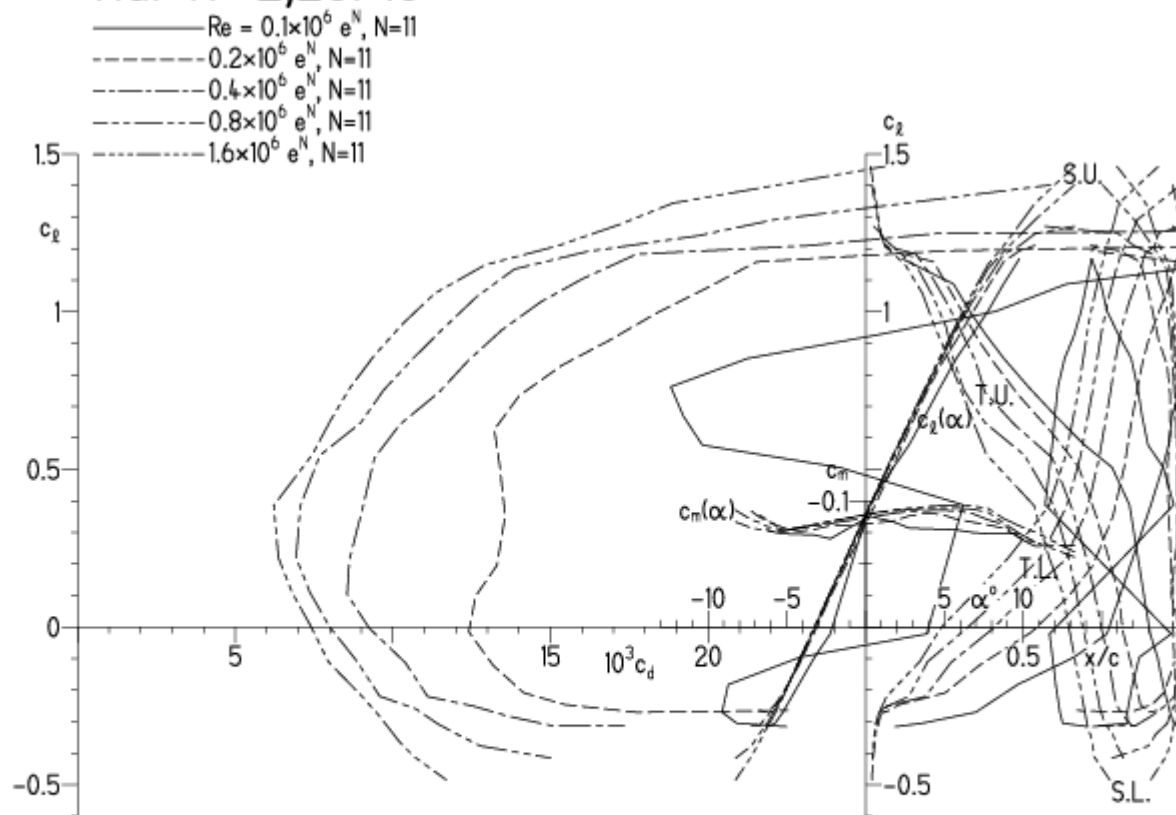
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

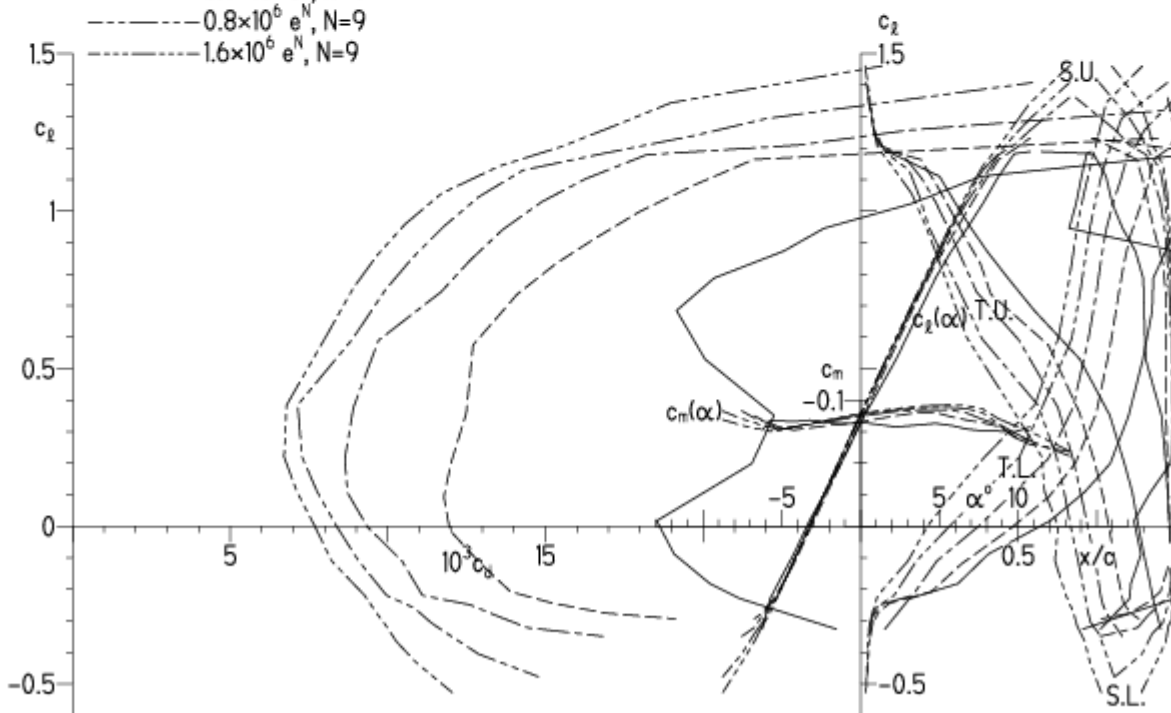
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

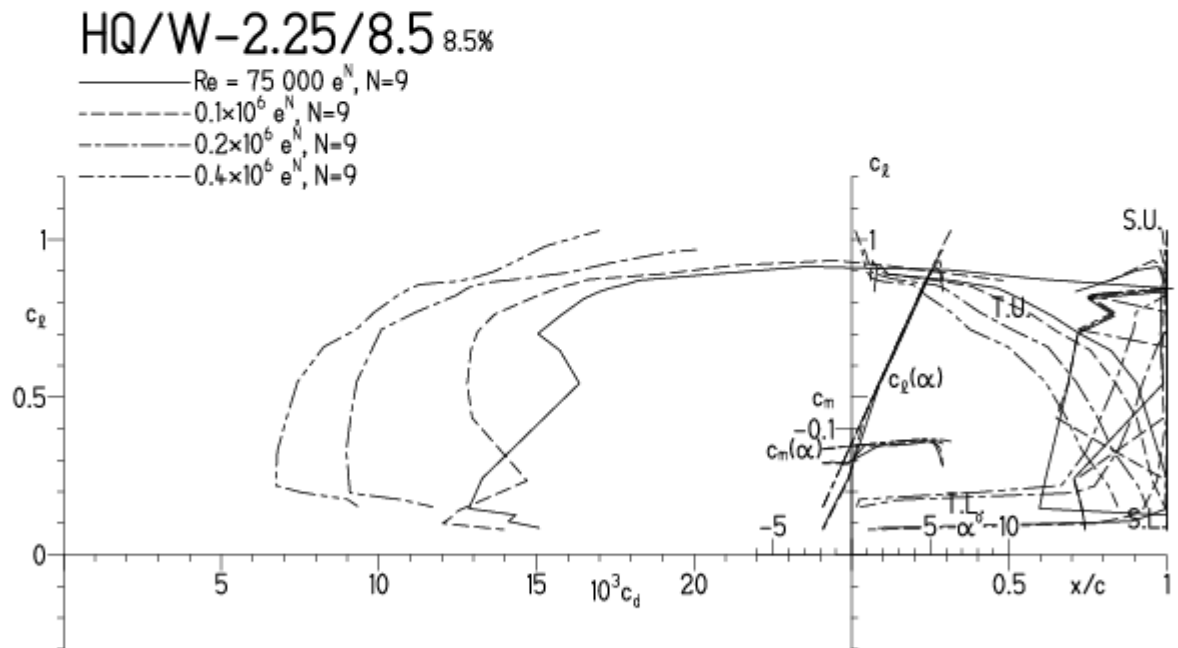


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

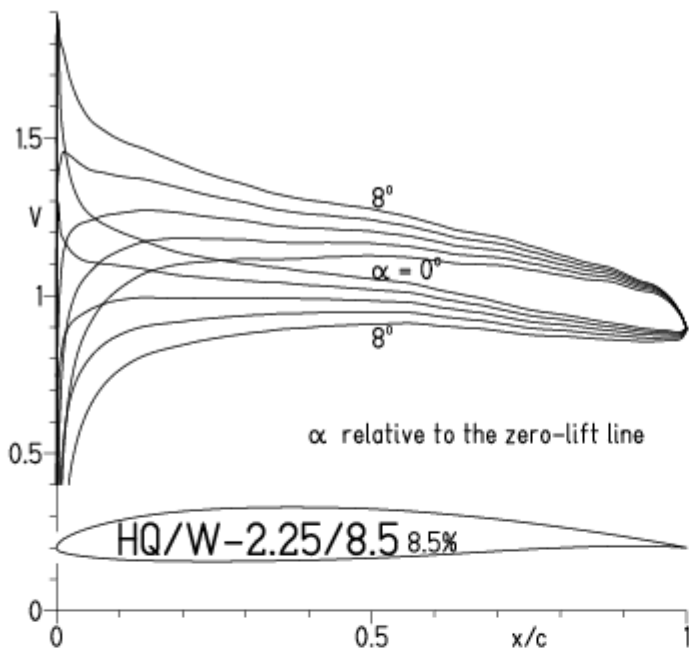


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

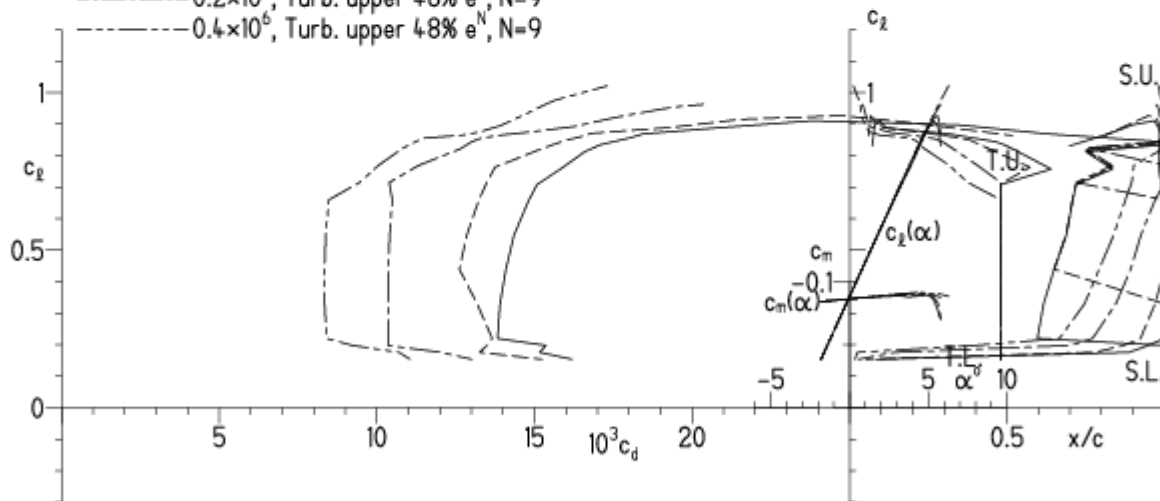
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

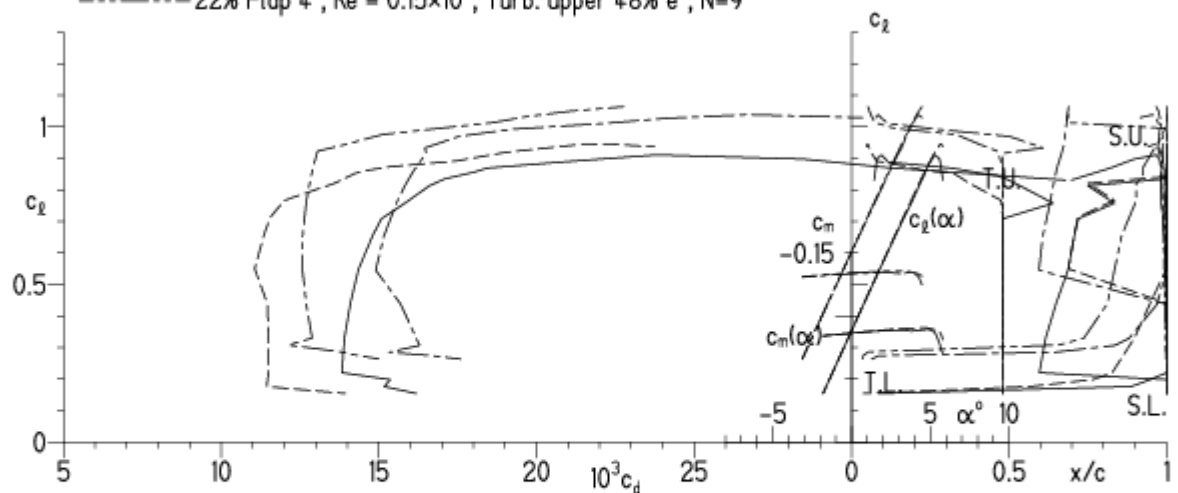


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



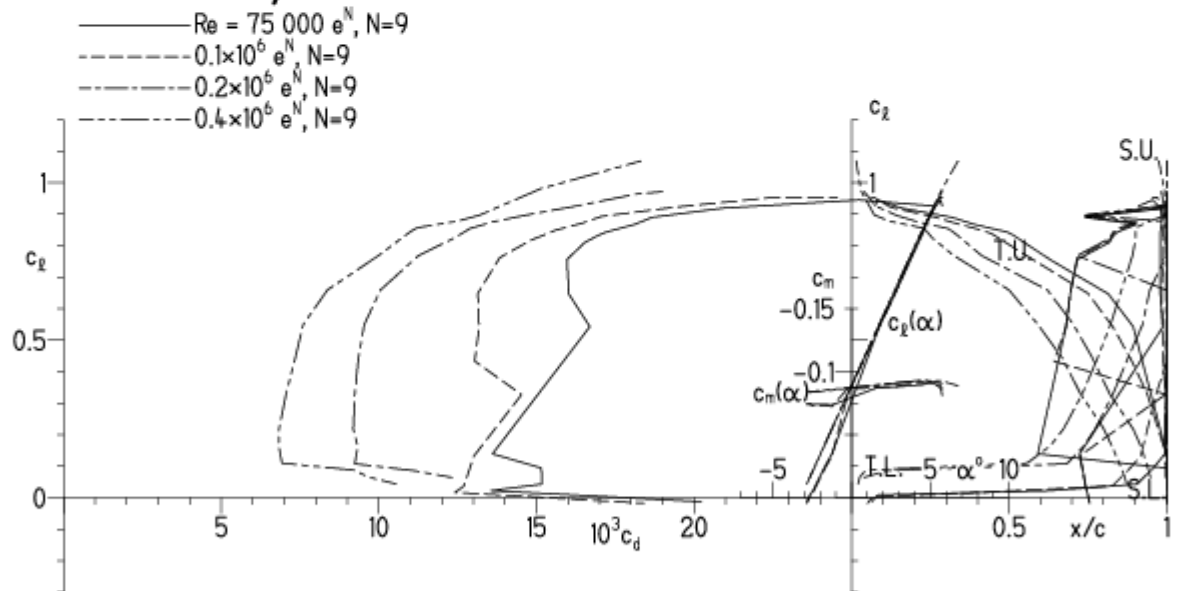
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

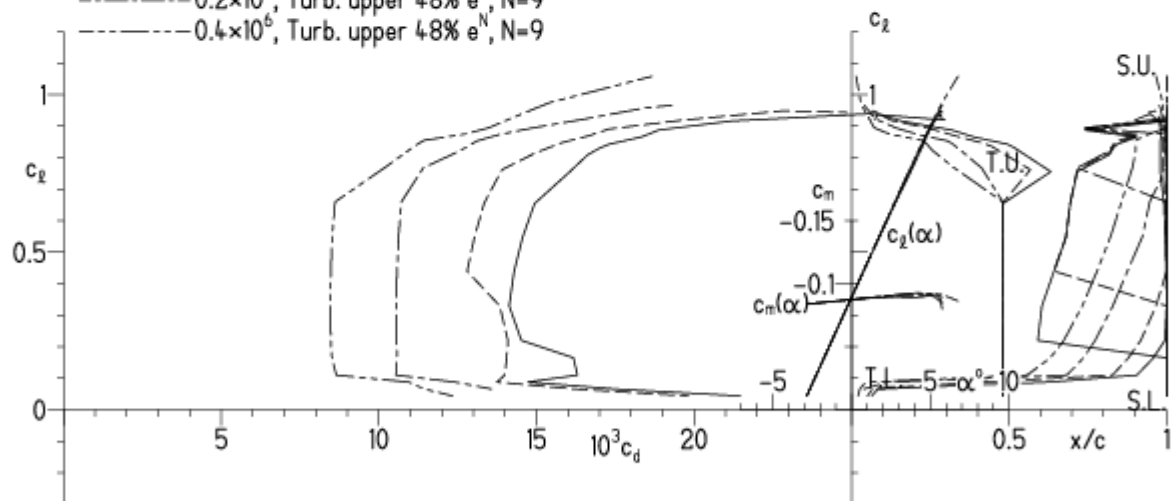
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38

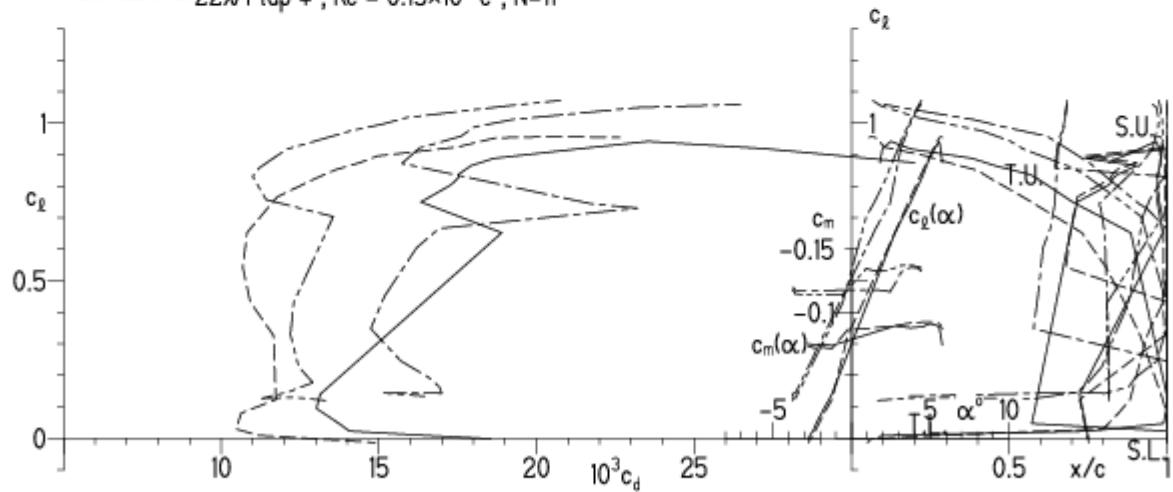


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

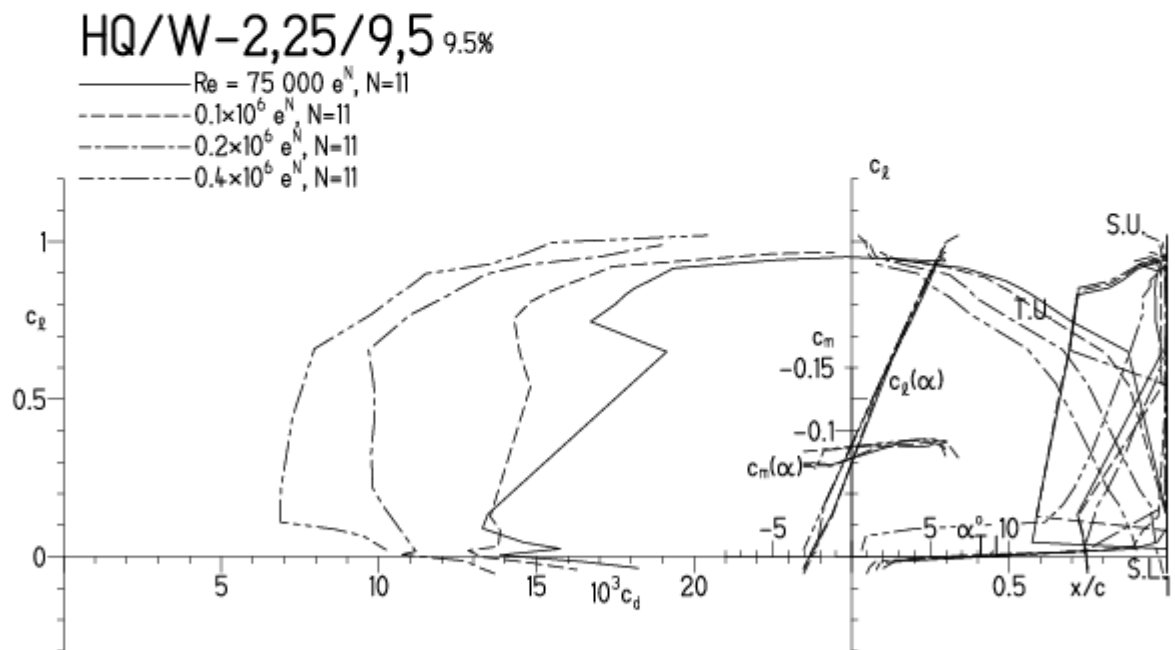


HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

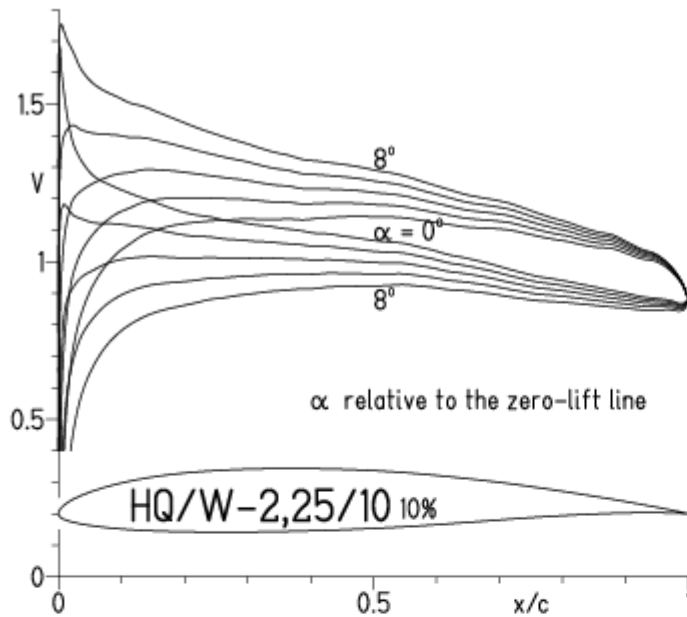


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

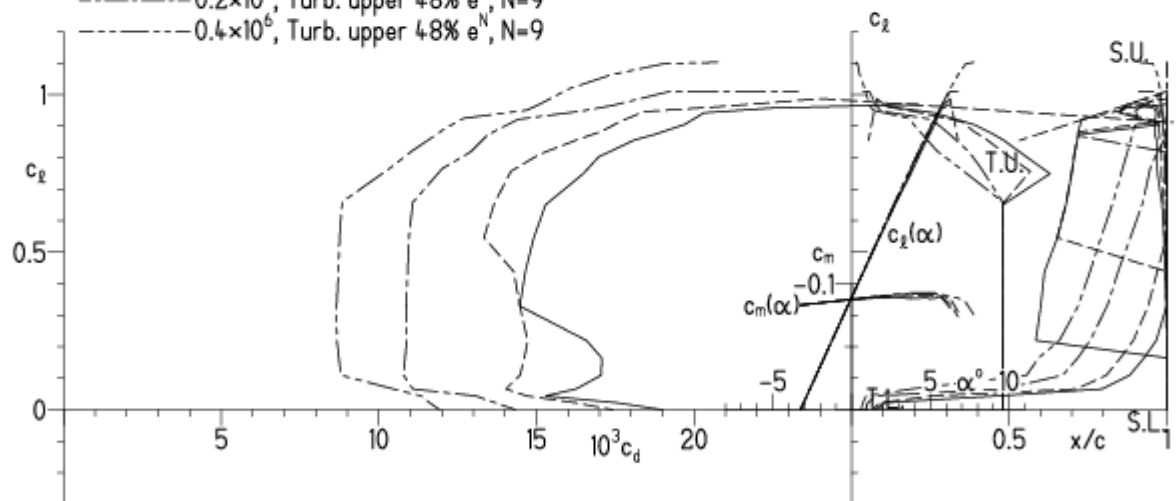
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

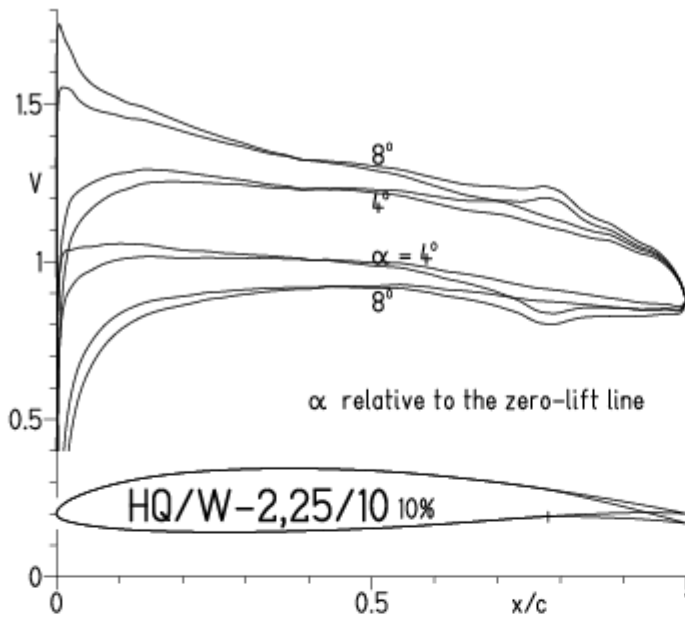
HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

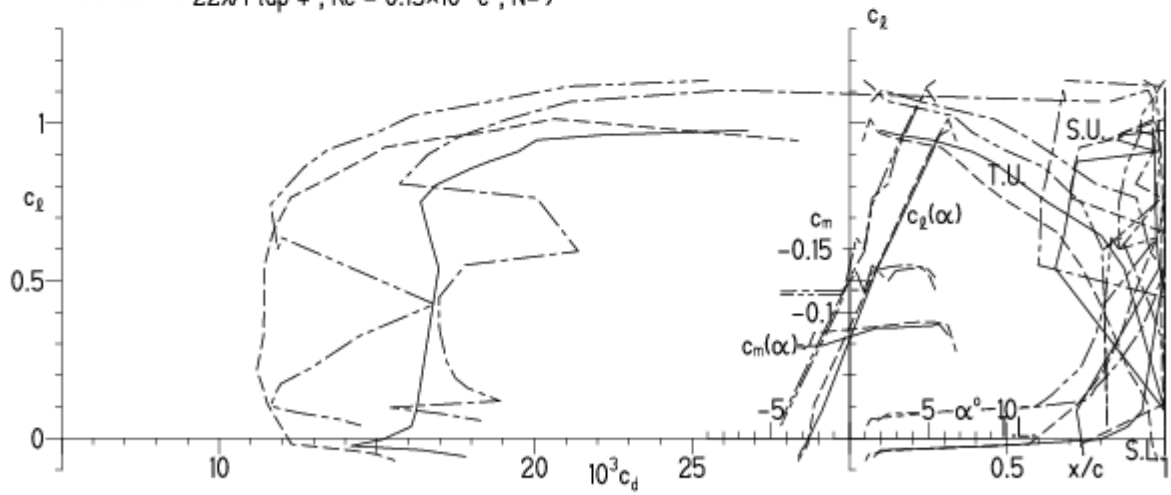


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

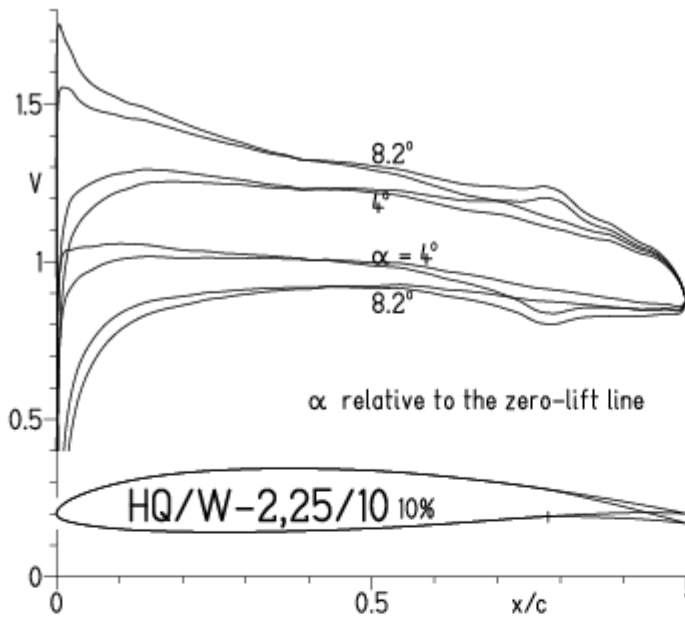
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

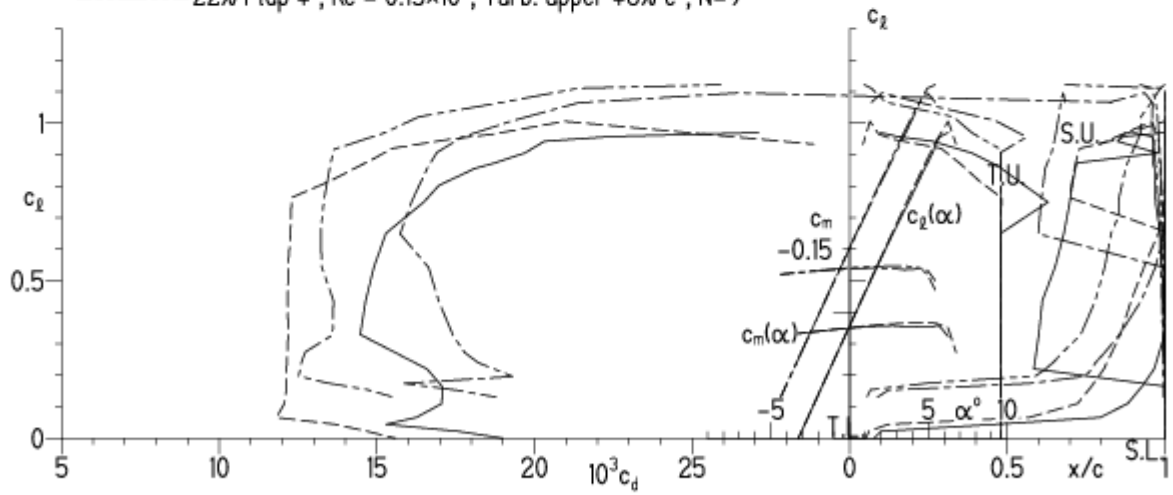


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

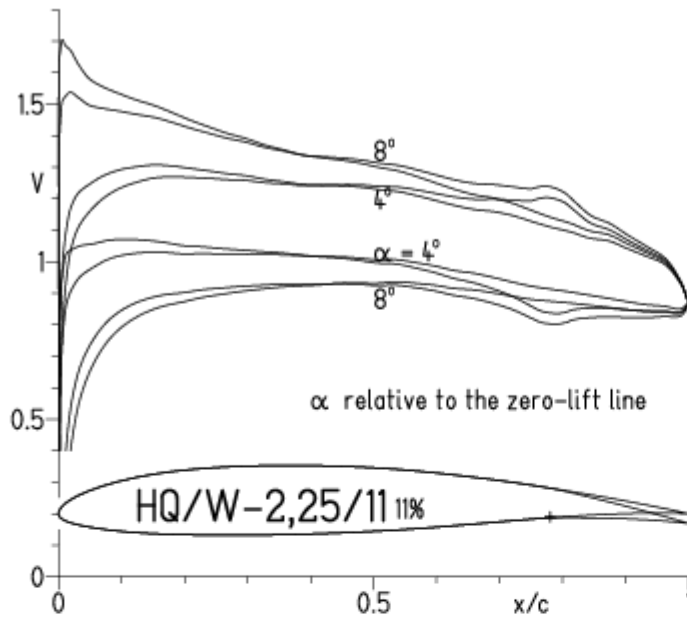
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

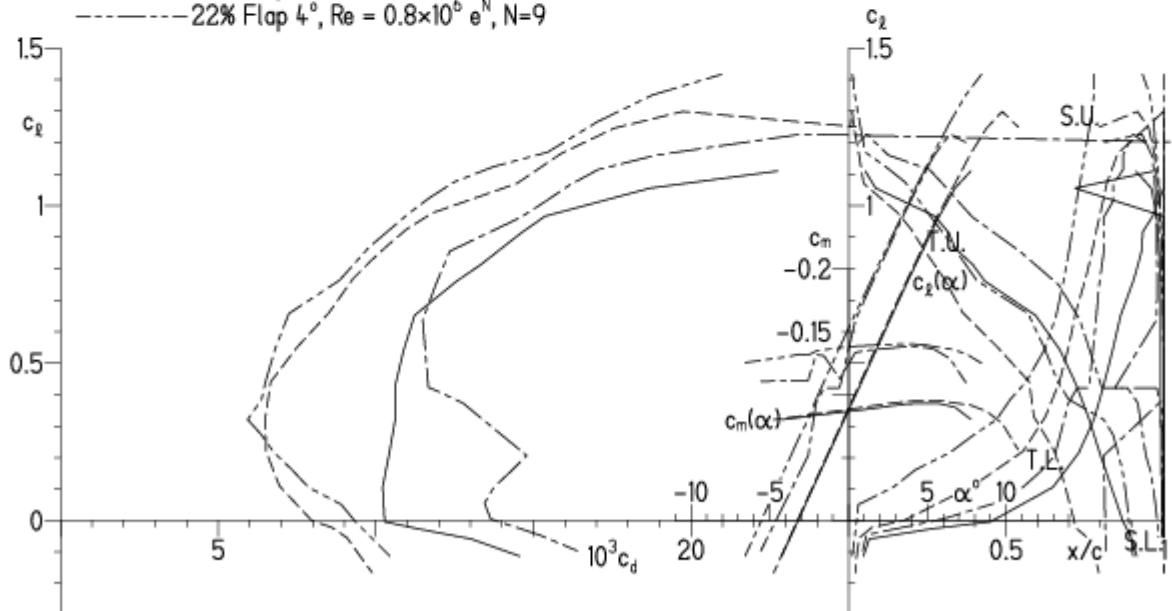


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

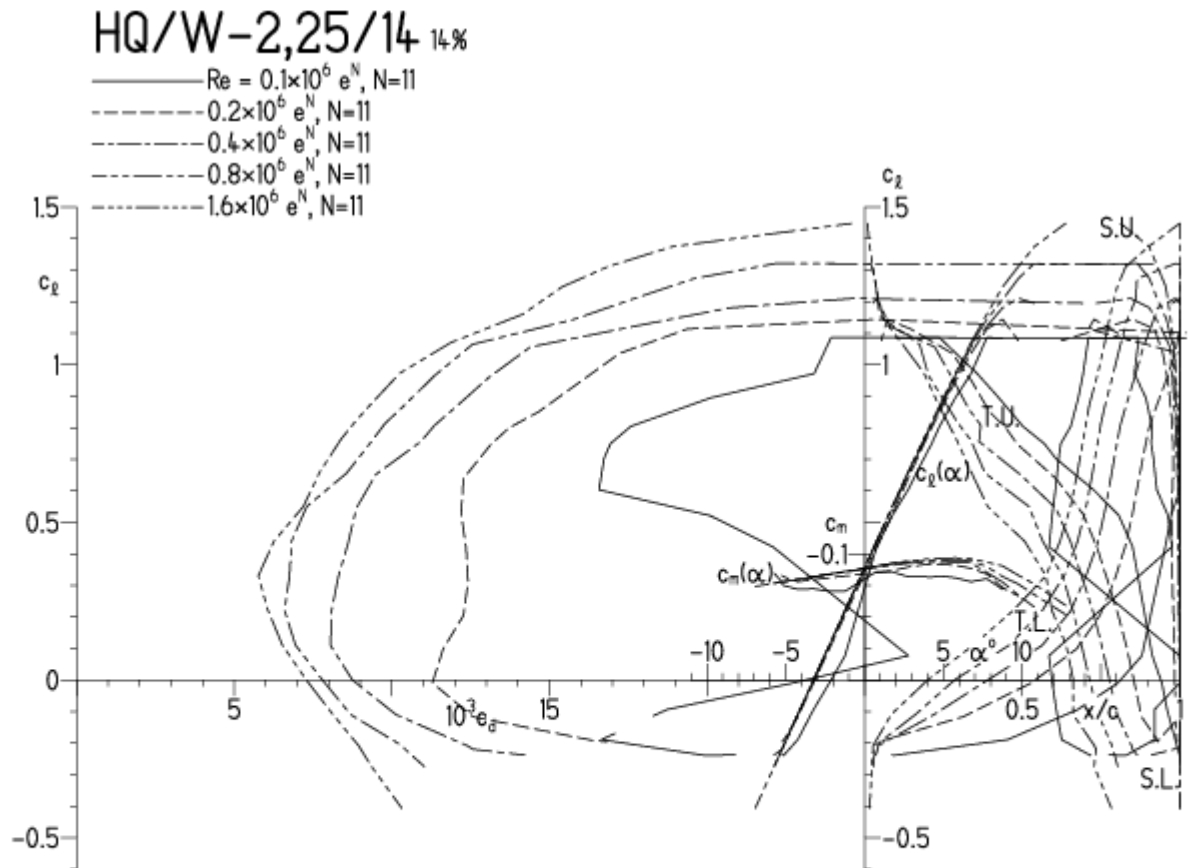


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

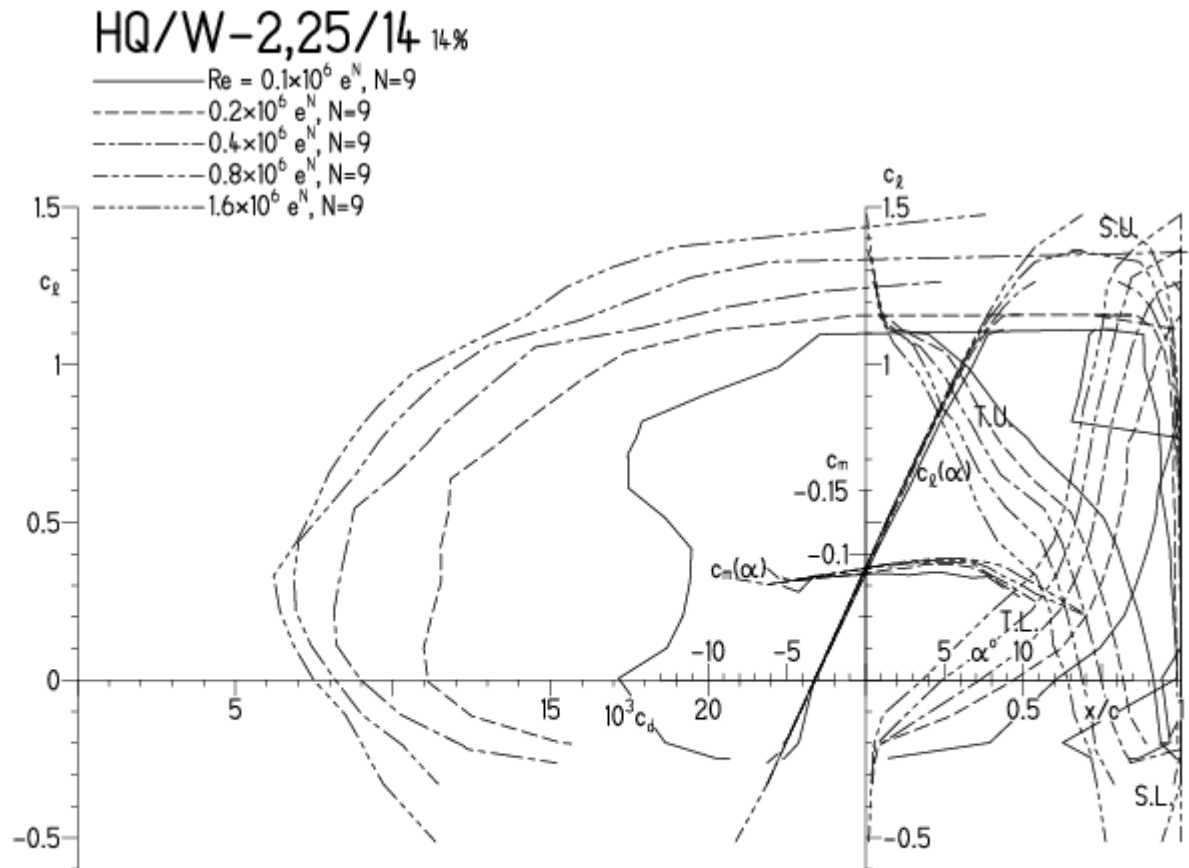


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

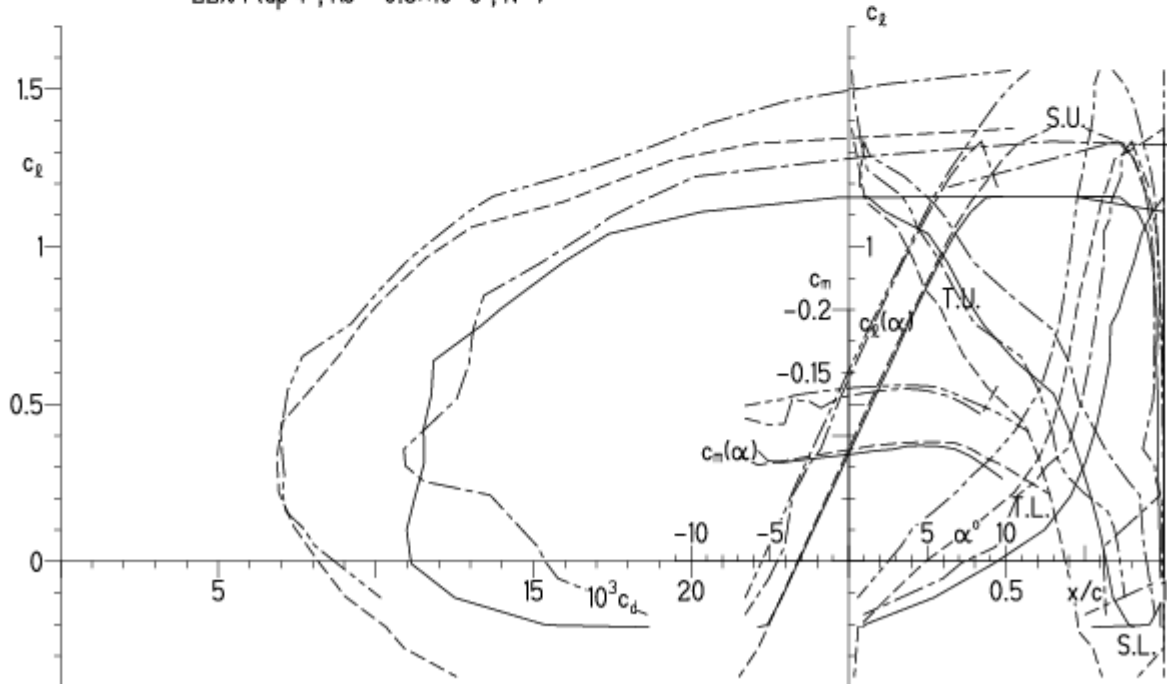


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

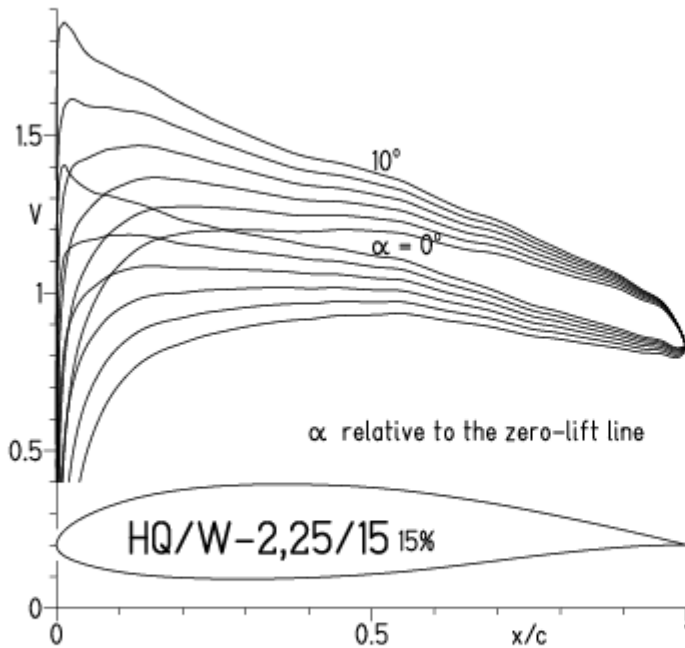


EPPLER 2005 V. 8.5.07

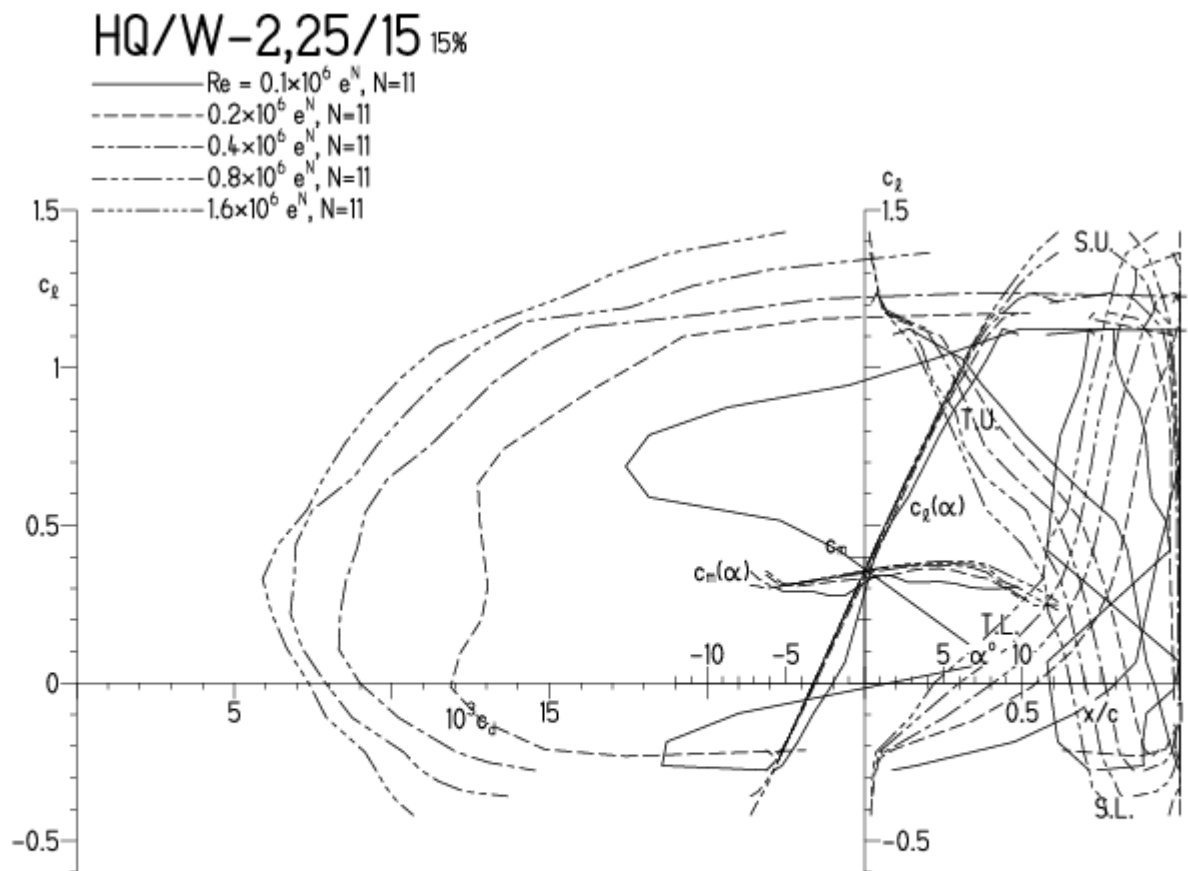


HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

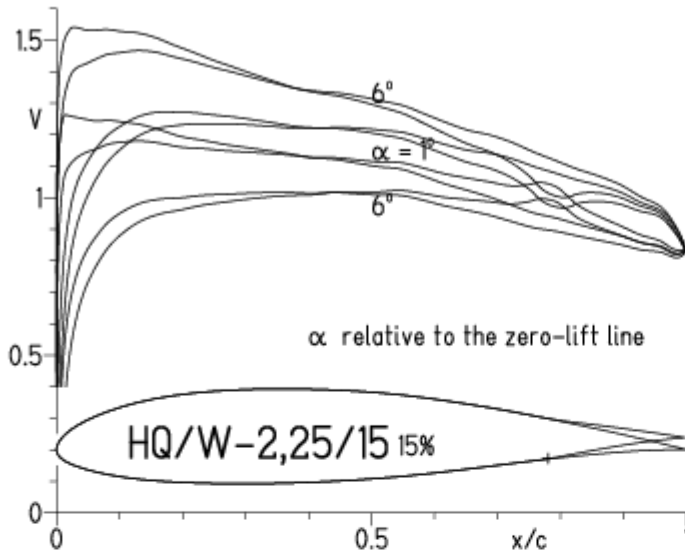


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04

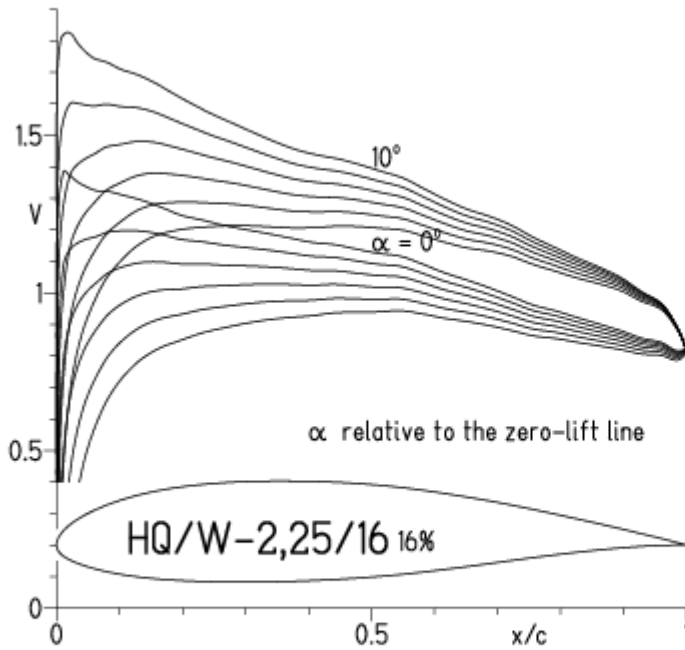


EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

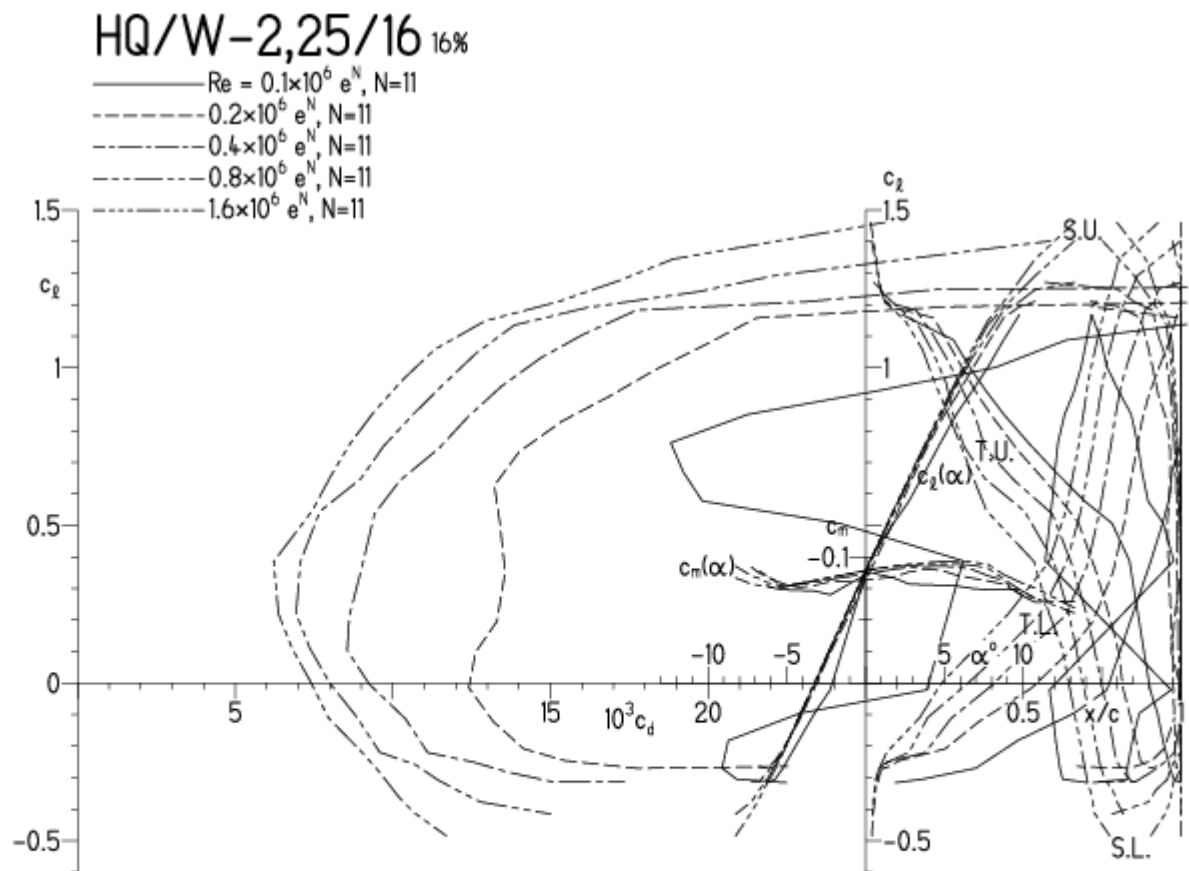


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

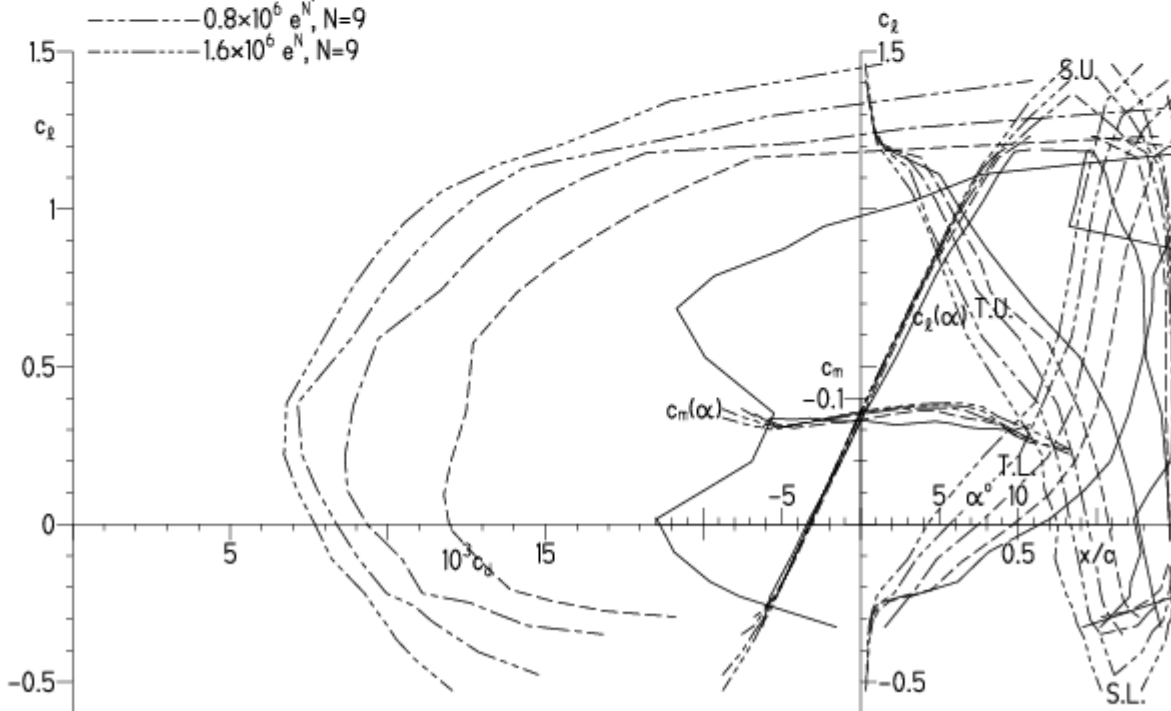
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

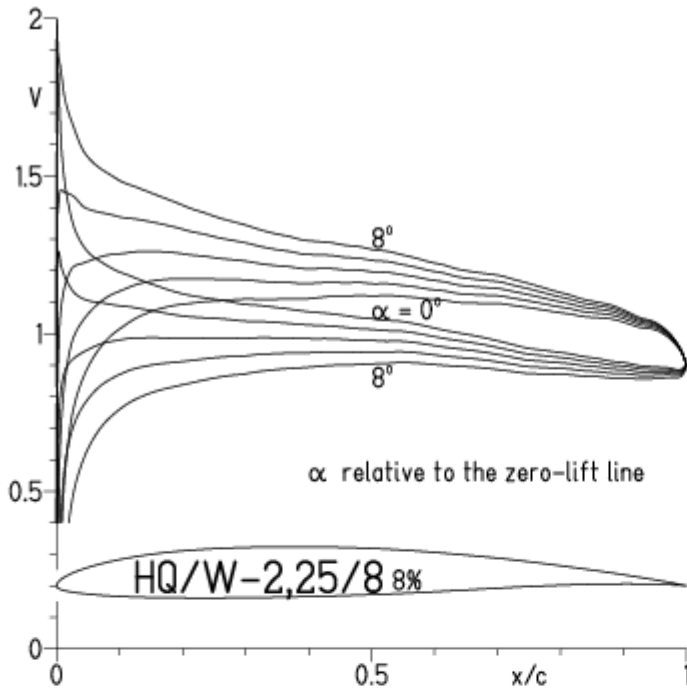
HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

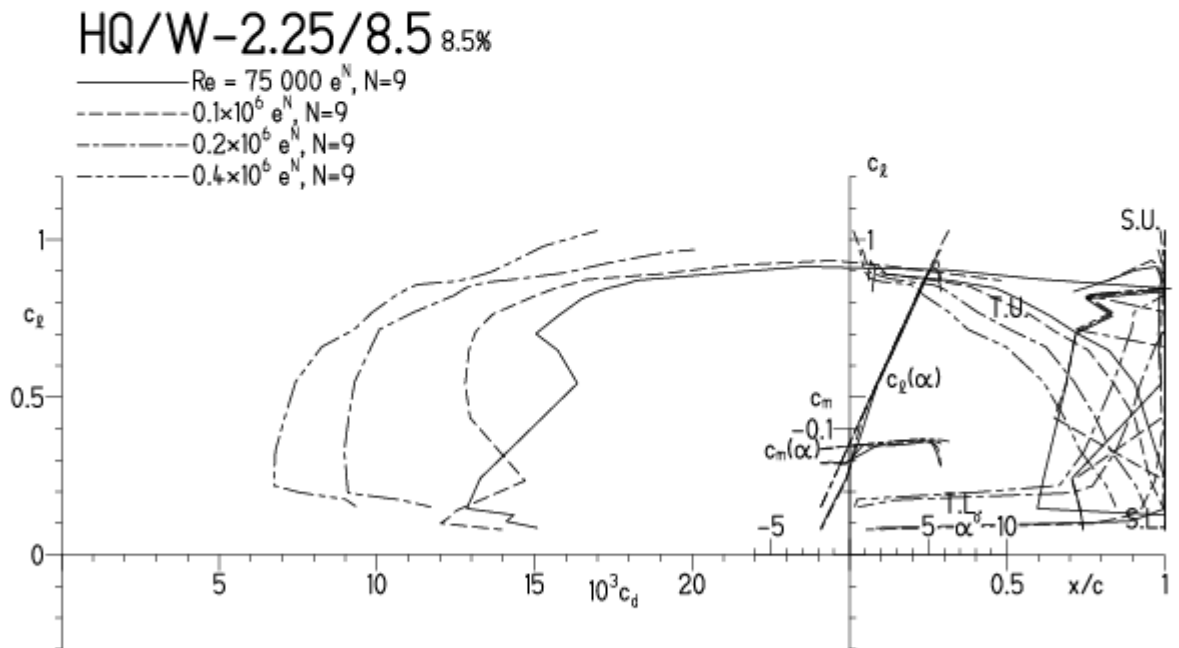


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

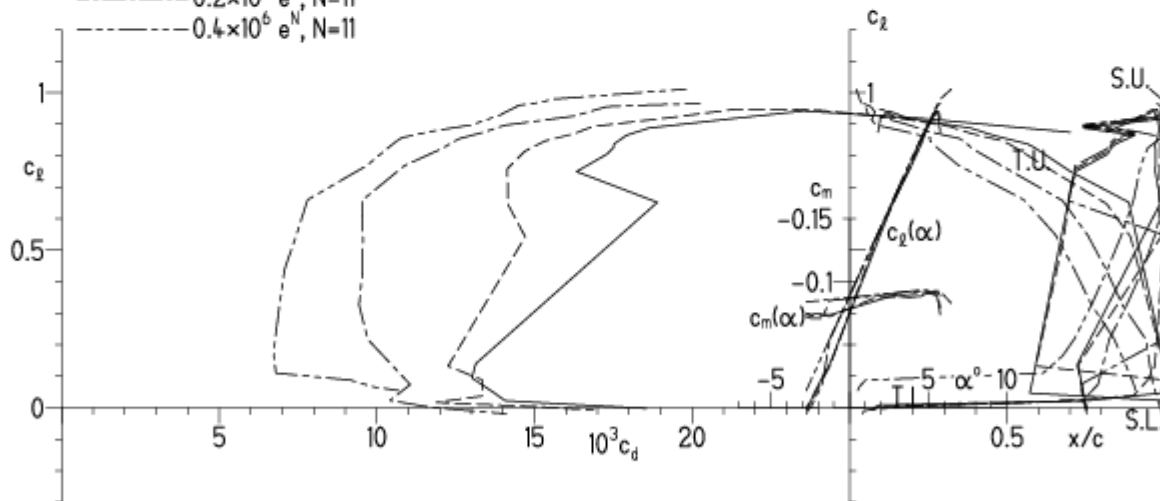
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

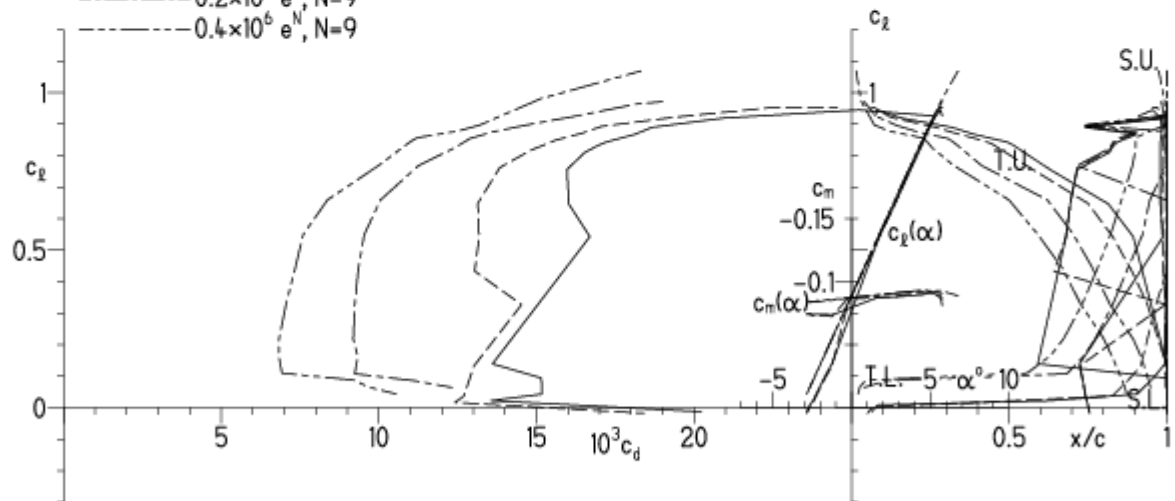
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

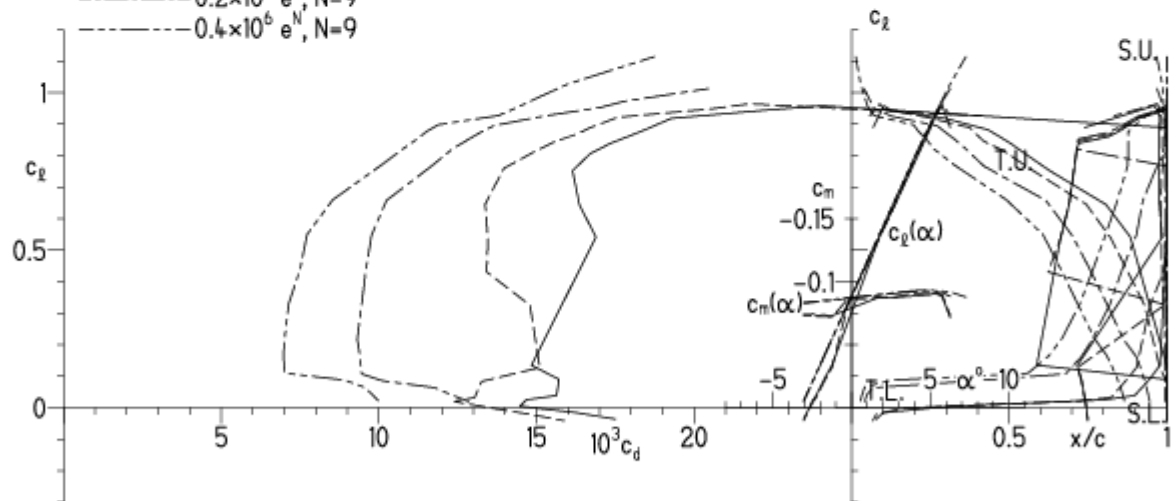
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

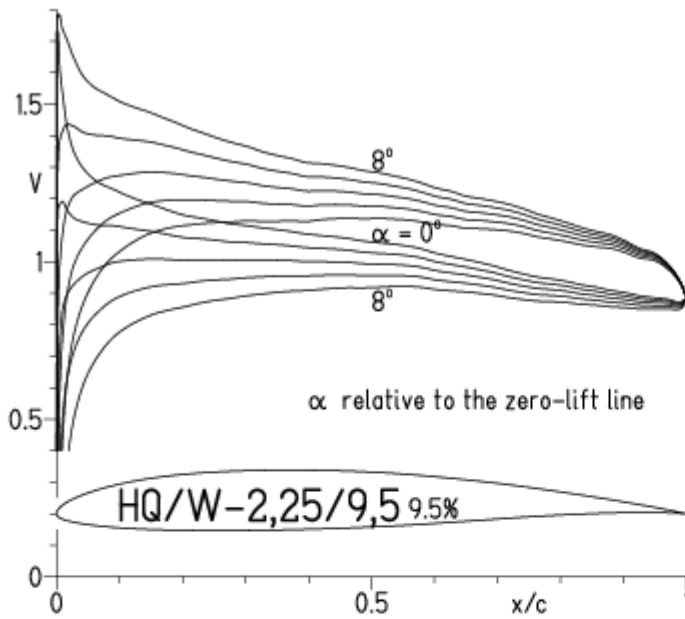
HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

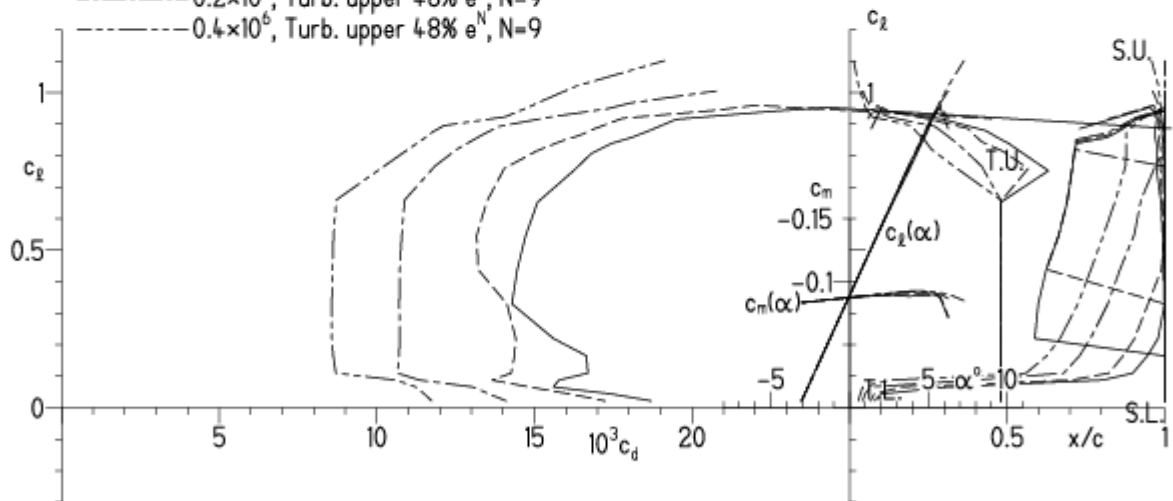
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

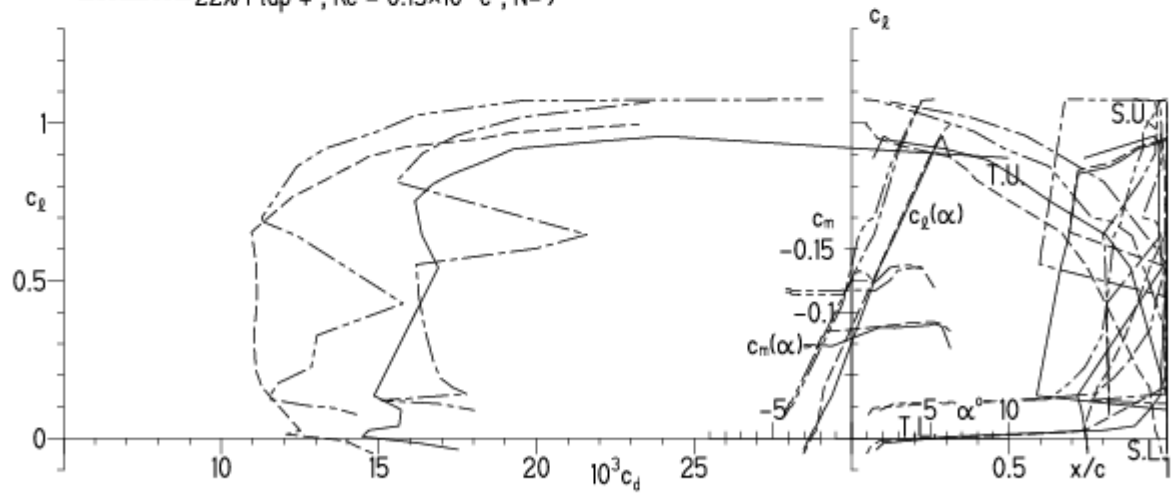


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

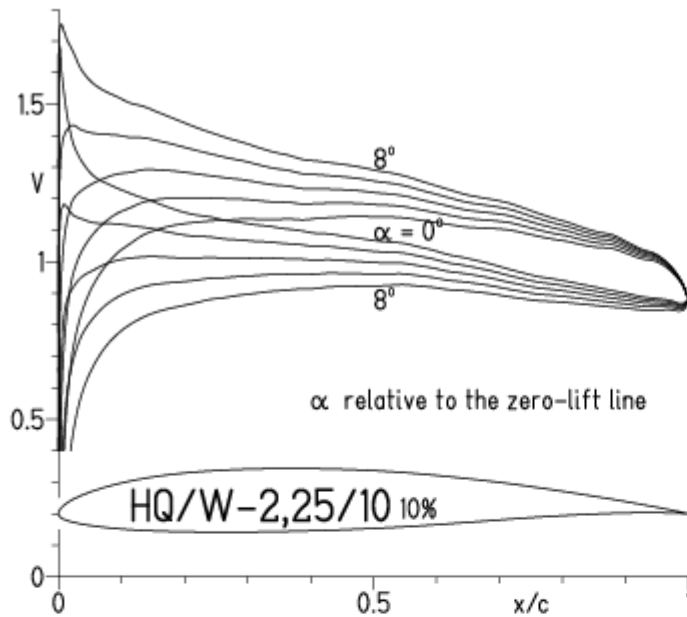


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

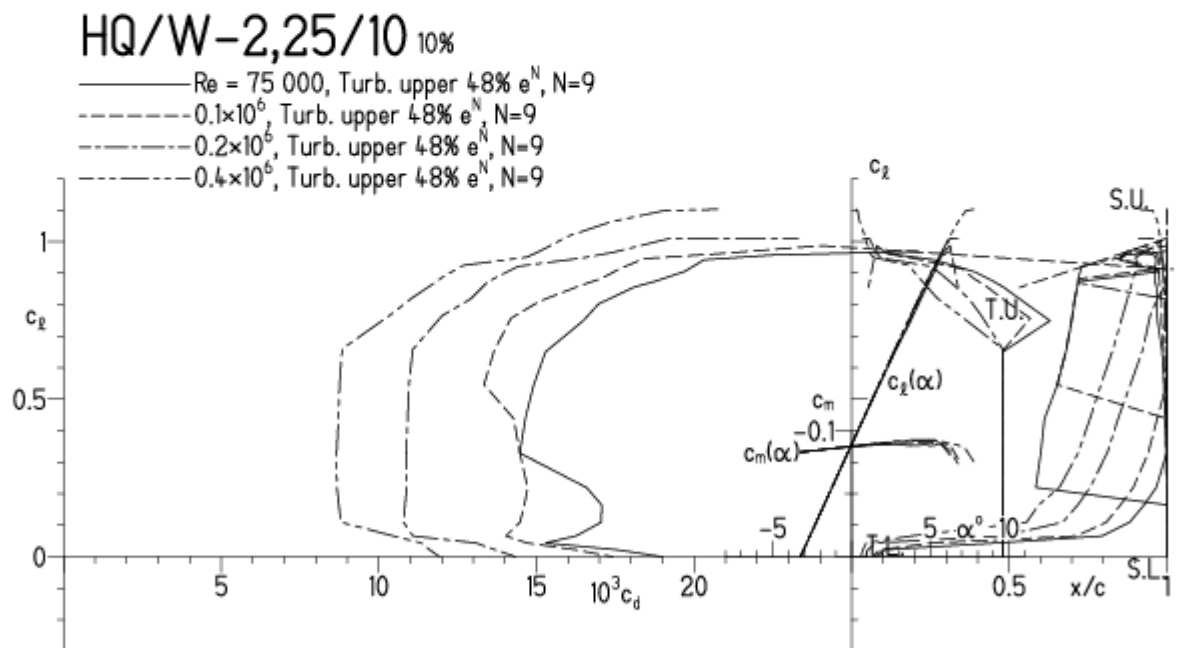


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

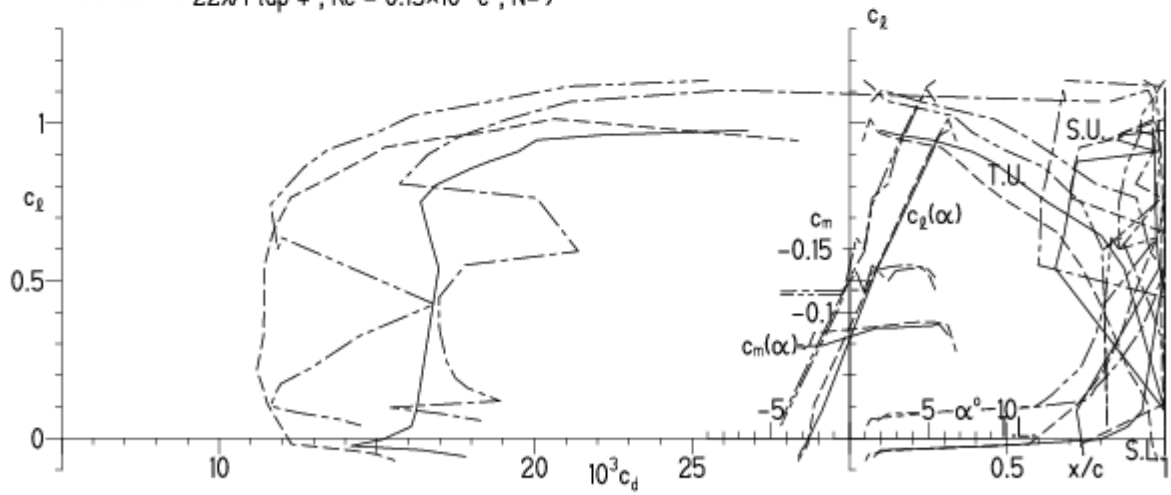


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

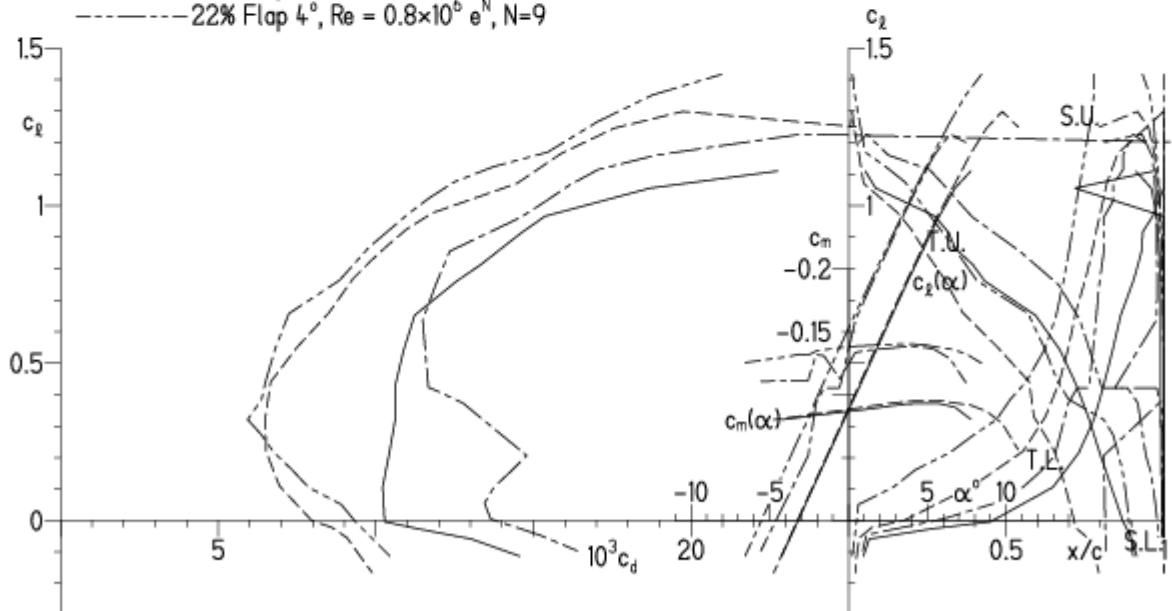


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

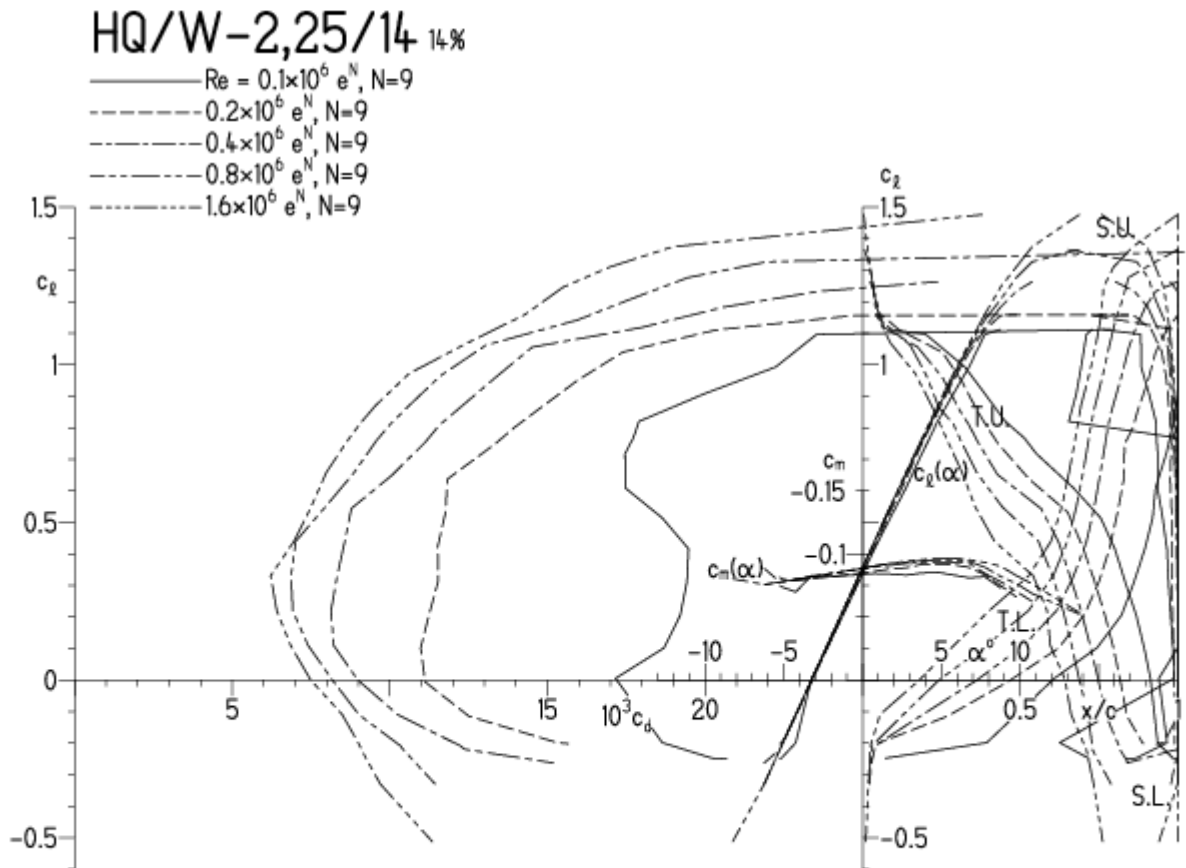


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

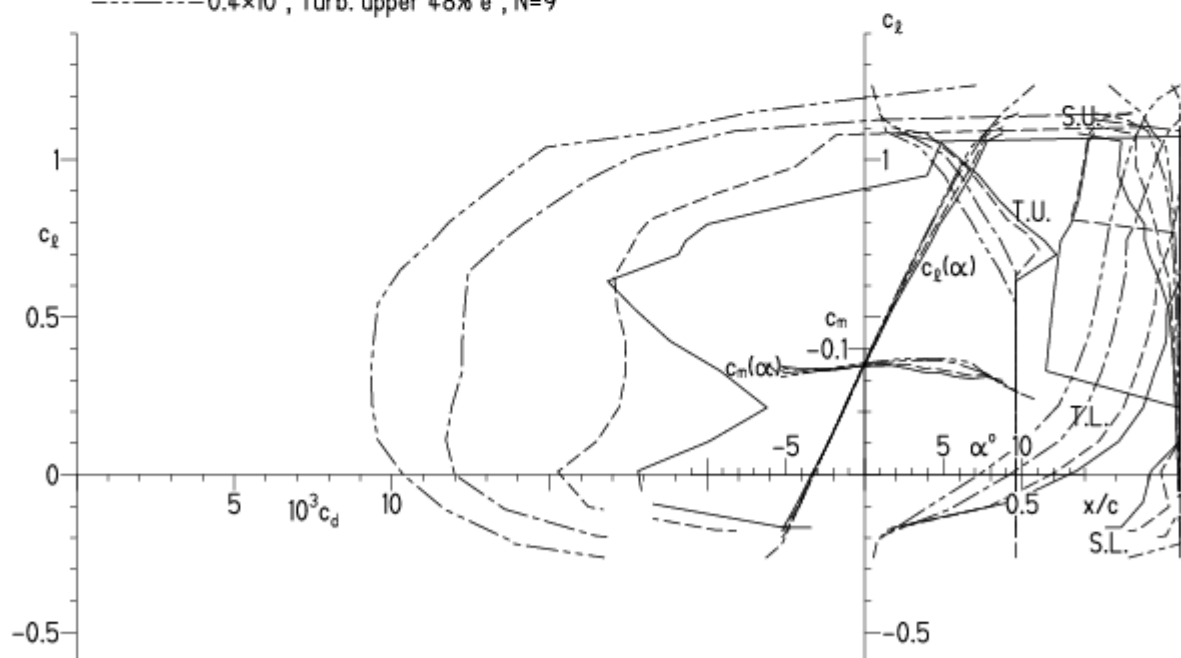
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

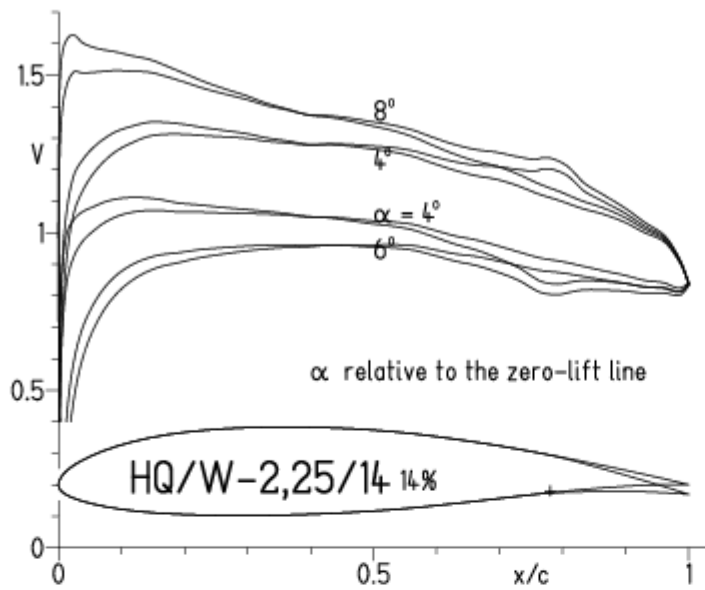
HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

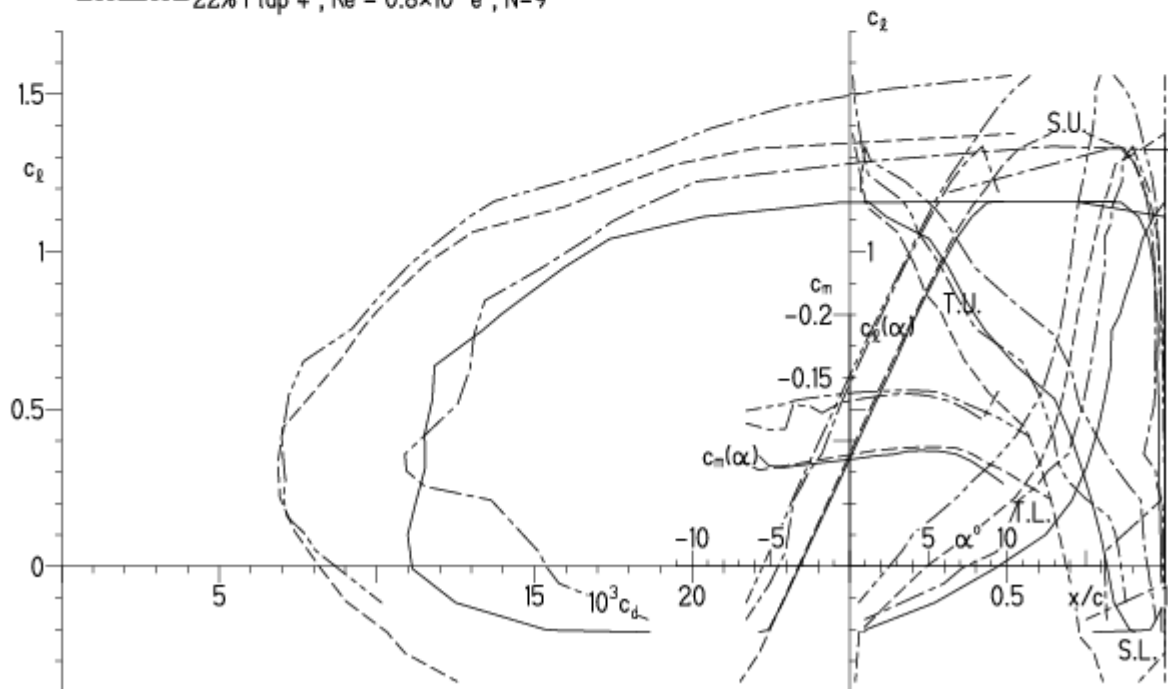


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

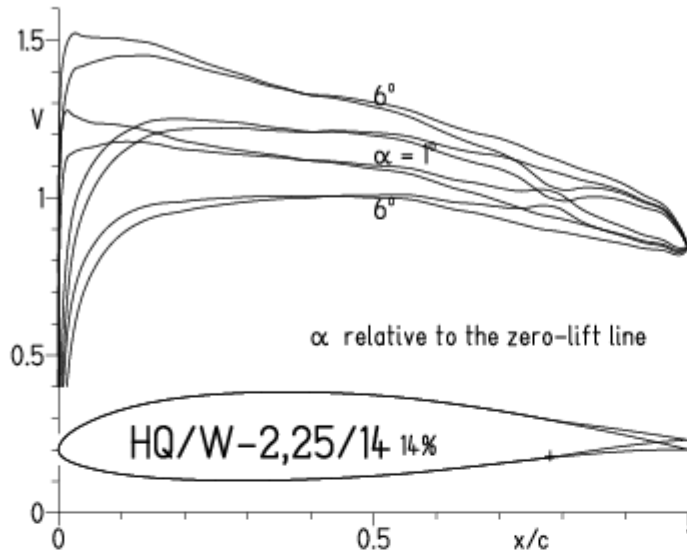
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

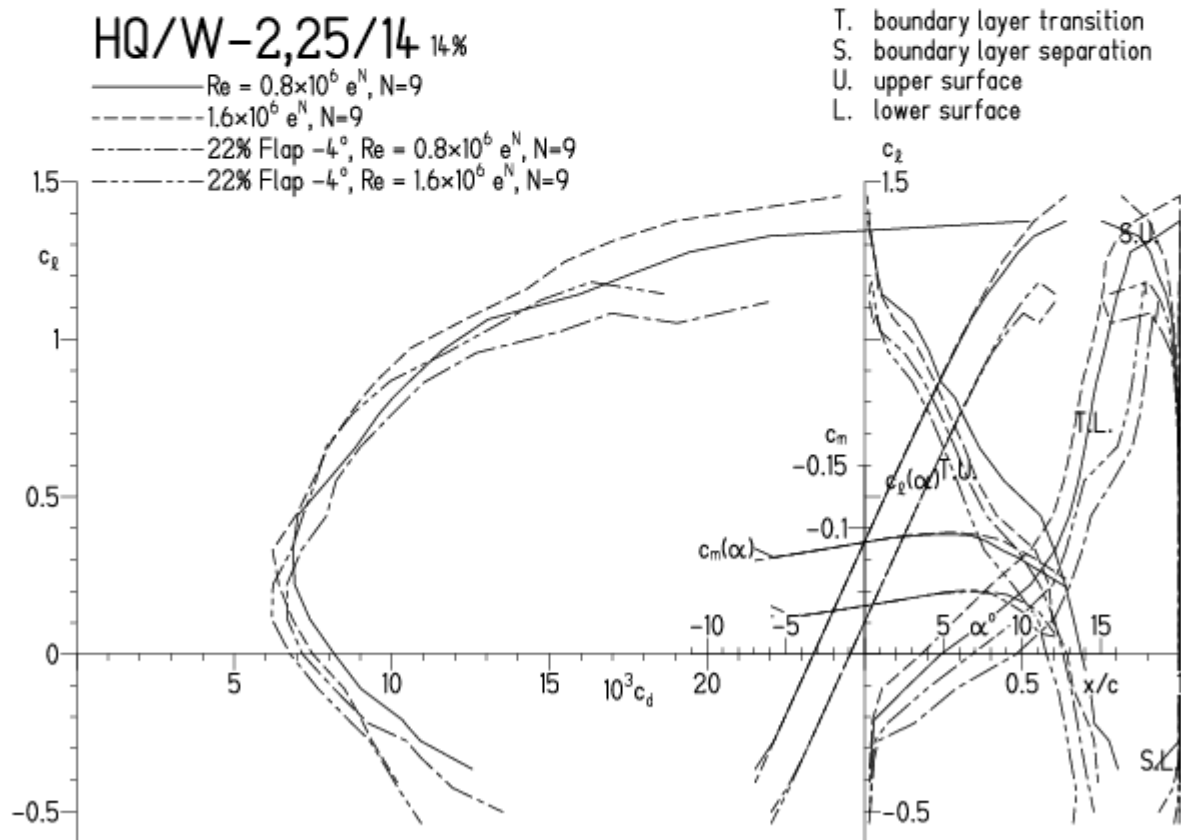


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

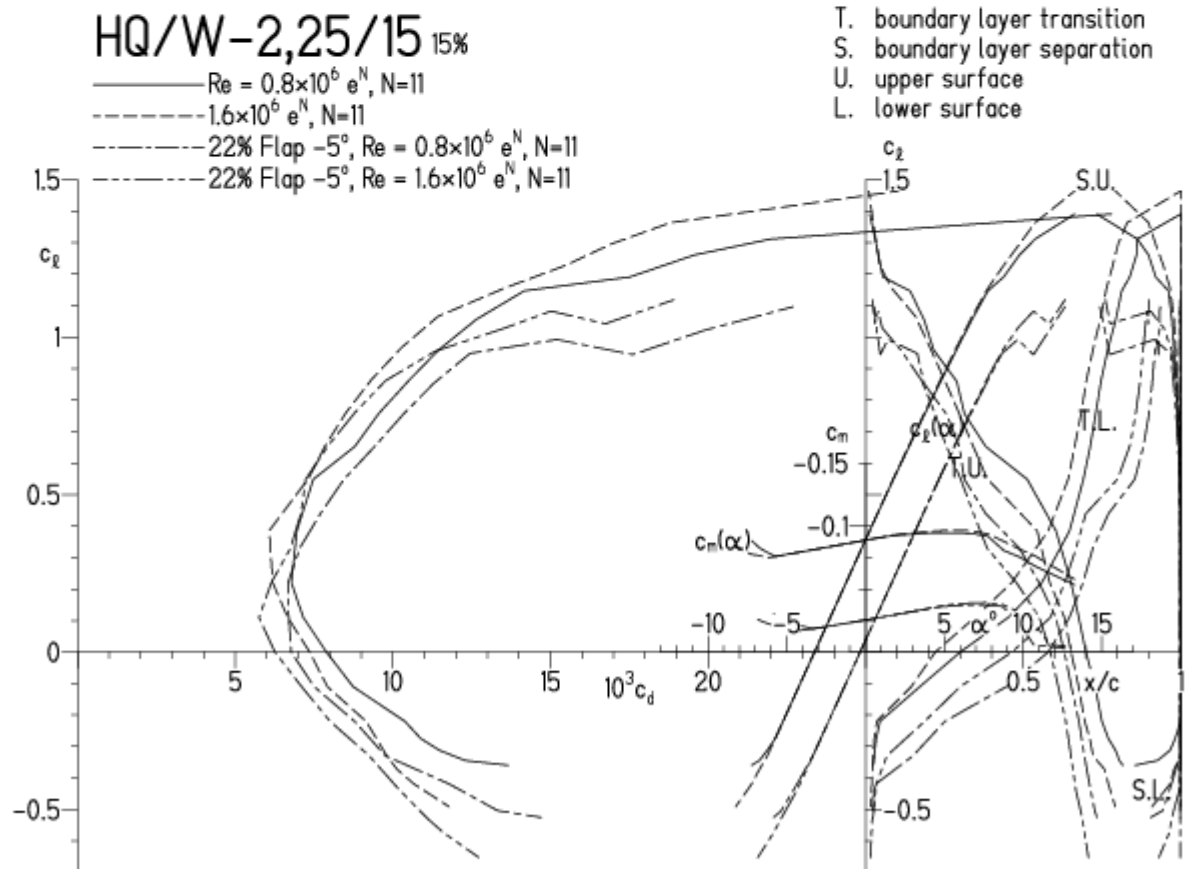
Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

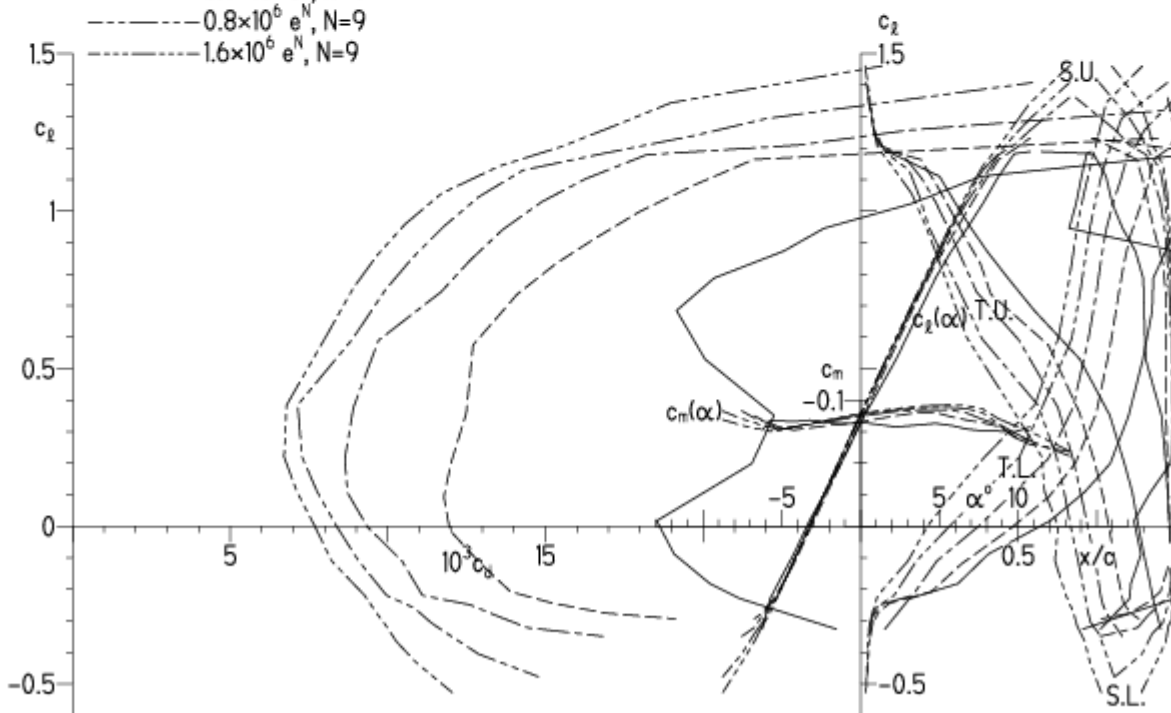
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41

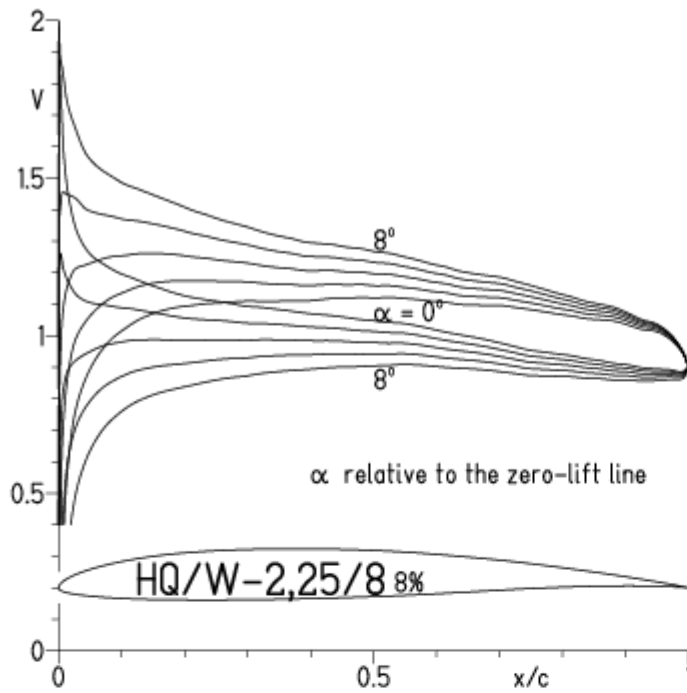


EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

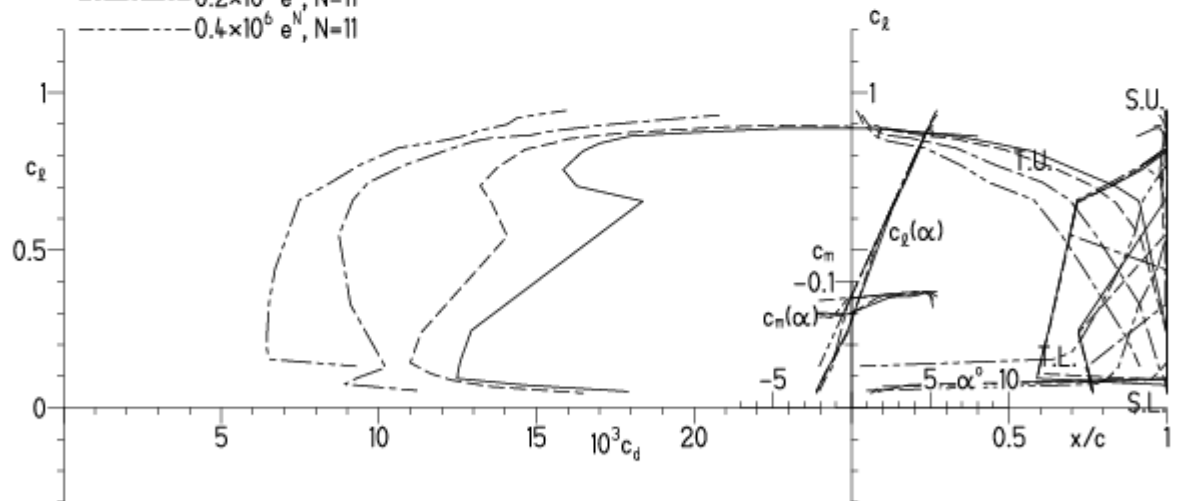
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23

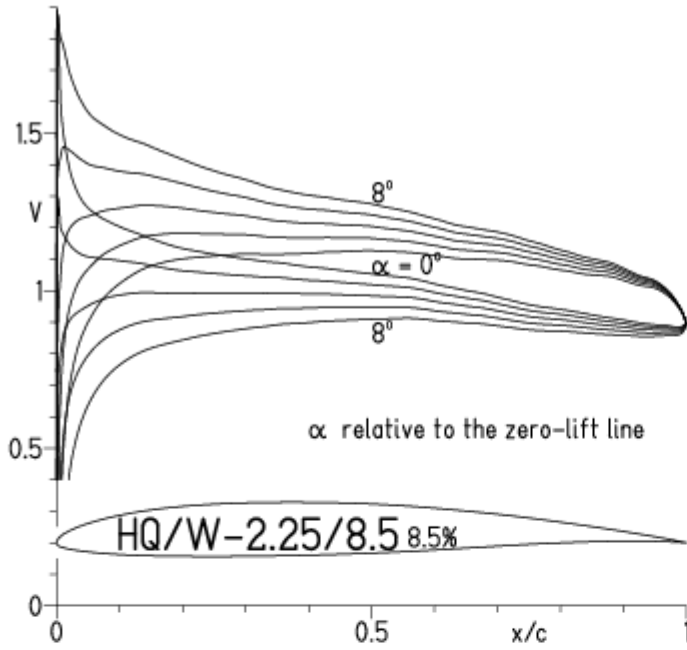


EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

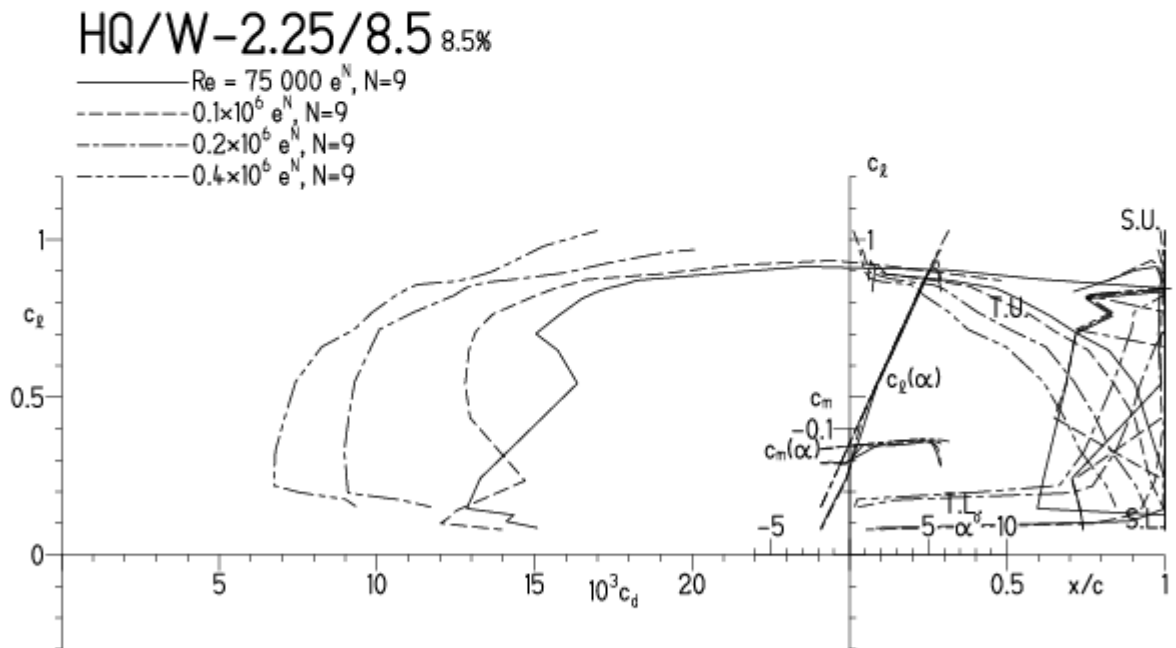


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

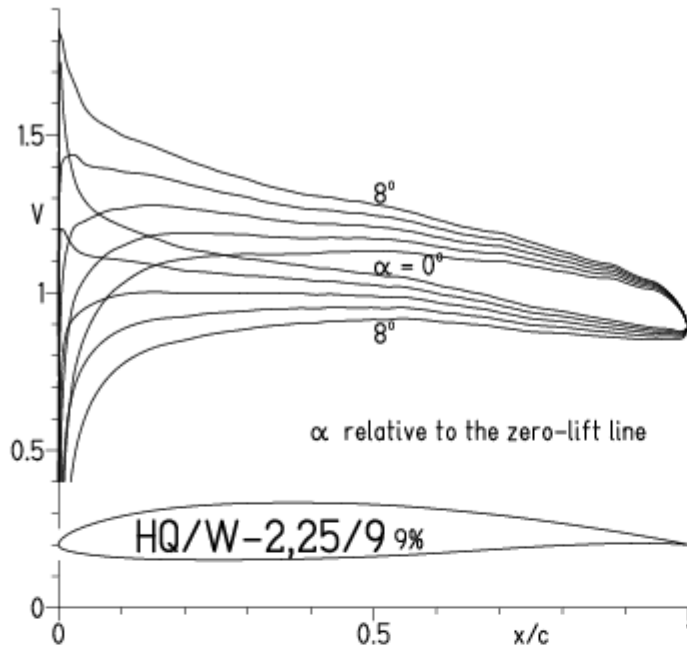


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

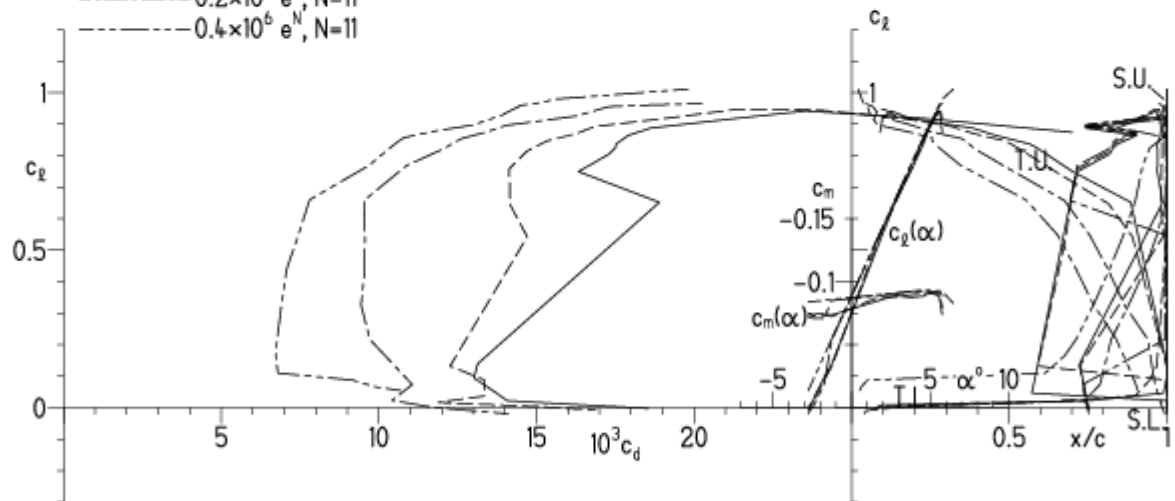
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



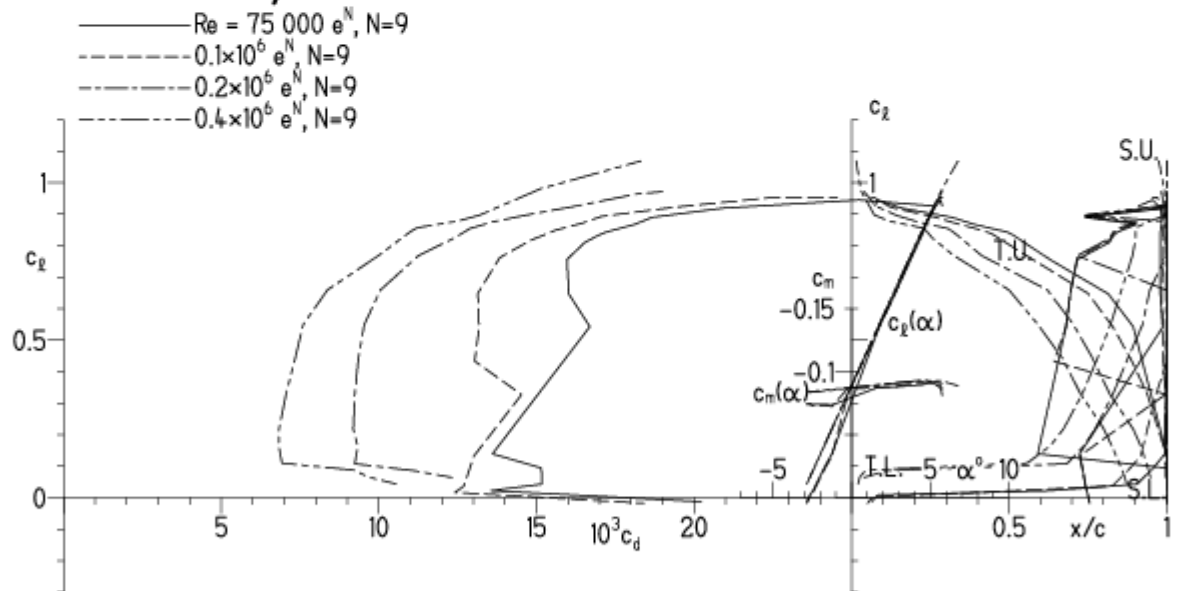
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

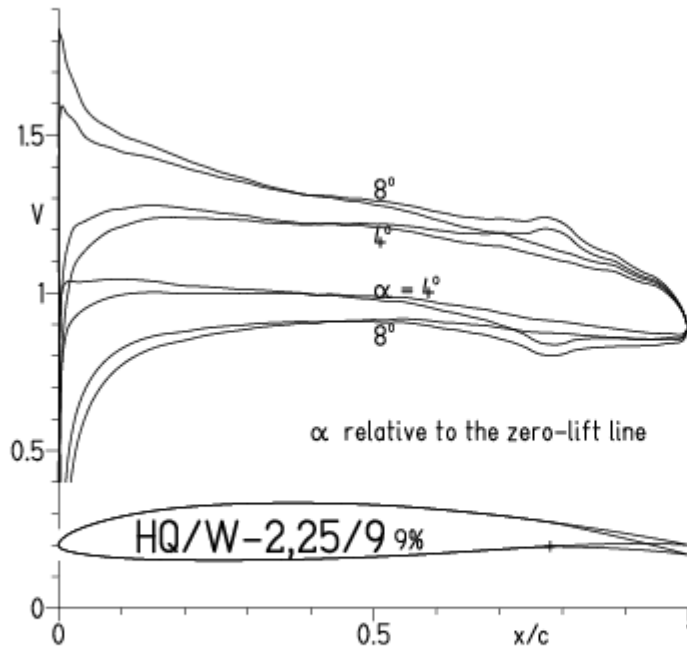
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

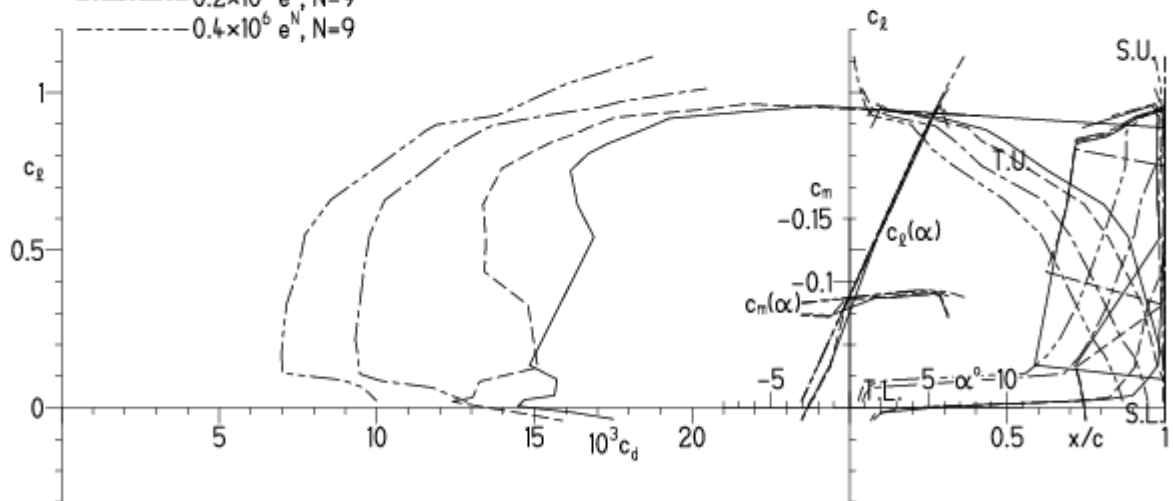
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

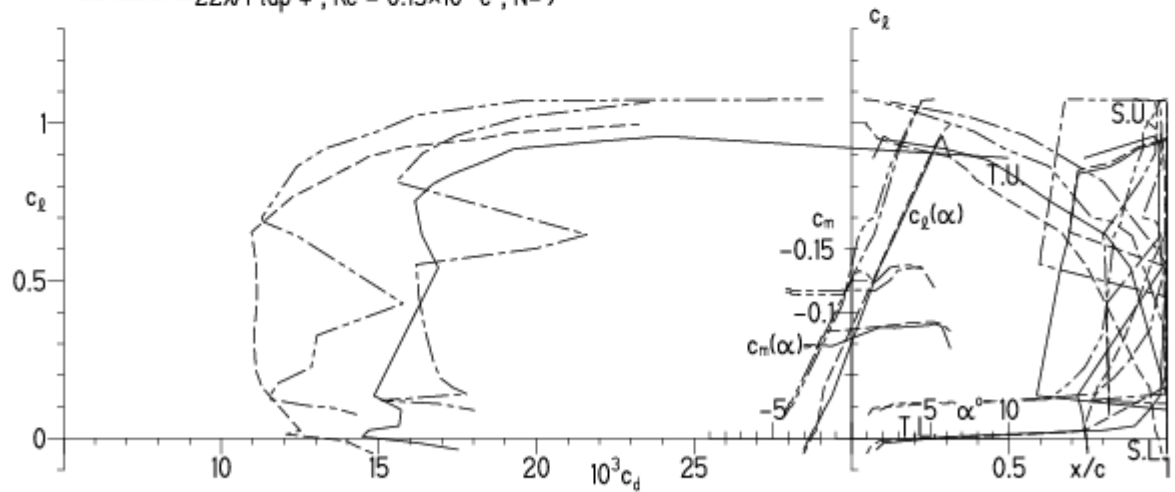


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

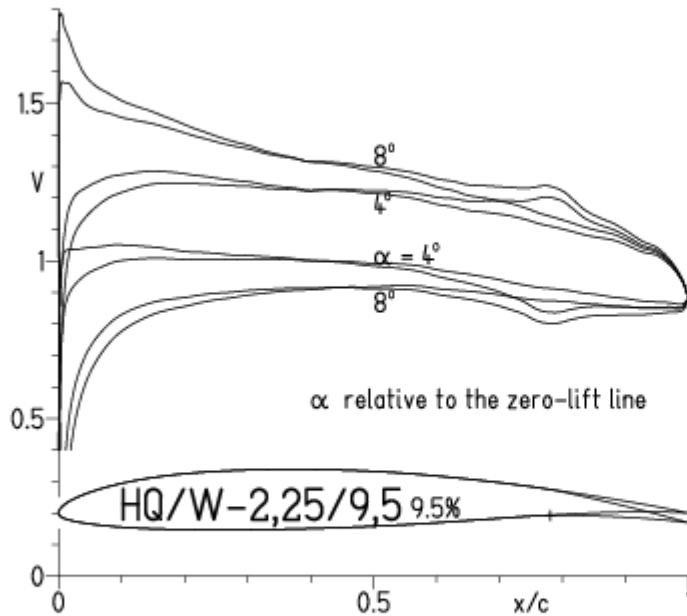
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

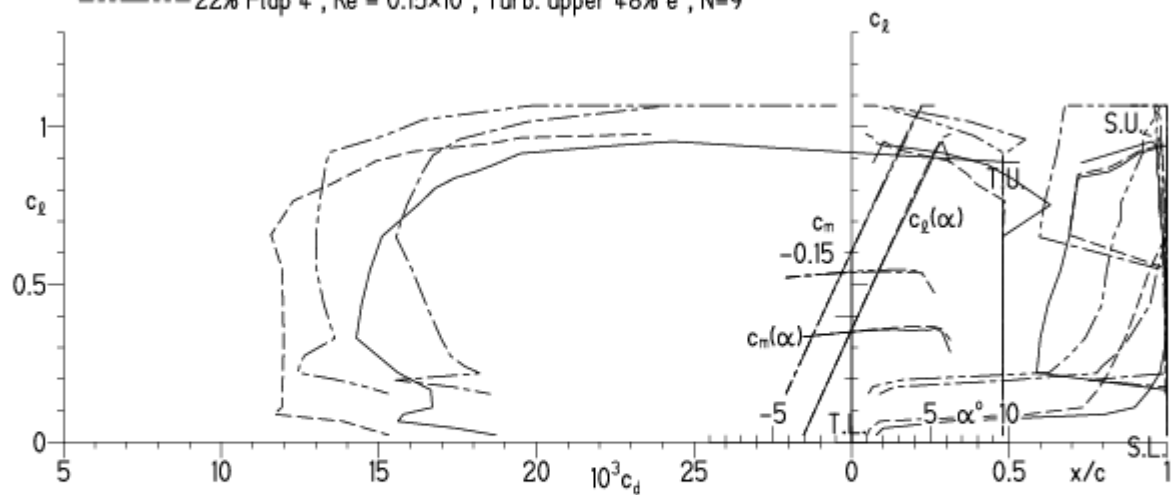


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

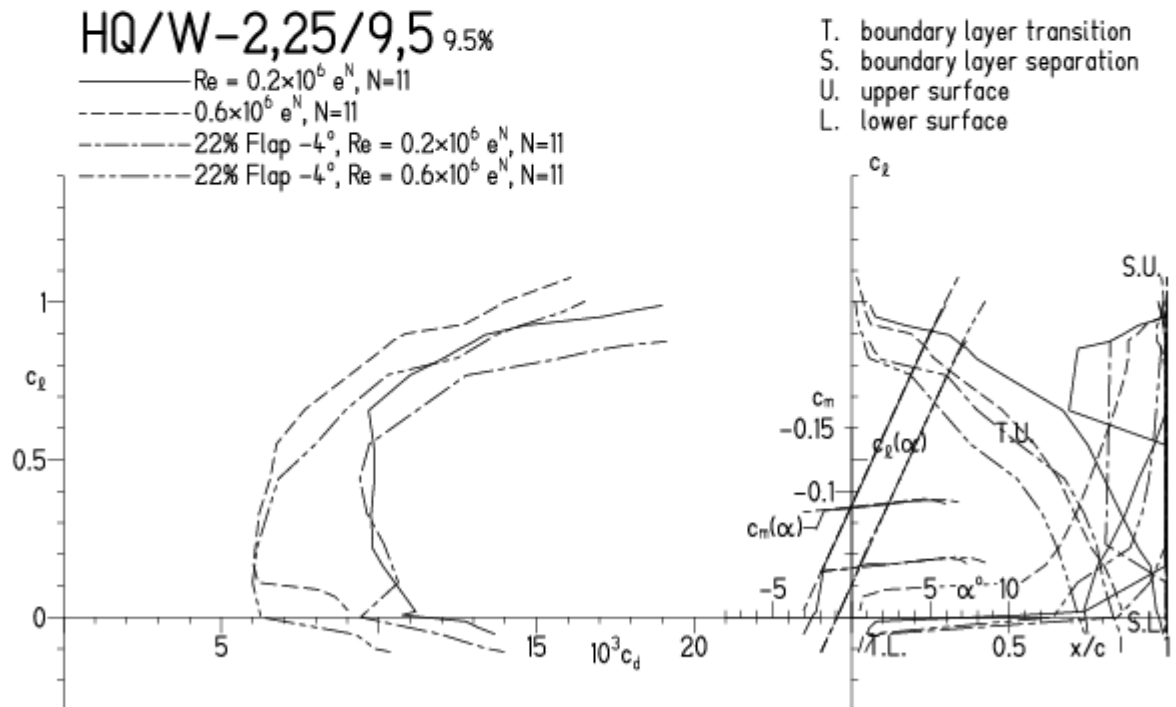


HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

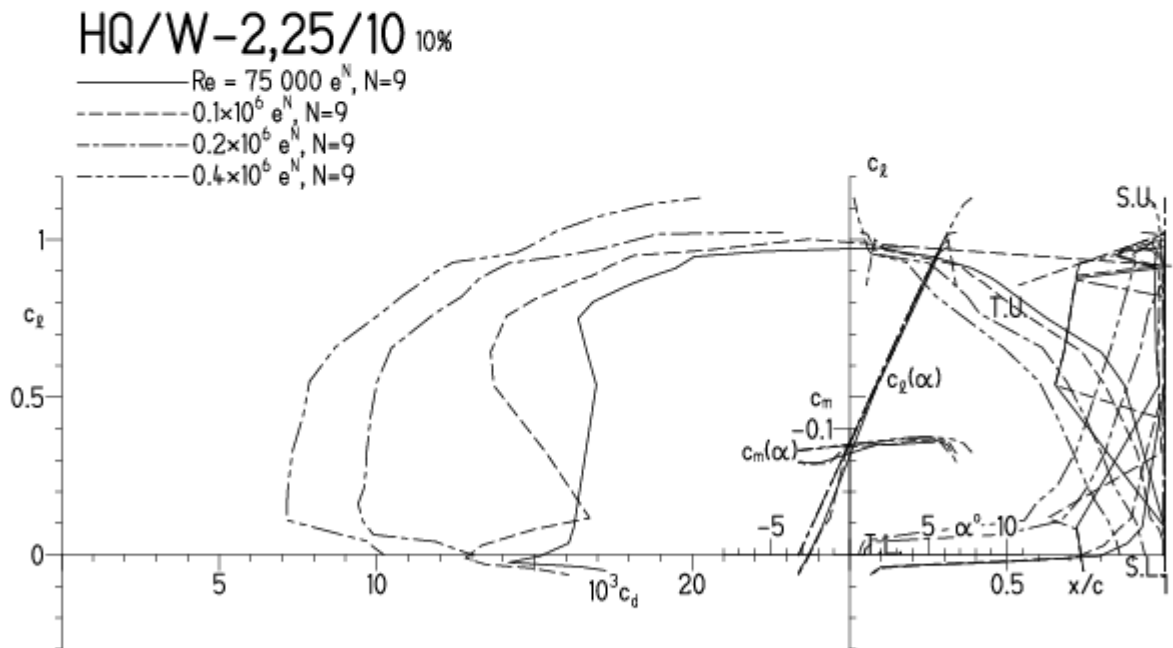


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

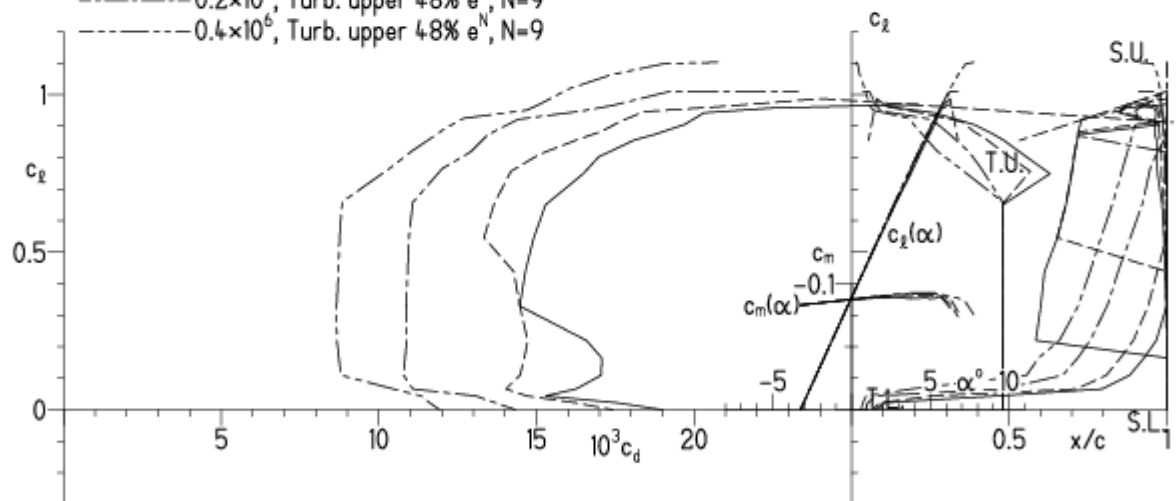
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

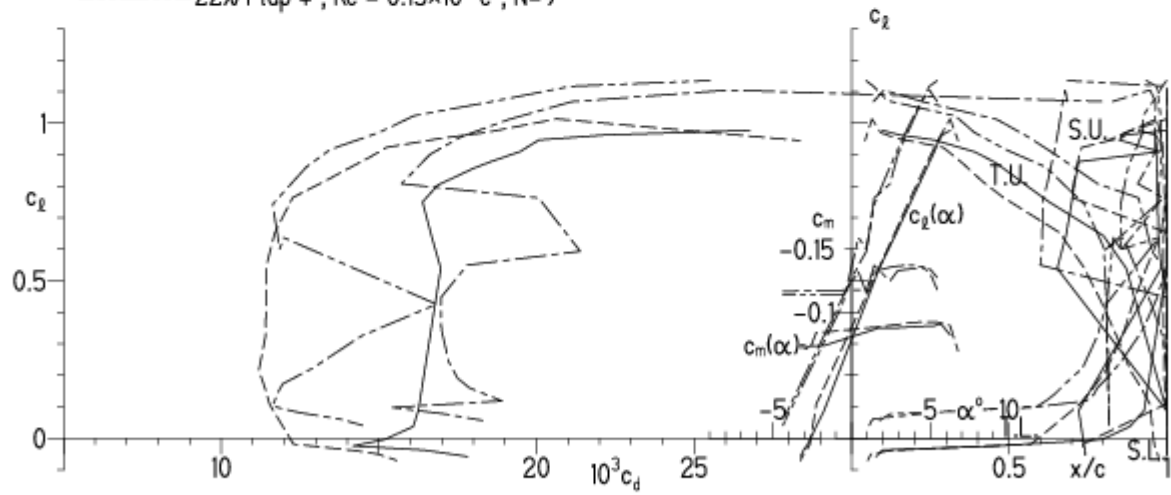


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

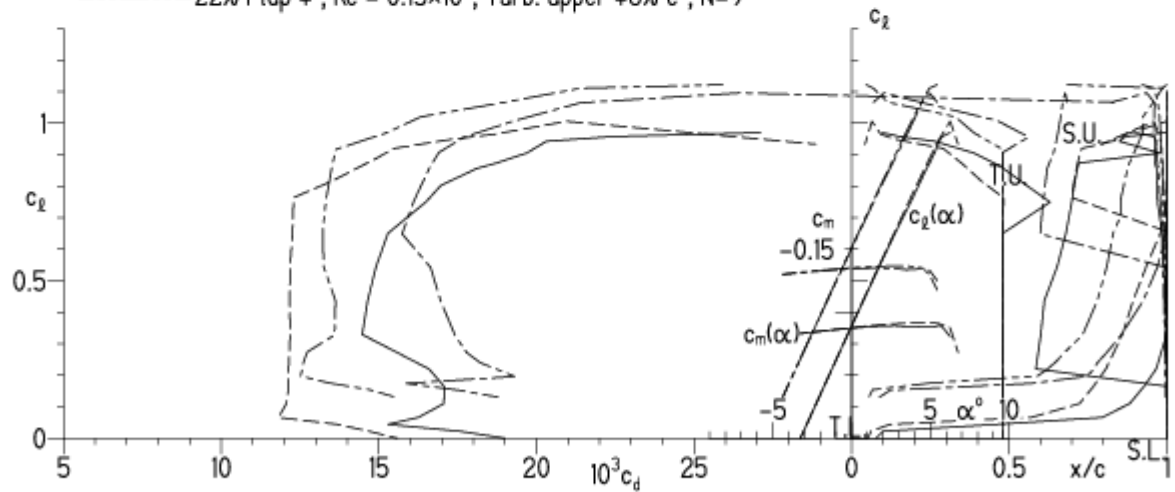


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

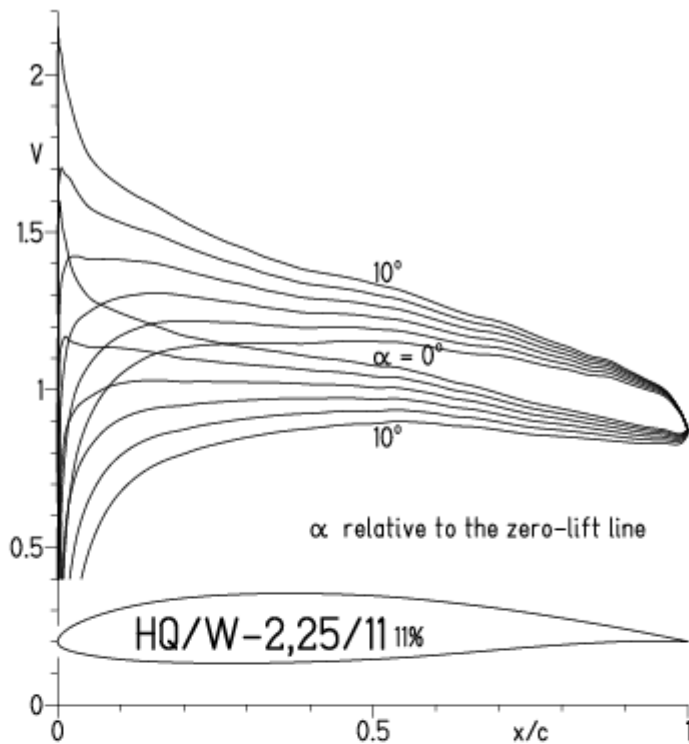


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

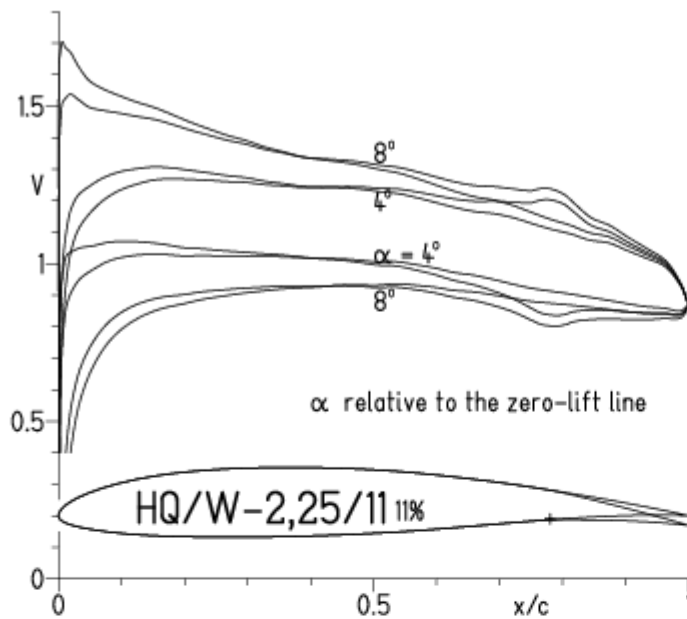
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

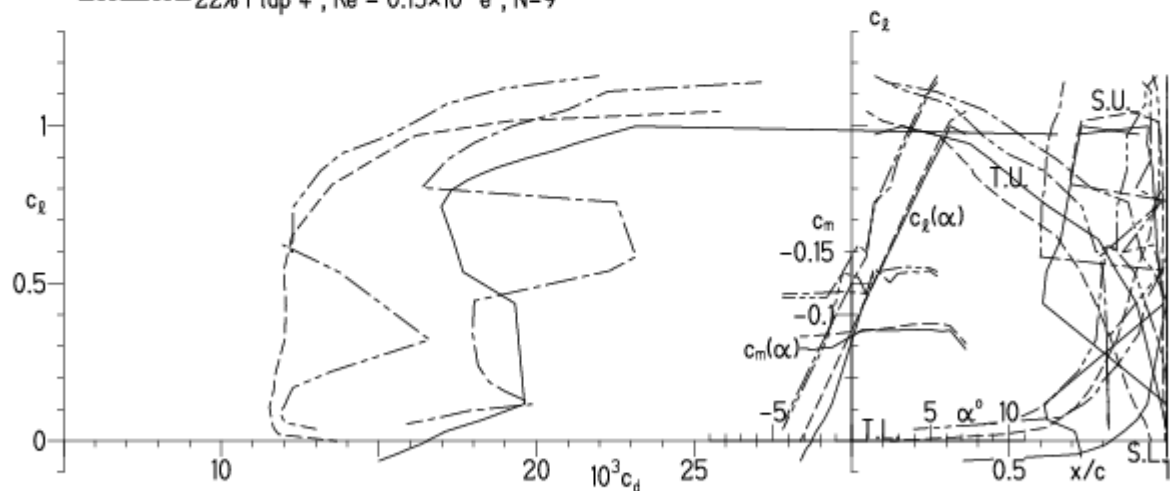


EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

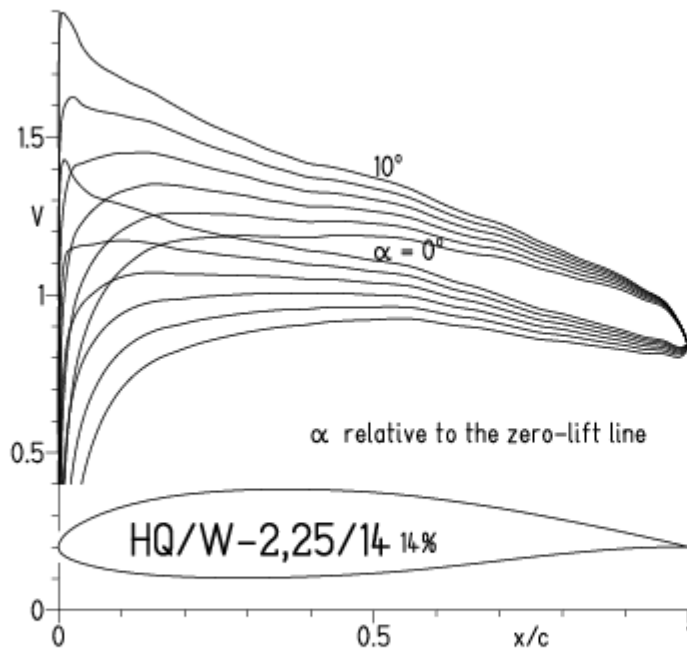


EPPLER 2005 V. 8.

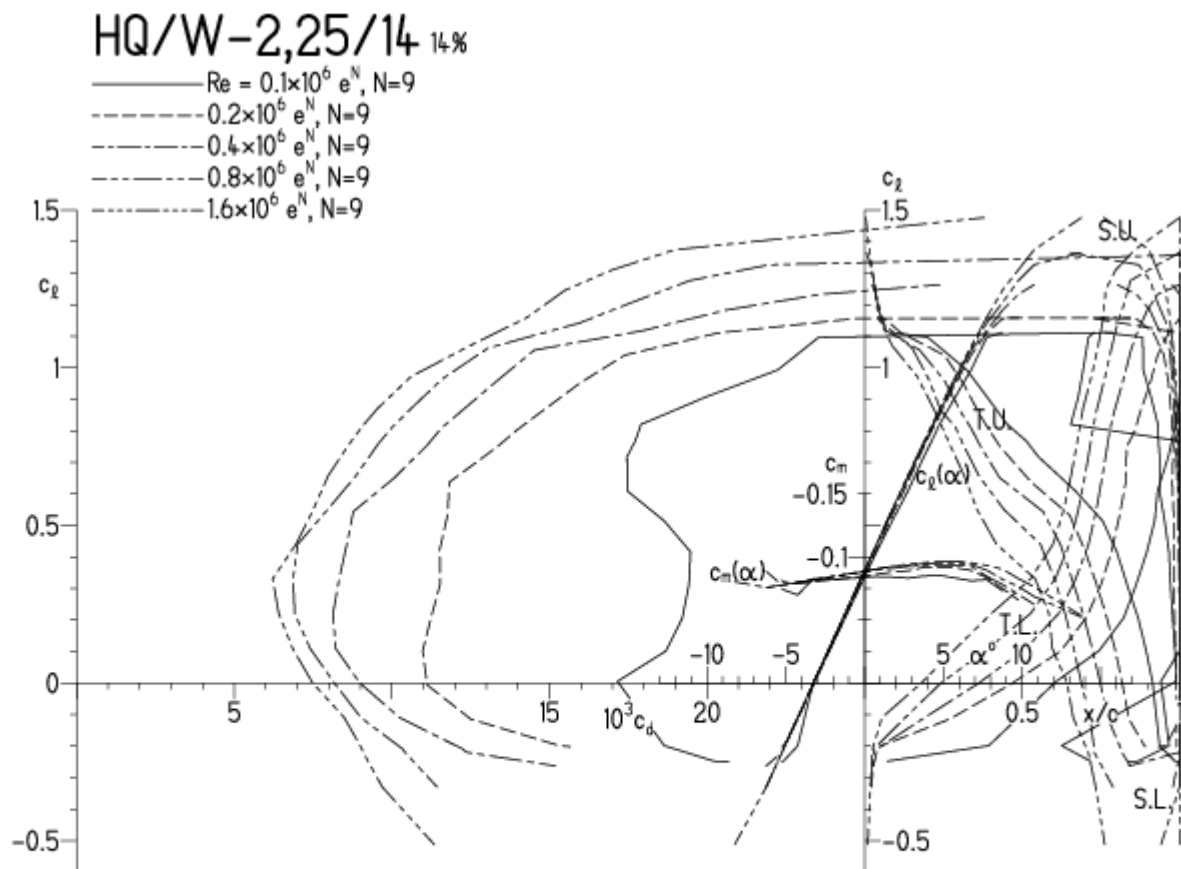


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

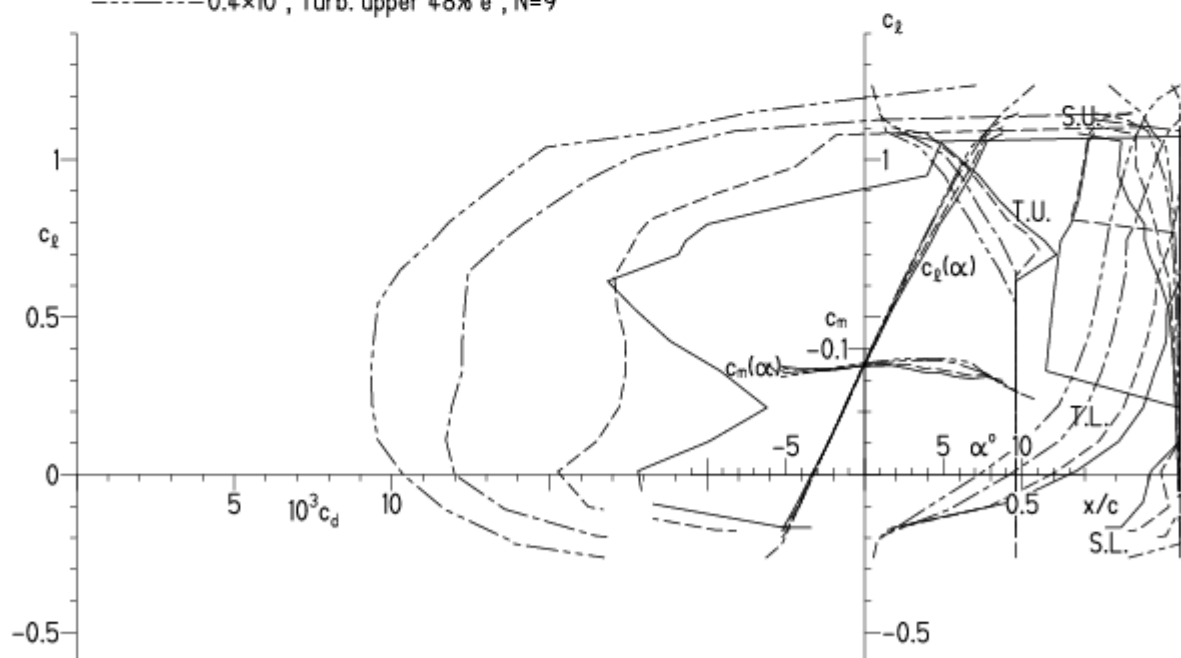
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · · 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

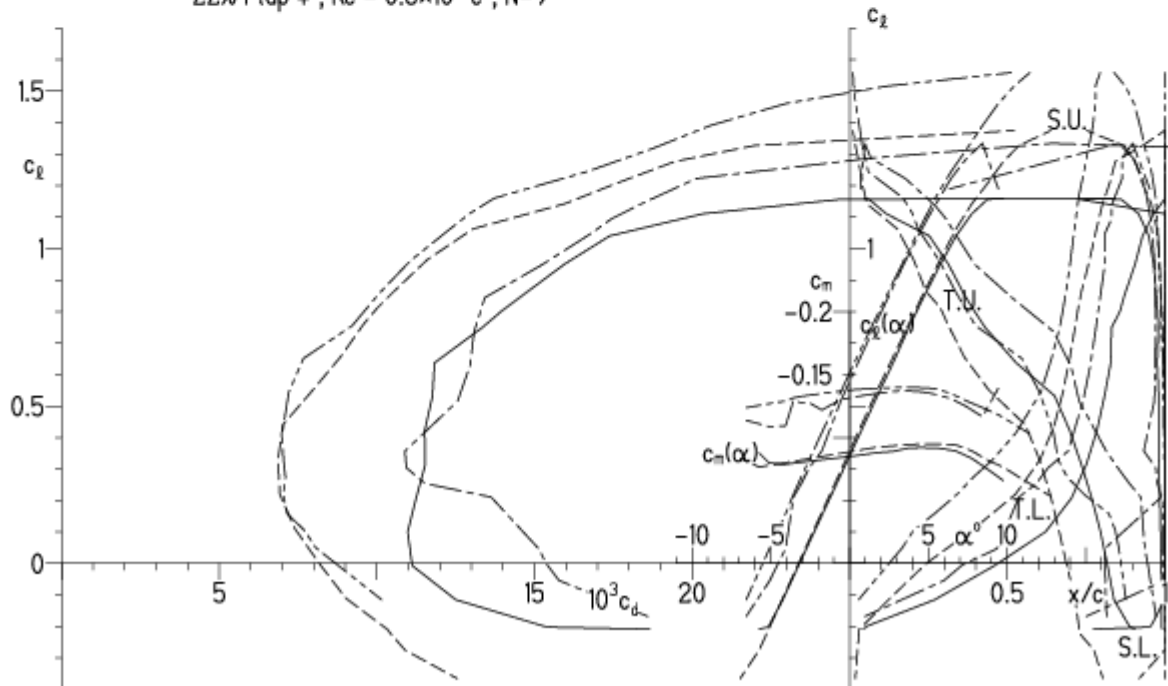


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

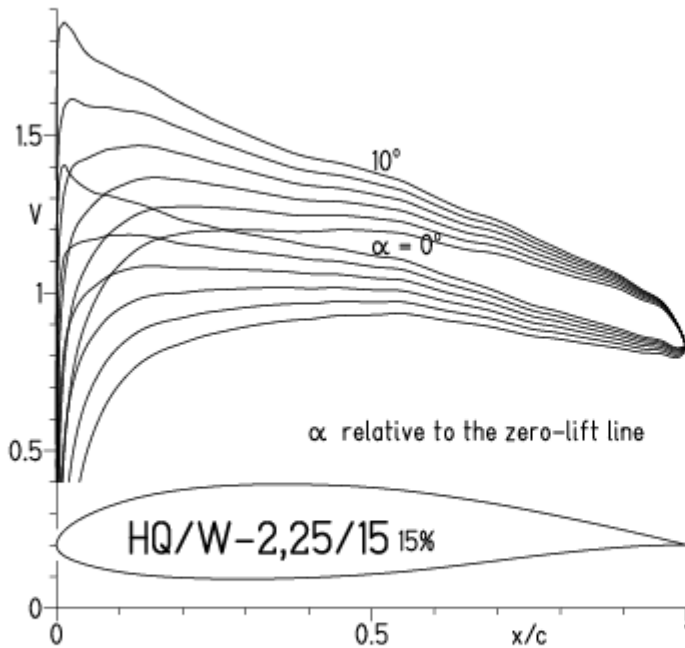


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

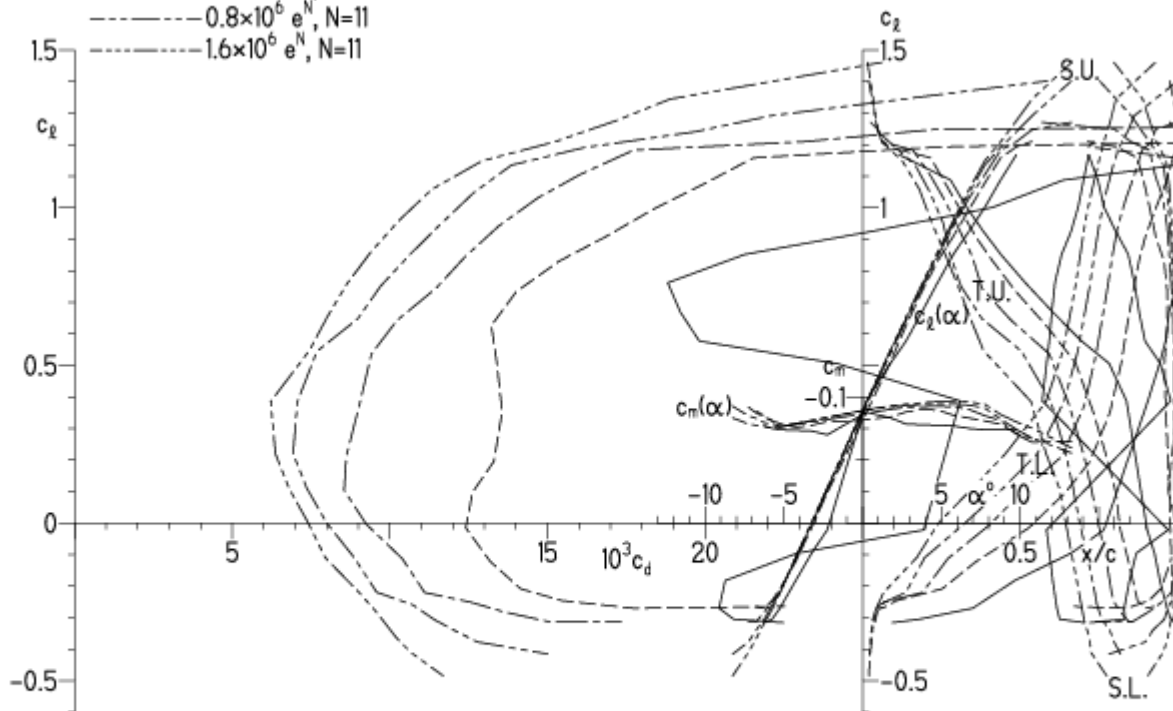
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/16, N=9

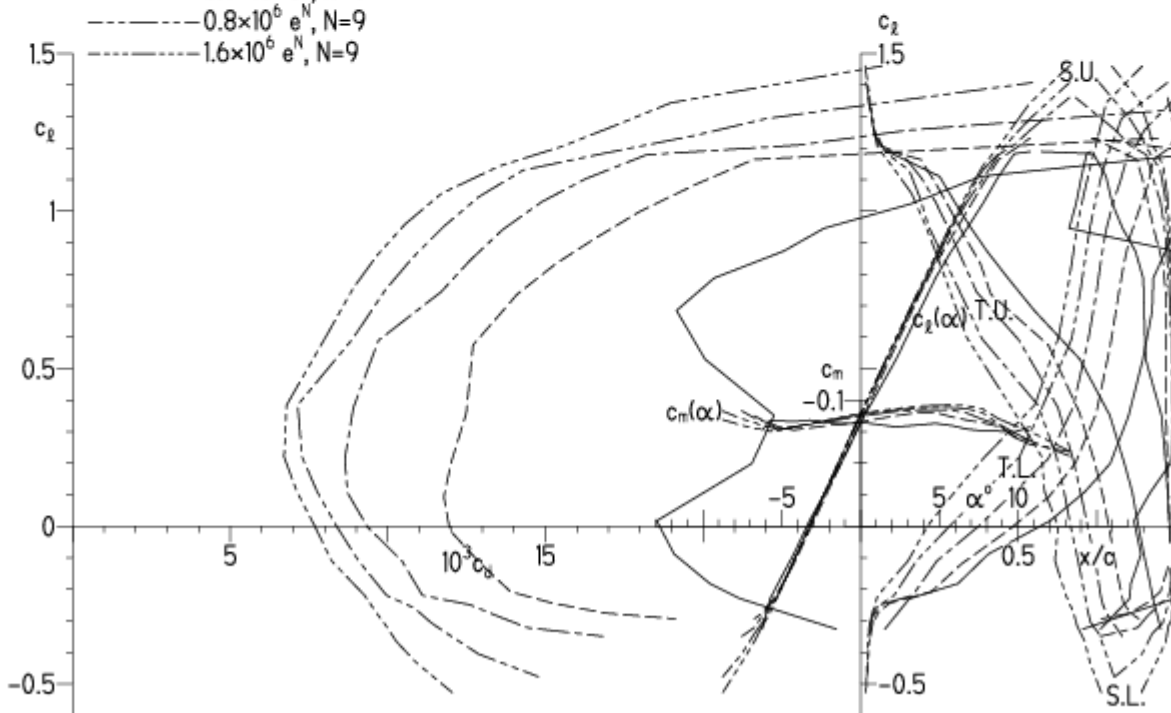
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

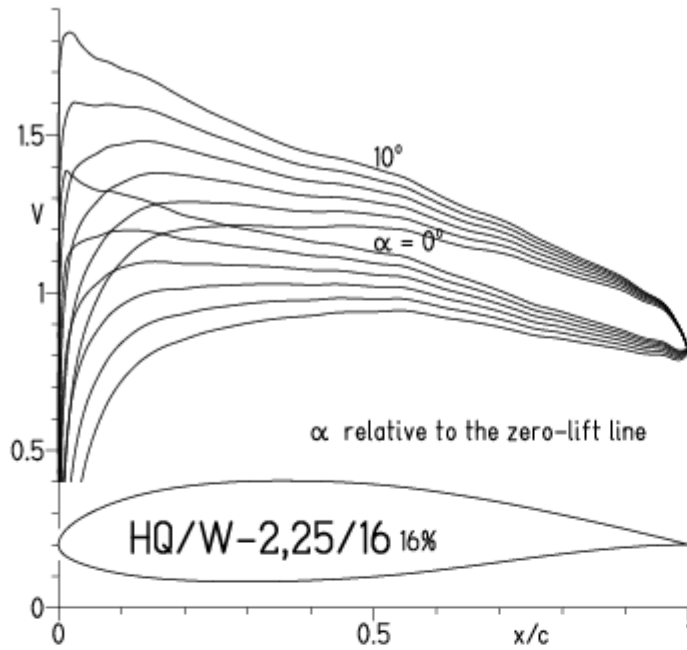
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

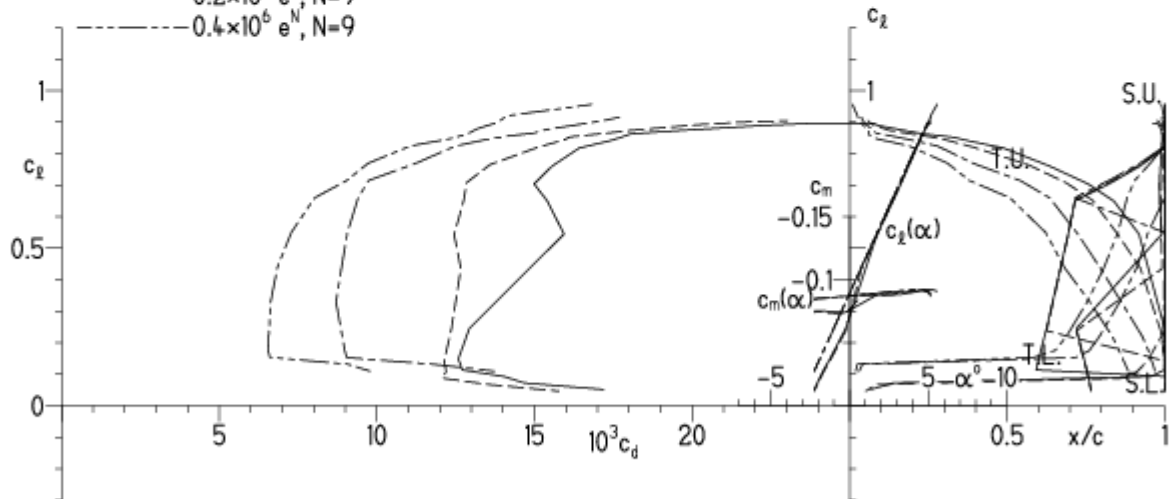
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

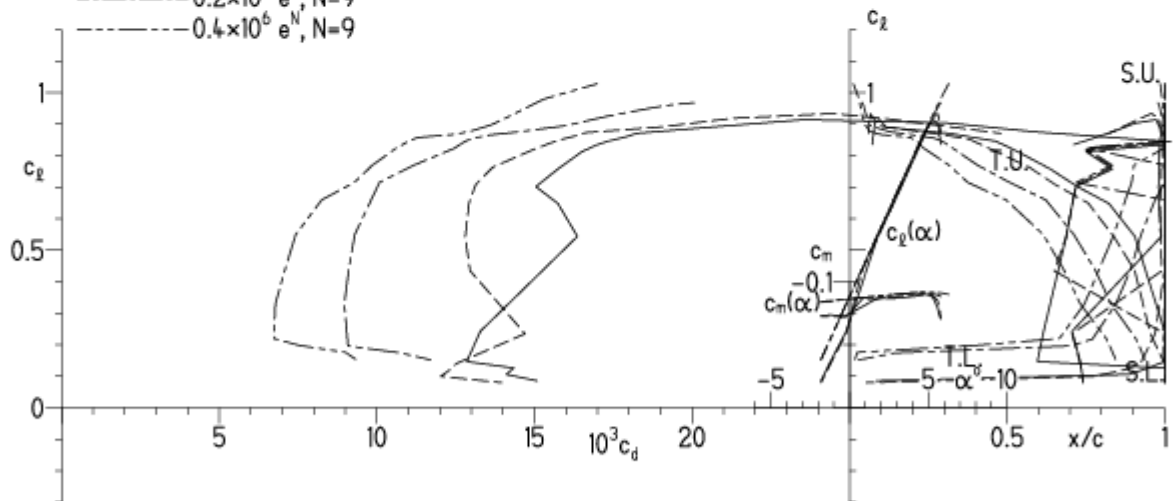
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

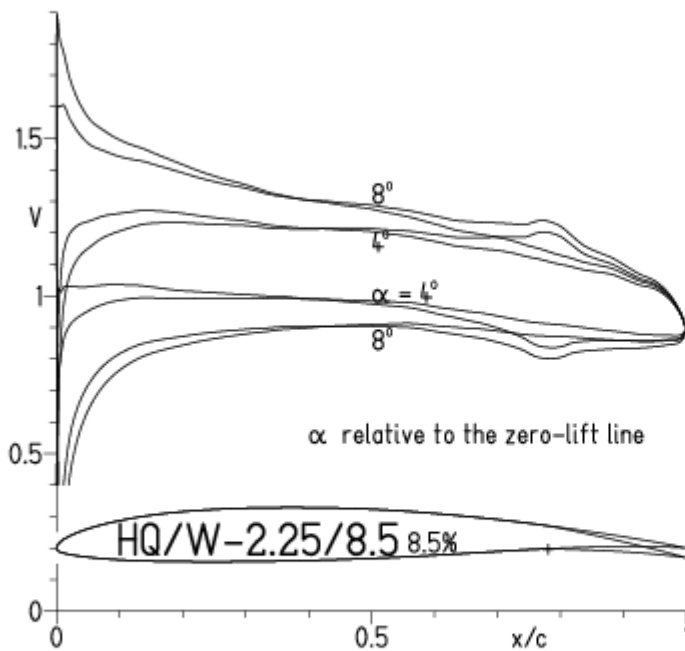
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

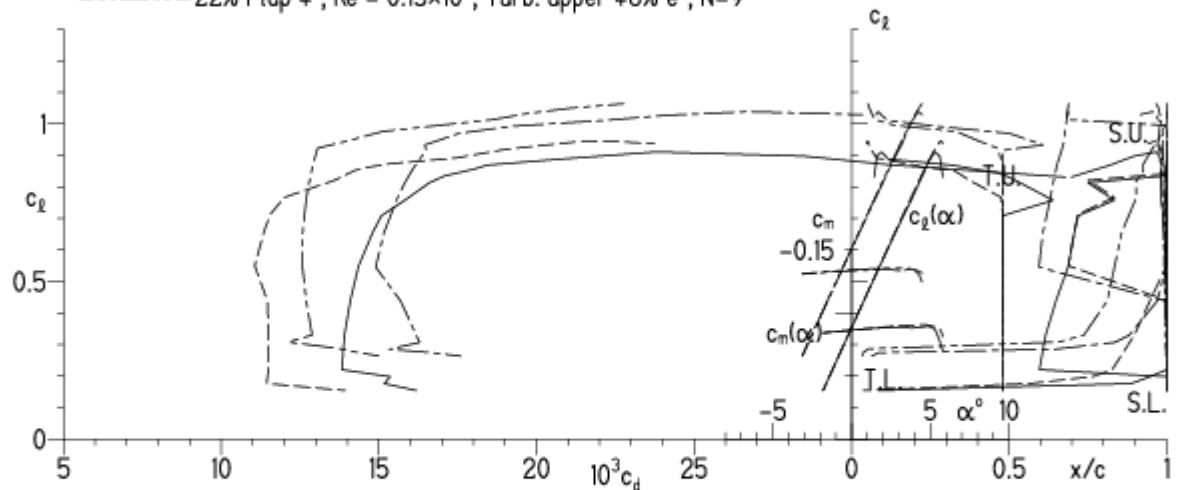


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

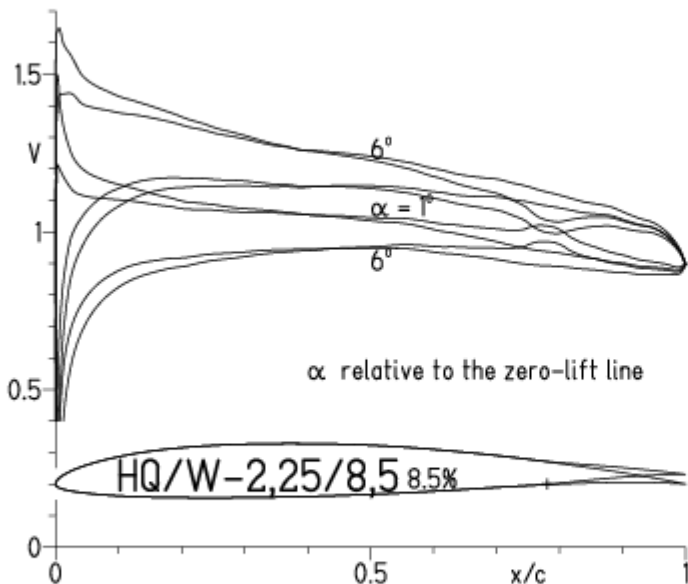
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\ 000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

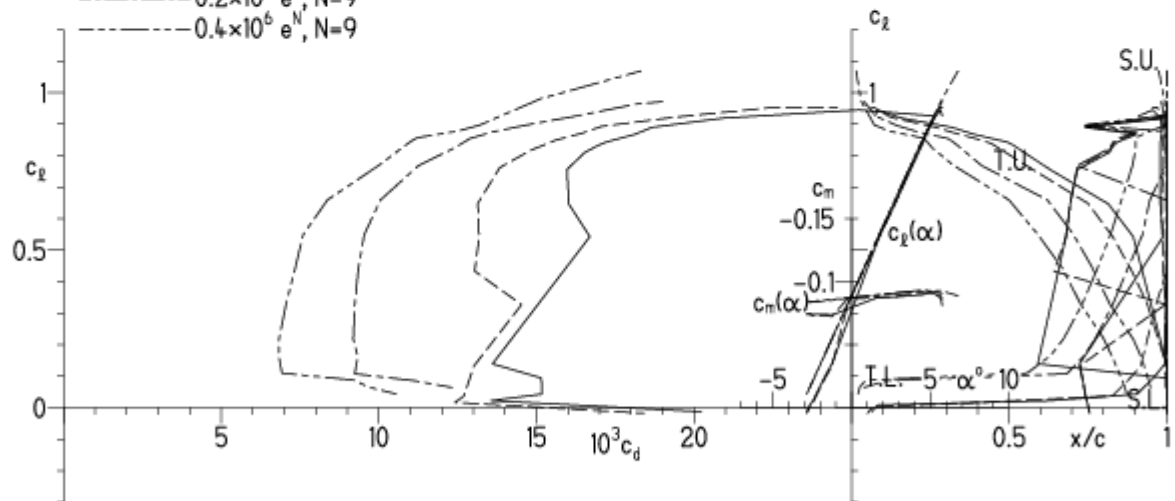
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

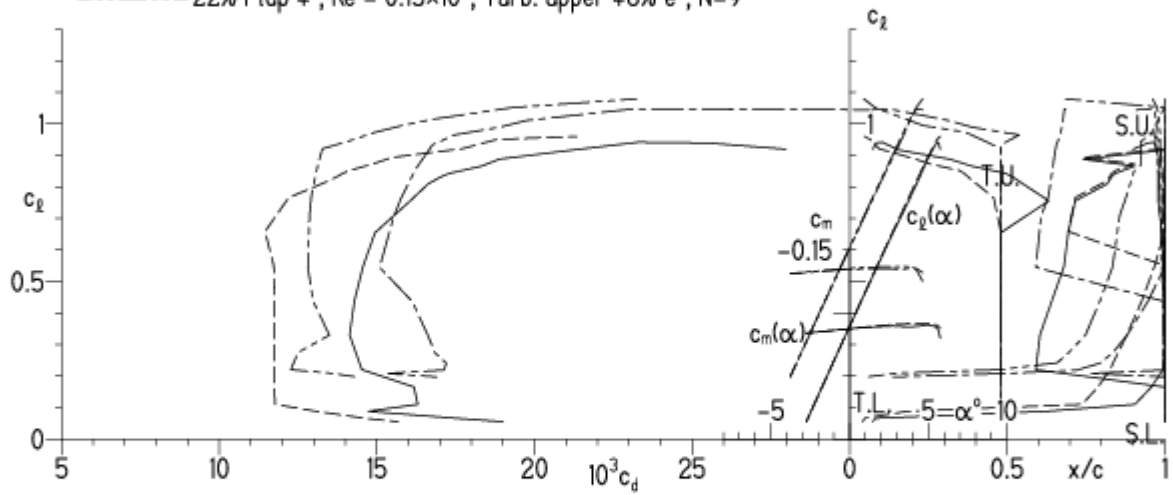


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17

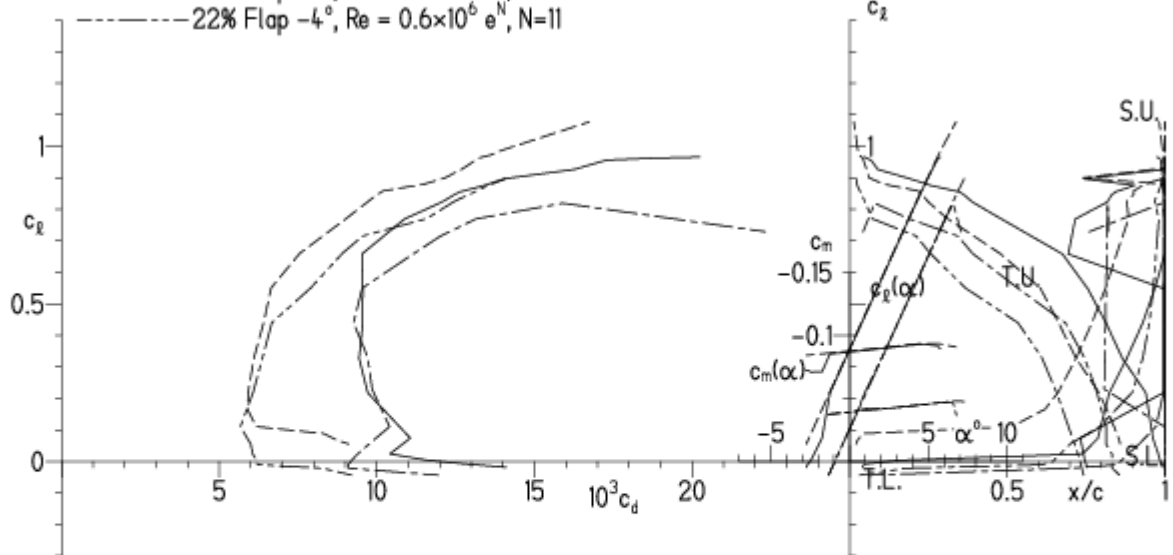


EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

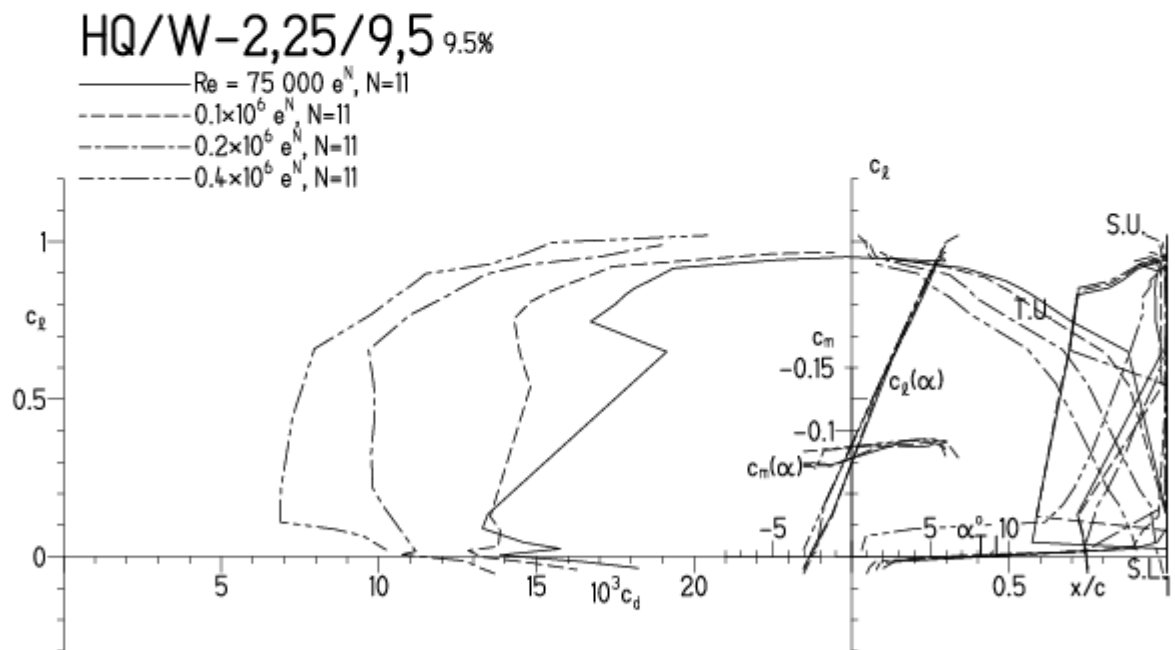


HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

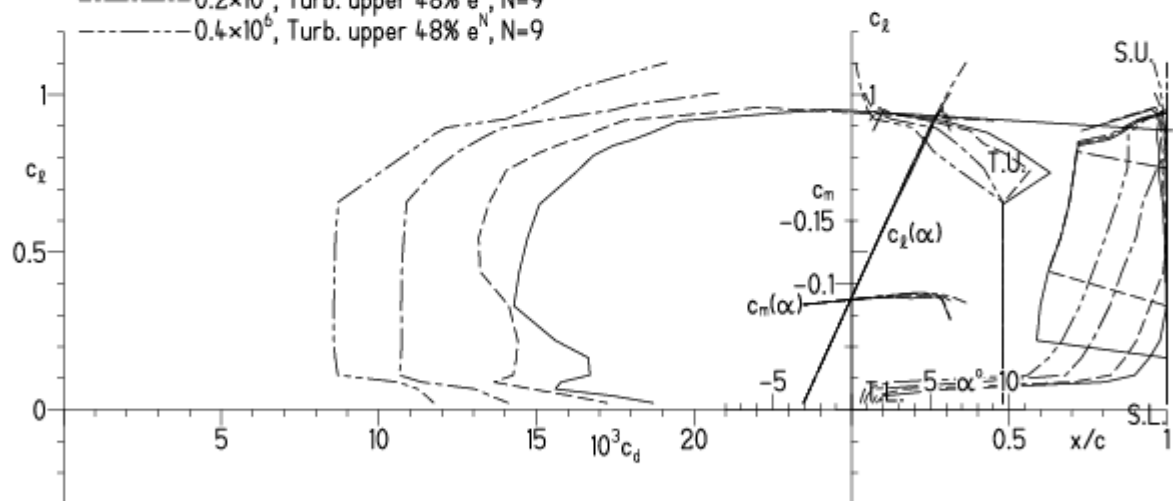
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

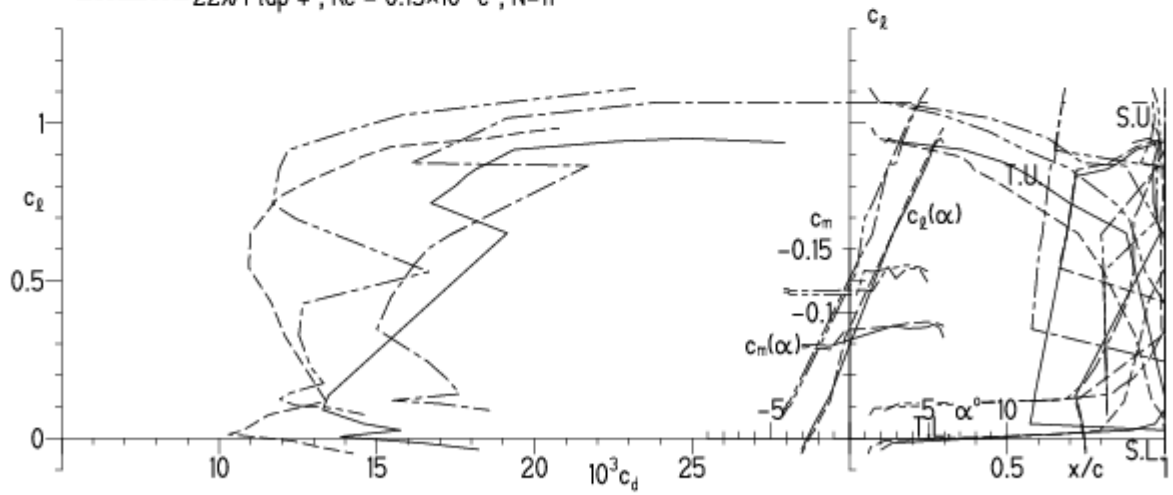


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

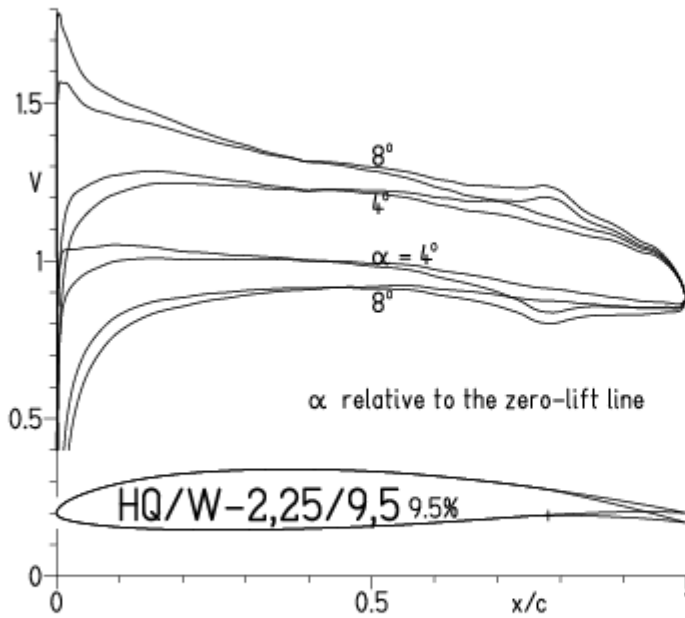
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

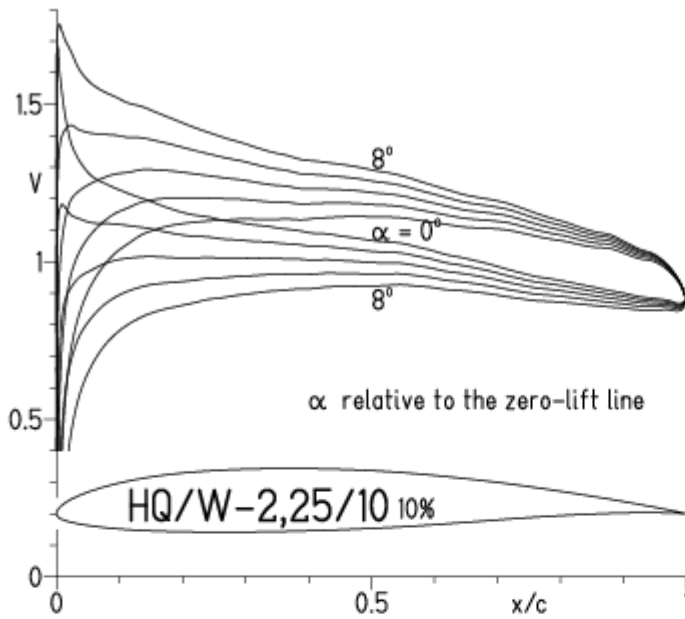


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

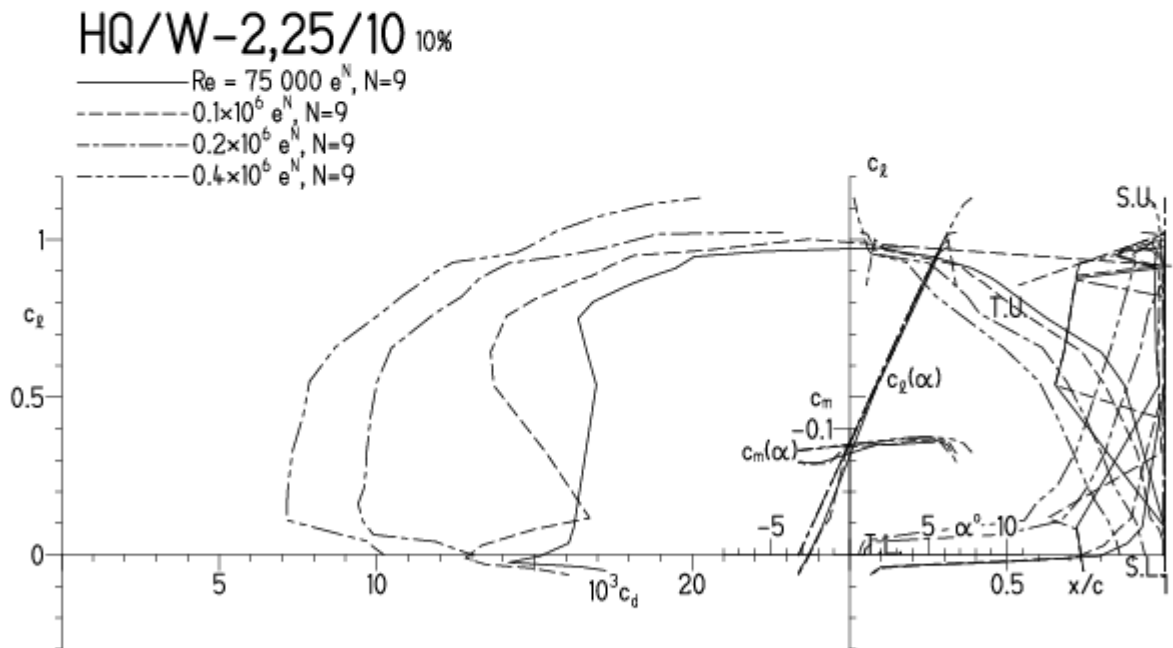


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

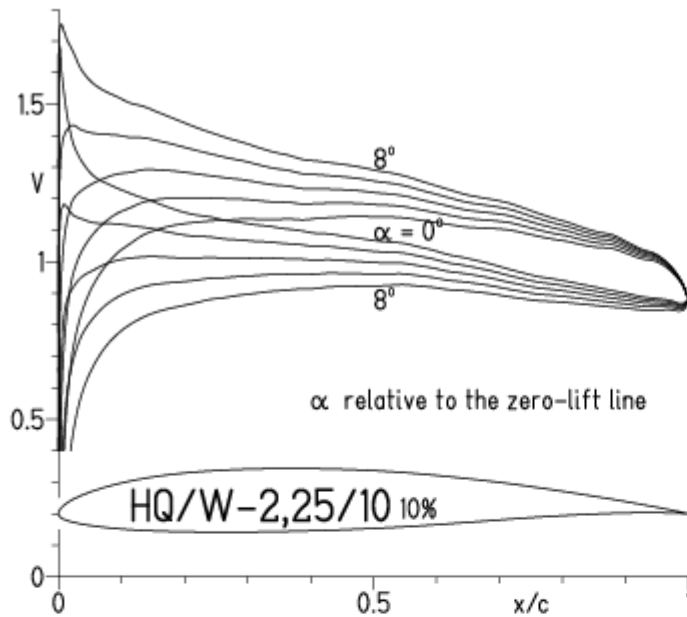


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

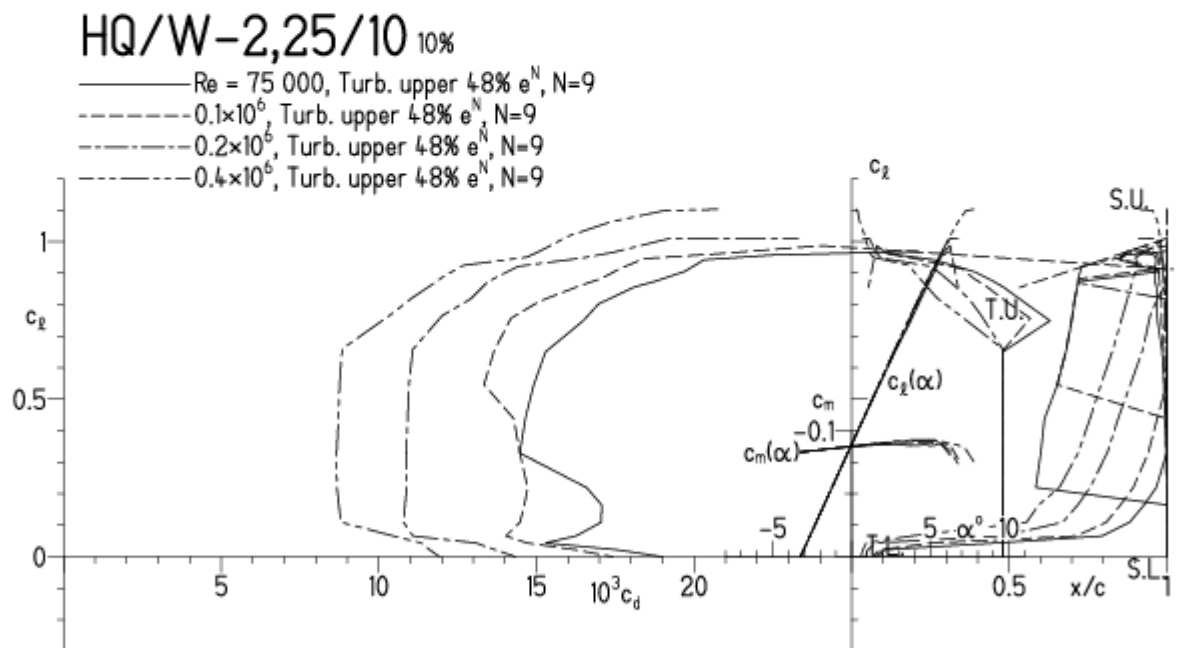


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

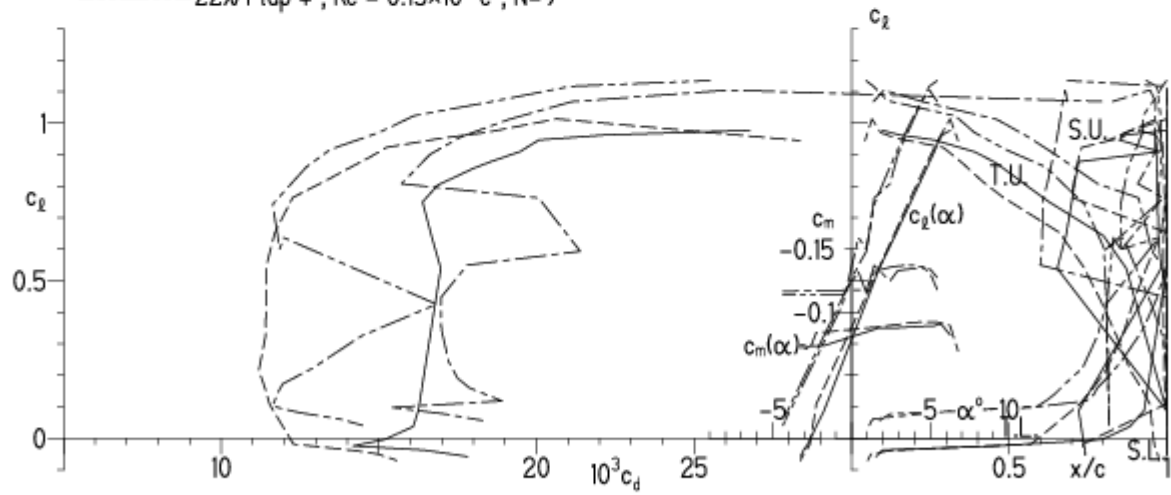


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

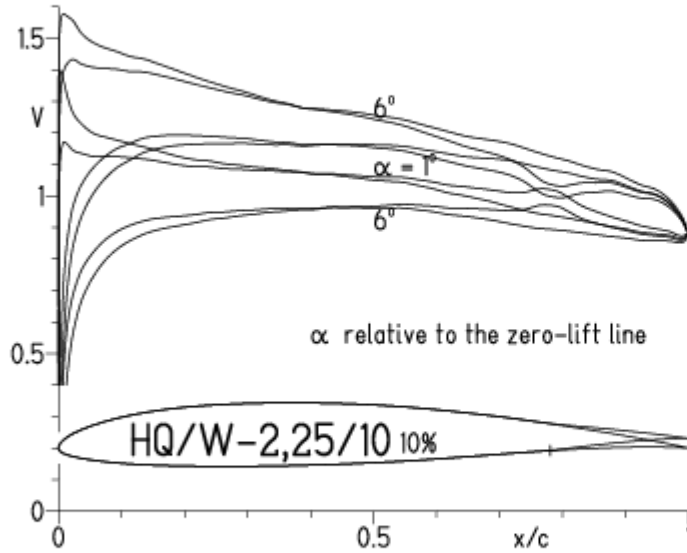
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

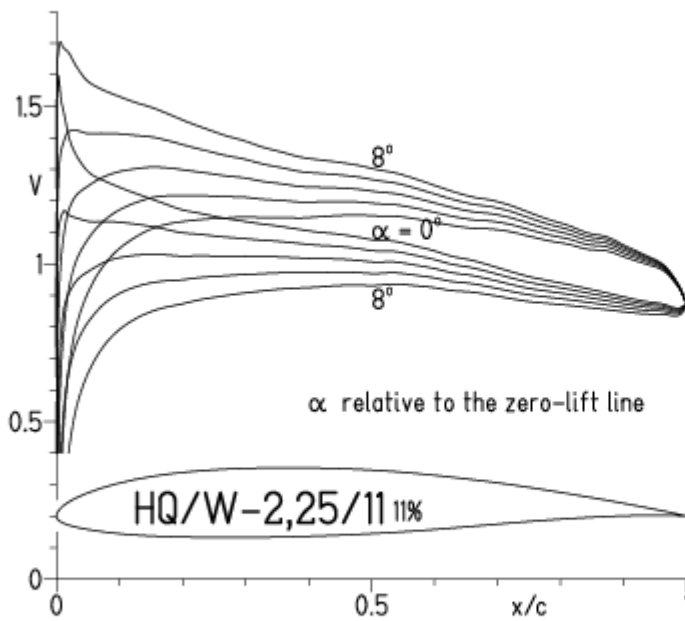


EPPLER 2005 V. 8.5.07 RUN

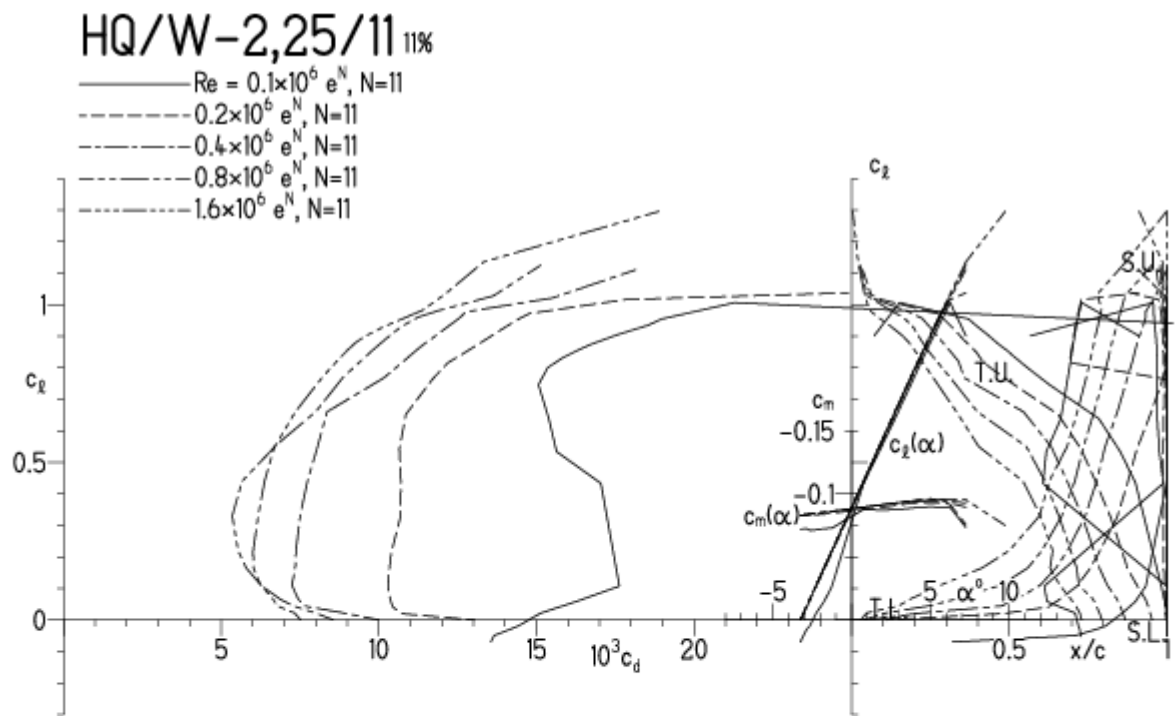


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

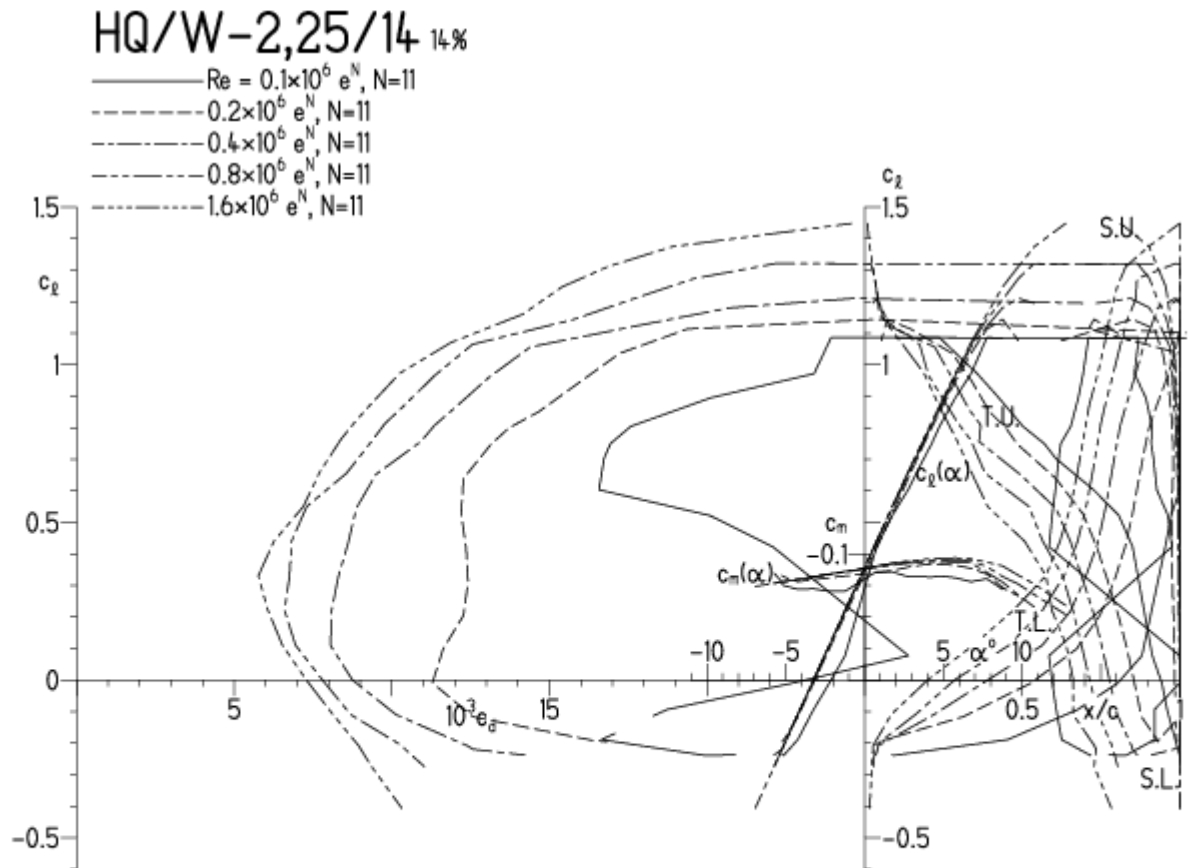


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

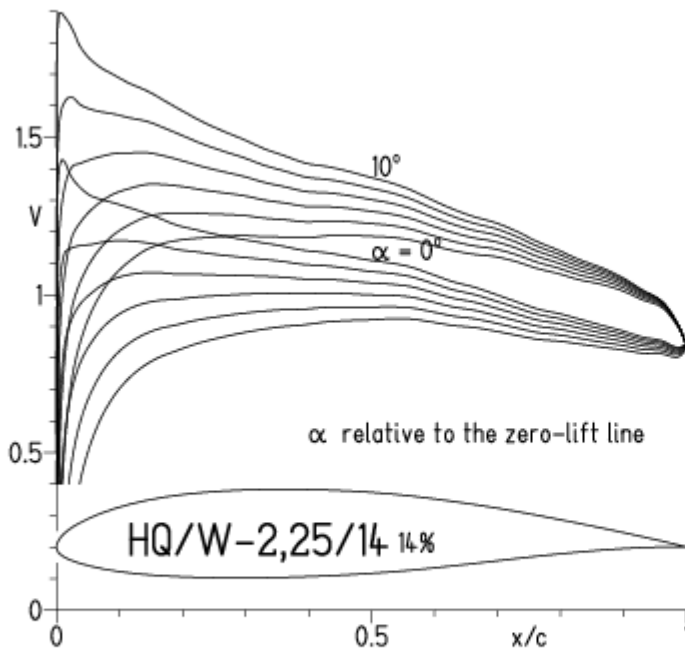


EPPLER 2005 V. 8.

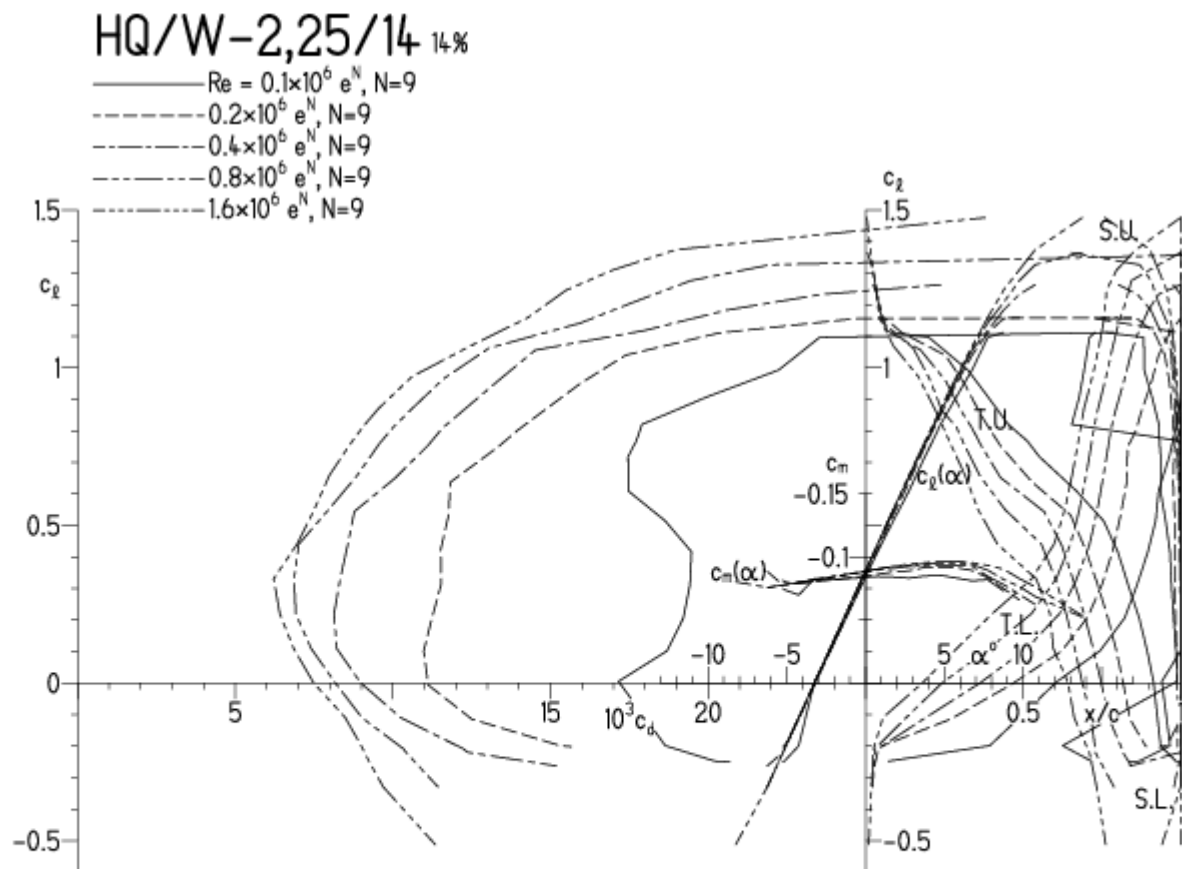


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

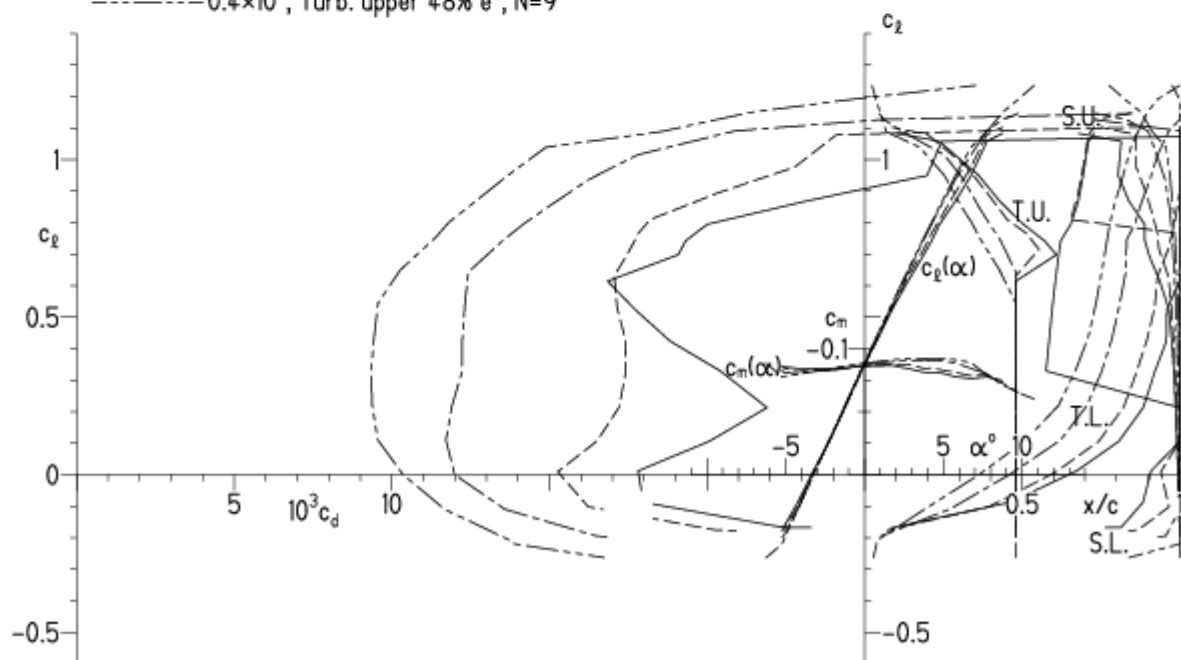
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

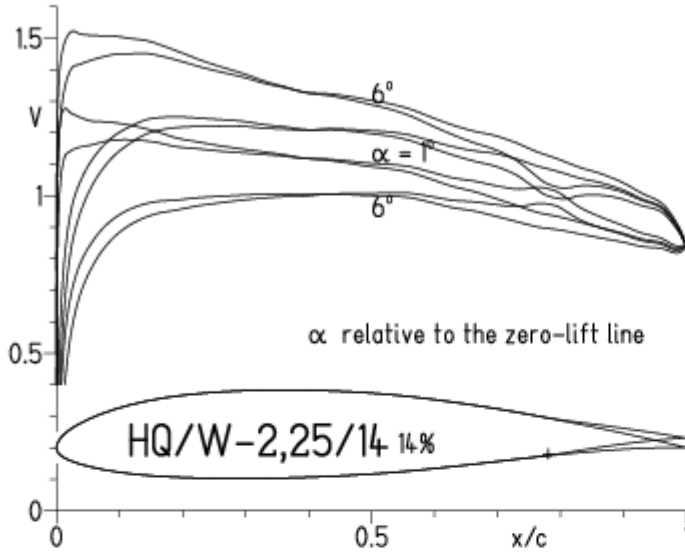
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

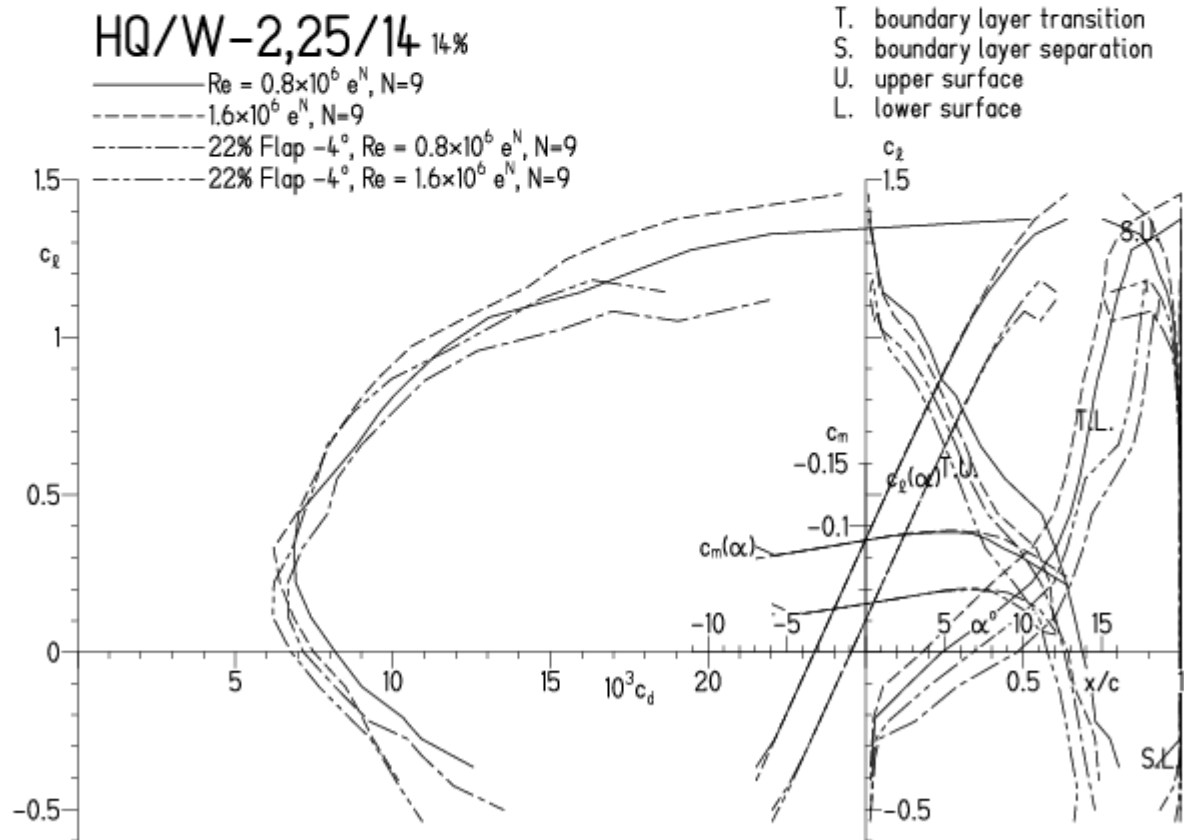


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

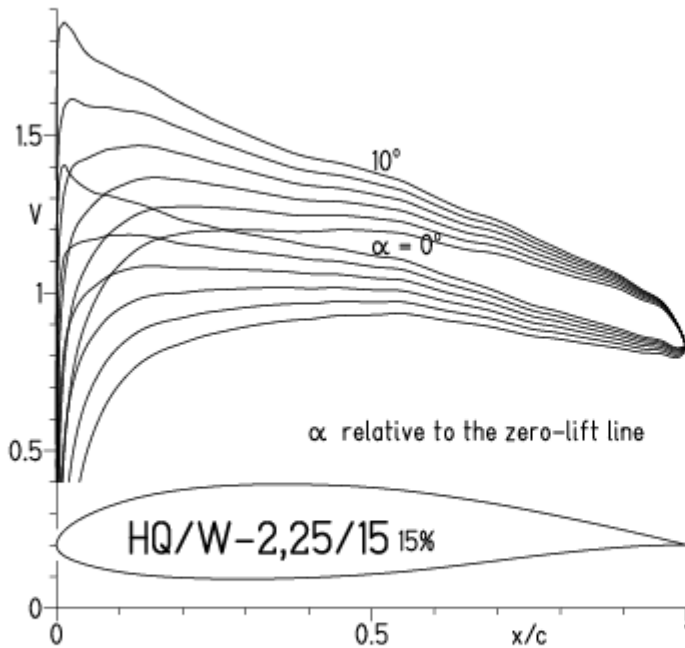


EPPLER 2005 V. 8.5.07

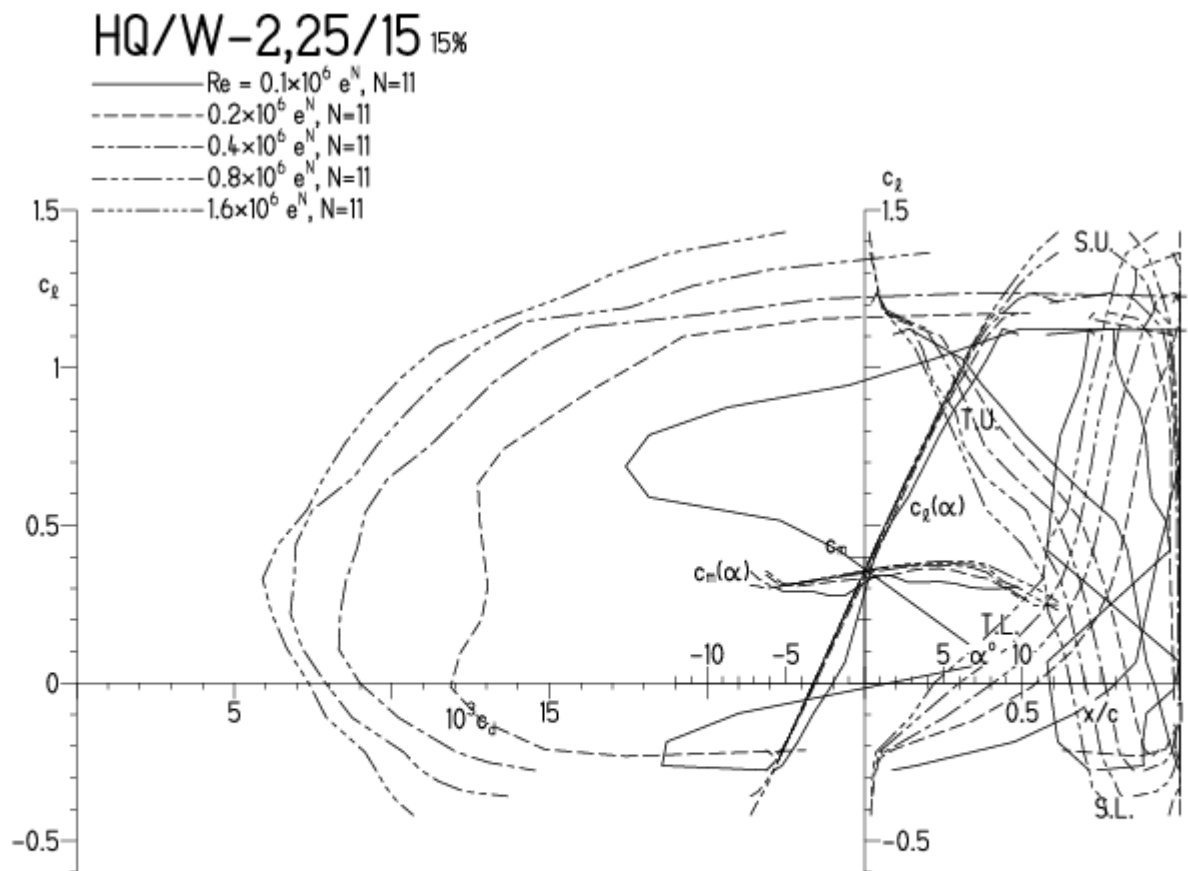


HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

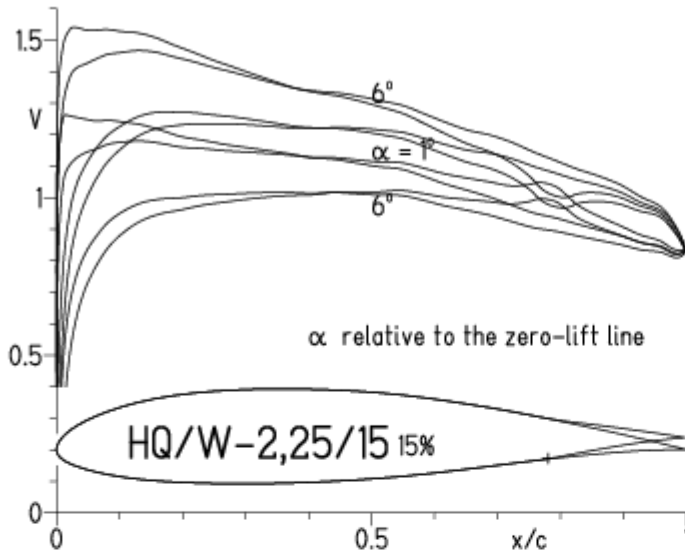


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

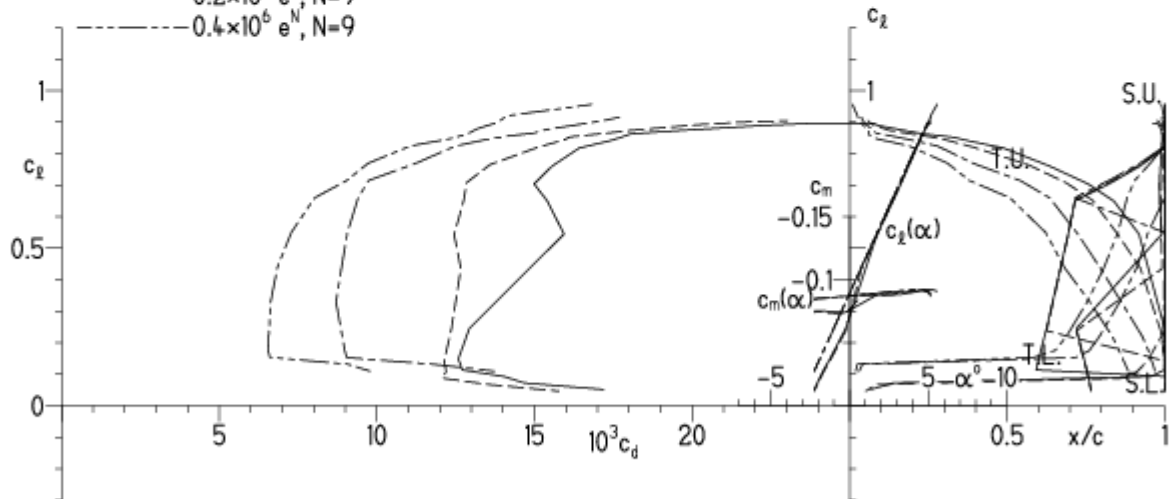
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

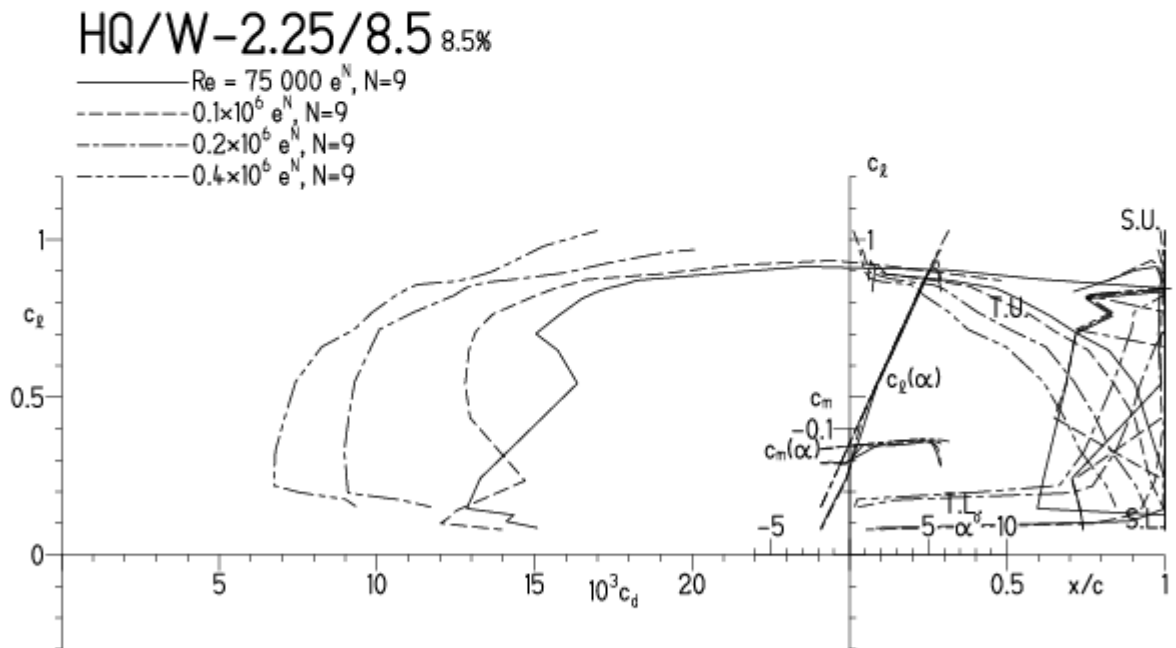


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

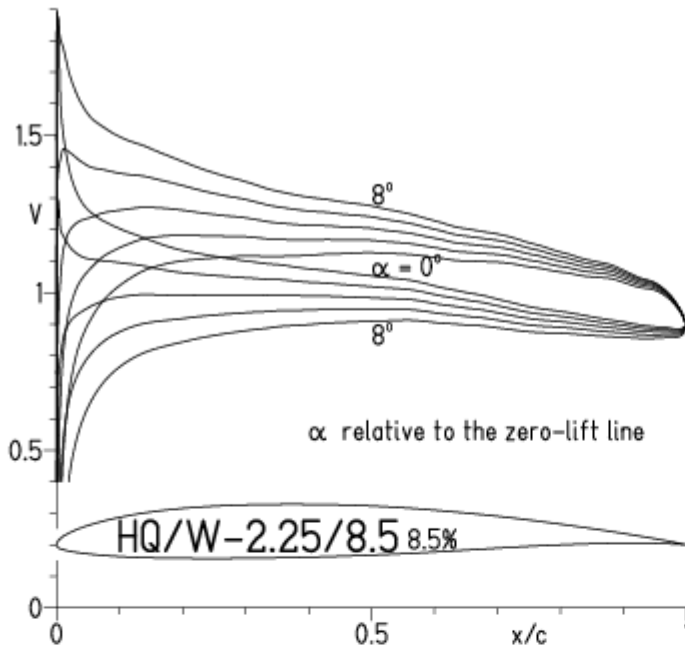


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

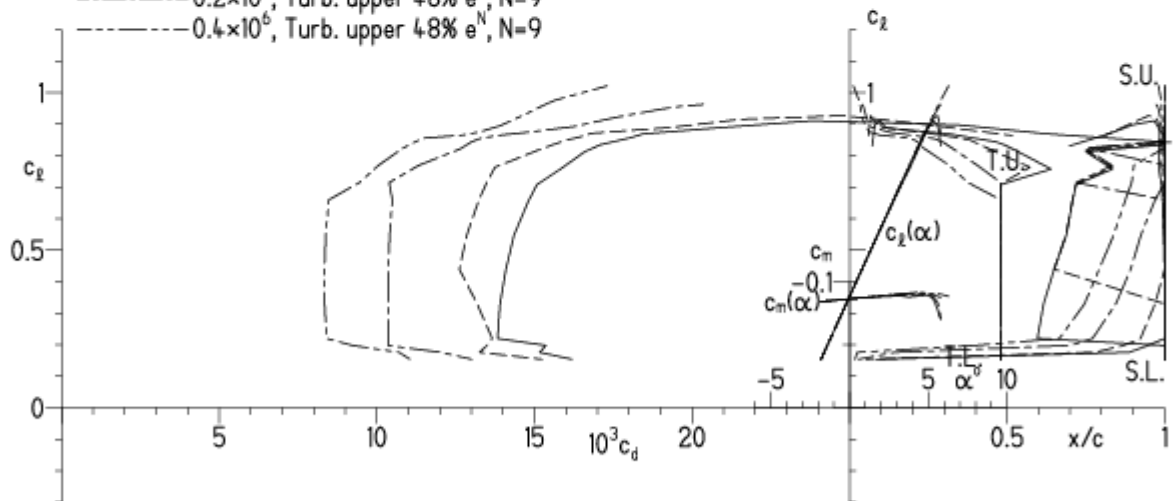
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

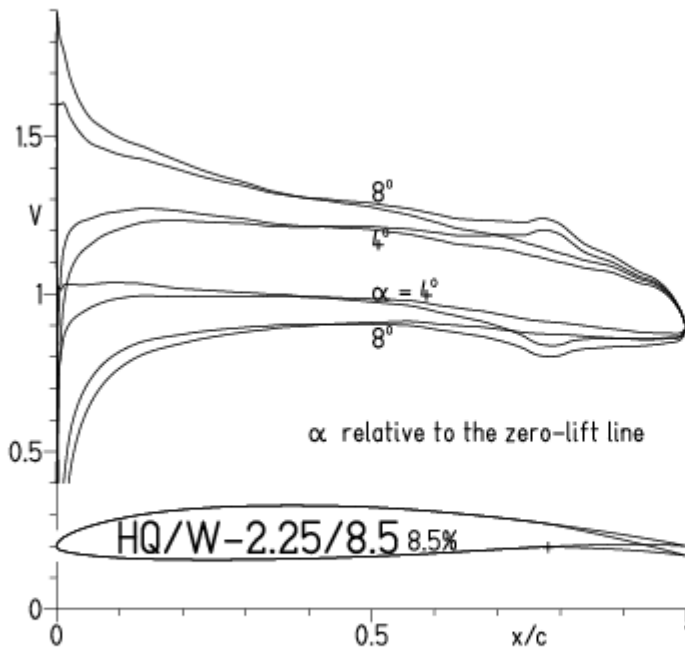
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

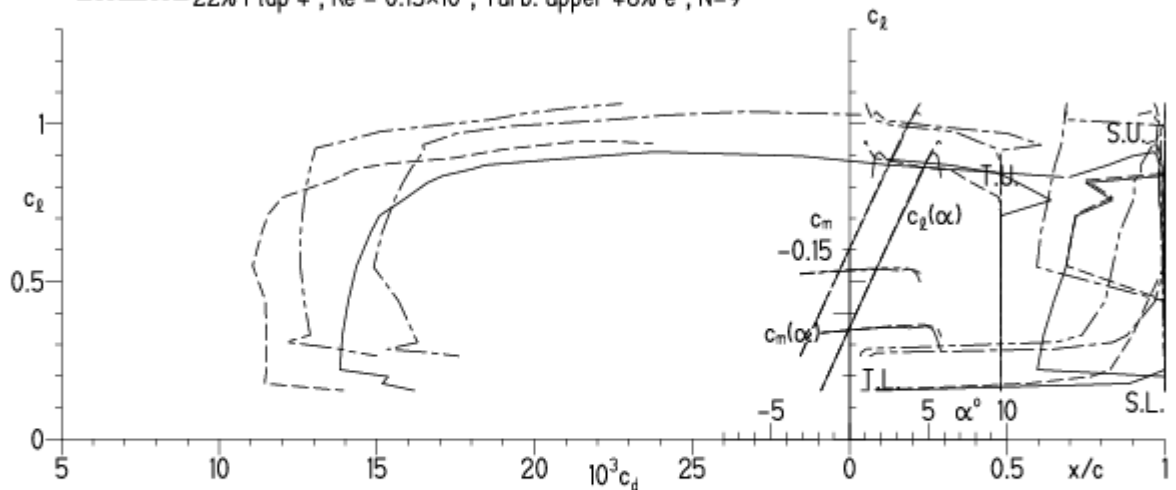


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15 × 10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

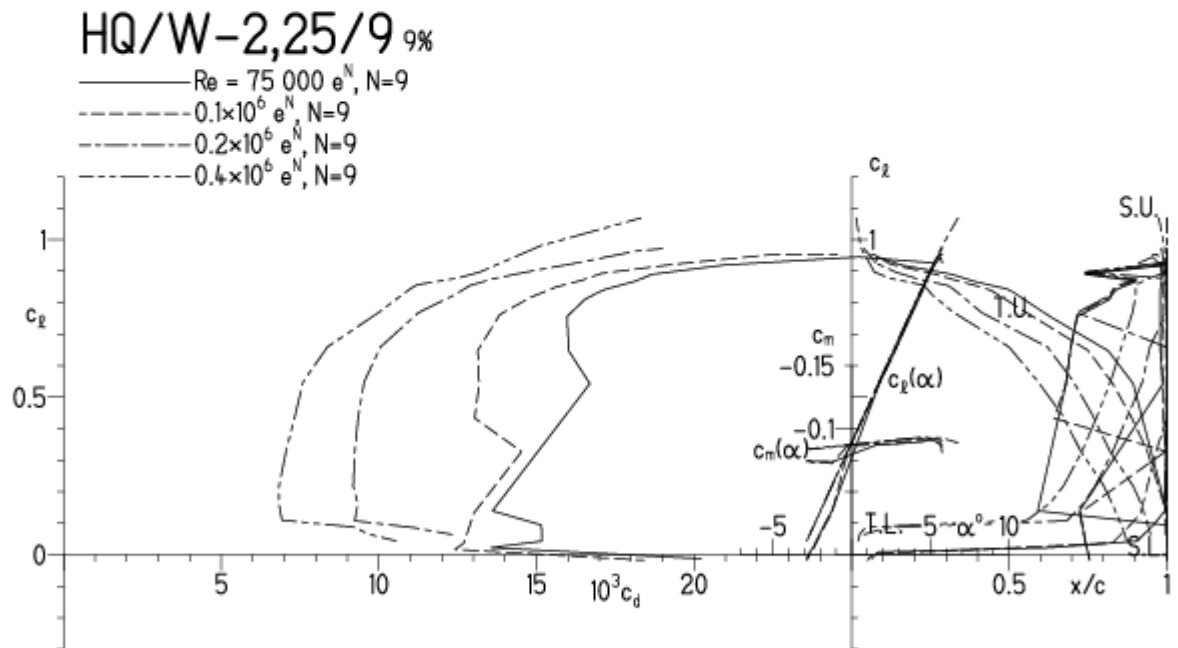


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

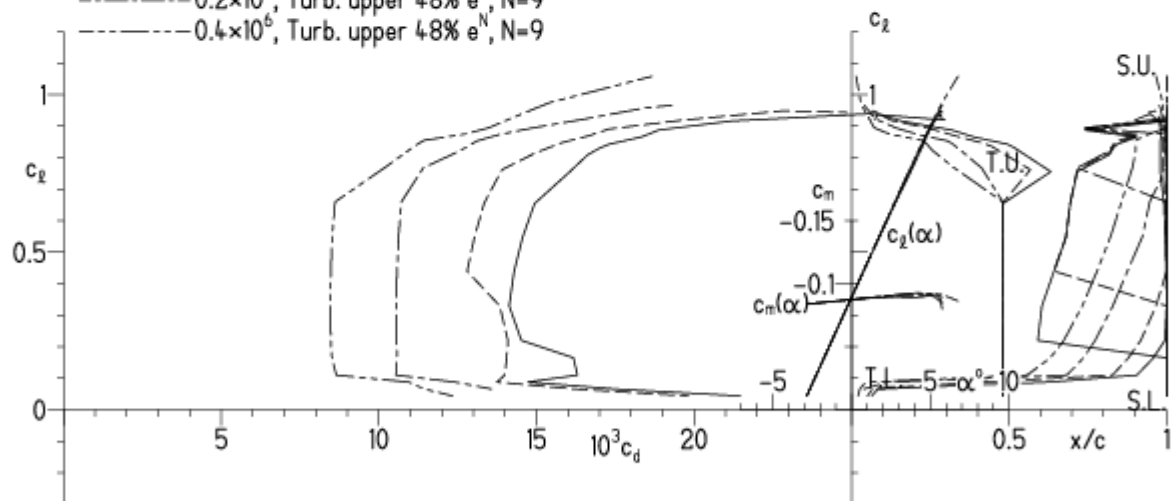
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17

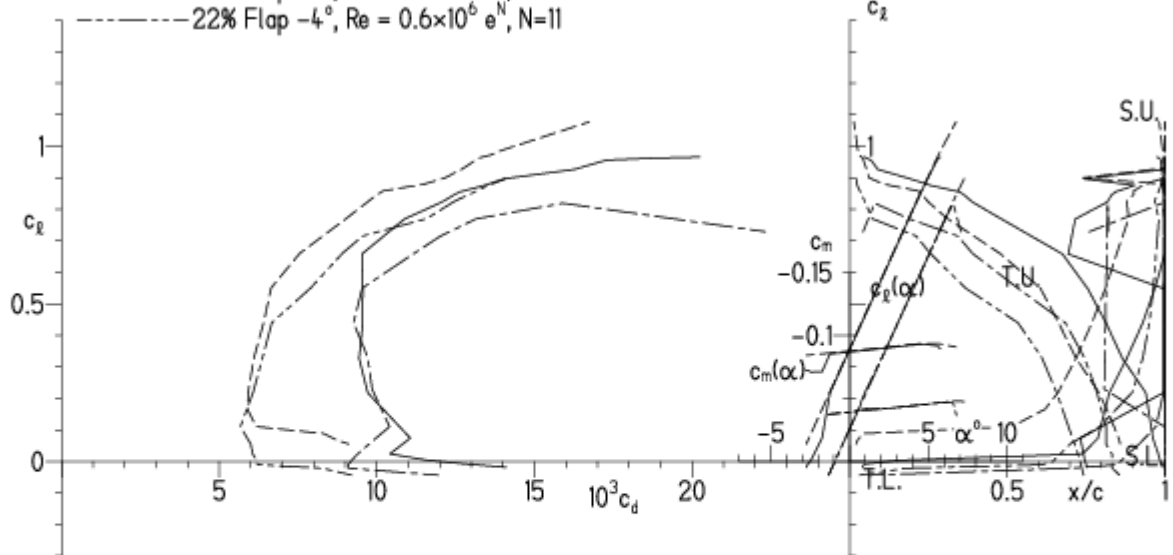


EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

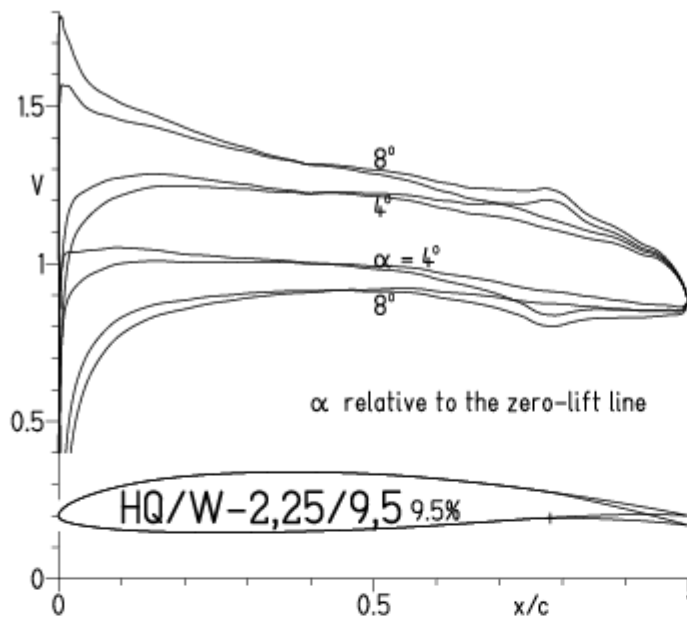
- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
(Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

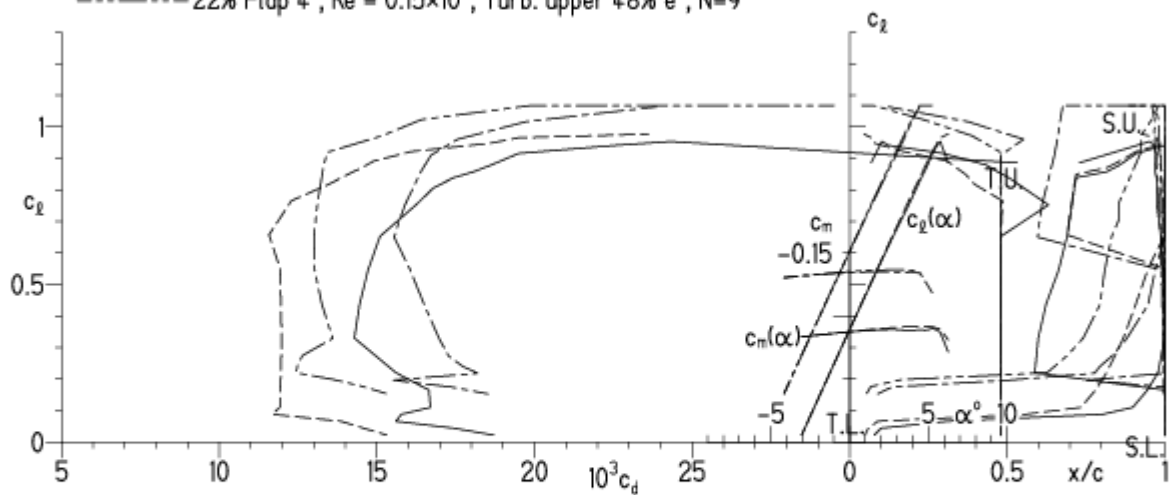


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



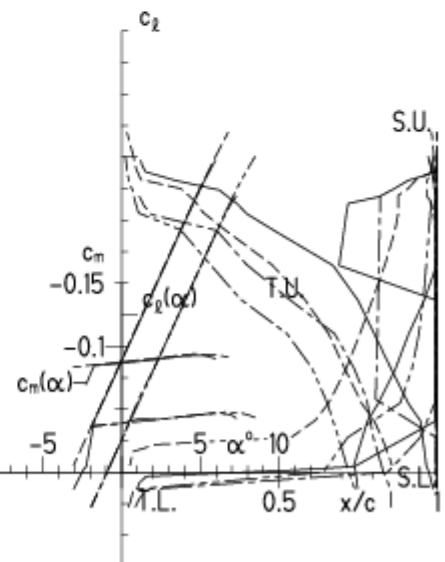
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

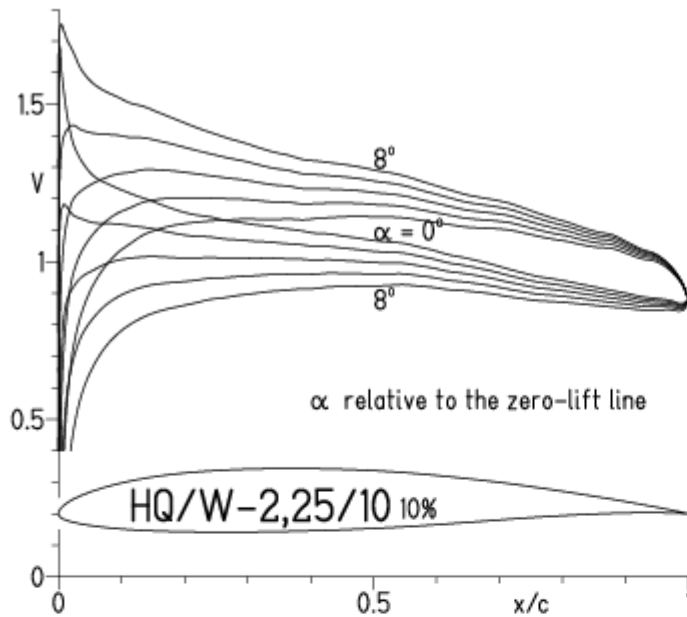


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

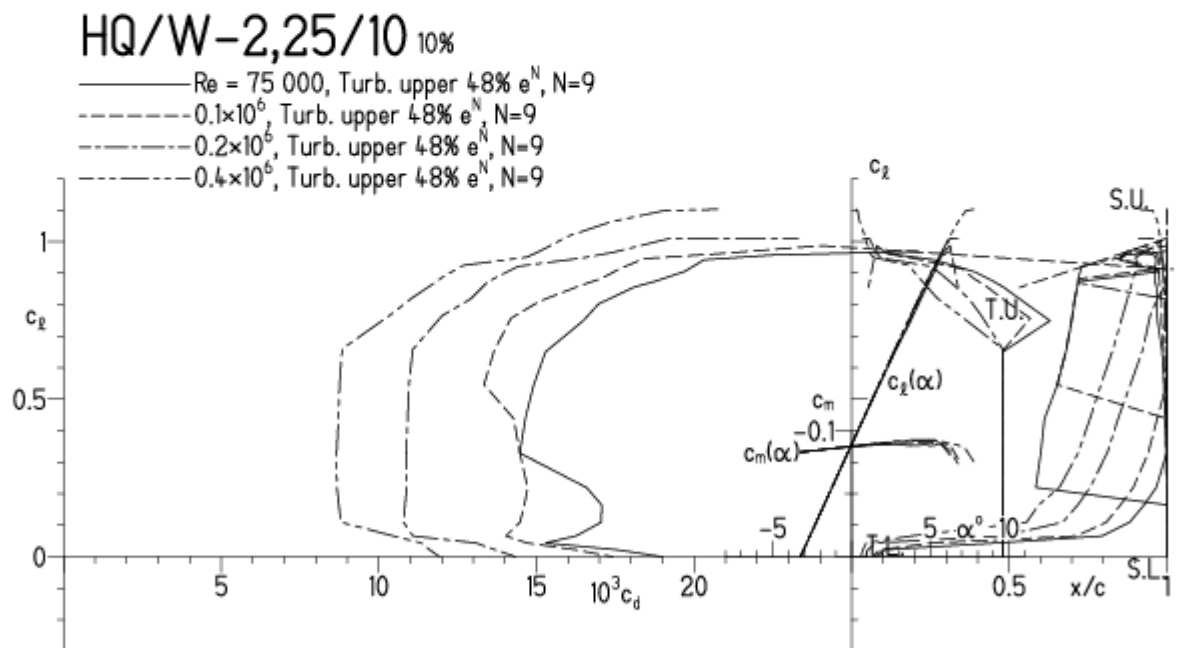


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

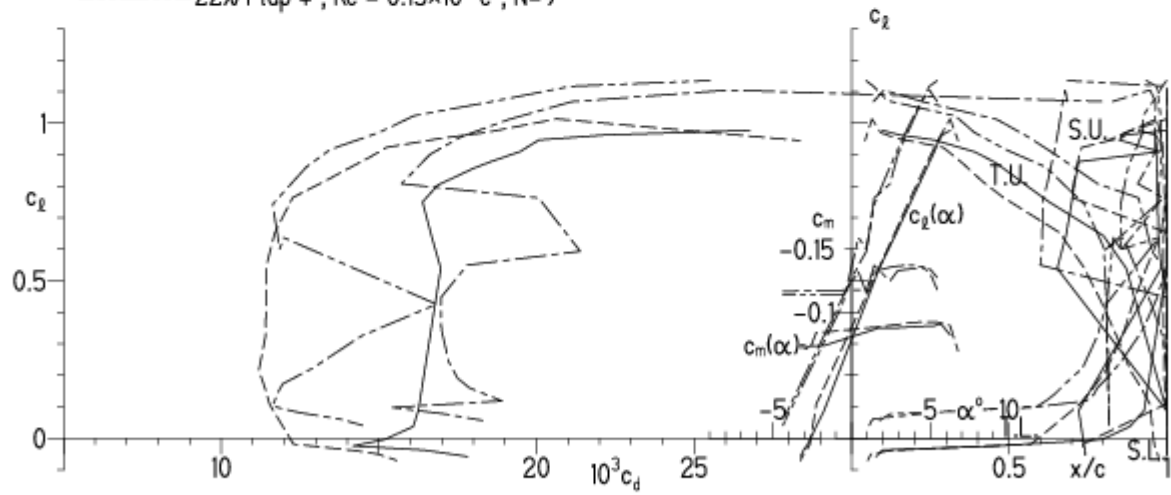


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

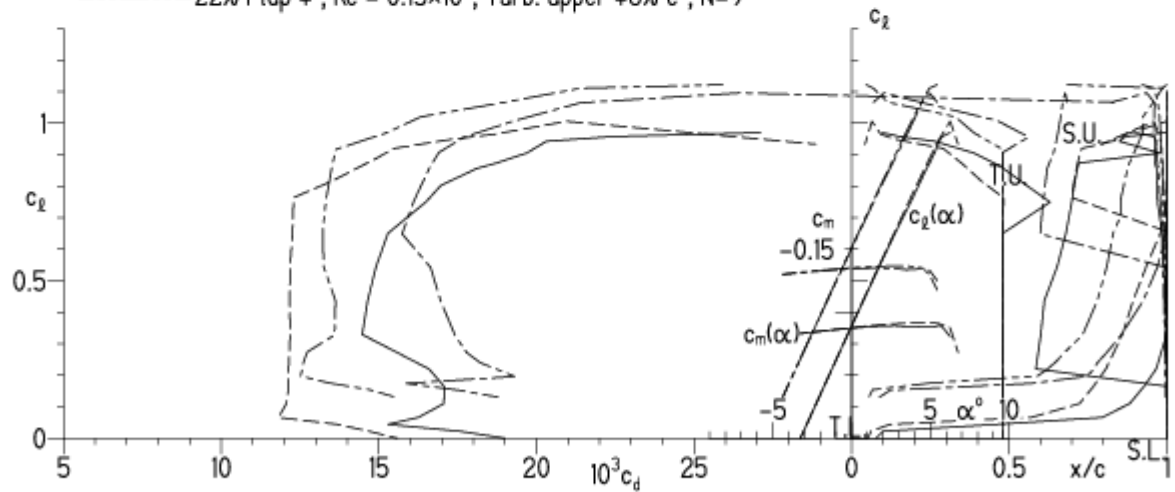


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

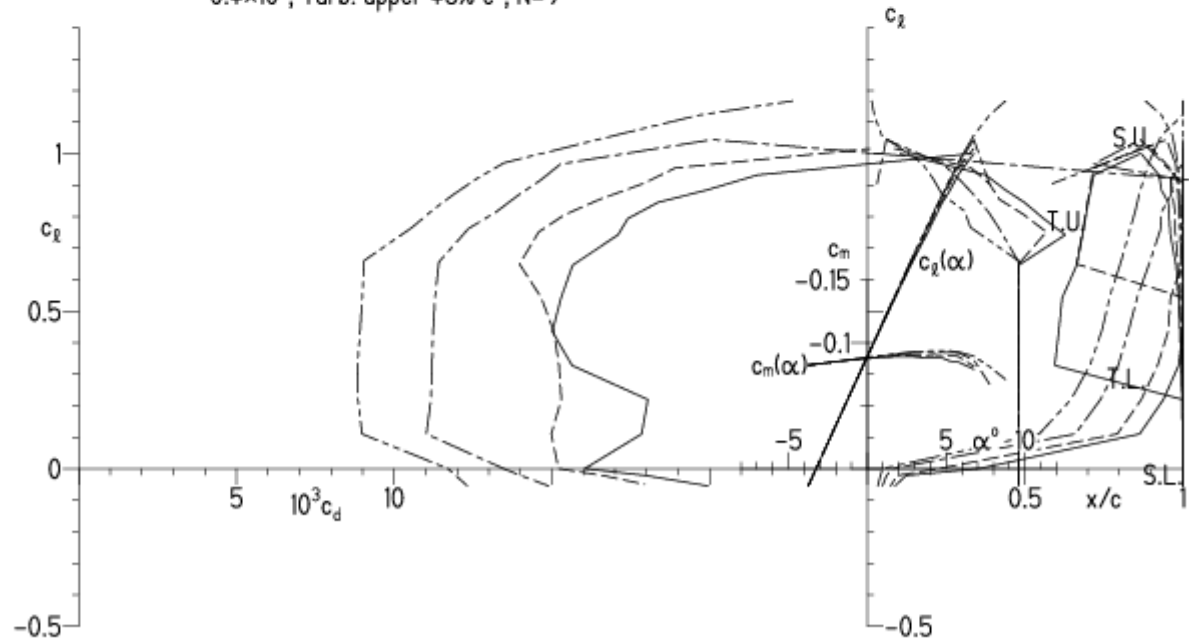
EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - $0.8 \times 10^6 e^N, N=11$
- · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

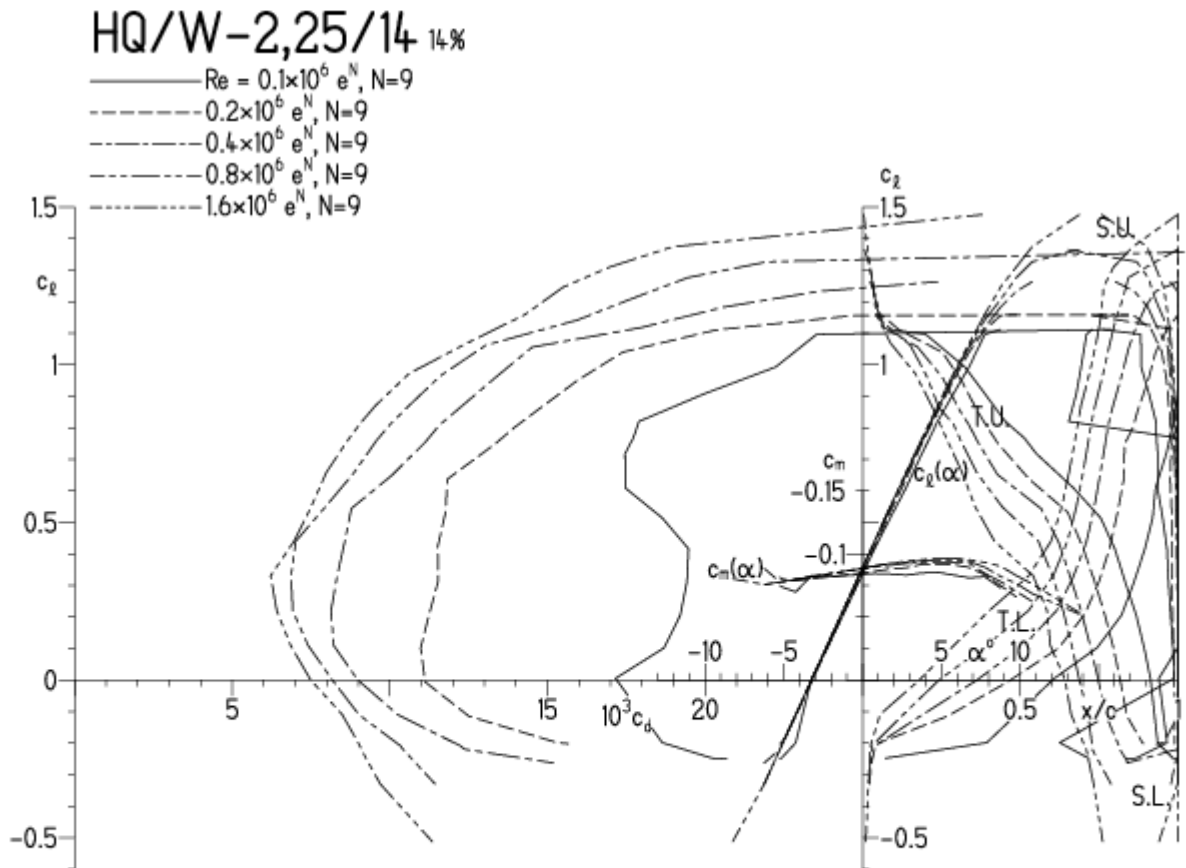


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

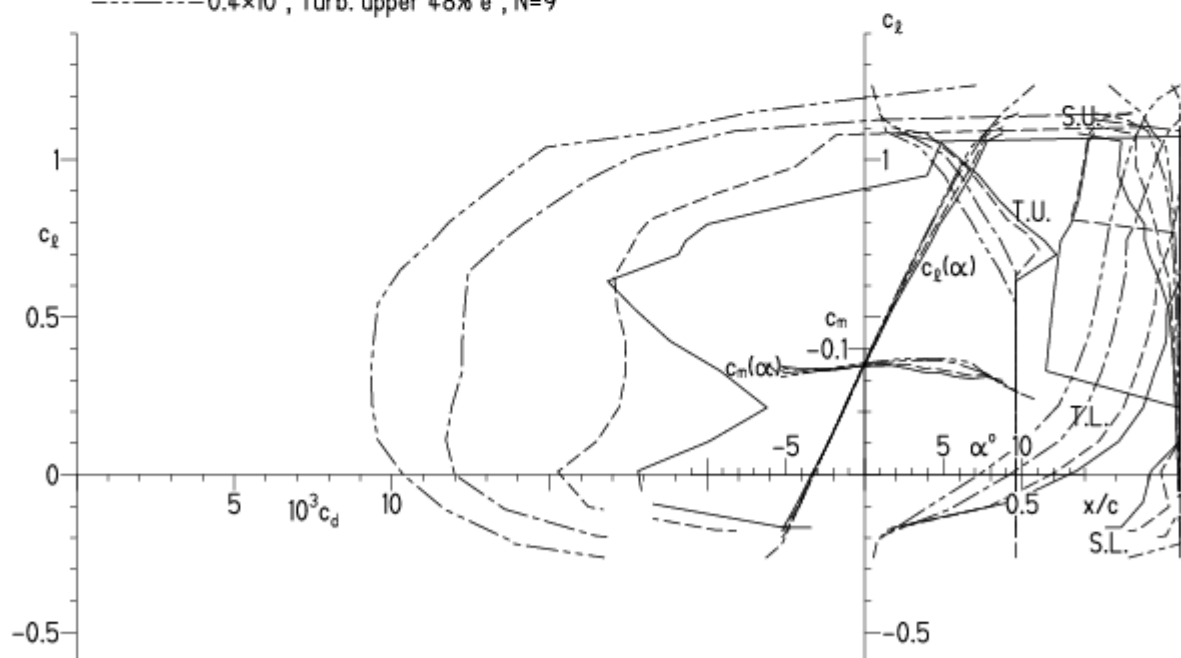
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31

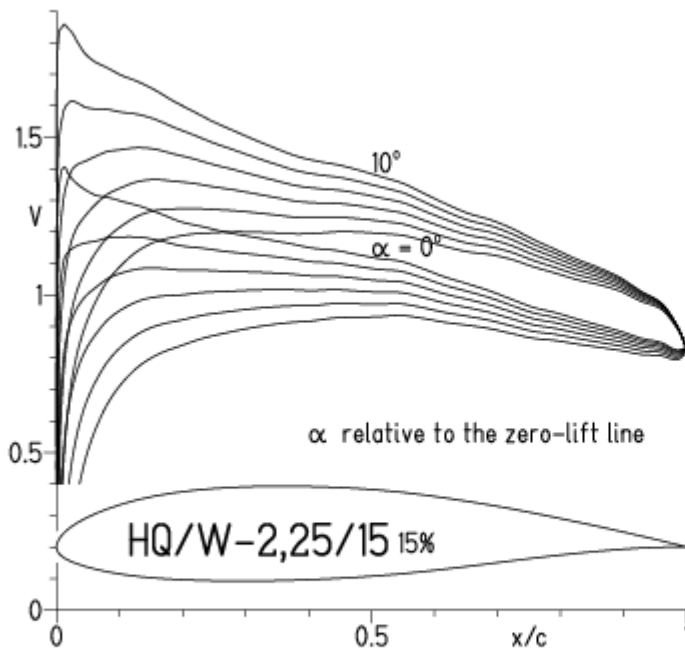


EPPLER 20

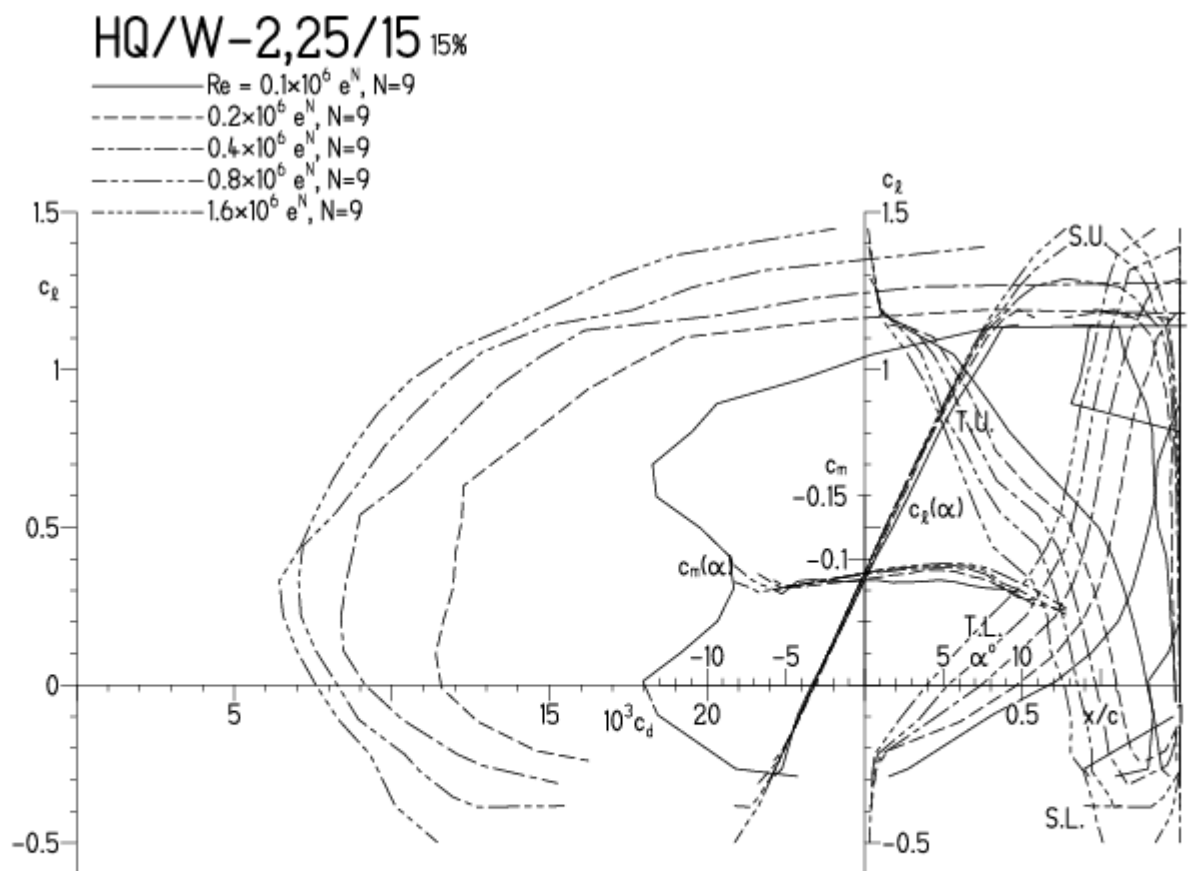


HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



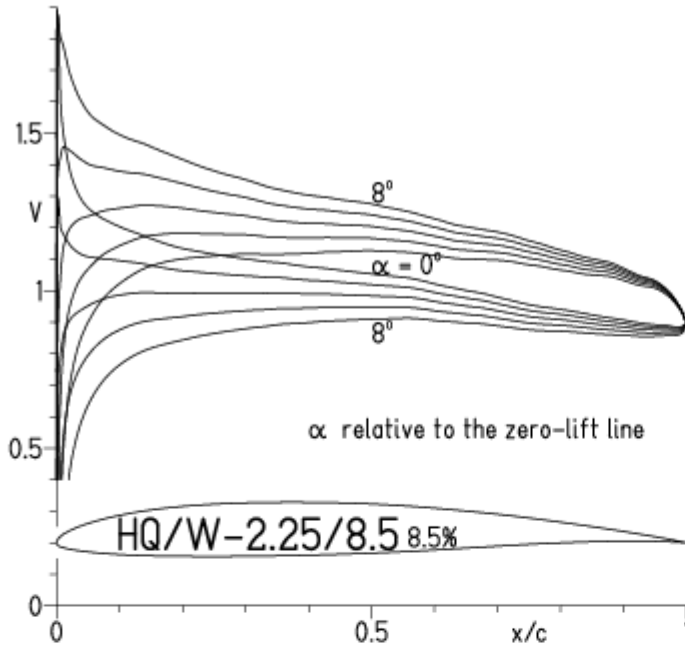
EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

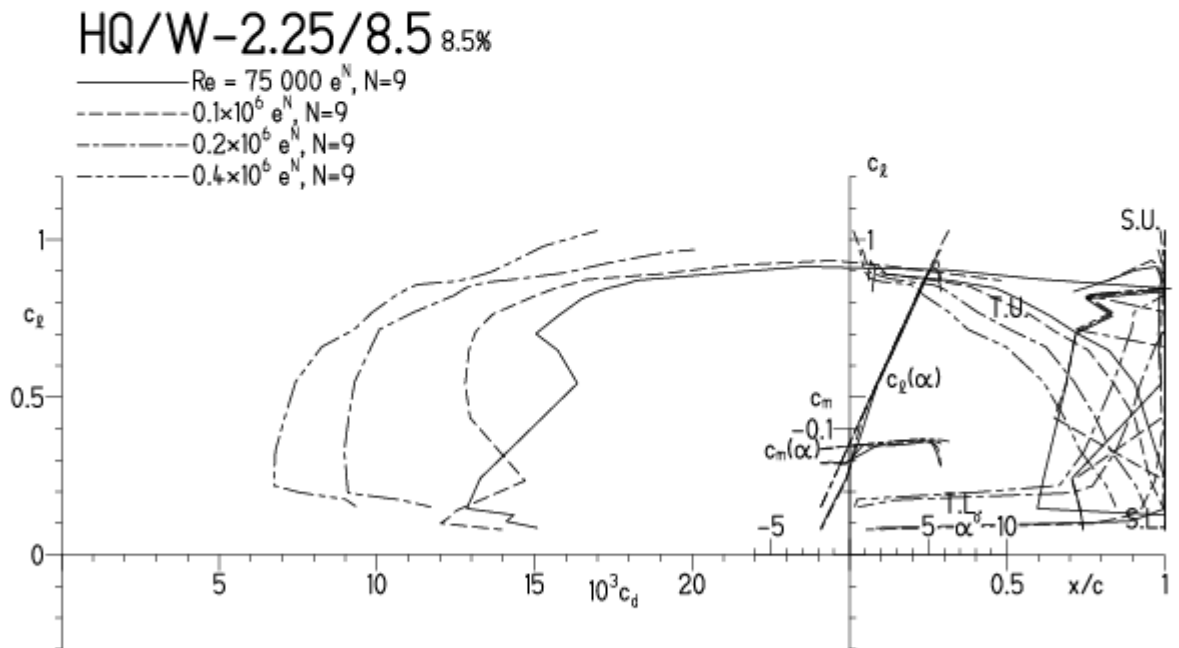


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

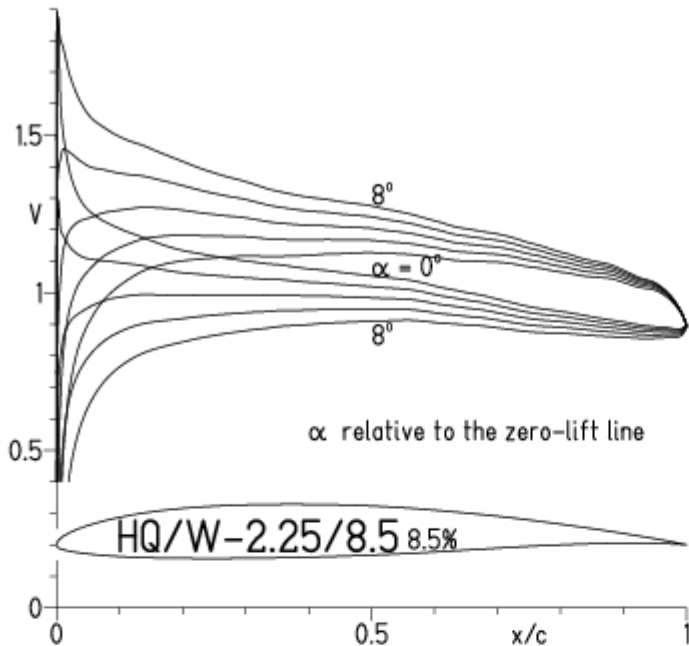


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

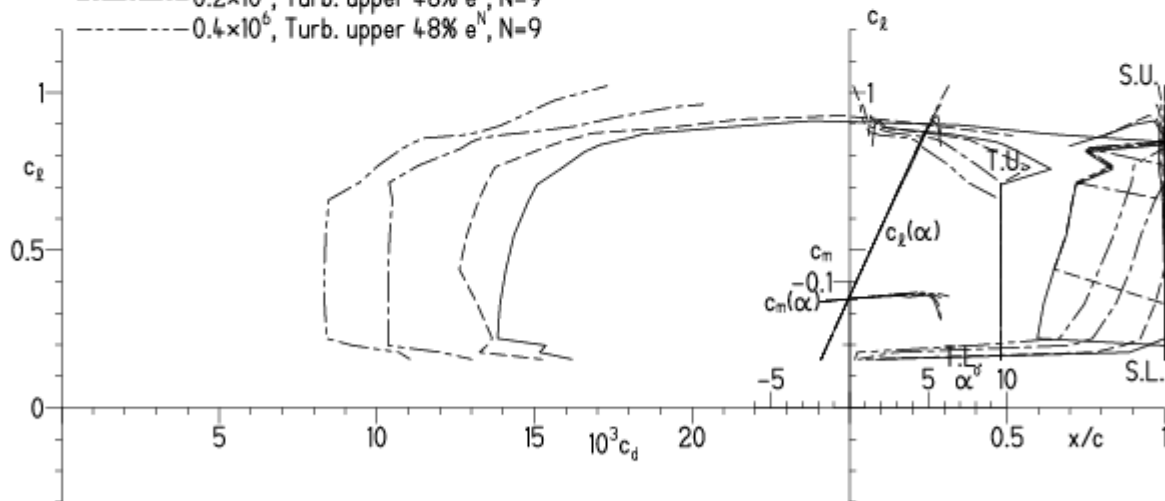
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

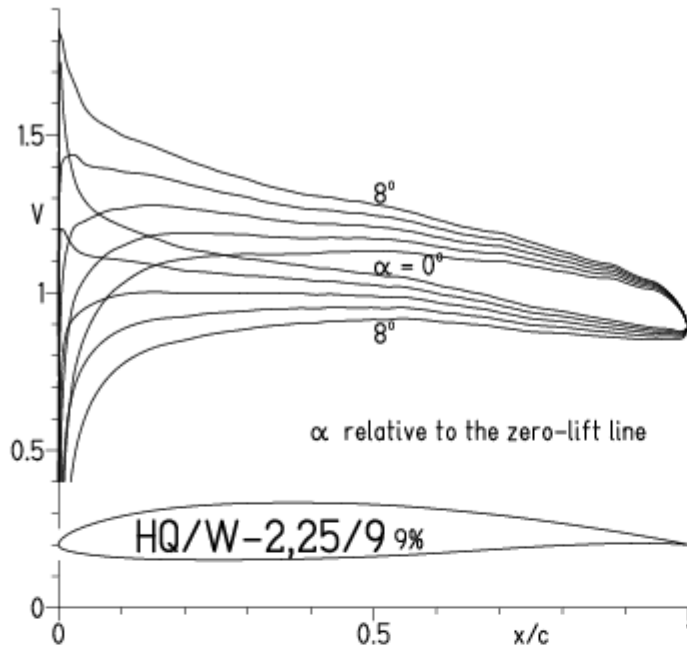


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

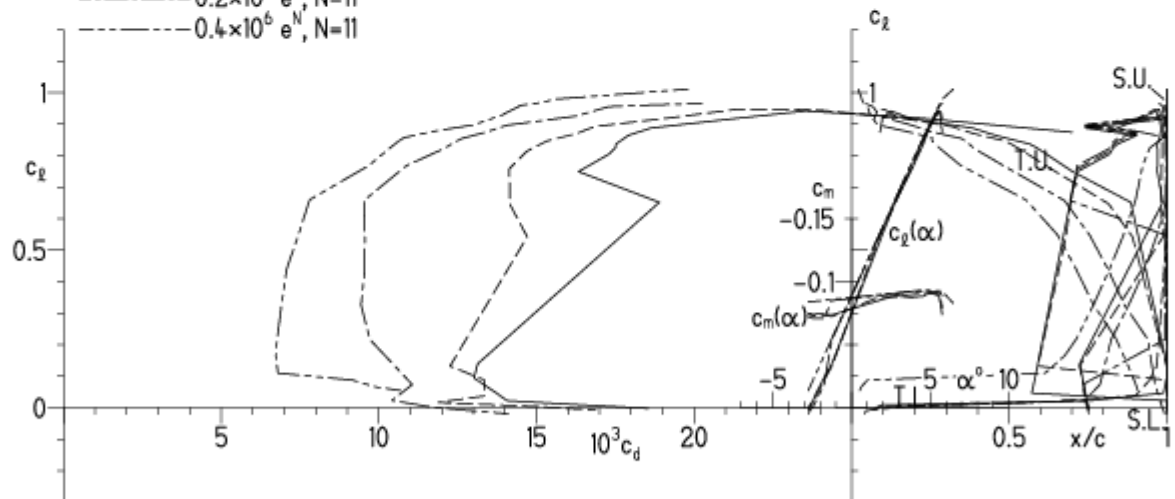
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

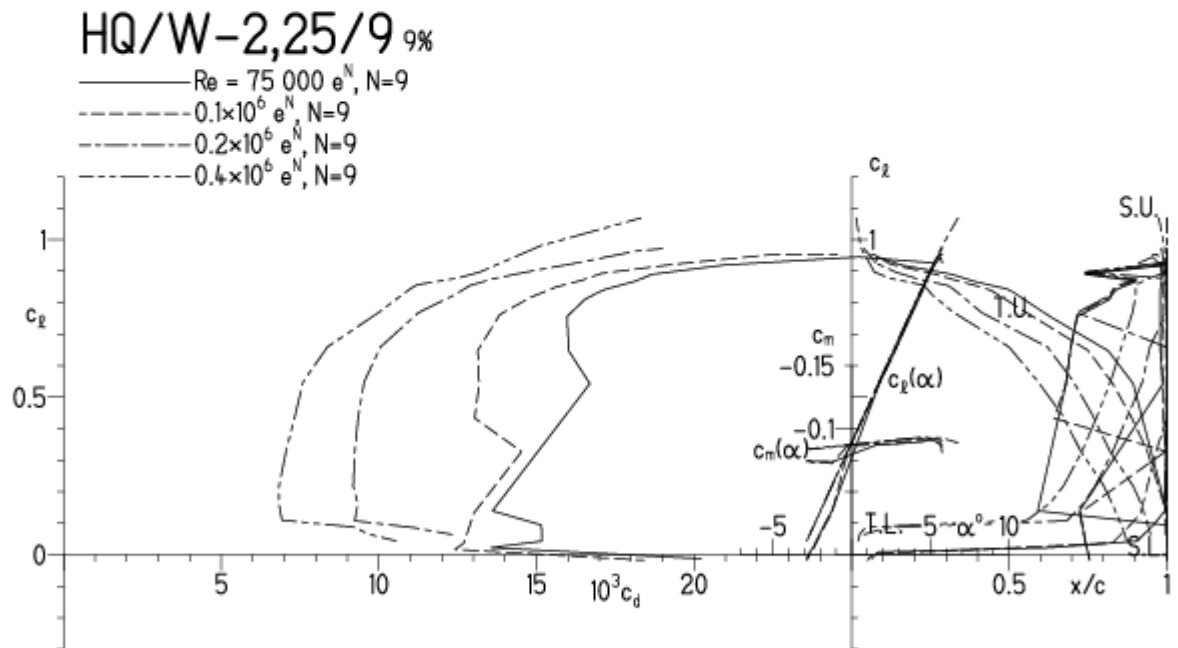


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

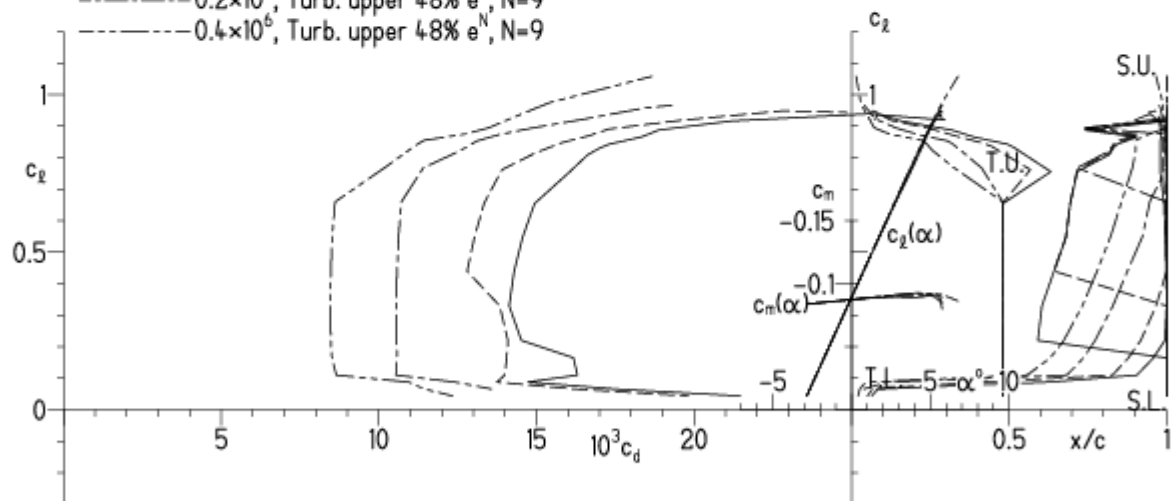
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

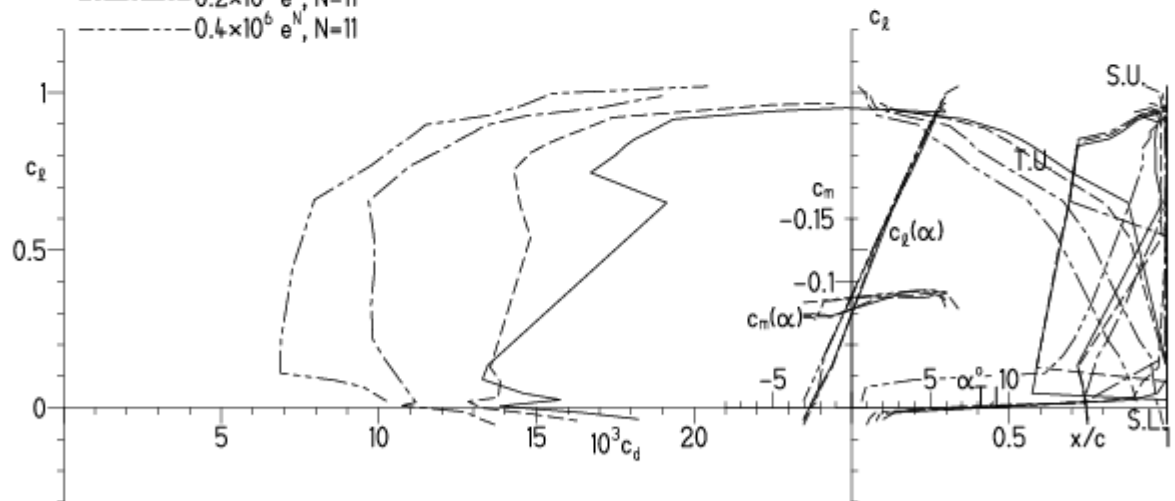
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



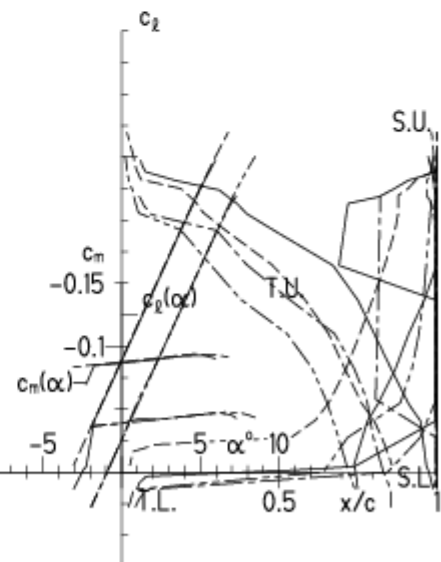
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

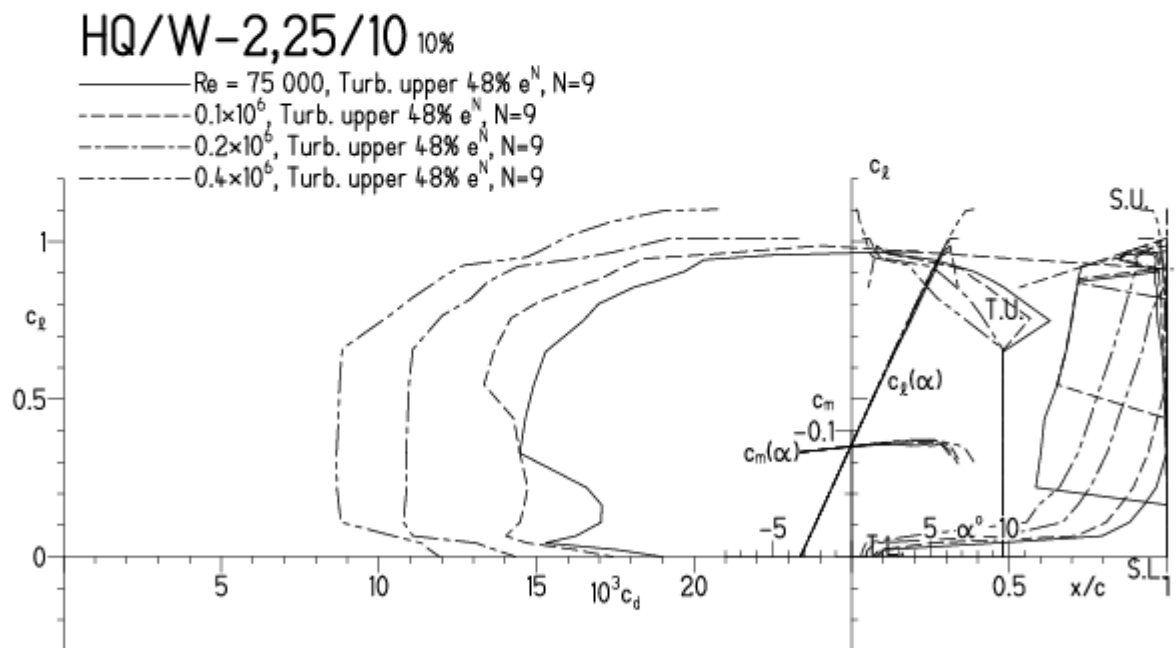


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

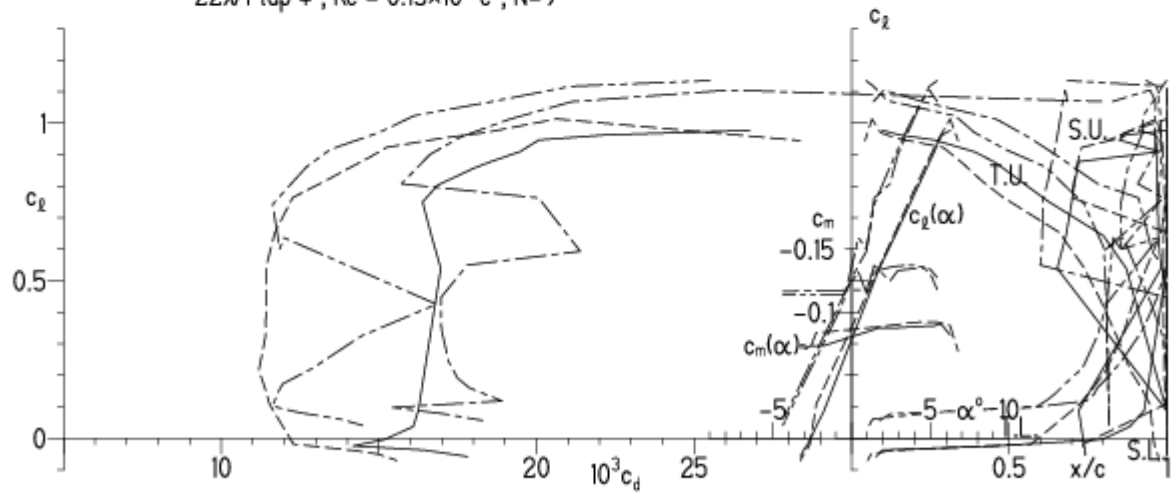


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

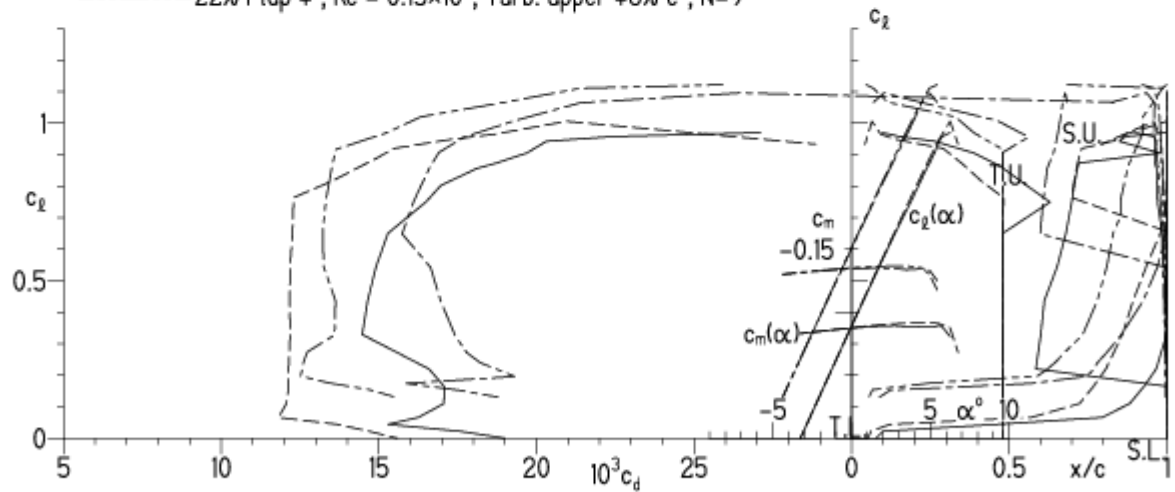


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

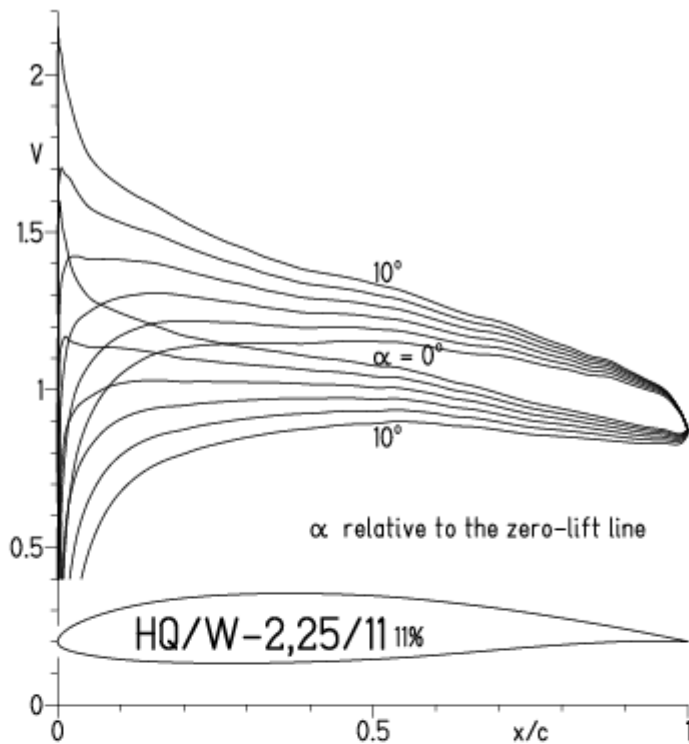


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - $0.8 \times 10^6 e^N, N=11$
- · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

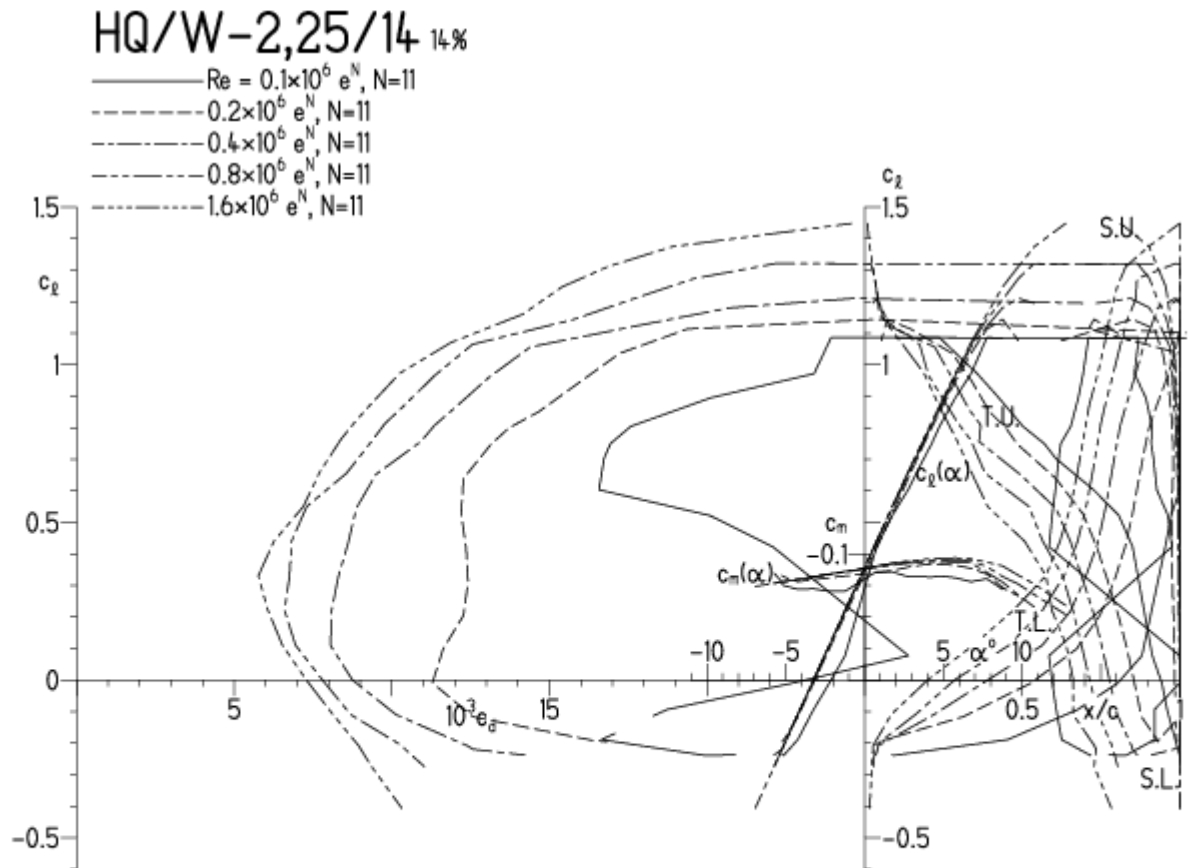


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

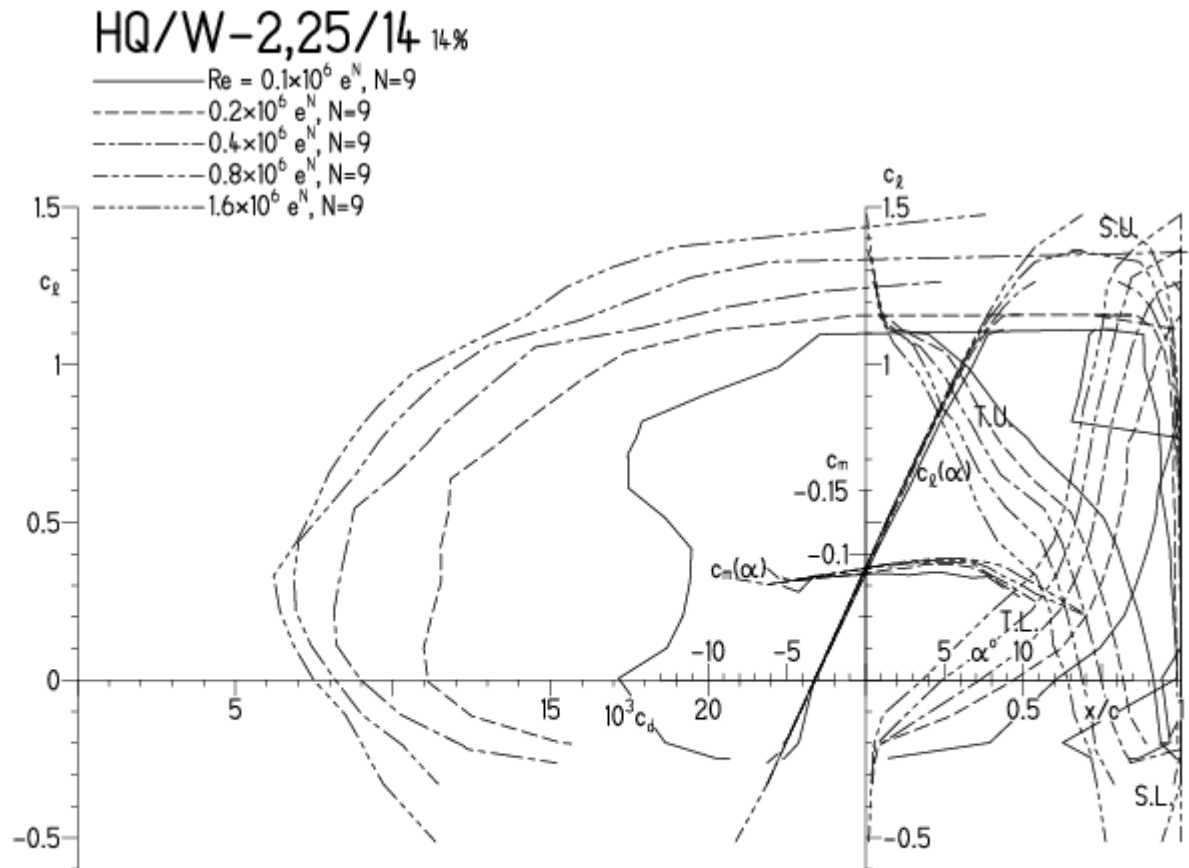


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

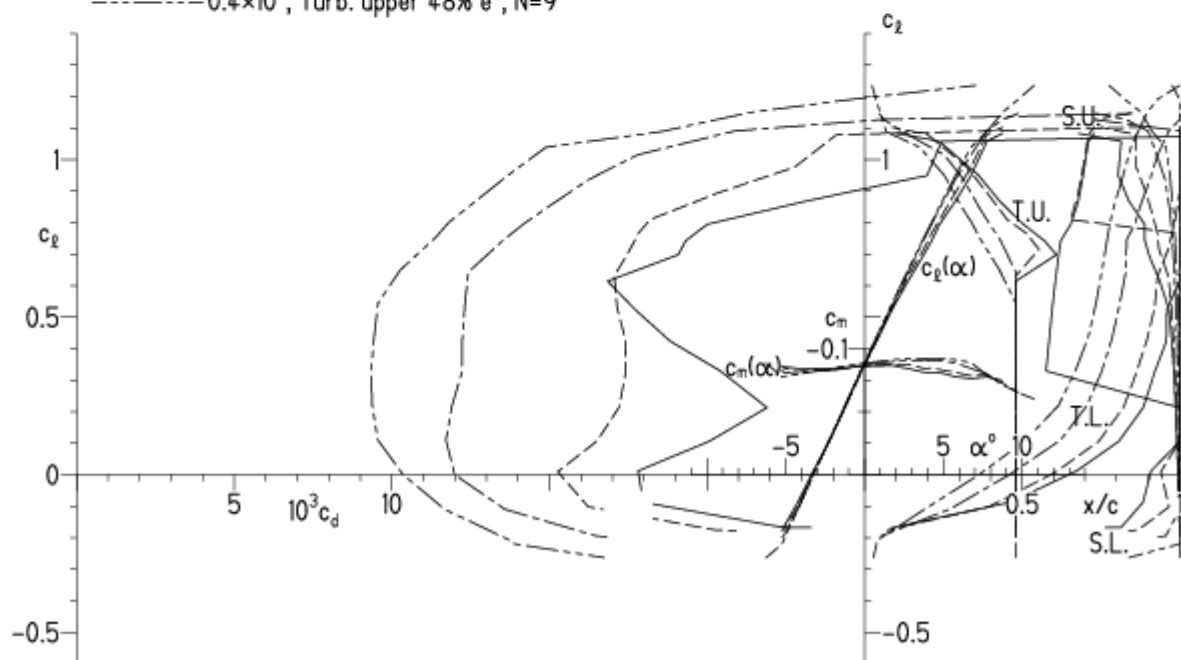
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

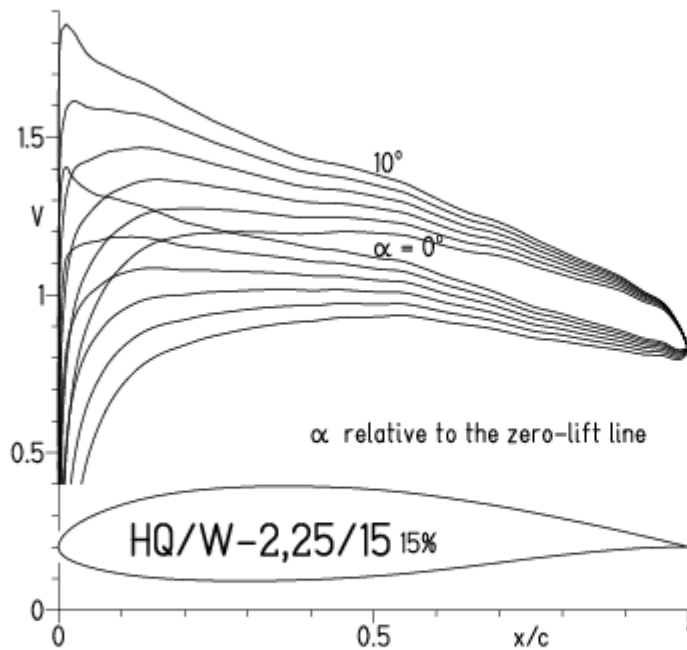


EPPLER 2005 V. 8.5.07

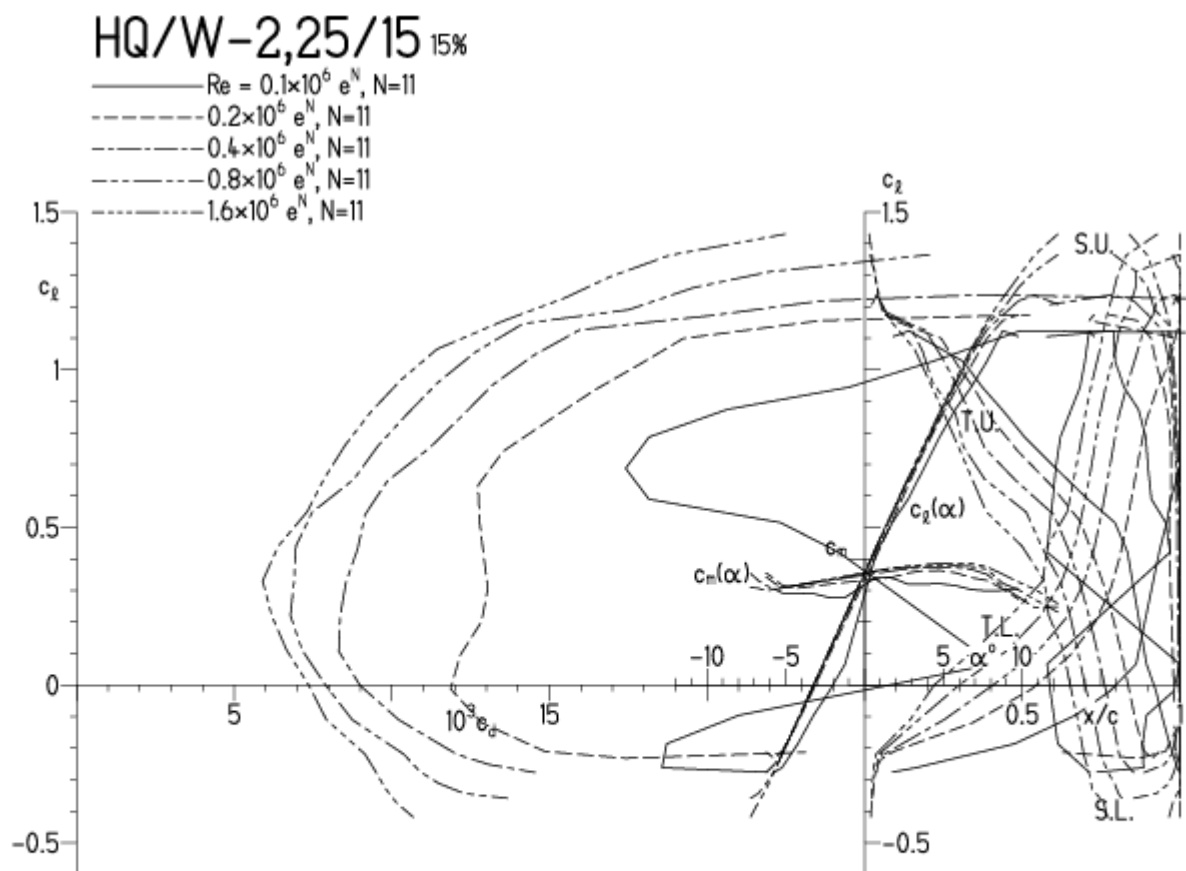


HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2,25/8,5 8.5%

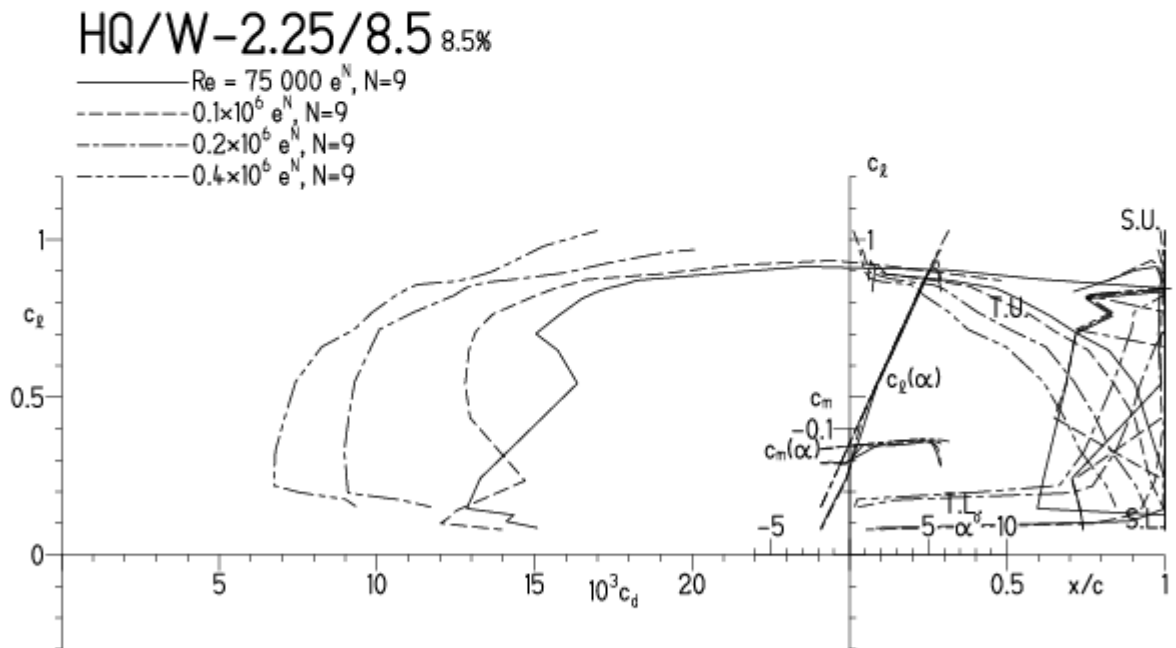


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

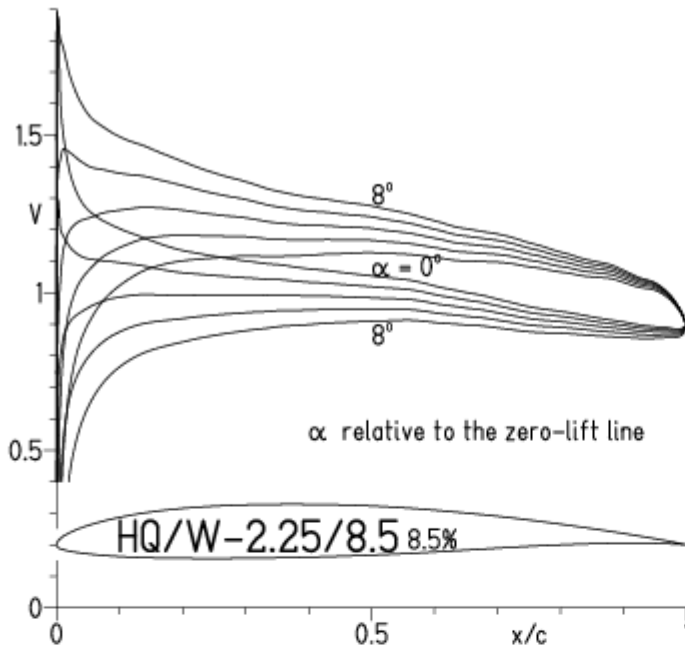


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

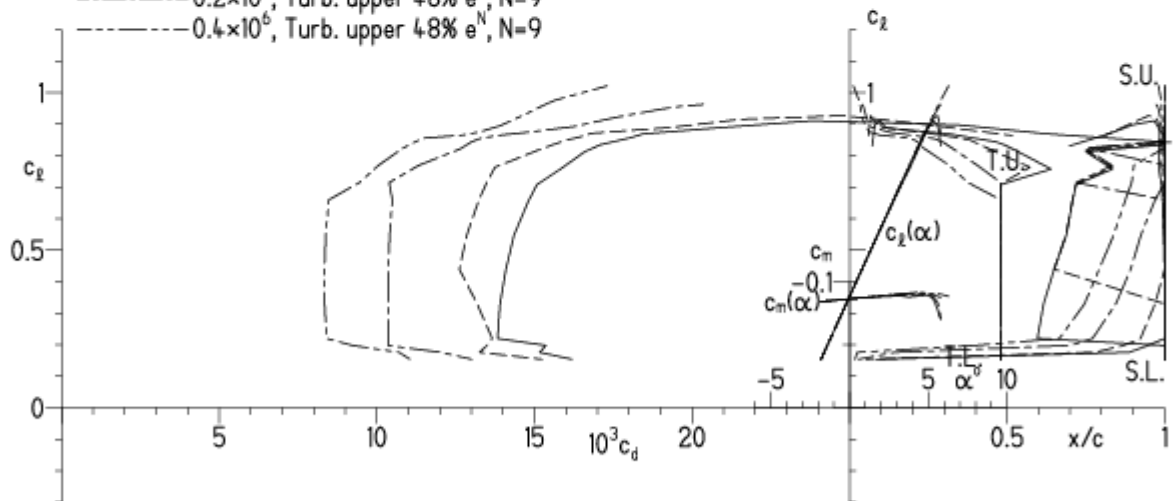
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

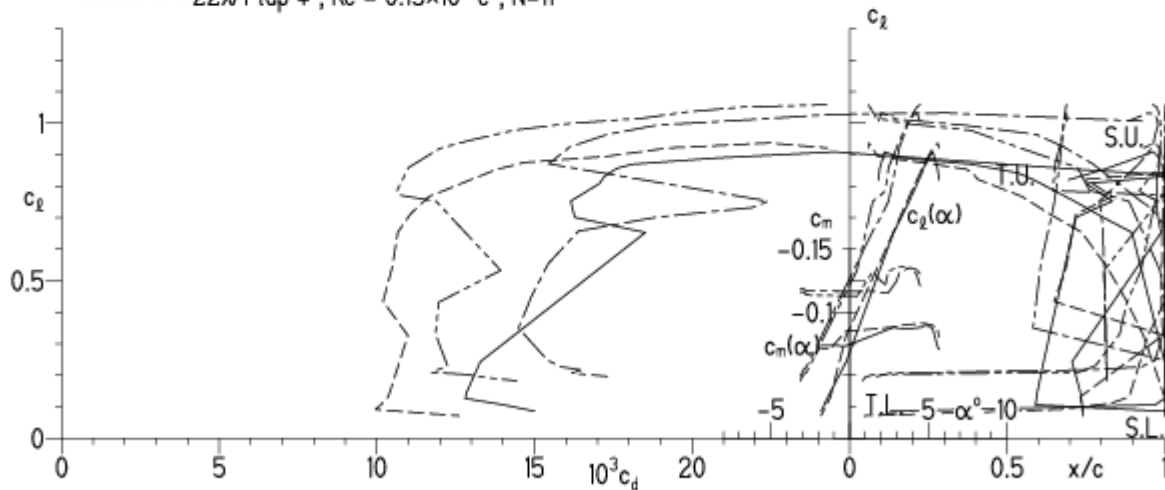


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

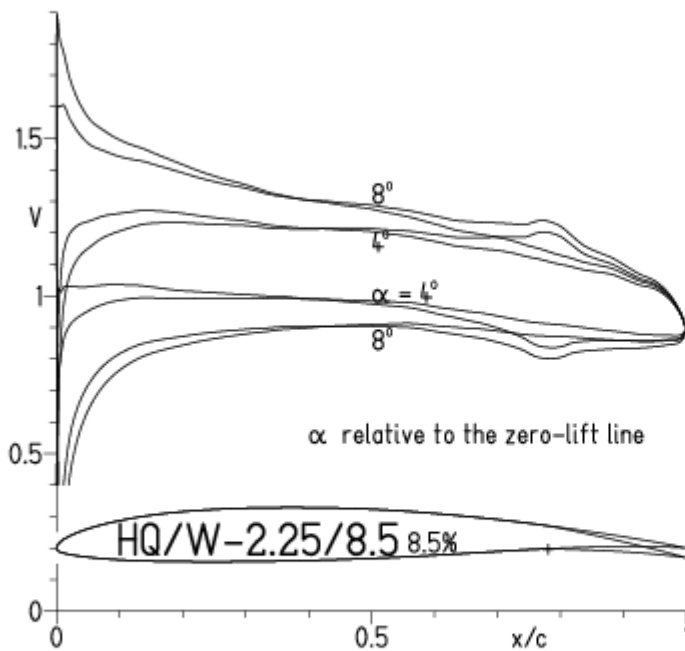
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

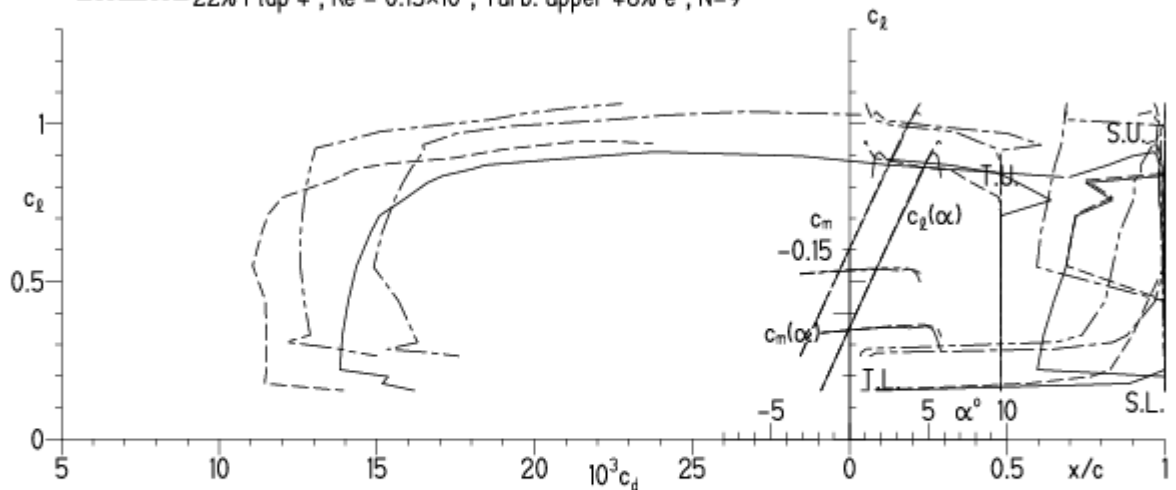


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

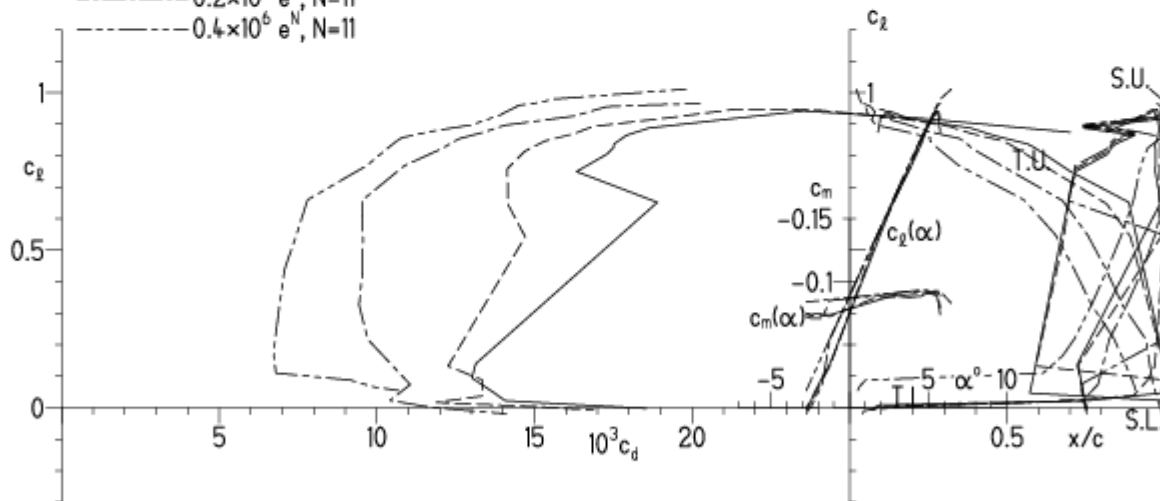
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

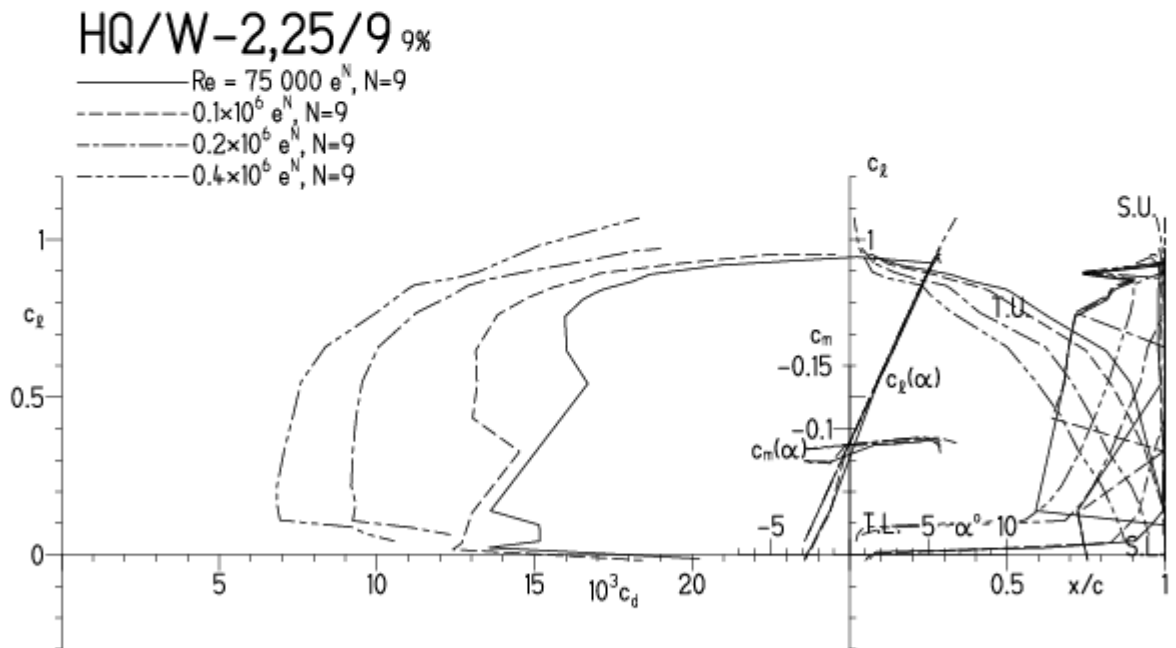


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

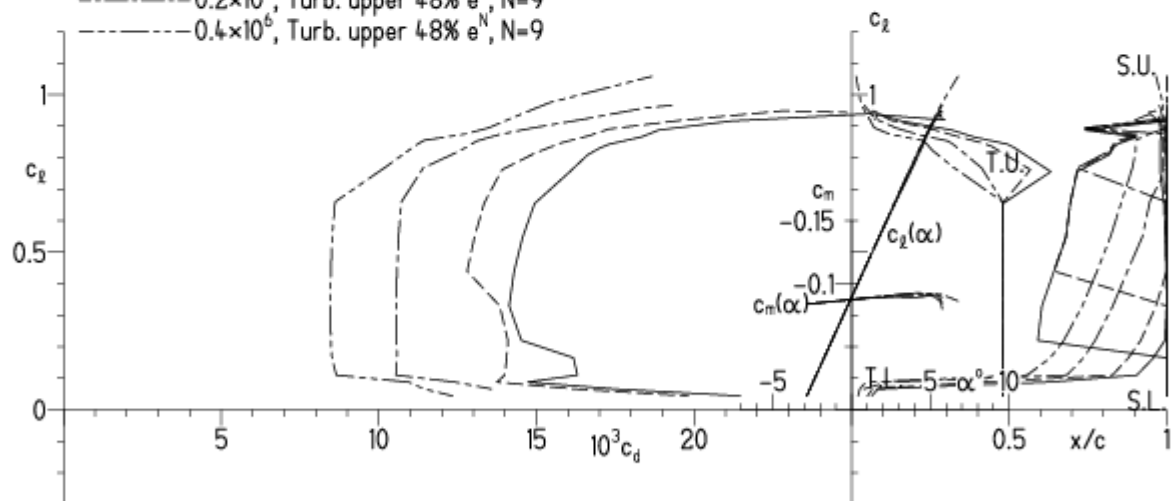
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38

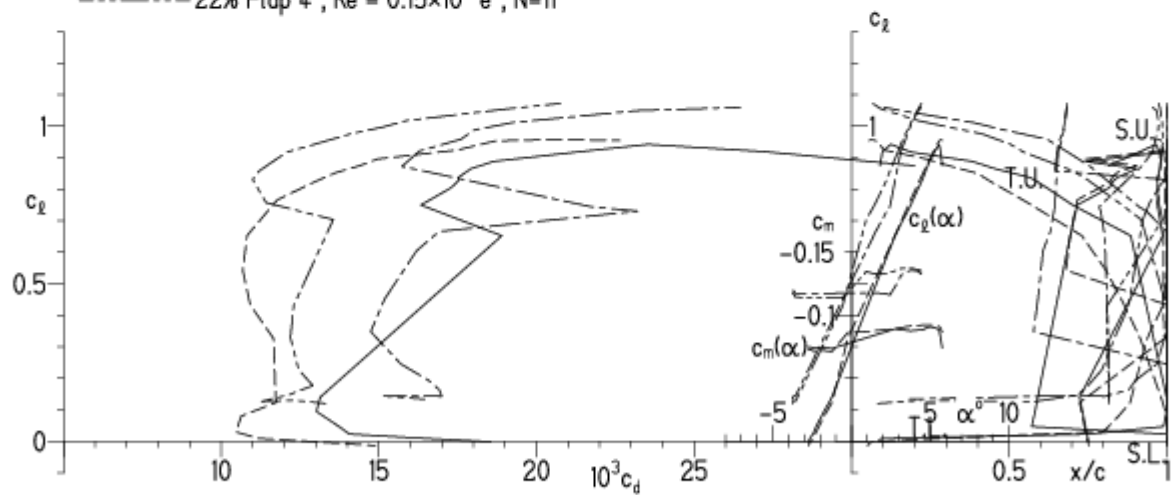


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

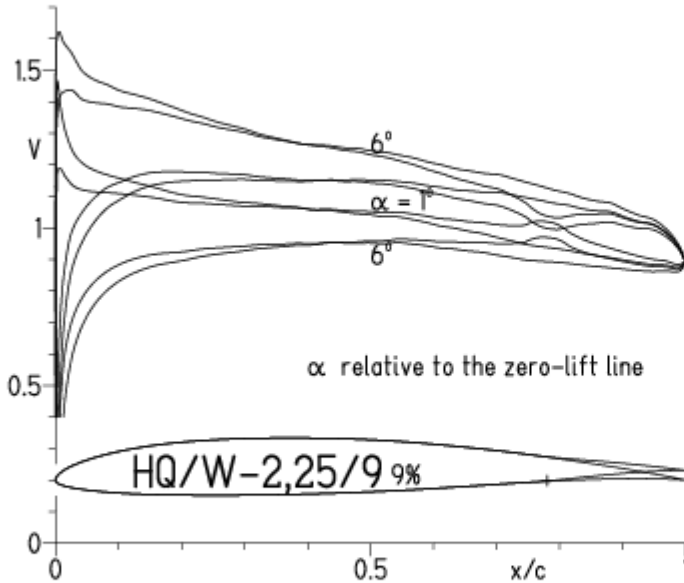
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17

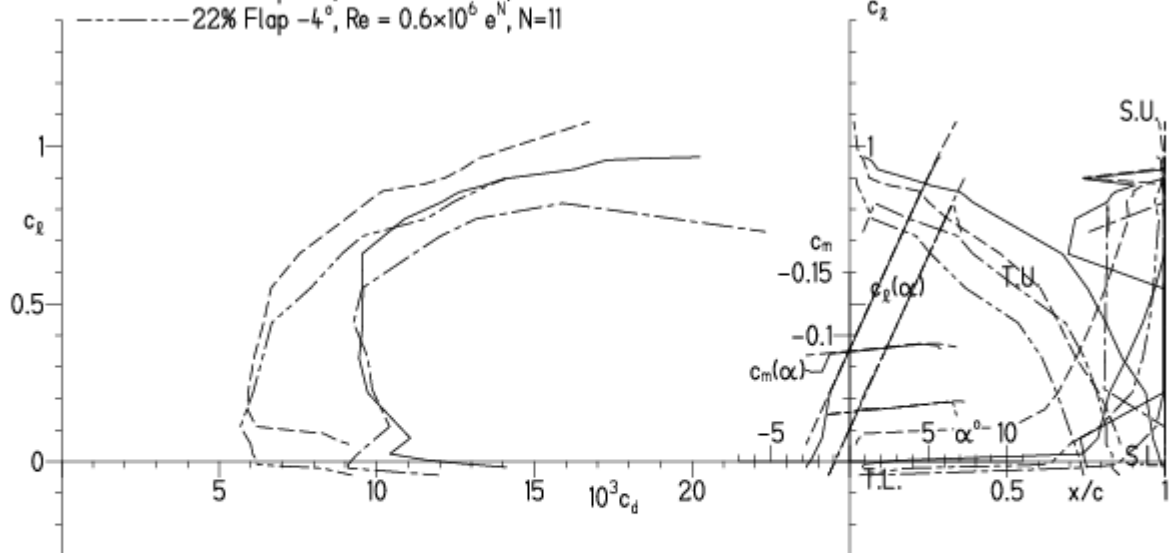


EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

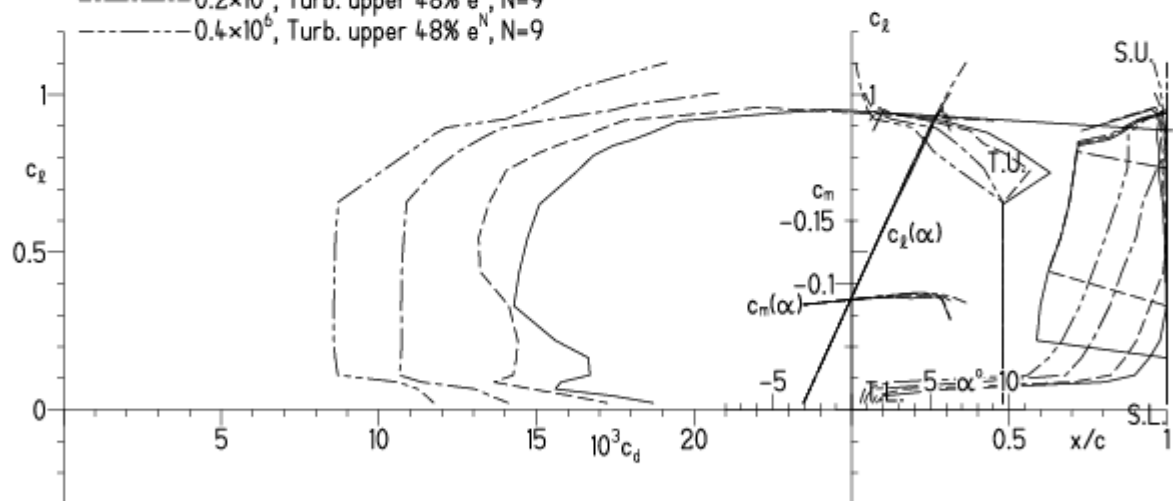
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

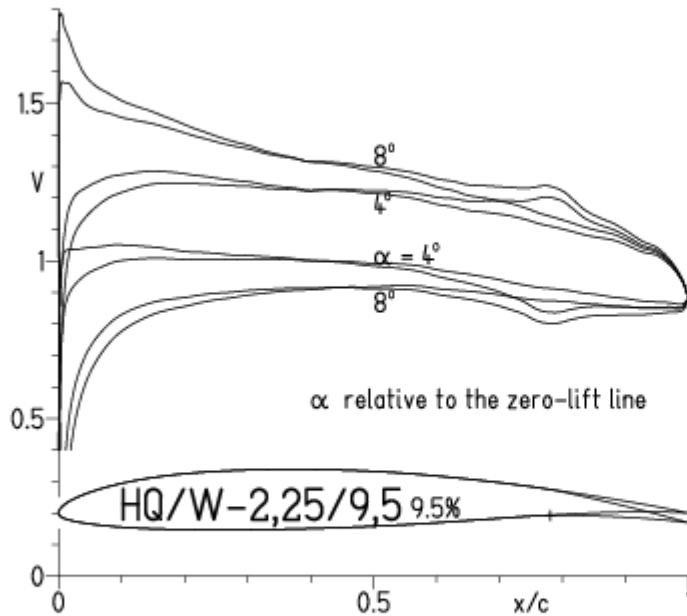
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

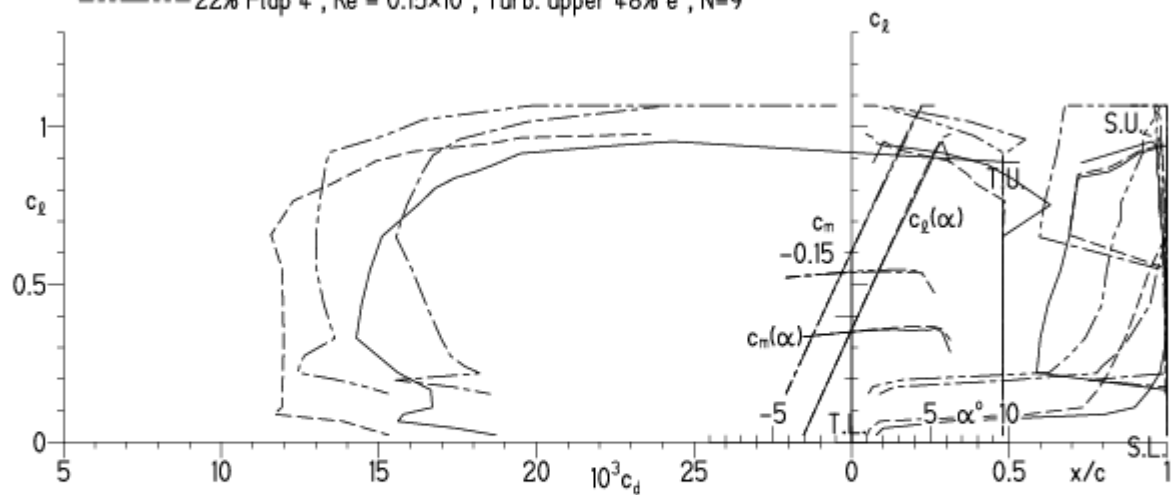


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



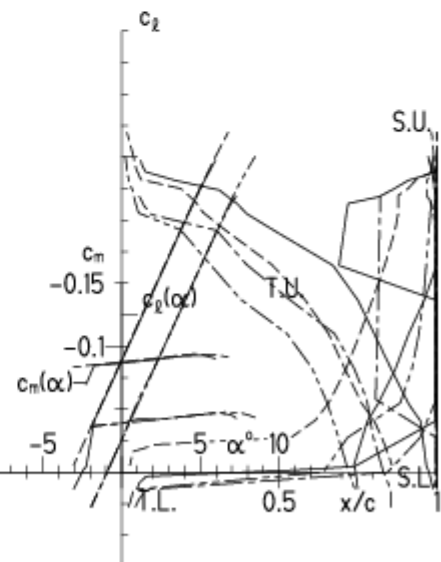
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

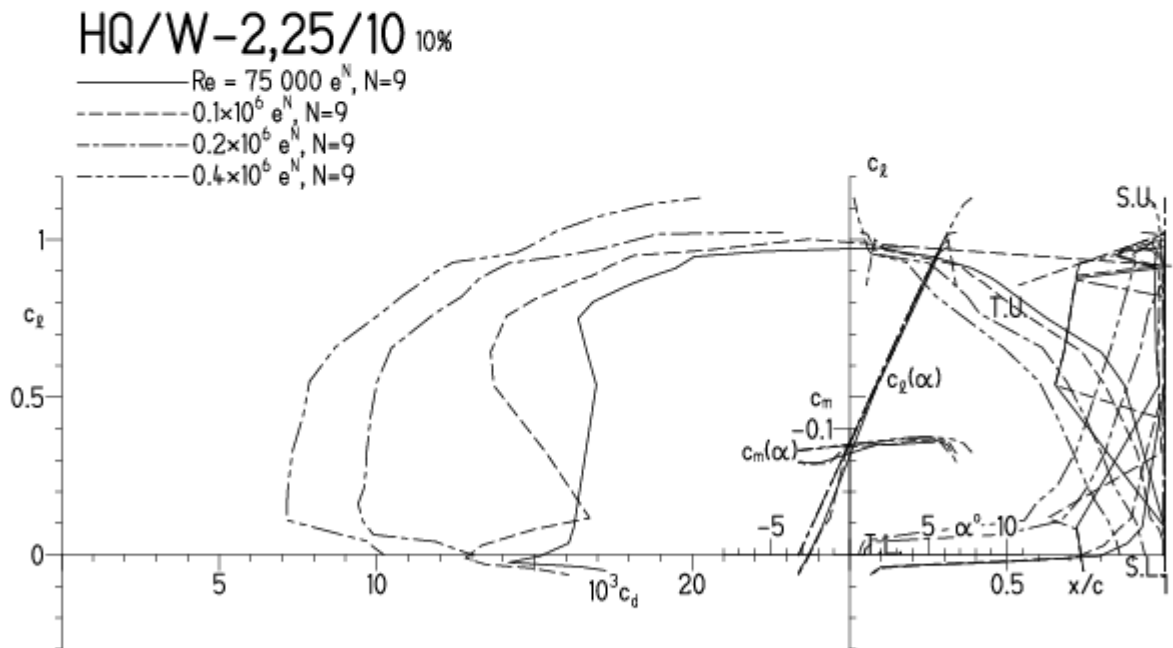


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

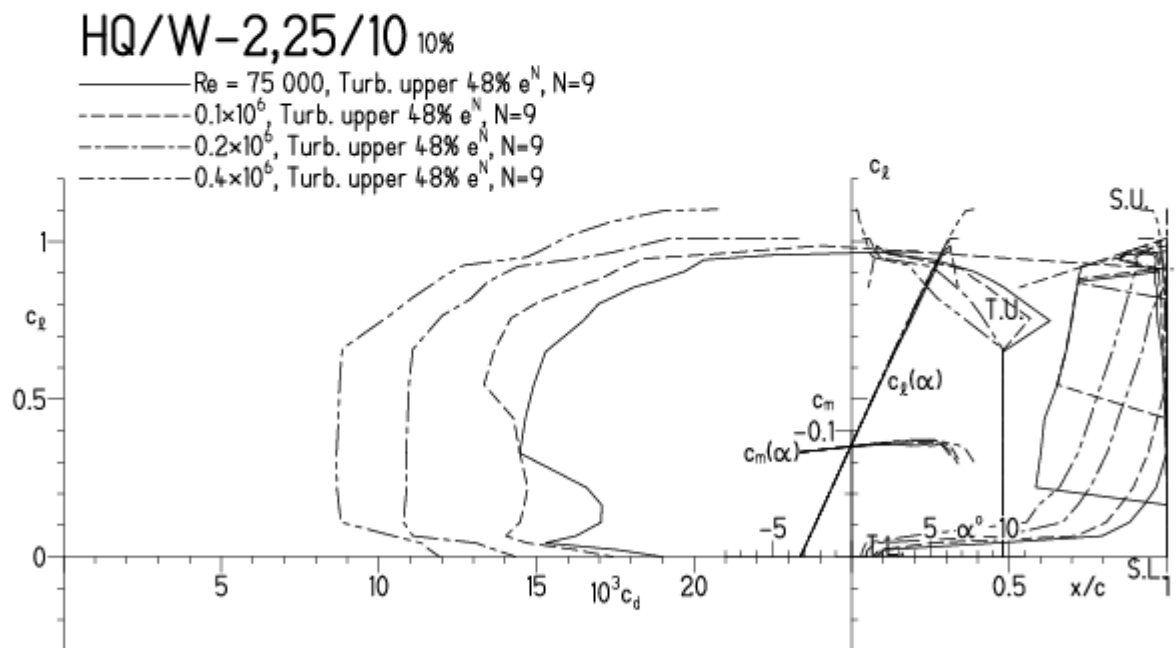


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

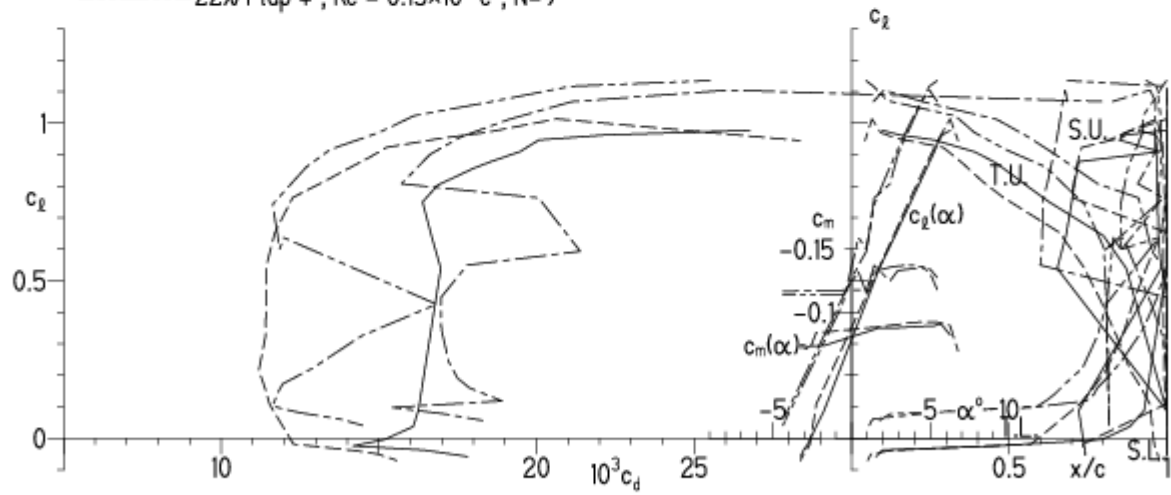


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

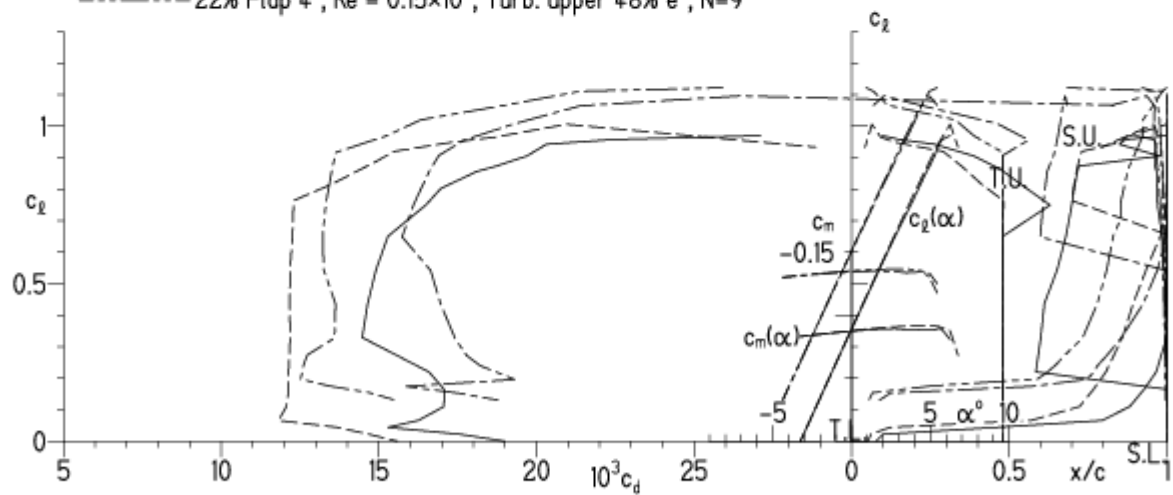


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

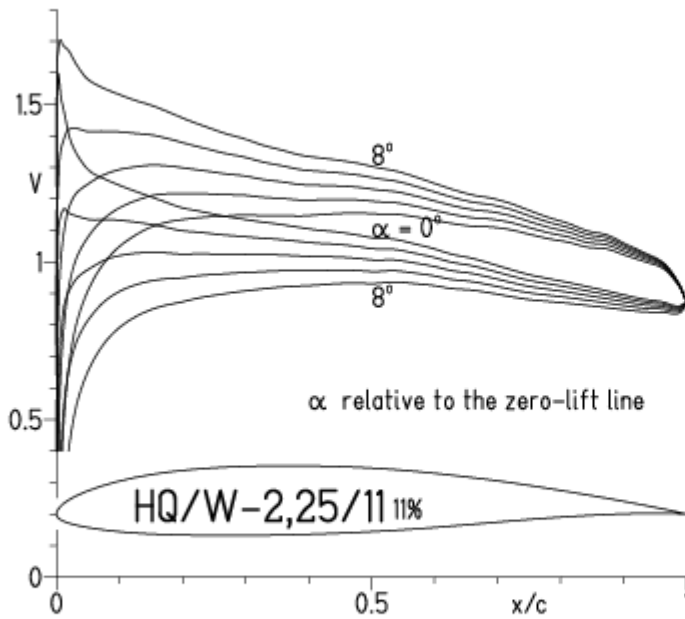


EPPLER 2005 V. 8.5.07 RUN

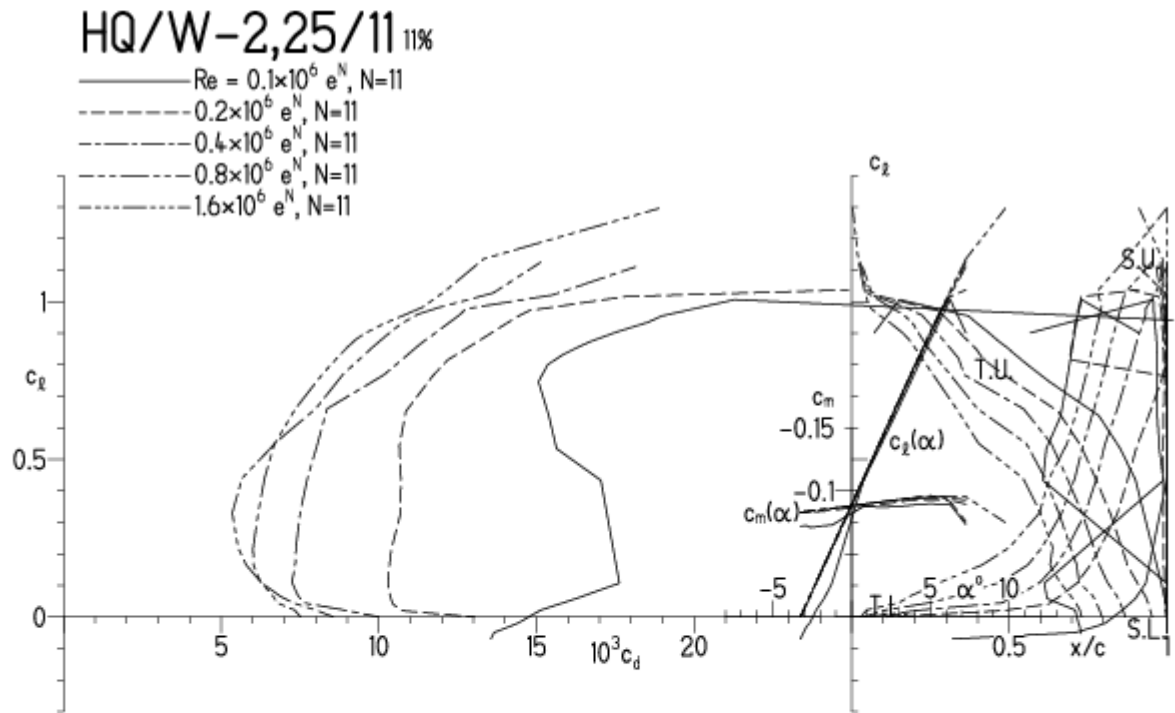


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

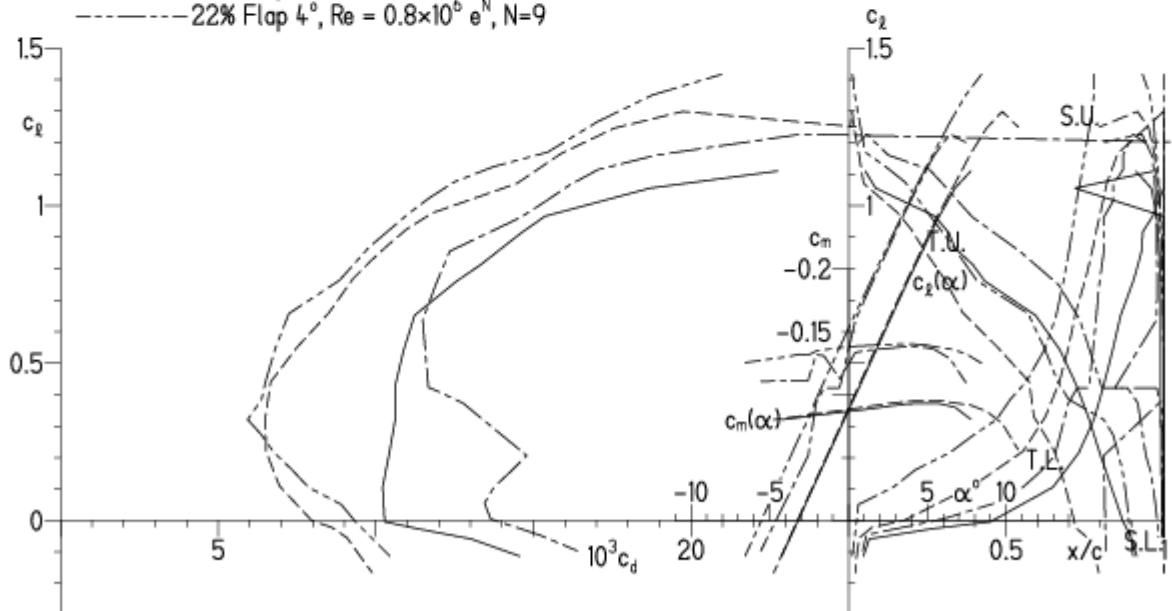


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

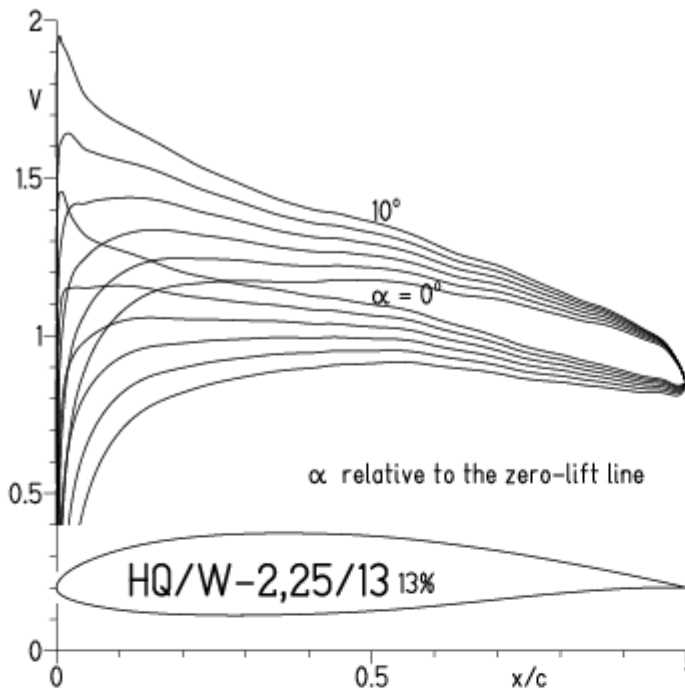
HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

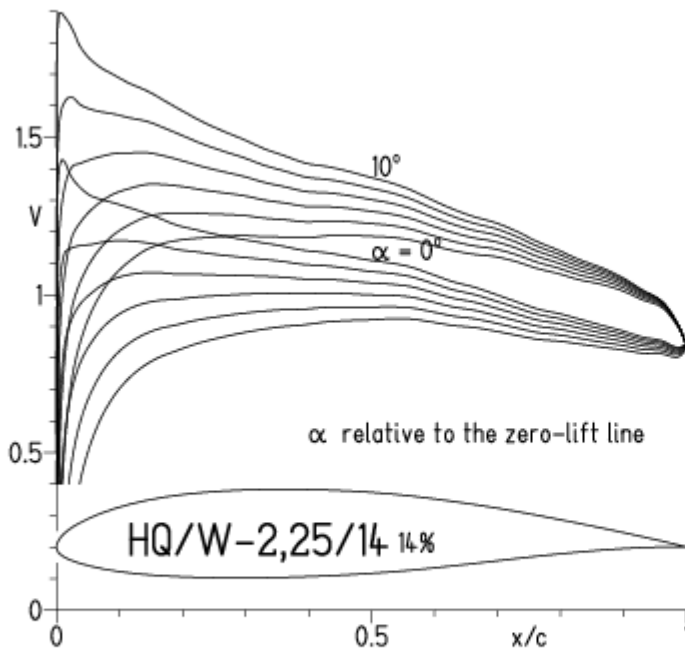


EPPLER 2005 V. 8.

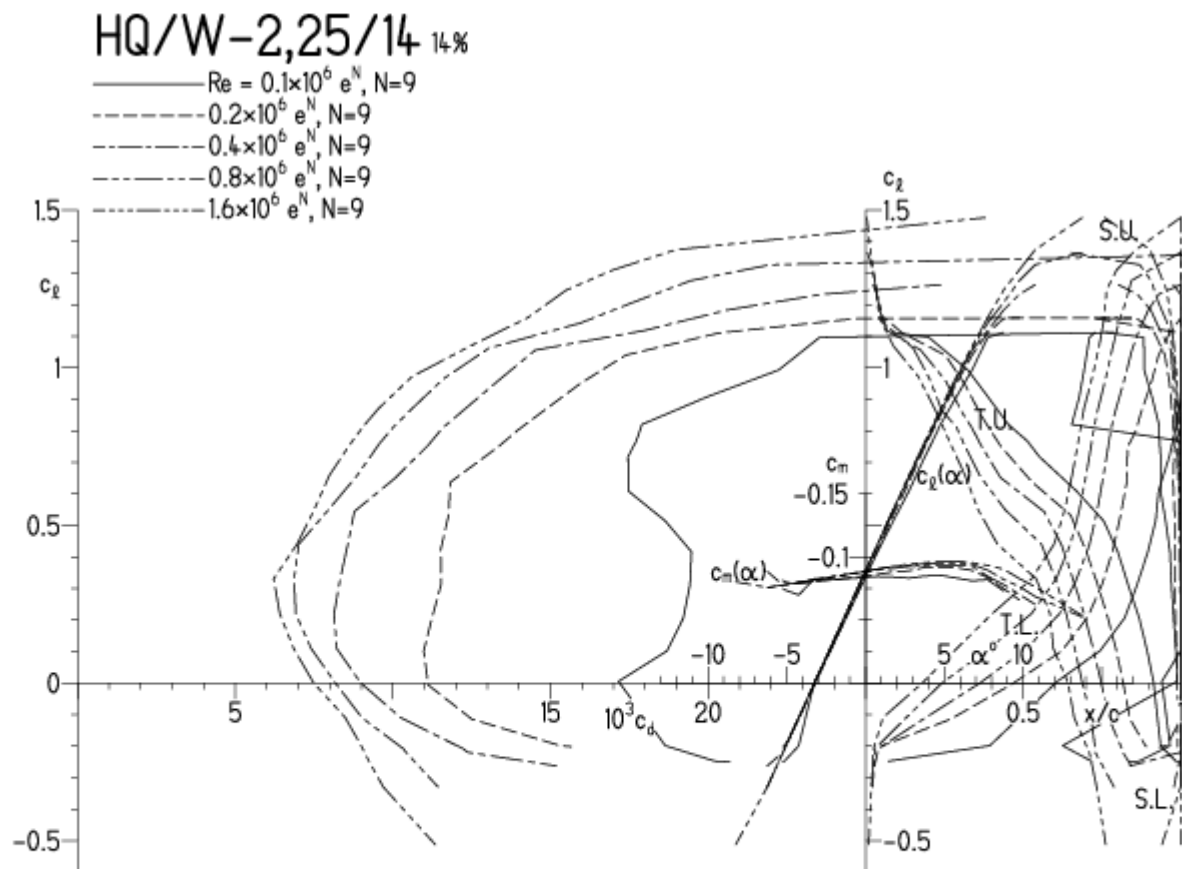


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

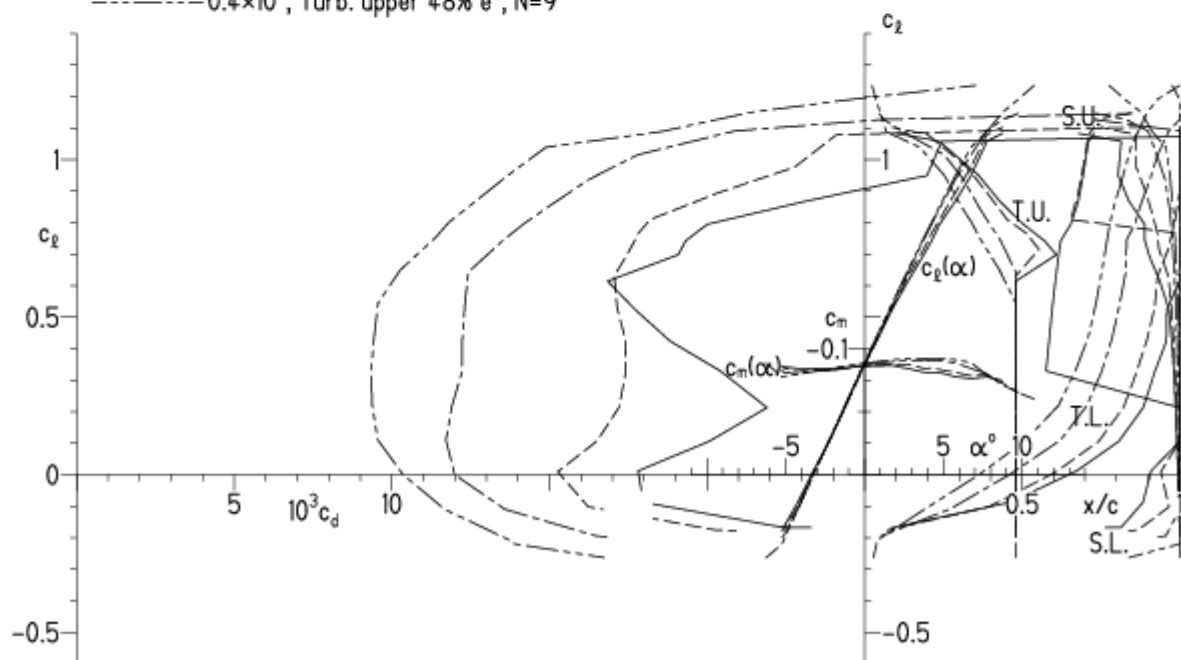
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

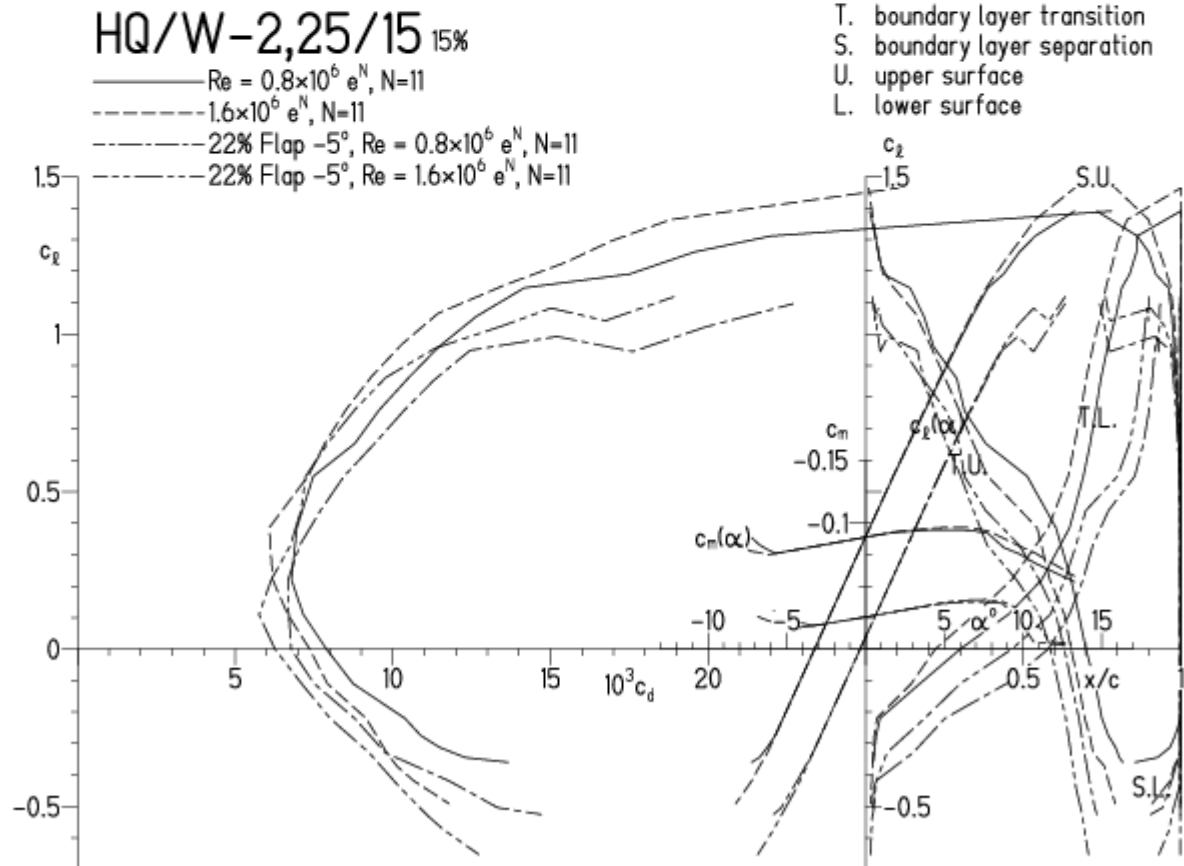
Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. $30 - 35 \text{ m/s}$ Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

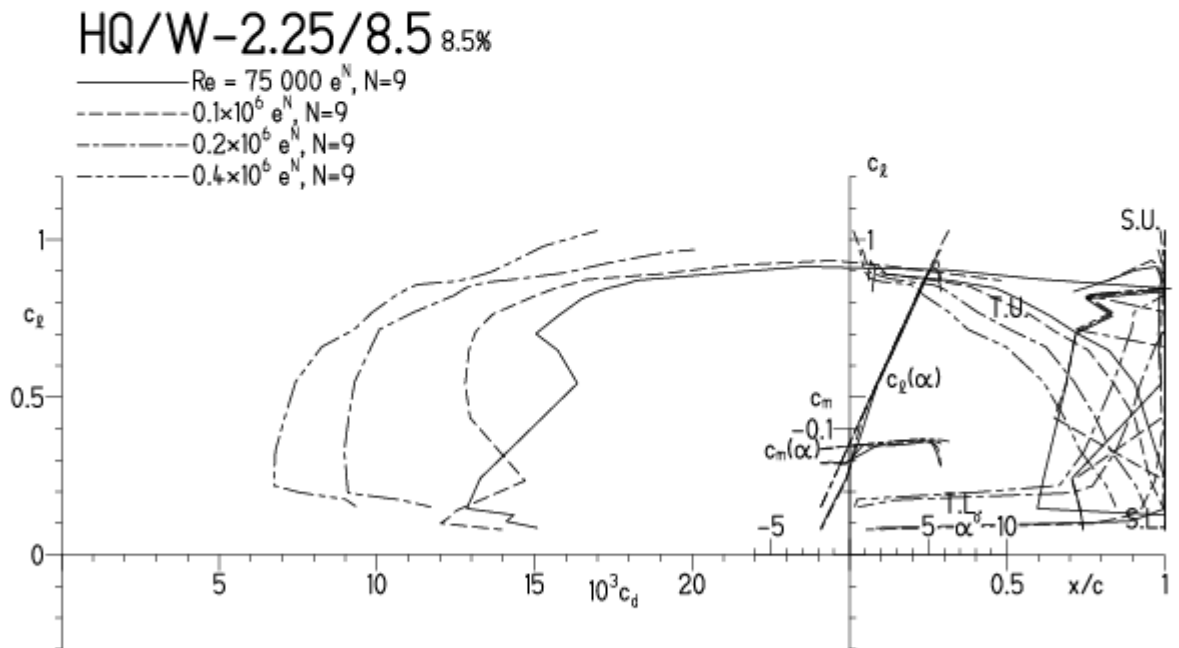


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

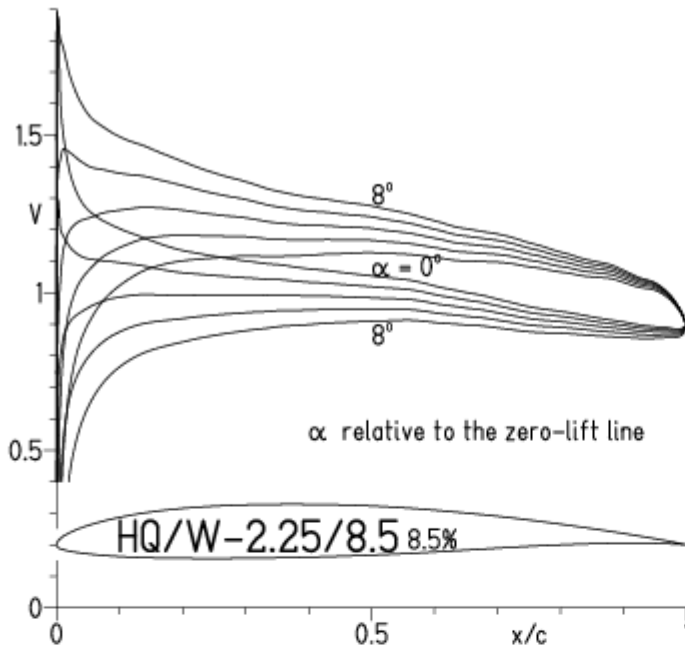


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

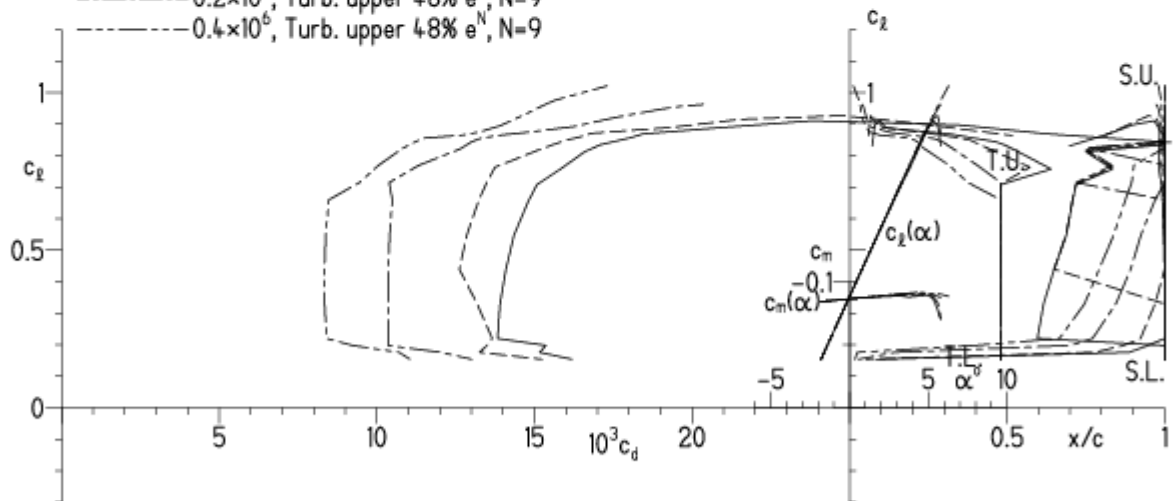
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

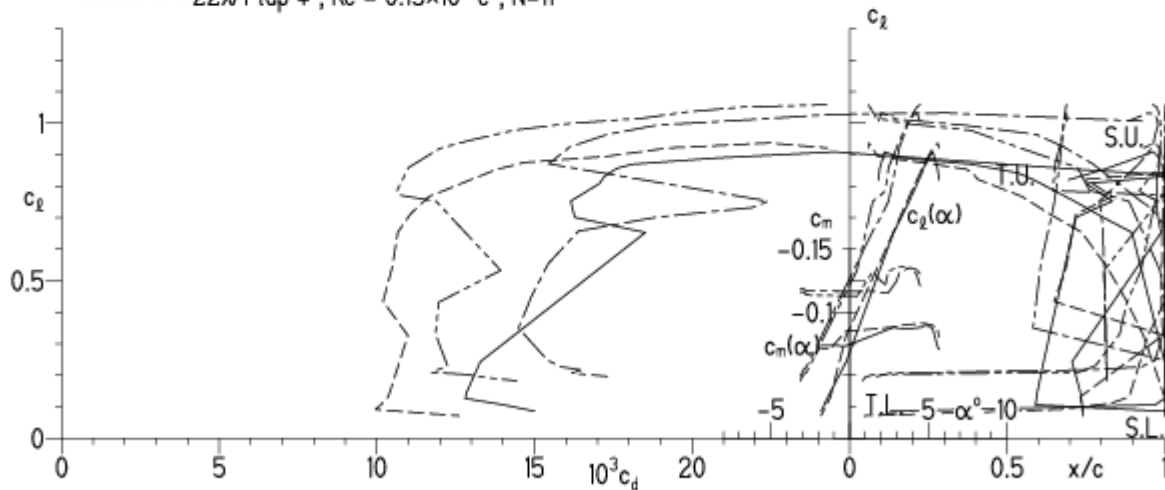


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

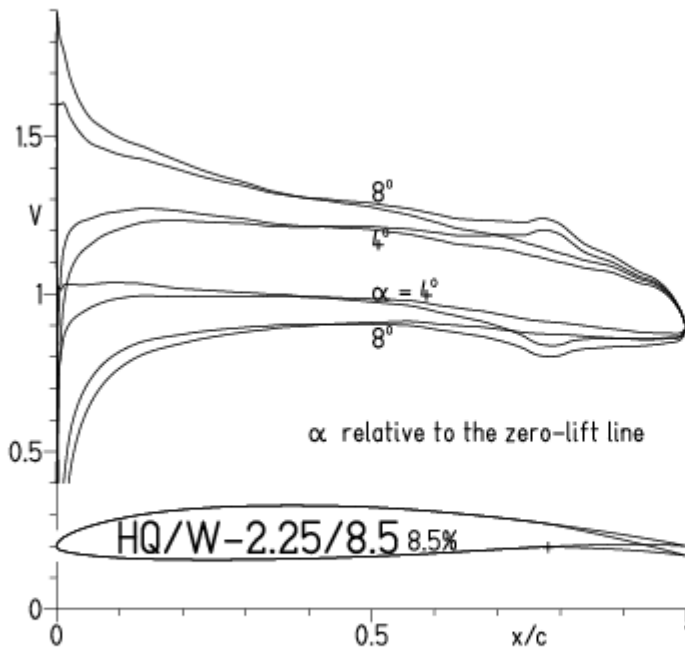
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

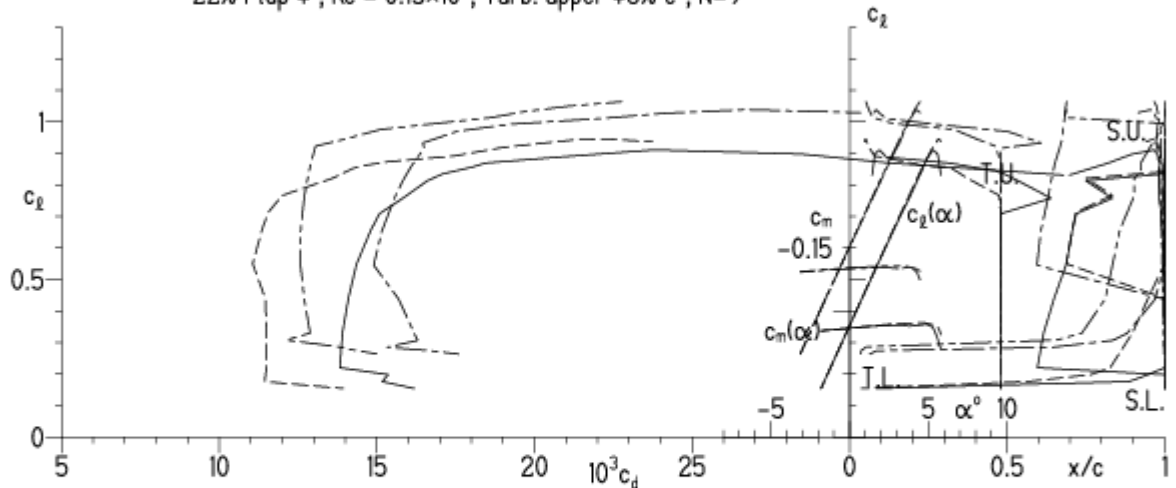


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

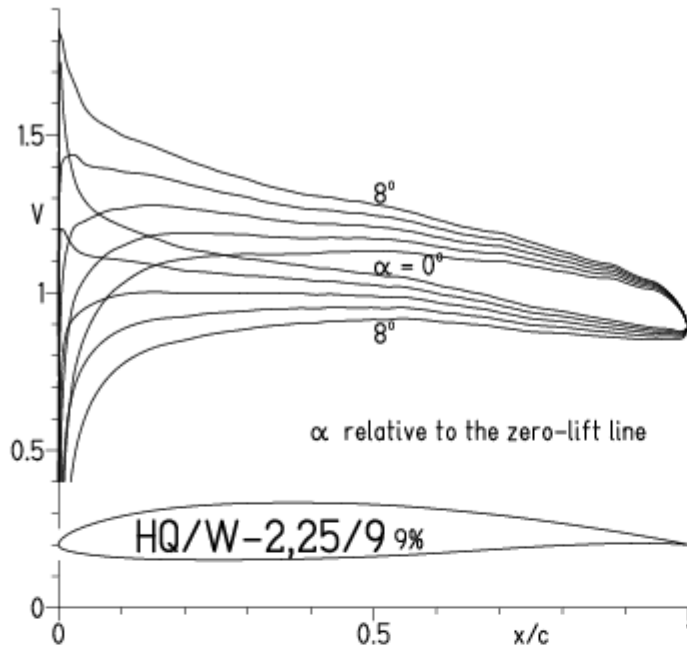


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

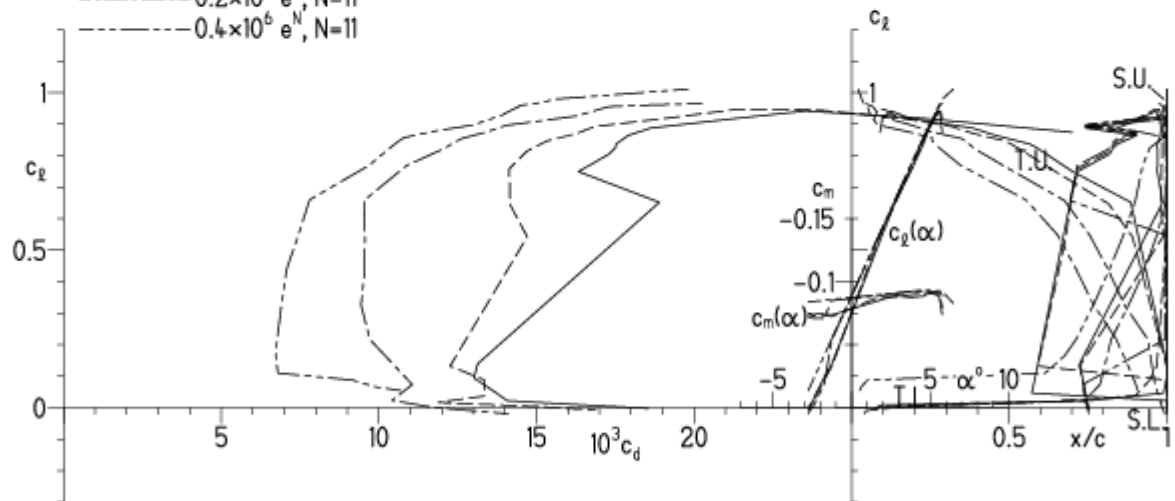
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

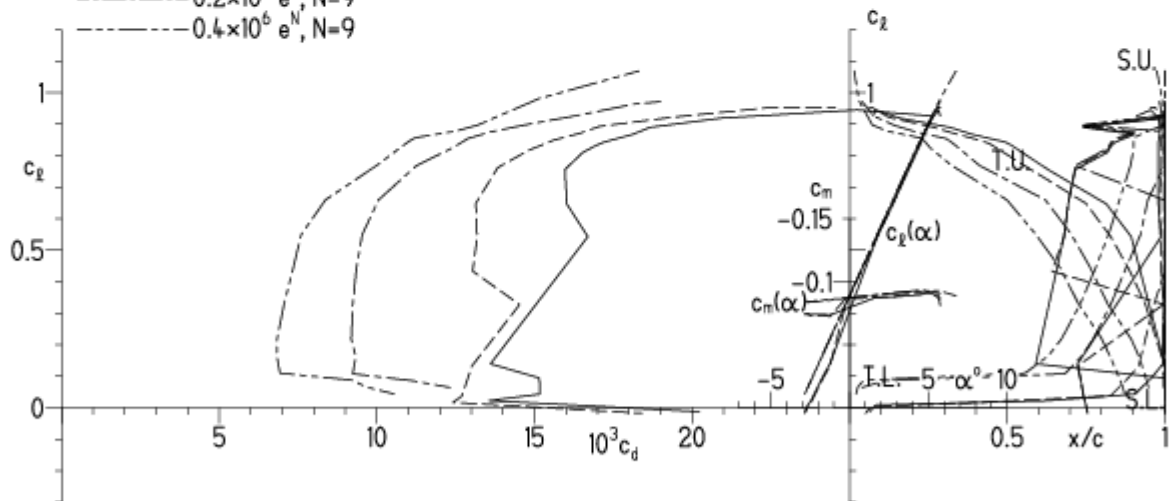
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

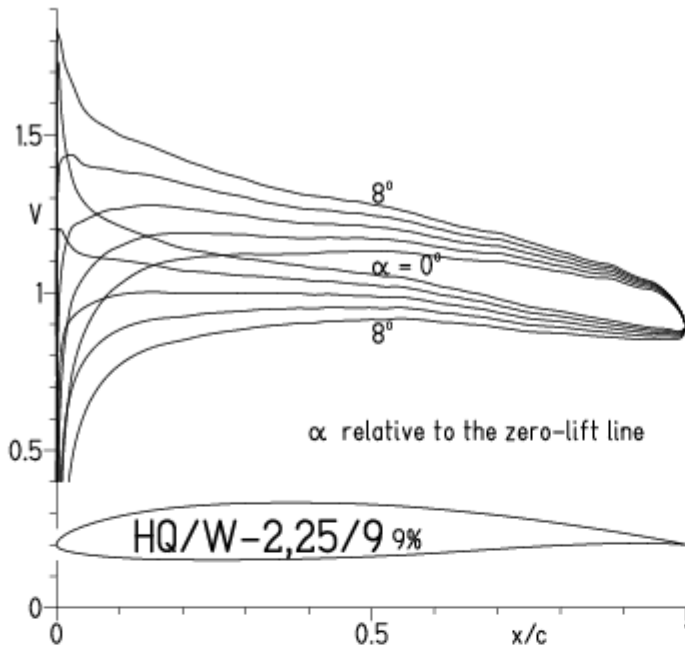
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

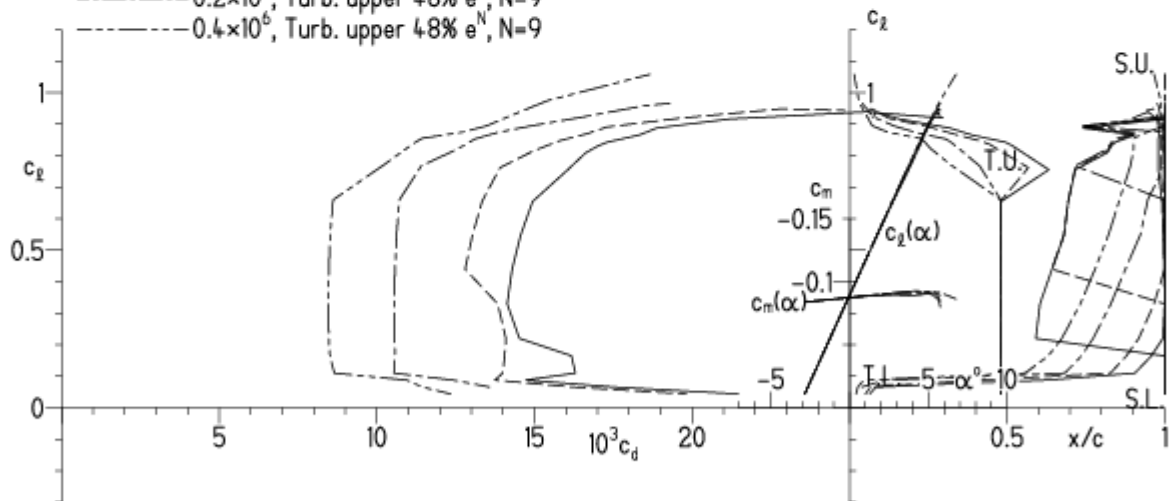
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

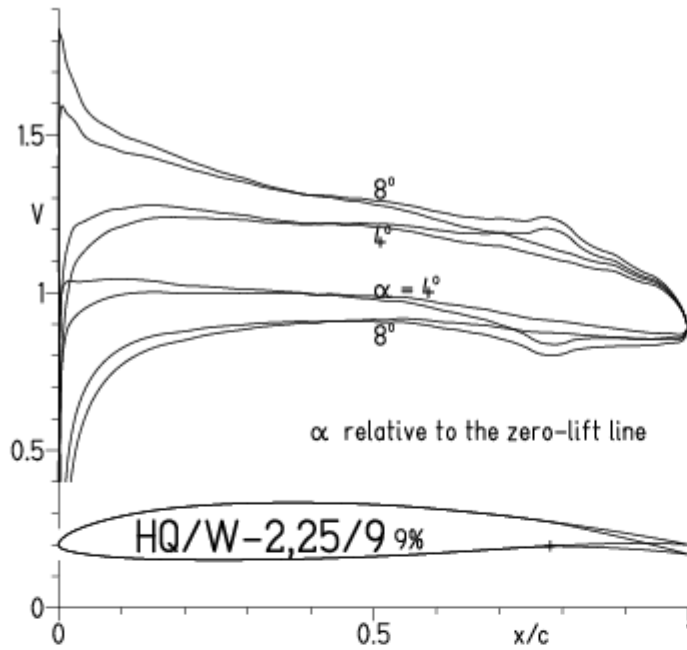
- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48

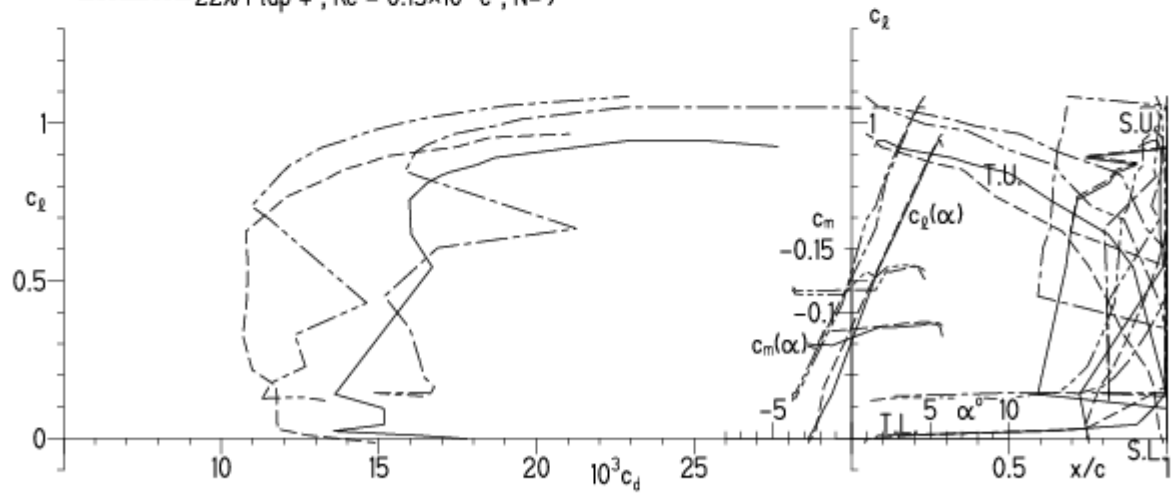


EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



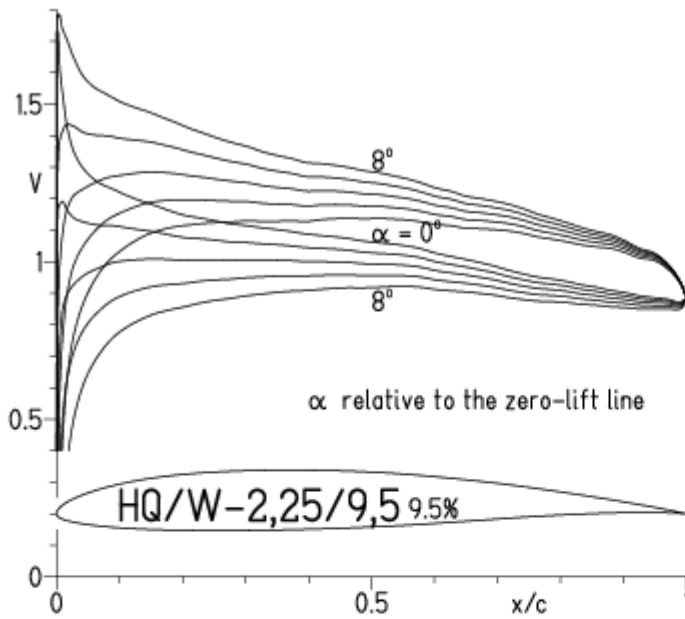
EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

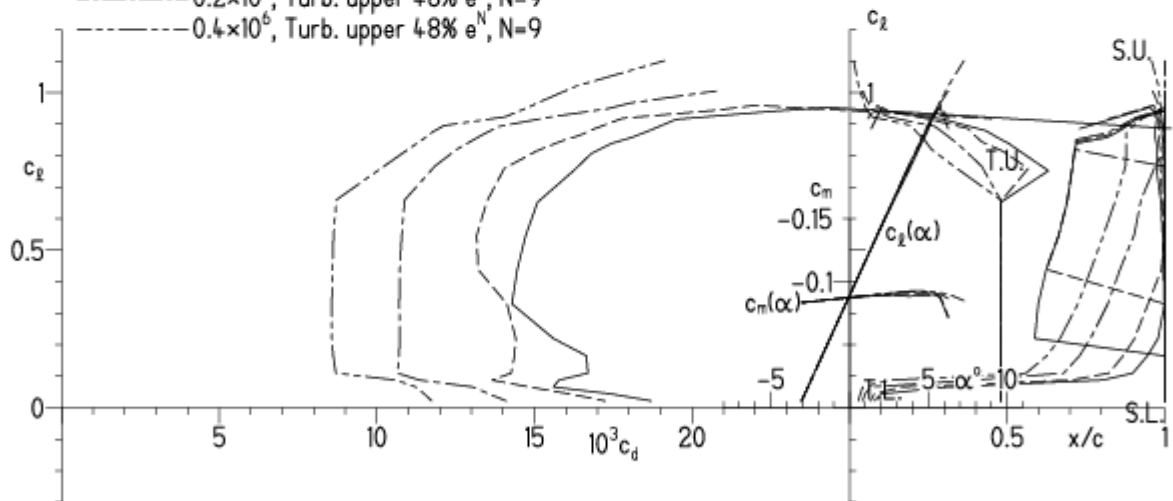
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

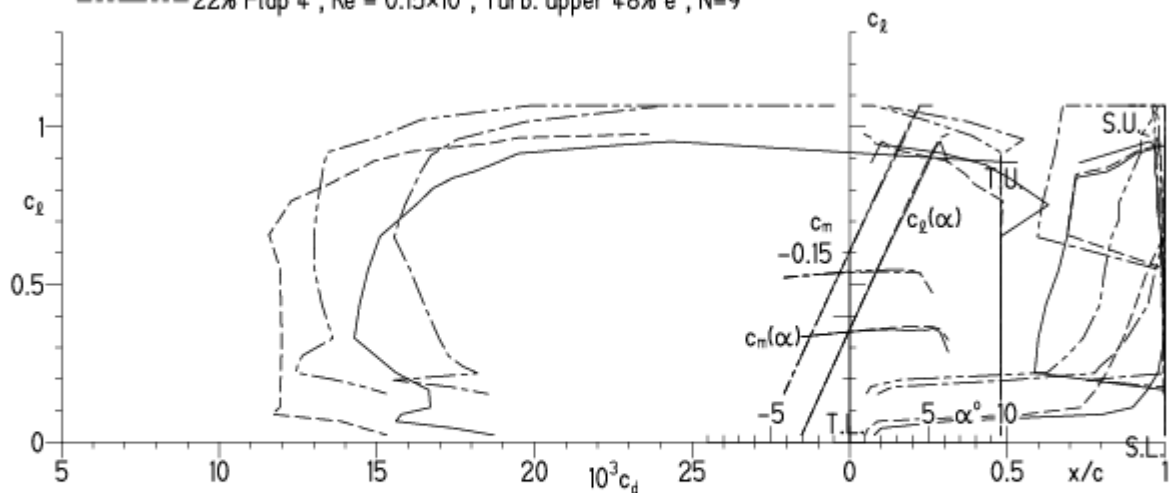


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



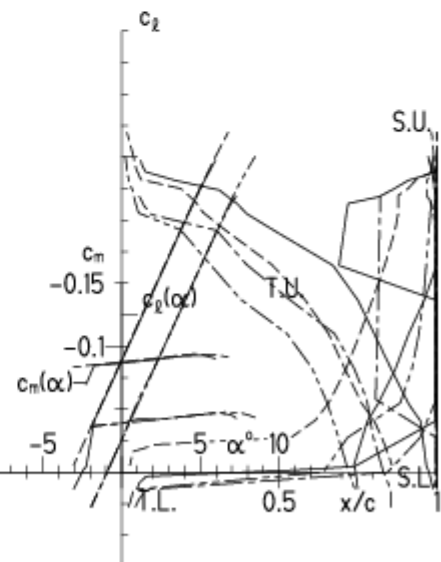
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

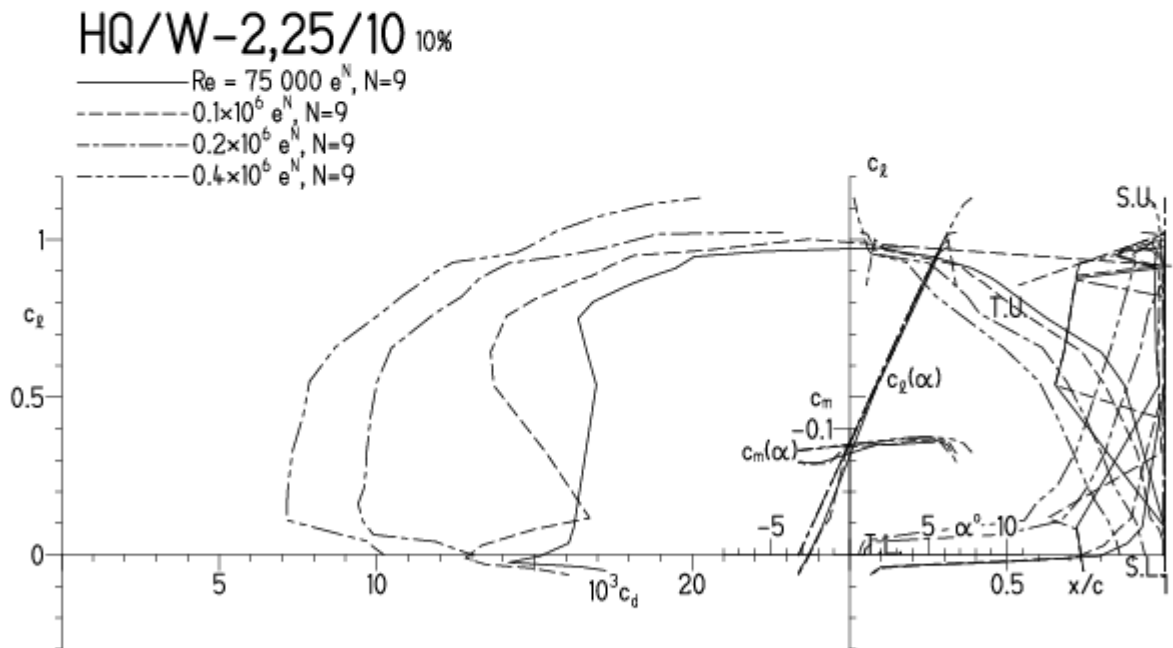


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

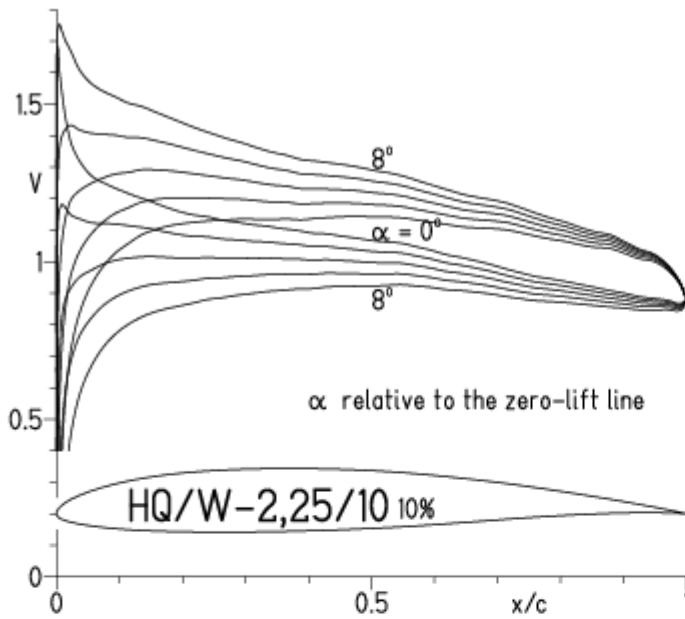


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

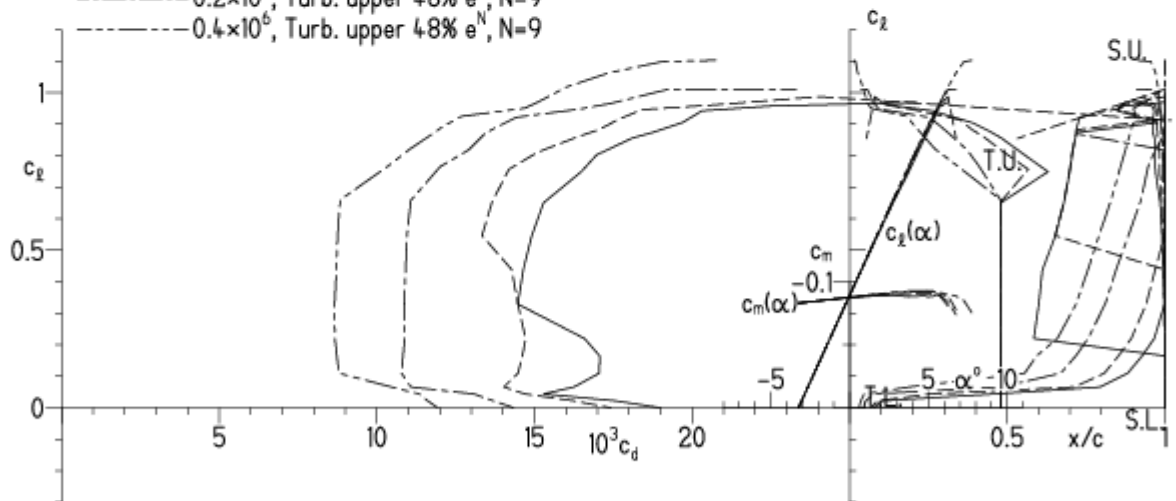
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

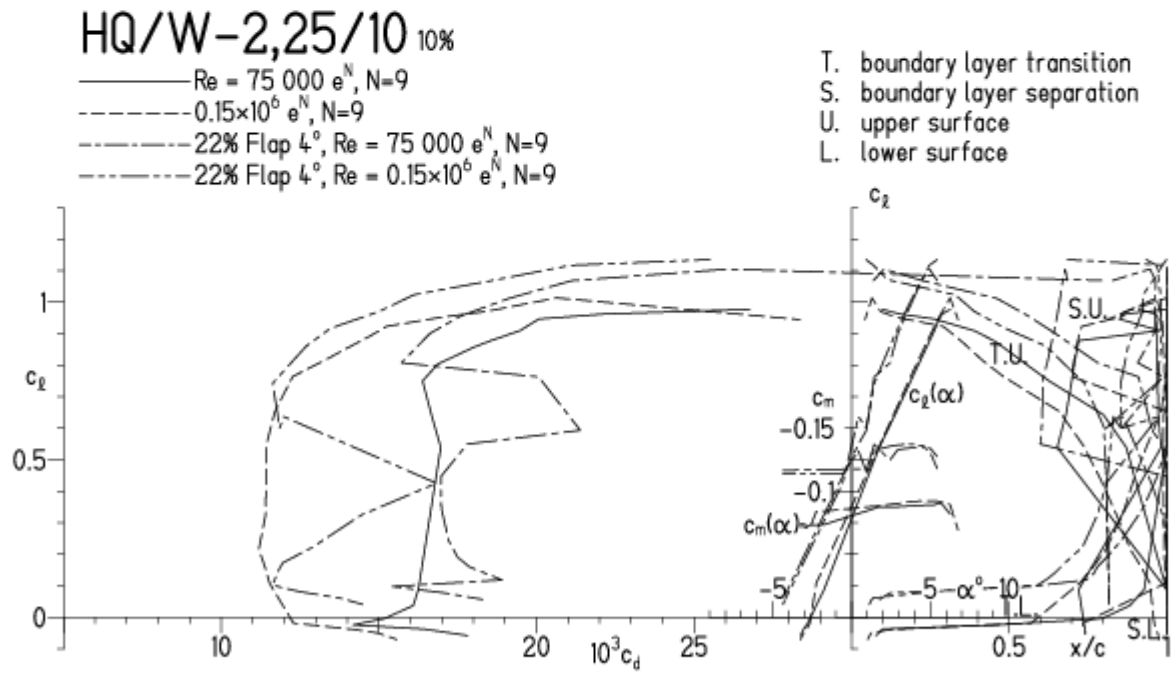


HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

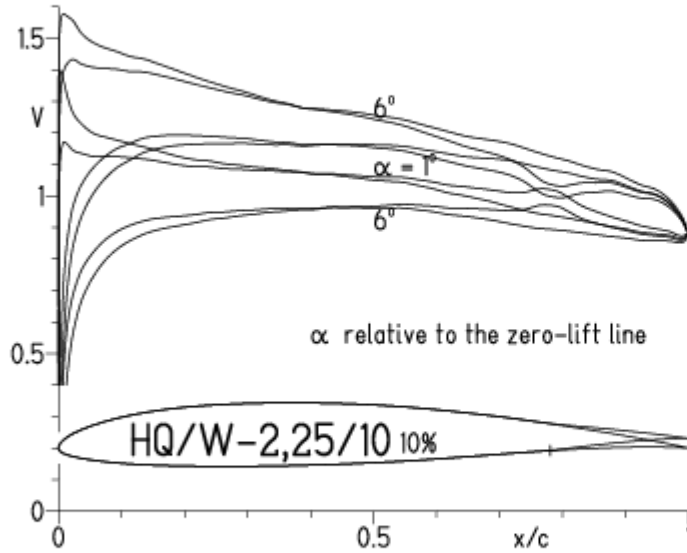
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

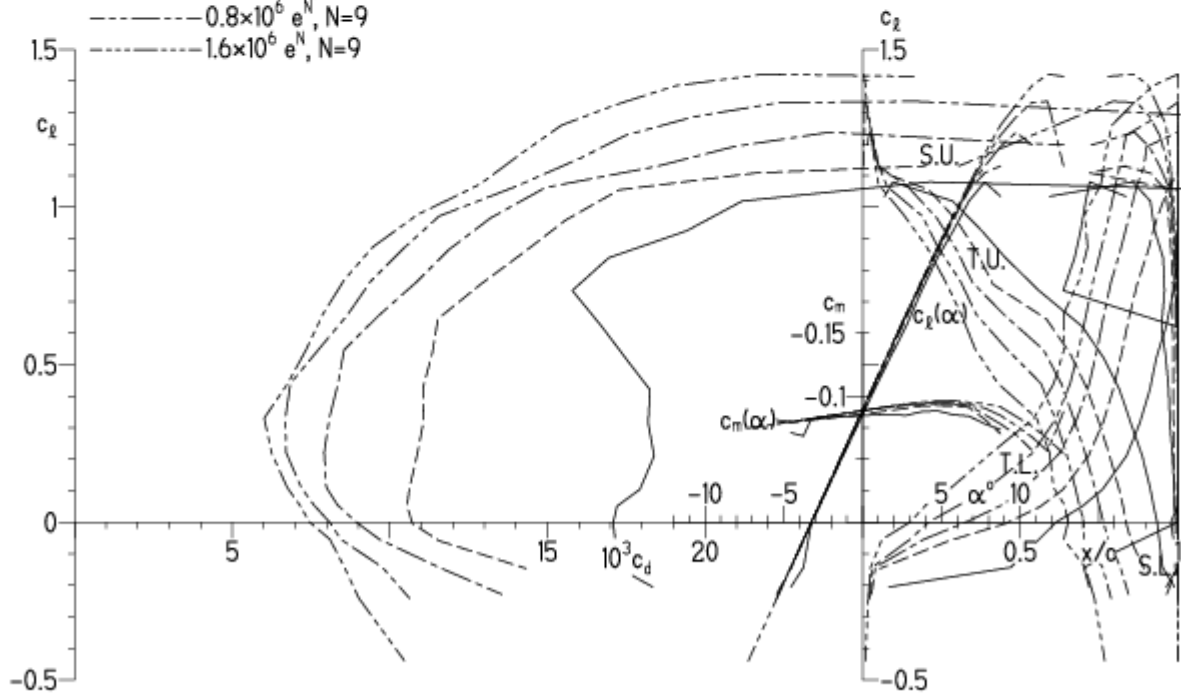
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

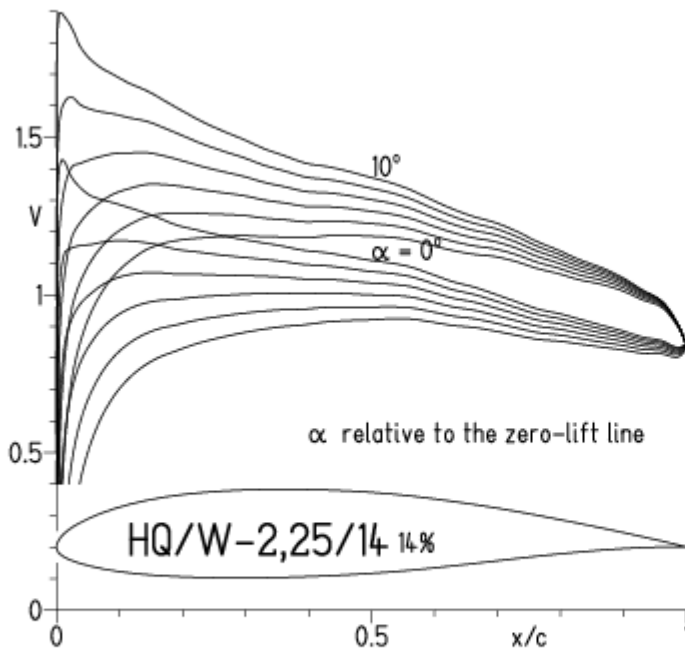


EPPLER 2005 V. 8.

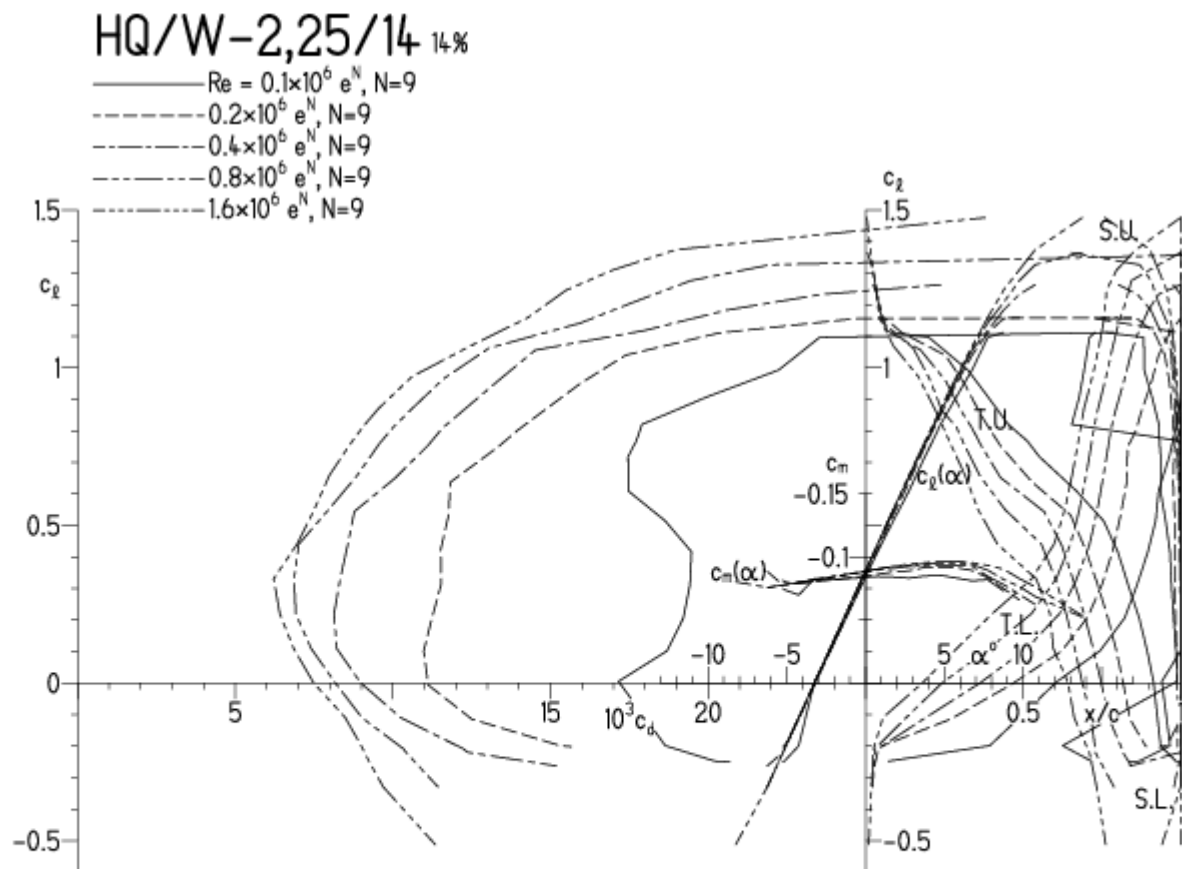


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

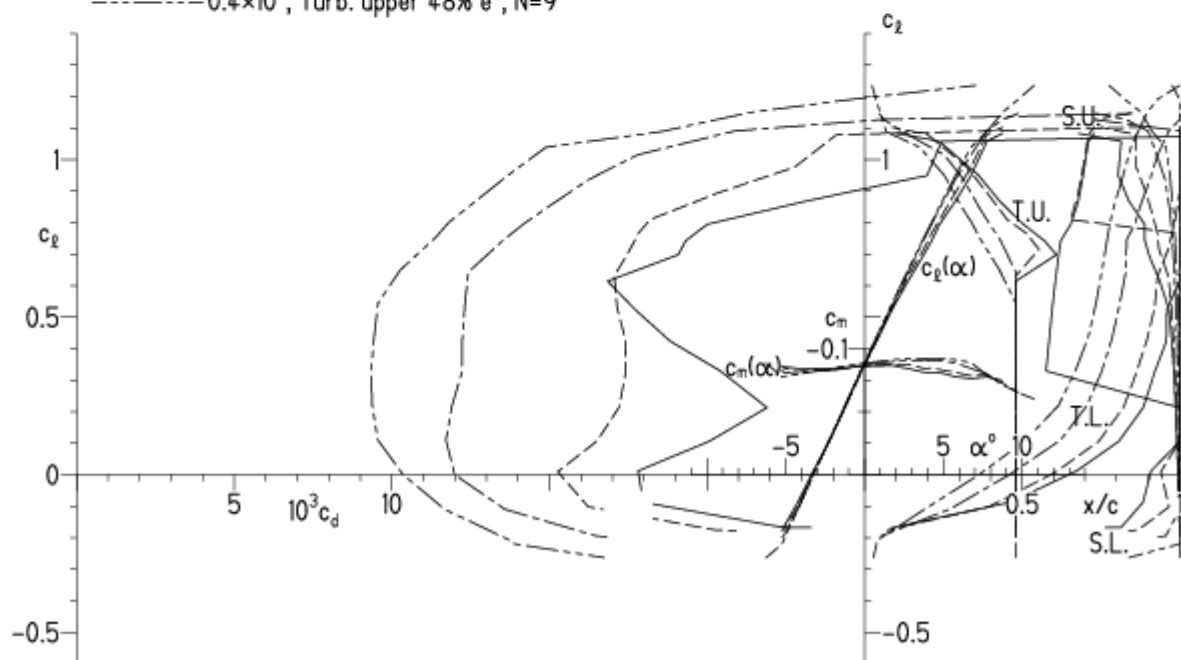
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

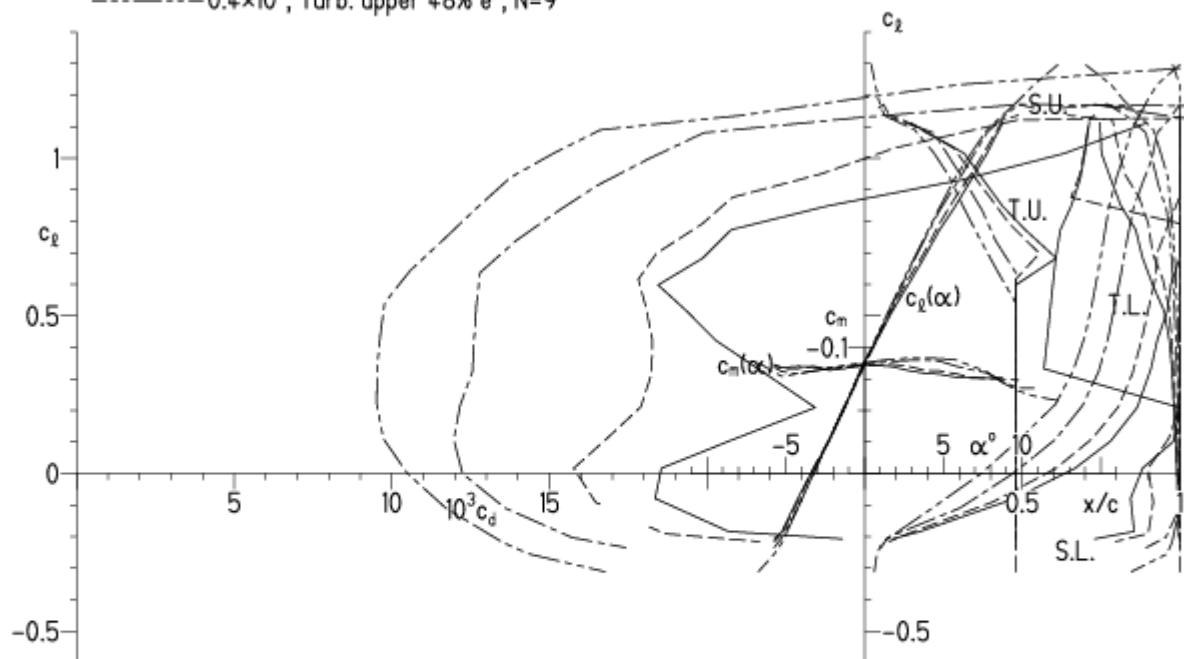
EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

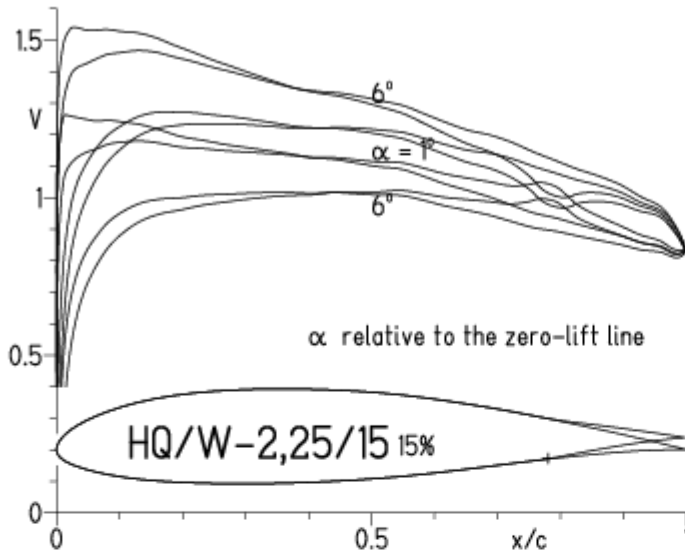


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

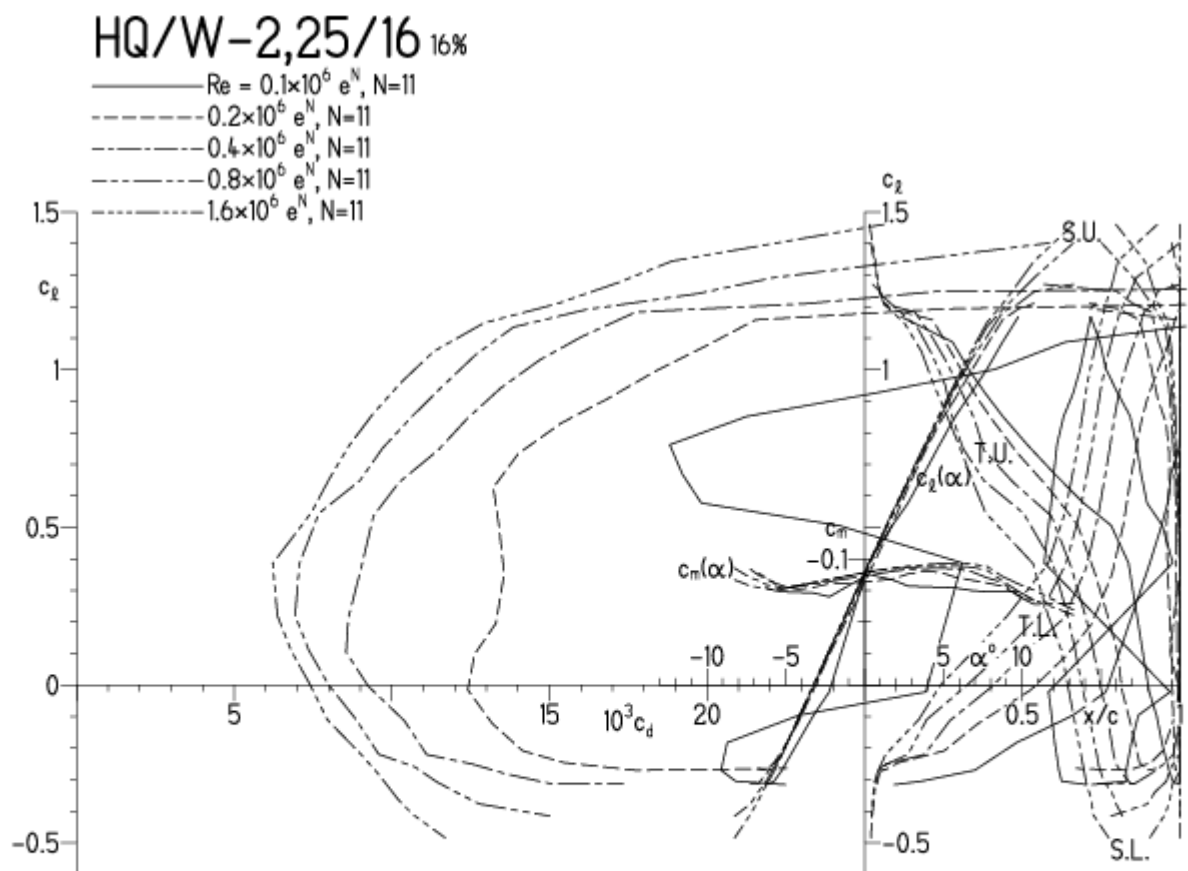


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

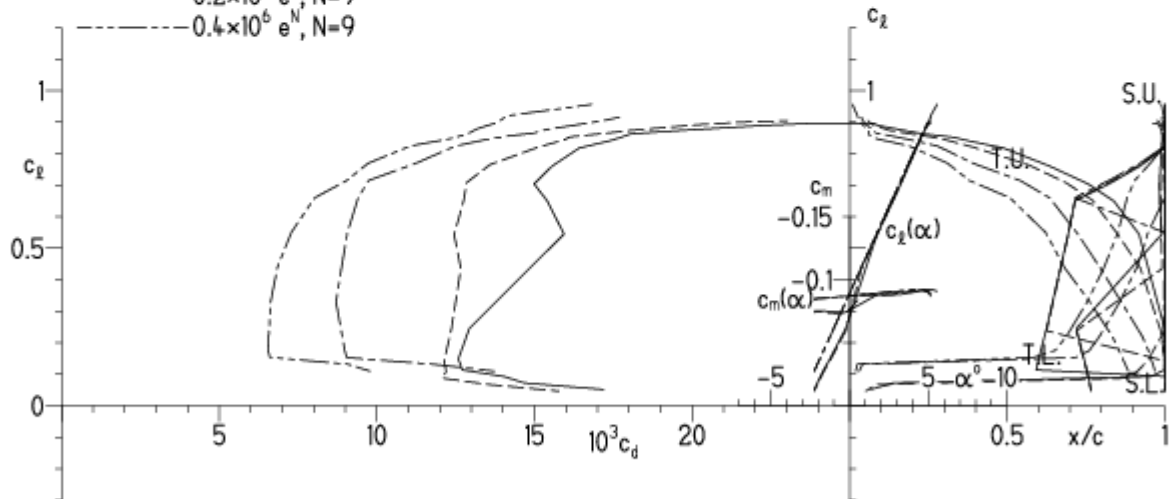
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



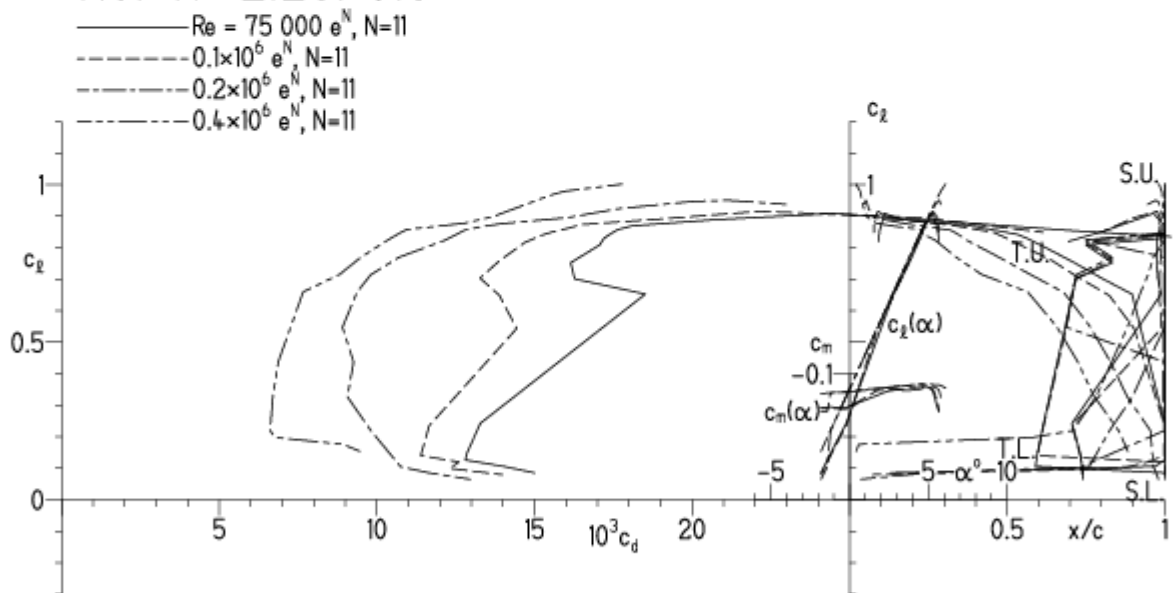
HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

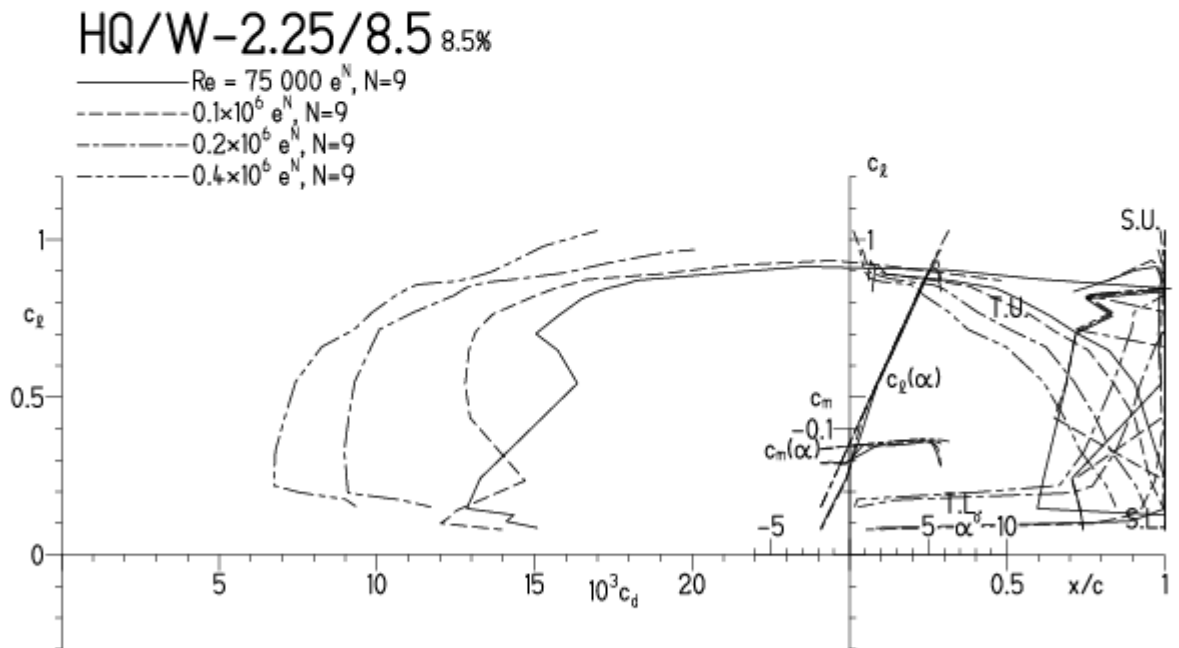


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

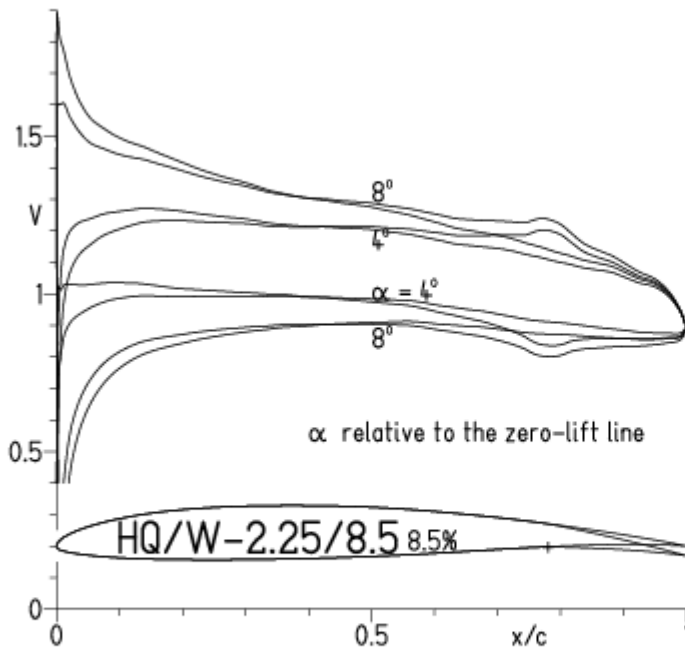
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

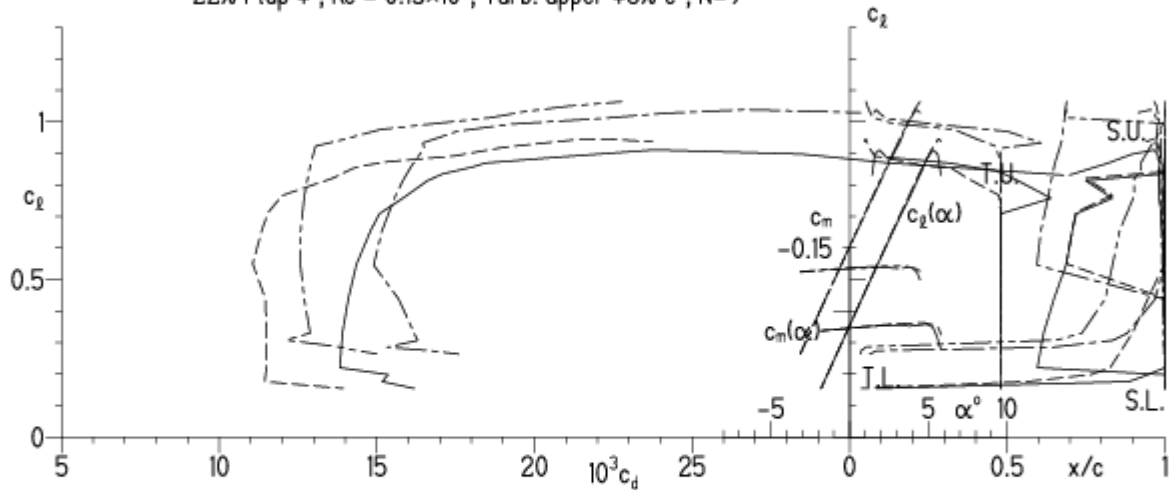


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

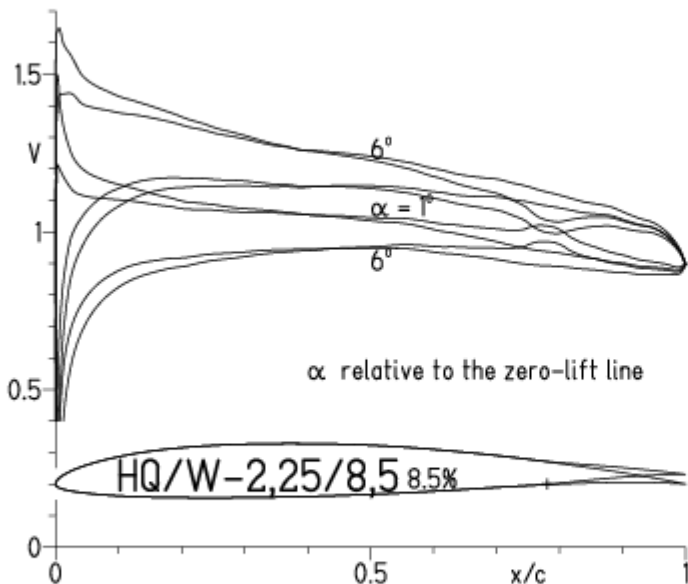
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15 × 10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

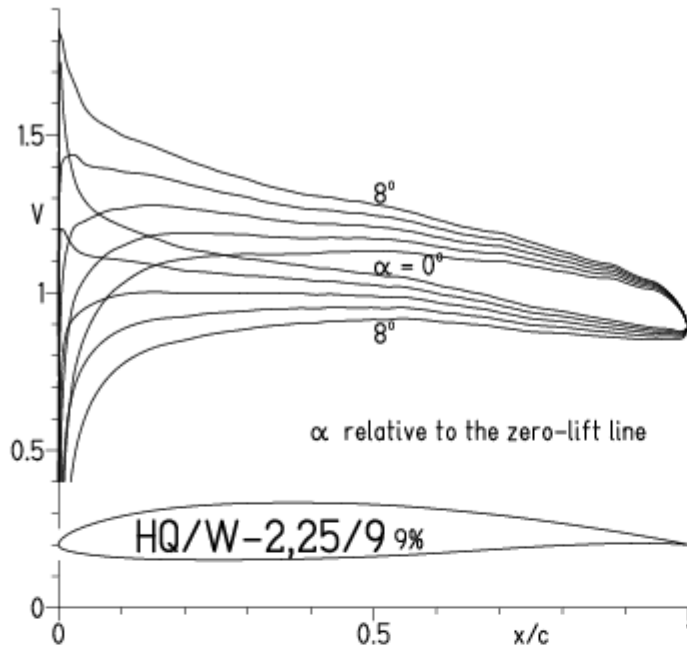


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

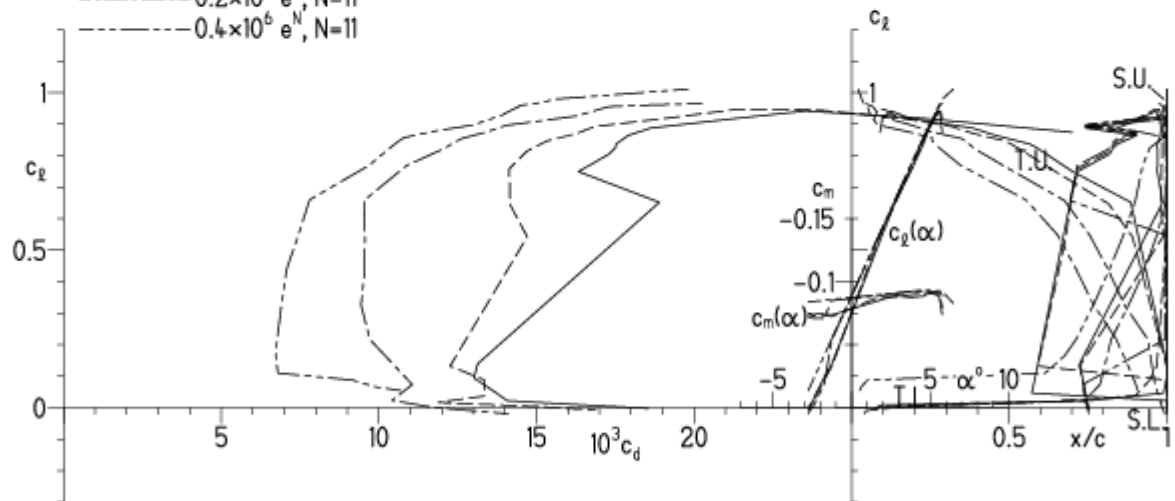
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

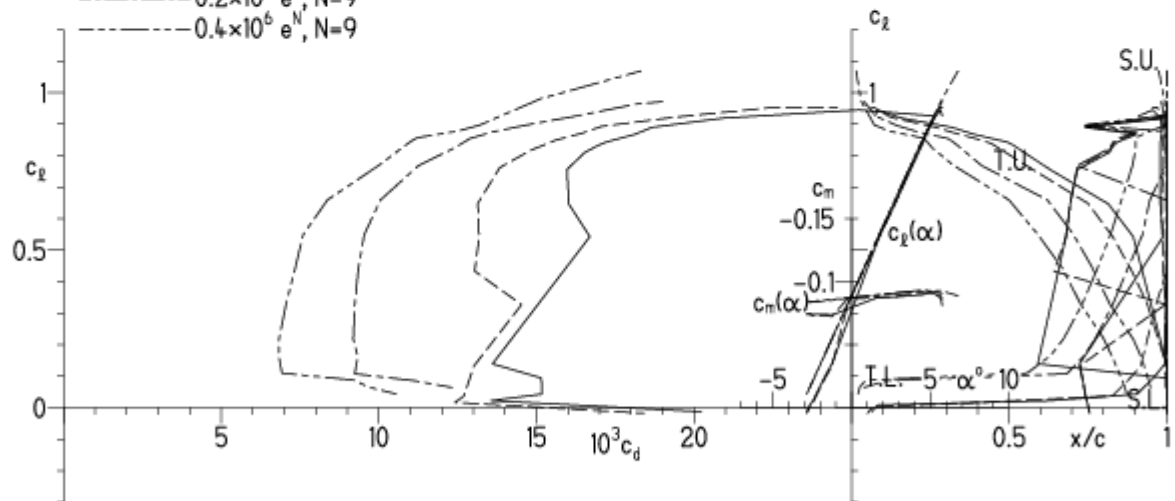
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

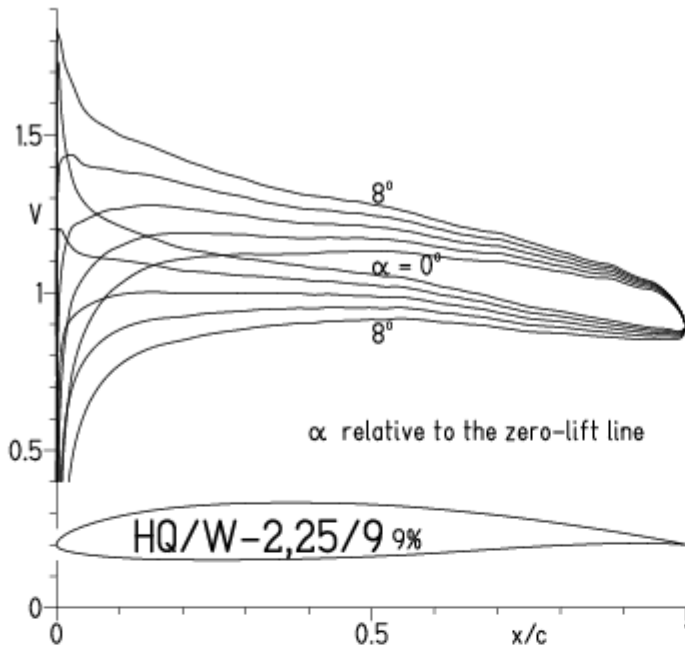
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

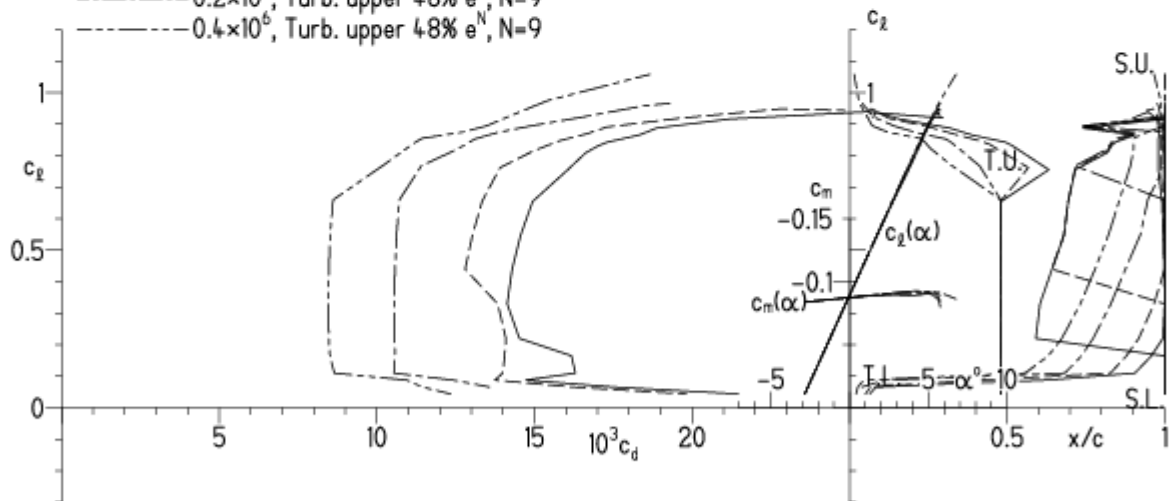
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48

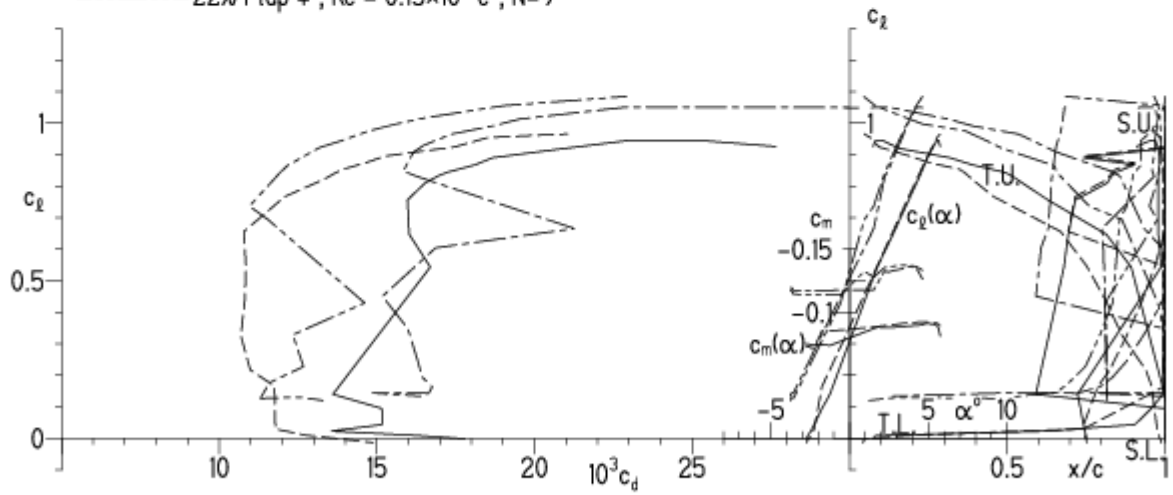


EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

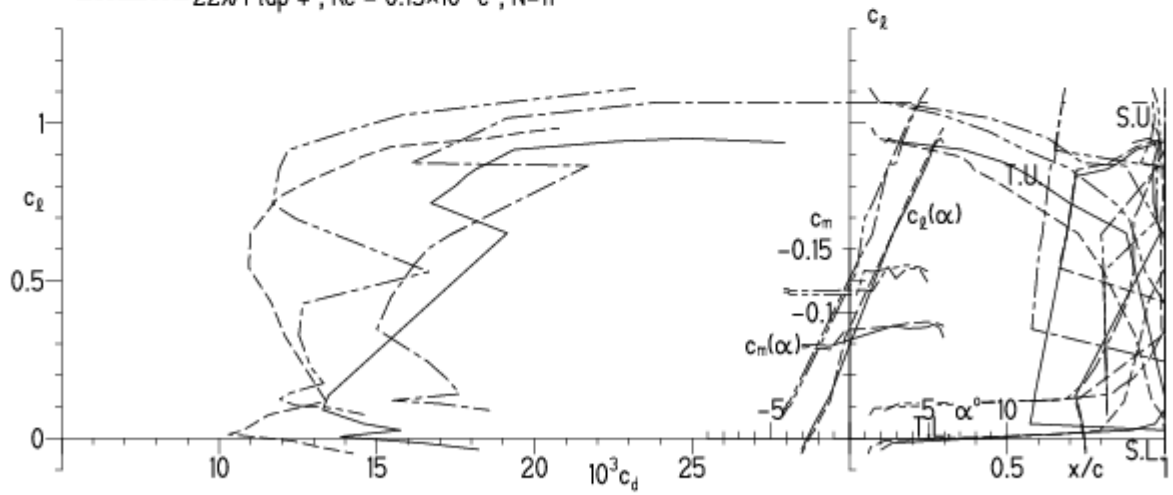


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

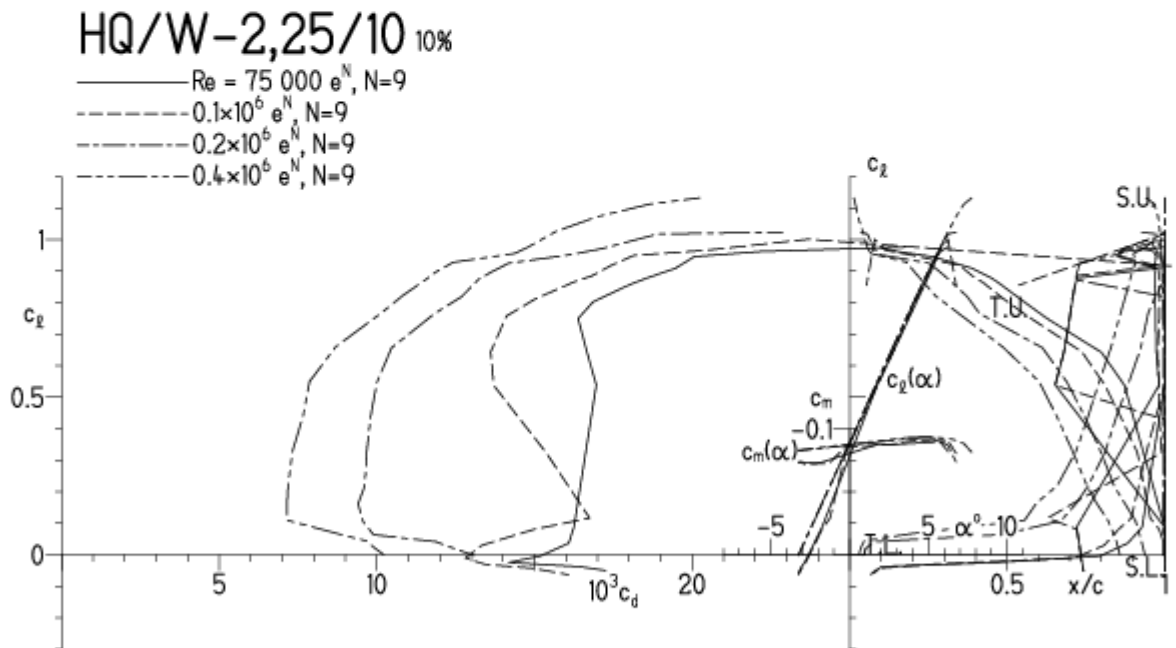


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

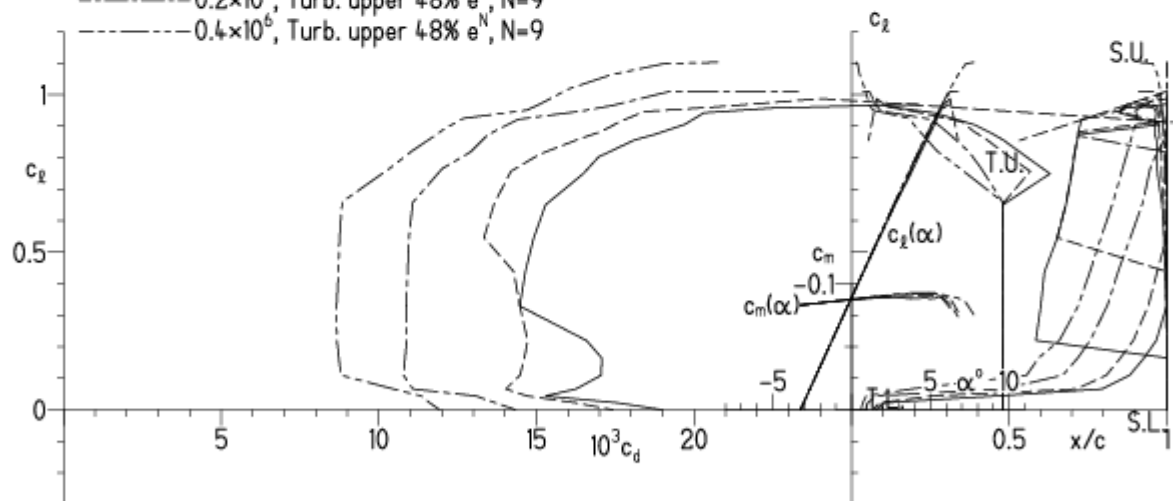
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

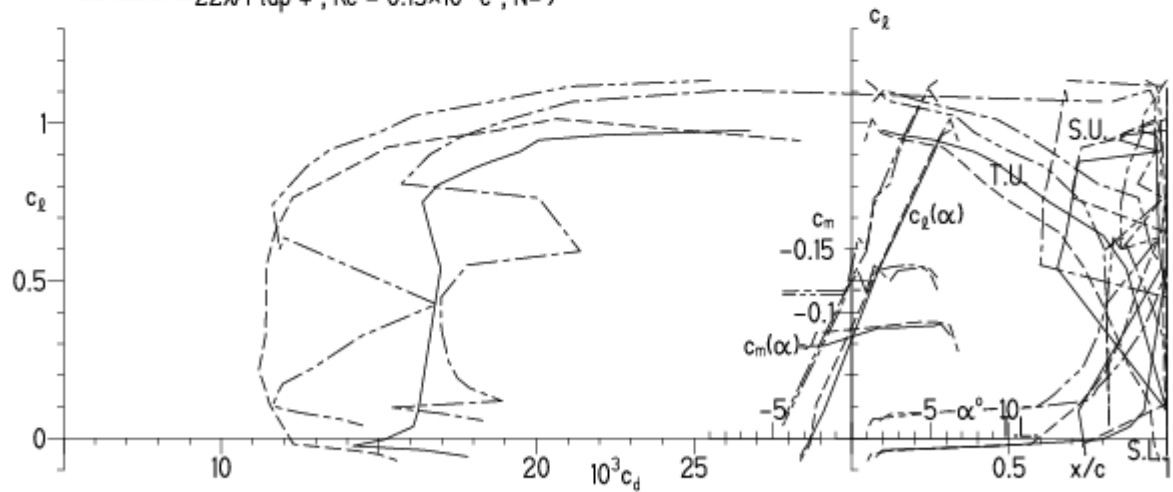


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

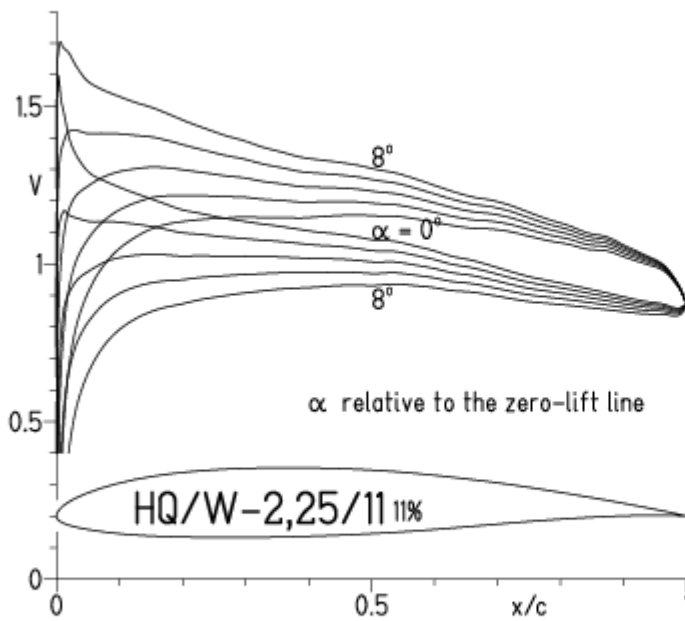


EPPLER 2005 V. 8.5.07 RUN

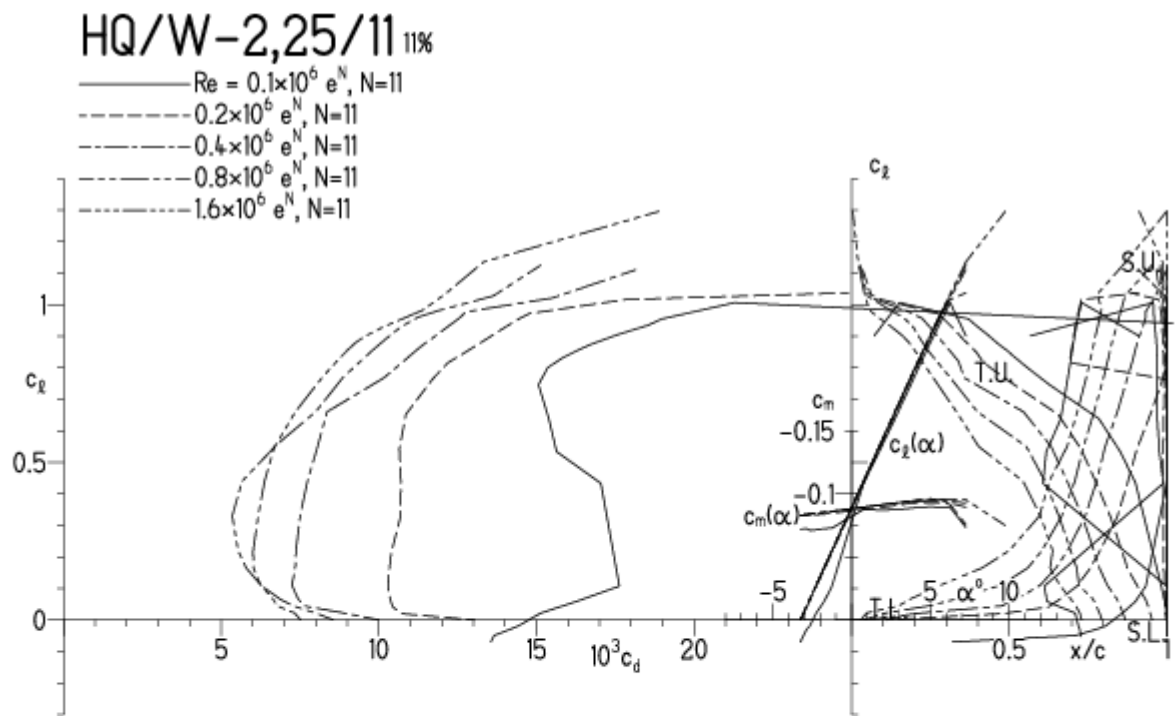


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

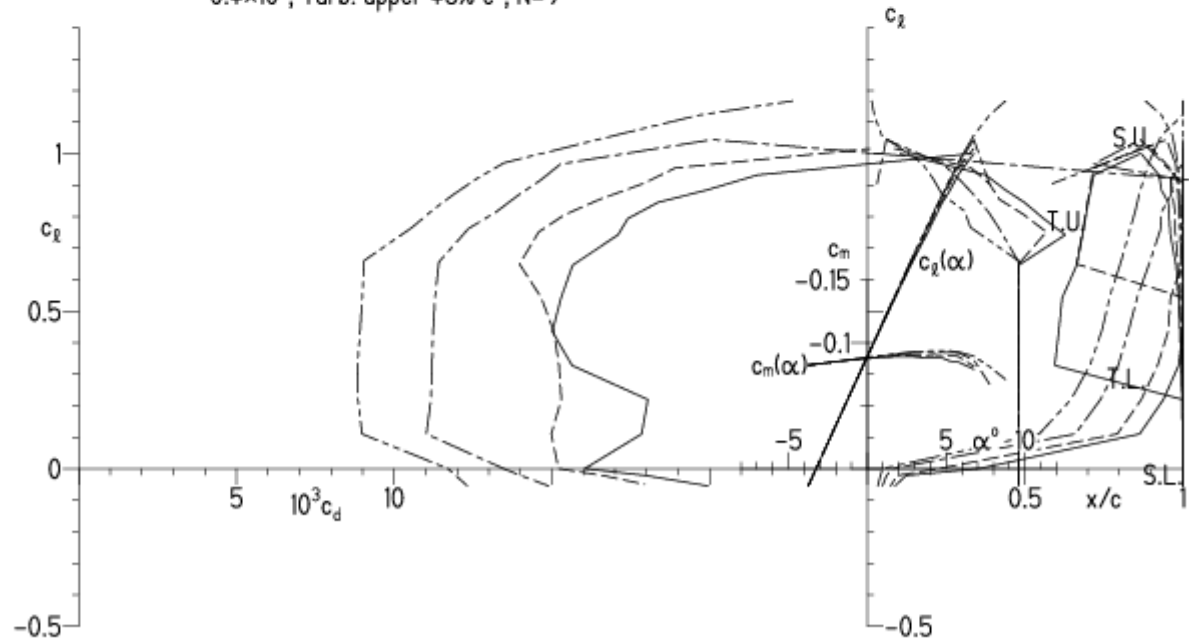
EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

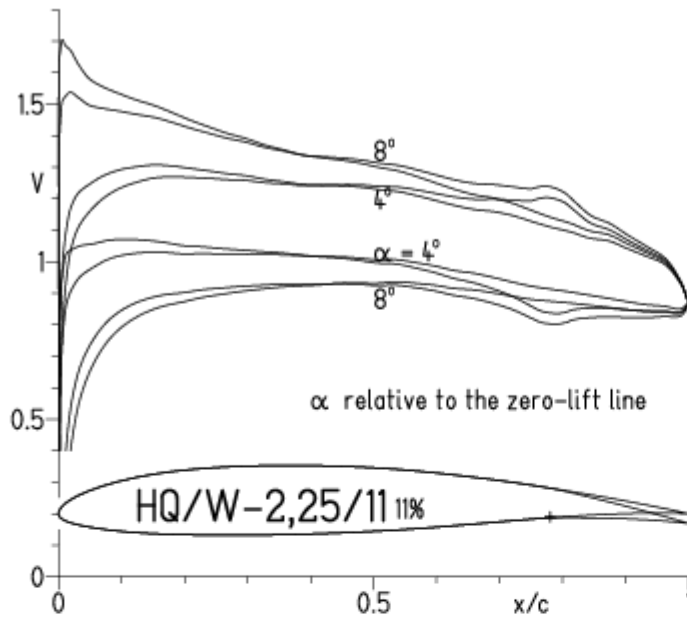
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6$, $N=11$
- - - 0.2×10^6 , $N=11$
- · - 0.4×10^6 , $N=11$
- · - 0.8×10^6 , $N=11$
- · - 1.6×10^6 , $N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

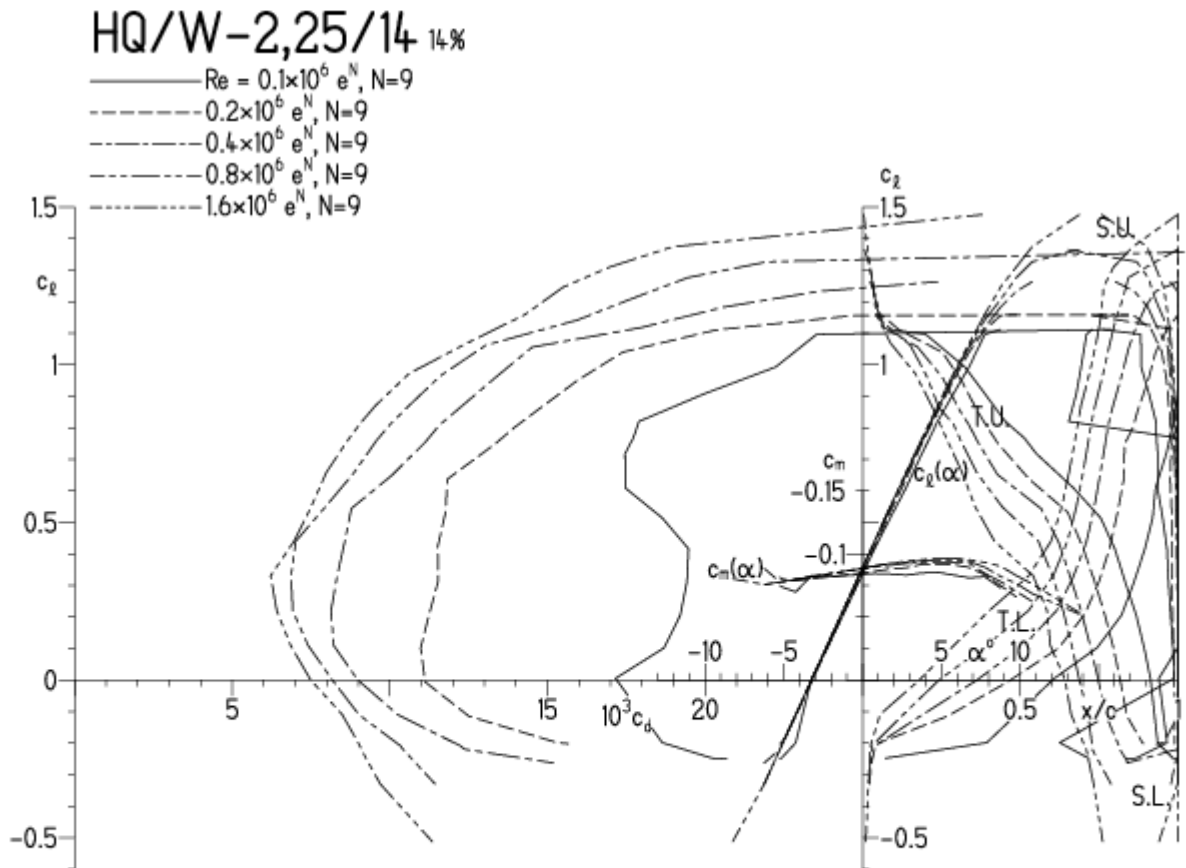


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

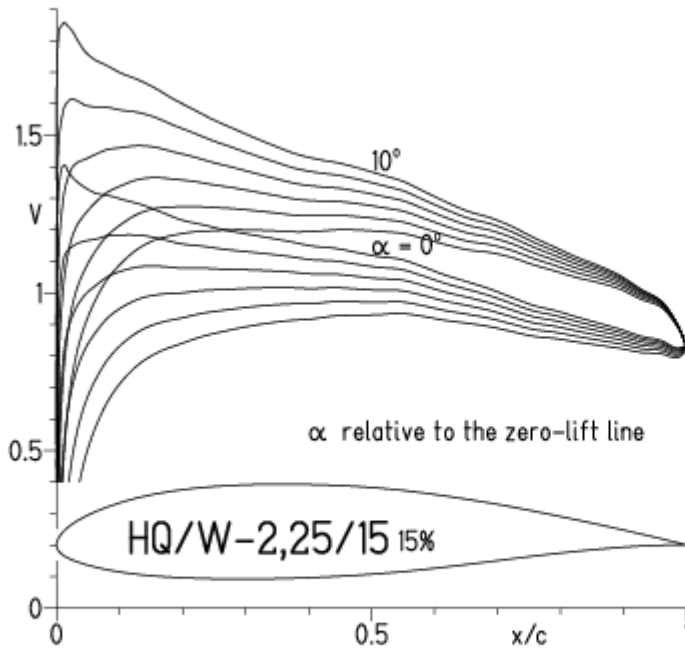


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

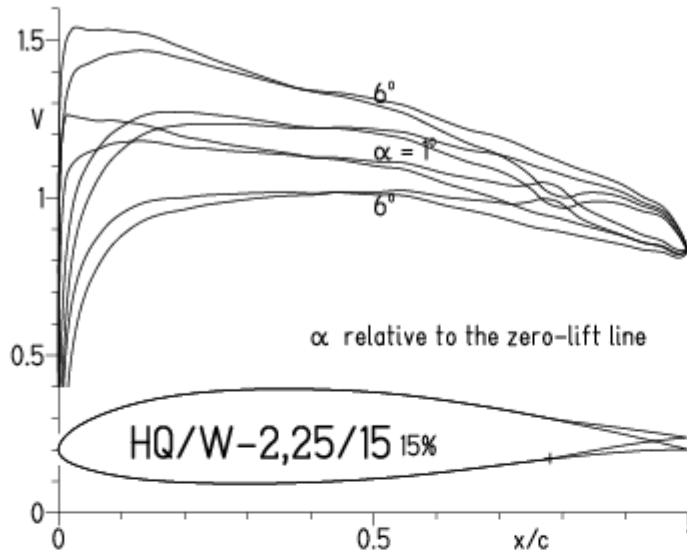


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

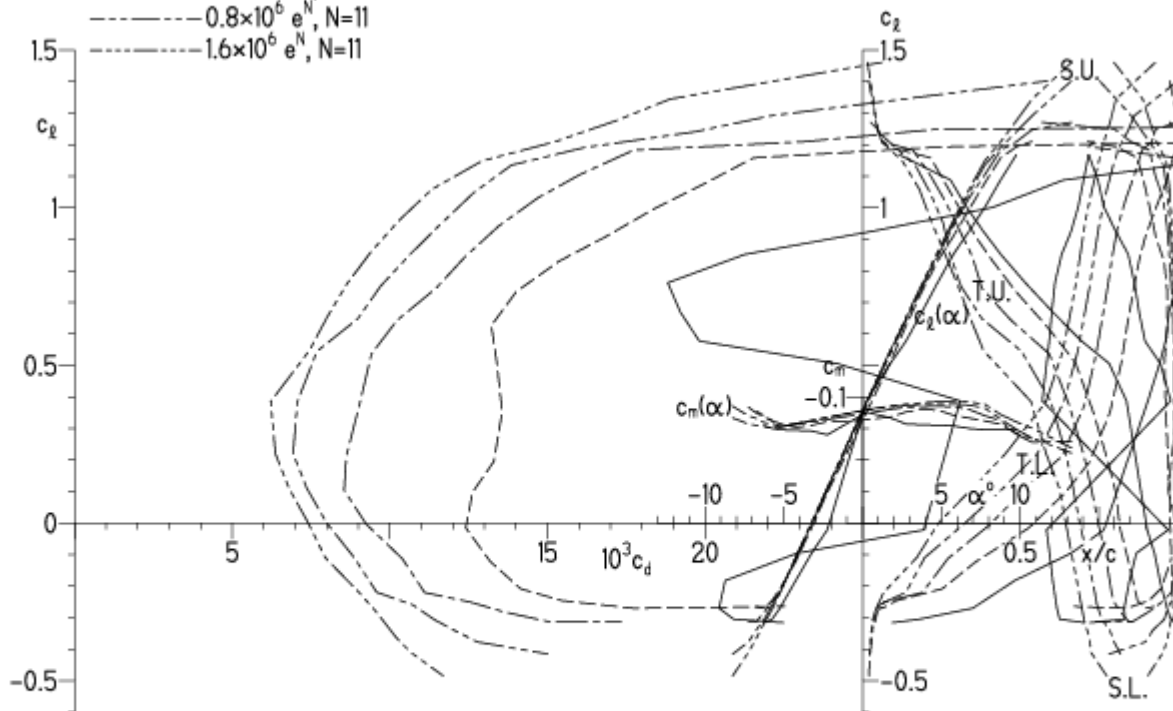
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · · - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2,25/8,5 8.5%

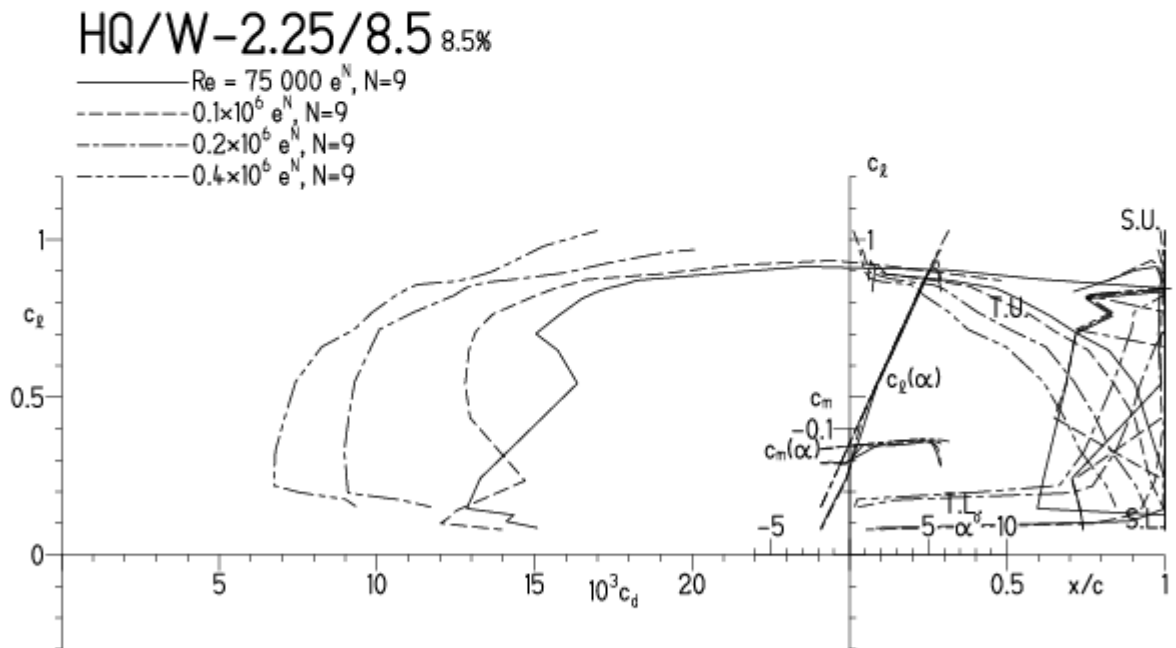


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

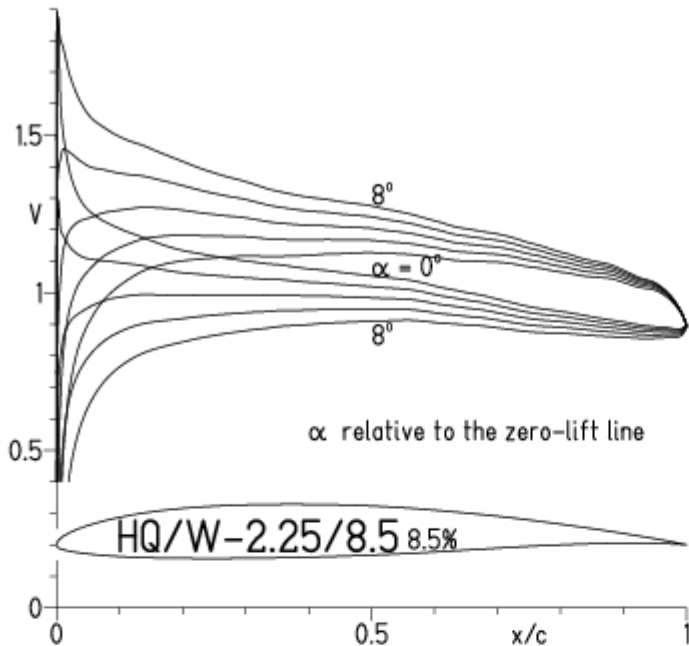


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

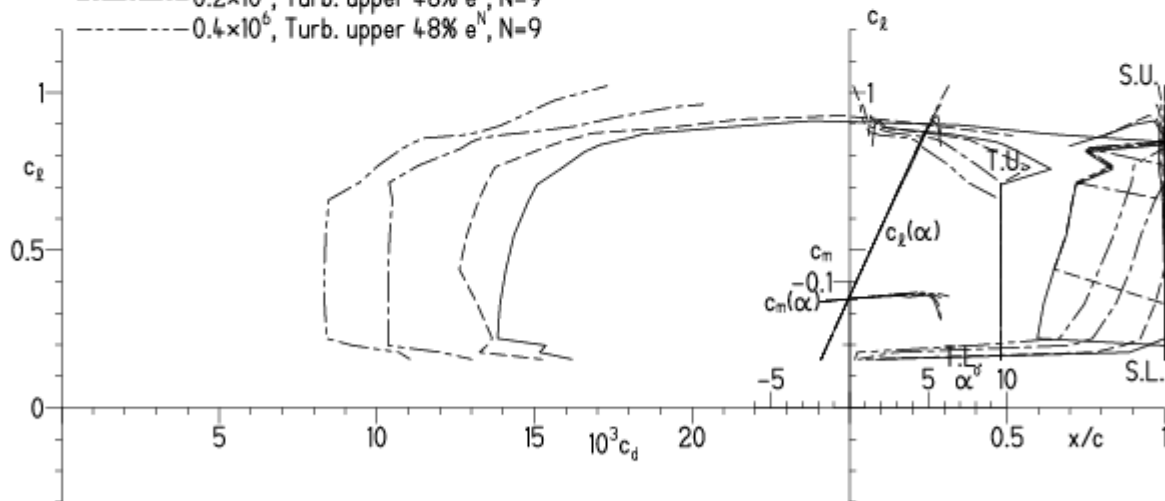
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4°, $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

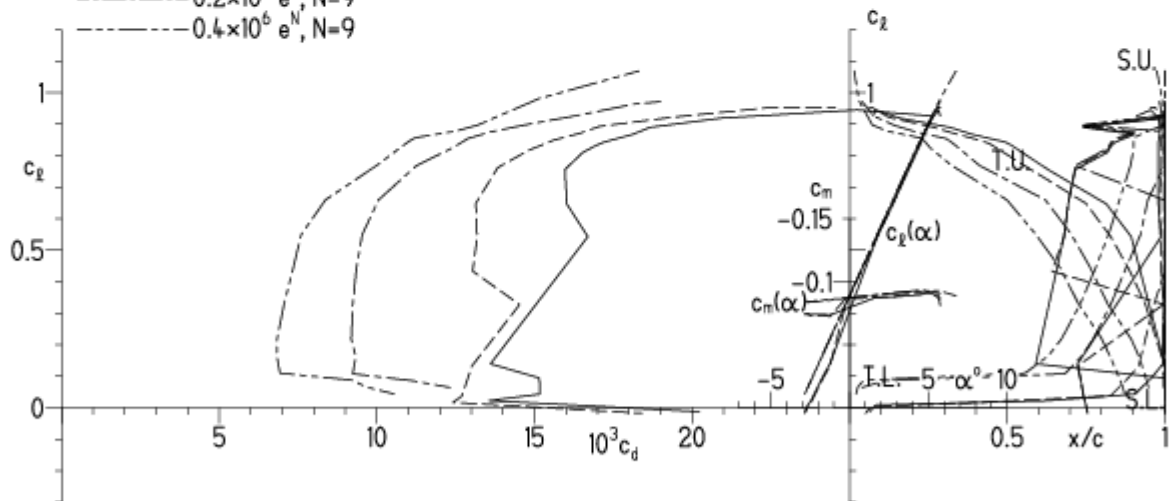
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

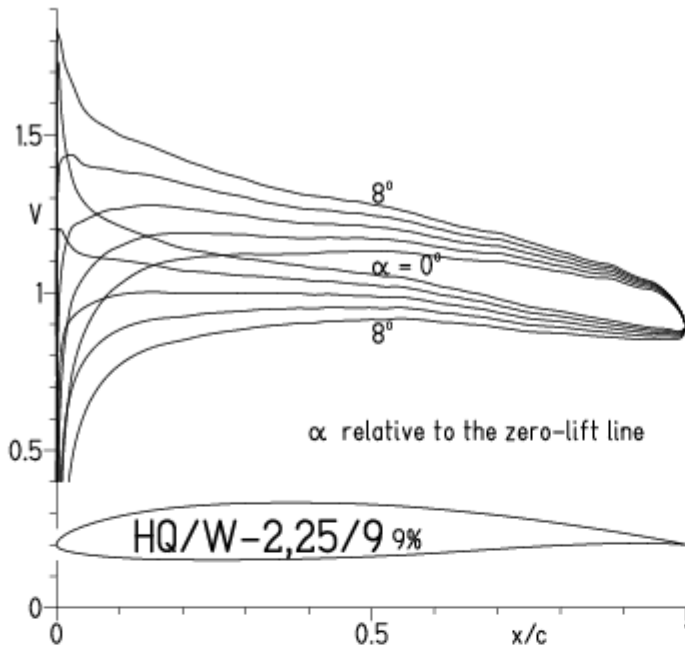
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · · - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

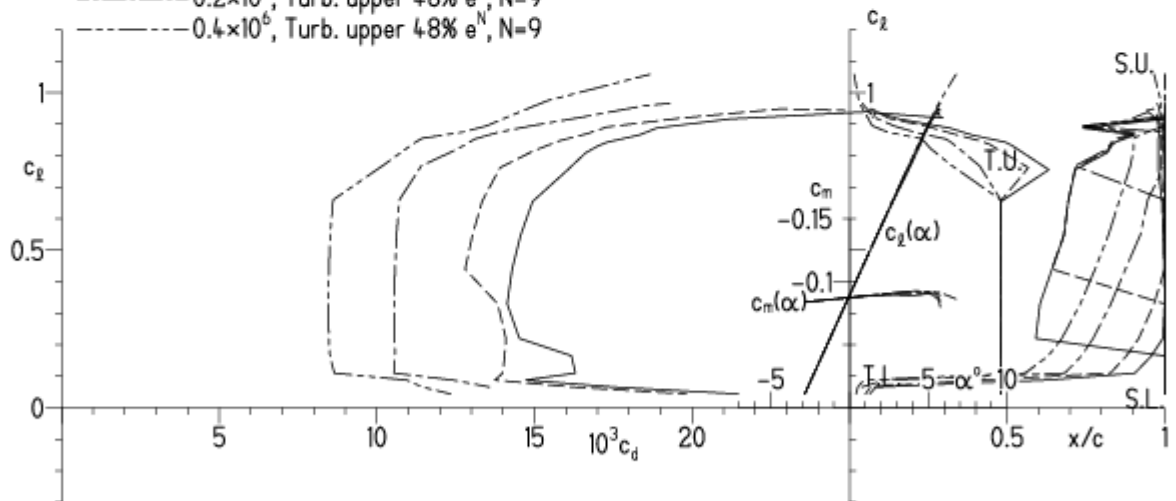
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

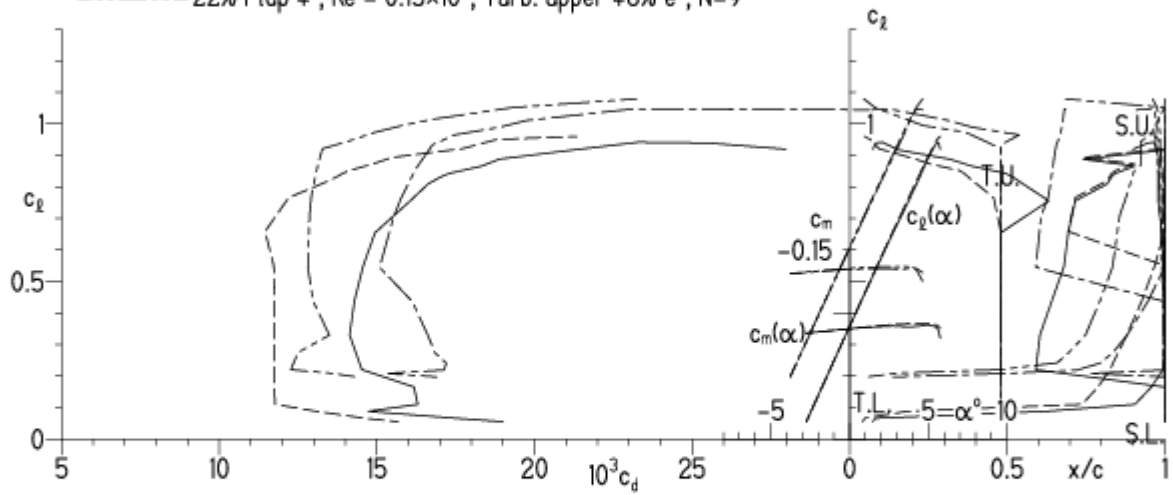


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

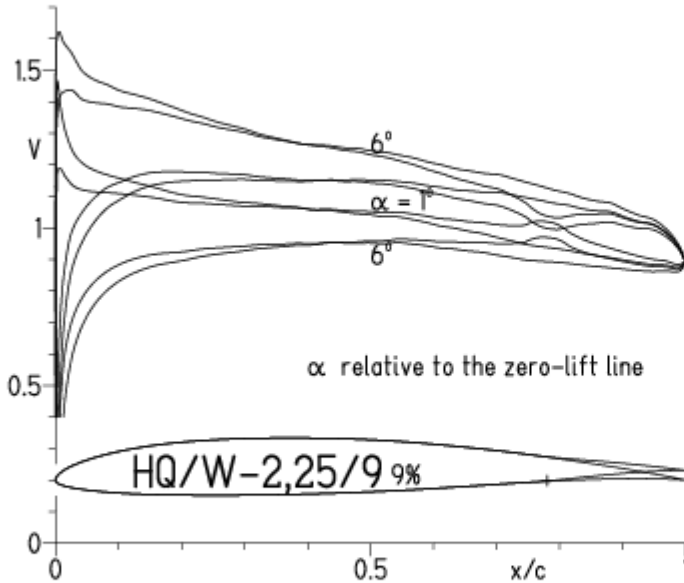
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

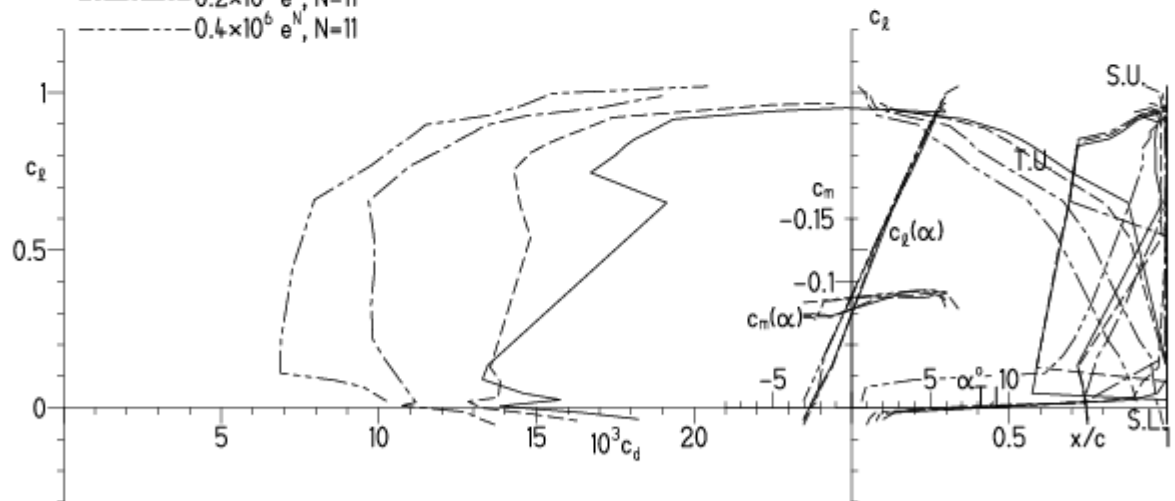
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



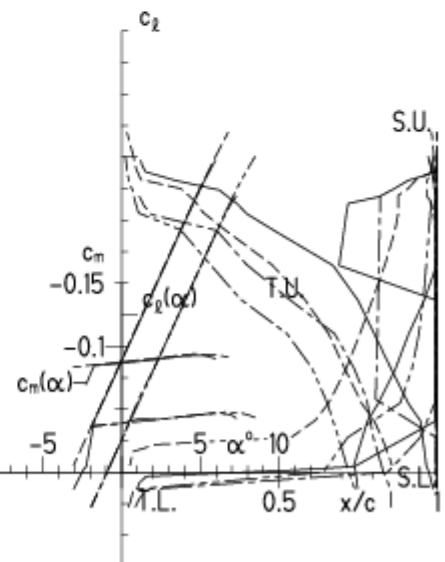
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

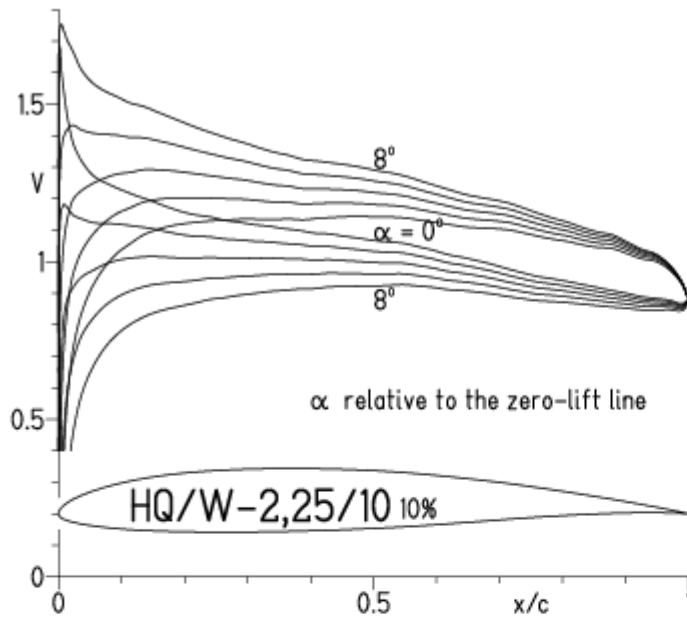


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

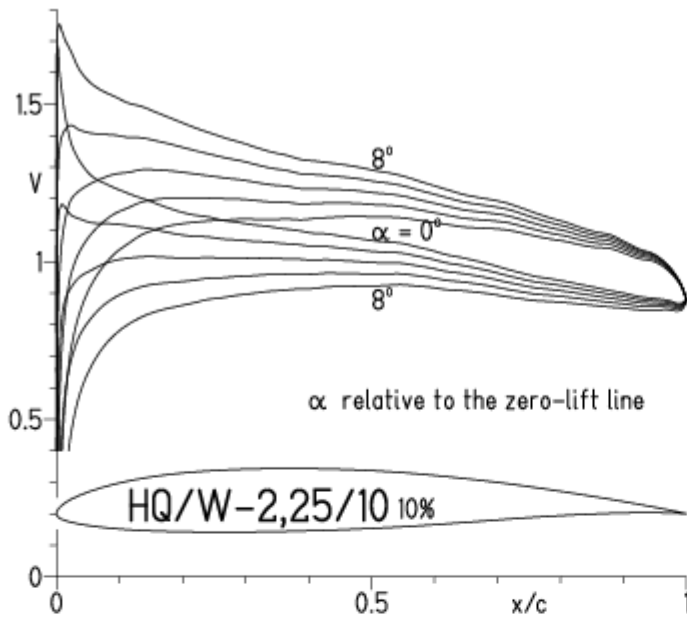


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

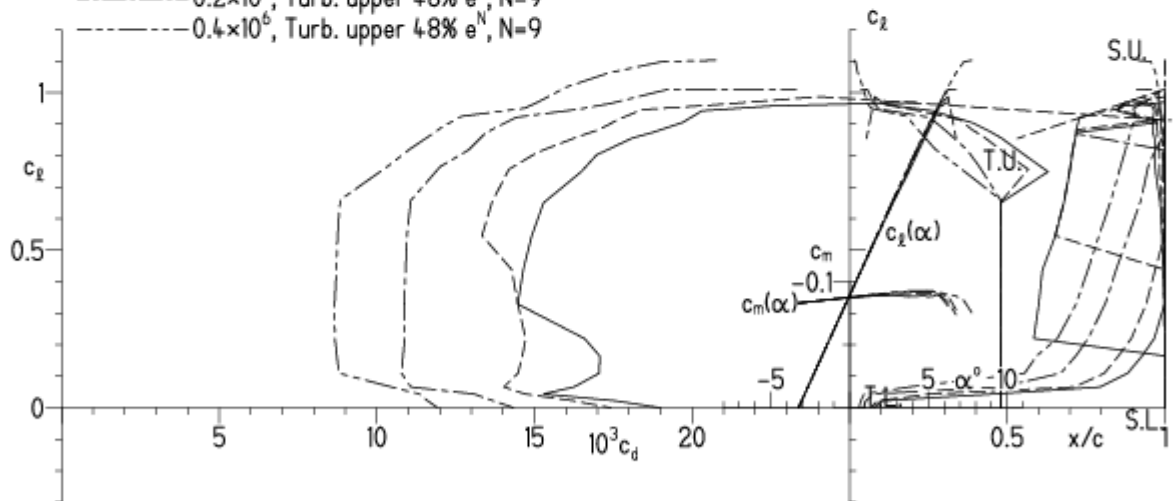
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - · 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

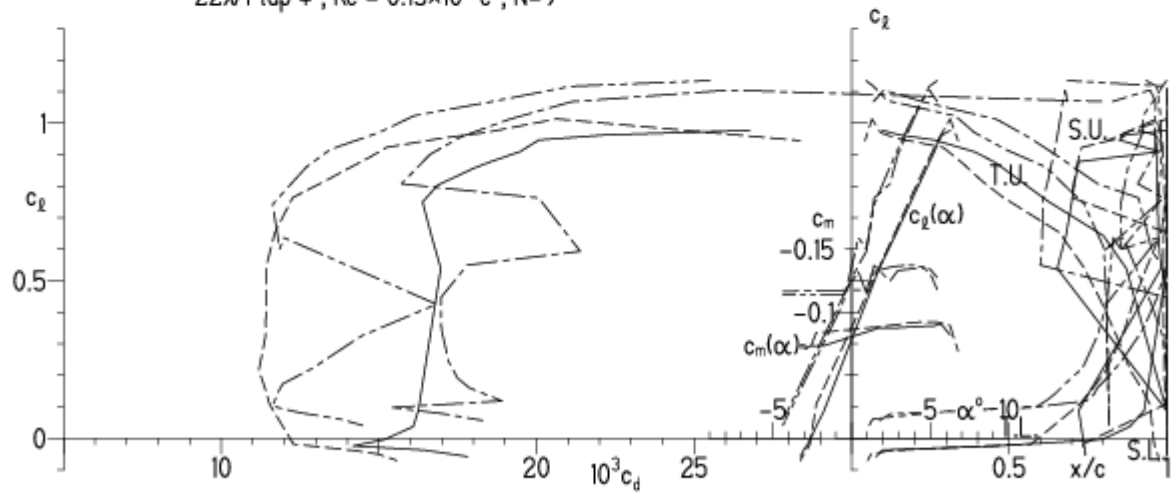


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

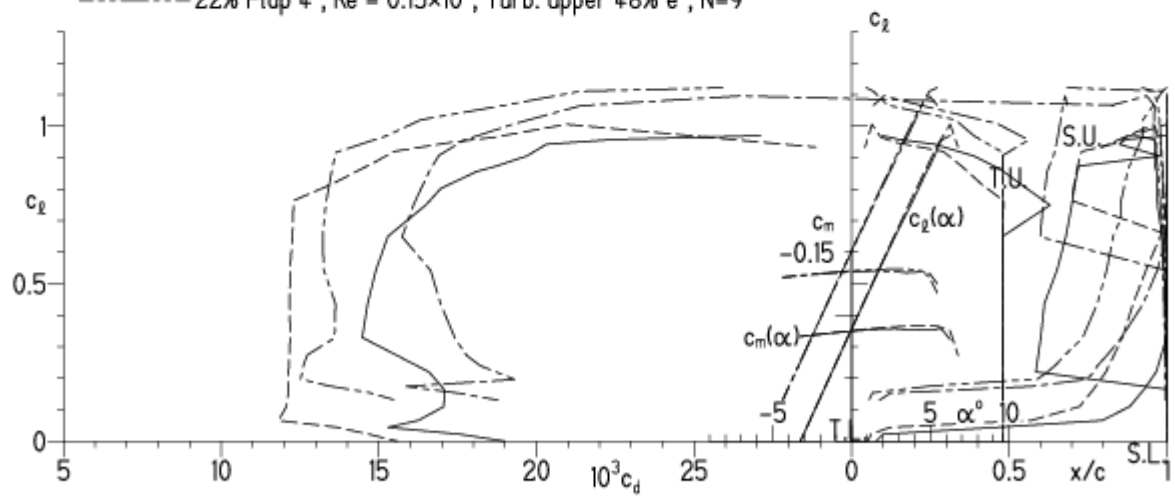


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52

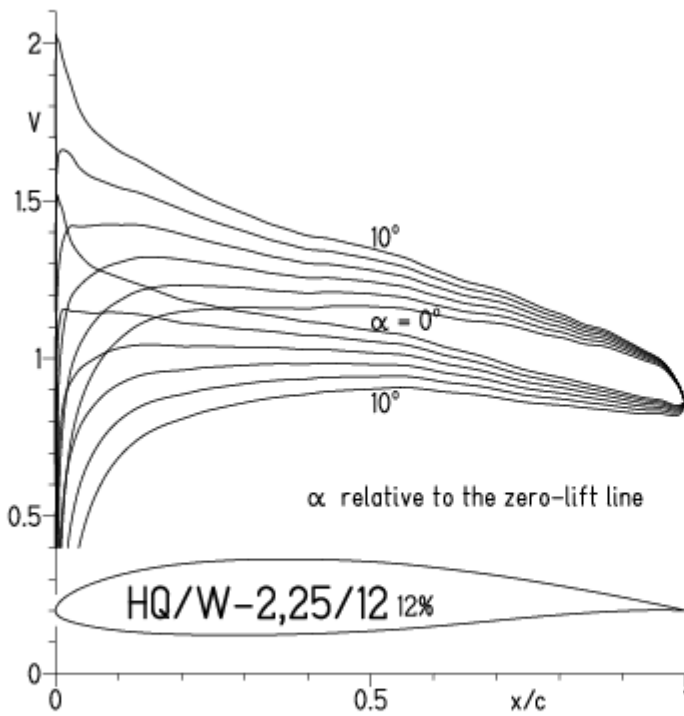


EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

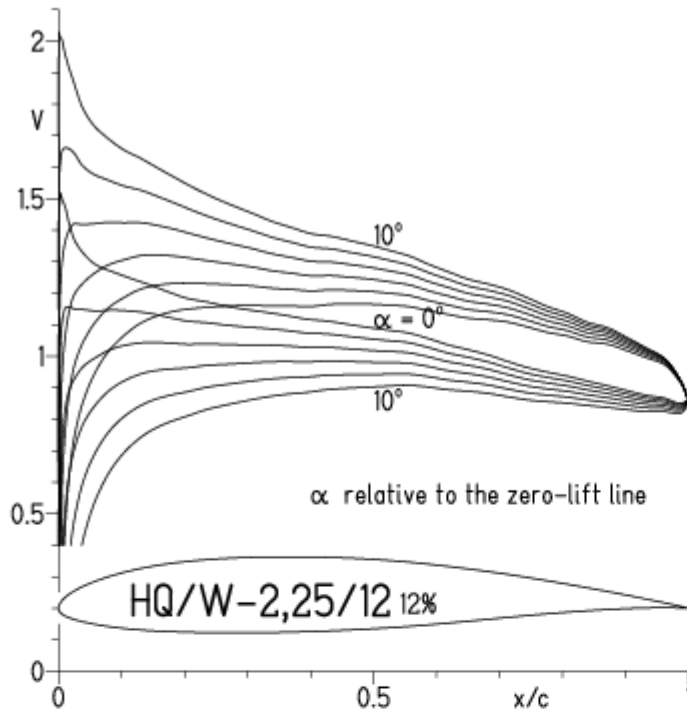
HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

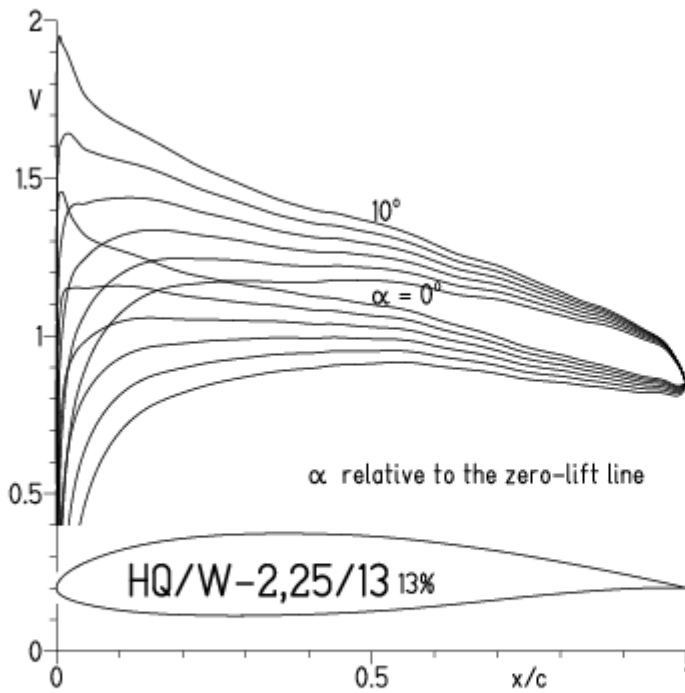


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

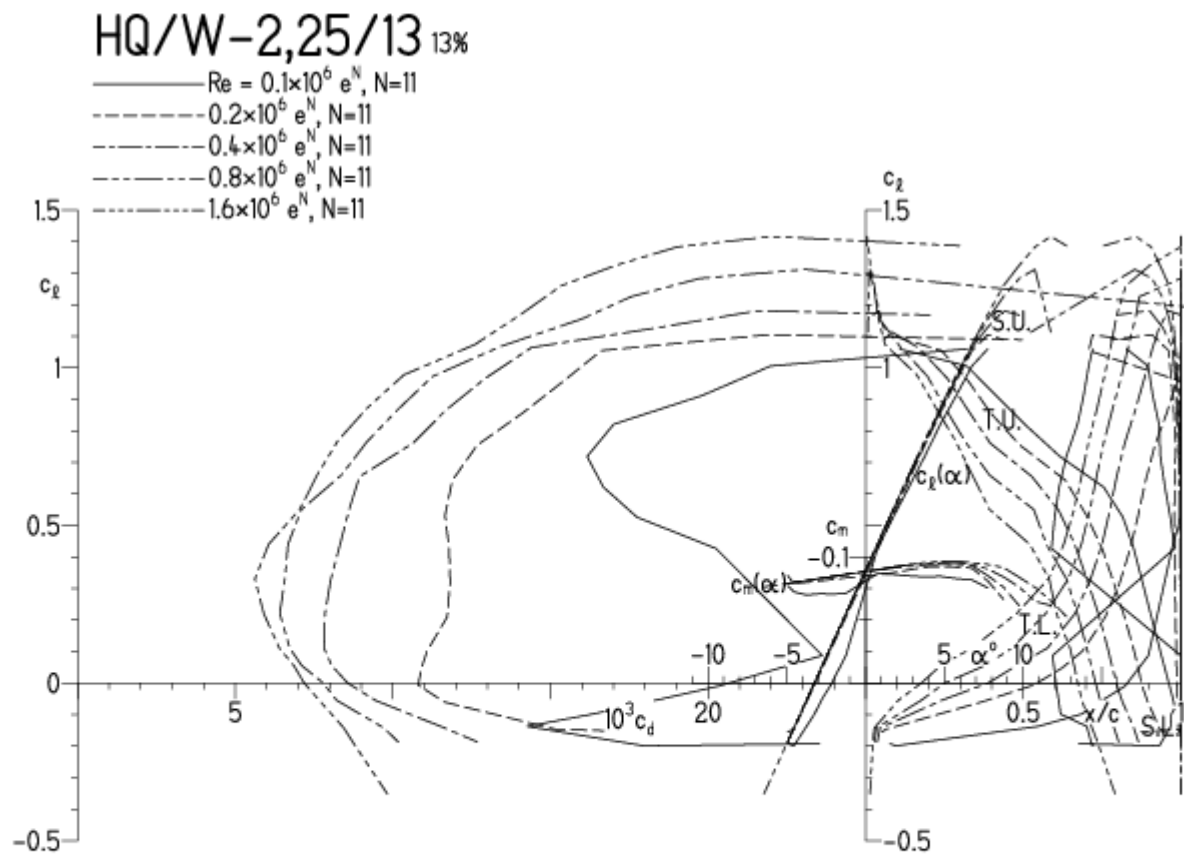


HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

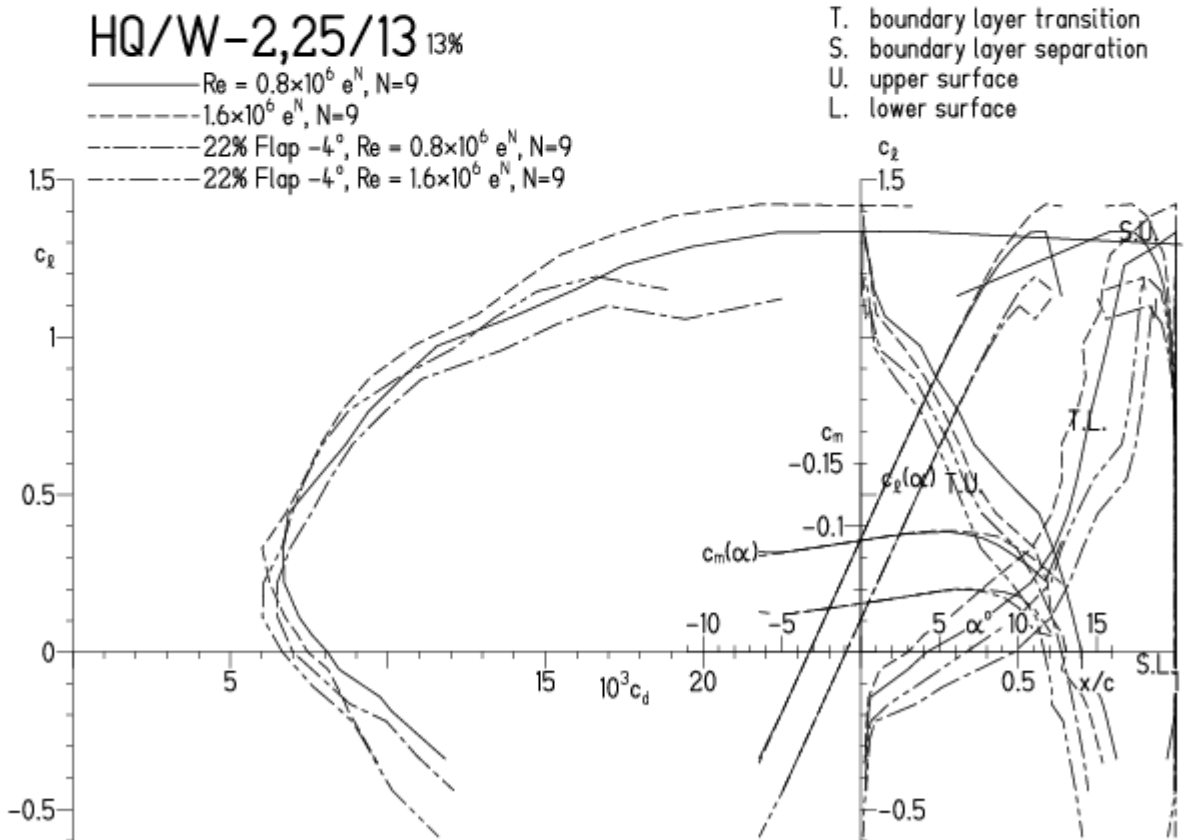


HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

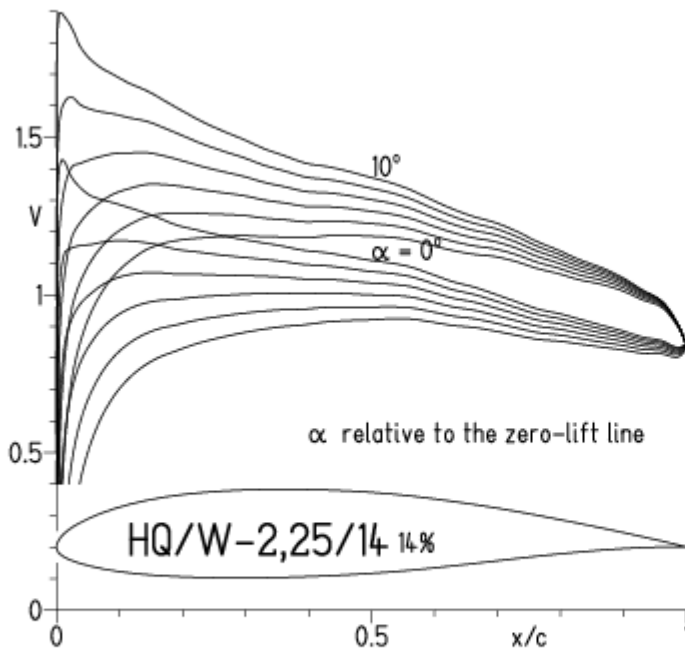


EPPLER 2005 V. 8.

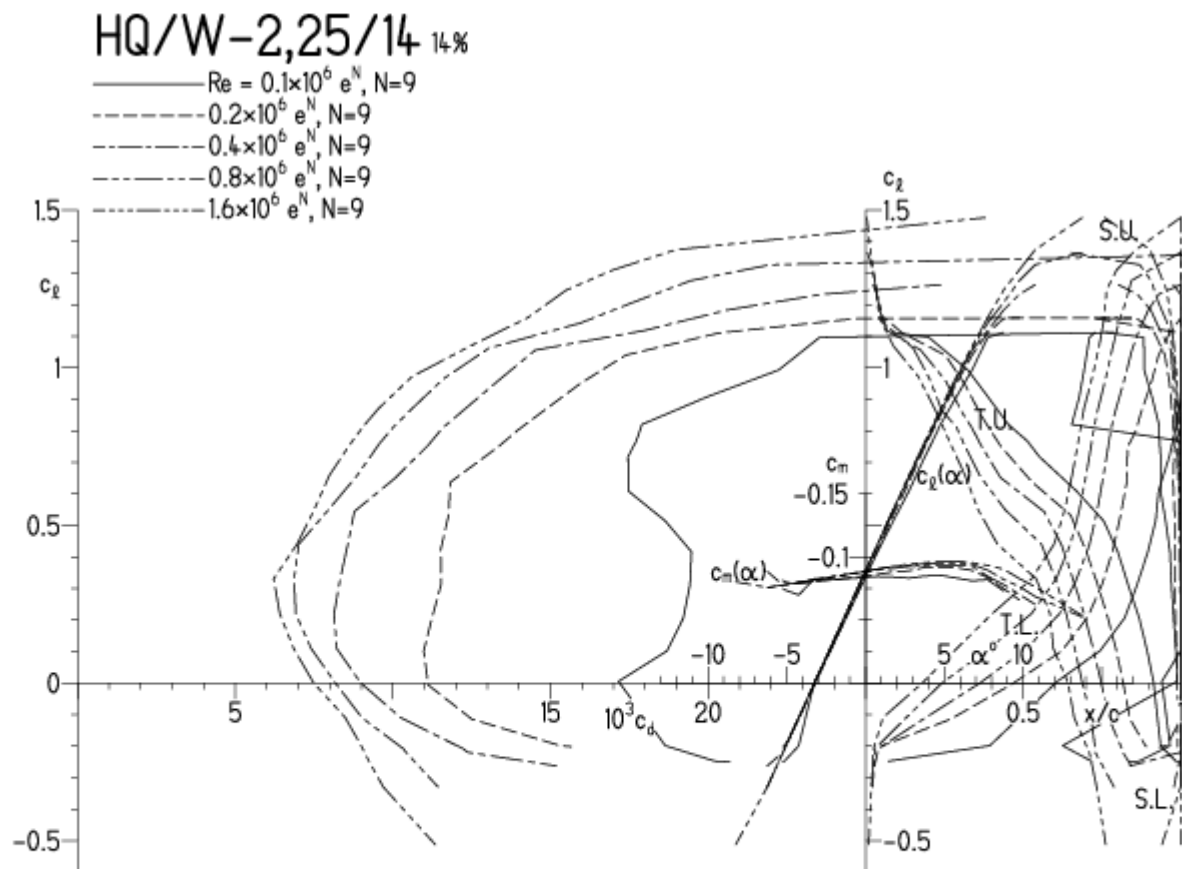


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

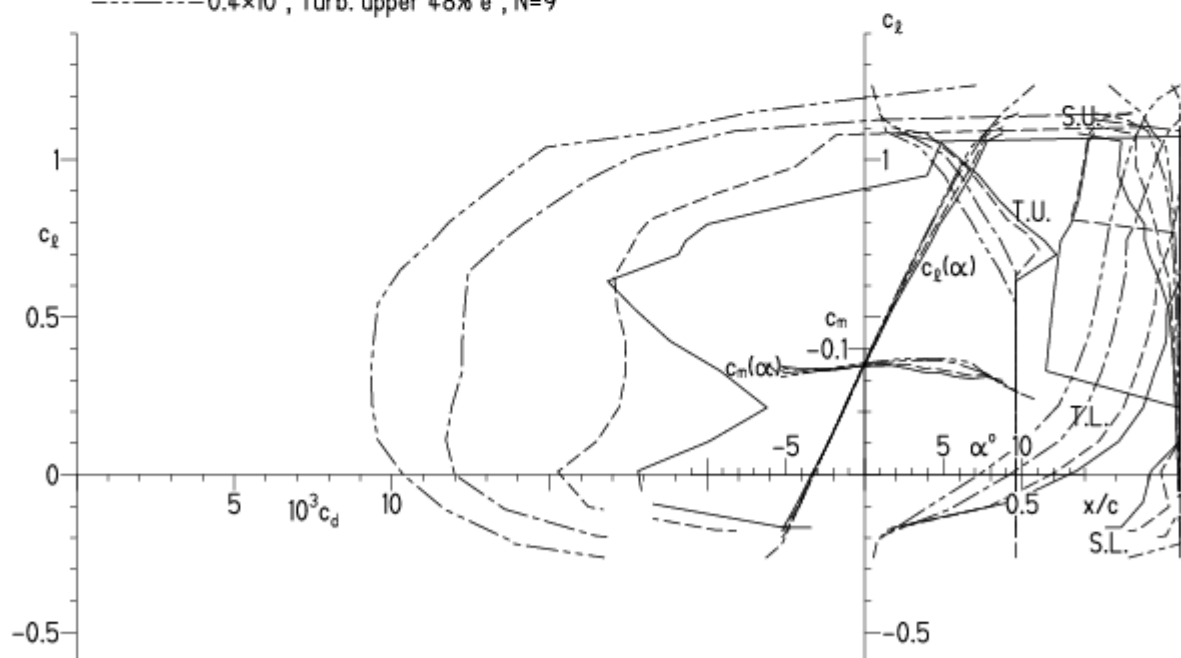
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

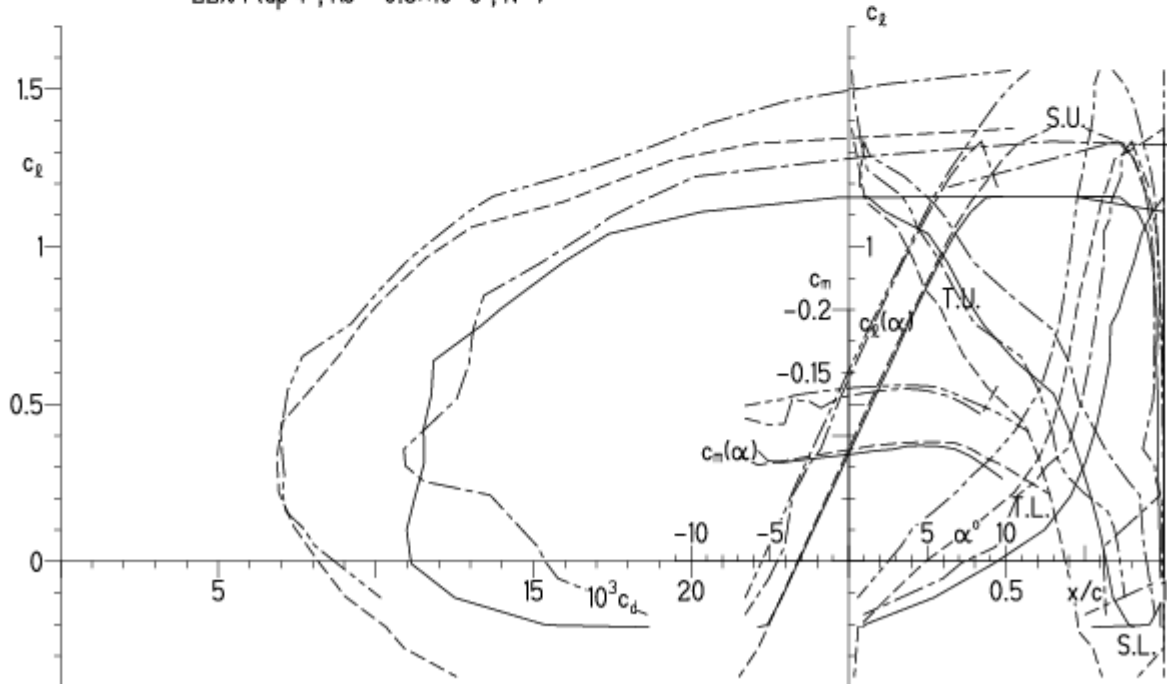


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

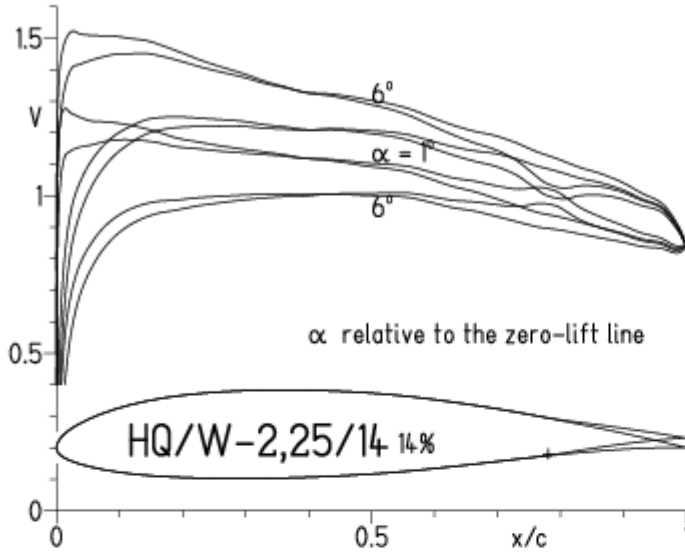
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

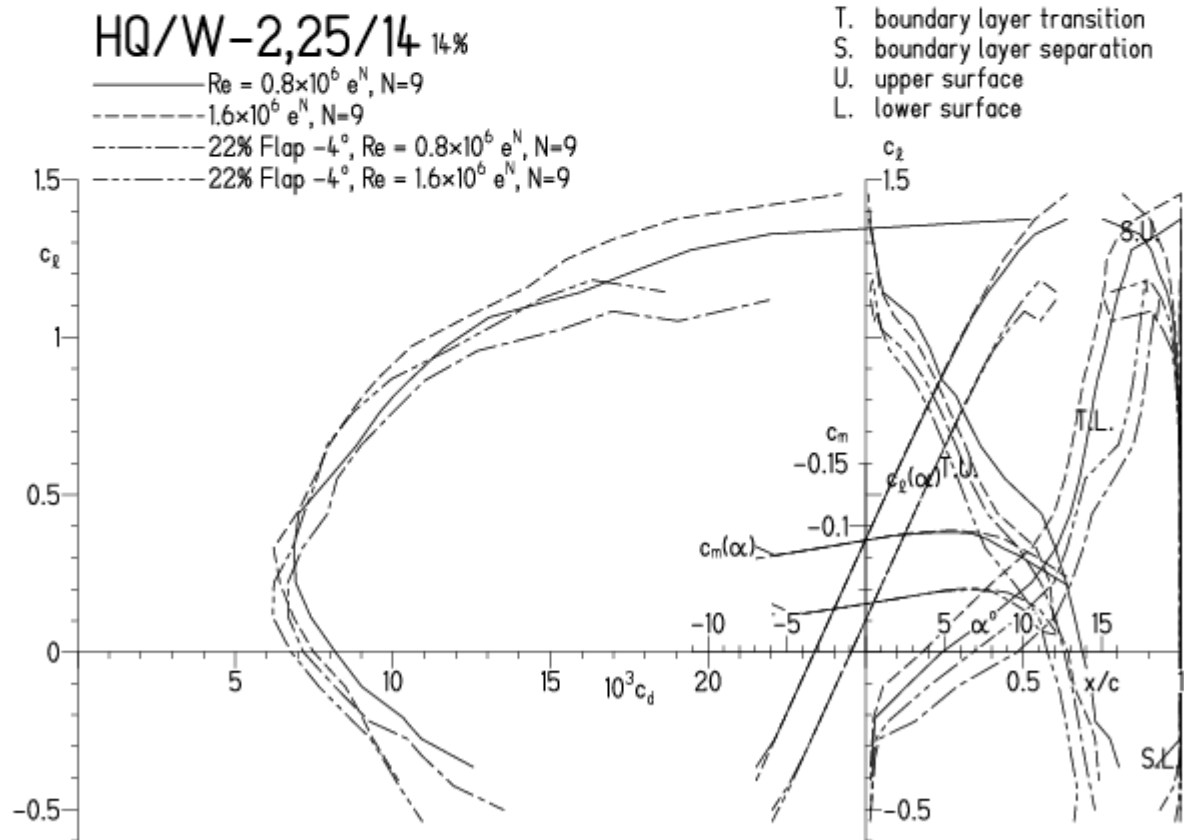


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

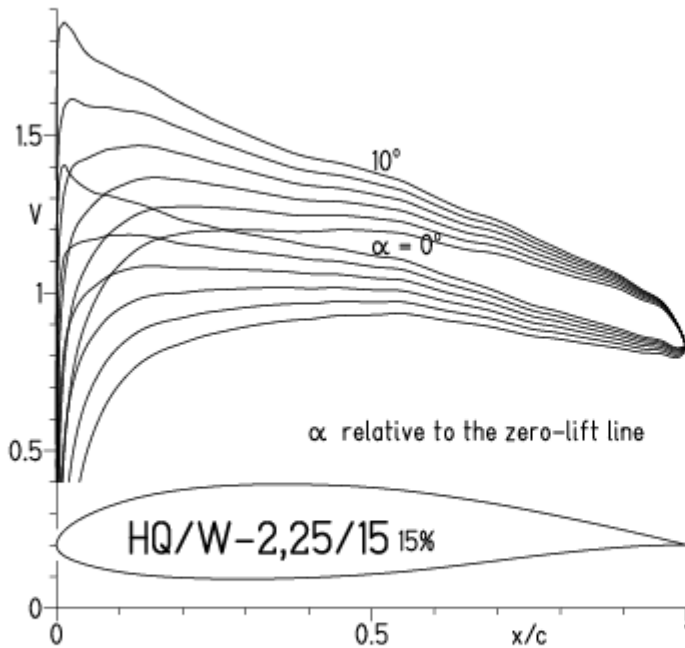


EPPLER 2005 V. 8.5.07

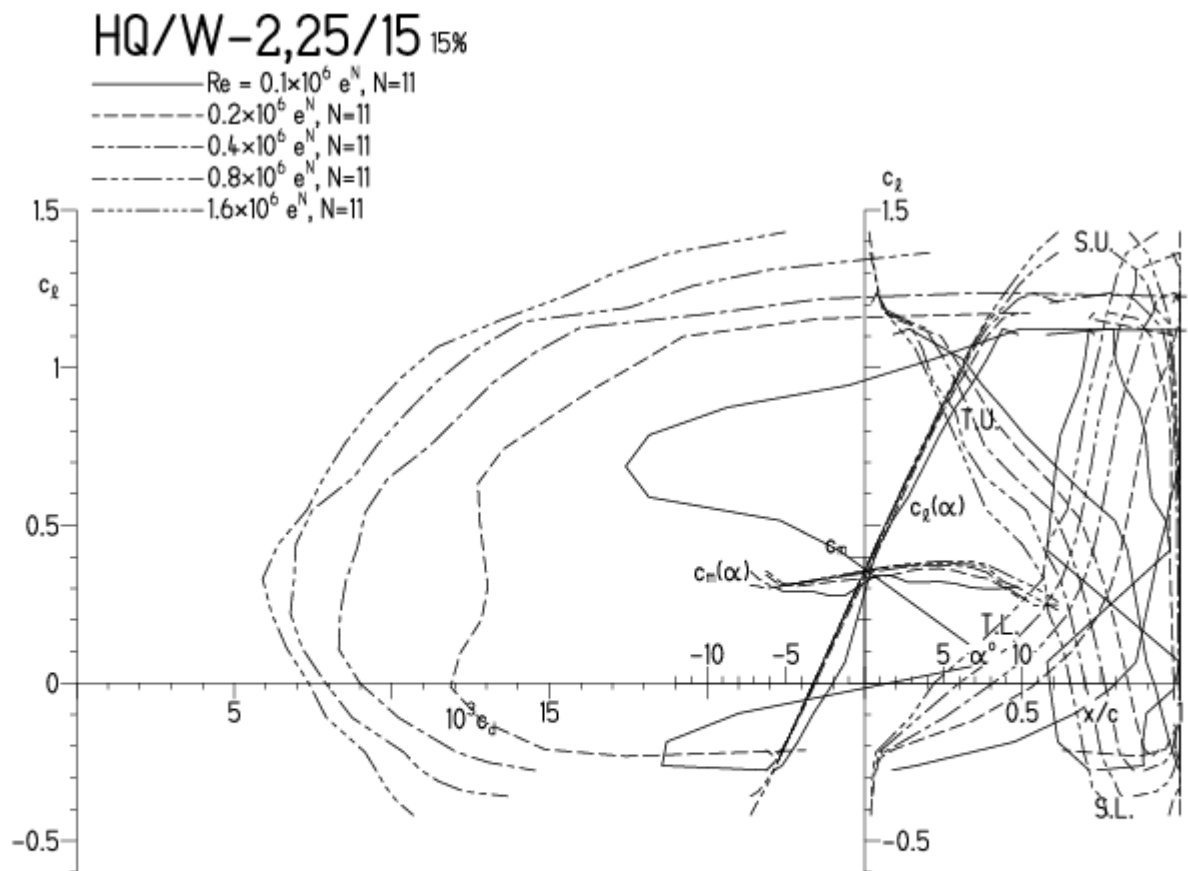


HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

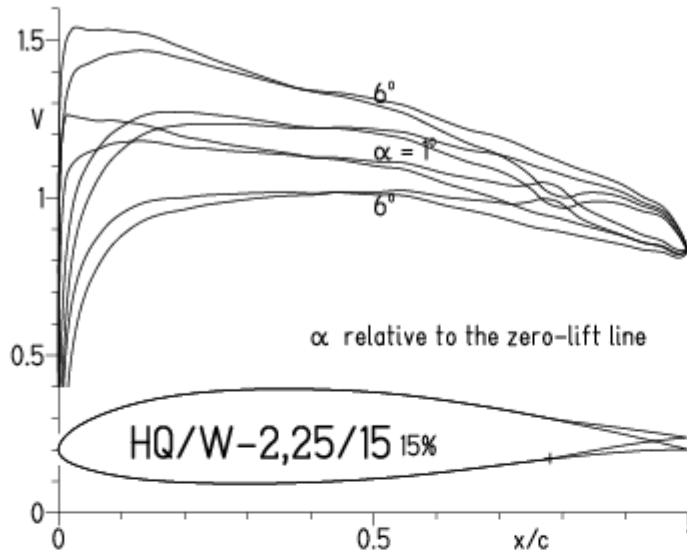


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

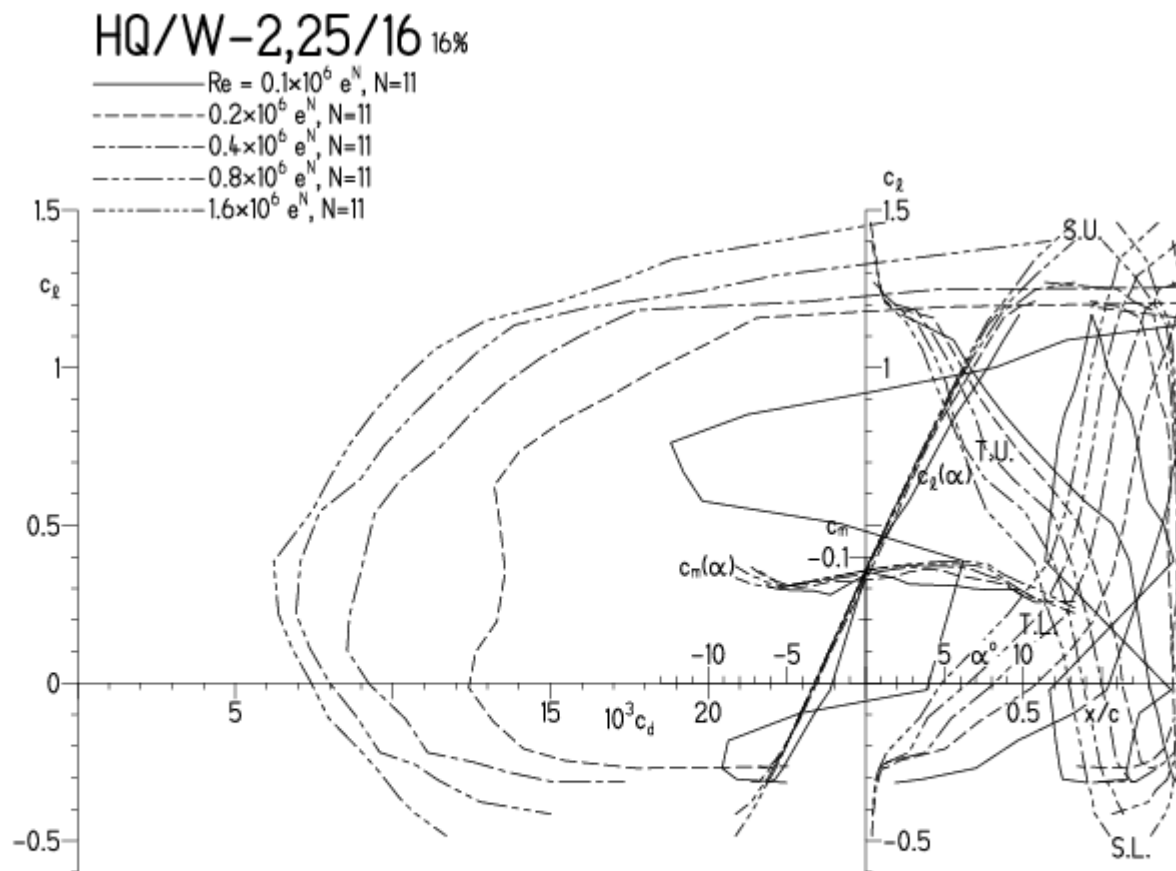


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. $30 - 35 \text{ m/s}$ Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



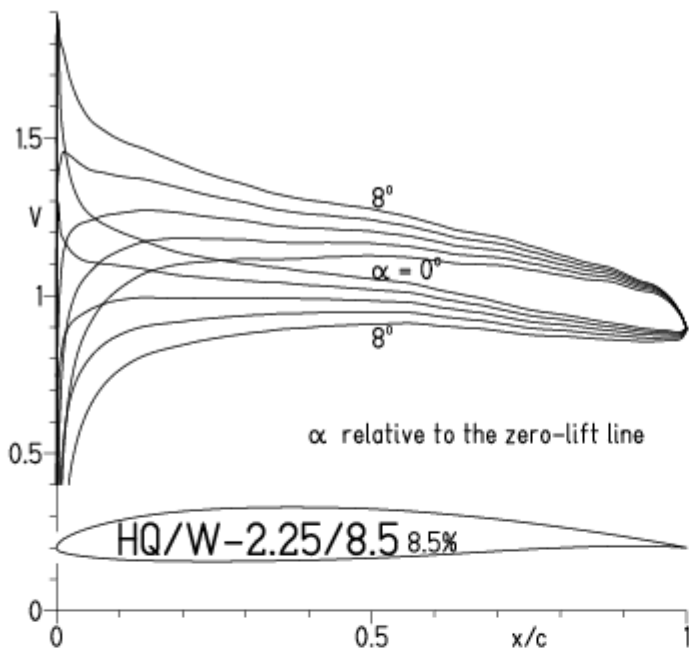
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

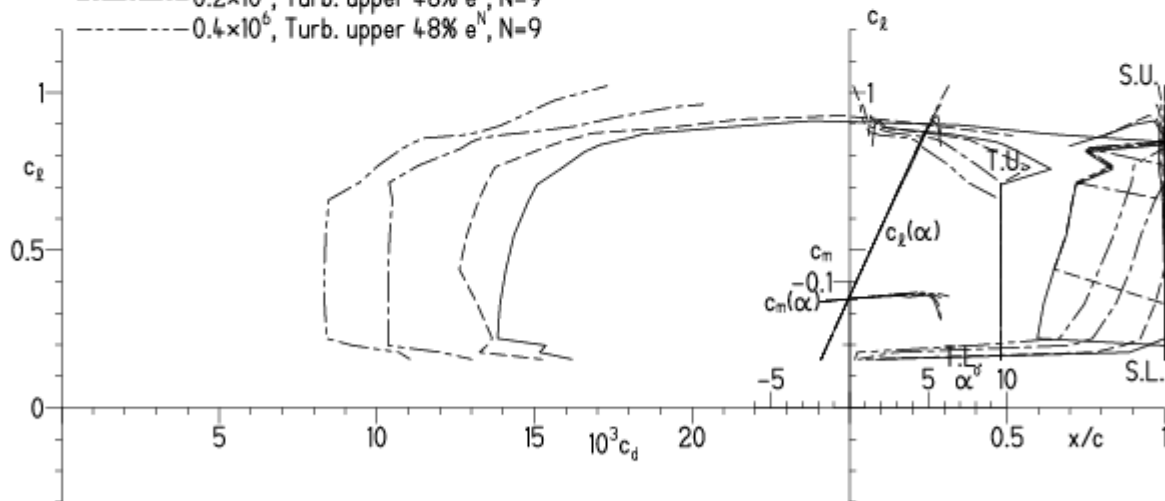
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

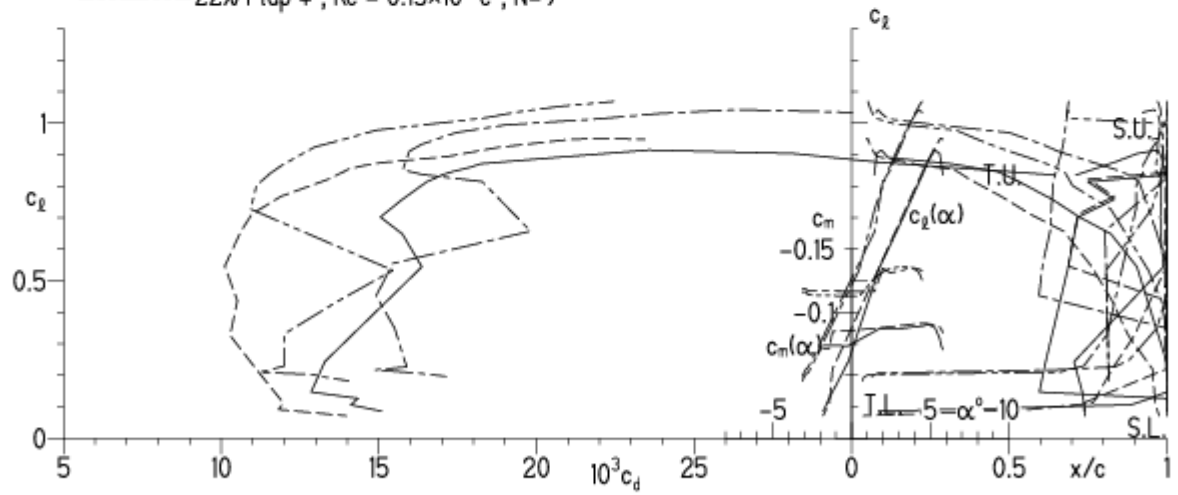


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4°, $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

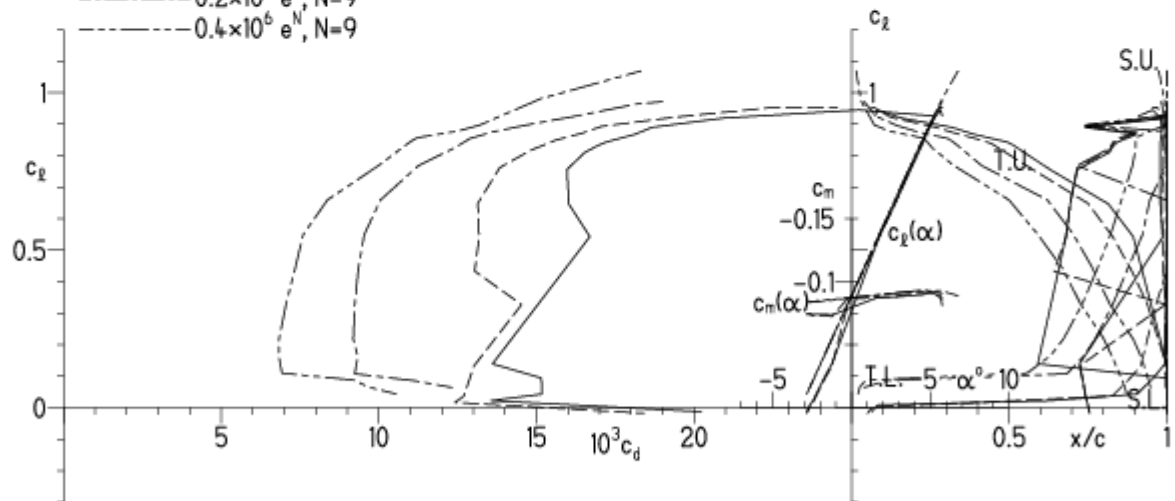
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

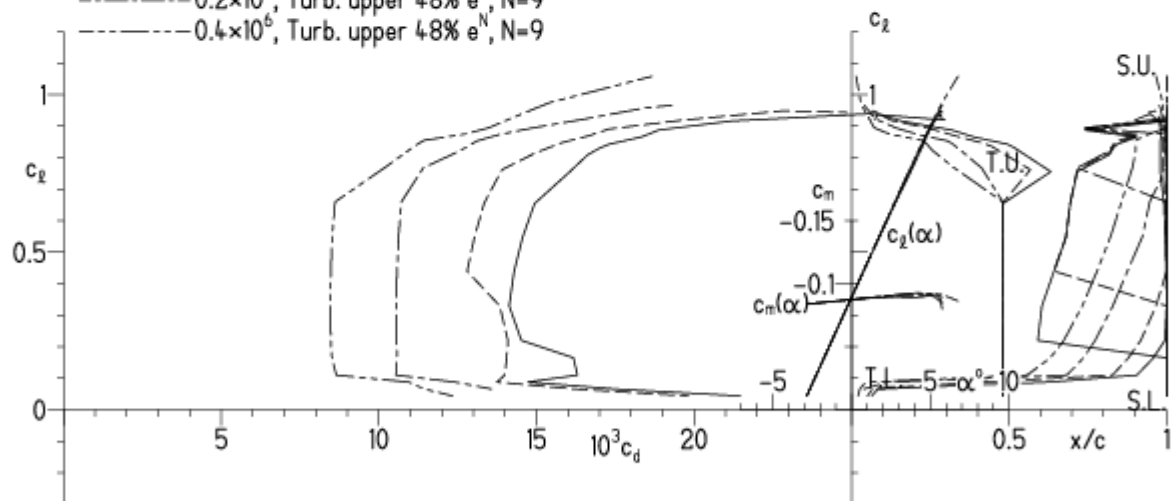
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

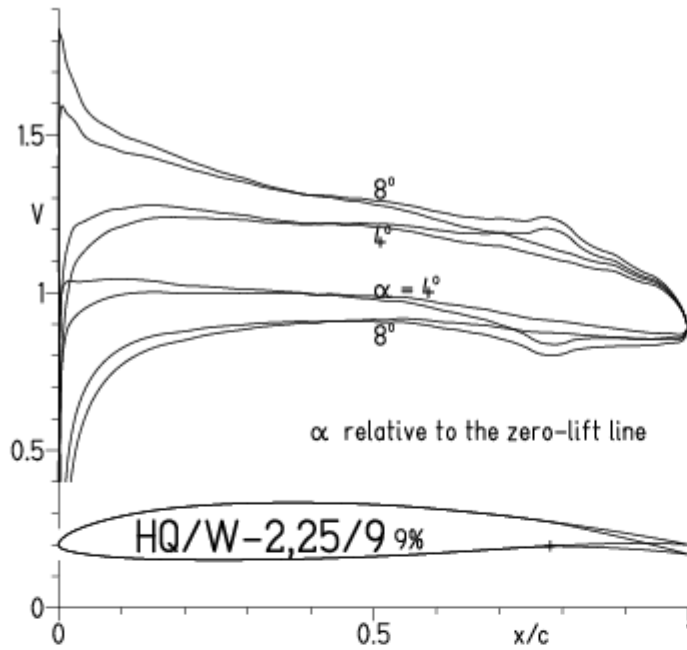
- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48

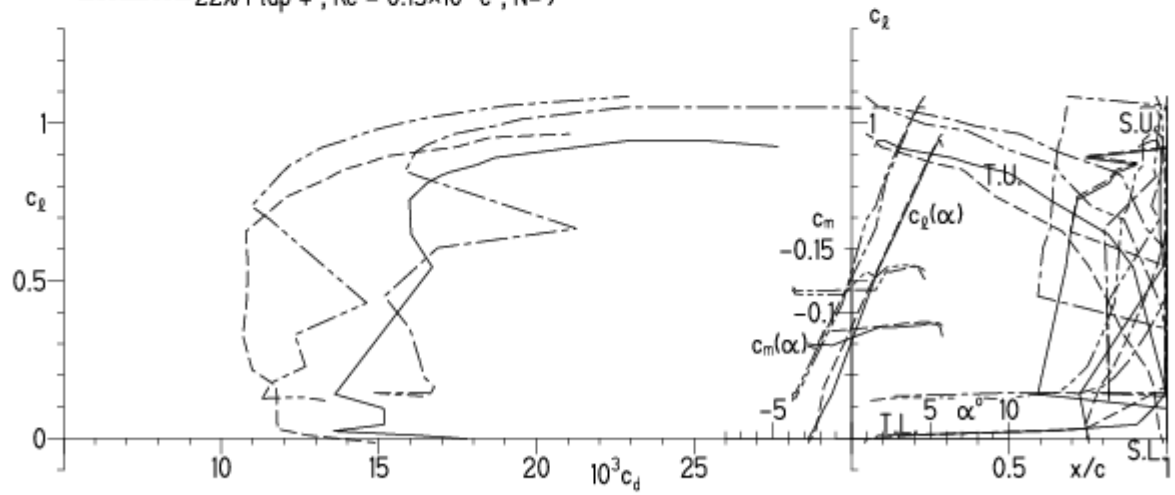


EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

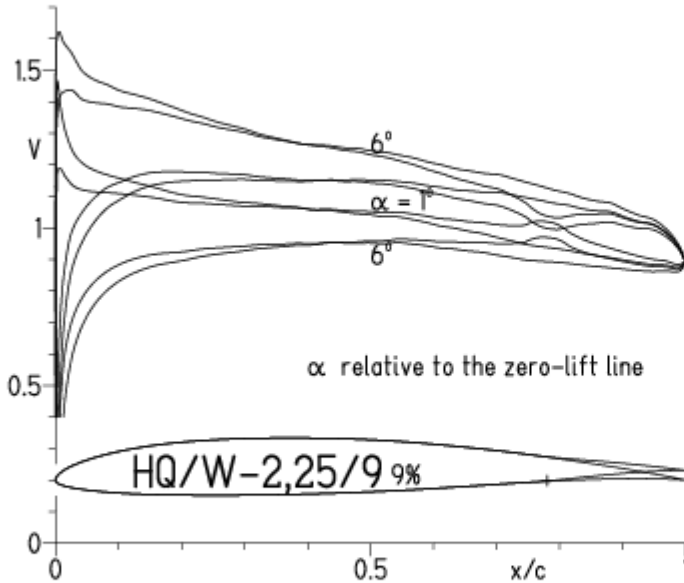
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

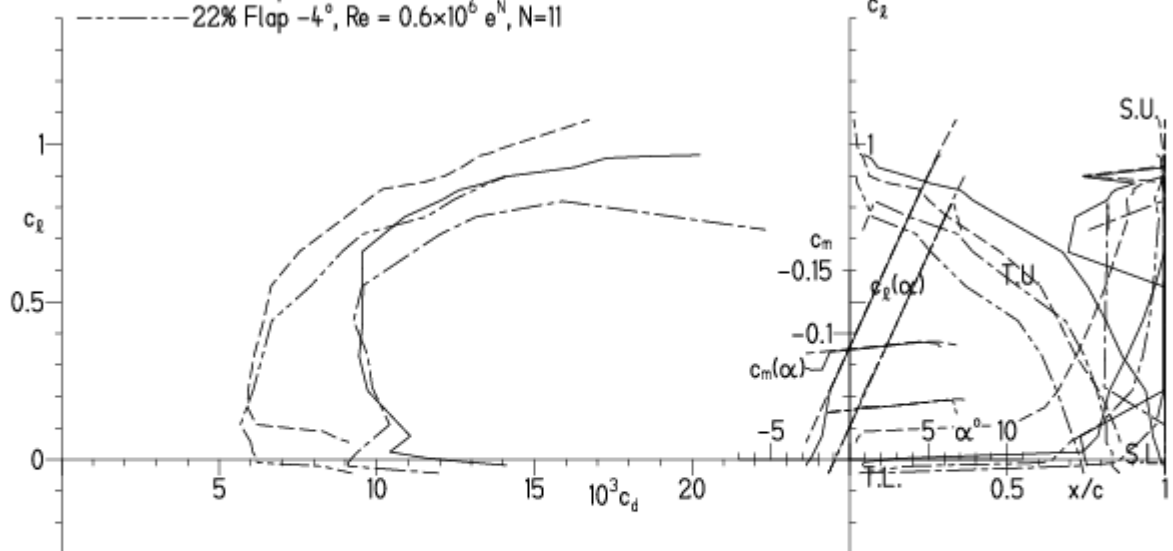
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2 × 10⁶ e^N, N=11
- - - 0.6 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.2 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.6 × 10⁶ e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

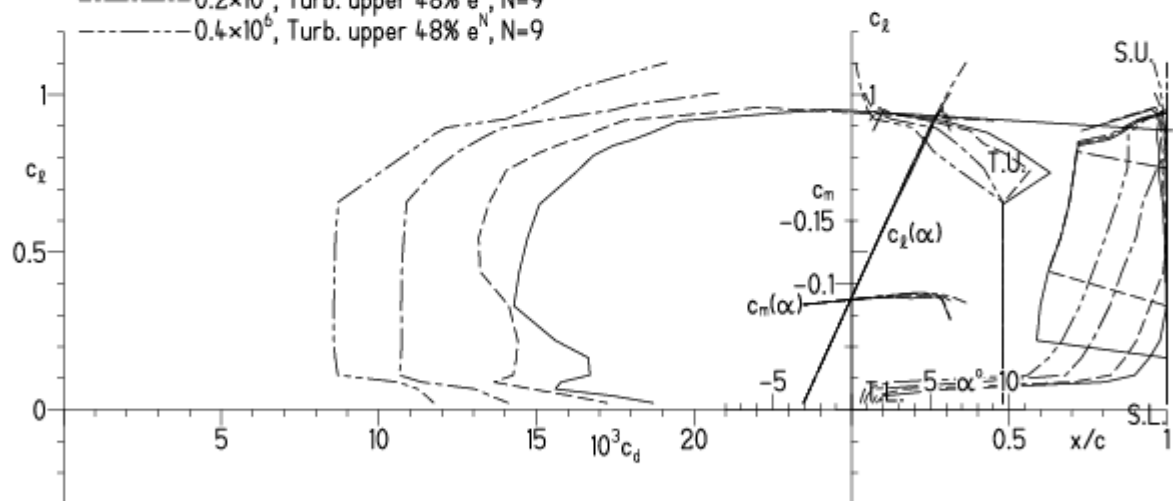
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

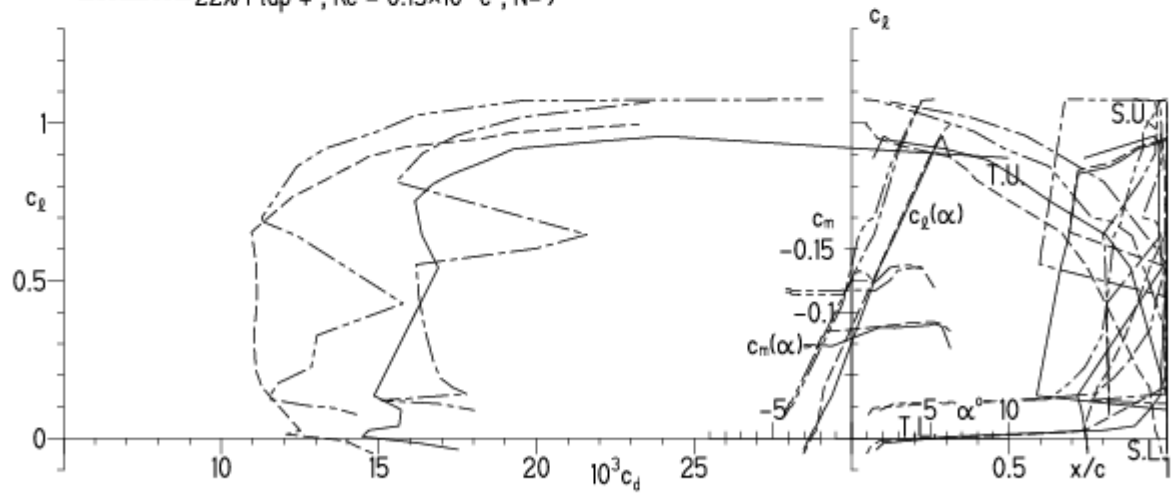


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- Re = 75 000 e^N, N=9
- - - 0.15x10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

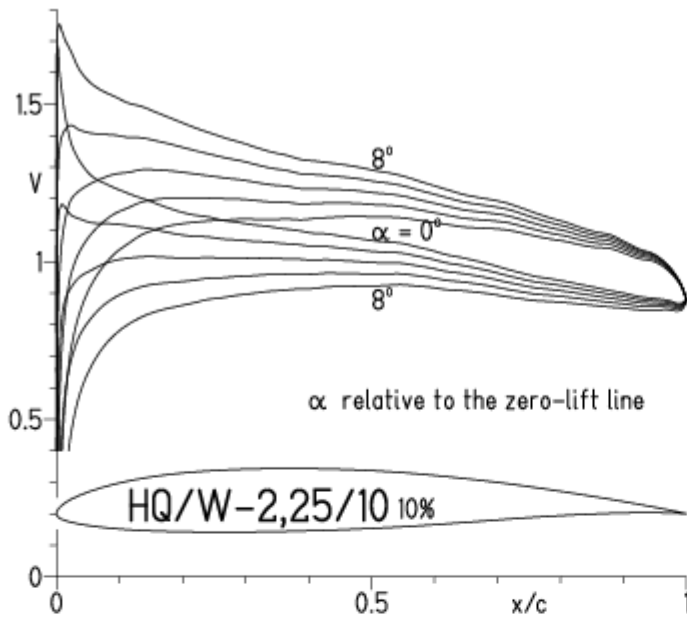


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

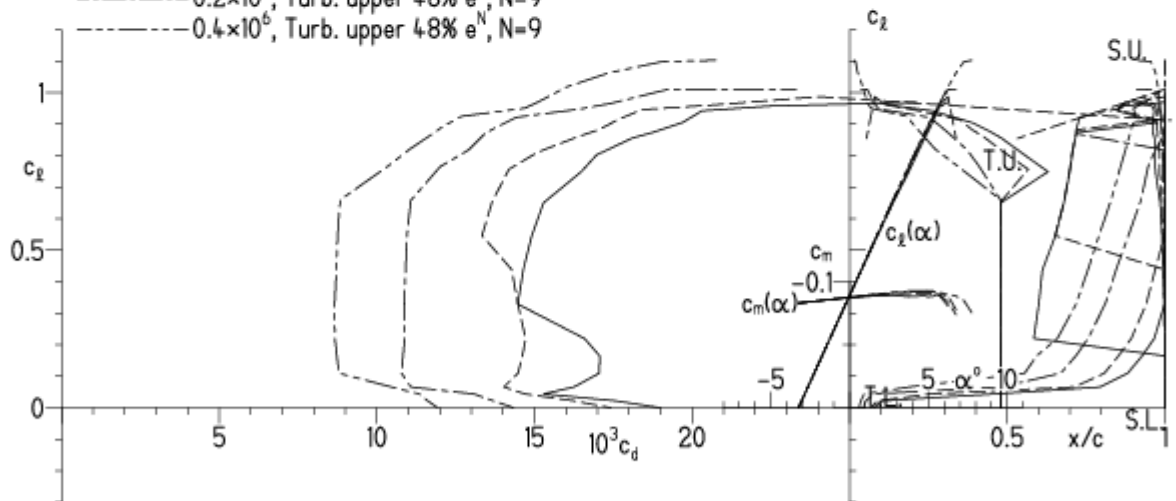
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

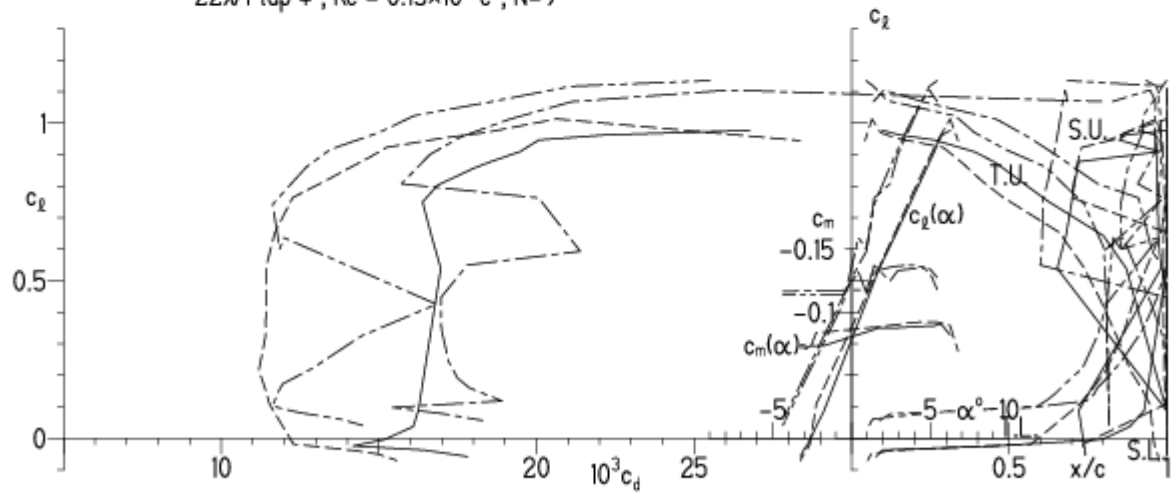


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

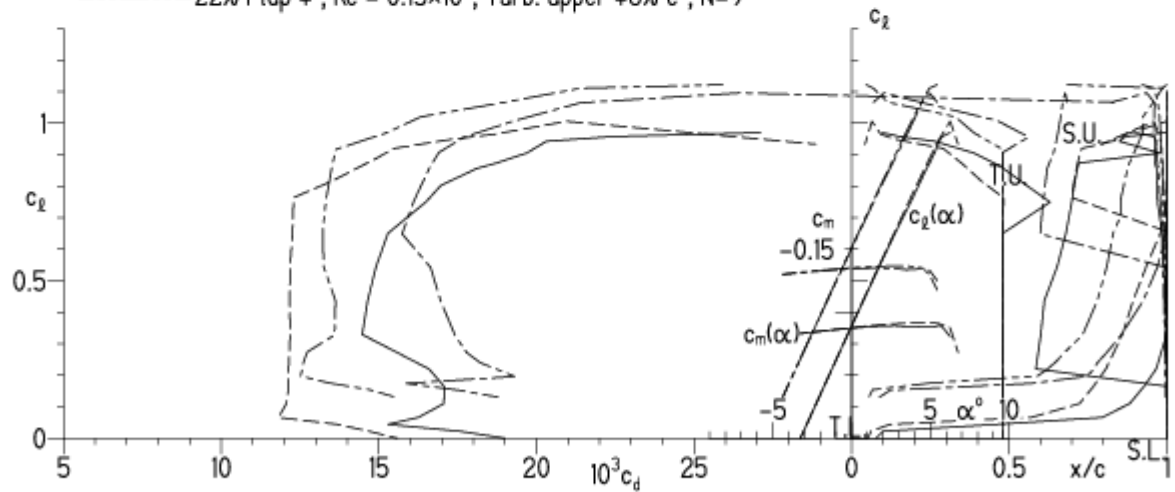


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

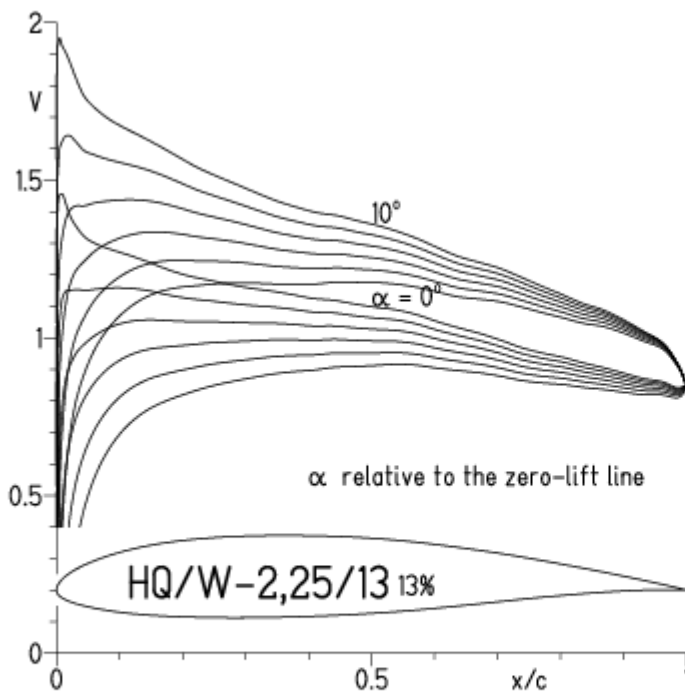


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

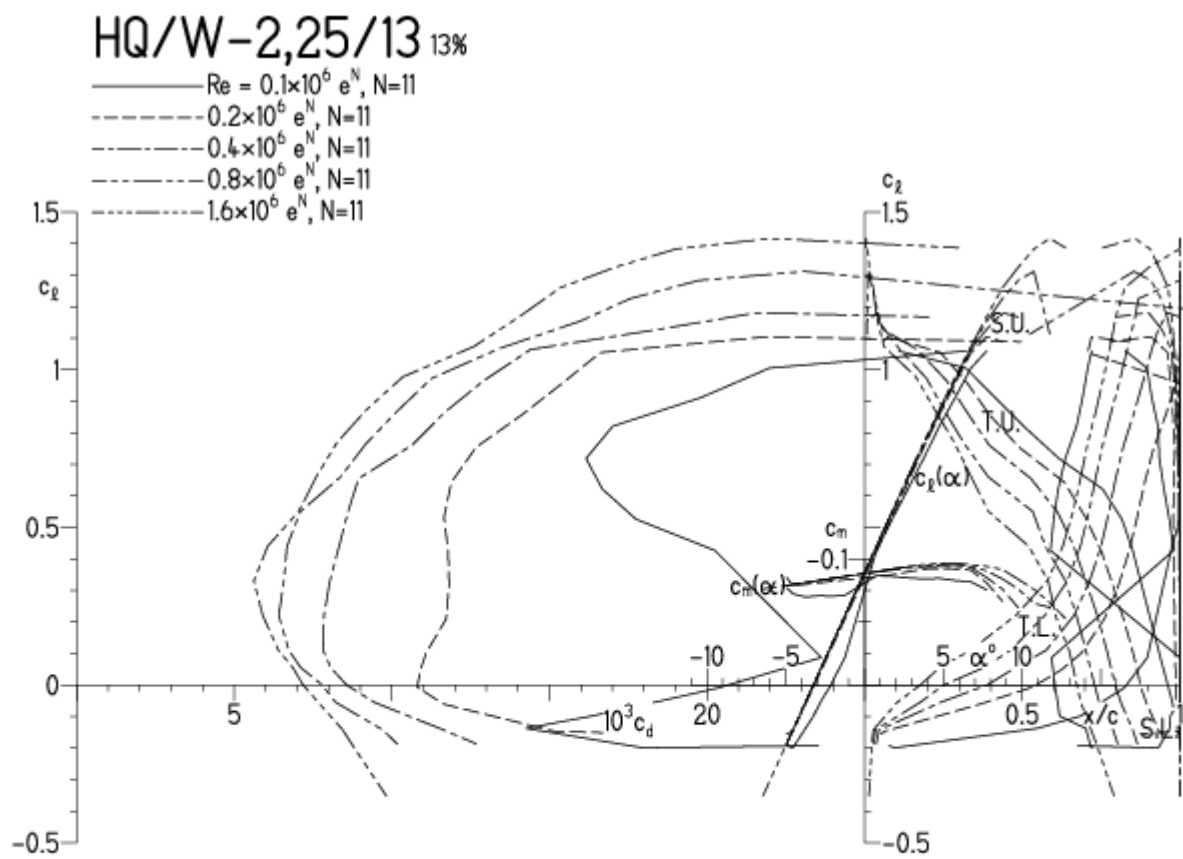


HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

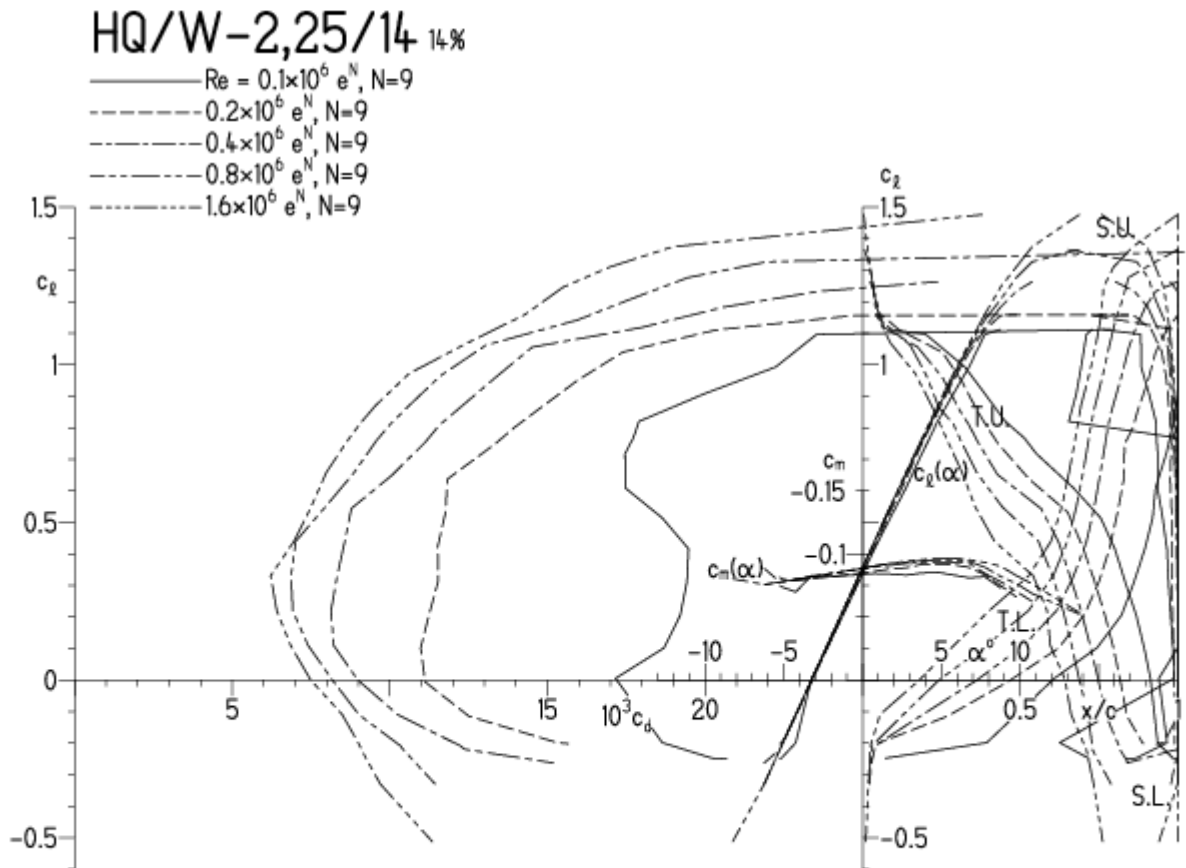


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

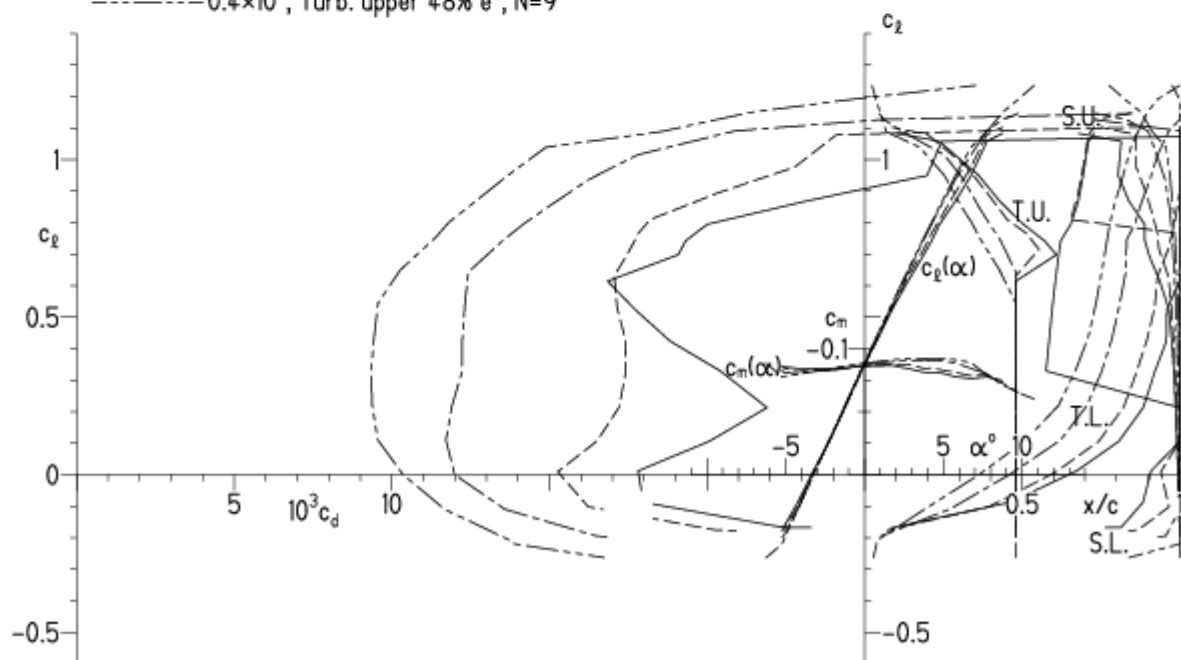
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

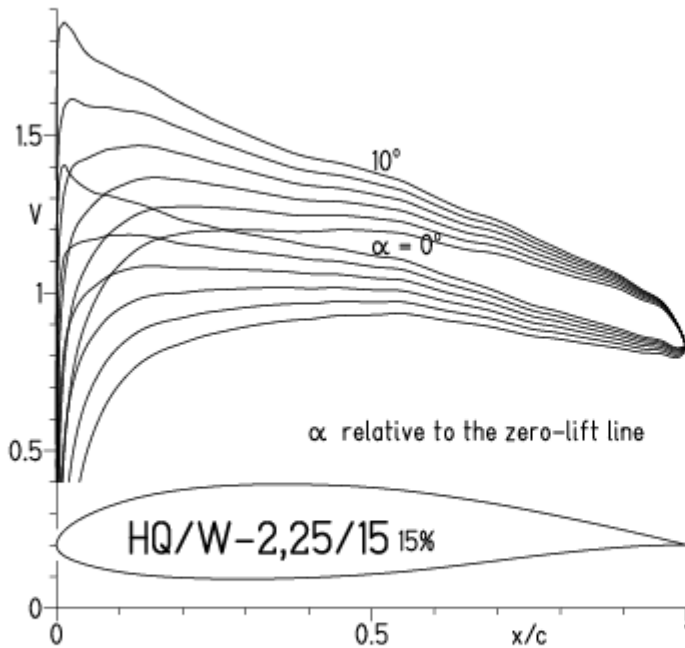


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

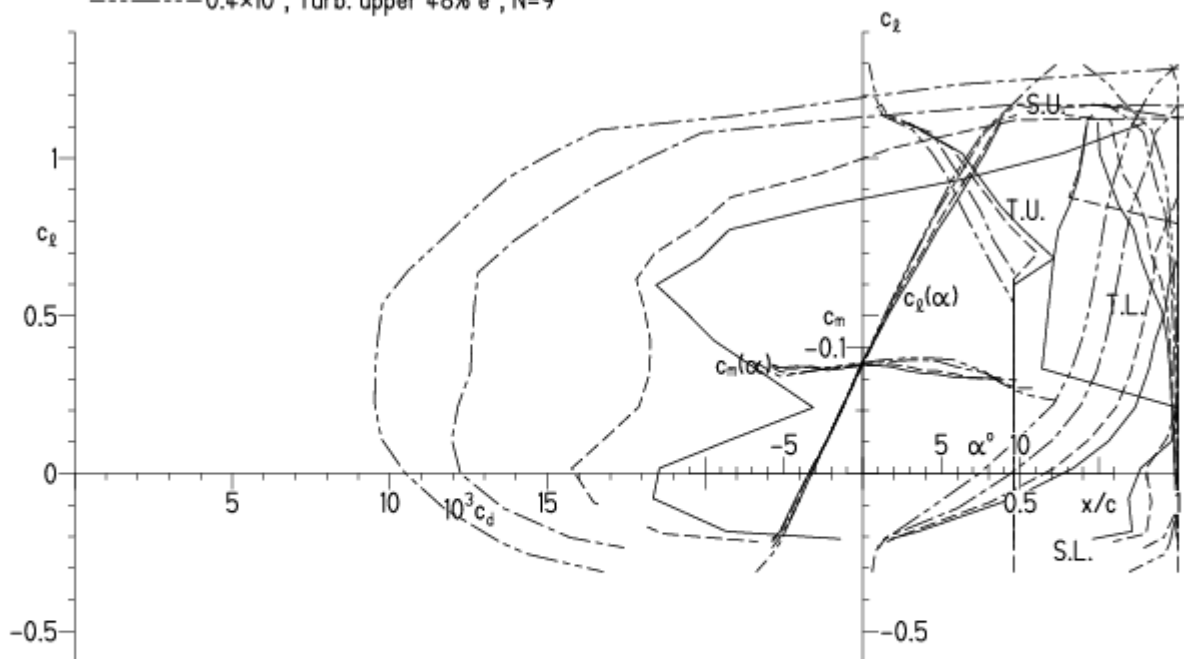
EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

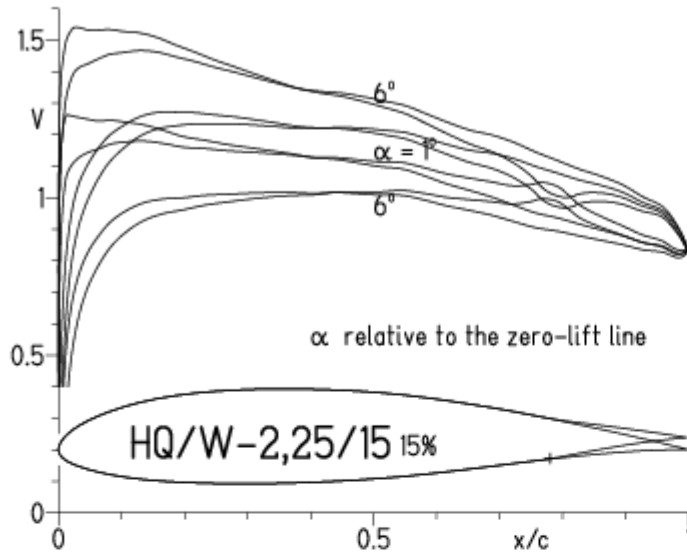


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

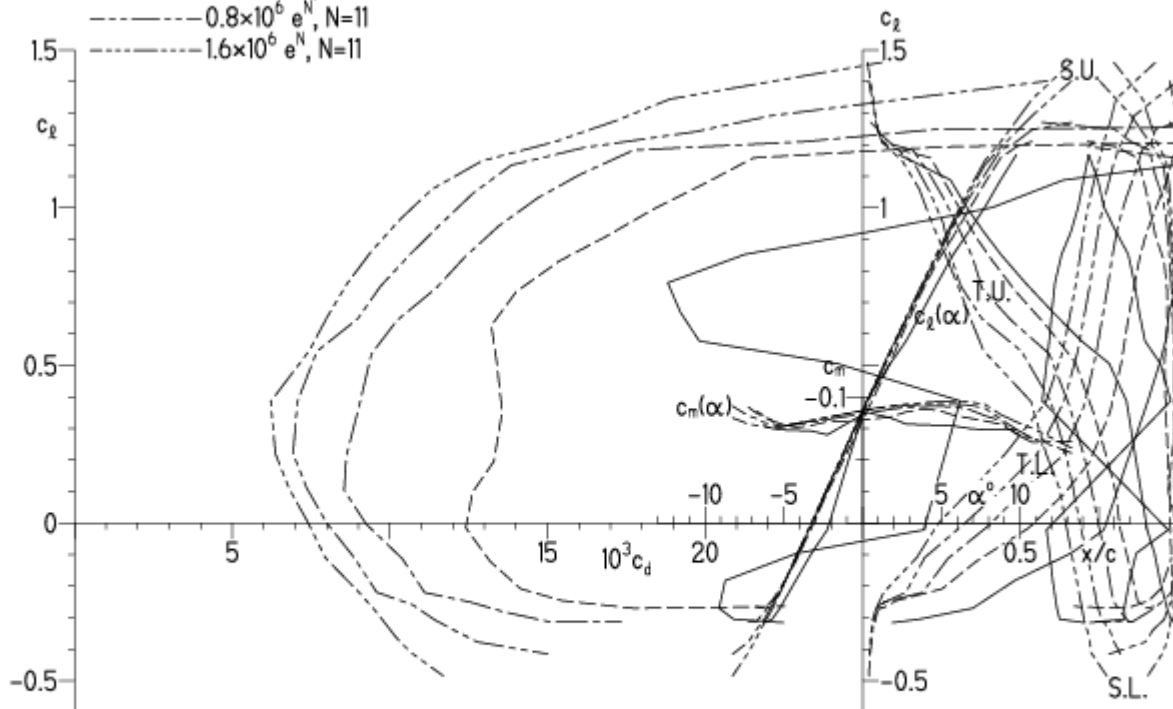
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

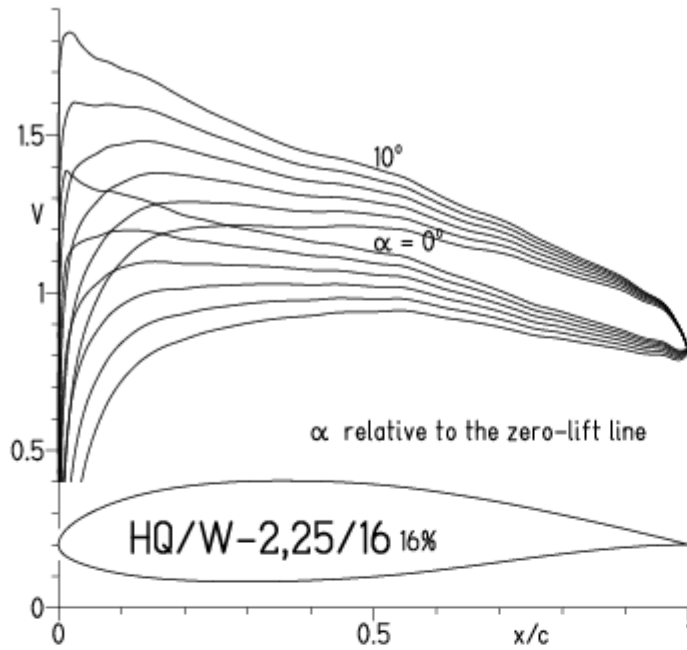
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · · - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - · 22% Flap 4°, Re = 75 000 e^N, N=9
- · - · 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

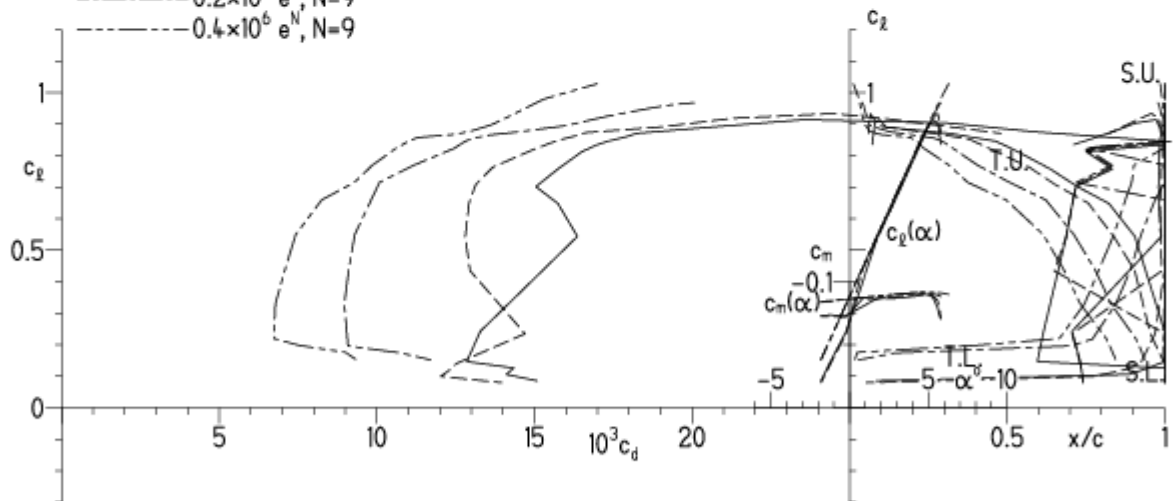
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

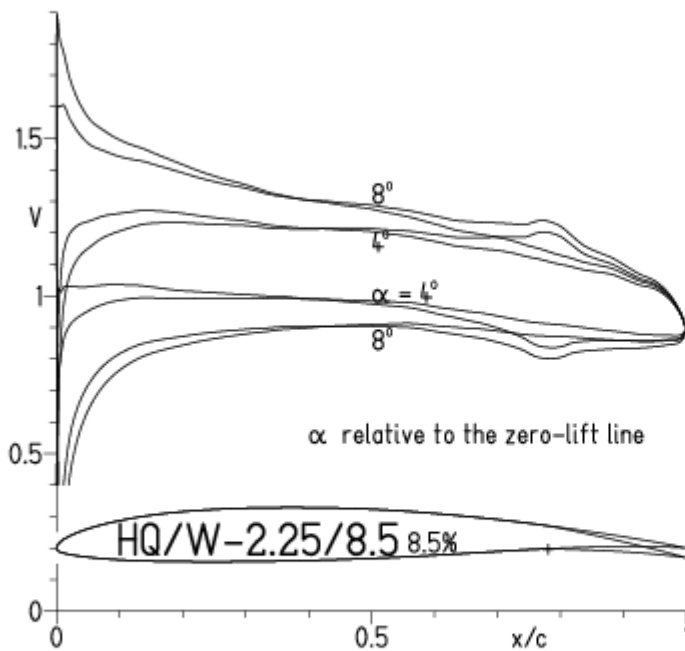
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

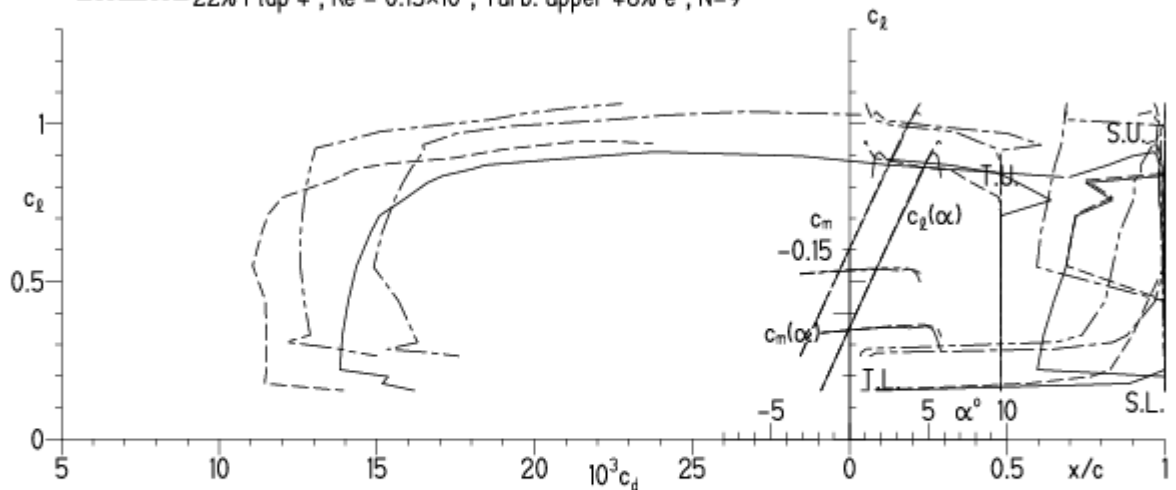


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

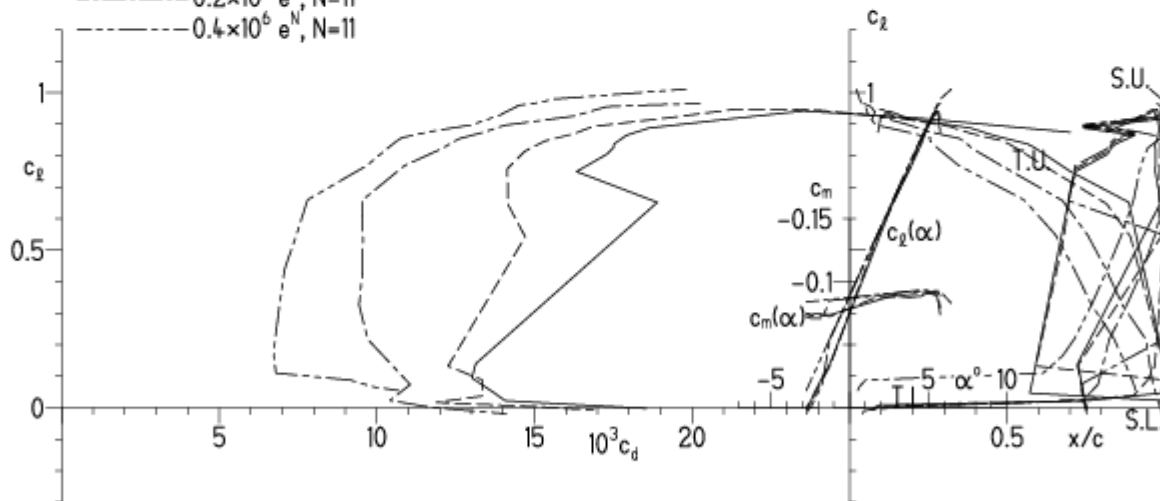
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$

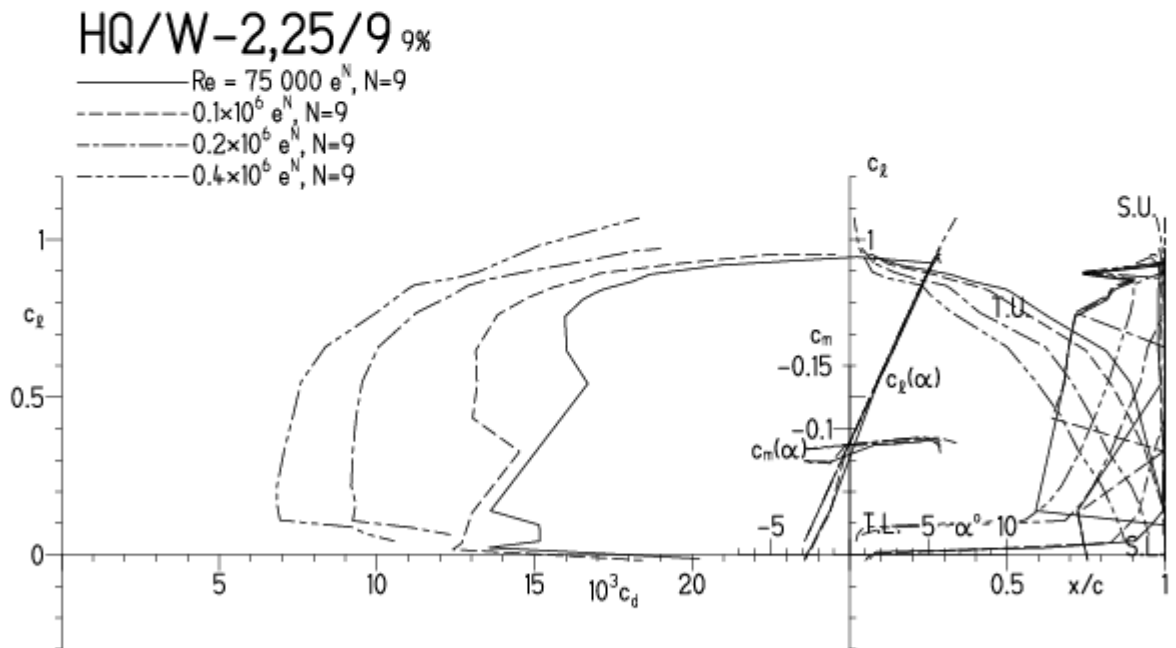


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08

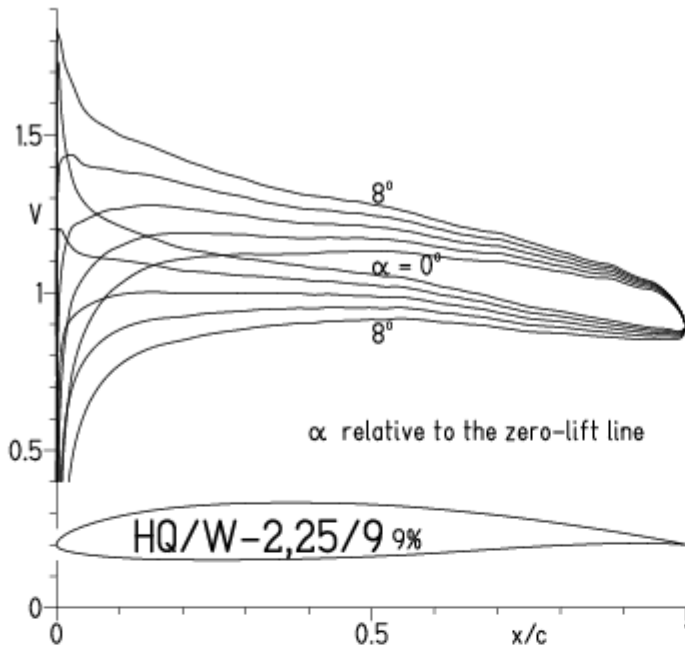


EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

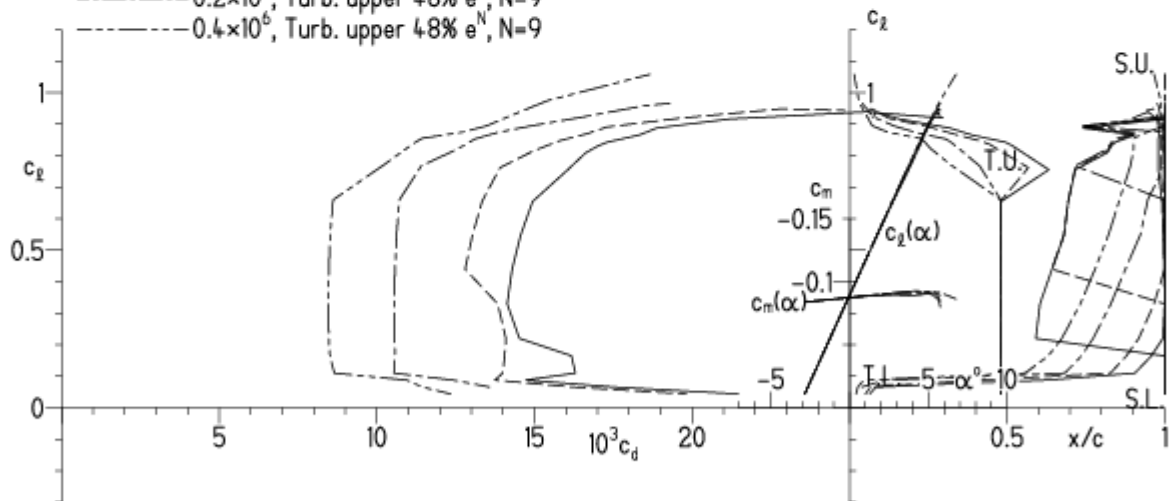
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

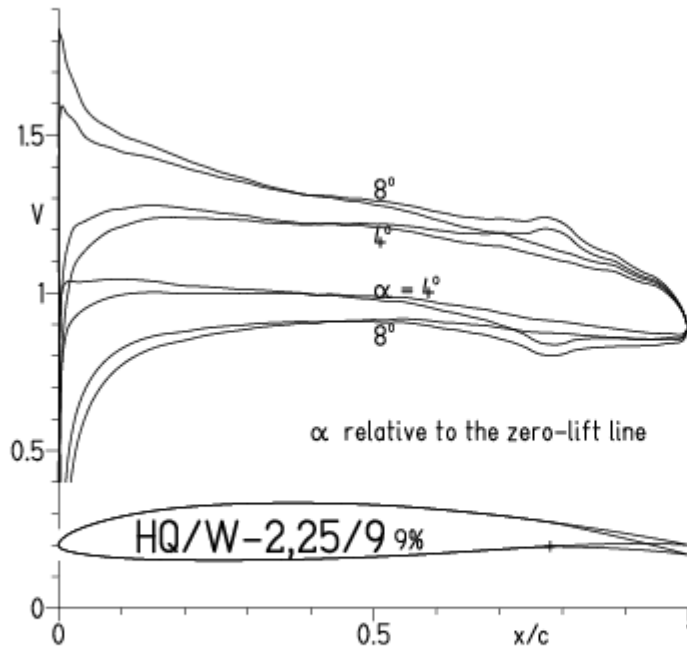
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · - 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17

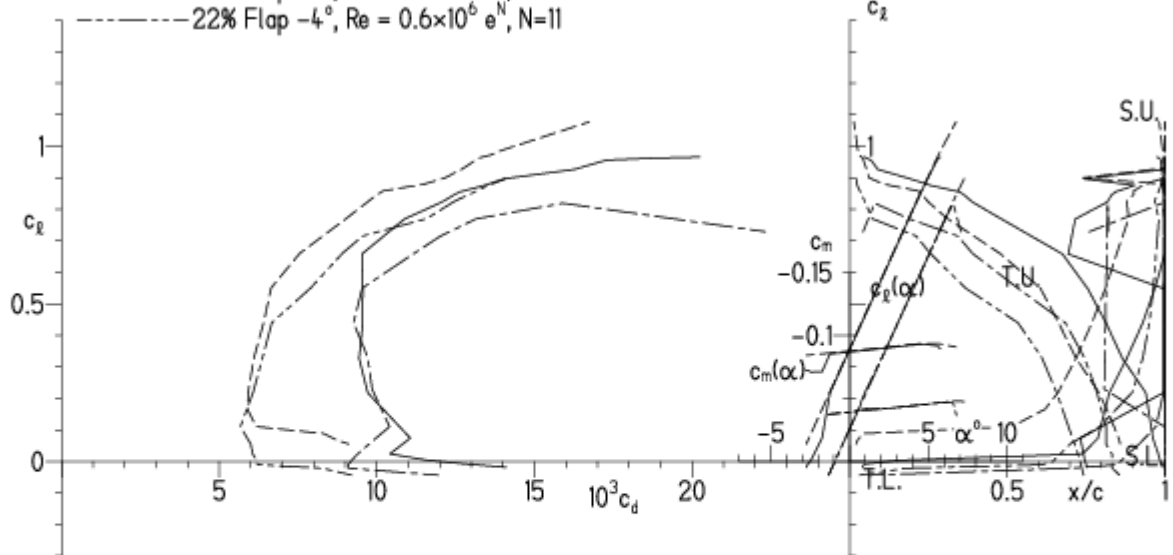


EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

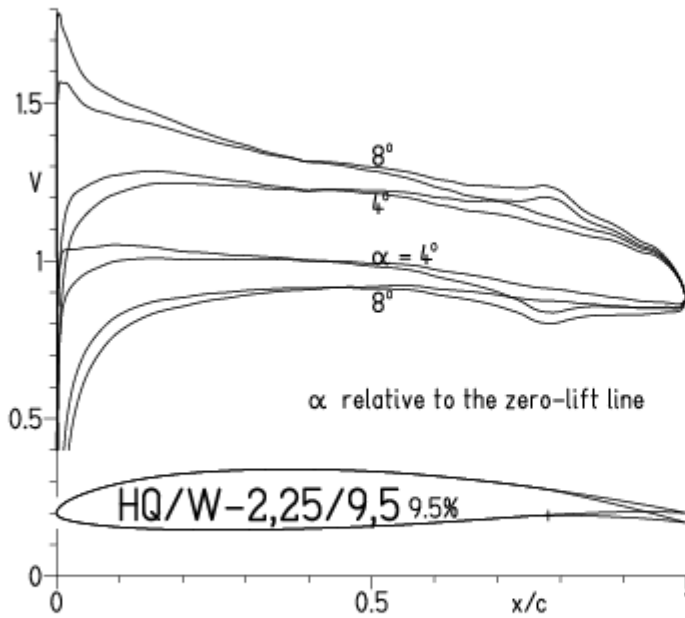
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

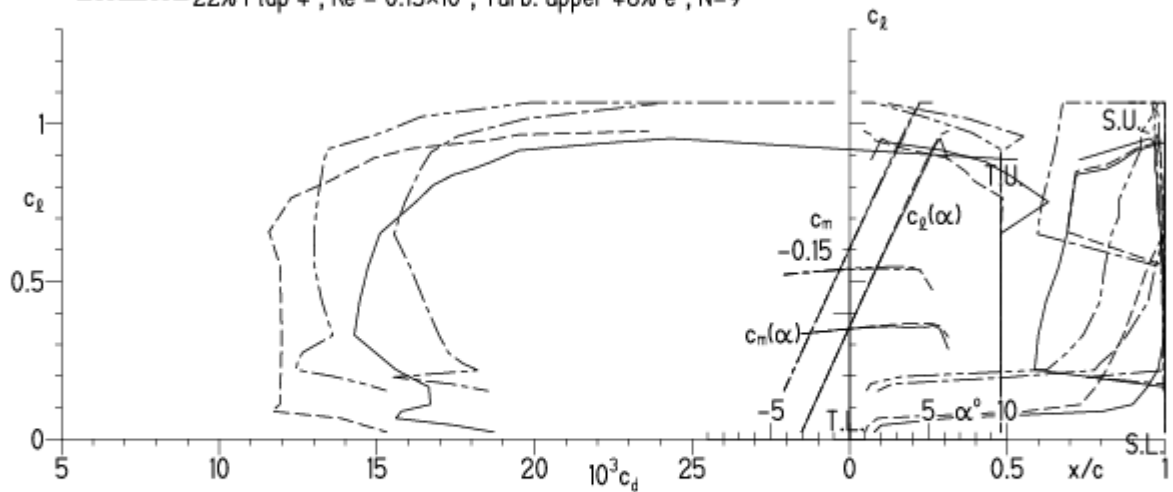


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



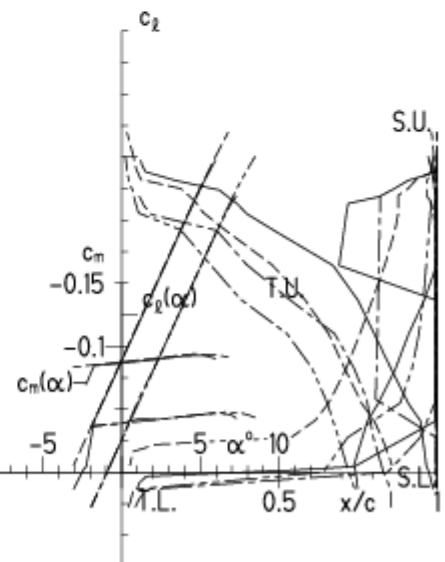
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

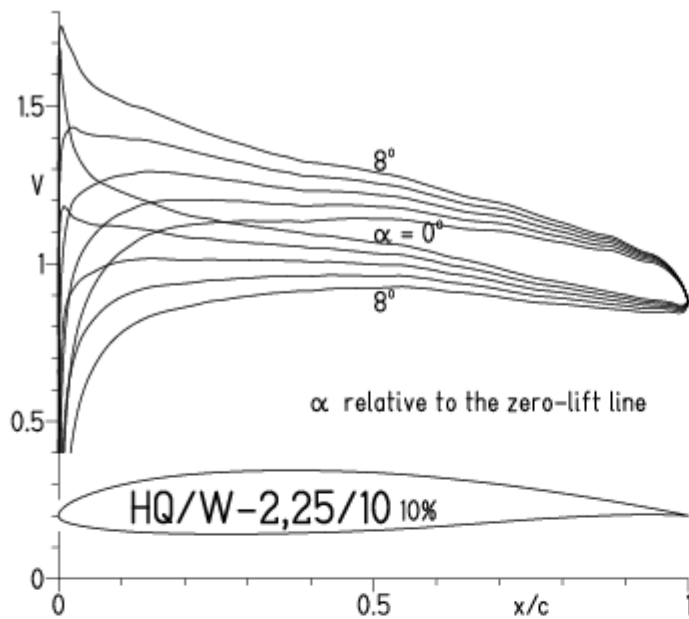


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

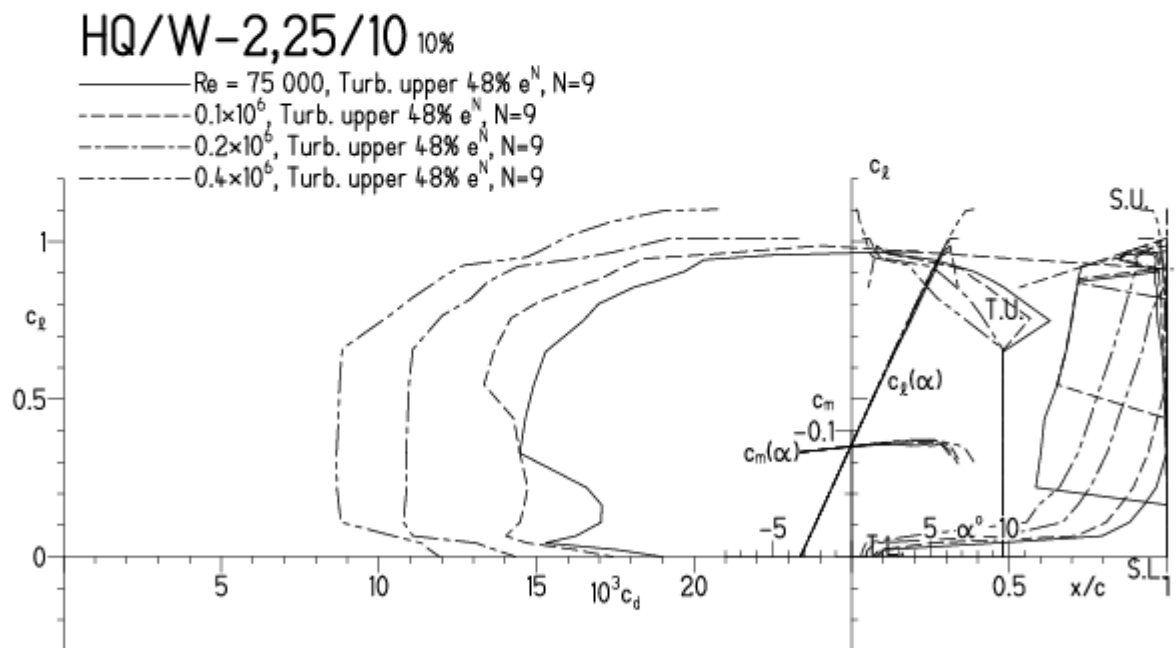


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

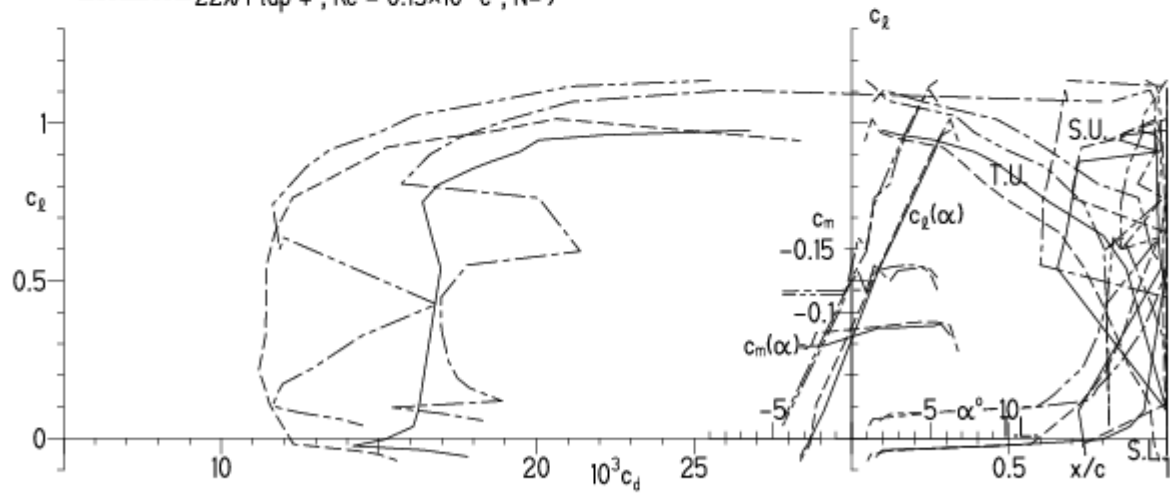


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

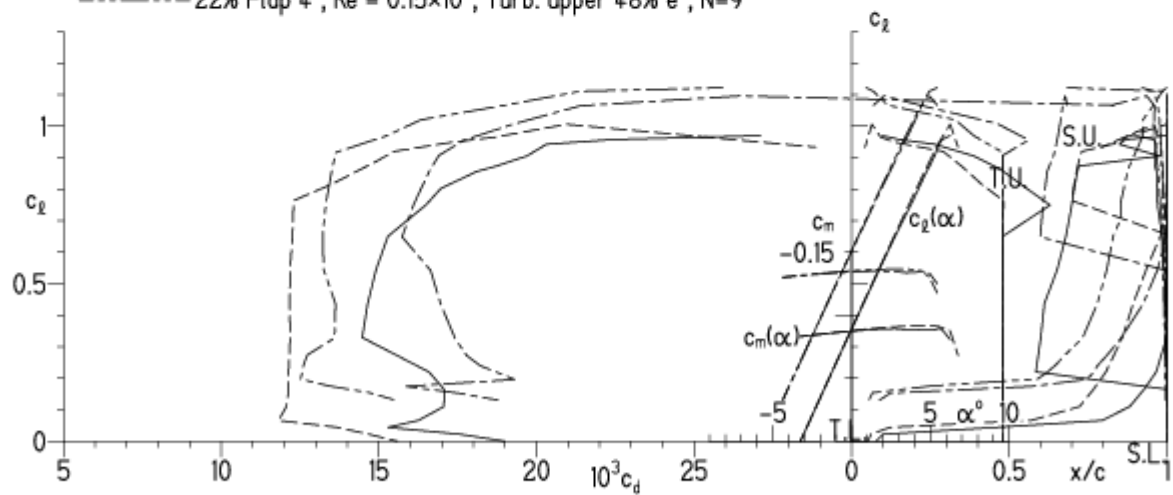


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

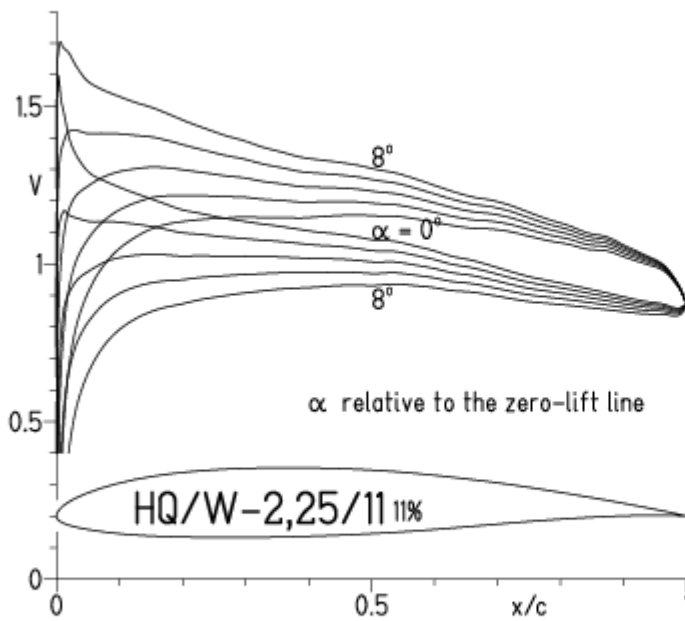


EPPLER 2005 V. 8.5.07 RUN

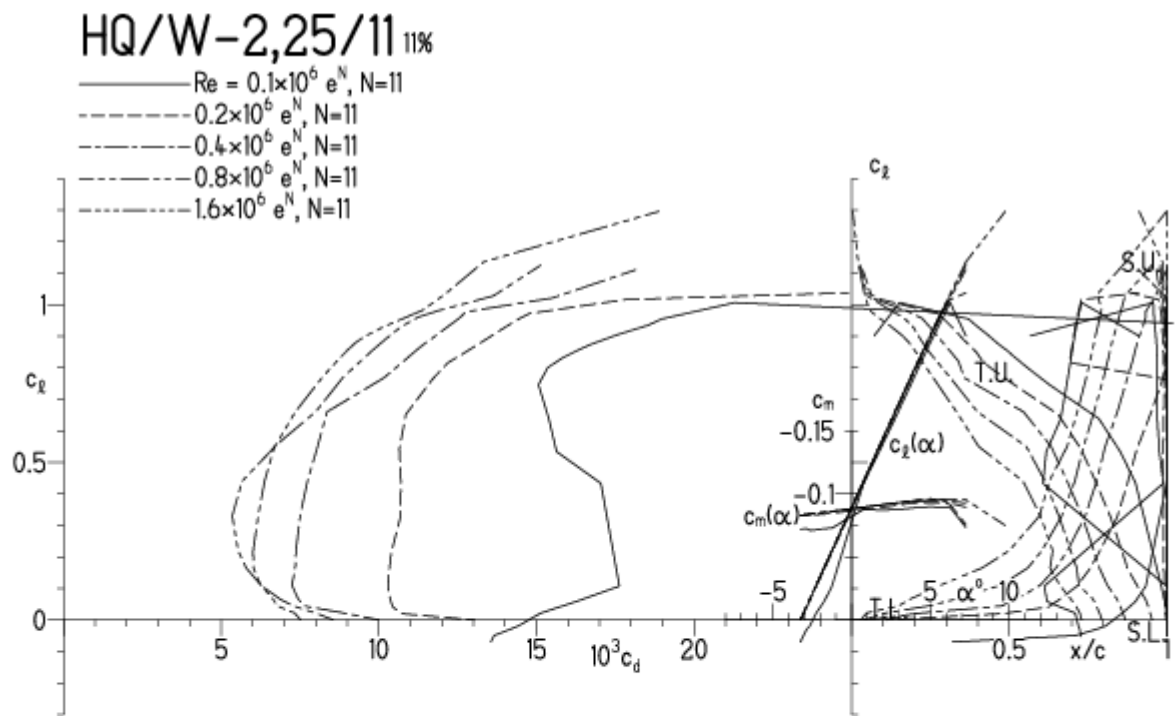


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

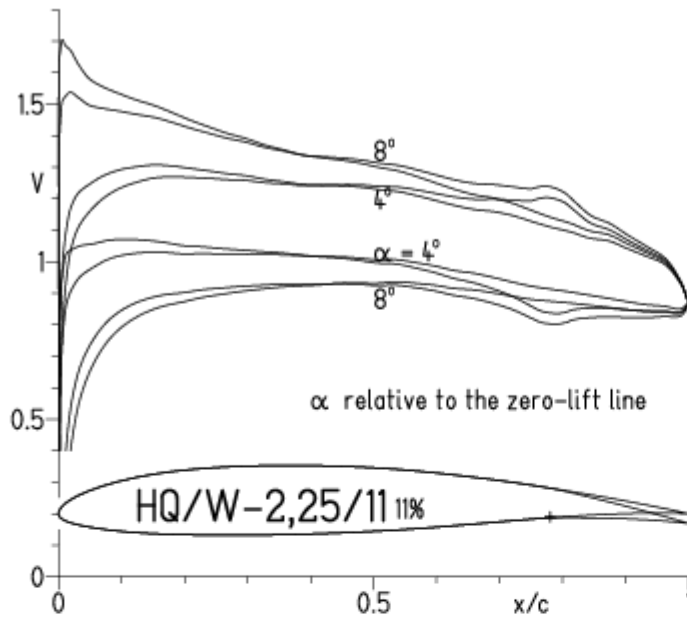
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

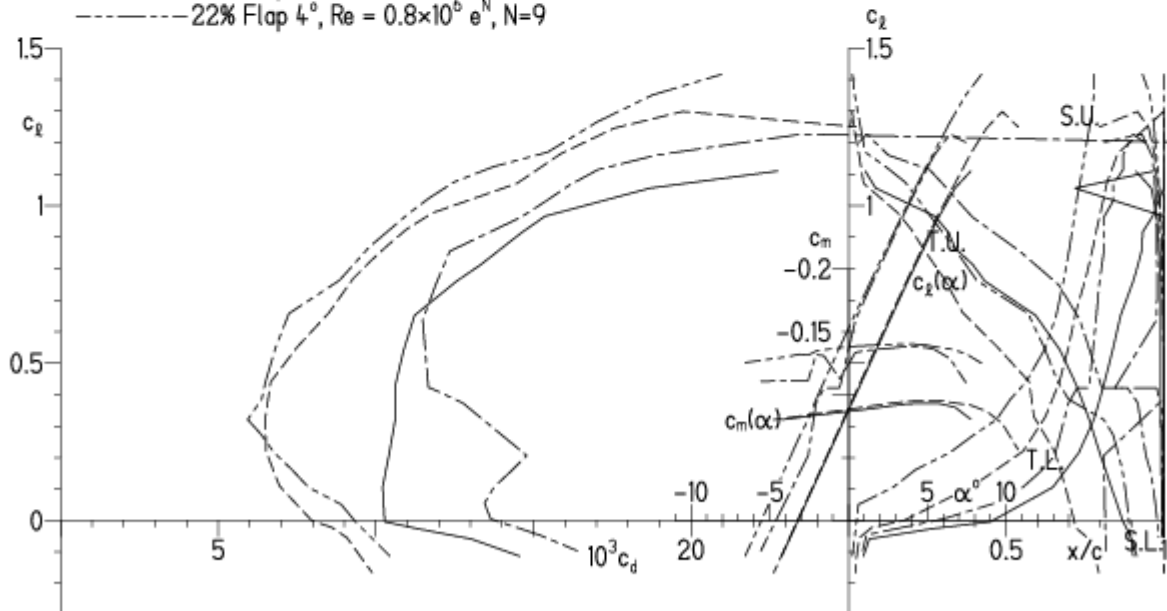


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

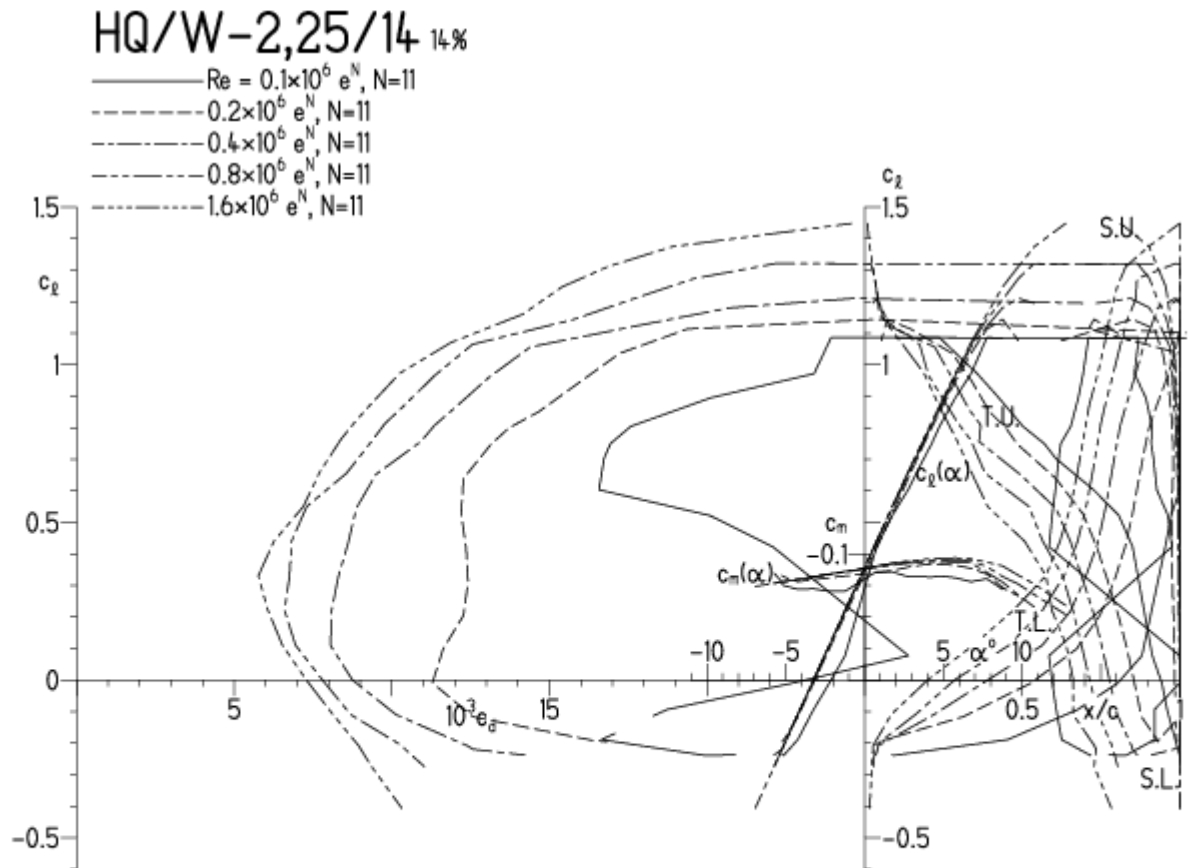


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

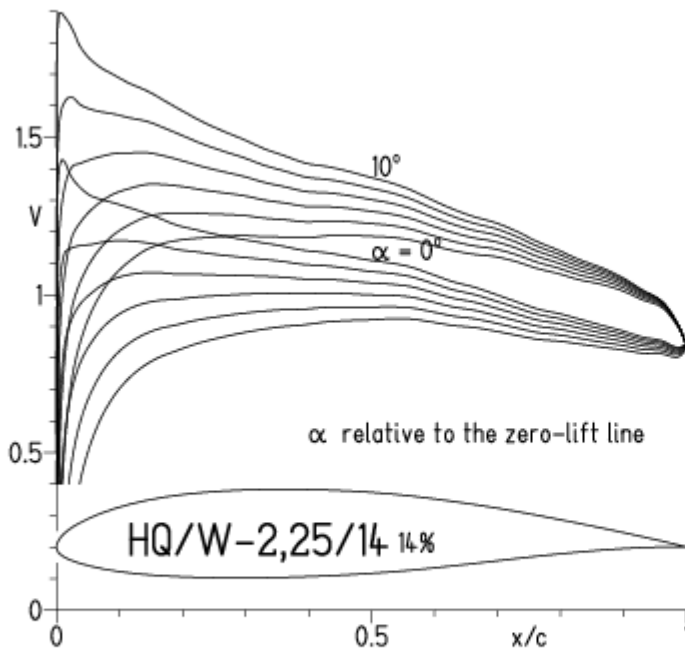


EPPLER 2005 V. 8.

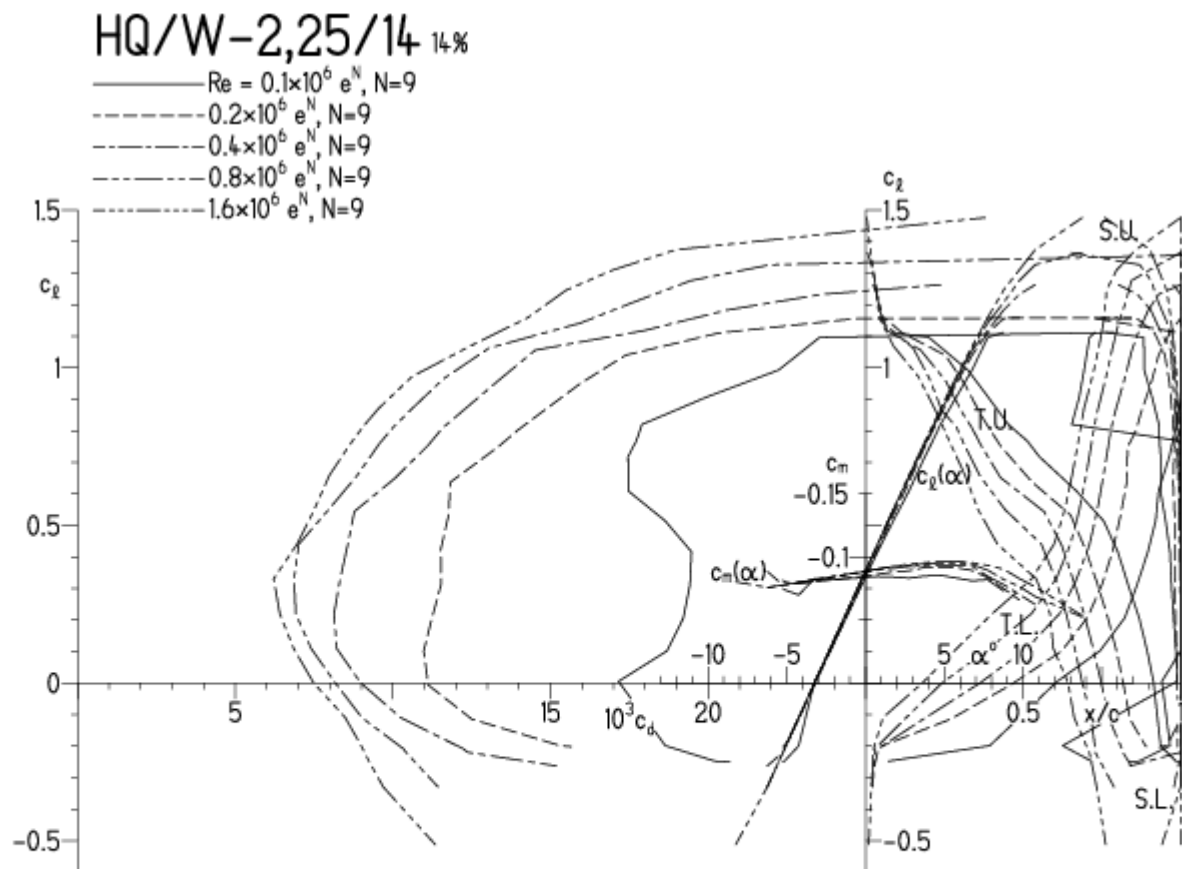


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

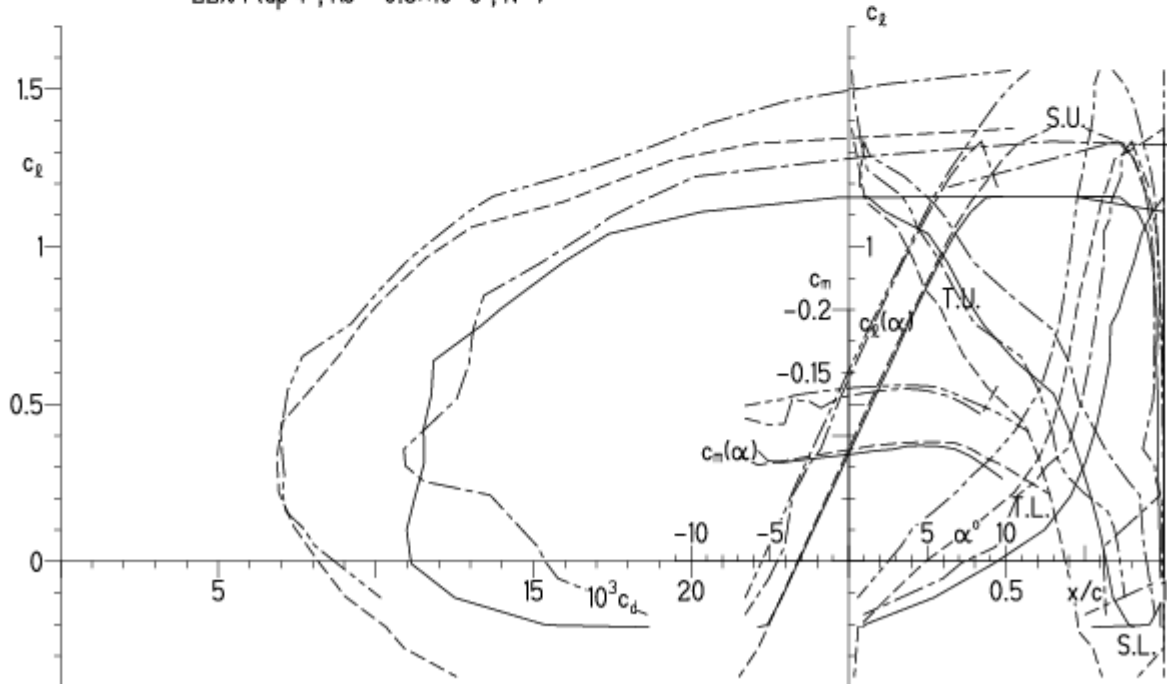


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

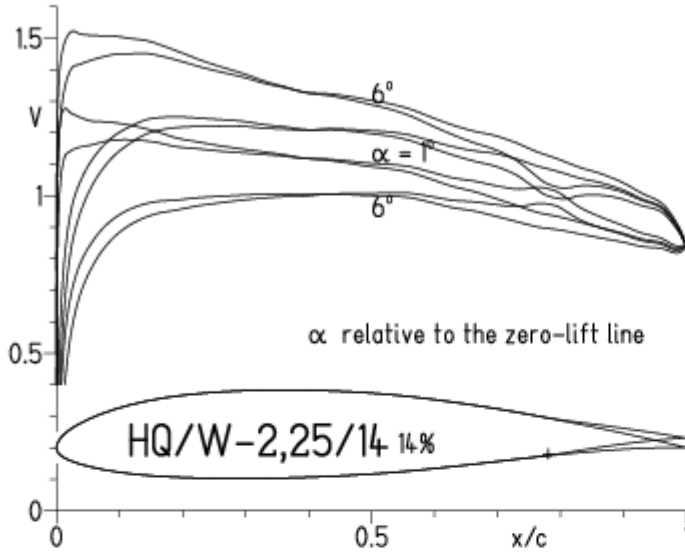
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

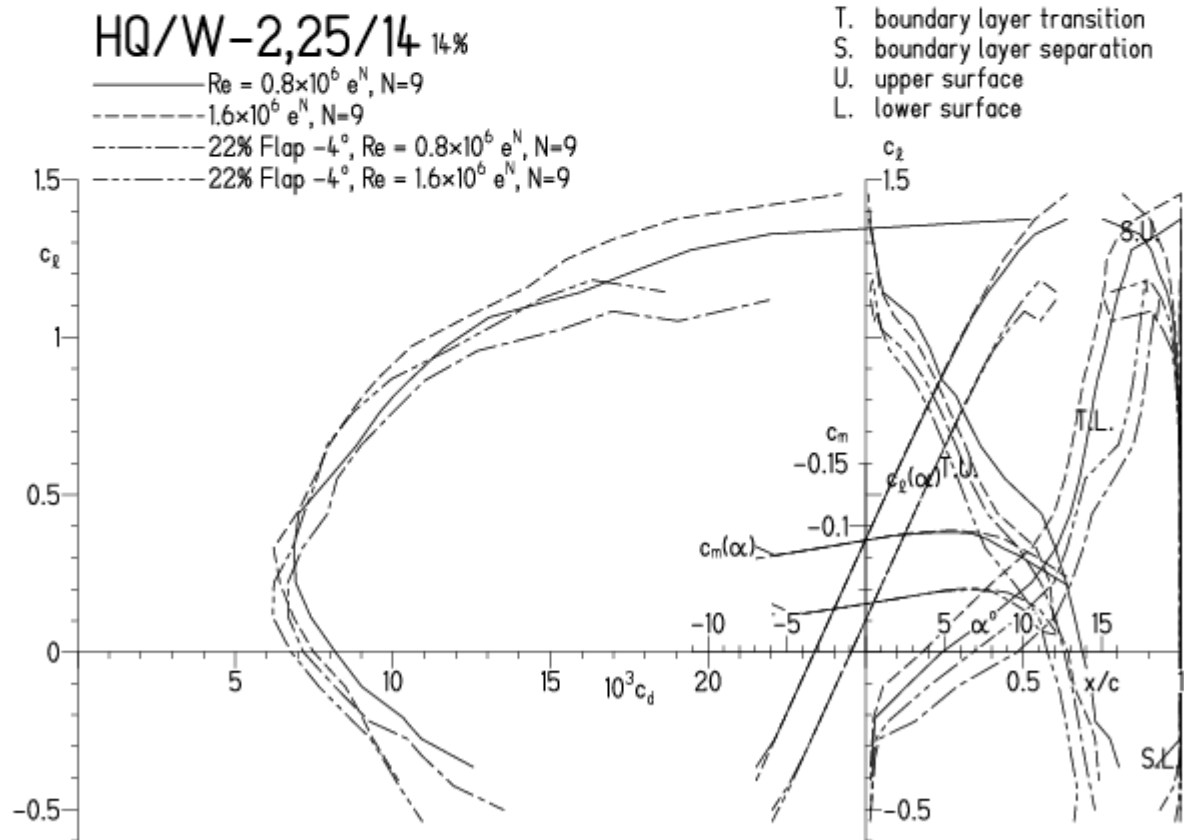


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

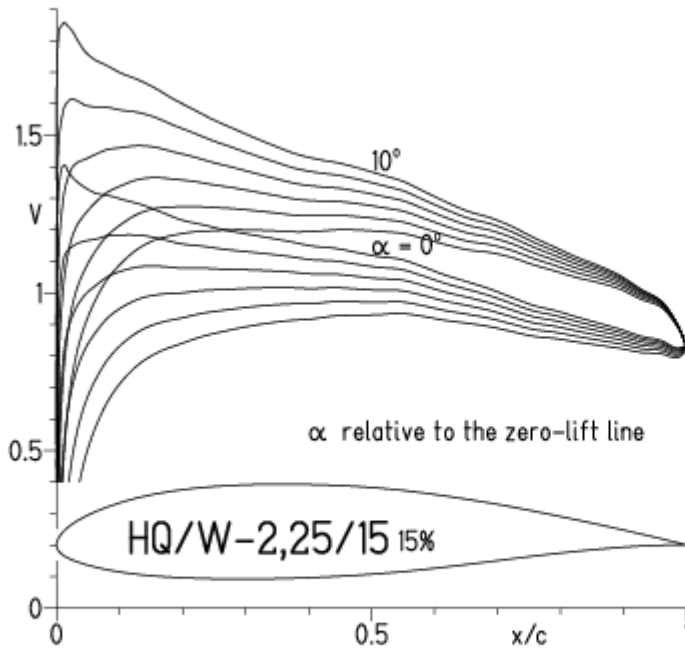


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

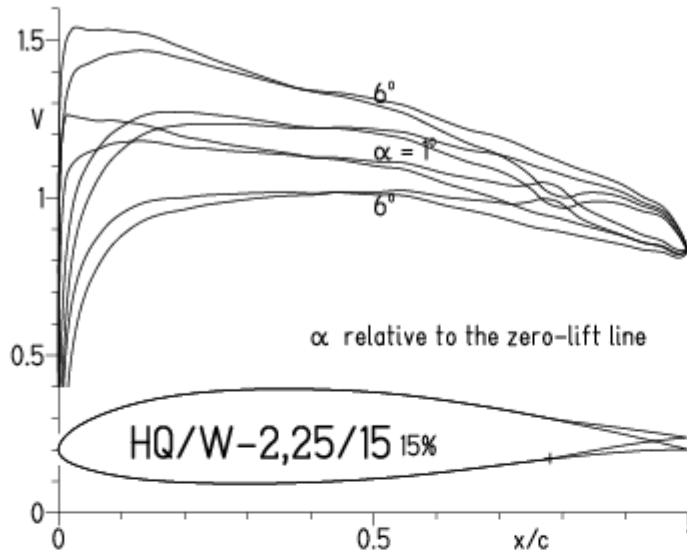


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

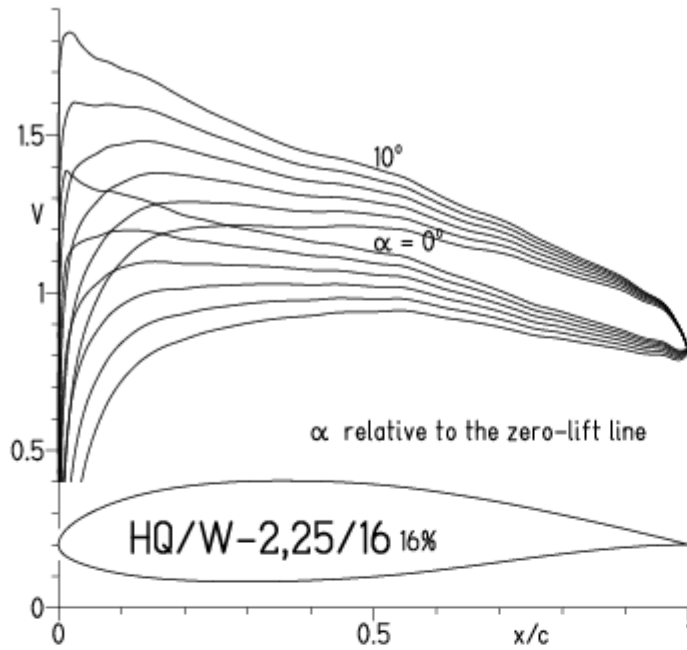
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

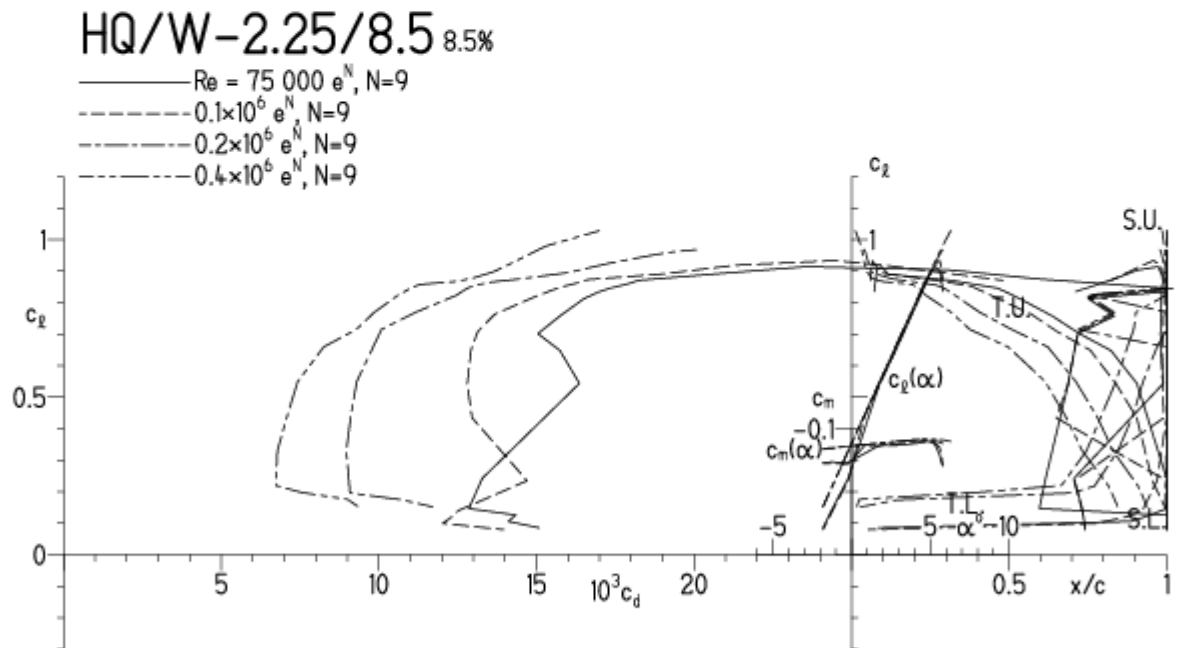


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

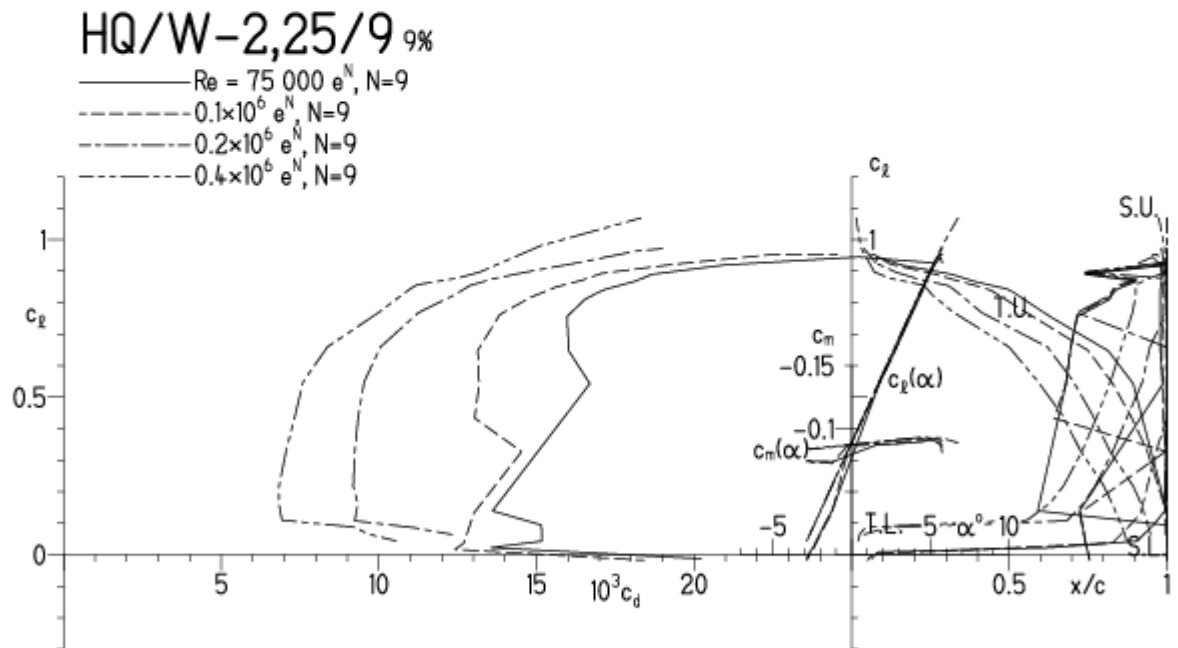


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

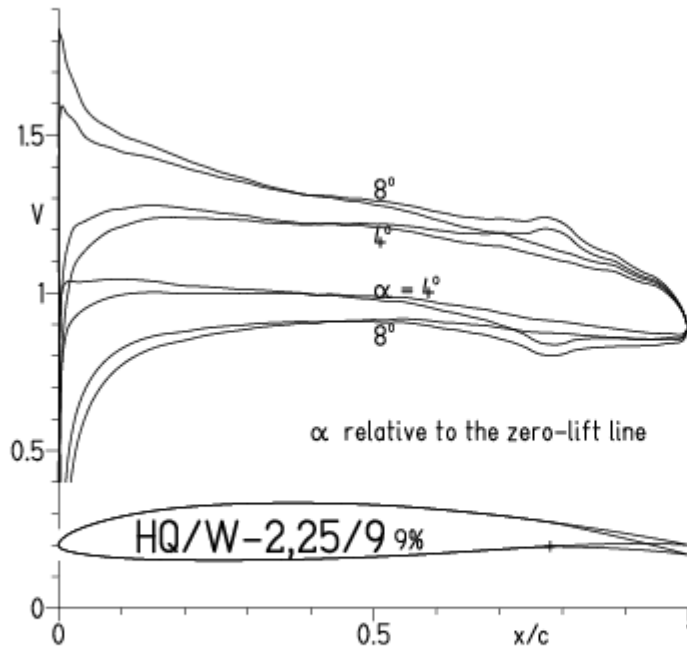
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

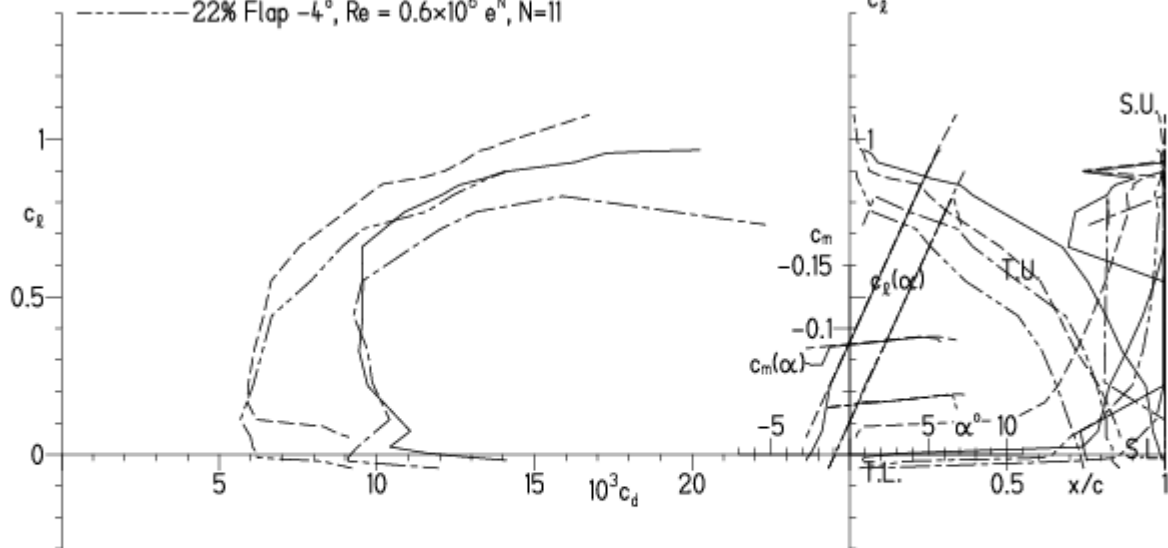
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

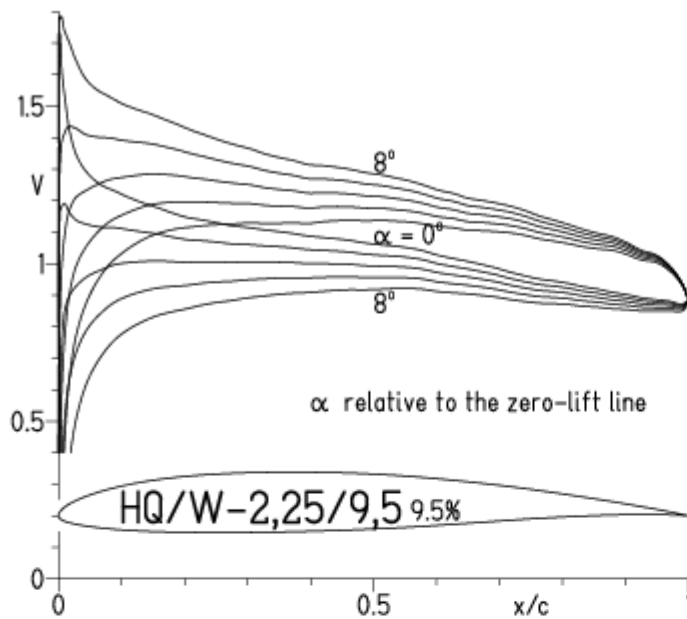
- Re = 0.2 × 10⁶ e^N, N=11
- - - 0.6 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.2 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.6 × 10⁶ e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

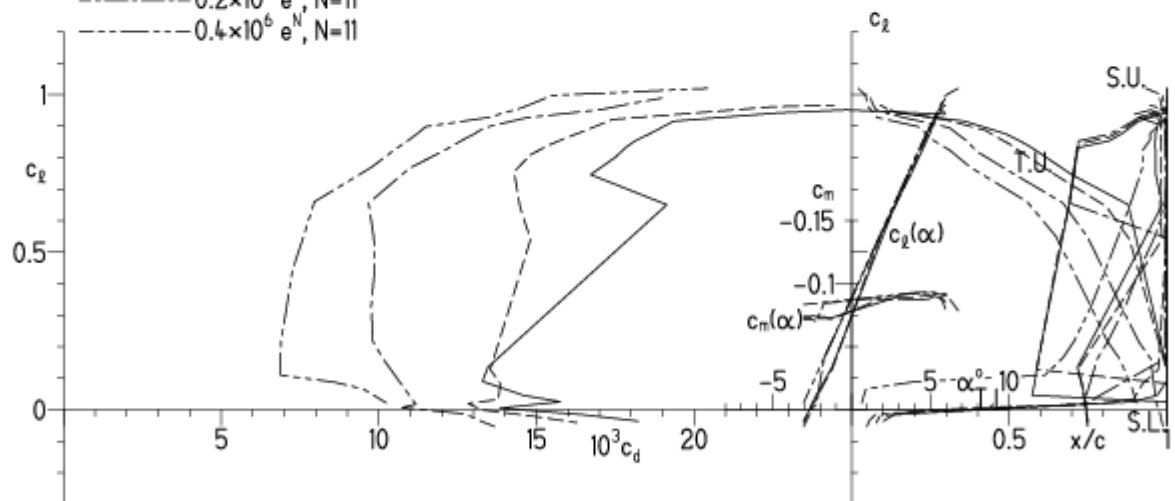
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
(Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



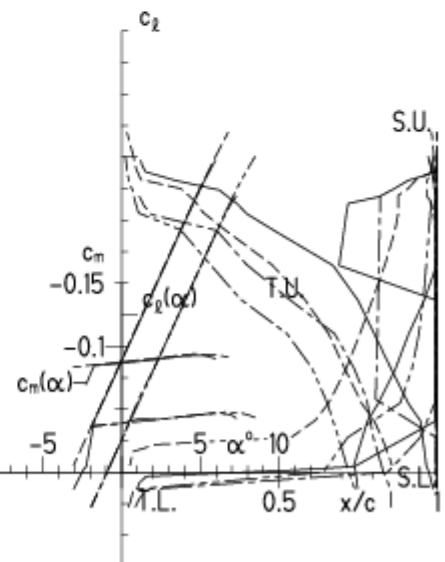
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

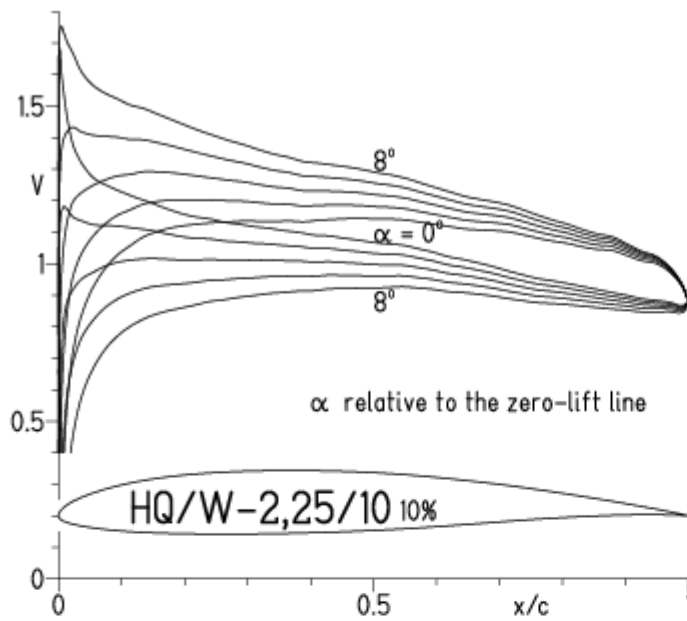


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

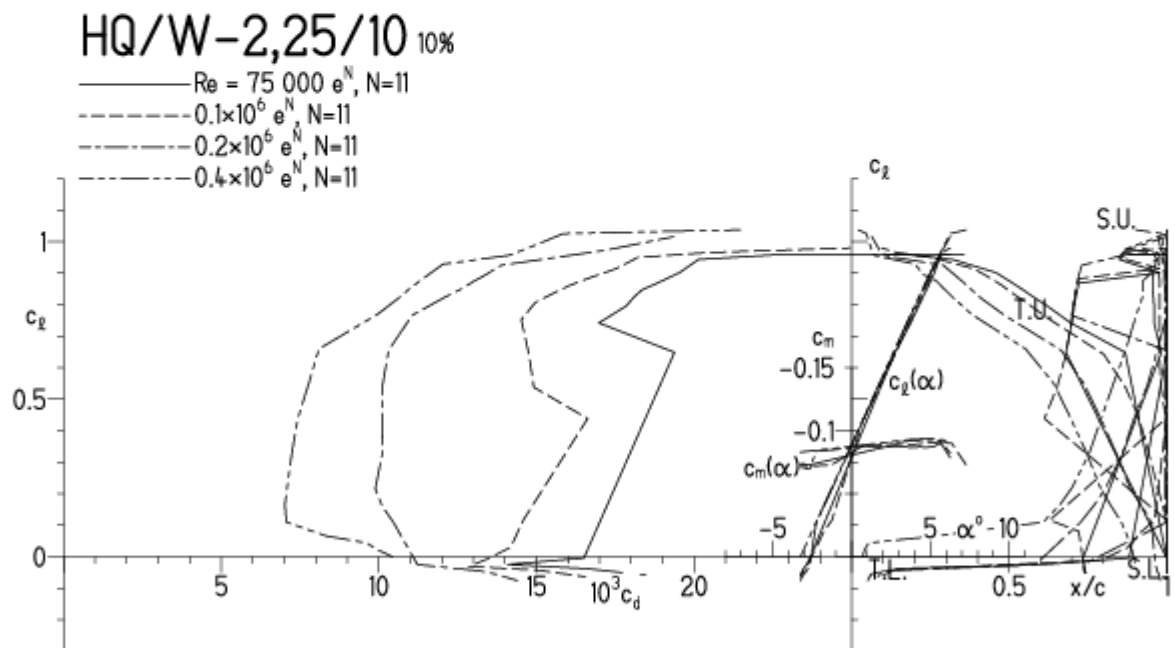


HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

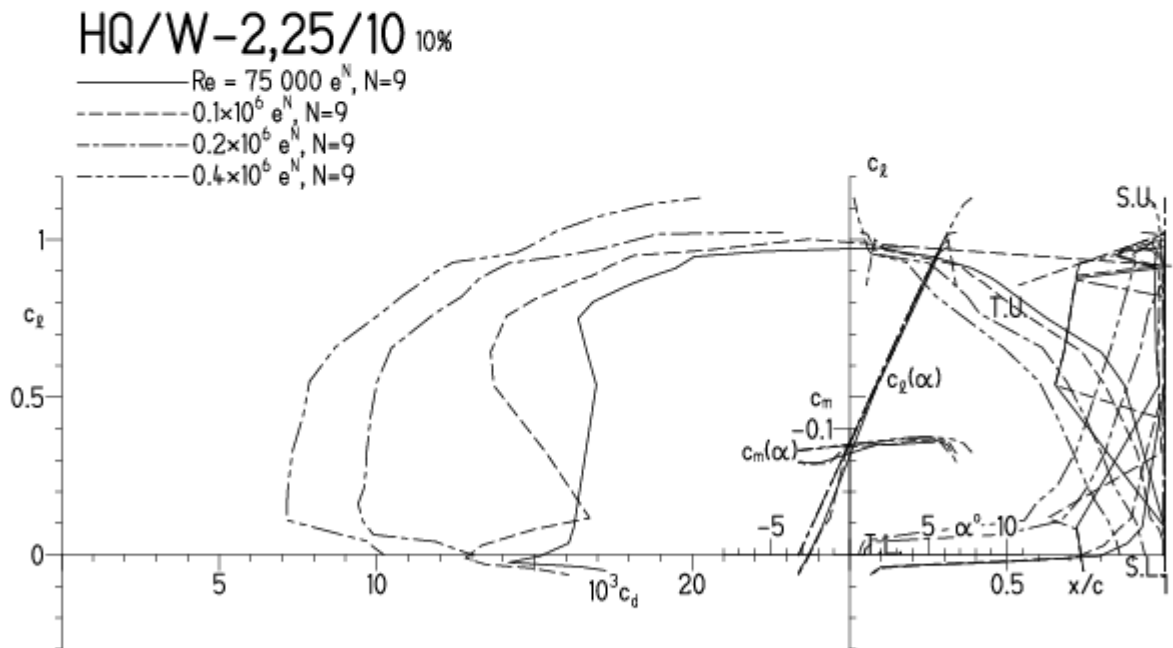


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

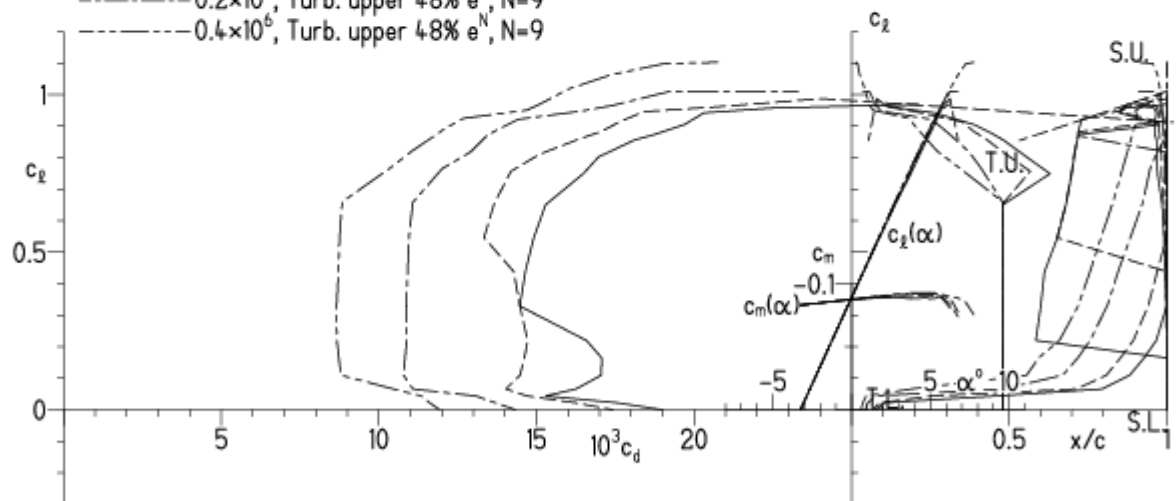
HQ/W-2,25/10 10%

— $Re = 75\,000$, Turb. upper 48% e^N , $N=9$

- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$

- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$

- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

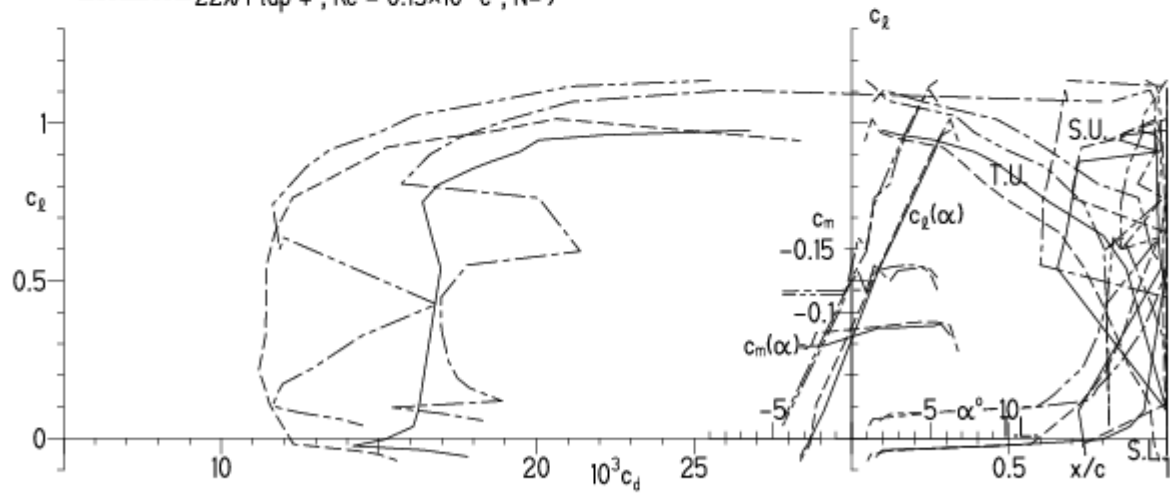


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

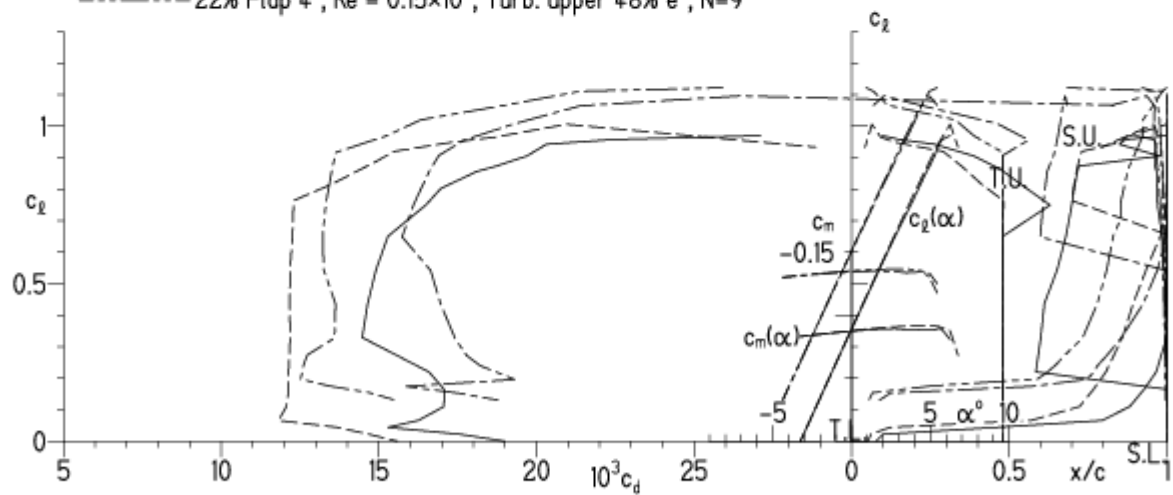


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

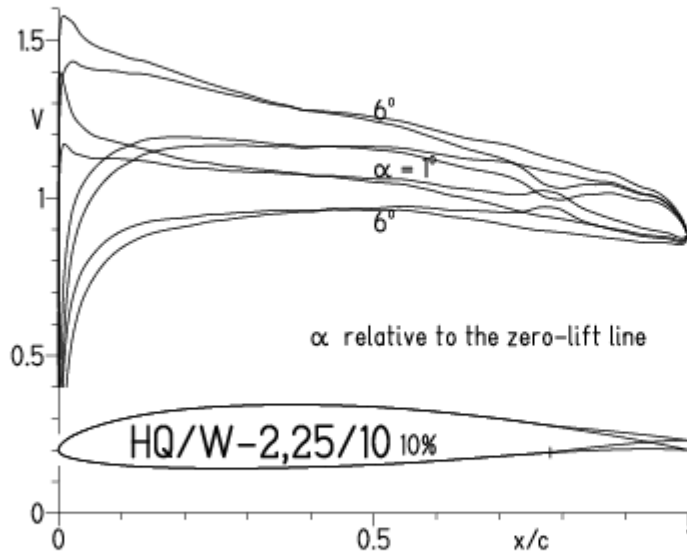
- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

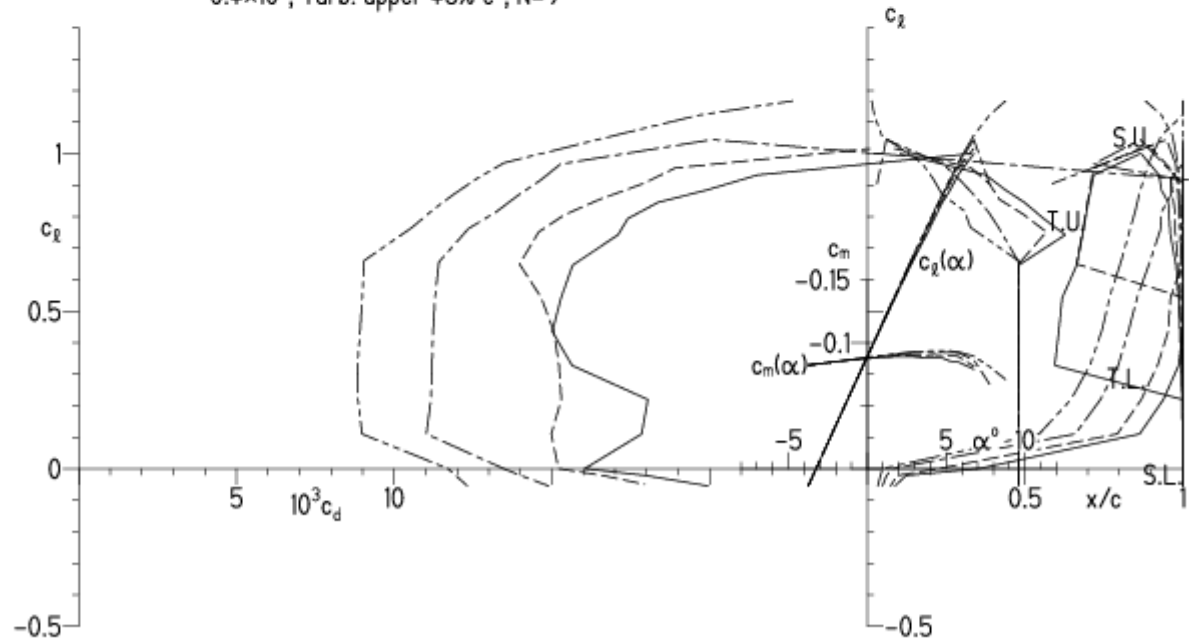
EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

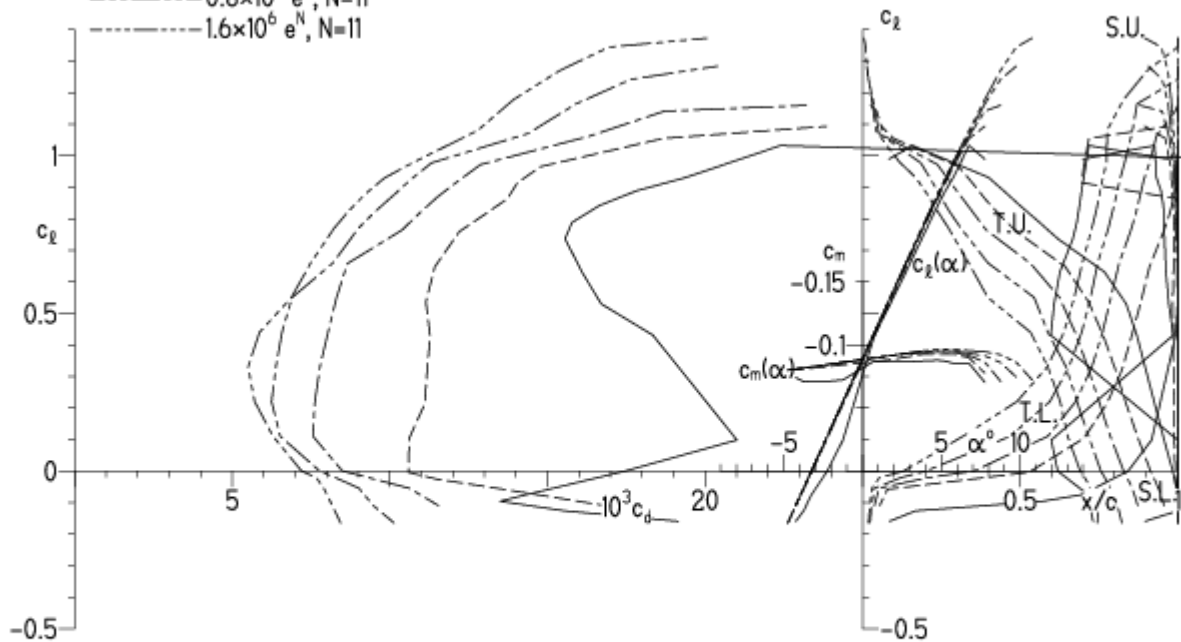
EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

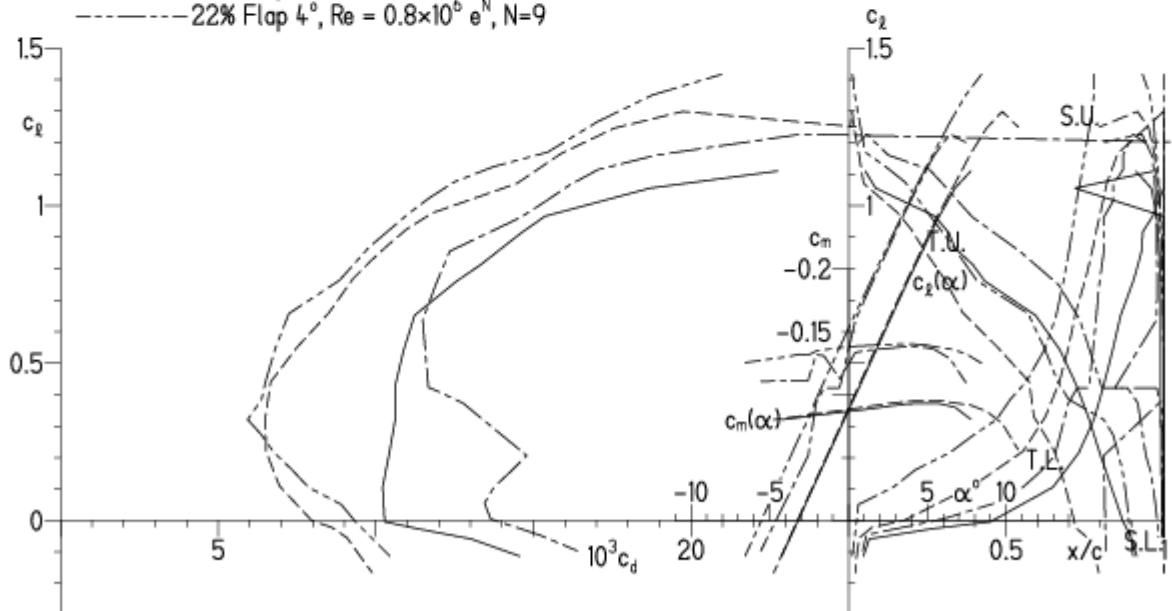


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

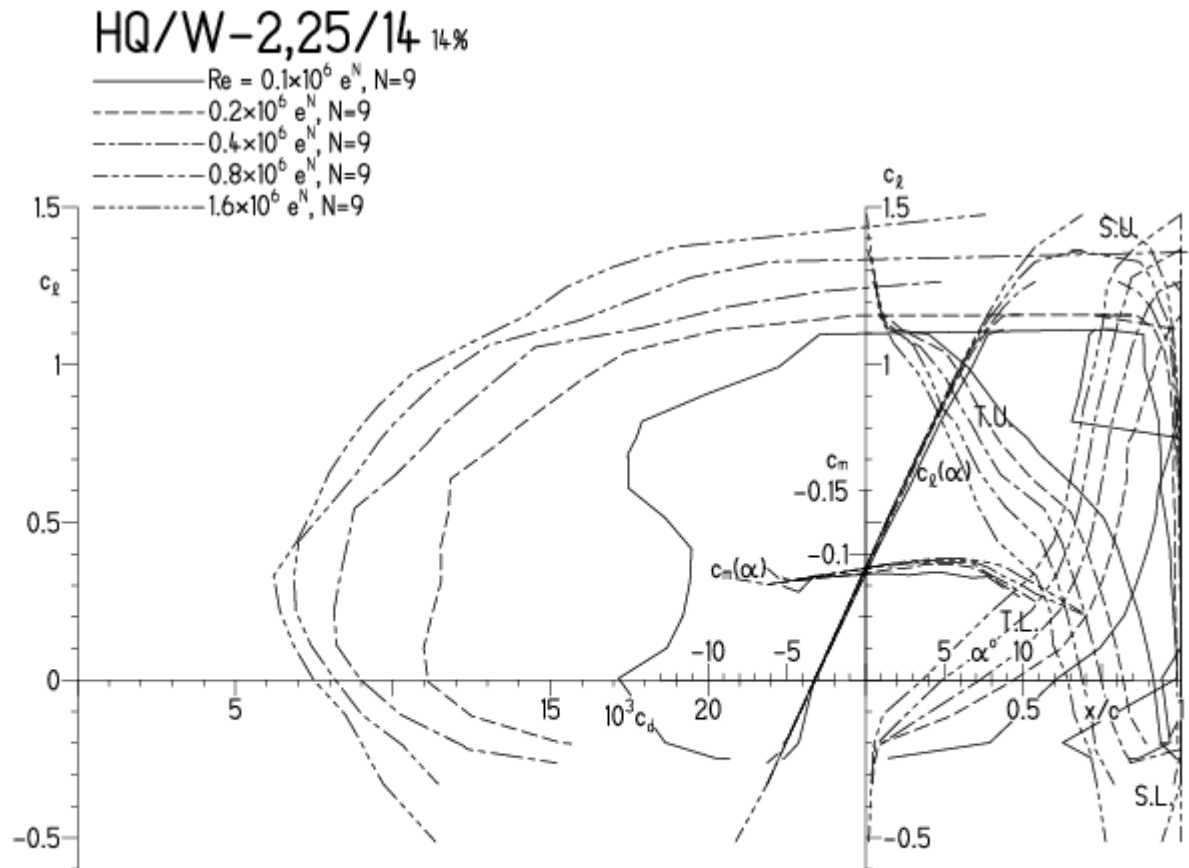


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

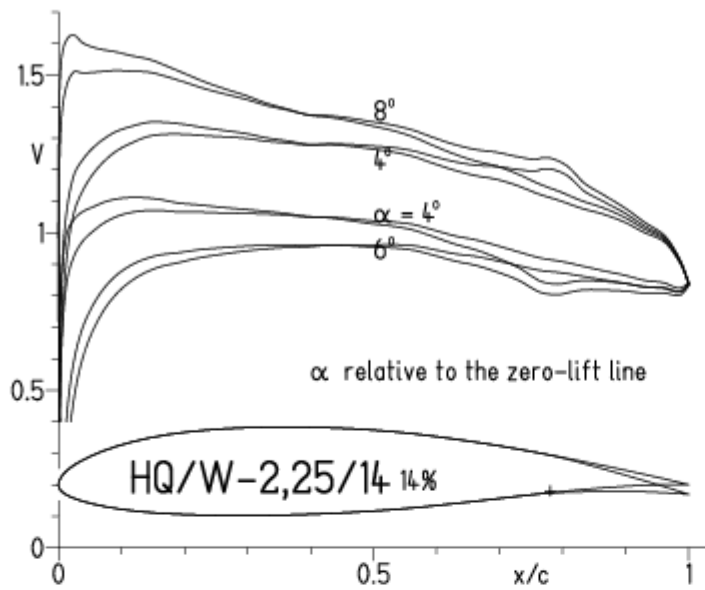
HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

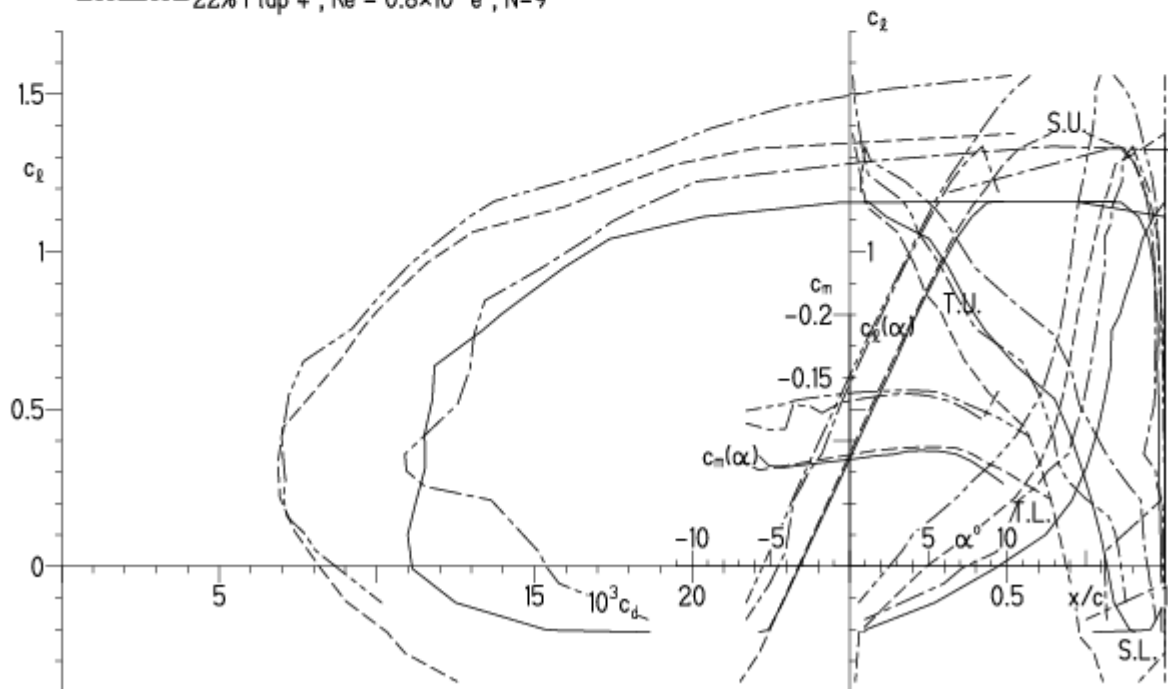


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20

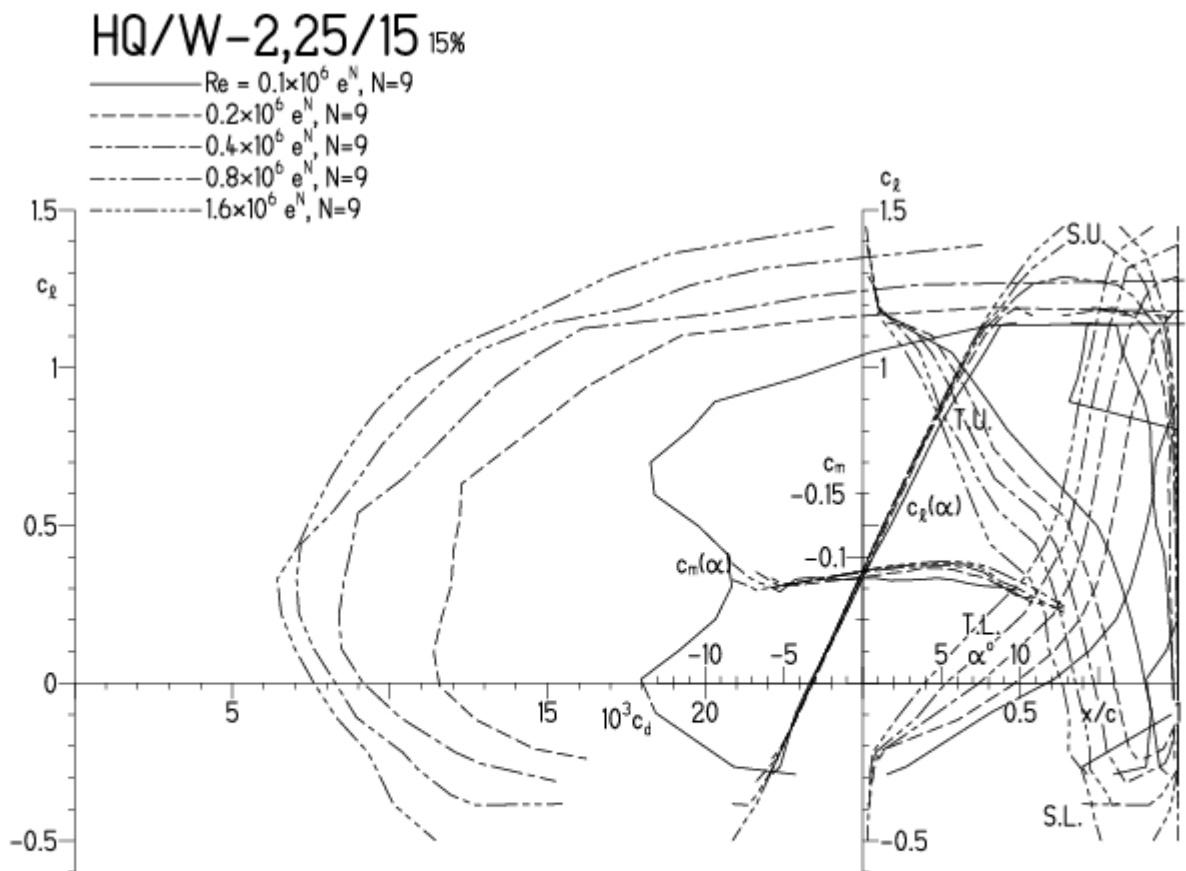


HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

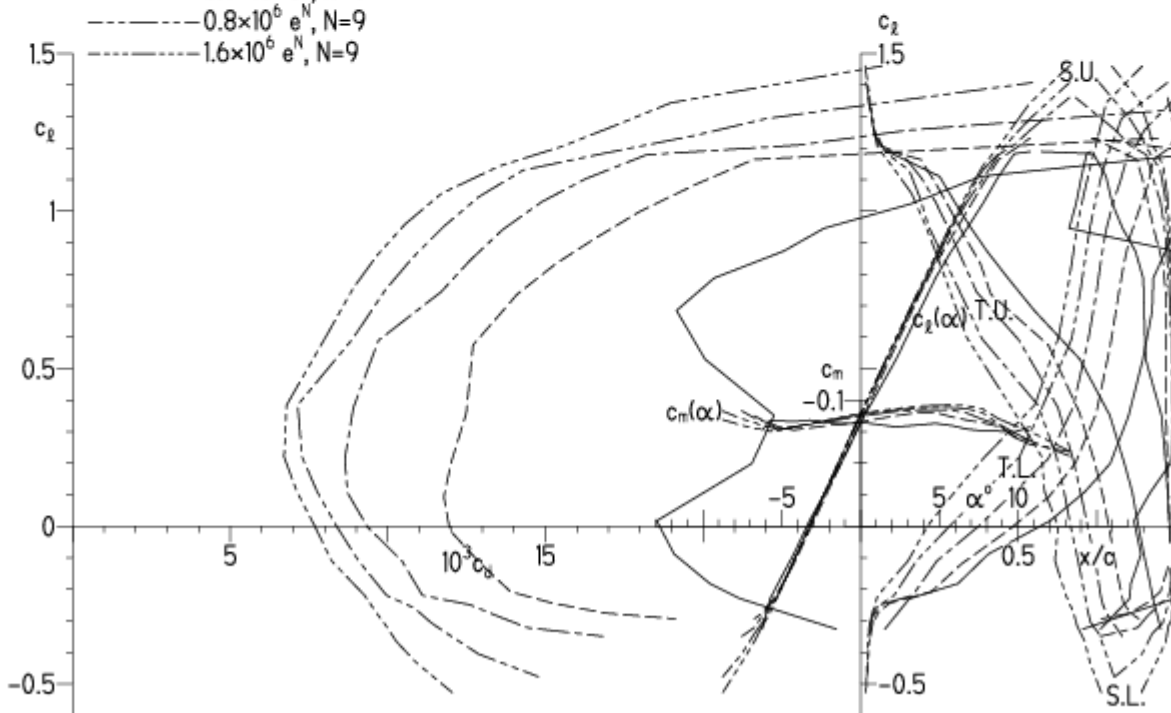
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



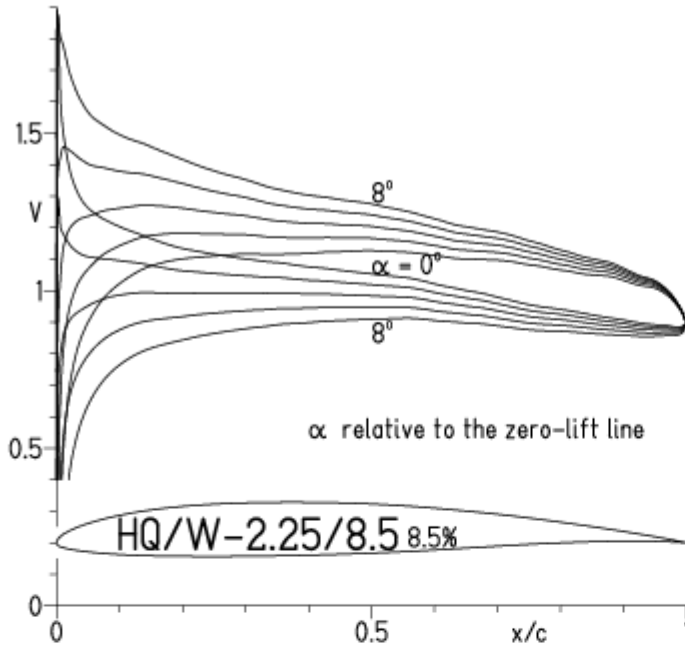
EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

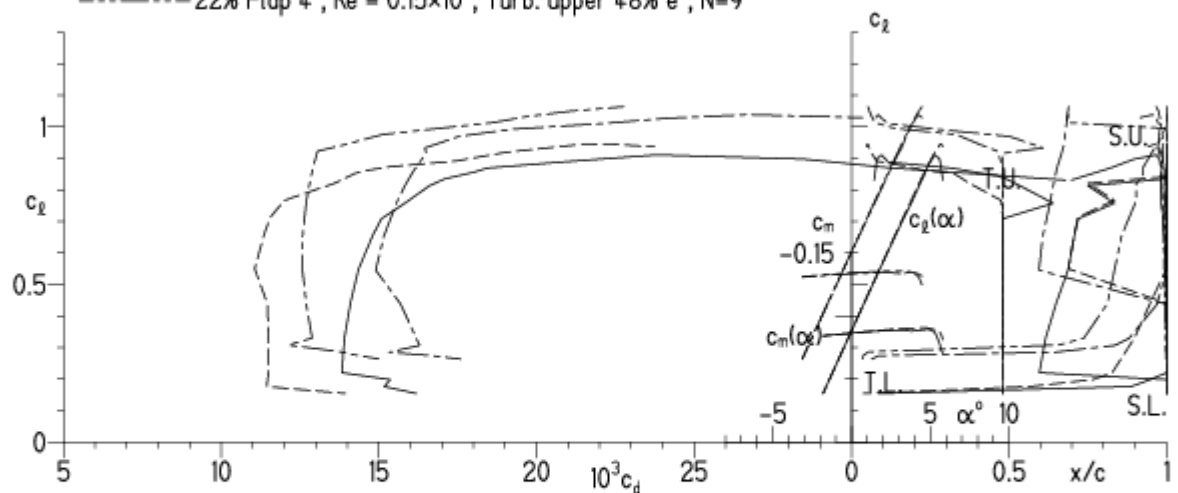


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

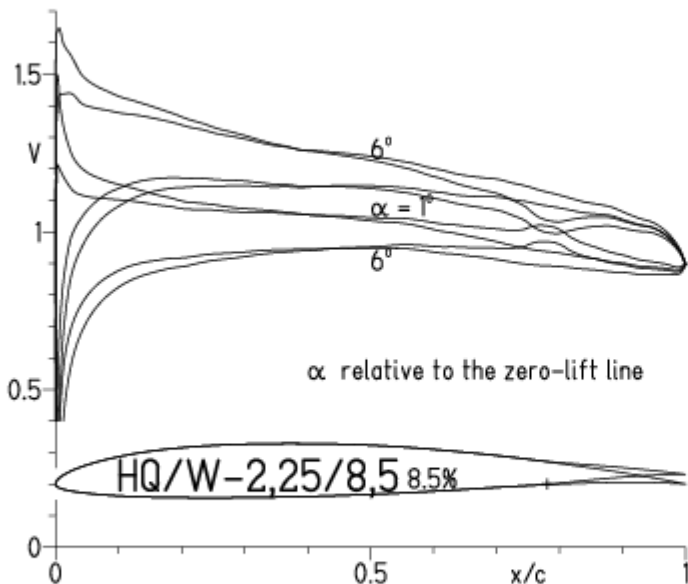
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

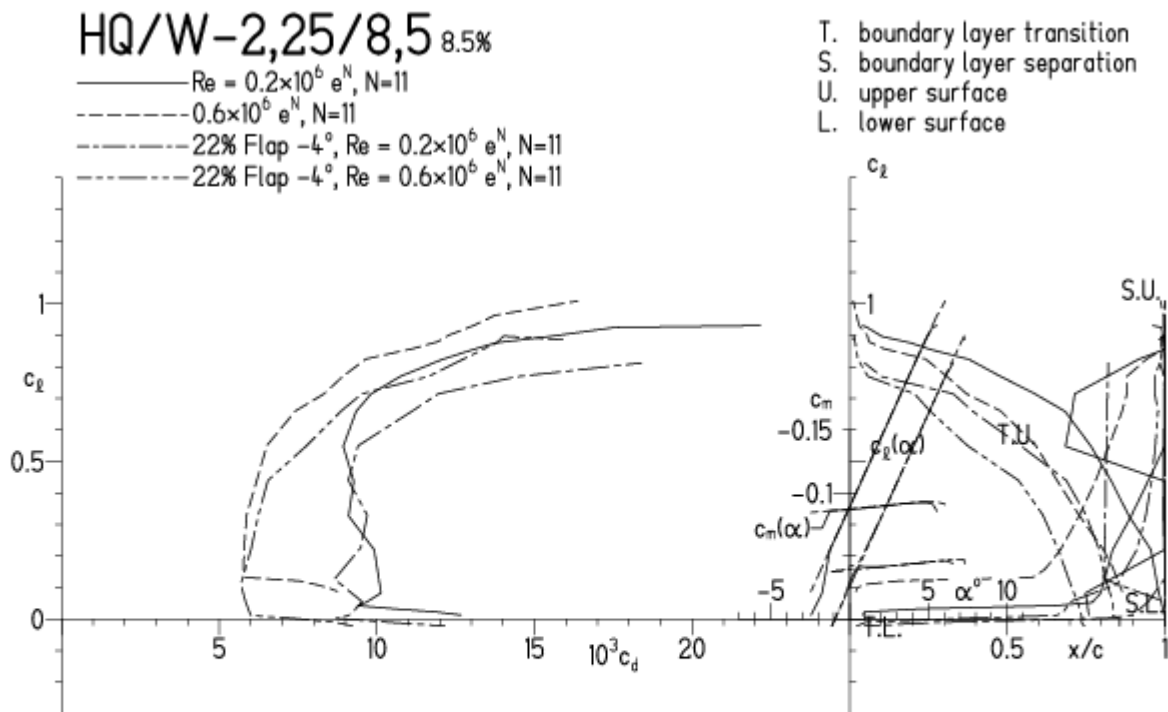


HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

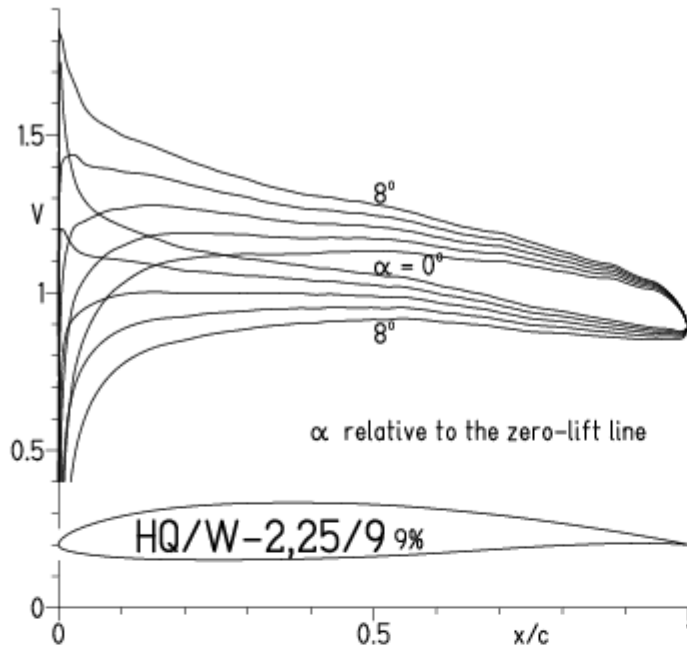


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

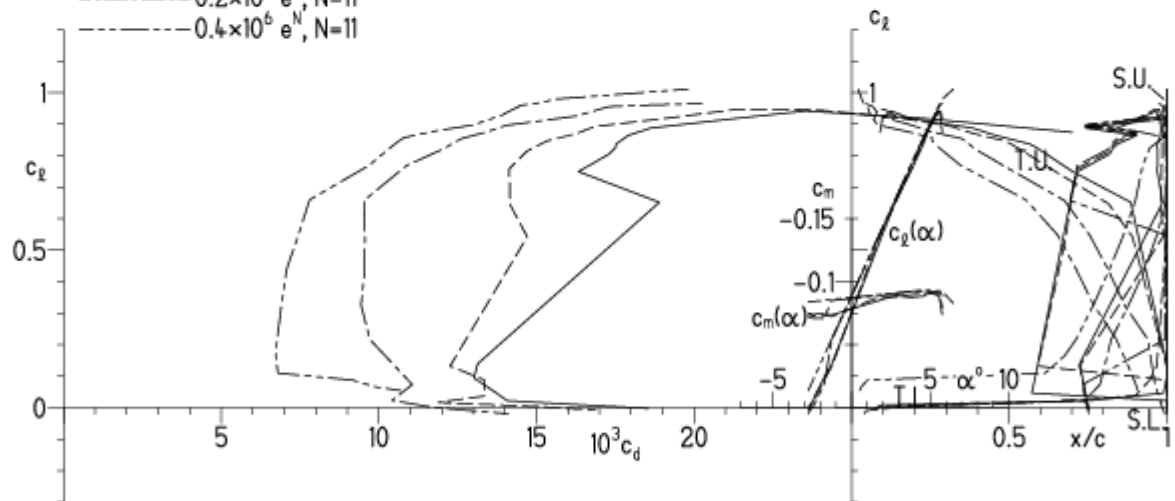
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

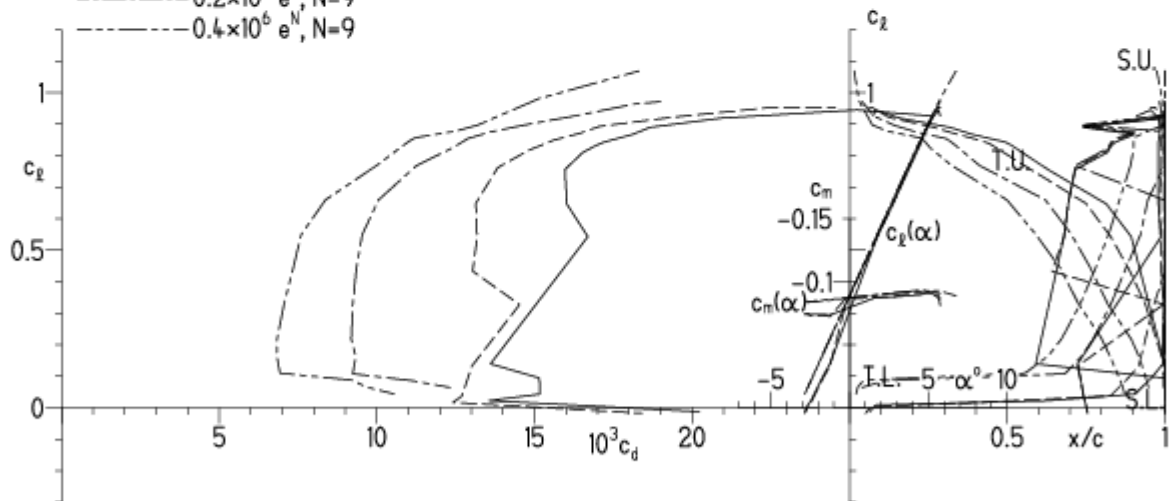
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

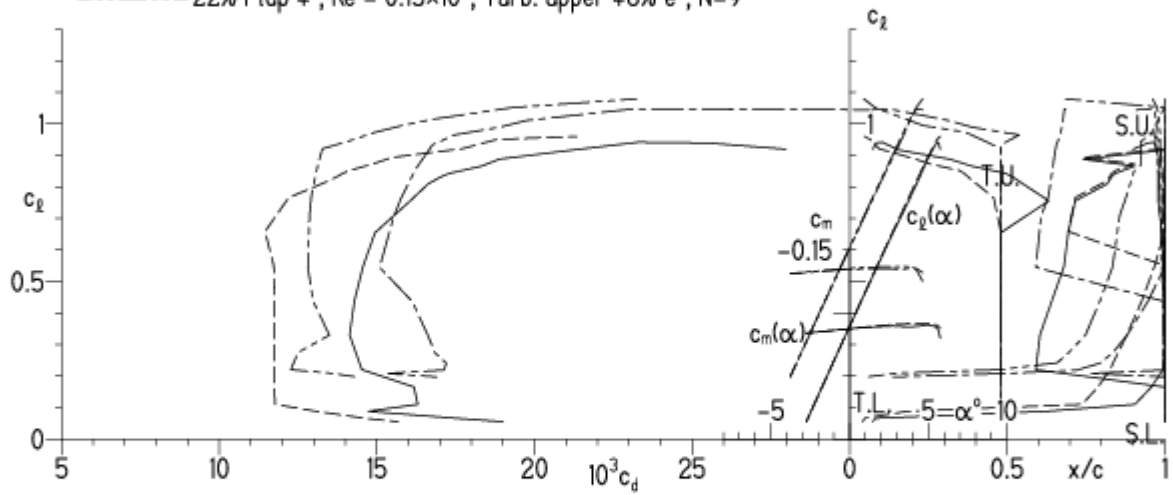


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

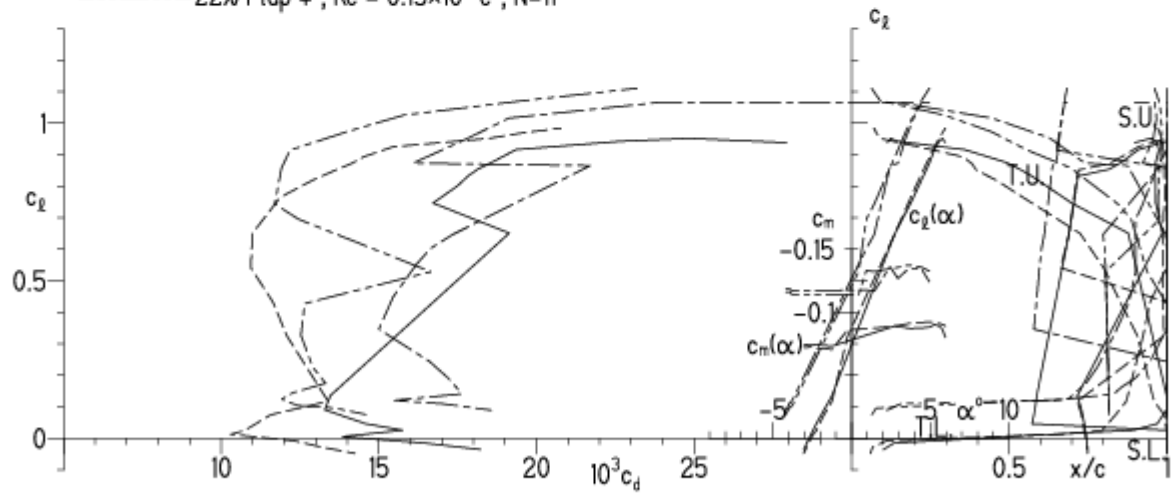


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



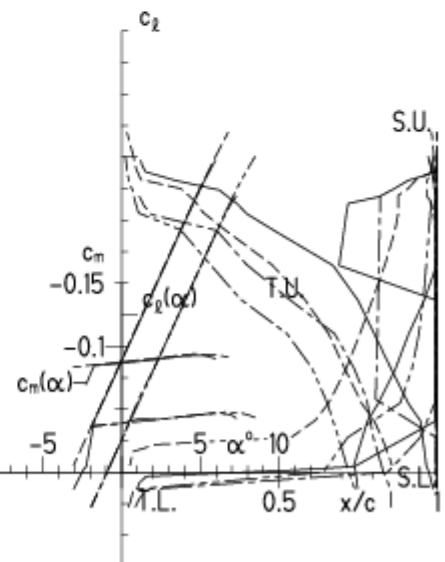
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

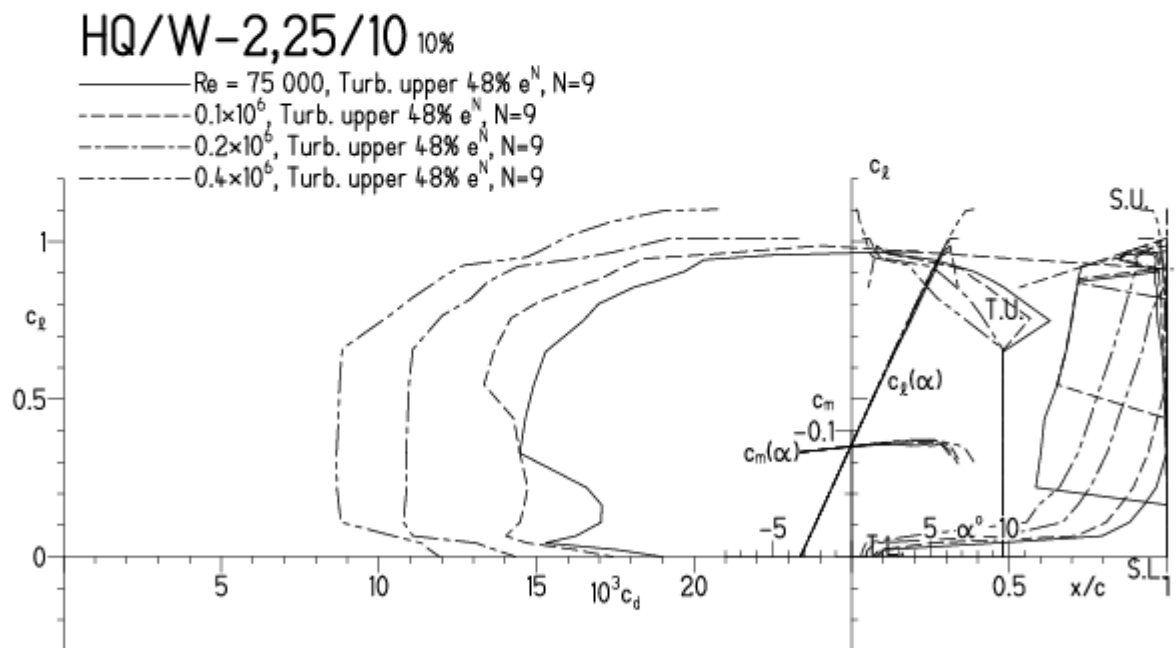


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

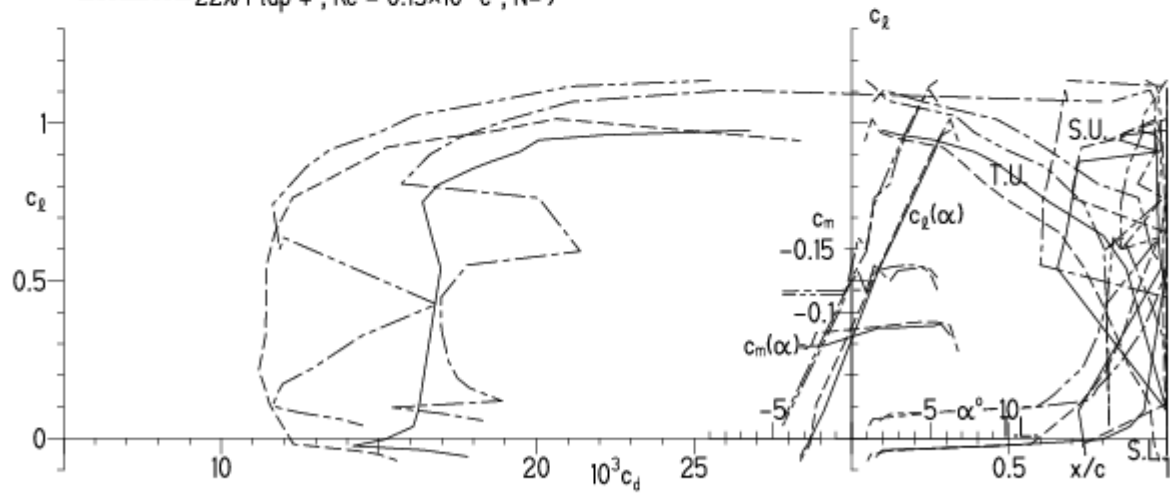


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

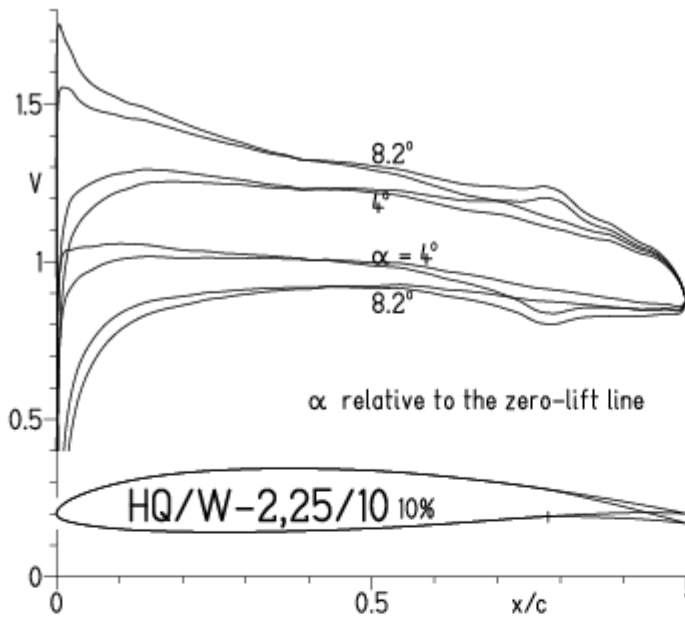
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

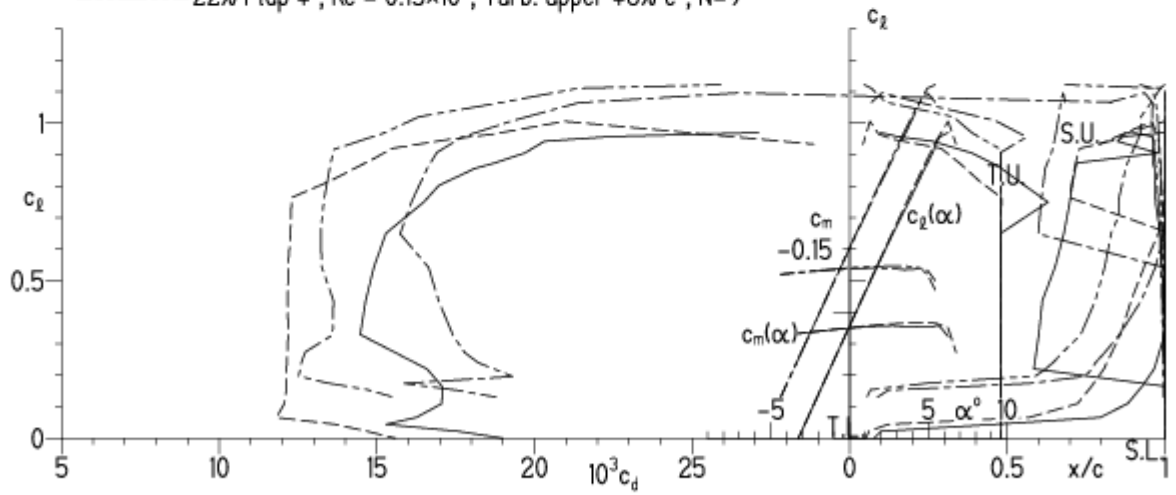


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

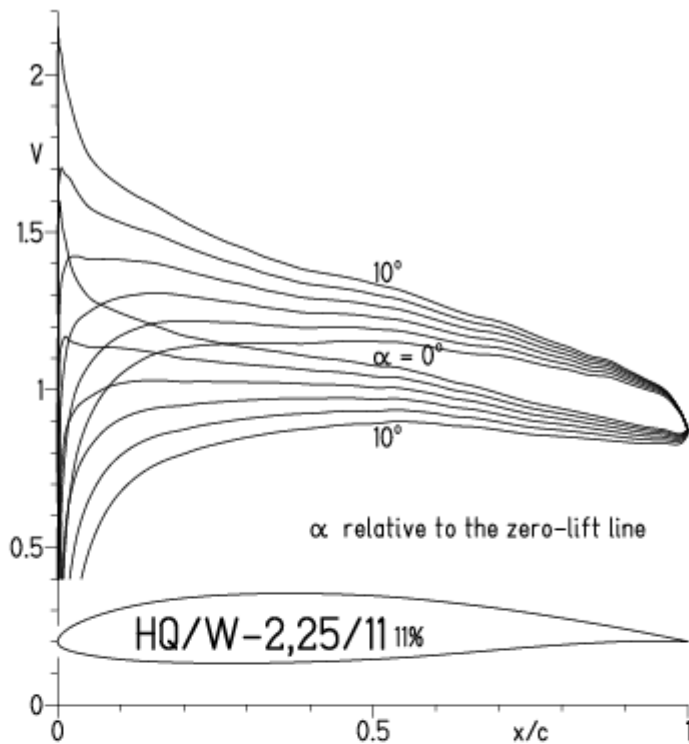


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

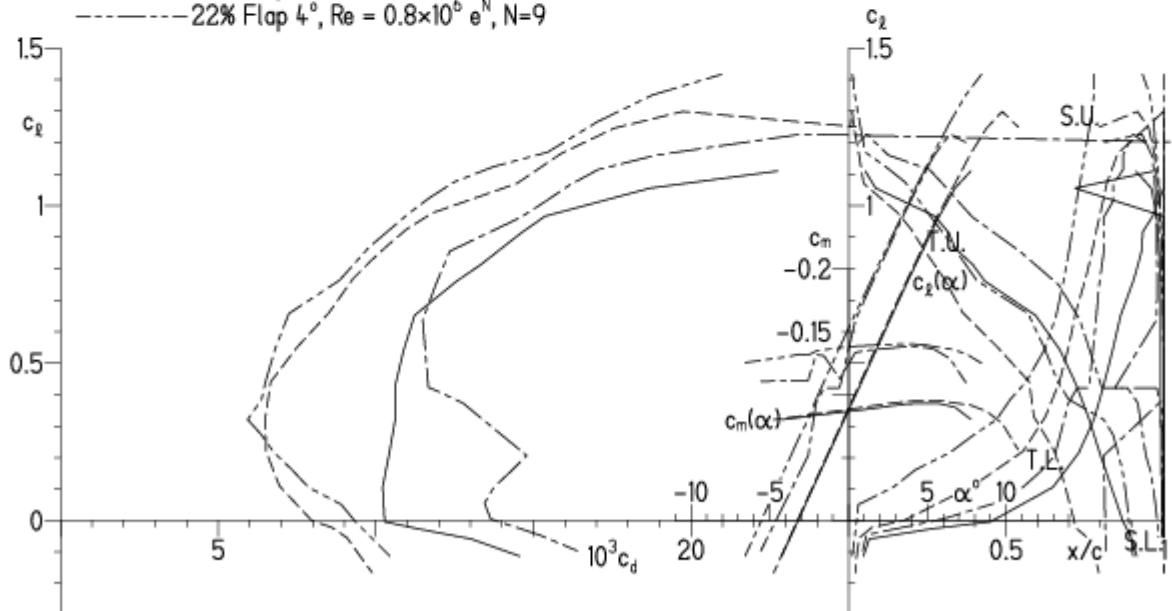


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

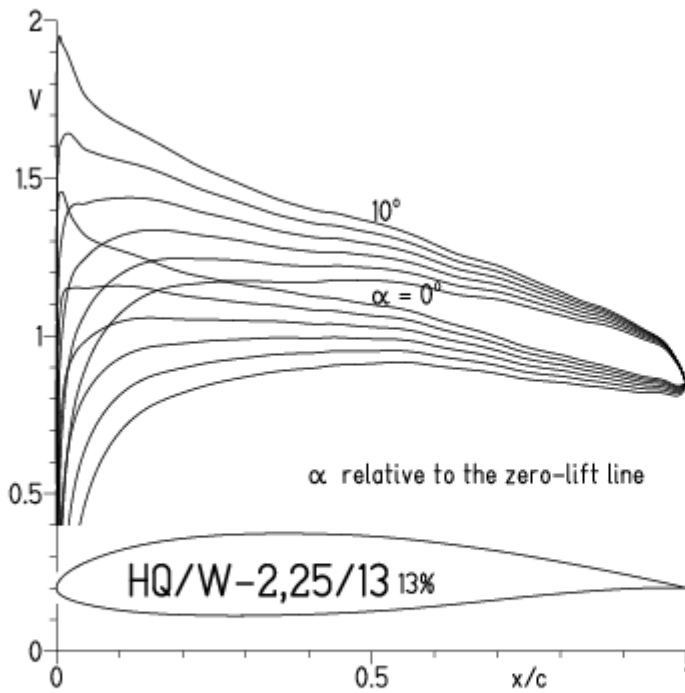


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

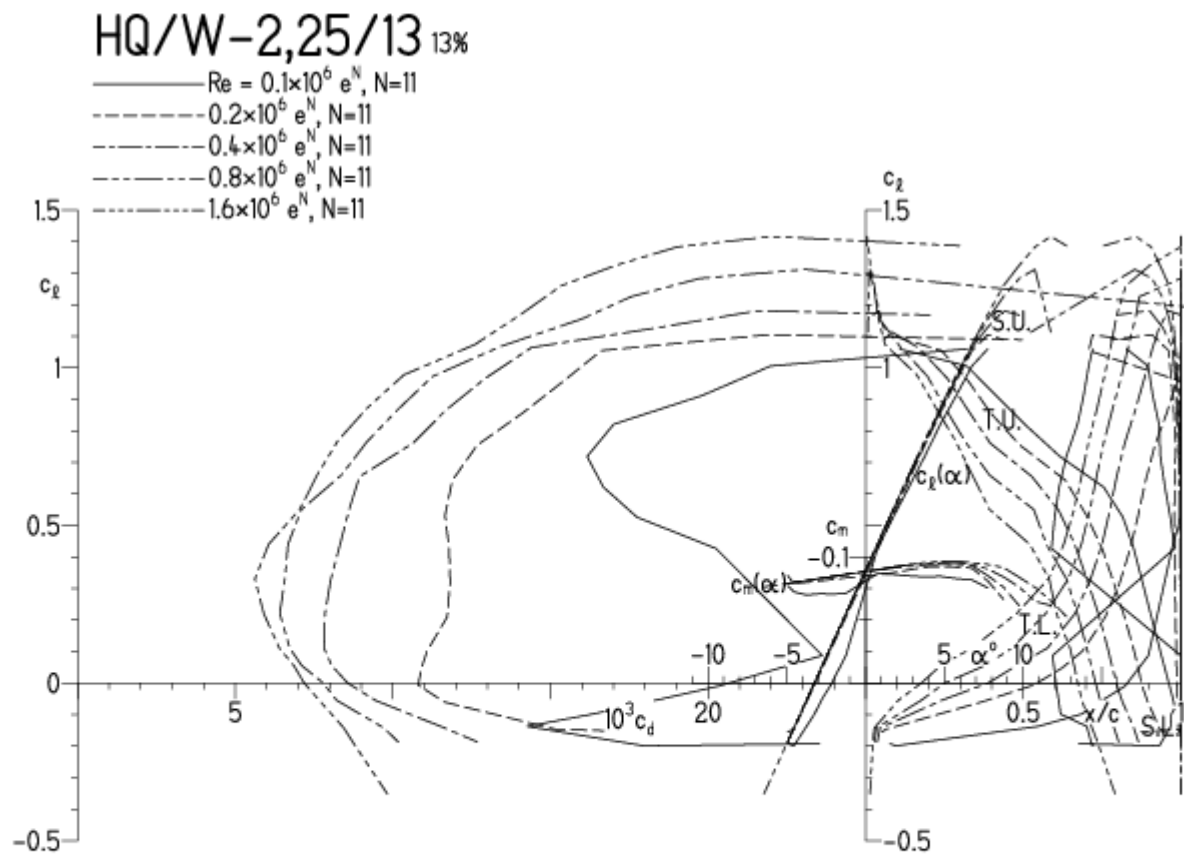


HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

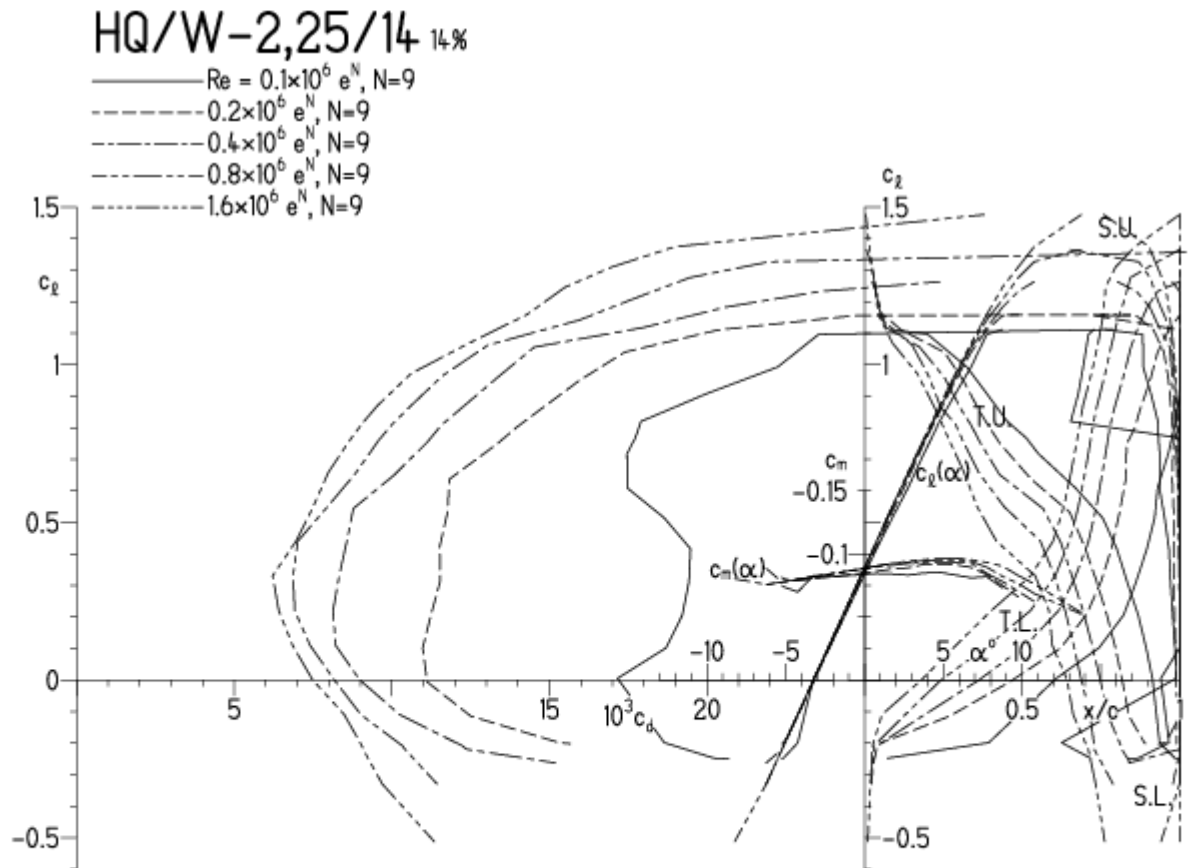


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

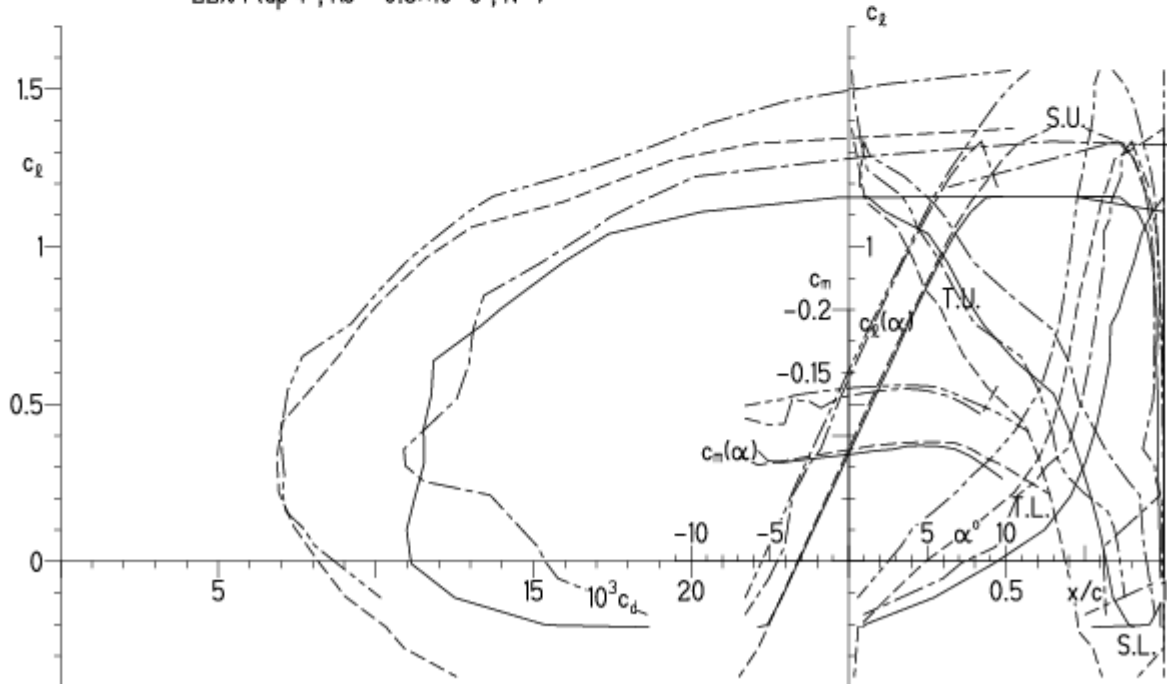


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

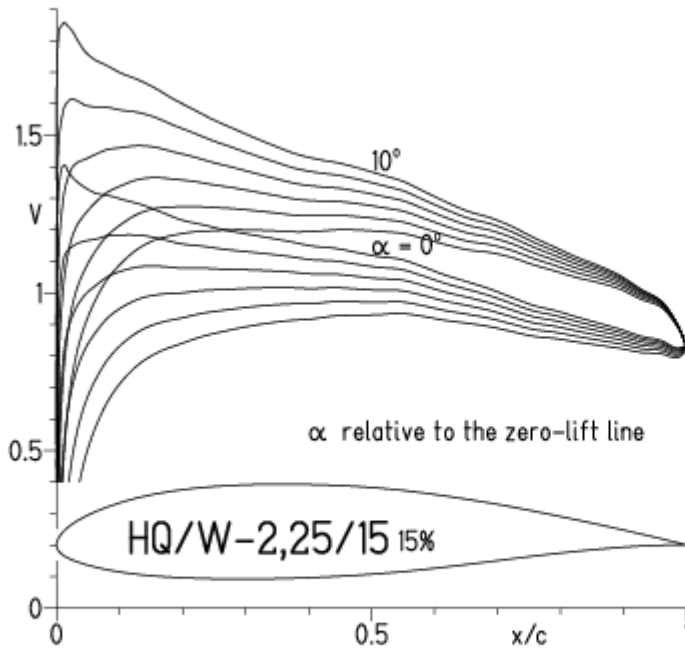


EPPLER 2005 V. 8.5.07

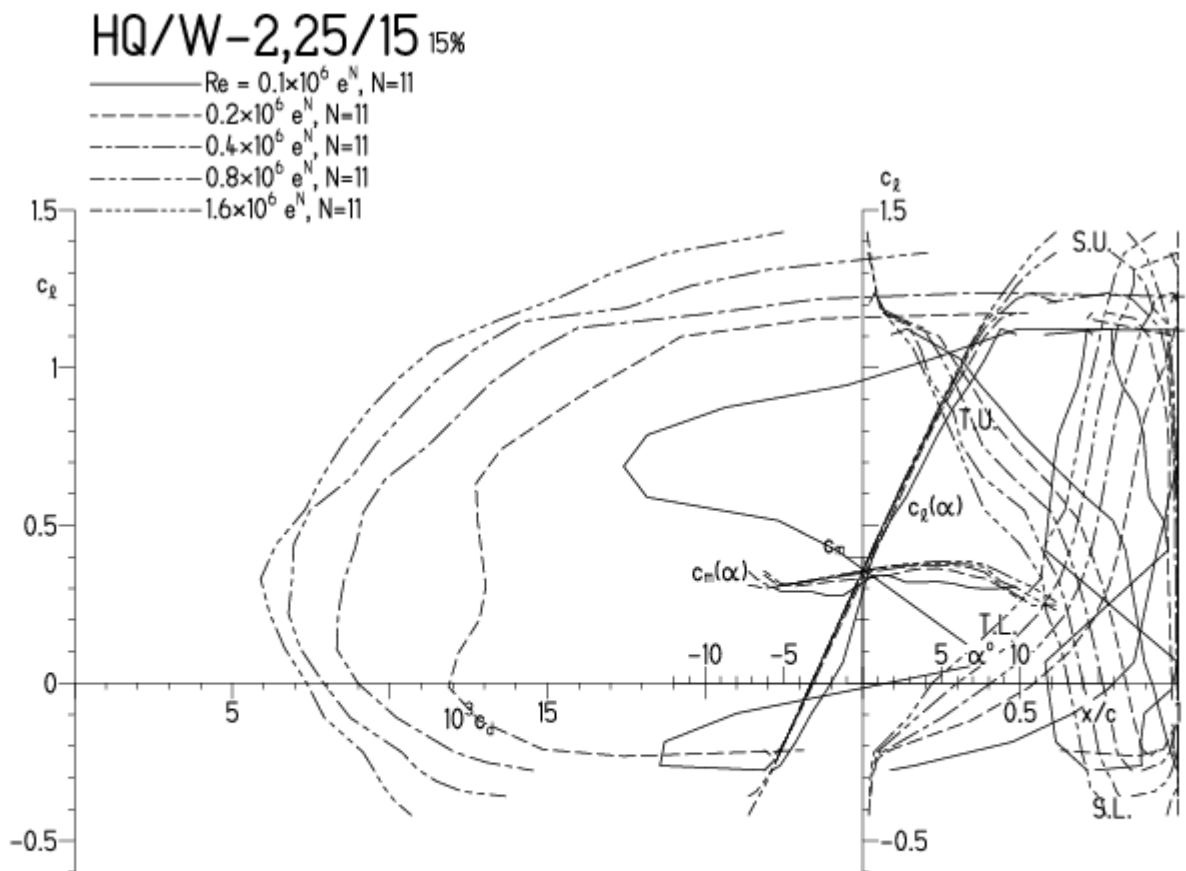


HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

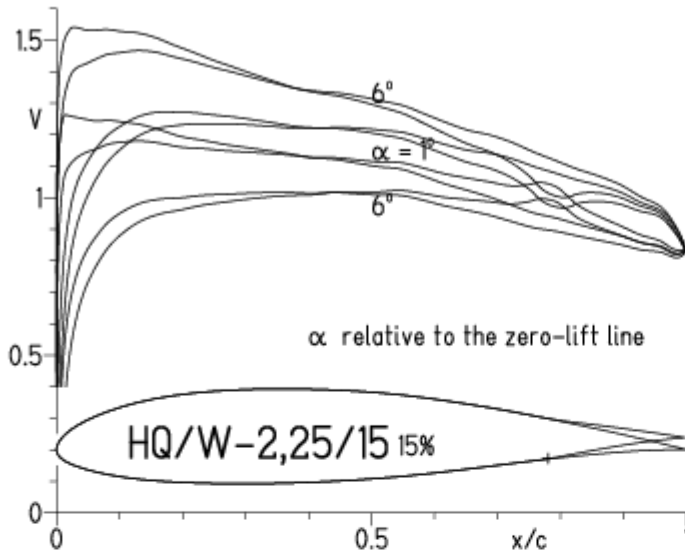


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



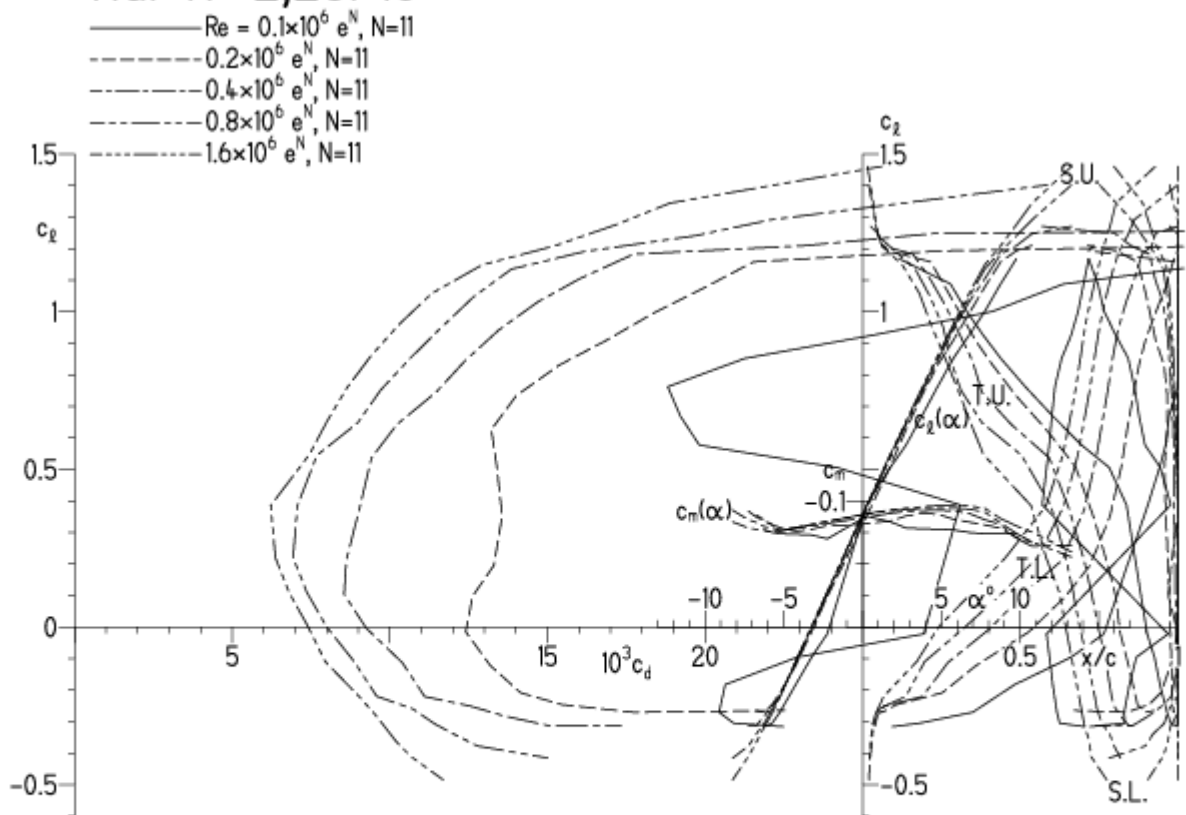
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

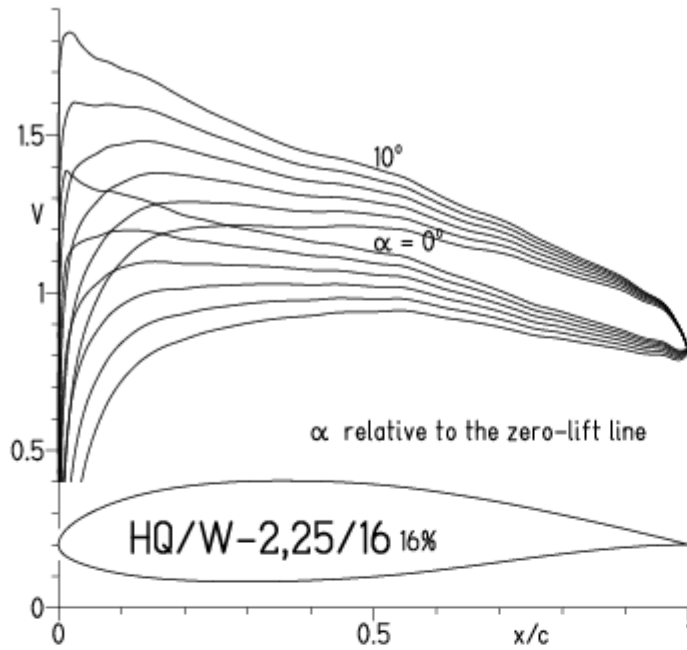
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41

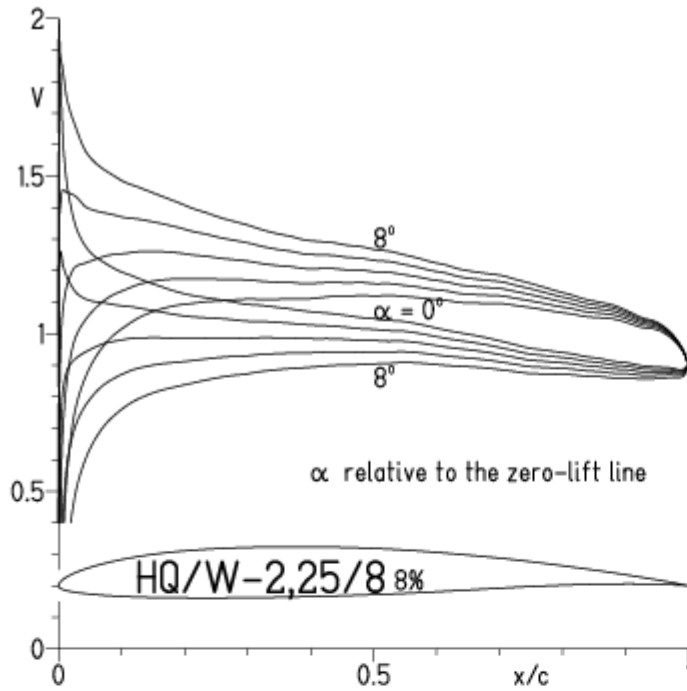


EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

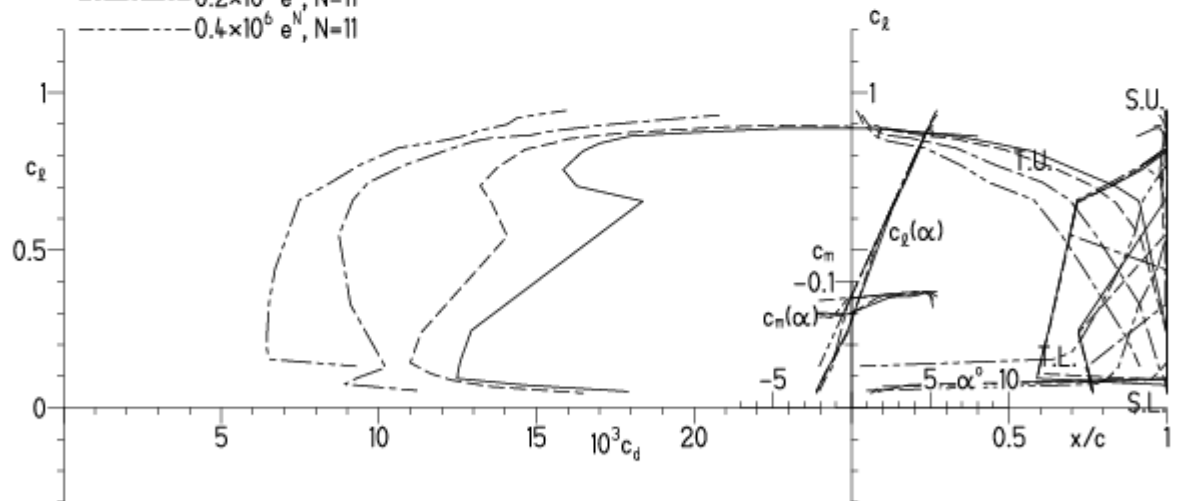
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

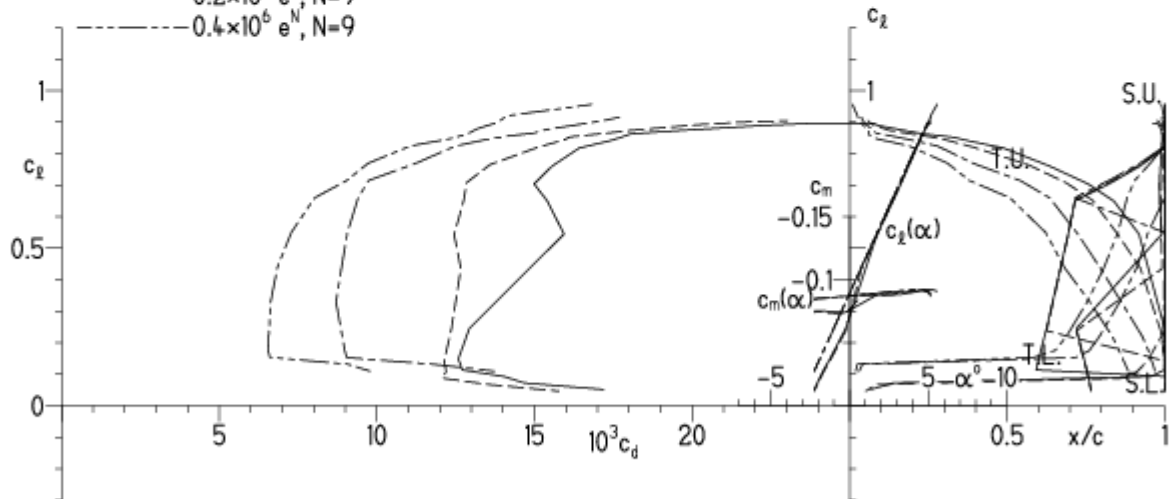
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - · 22% Flap 4°, Re = 75 000 e^N, N=9
- · - · 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

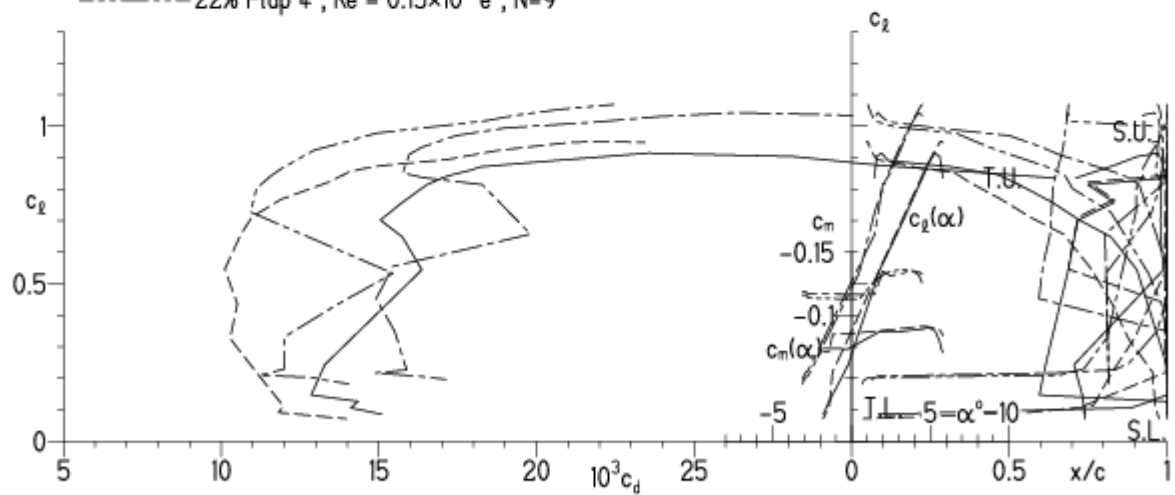


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

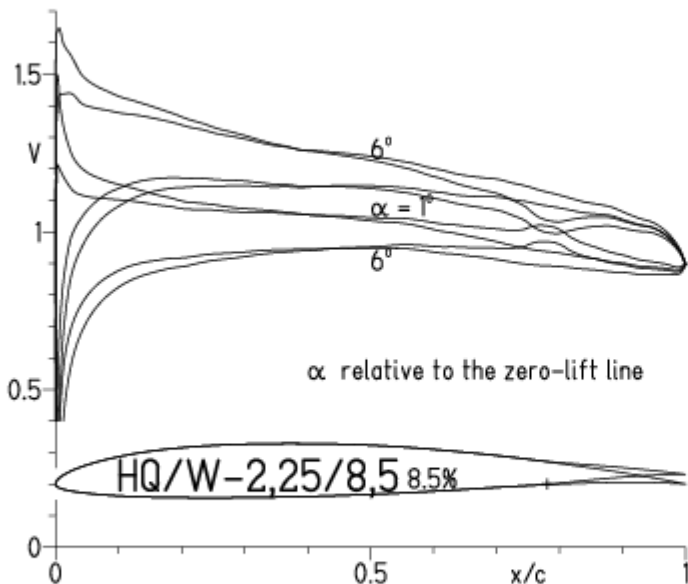
- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

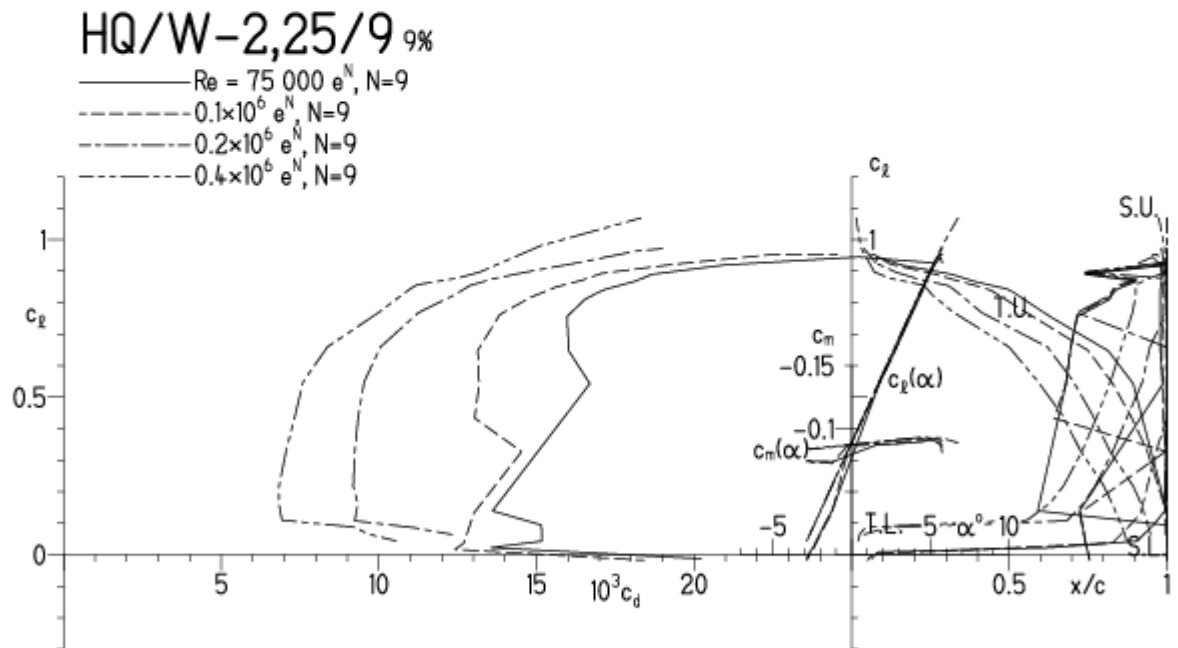


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

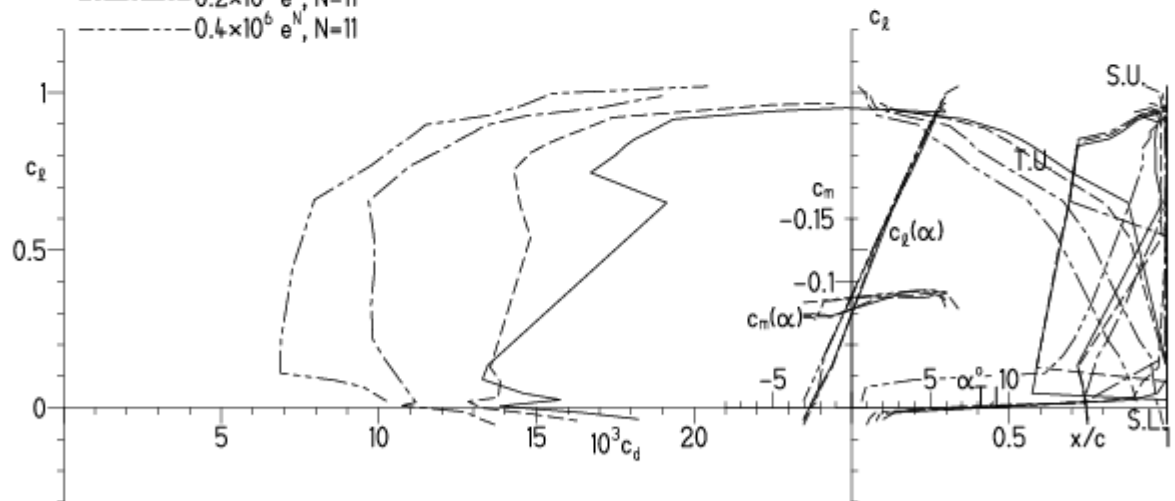
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

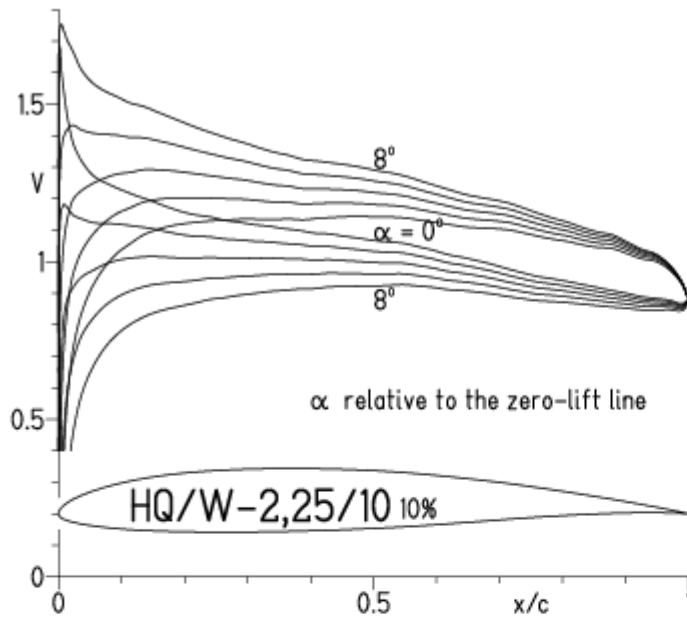


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

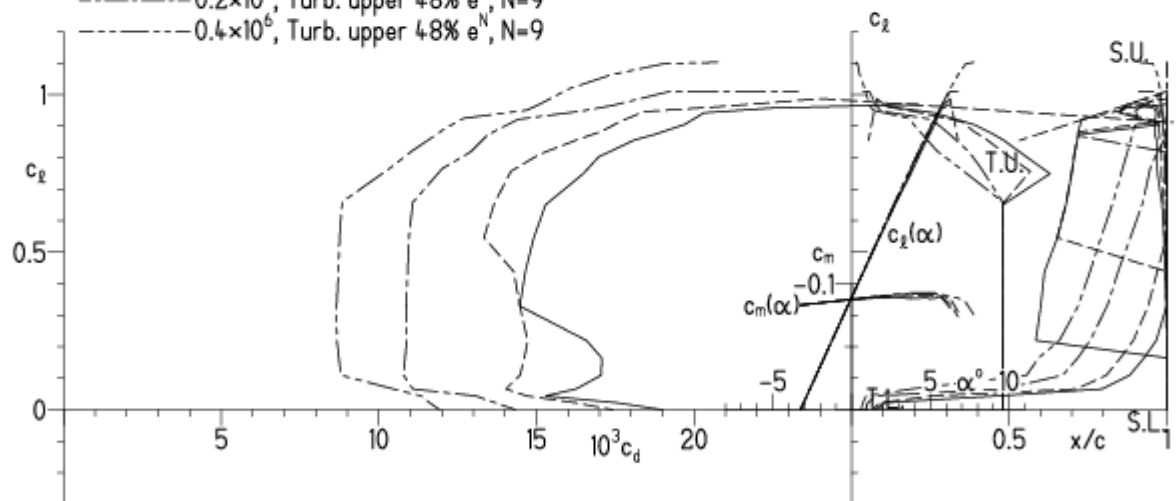
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

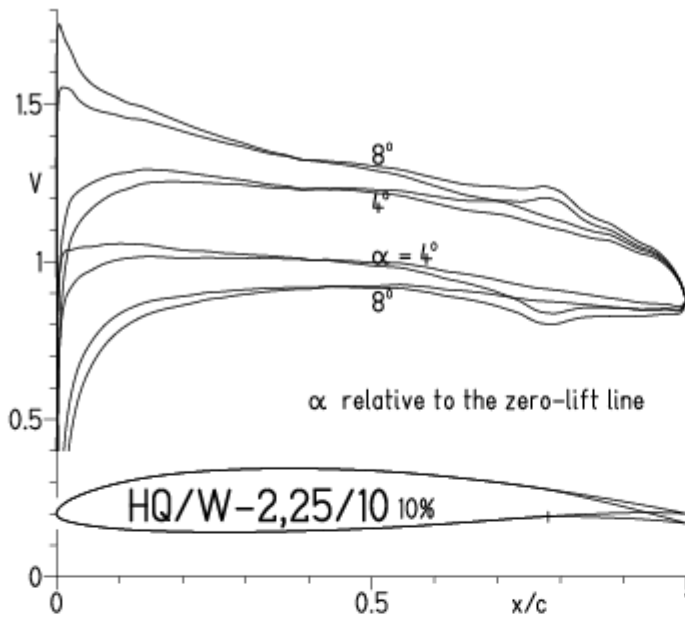
HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

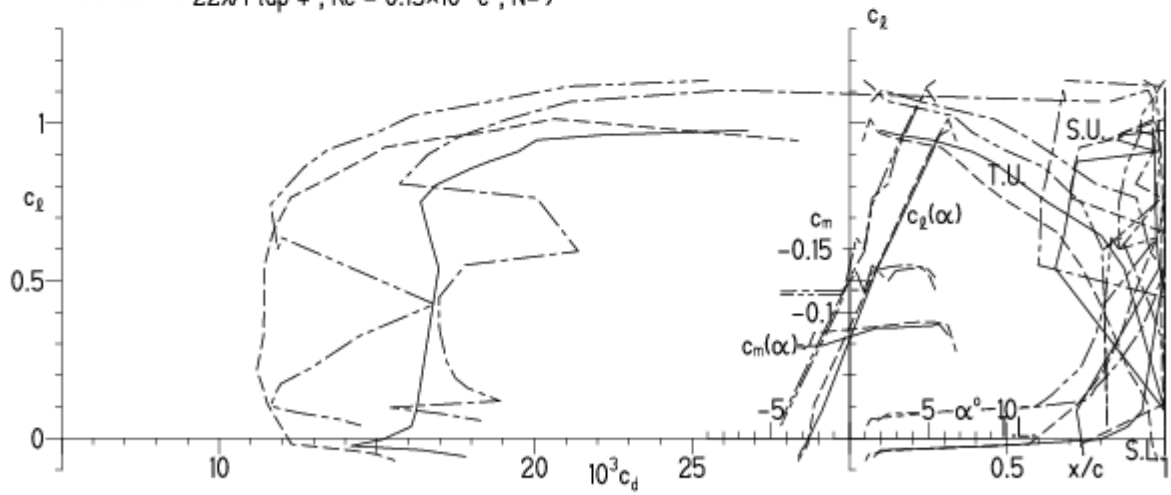


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

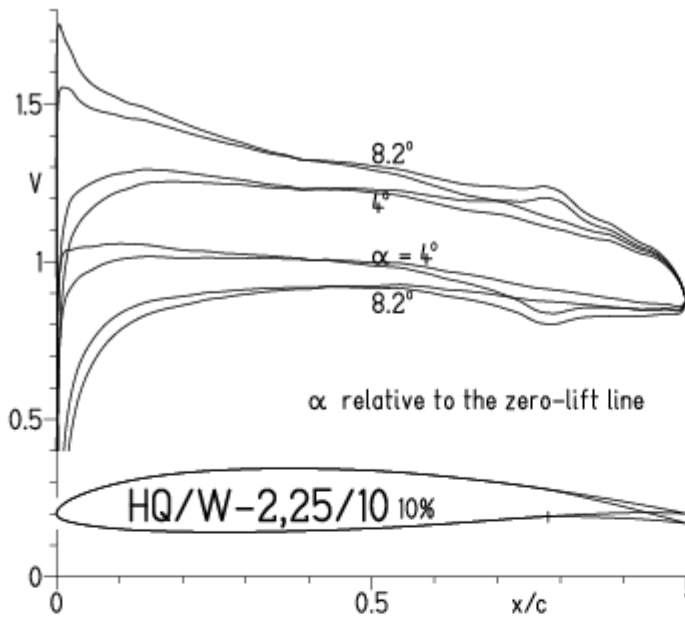
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

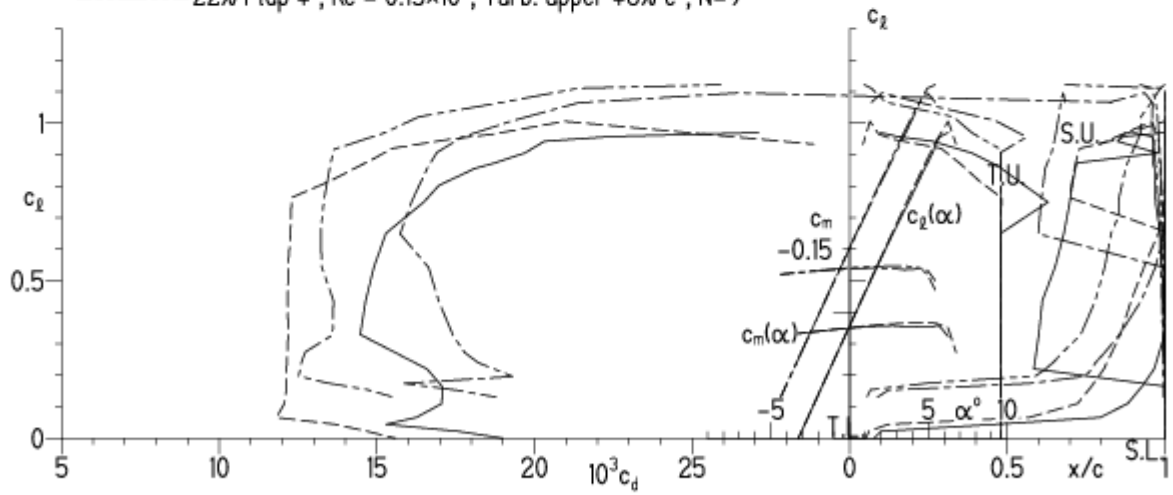


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

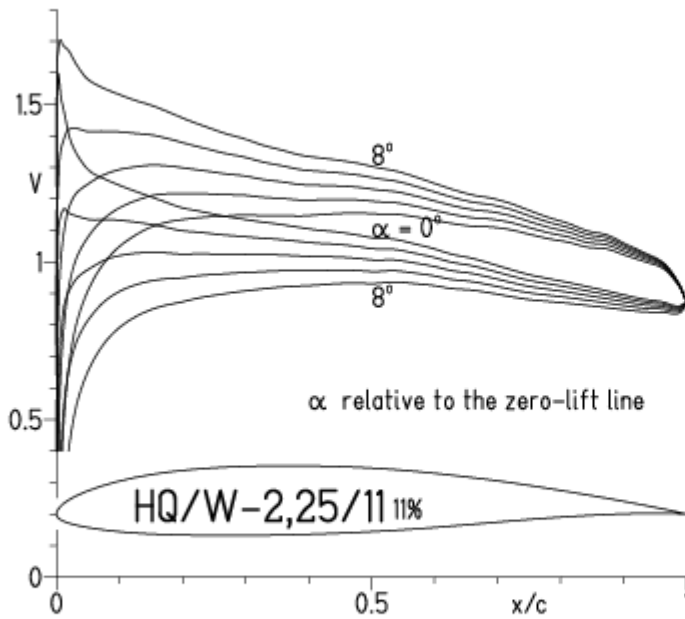


EPPLER 2005 V. 8.5.07 RUN

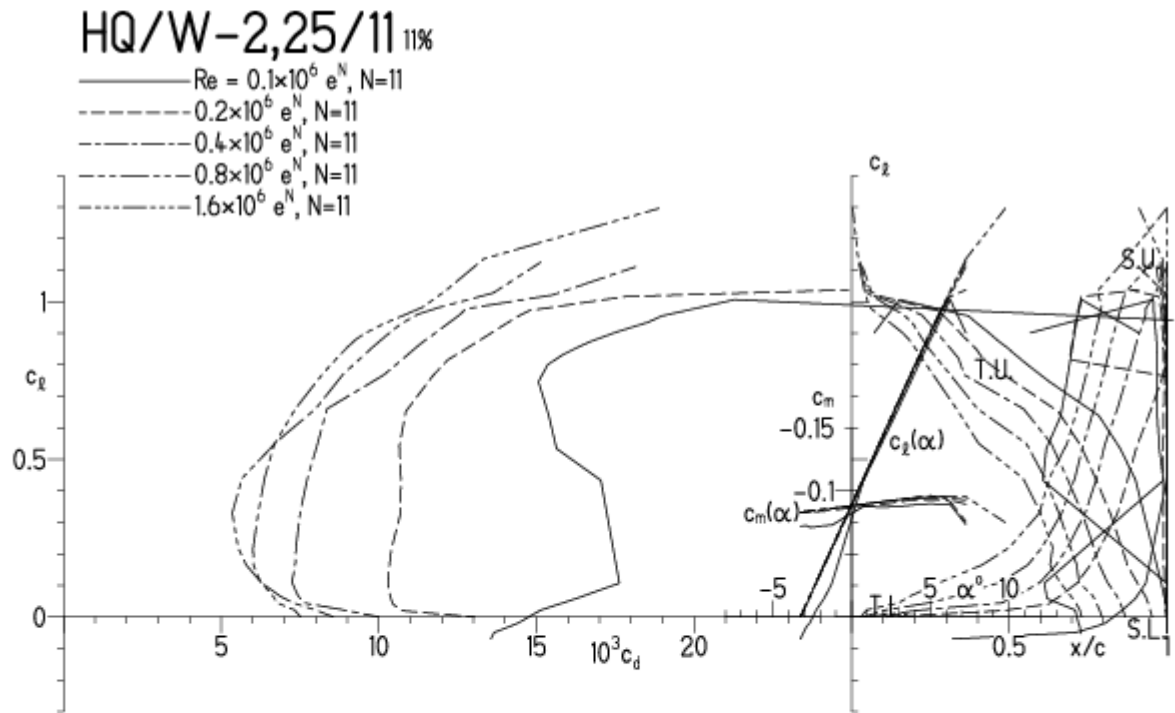


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

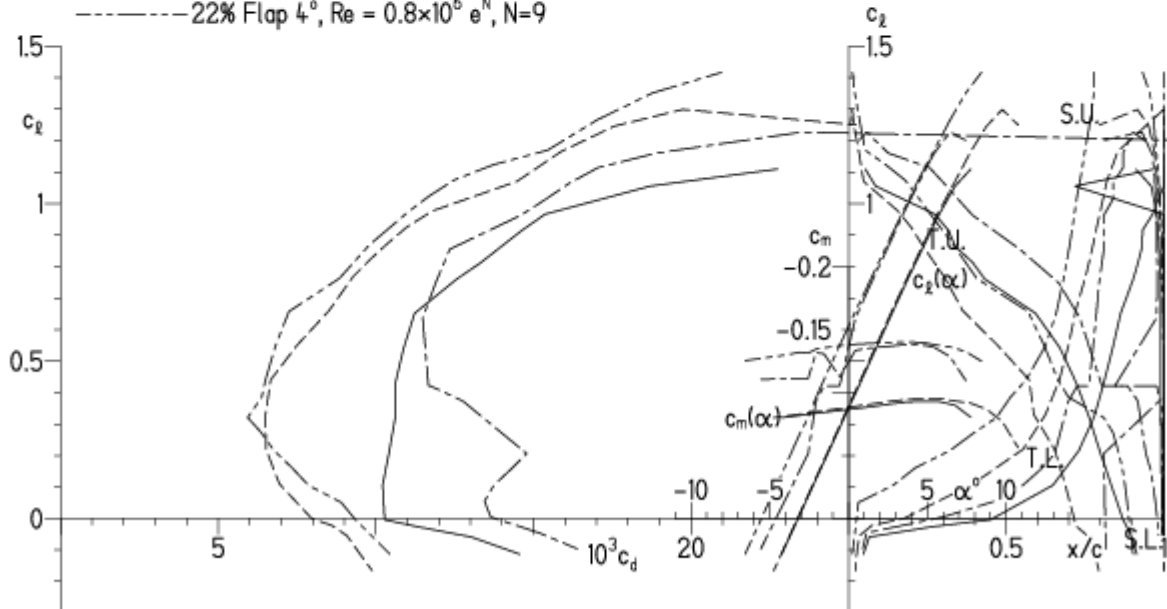


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

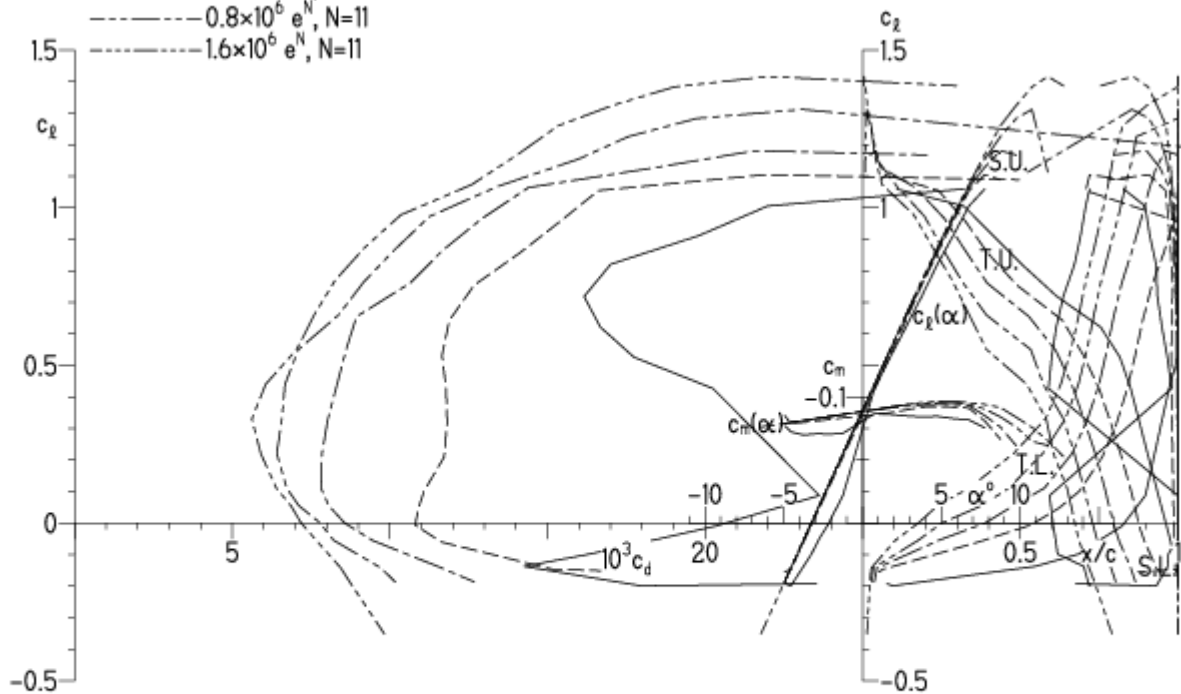
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

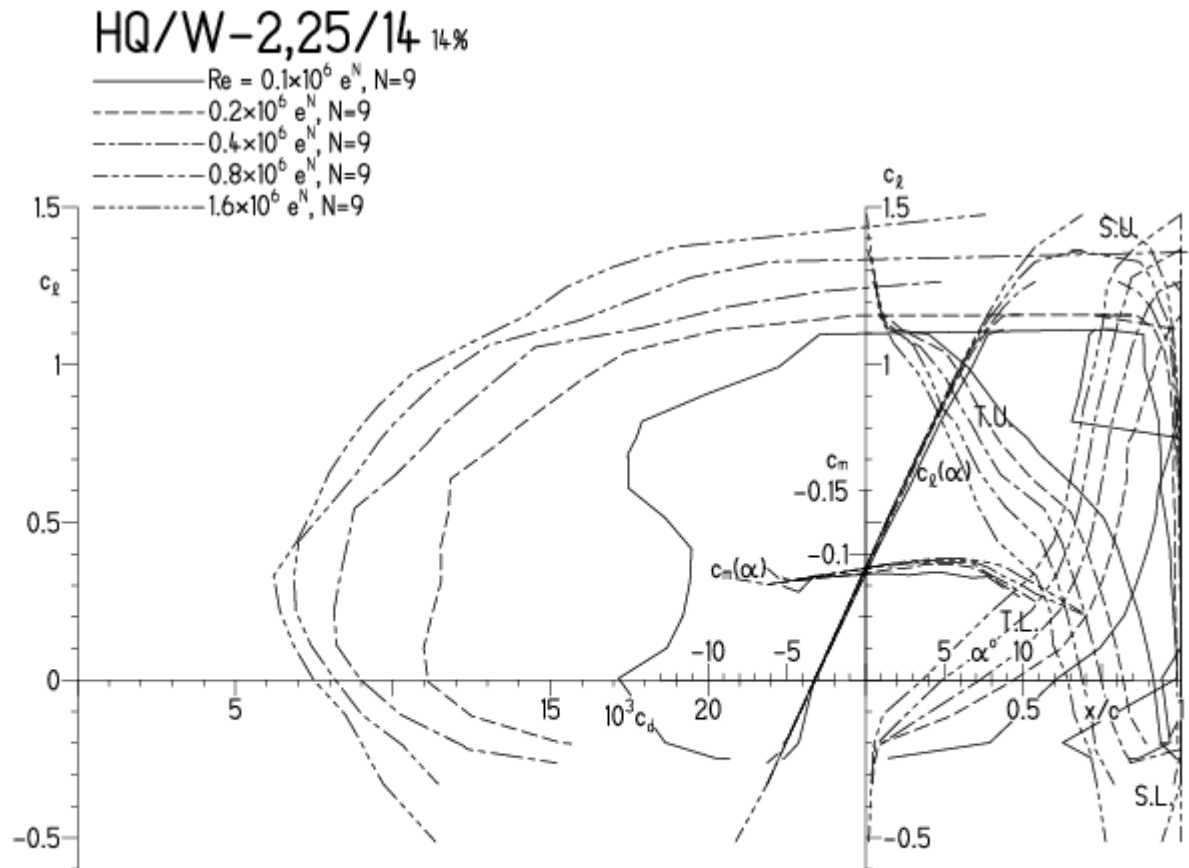


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

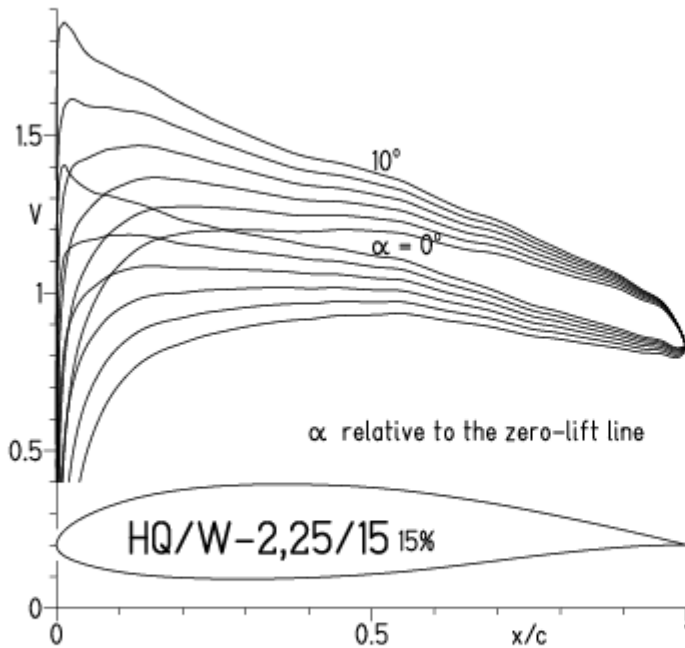


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

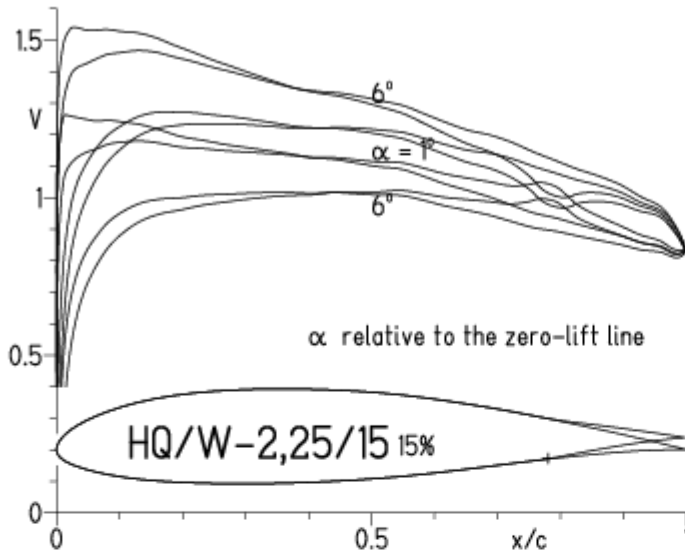


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

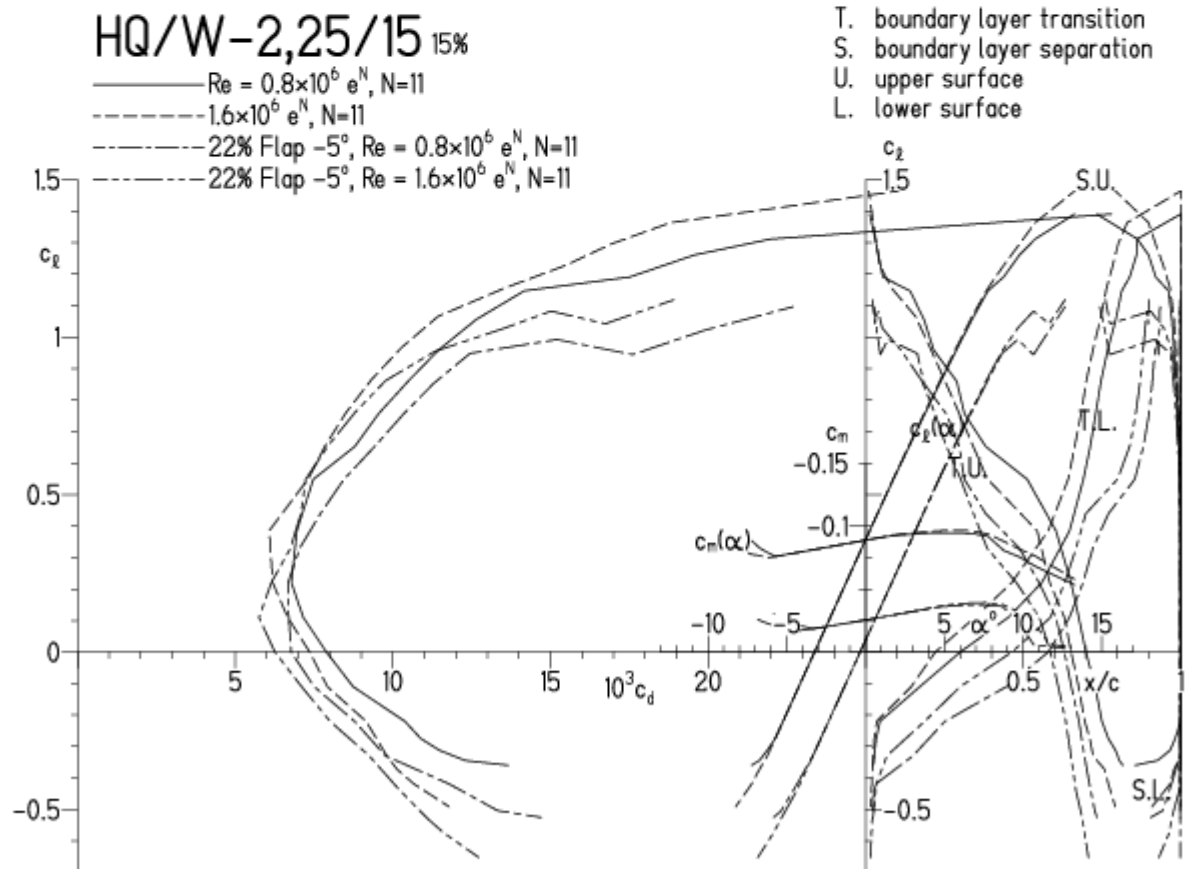
Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04

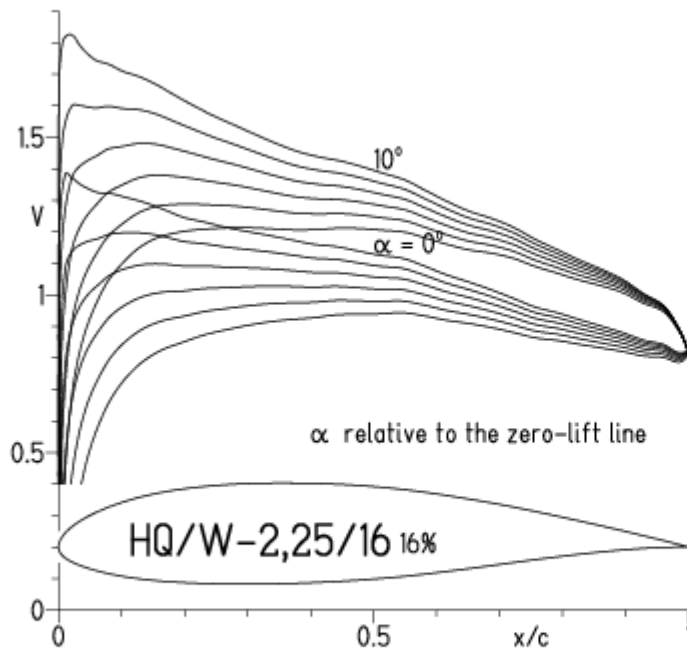


EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



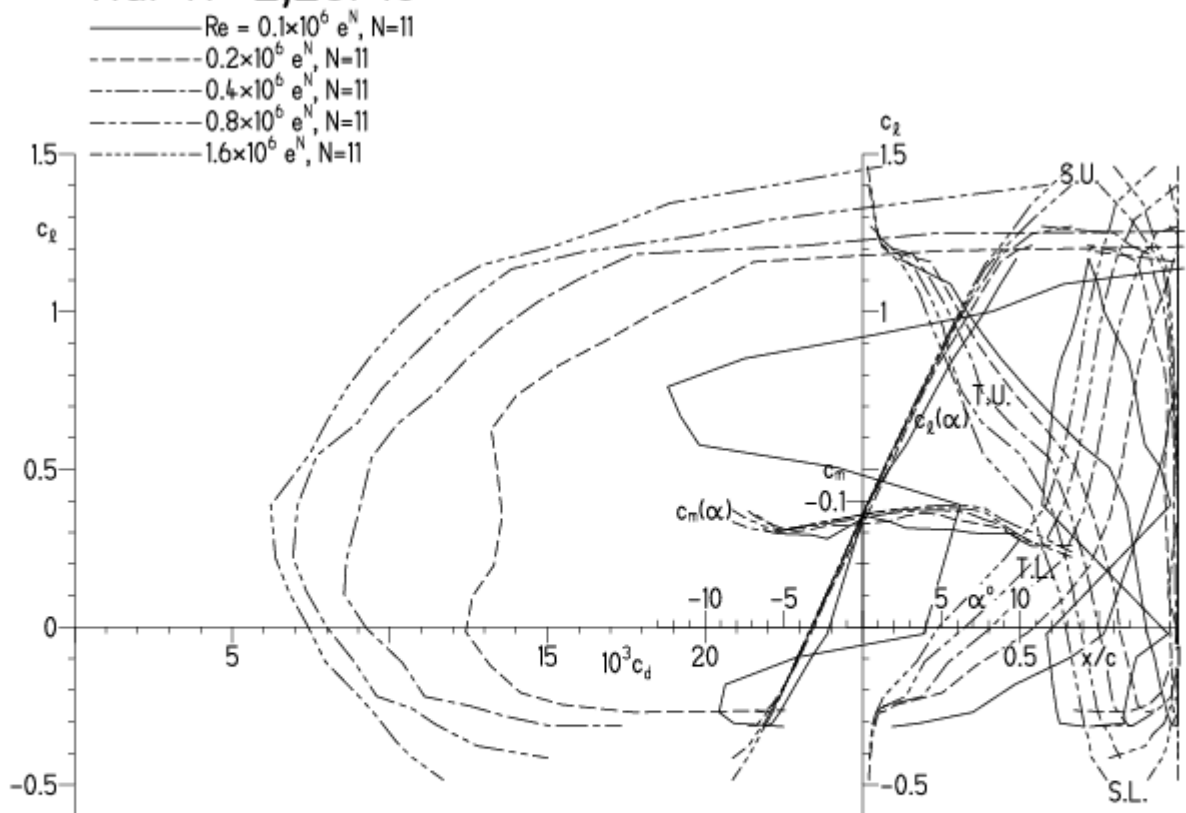
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

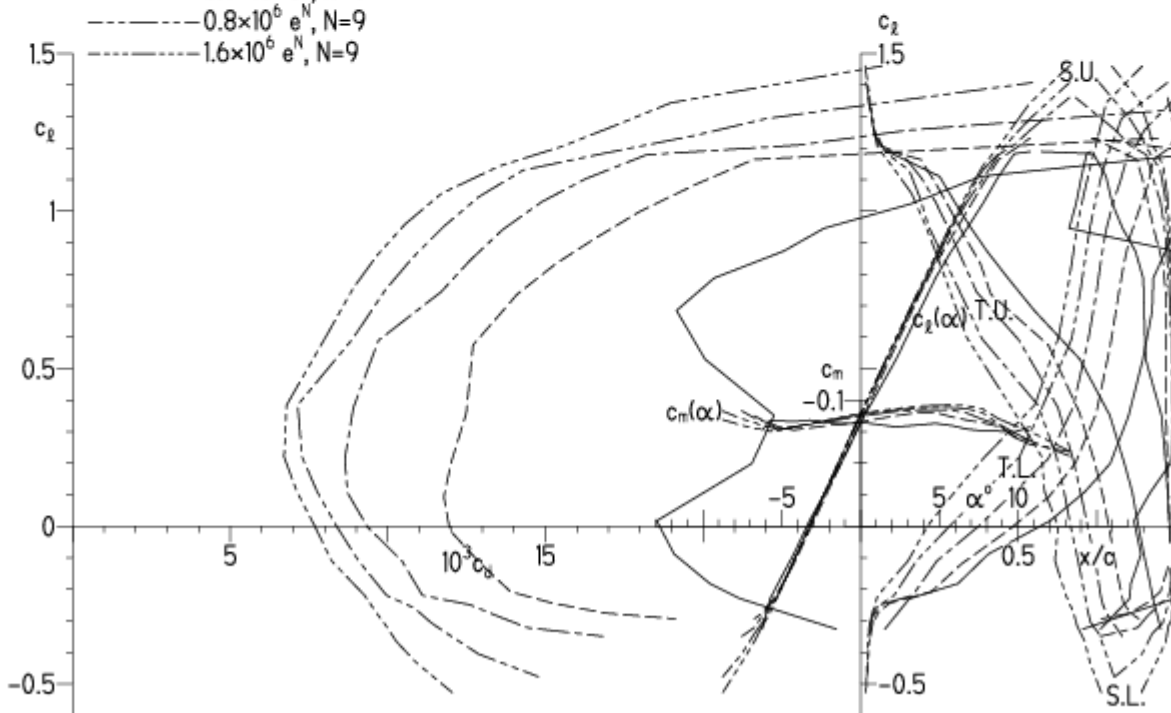
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - · 22% Flap 4°, Re = 75 000 e^N, N=9
- · - · 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2,25/8,5 8.5%



HQ/W-2,25/8,5, N=9

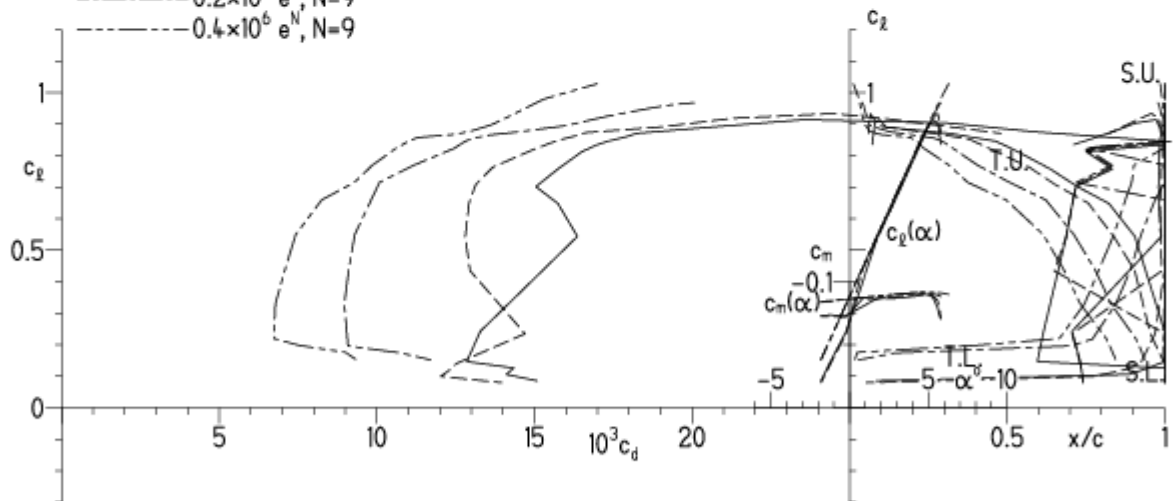
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

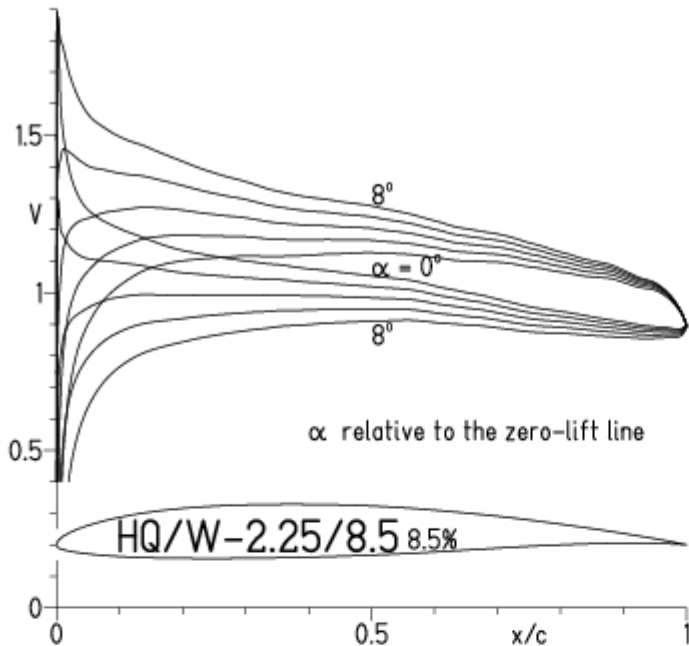
HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

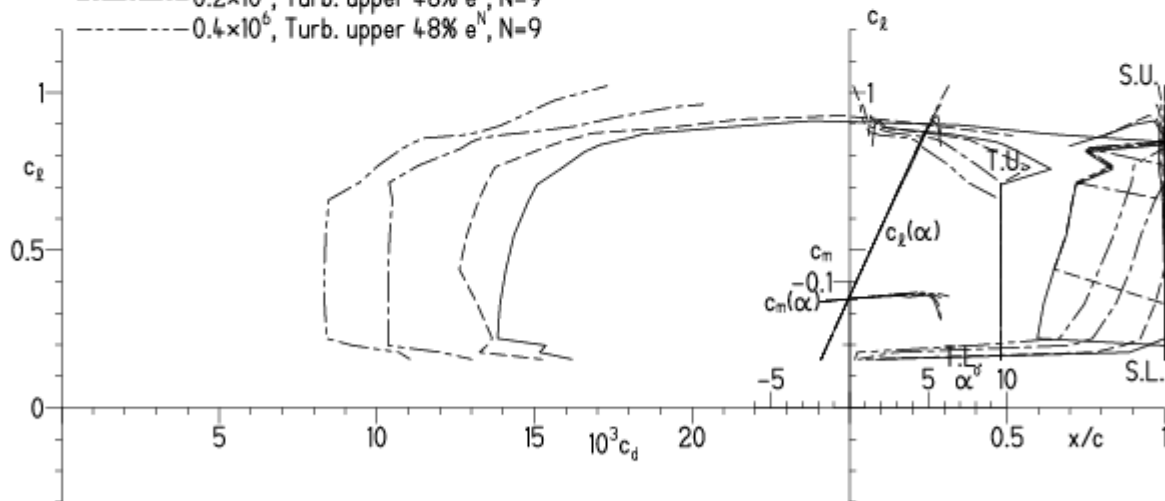
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

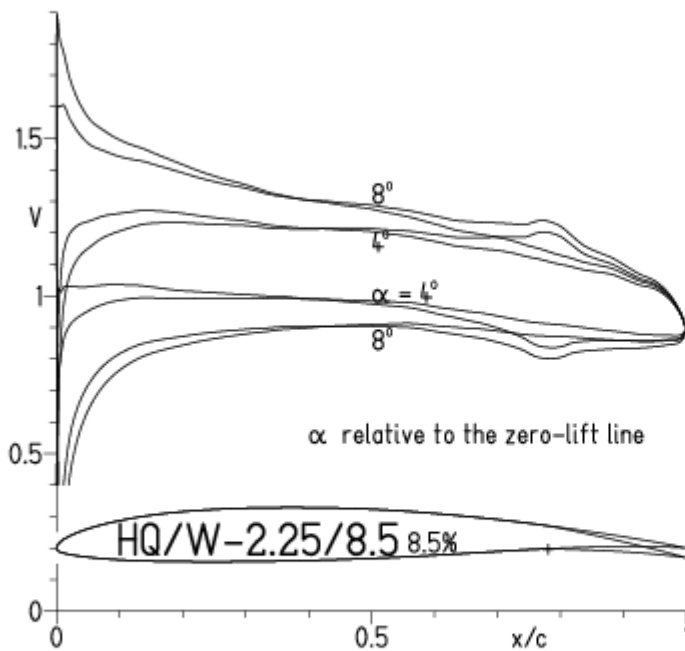
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

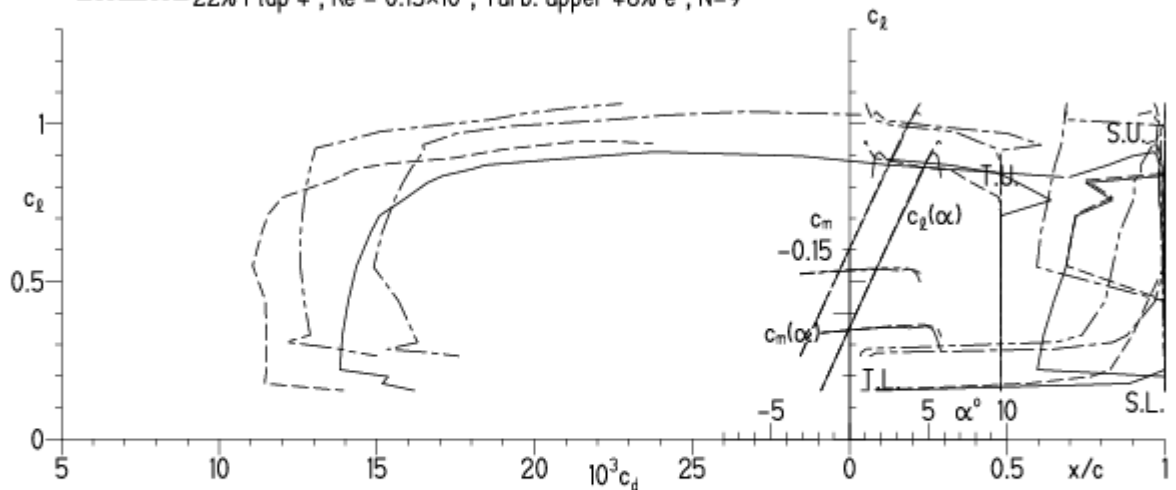


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

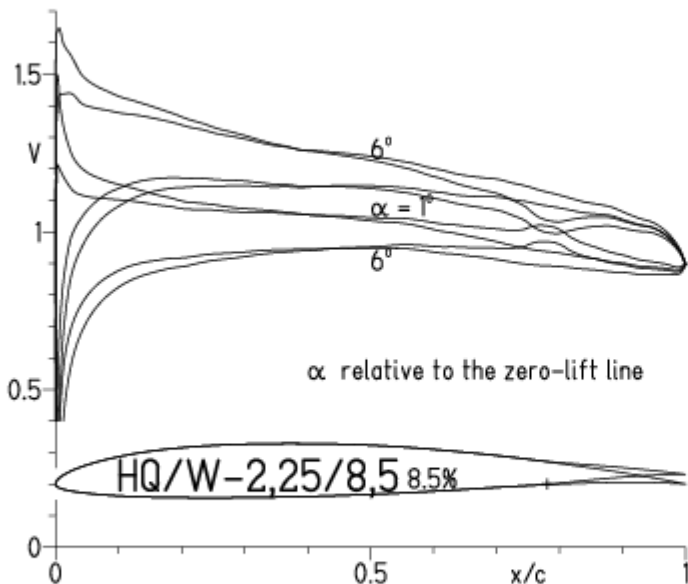
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



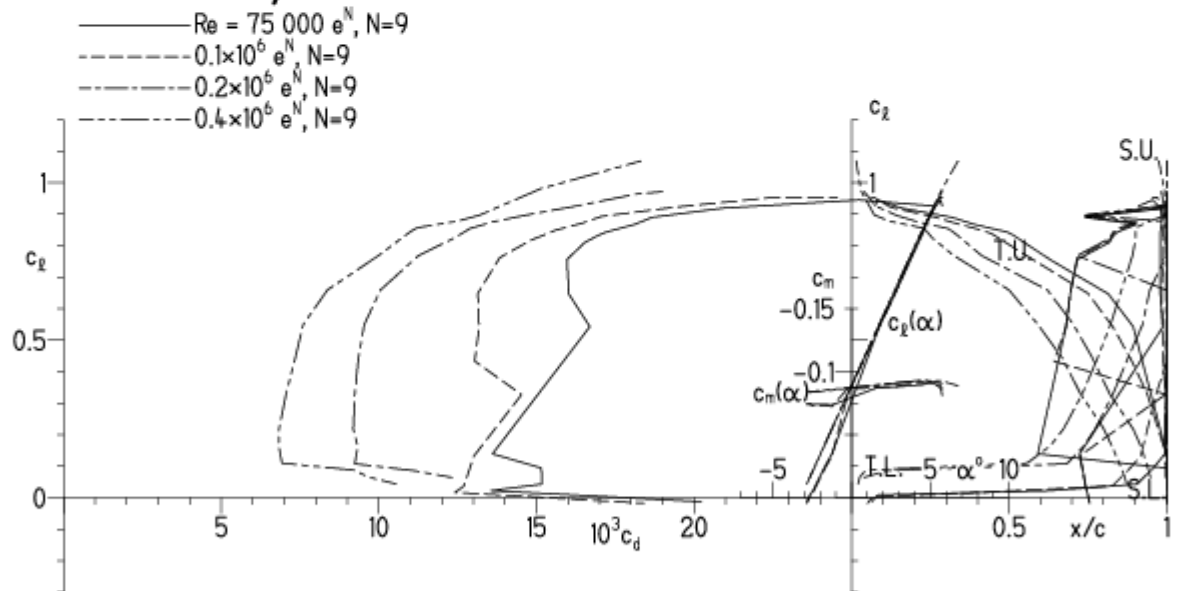
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$

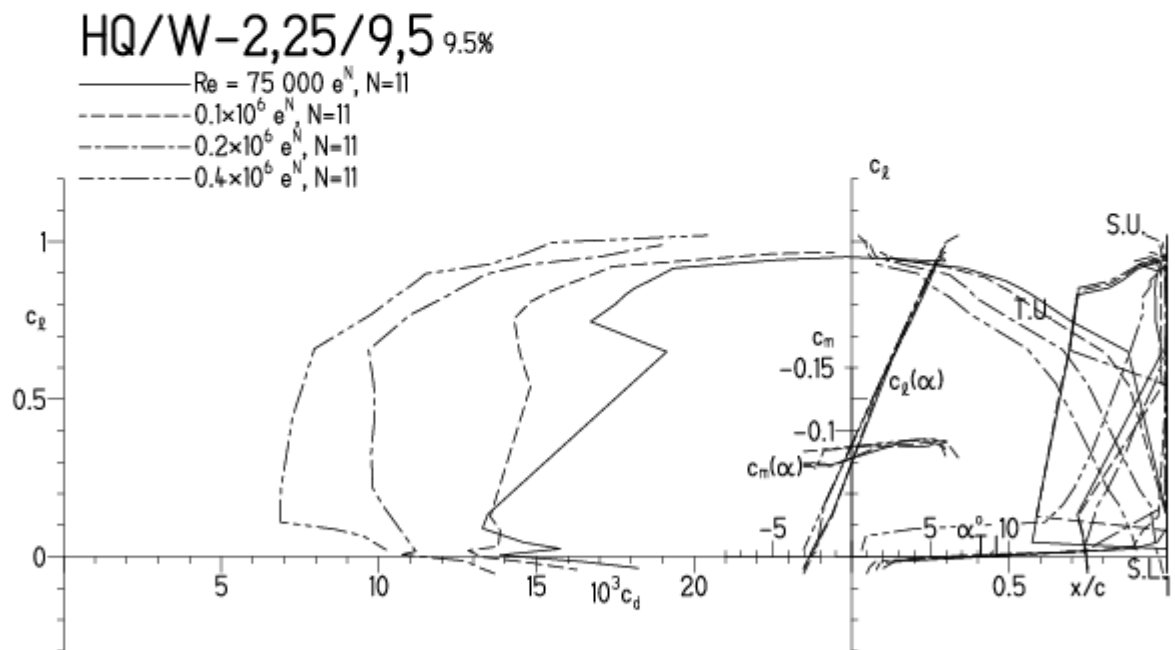


HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

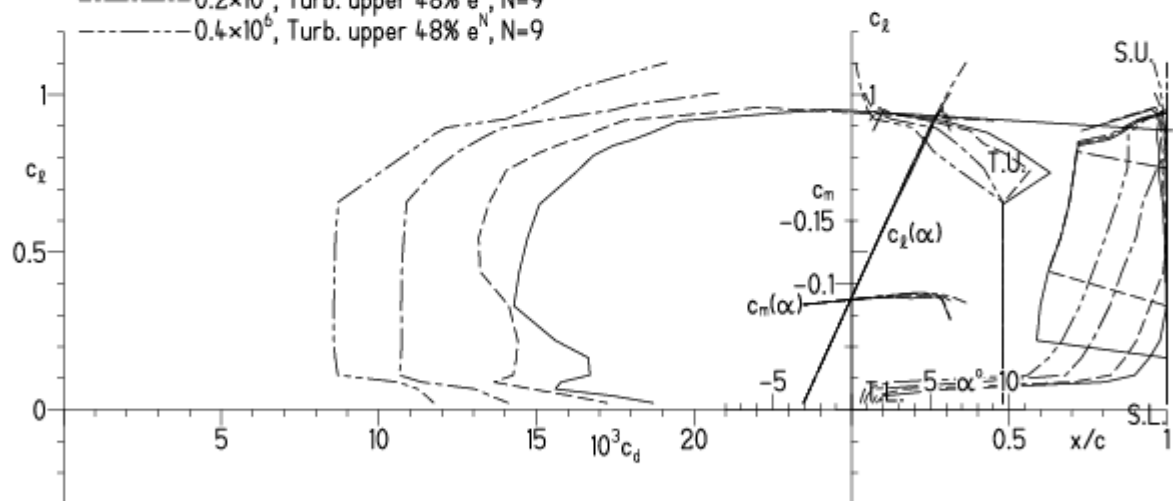
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

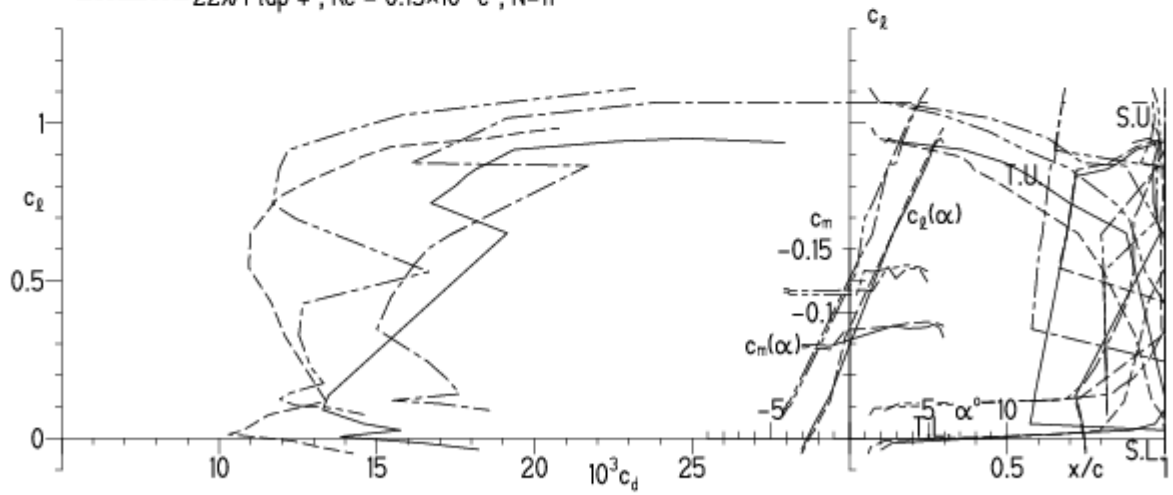


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



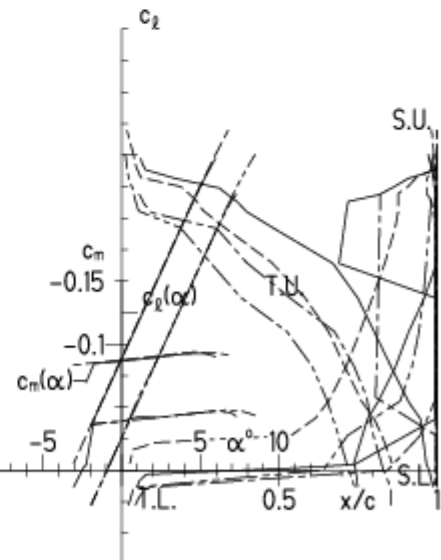
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

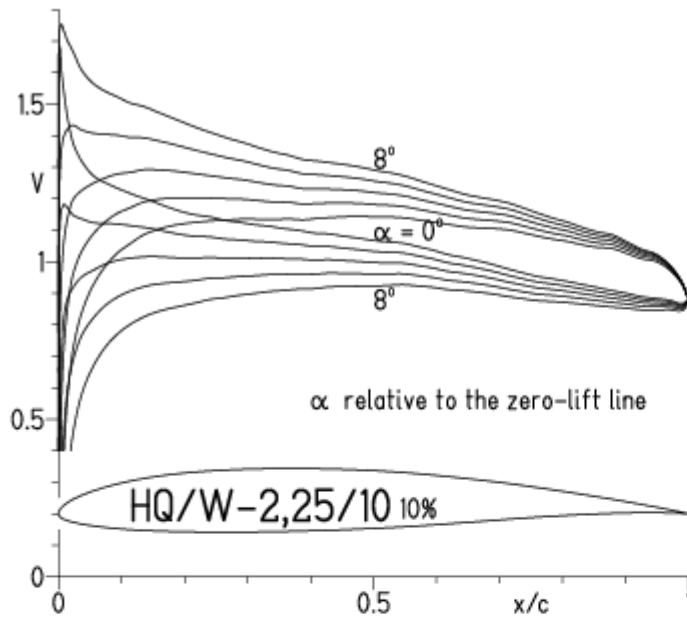


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

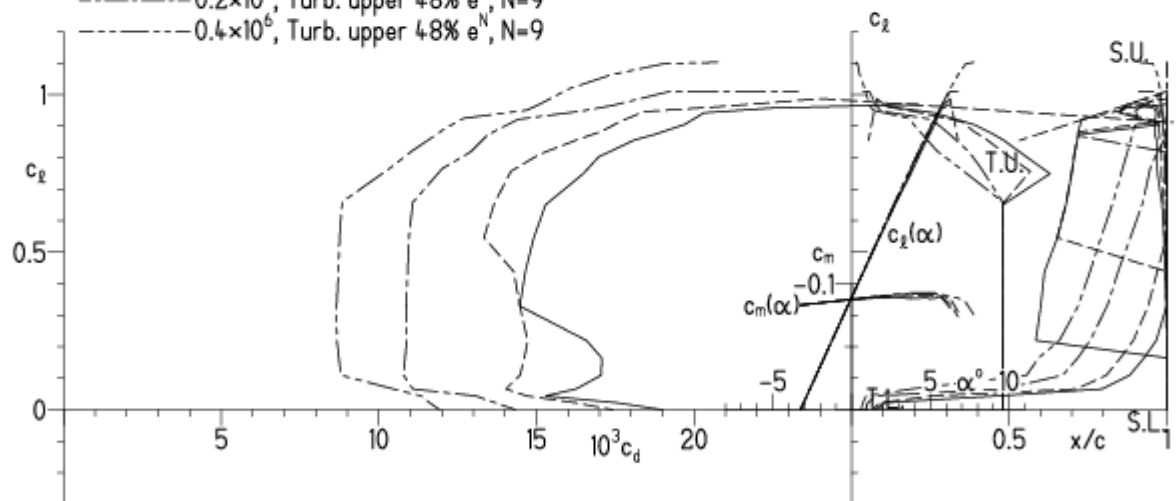
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

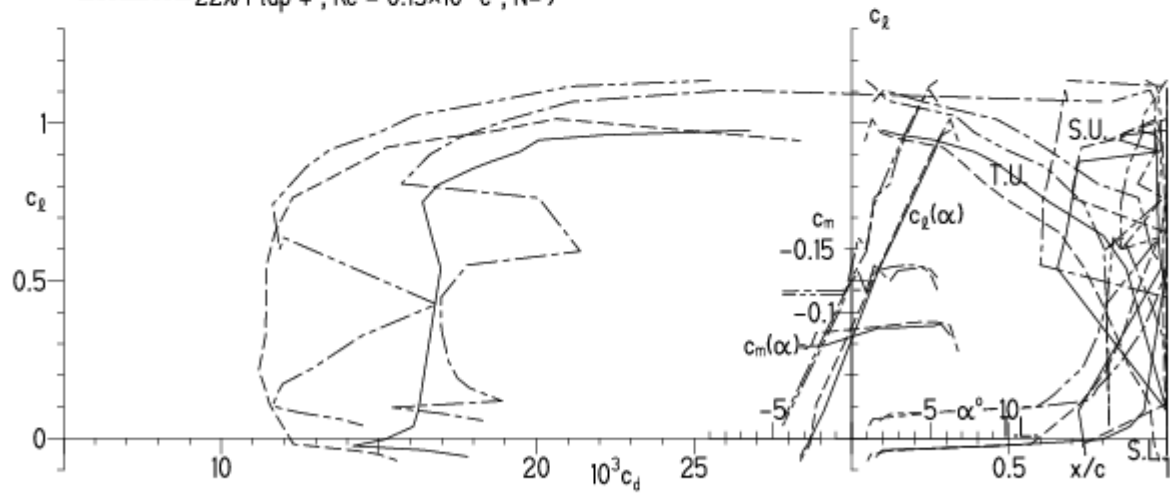


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

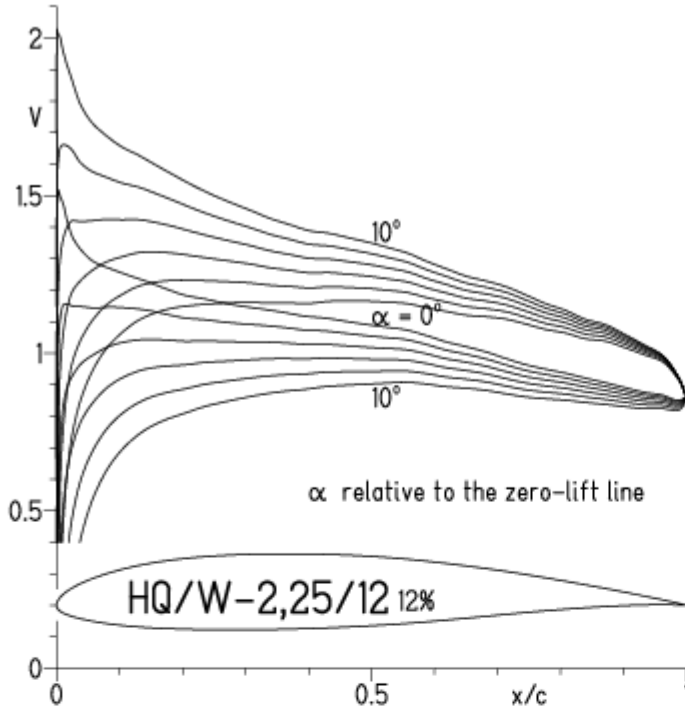
HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

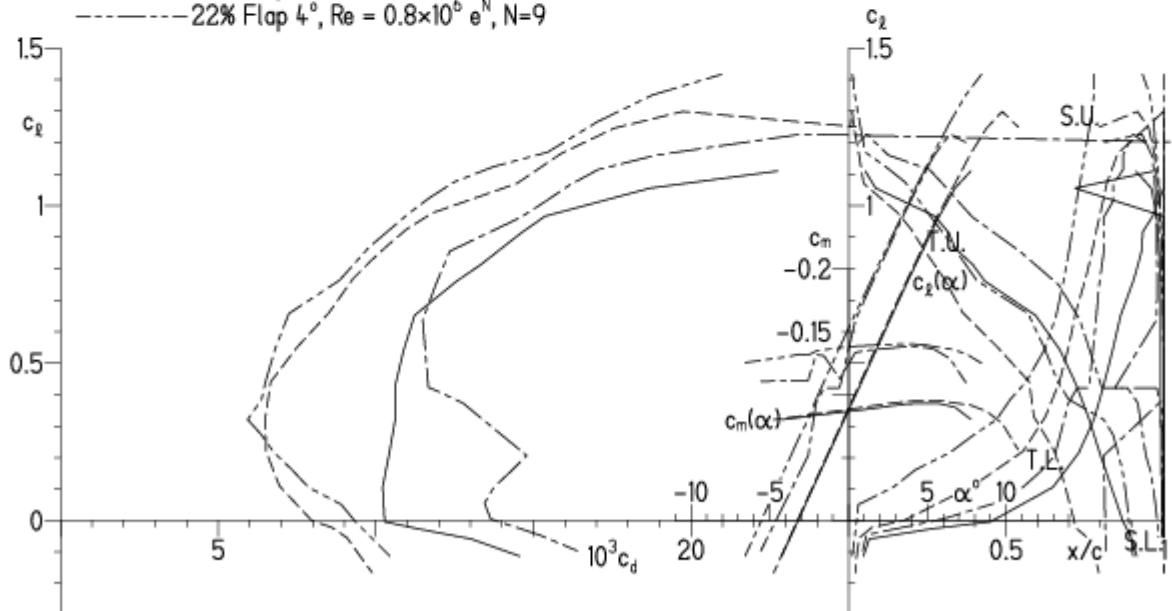


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

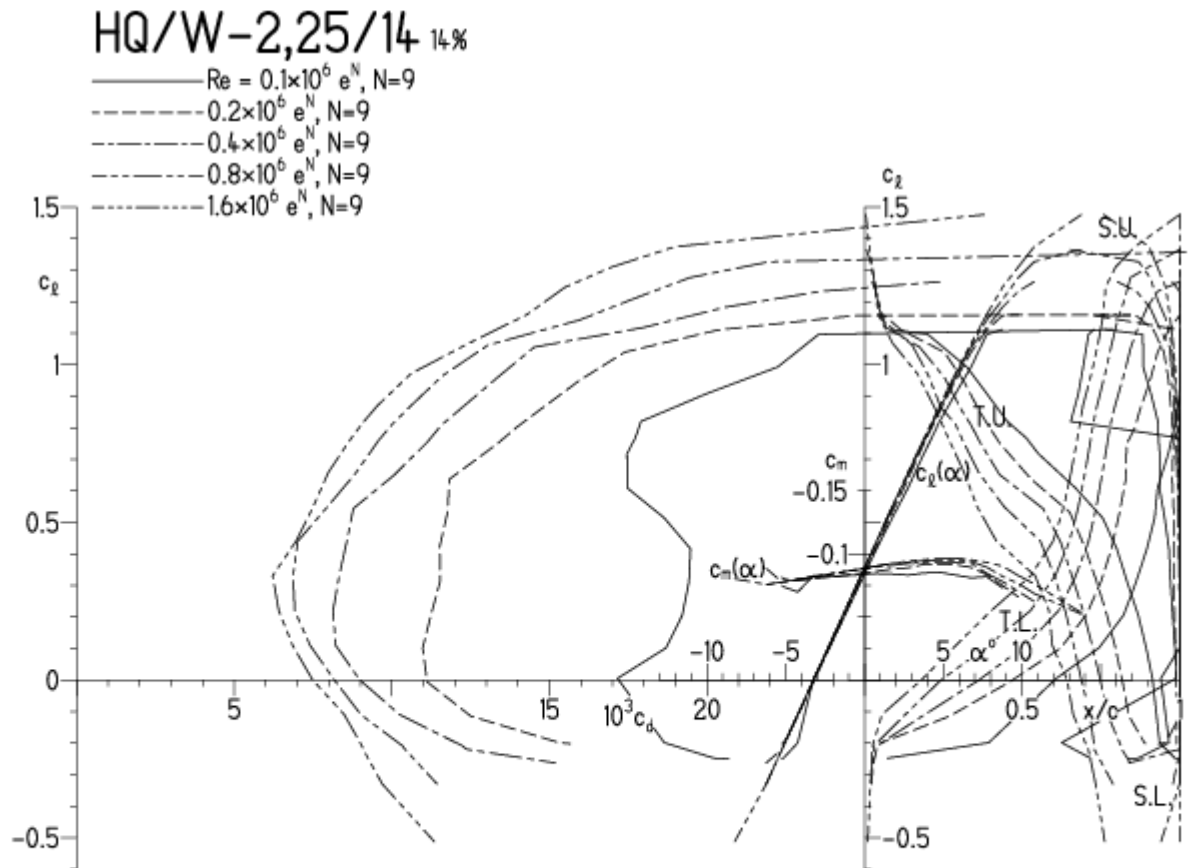


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

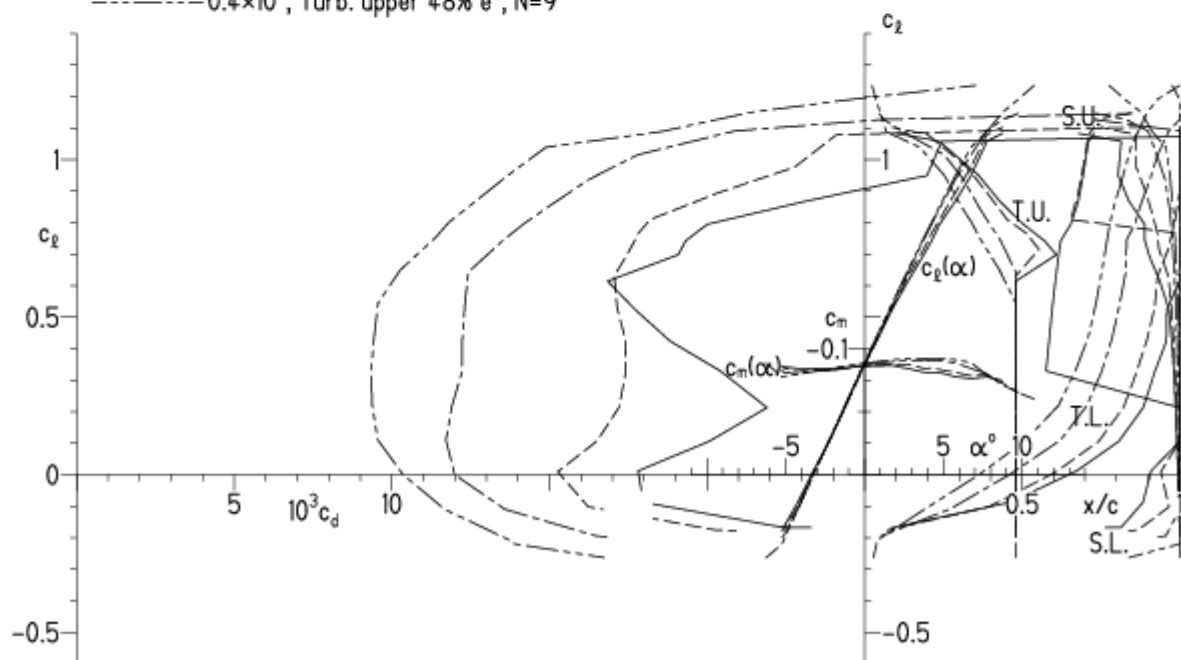
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

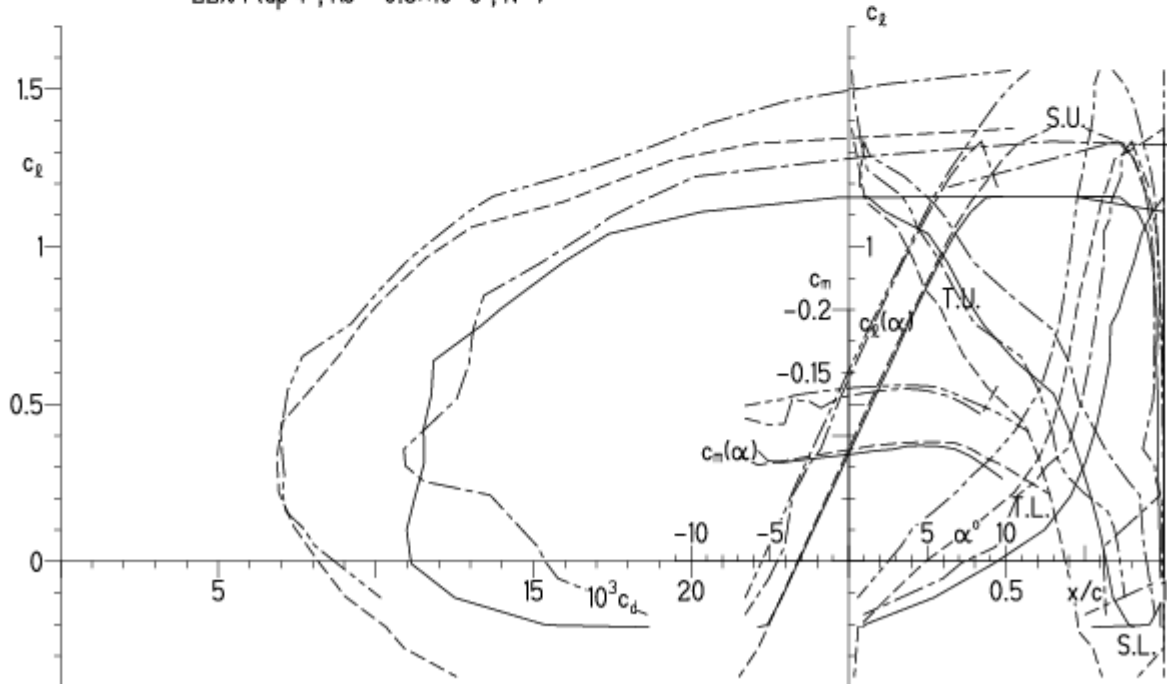


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

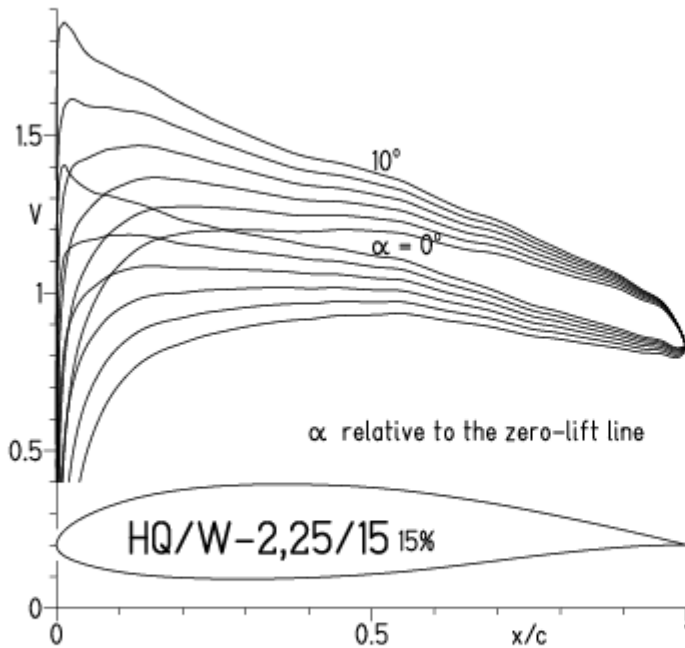


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

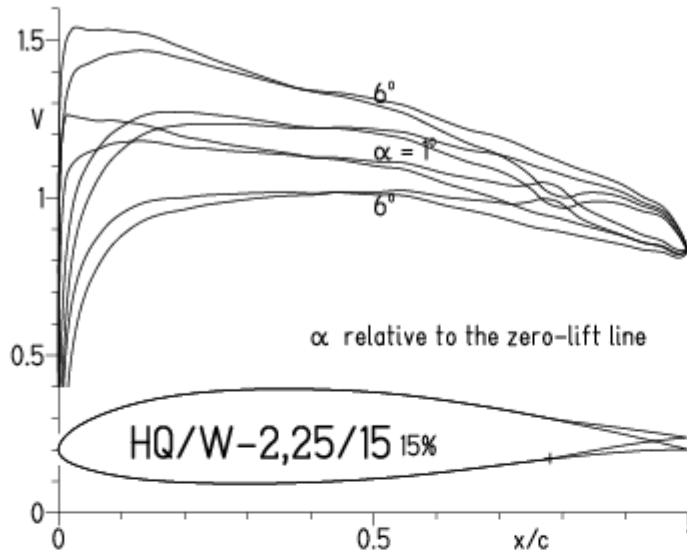


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

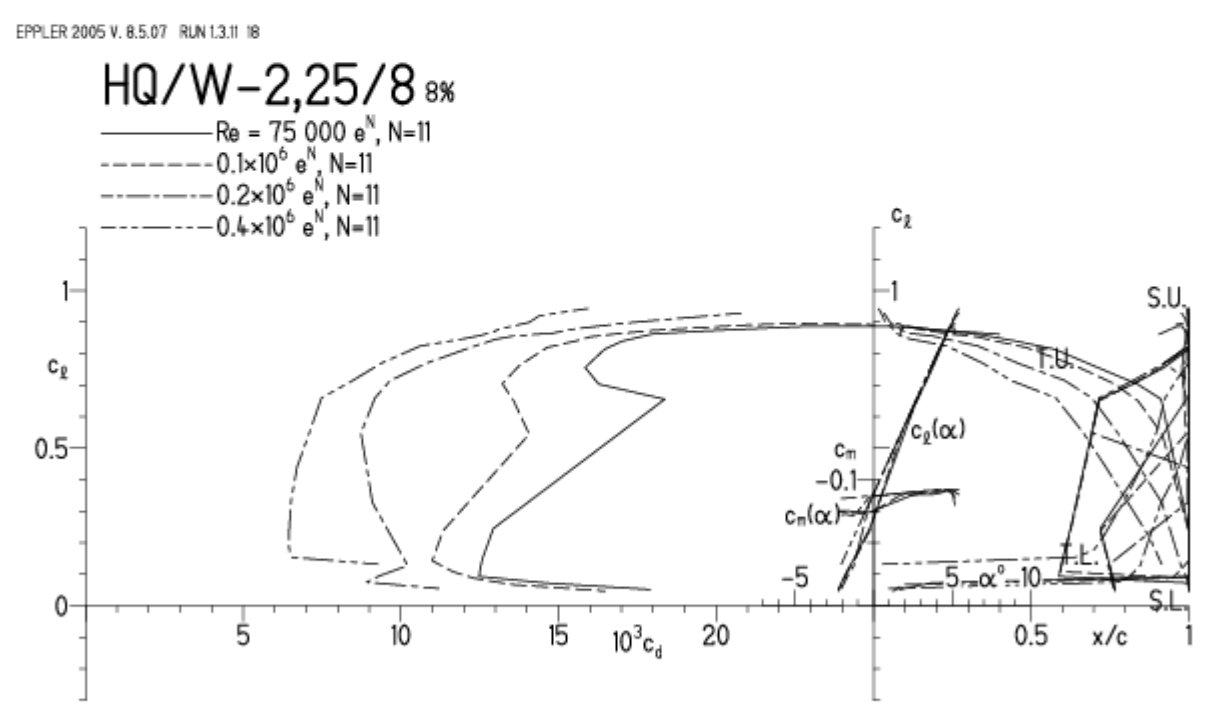
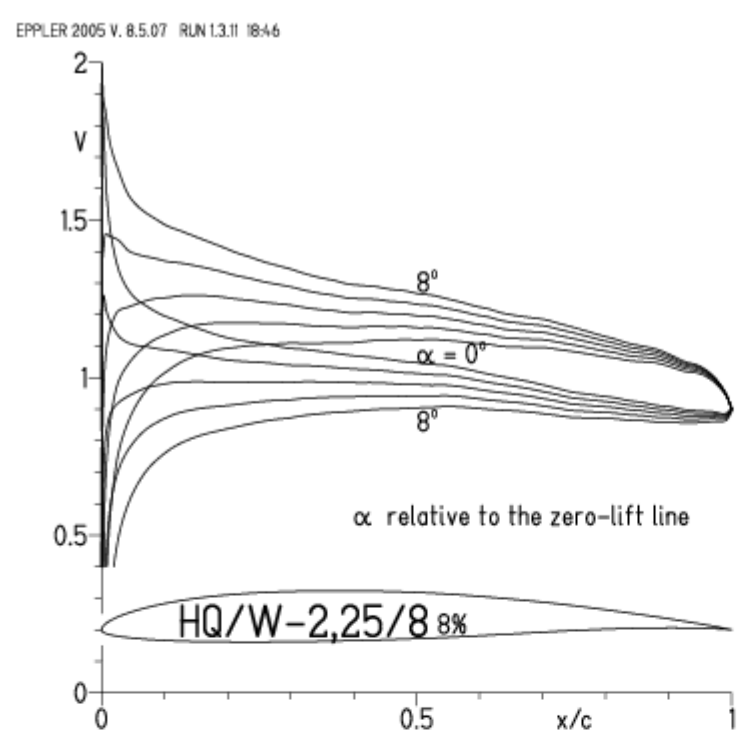
EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

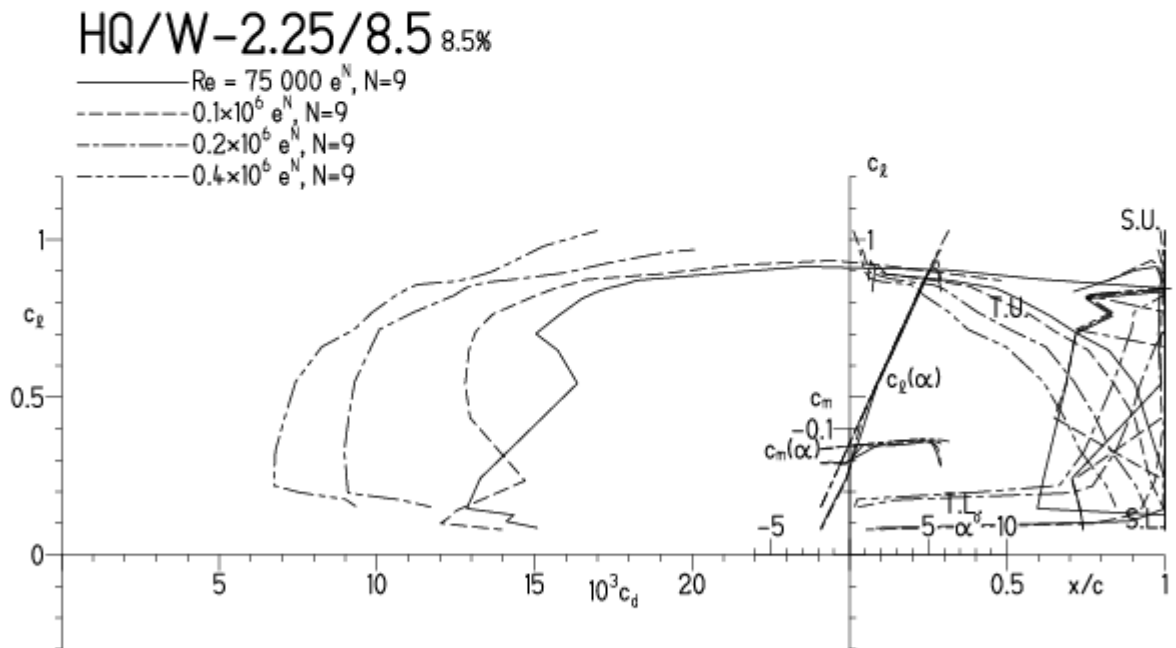


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

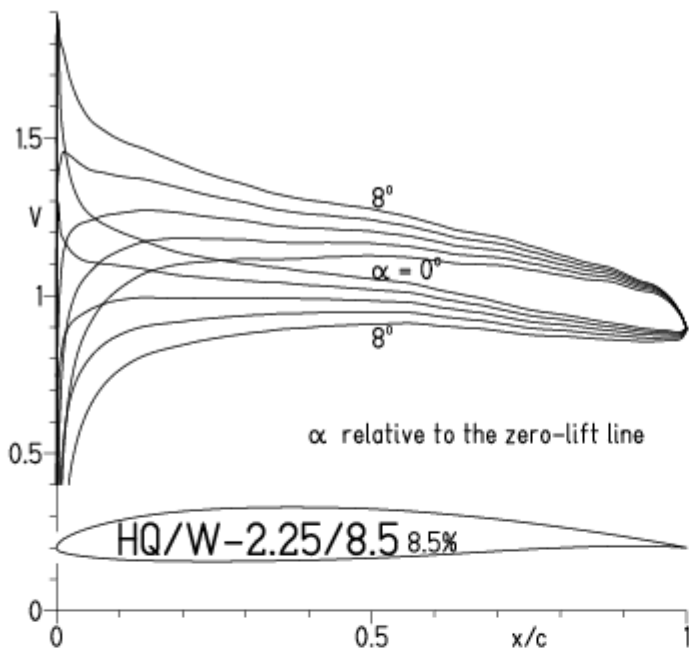


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

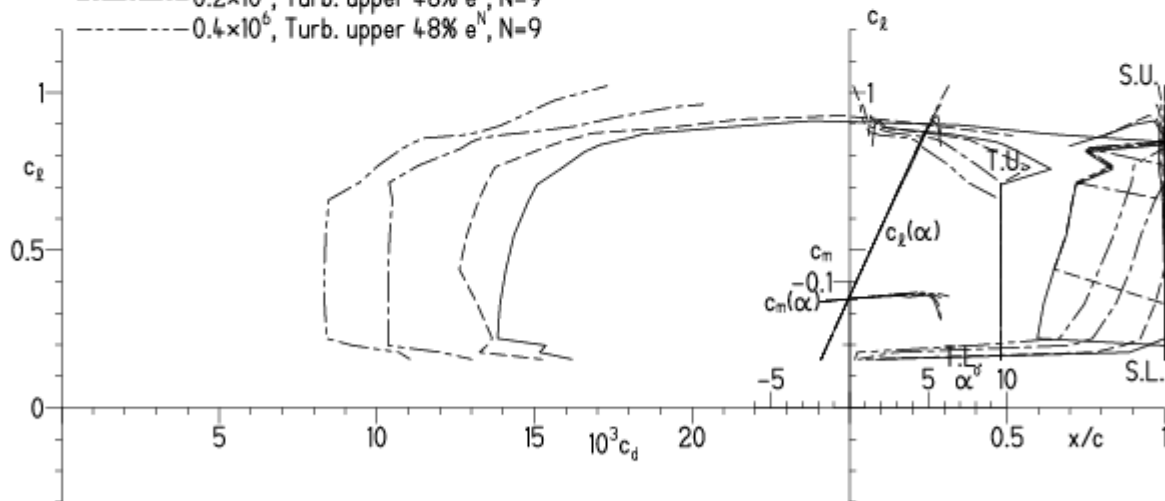
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

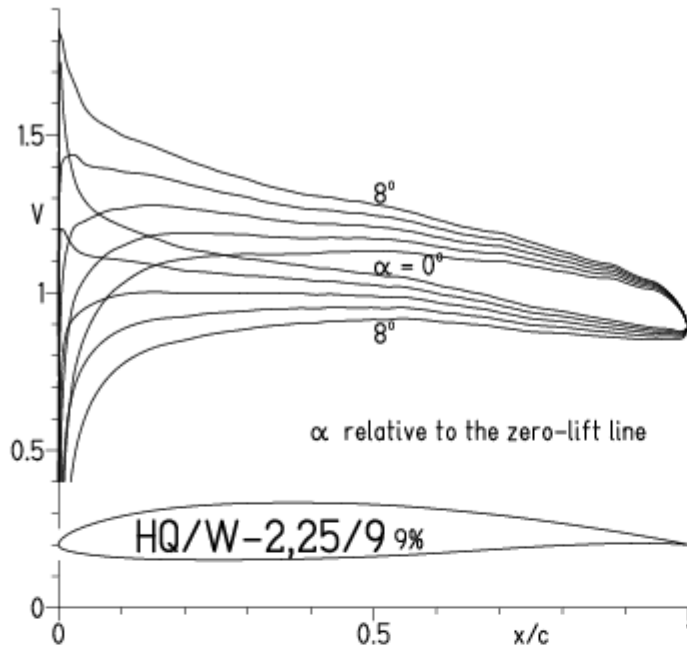


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

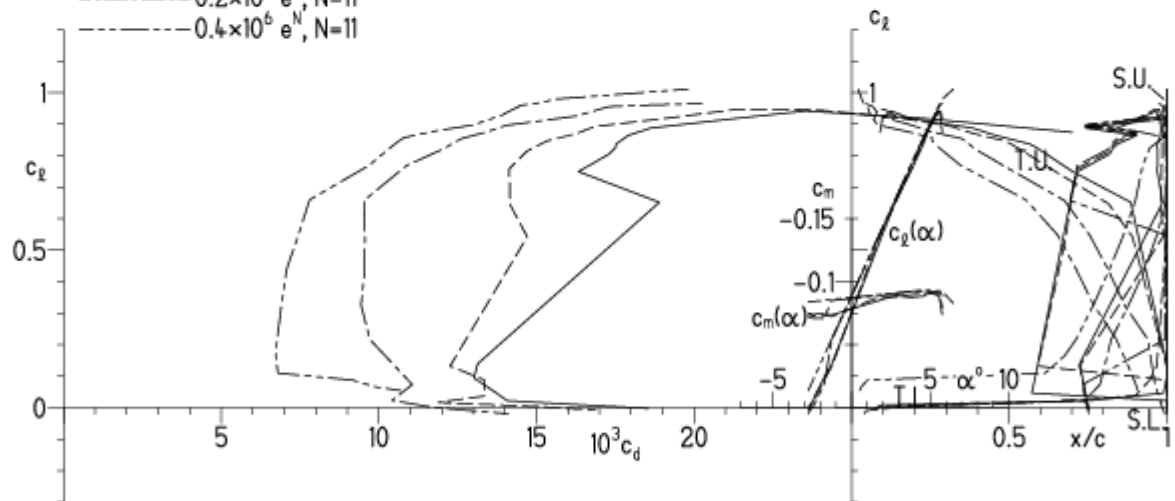
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

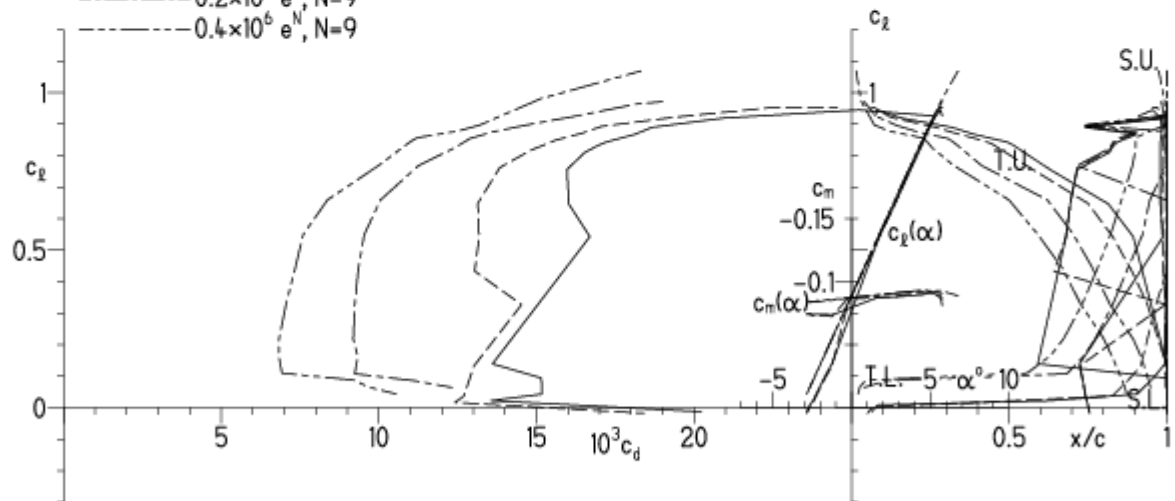
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

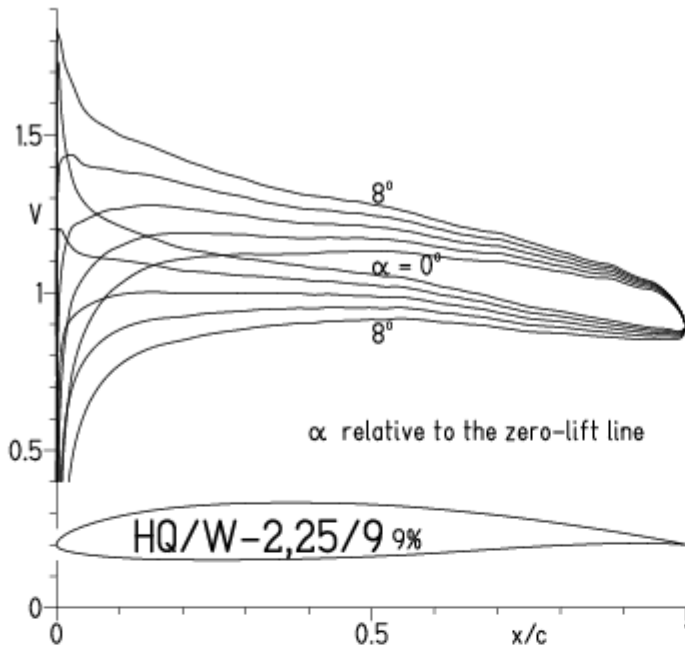
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

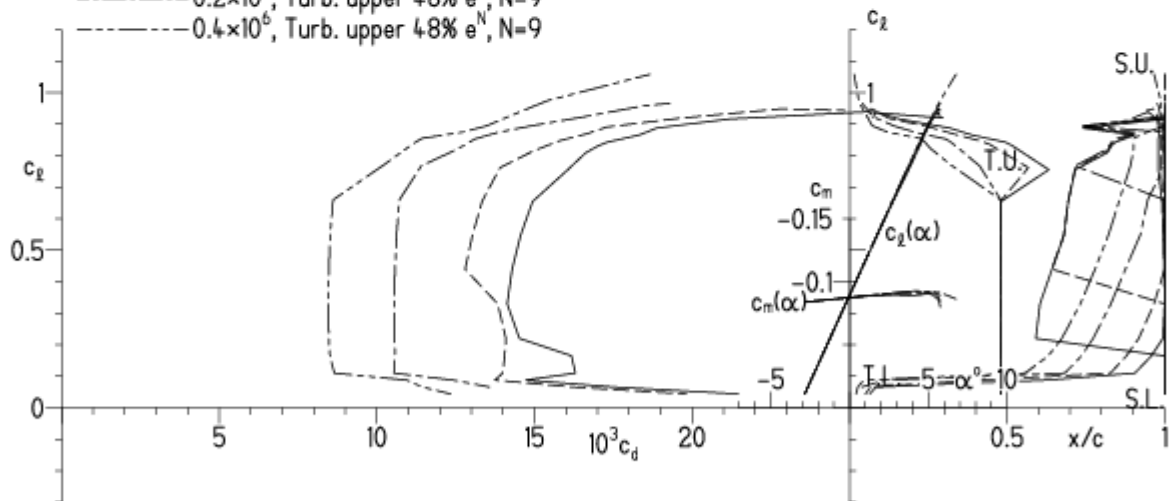
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

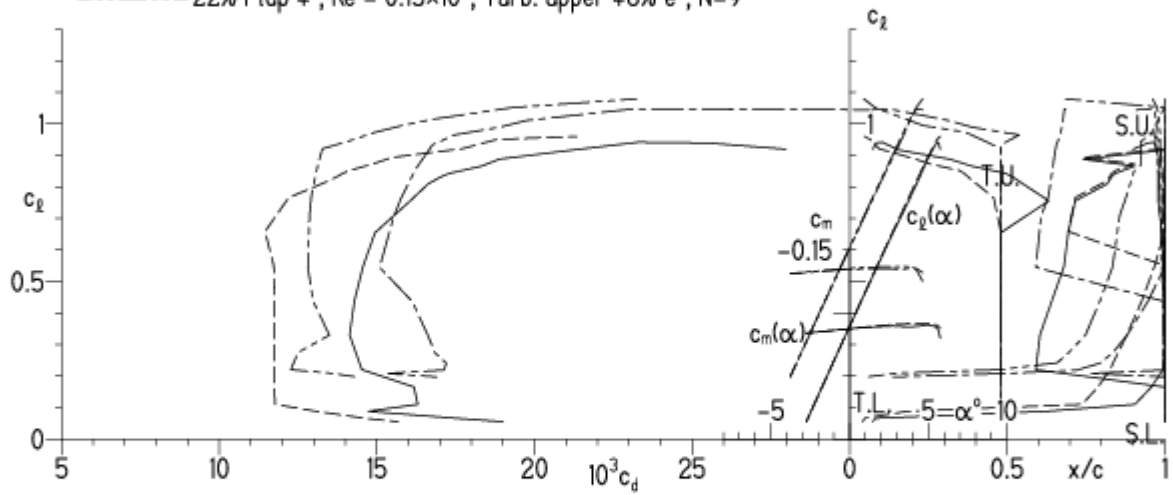


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

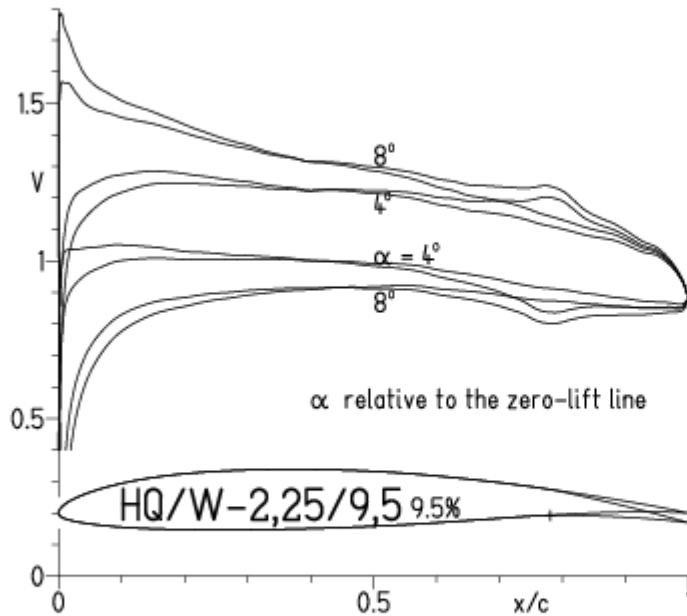
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

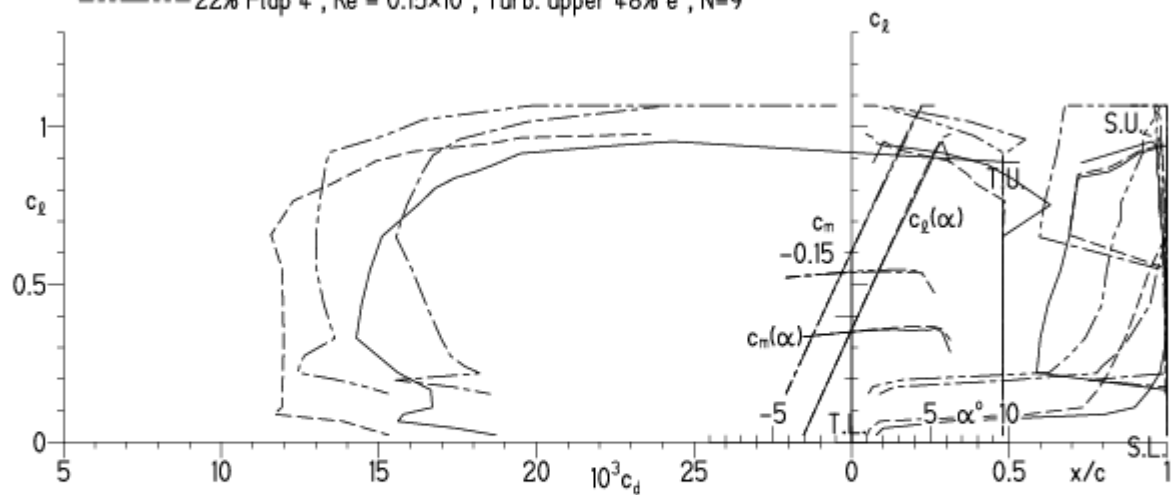


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



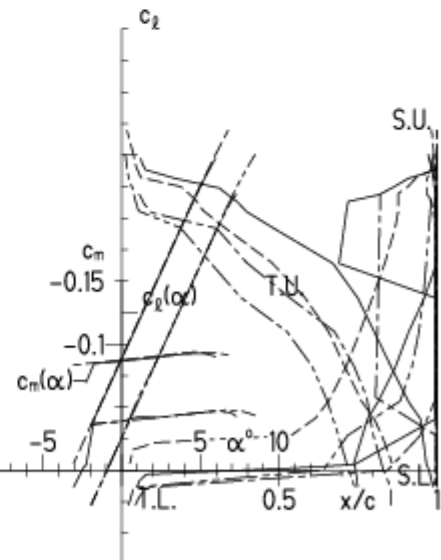
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

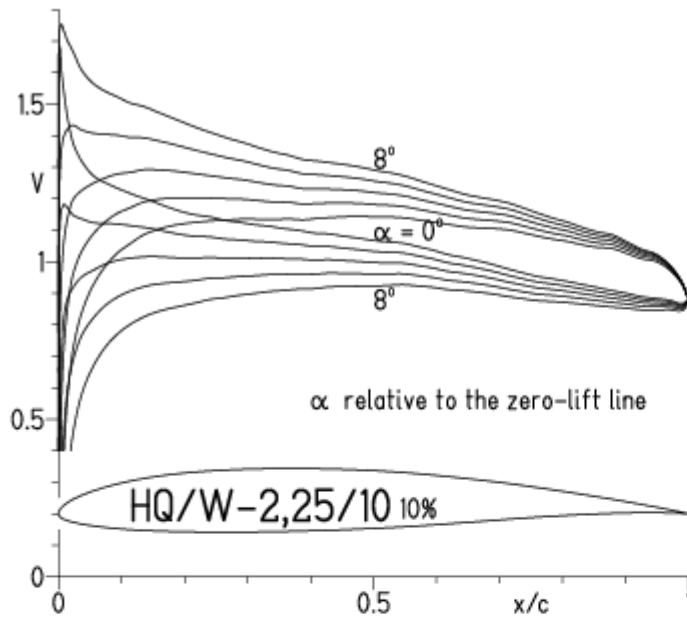


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

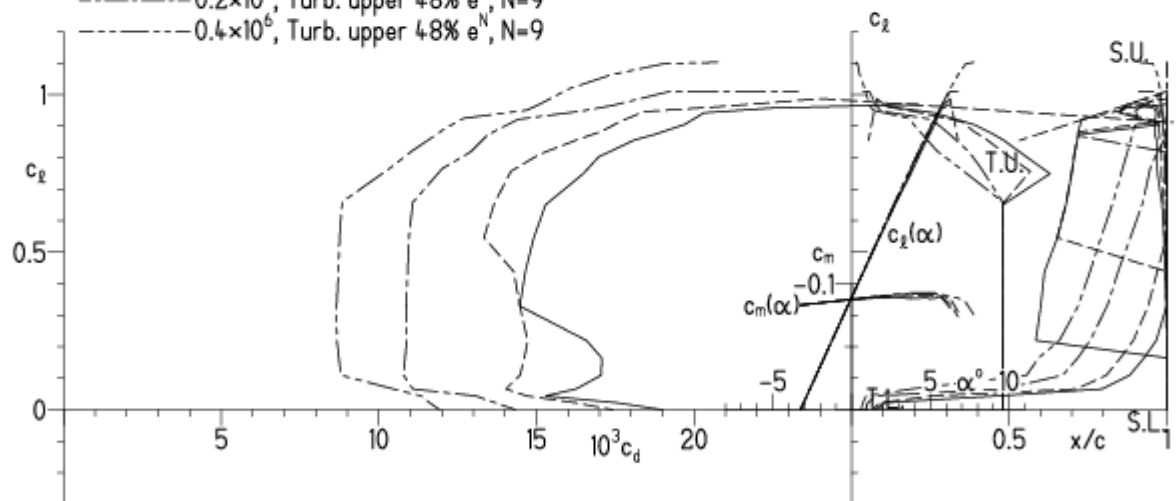
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

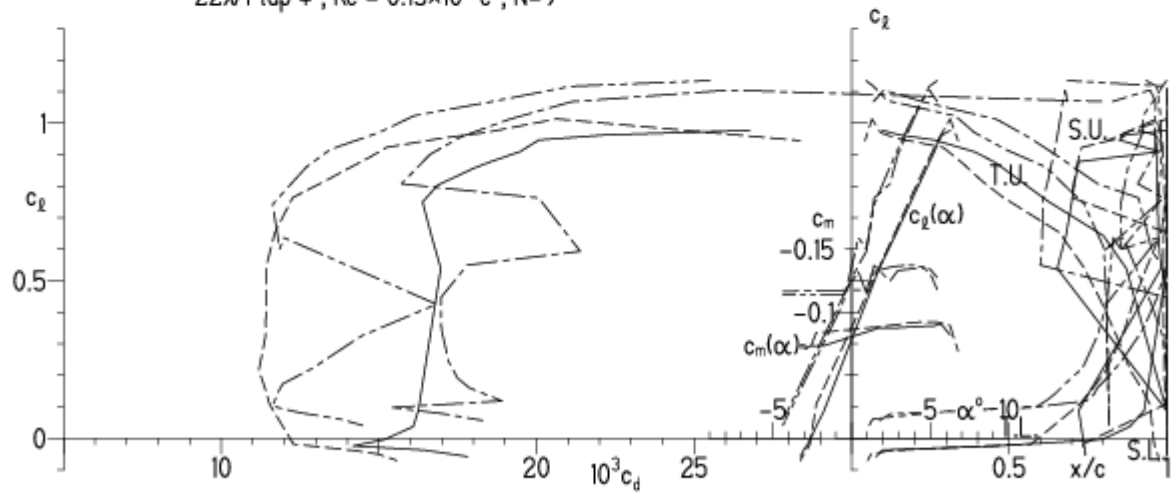


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

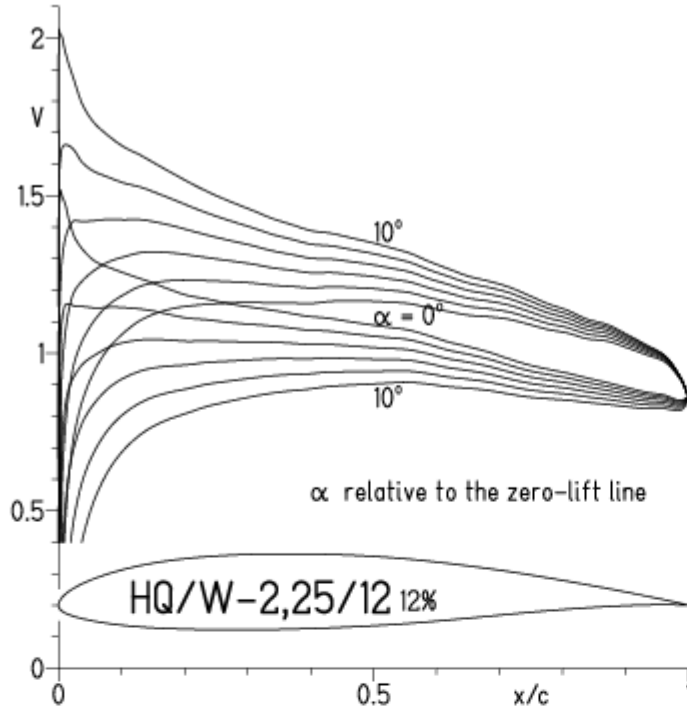
HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- Re = 0.2×10^6 e^N, N=9
- - - 0.8×10^6 e^N, N=9
- · - · 22% Flap 4°, Re = 0.2×10^6 e^N, N=9
- · - · 22% Flap 4°, Re = 0.8×10^6 e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

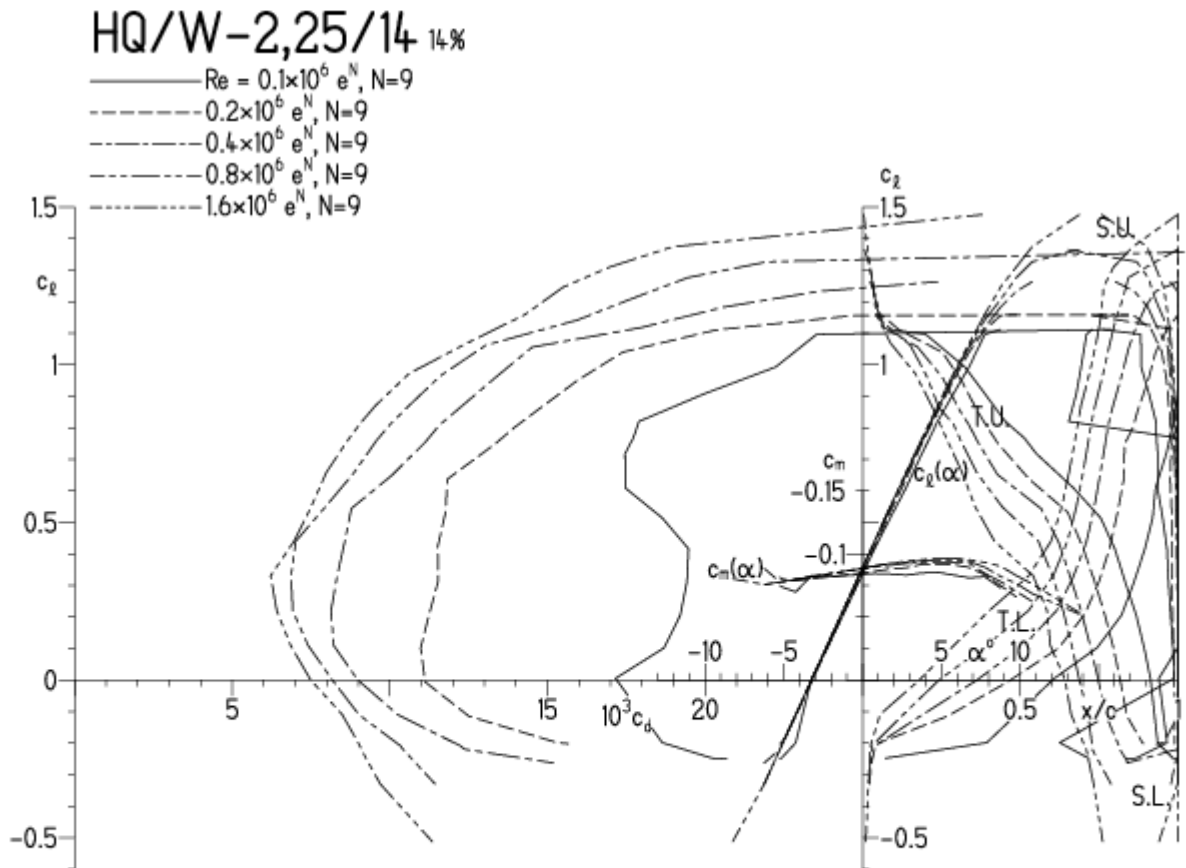


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

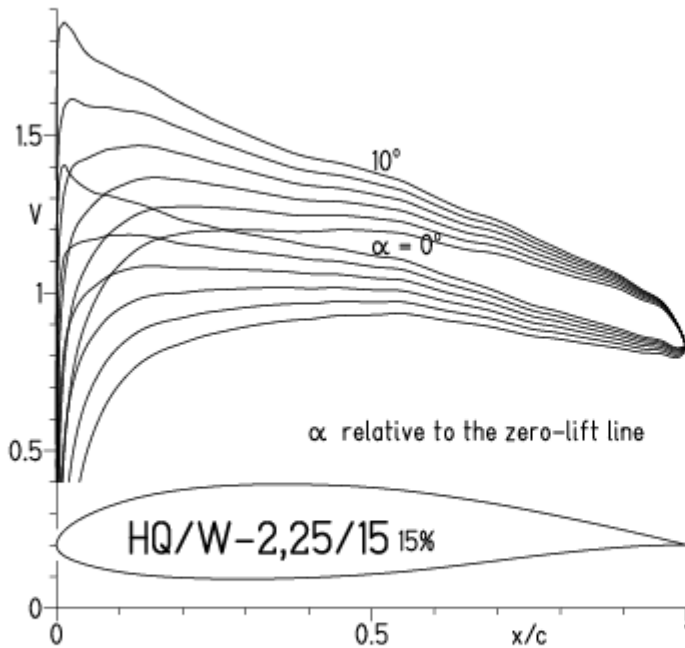


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

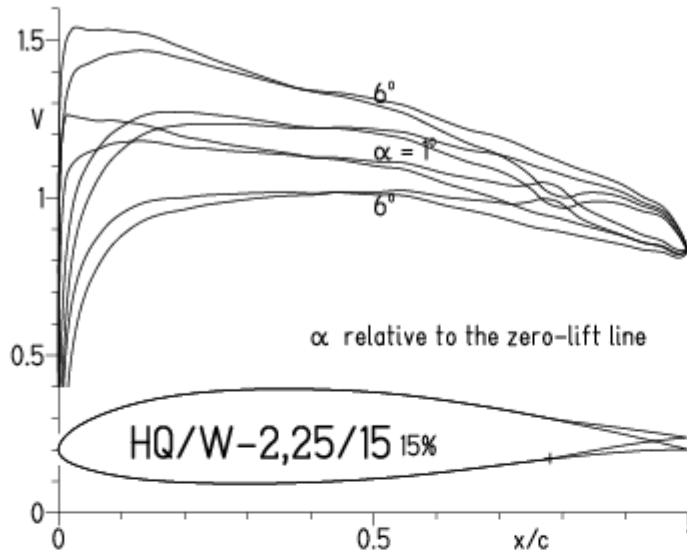


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

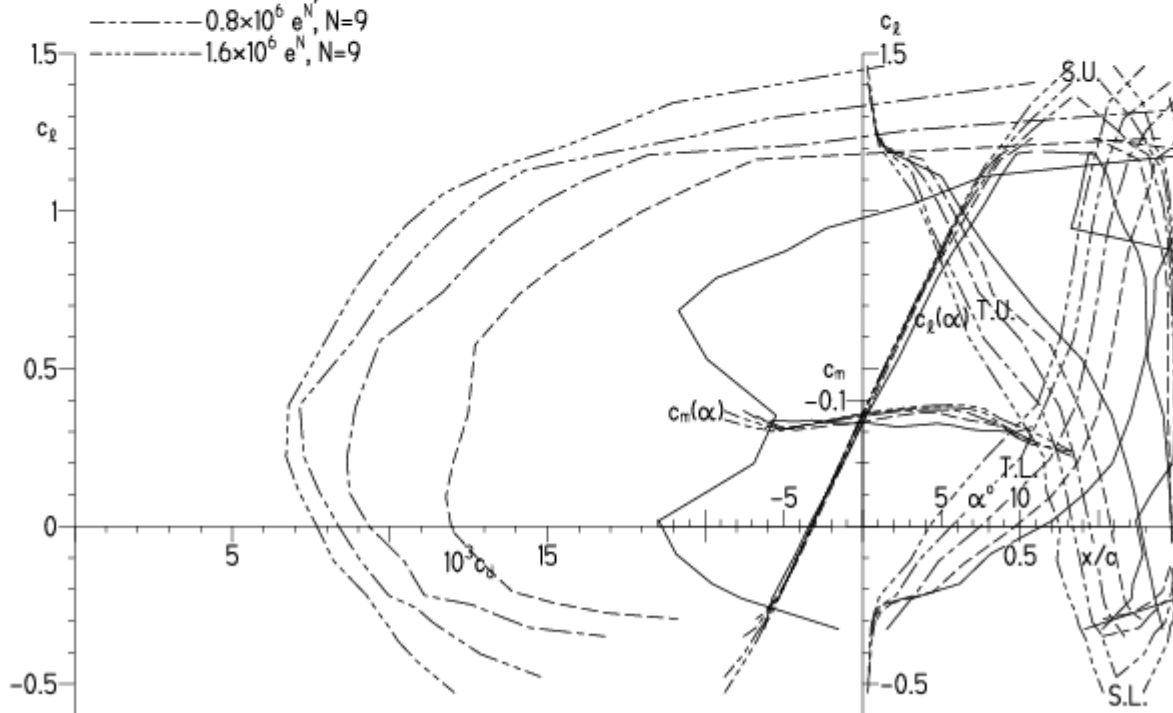
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

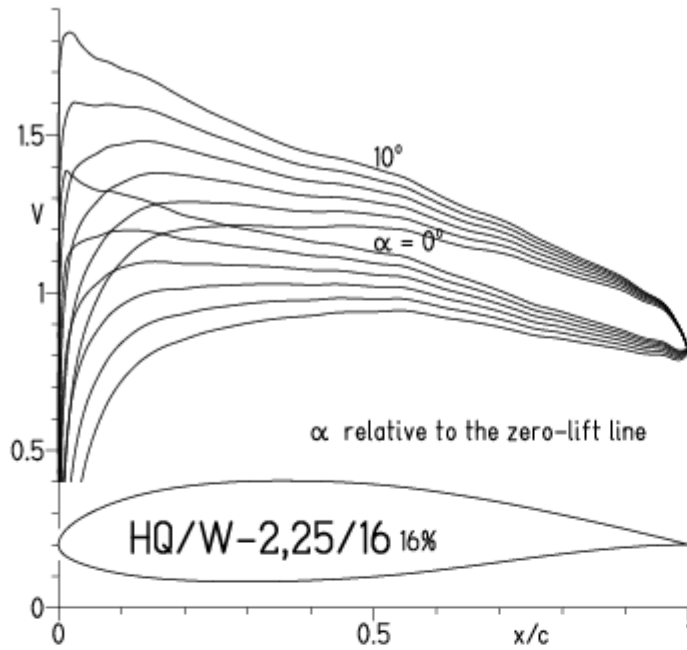
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

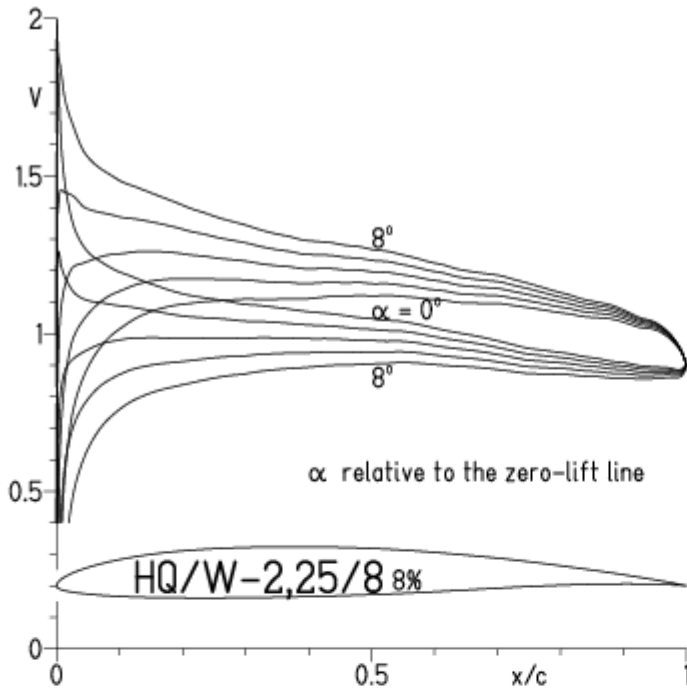
HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



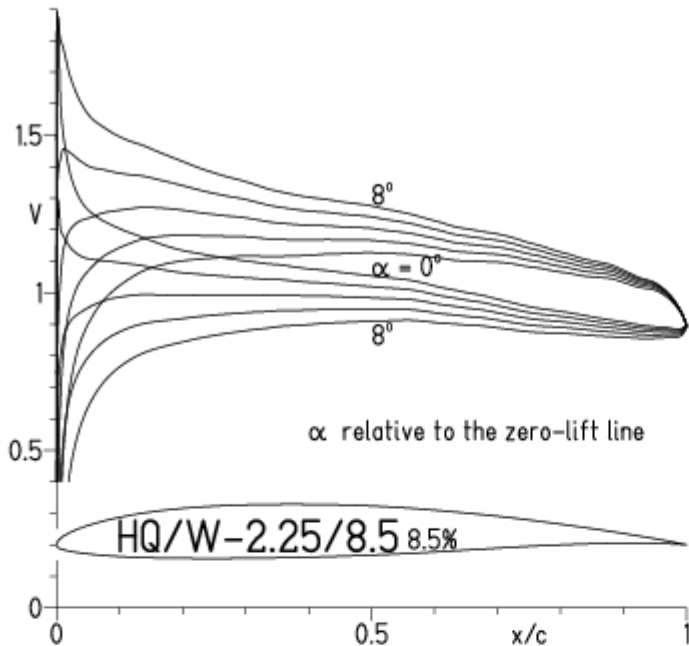
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

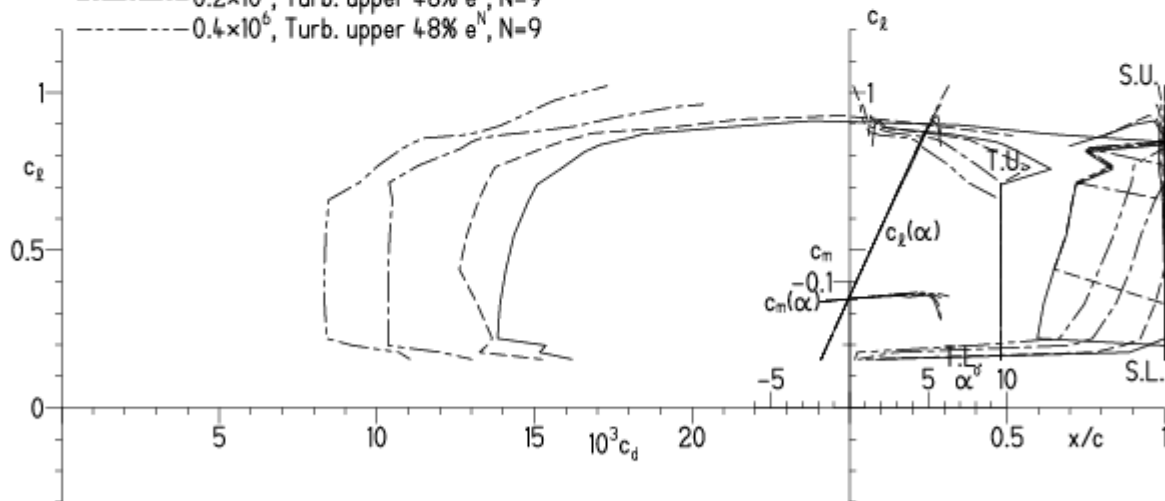
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - · 22% Flap 4°, Re = 75 000 e^N, N=11
- · - · 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

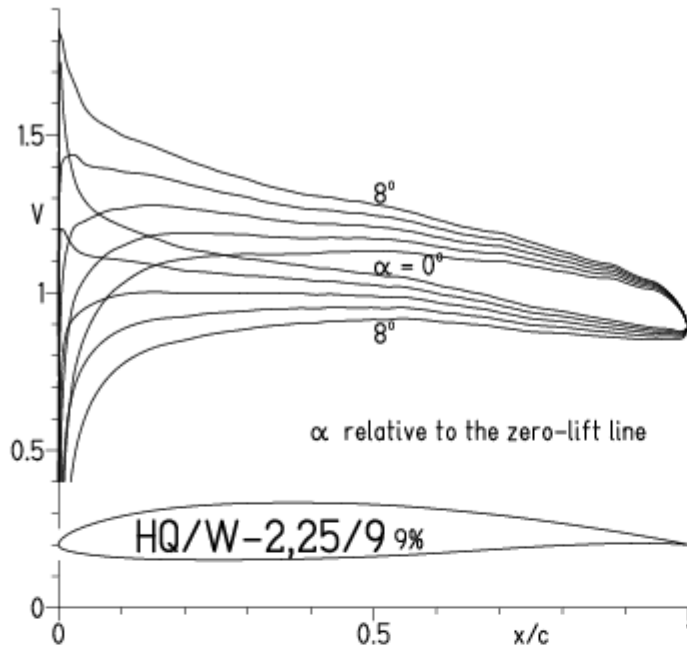


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

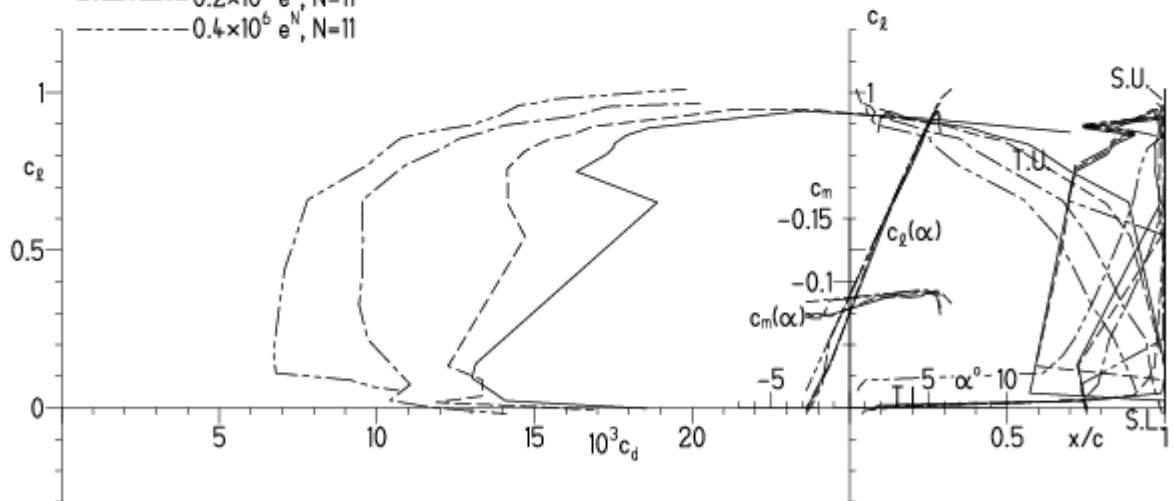
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



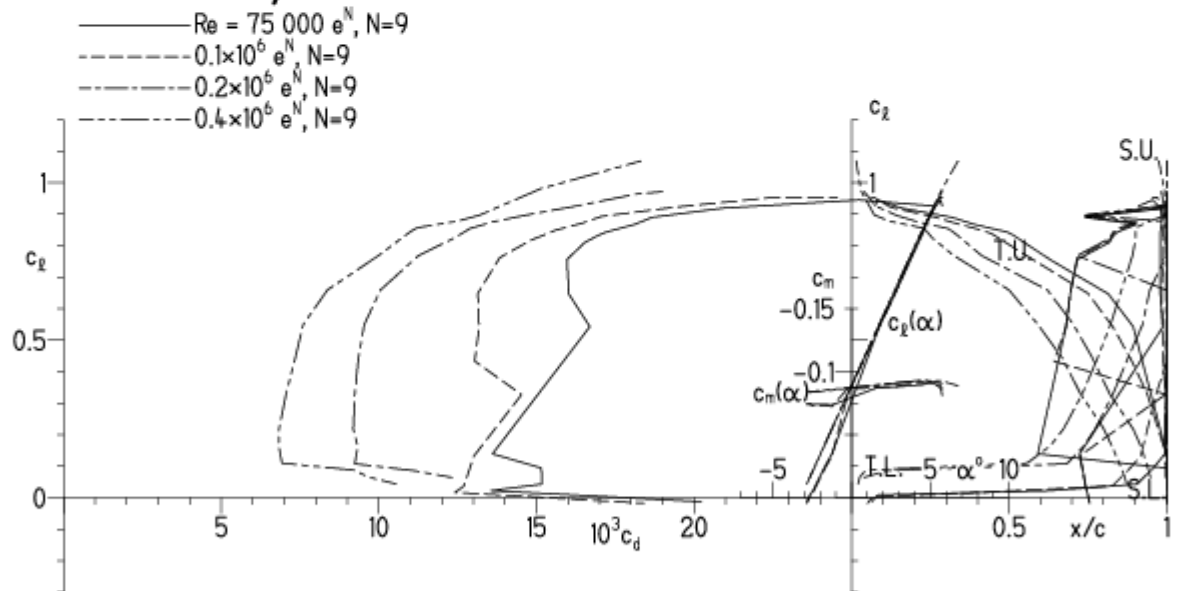
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

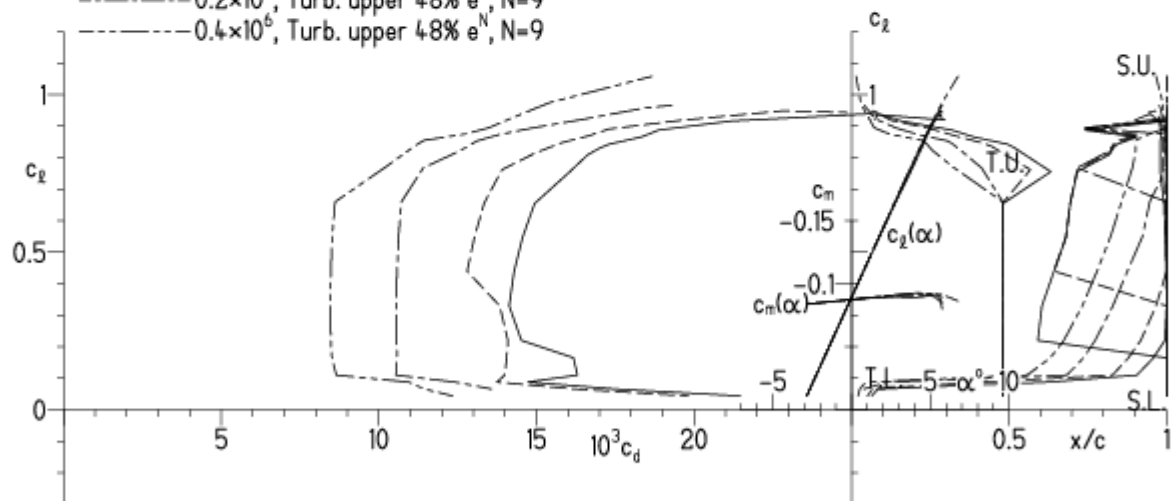
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

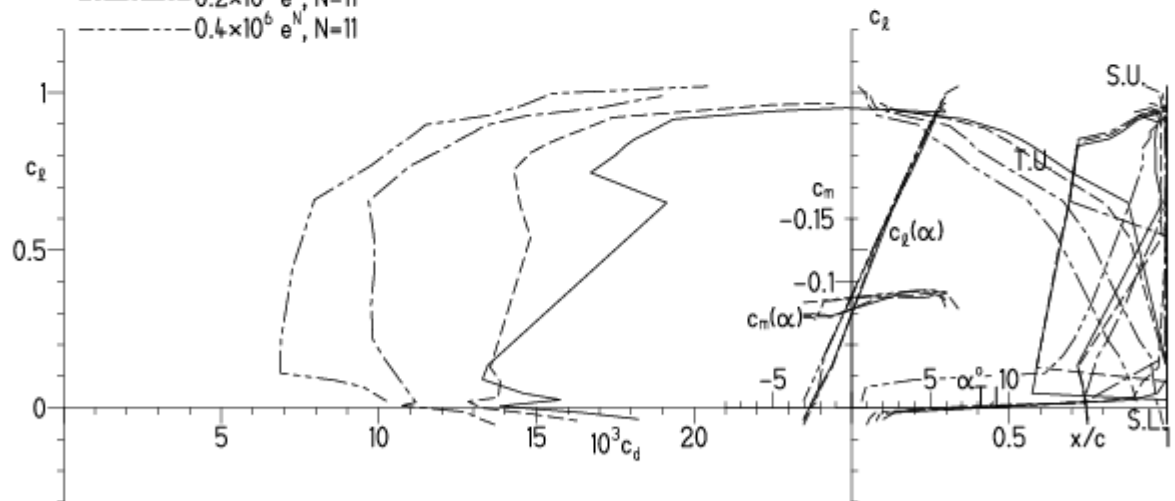
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



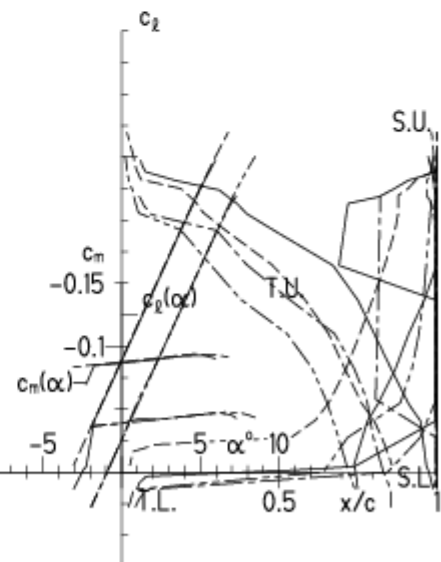
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

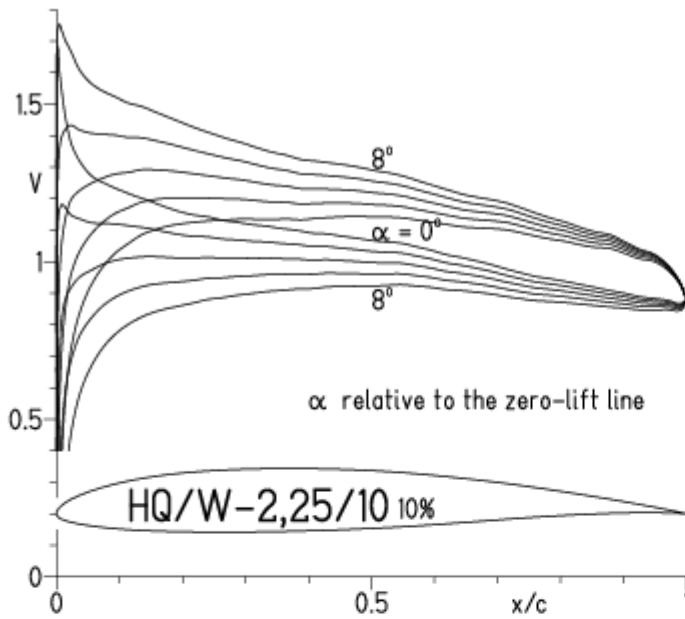


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

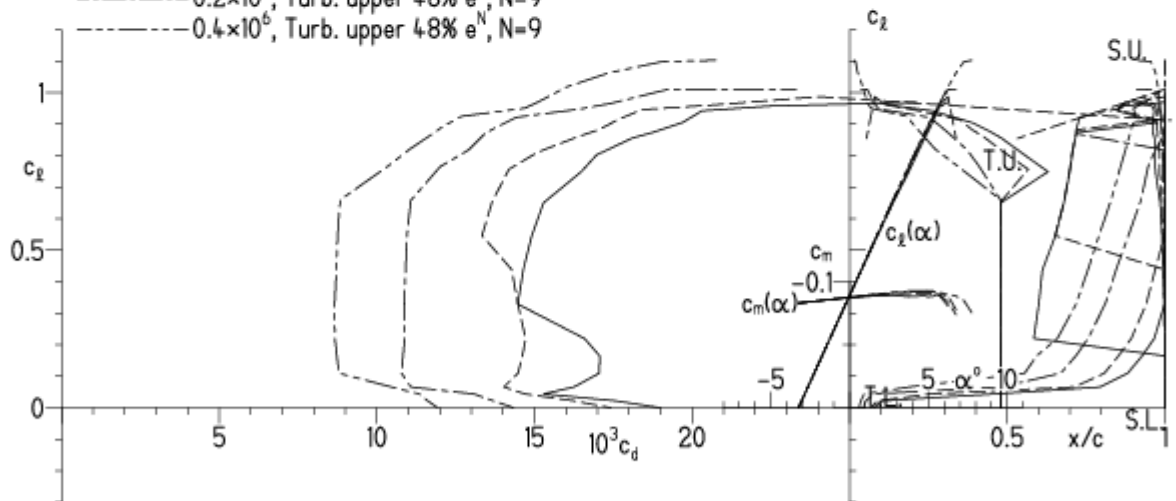
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

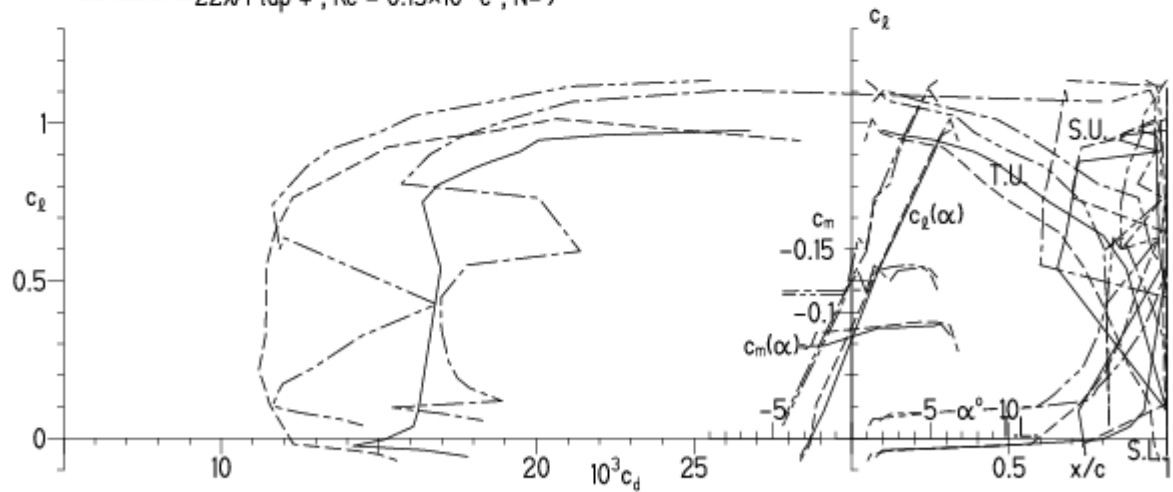


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

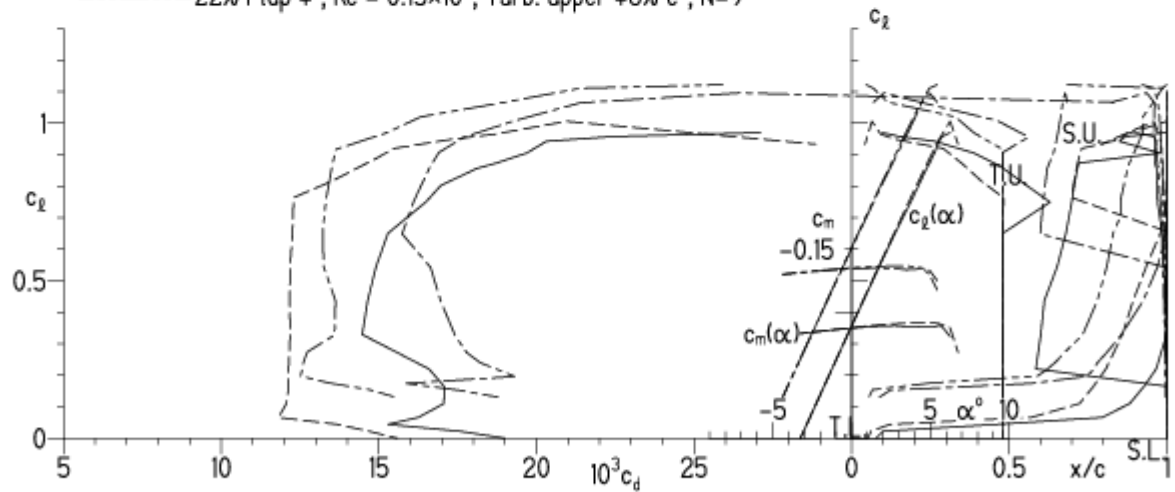


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

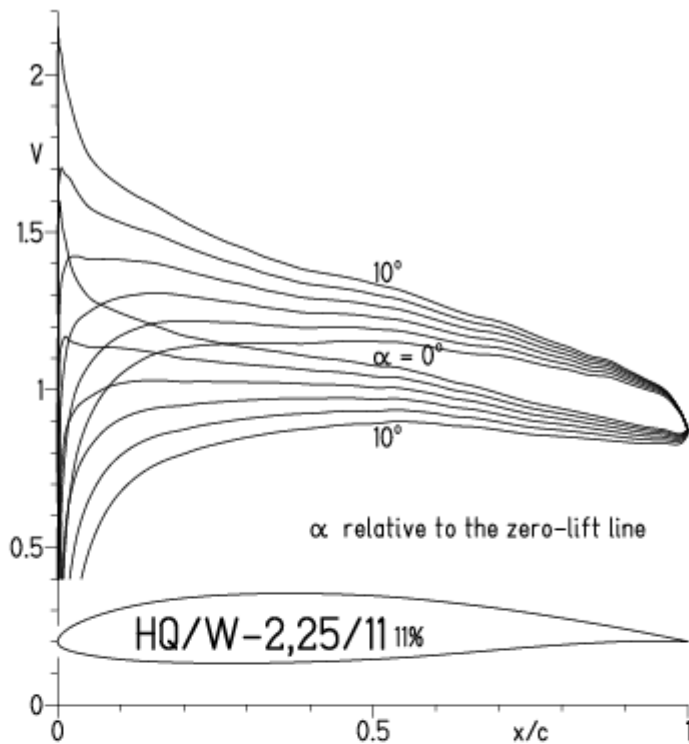


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - $0.8 \times 10^6 e^N, N=9$
- · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

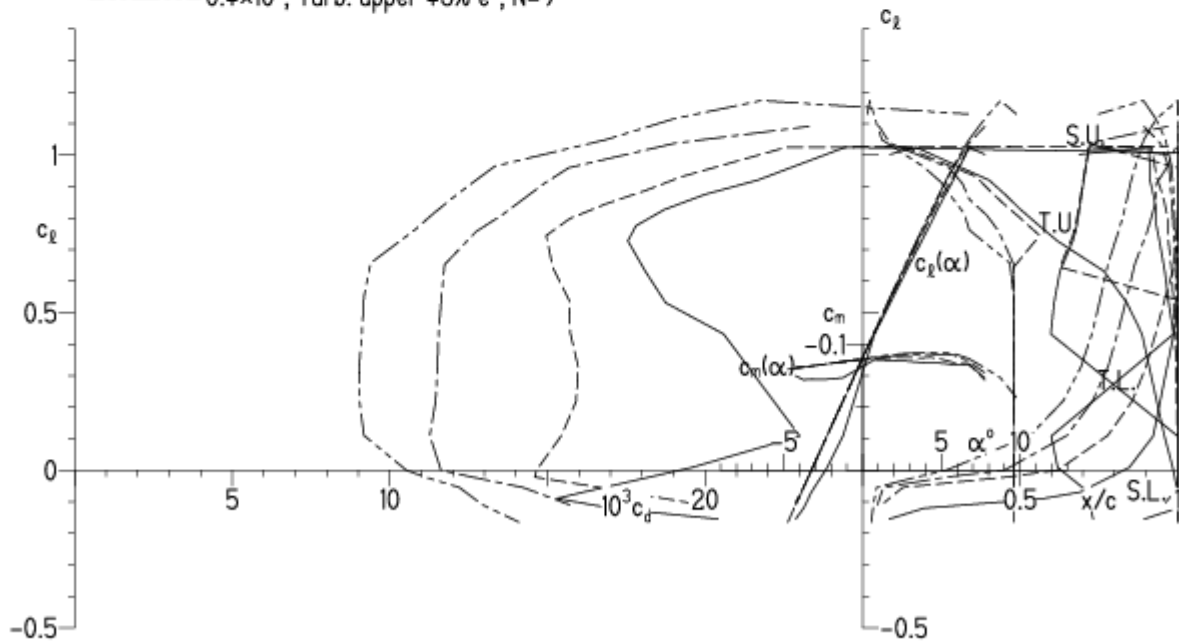
EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

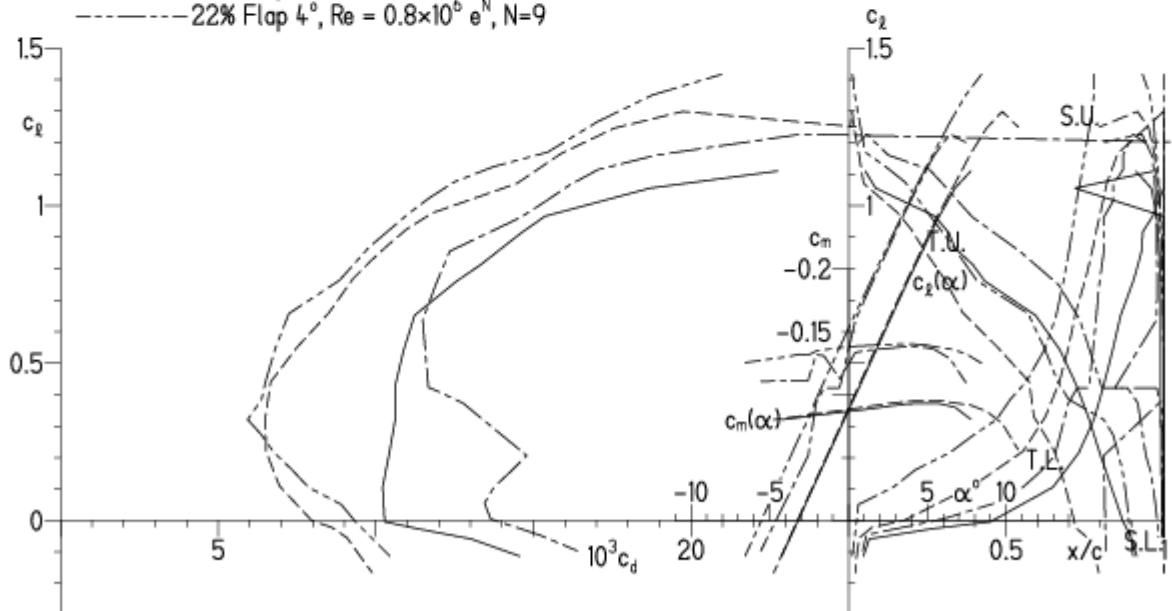


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

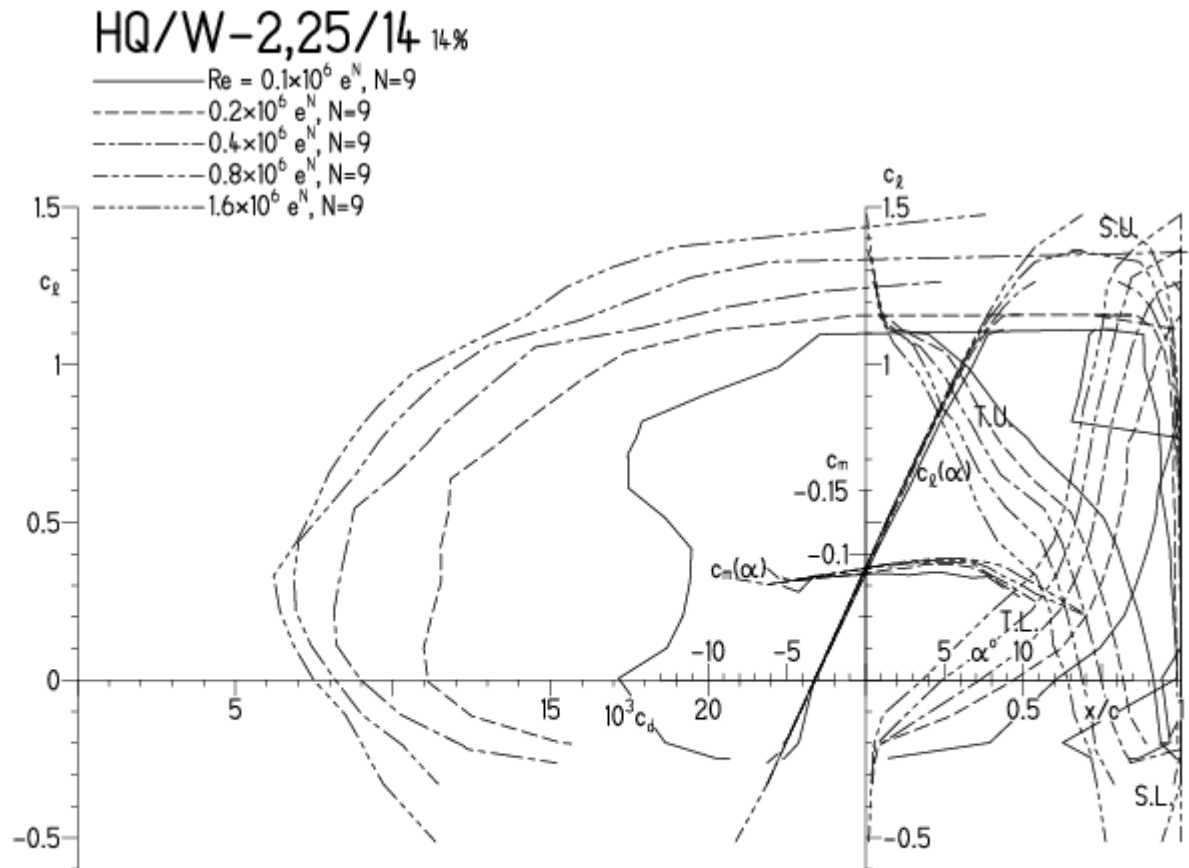


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

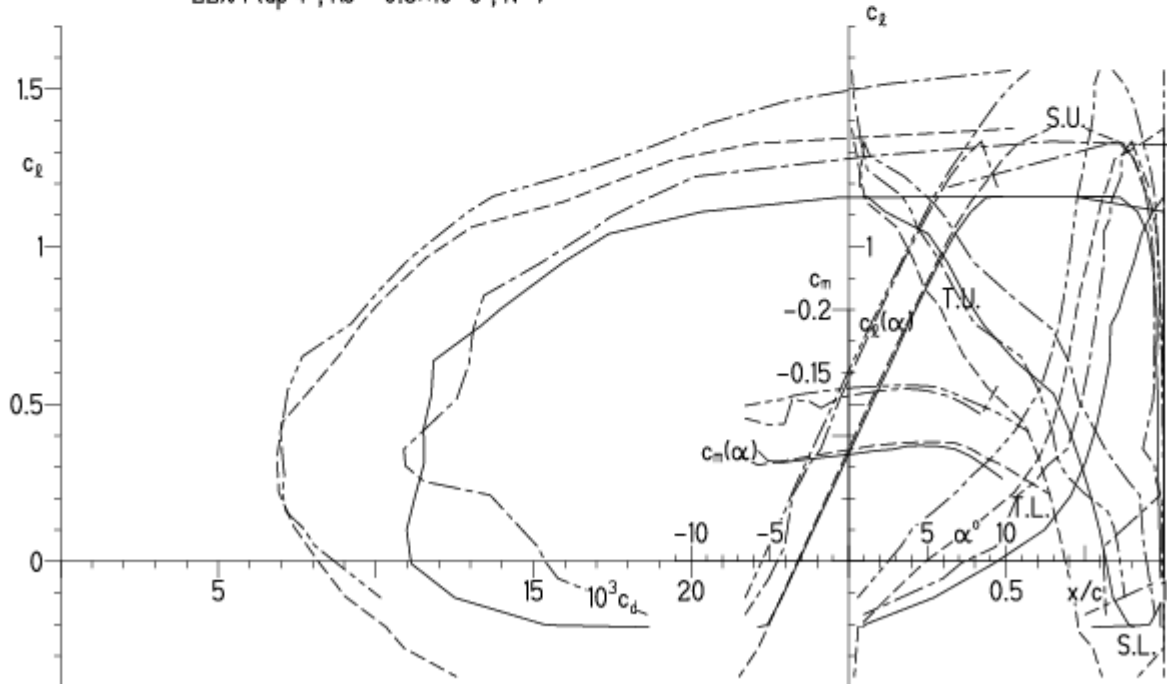


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

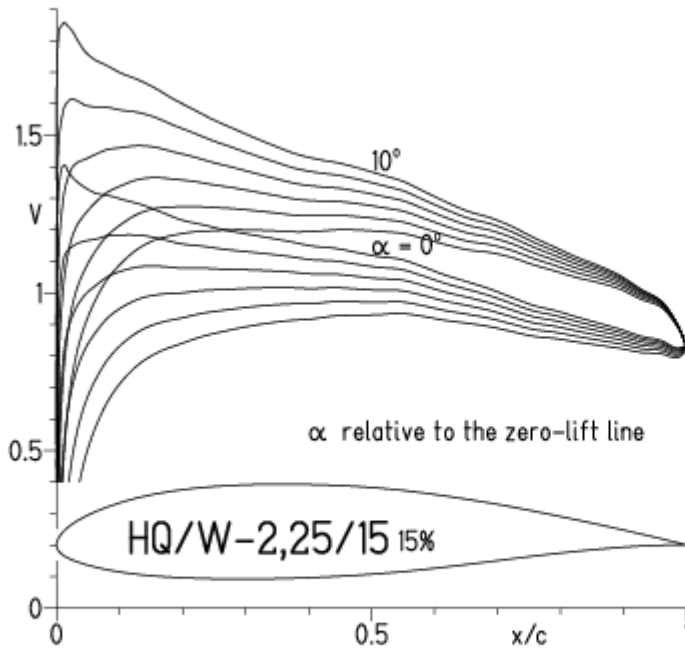


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

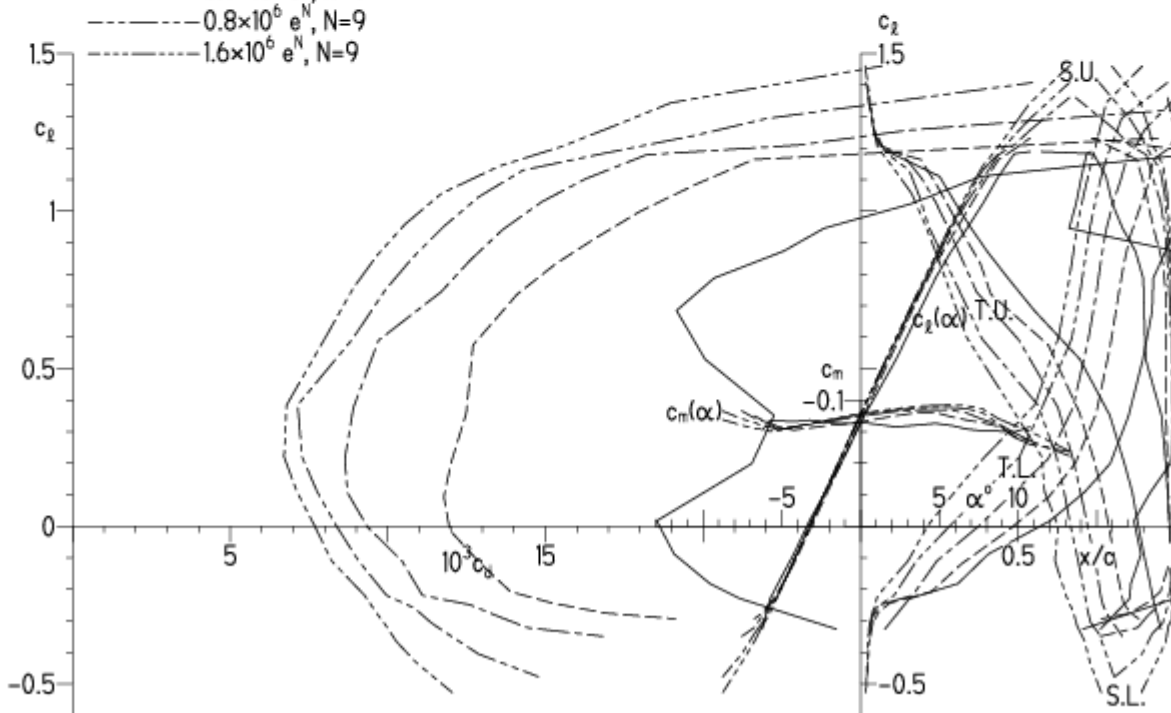
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

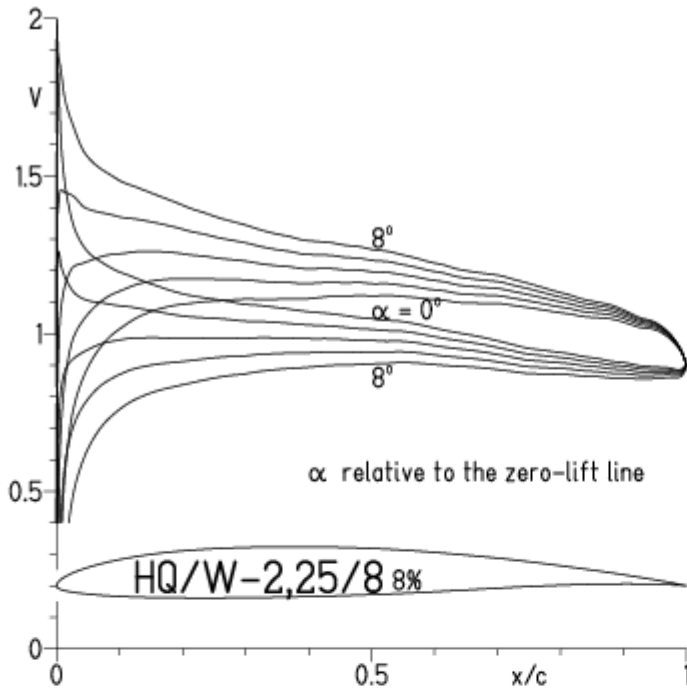
HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

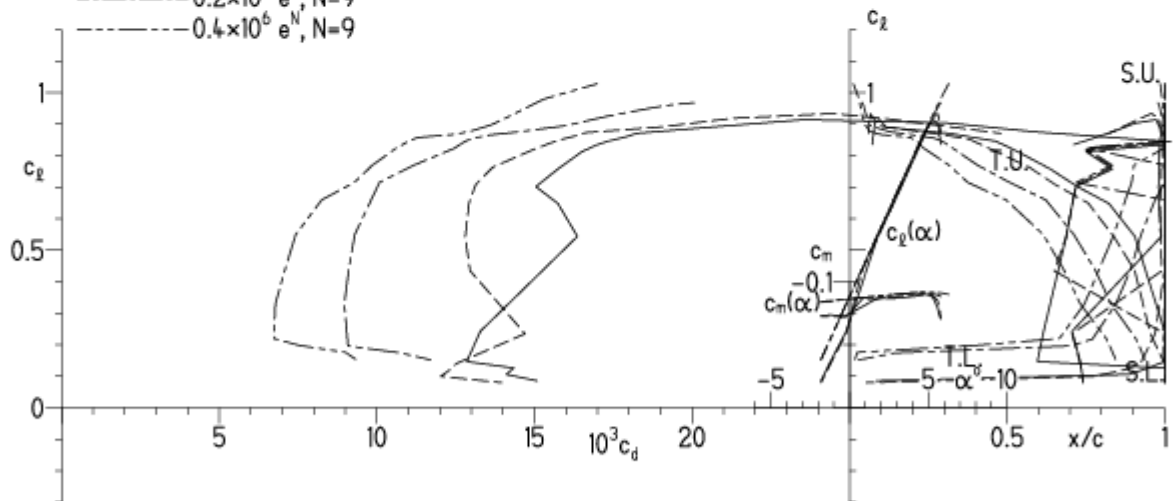
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

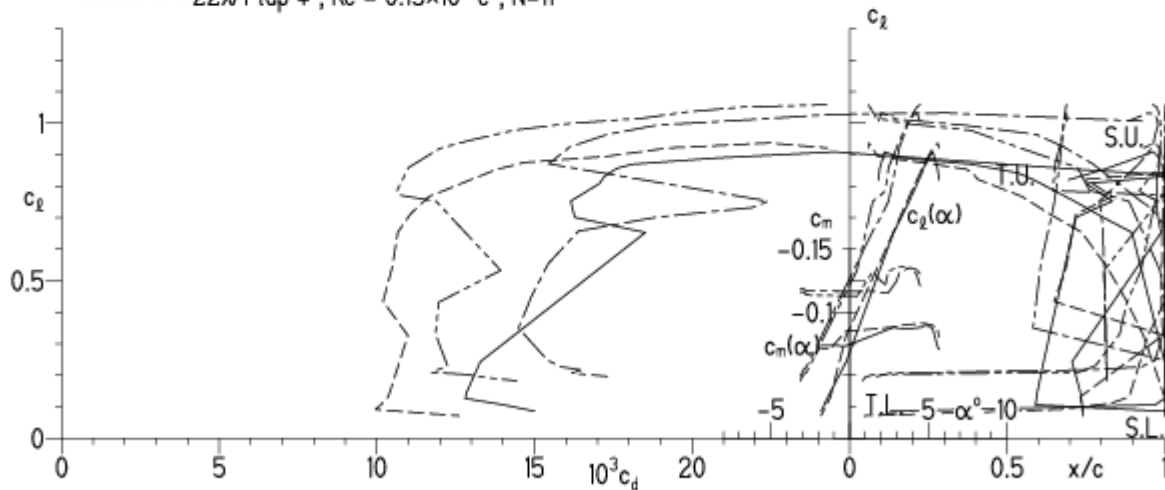


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

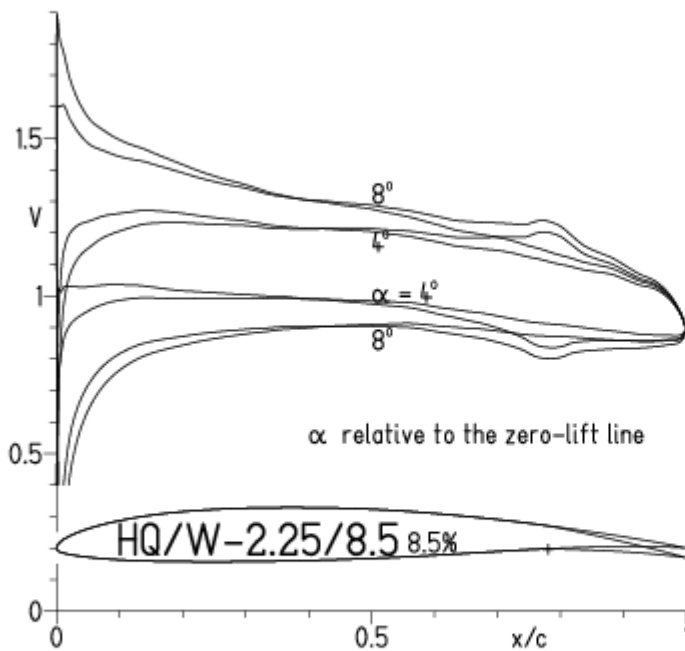
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

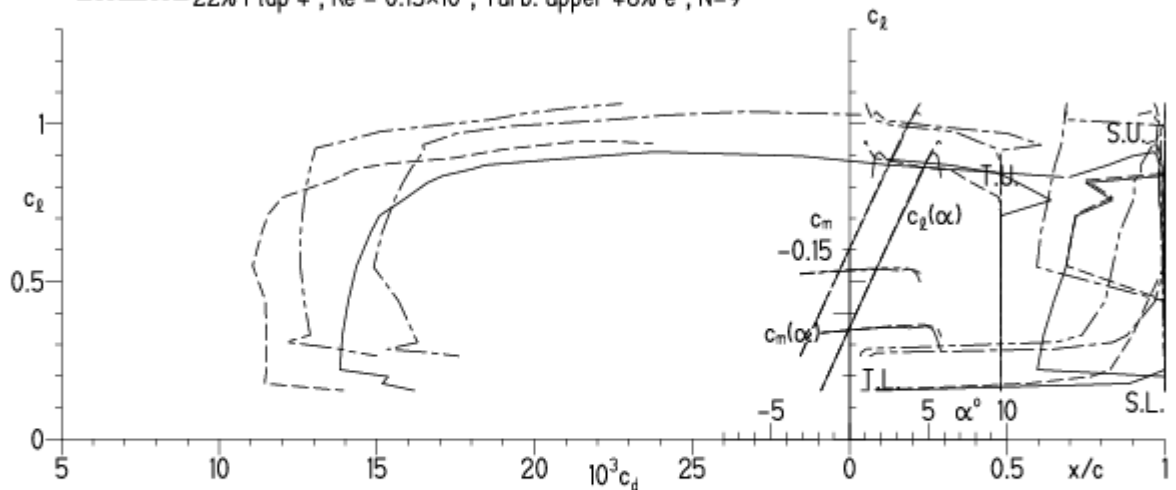


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$

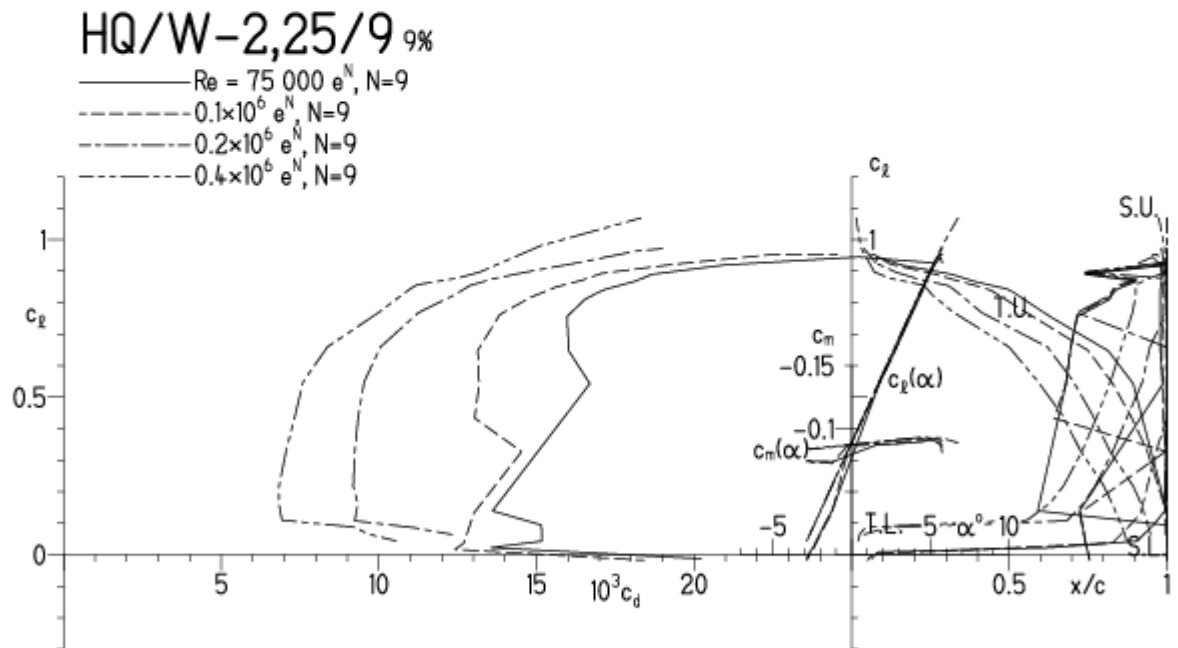


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

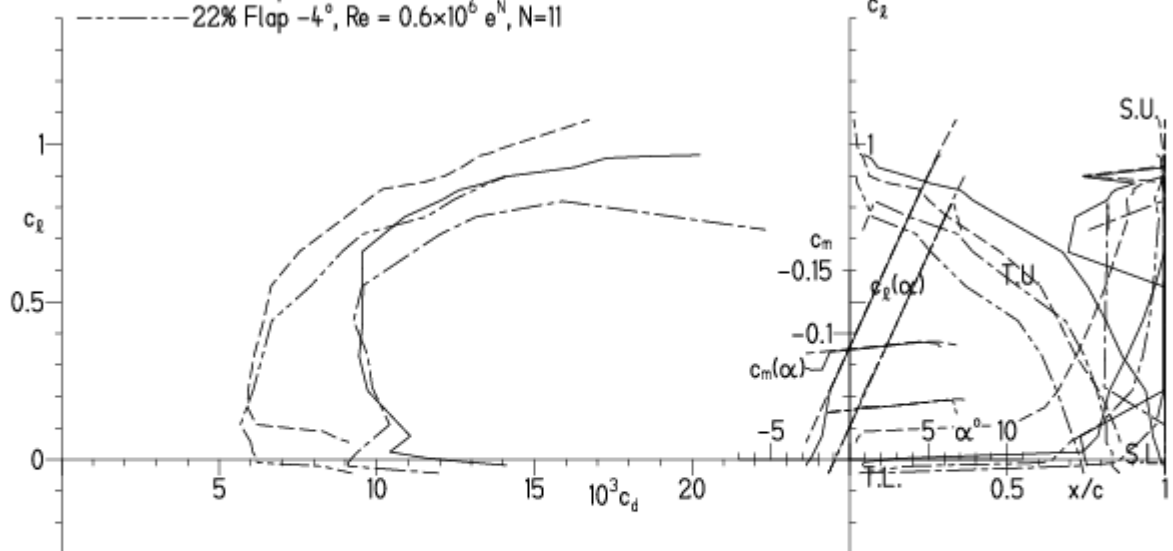
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

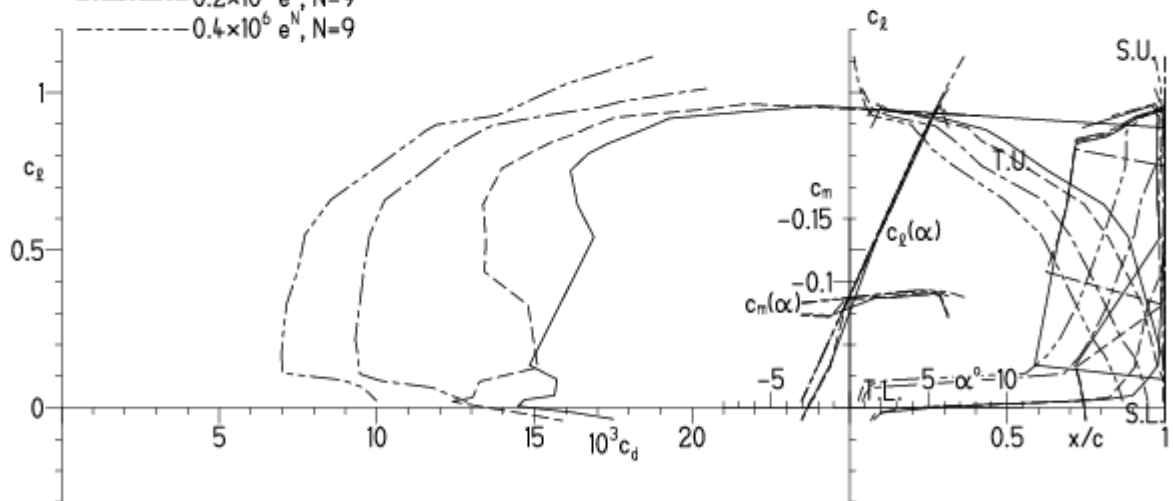
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

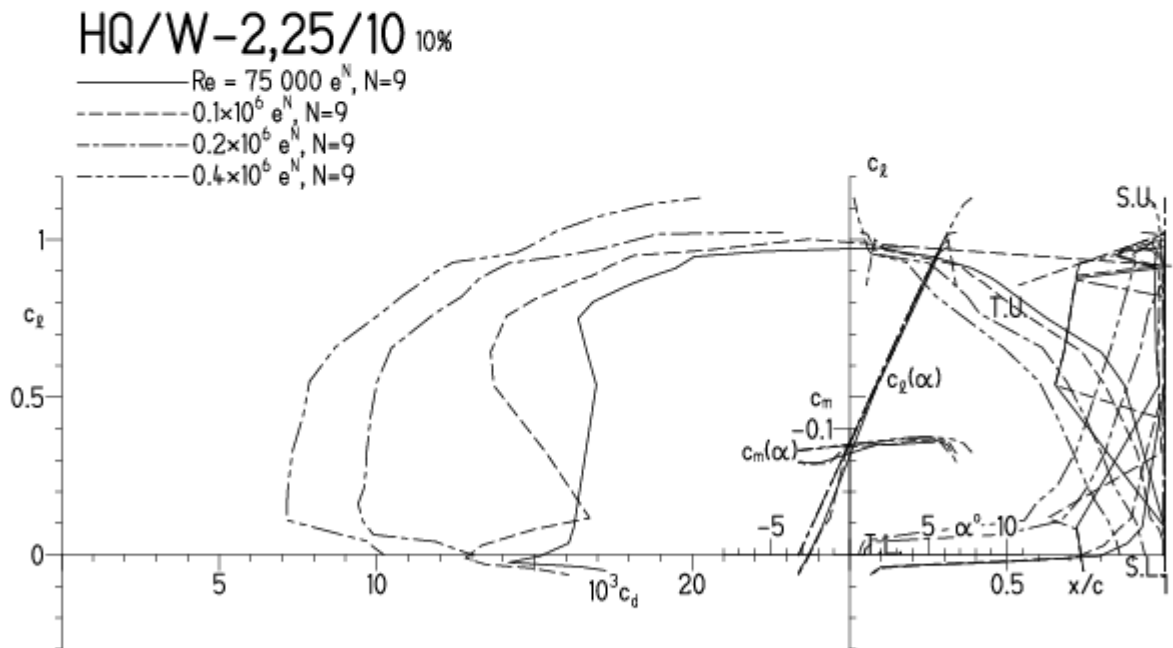


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

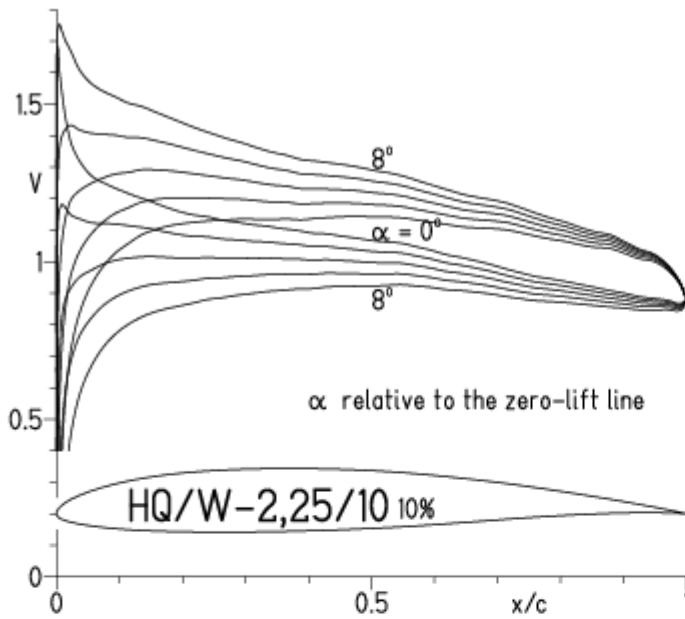


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

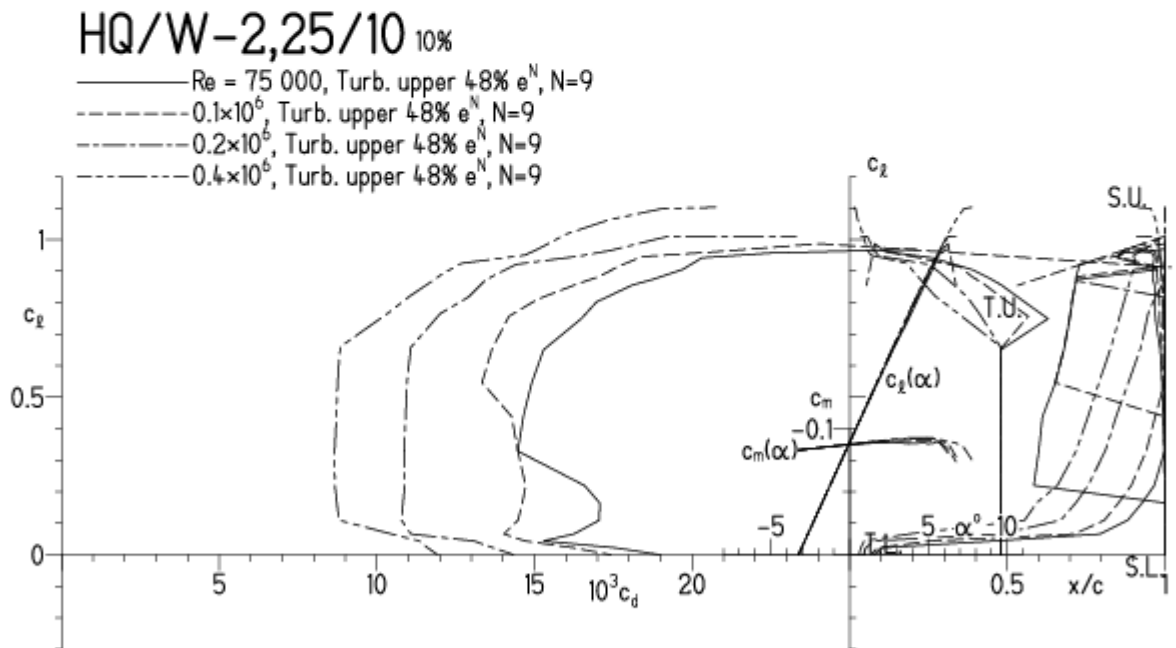


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

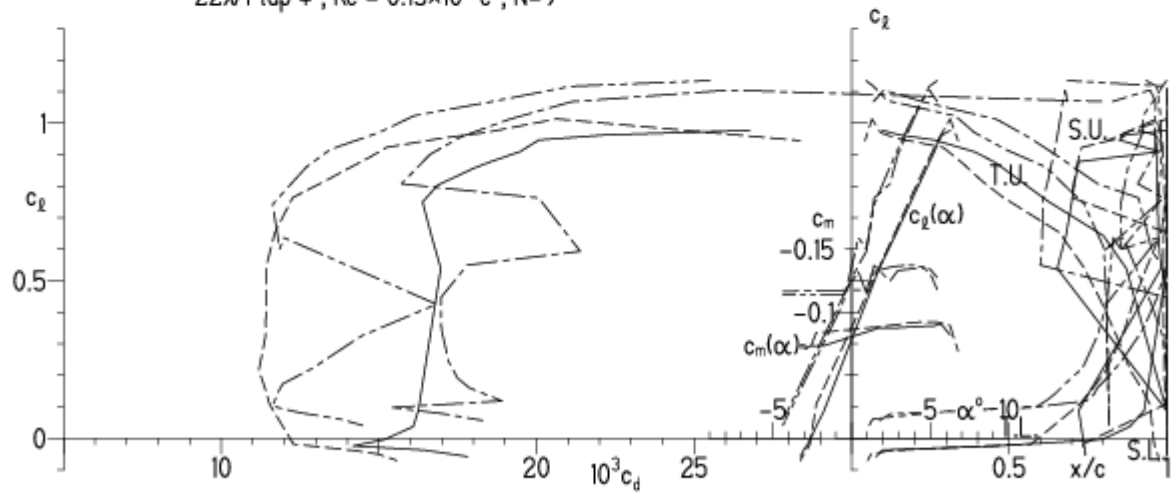


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

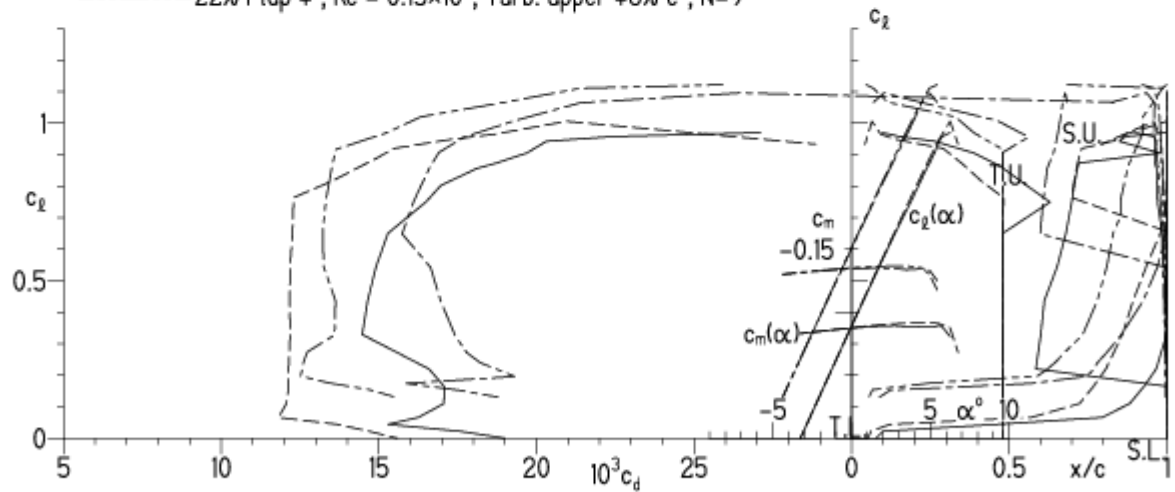


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

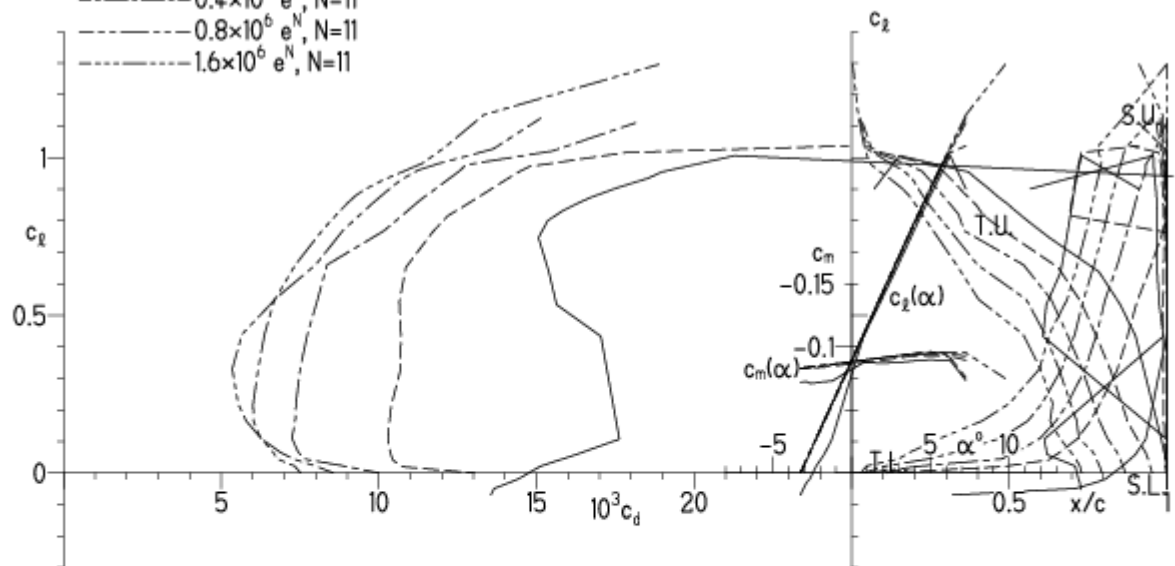
EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:

HQ/W-2,25/11 11%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

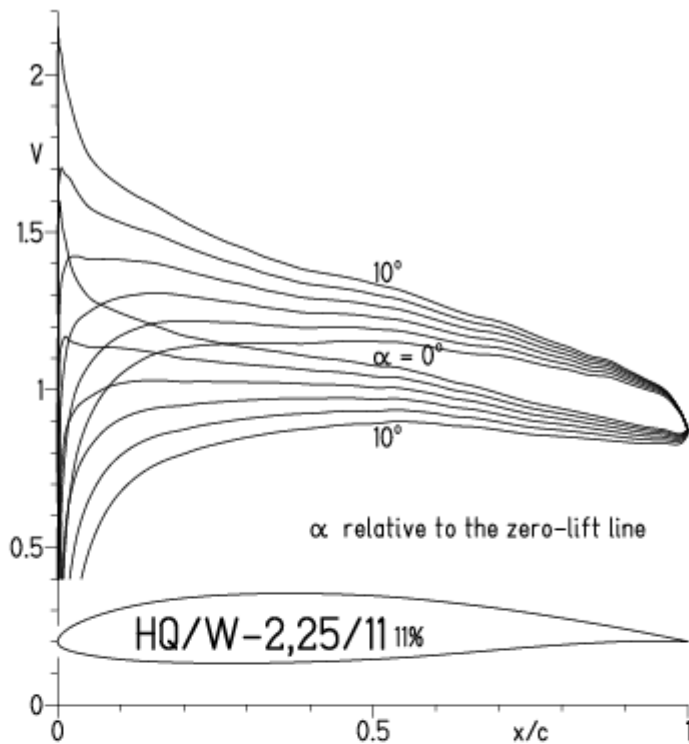


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6$ e^N, N=9
- - - 0.2×10^6 e^N, N=9
- · - 0.4×10^6 e^N, N=9
- · - · 0.8×10^6 e^N, N=9
- · - · - 1.6×10^6 e^N, N=9



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

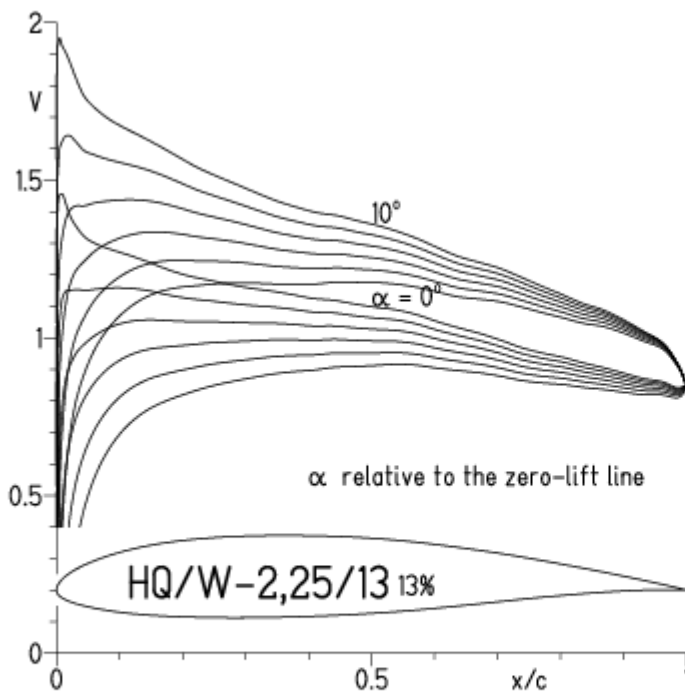


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

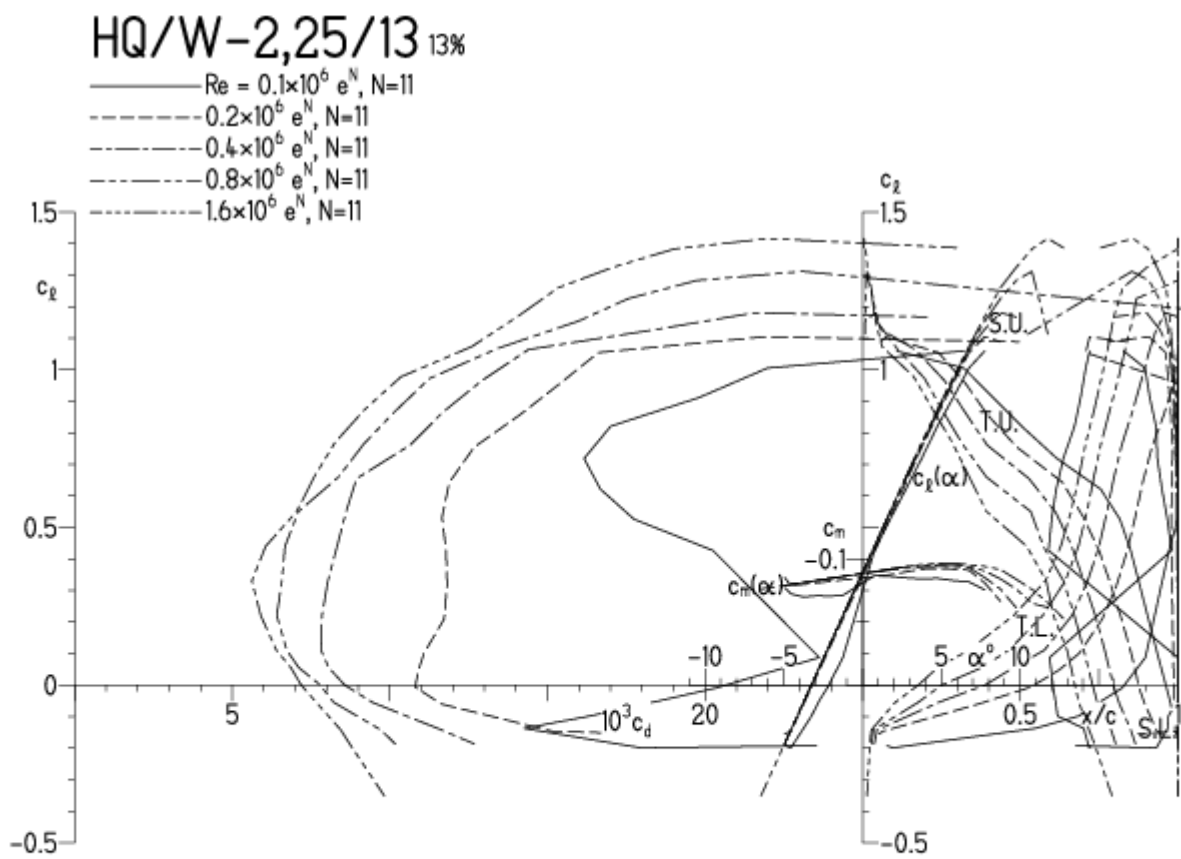


HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

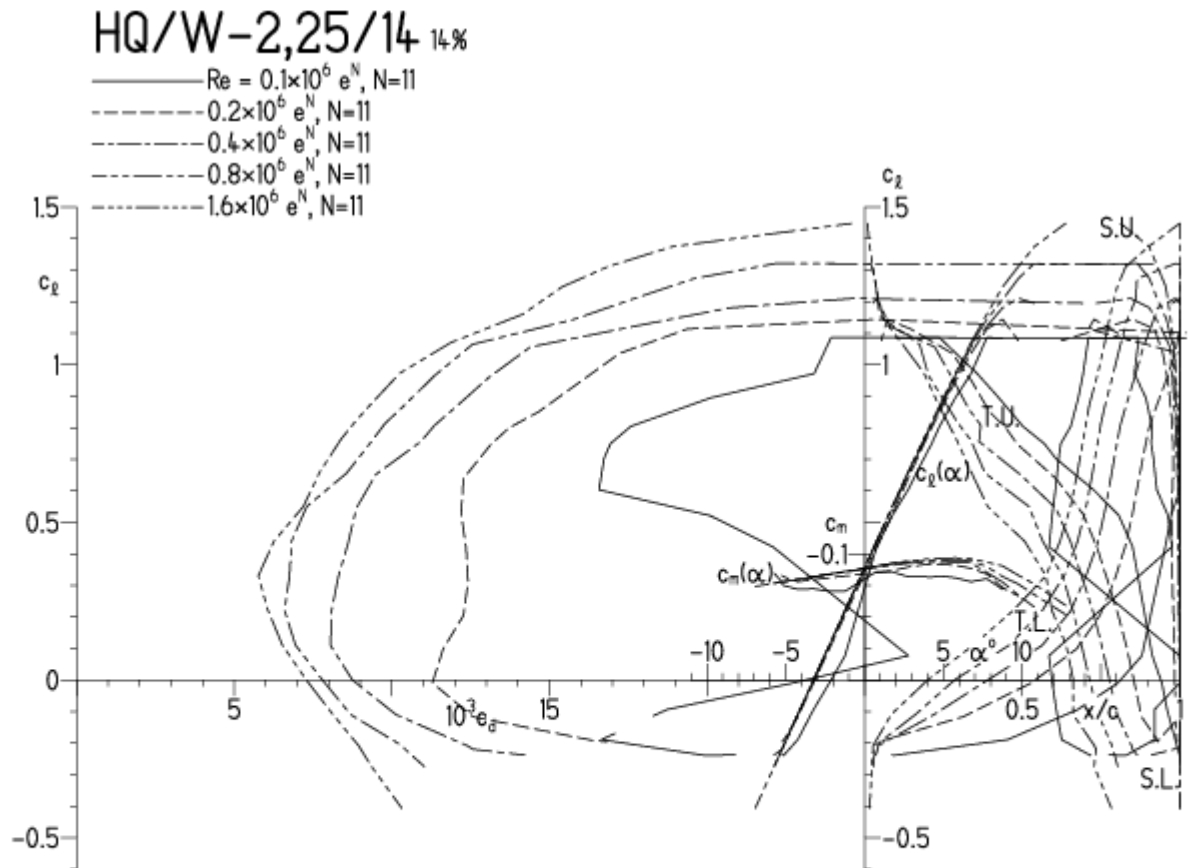


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

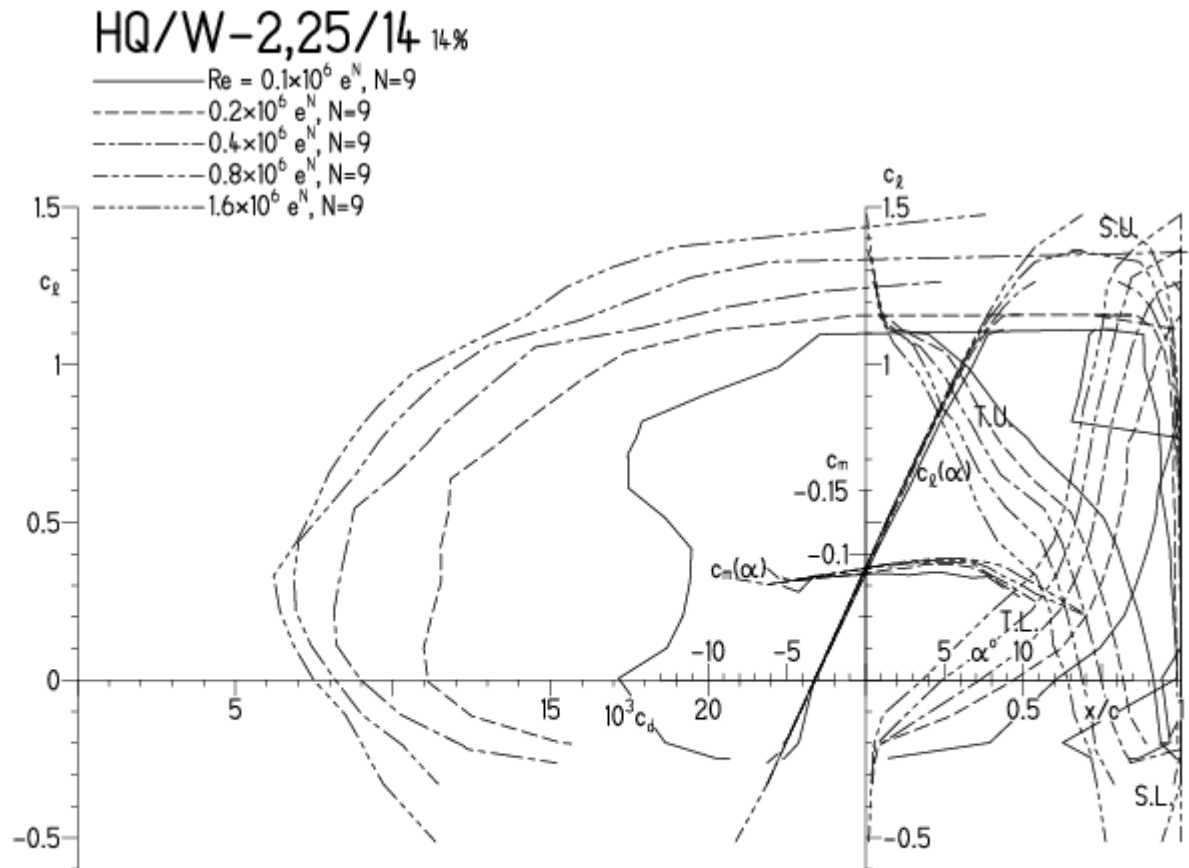


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

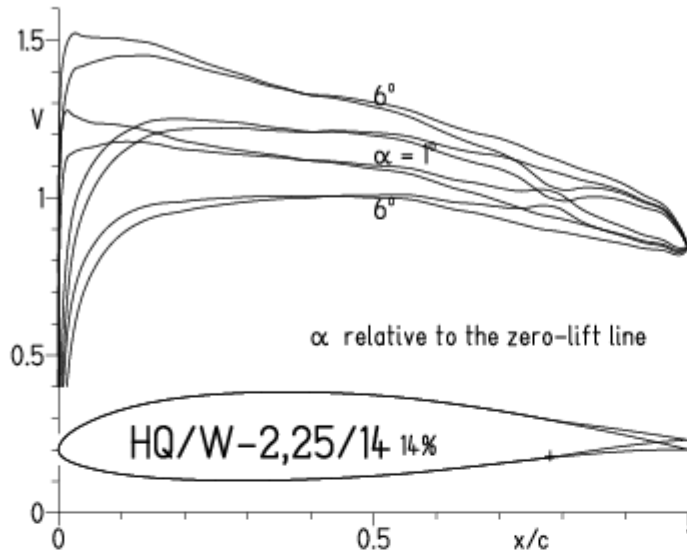
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

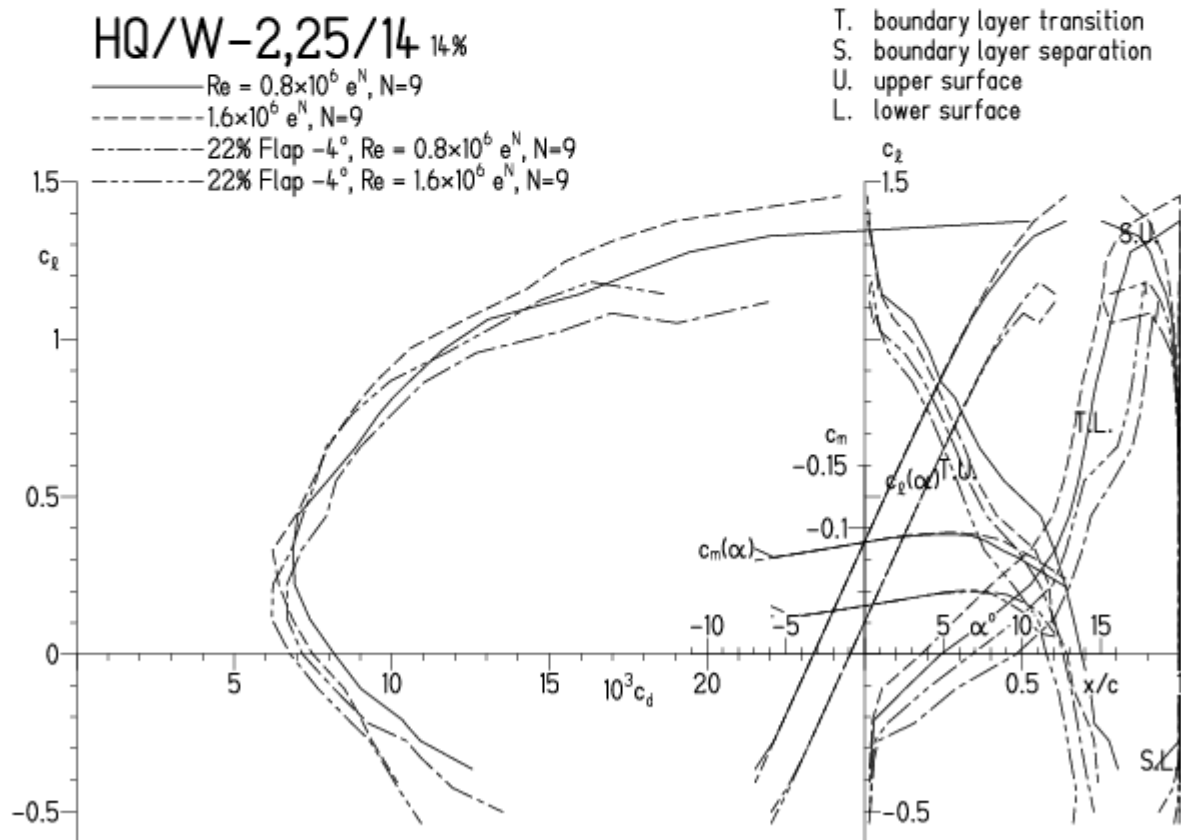


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

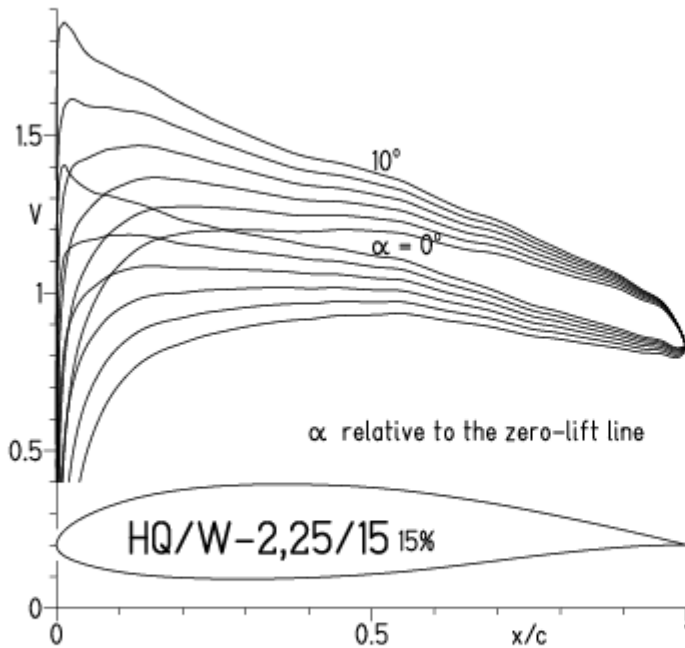


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



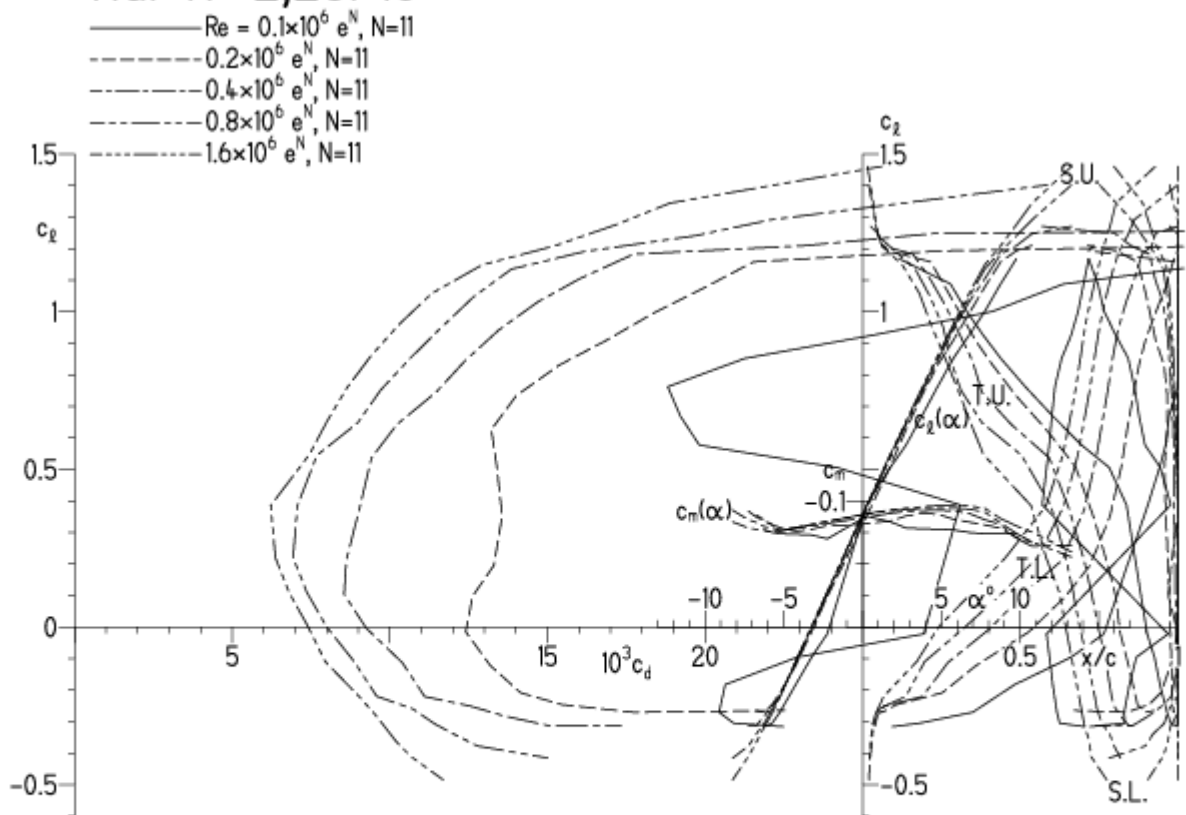
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

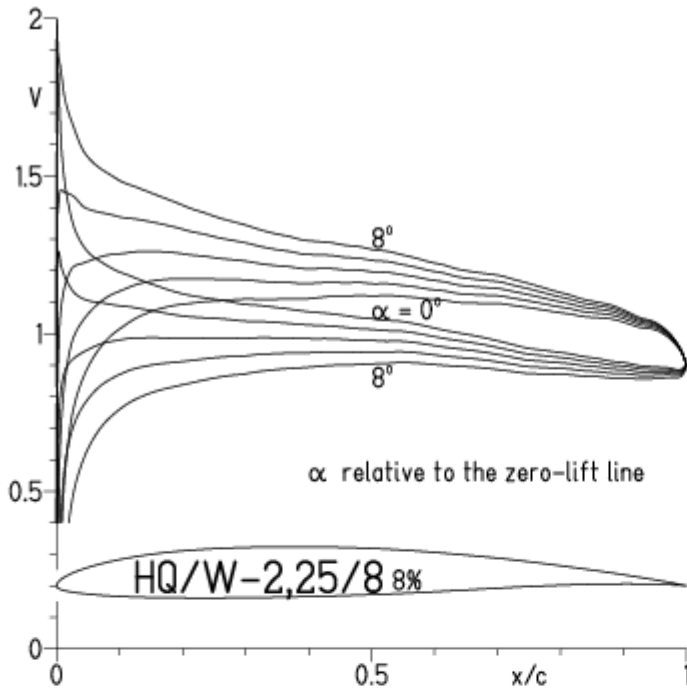
HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15x10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

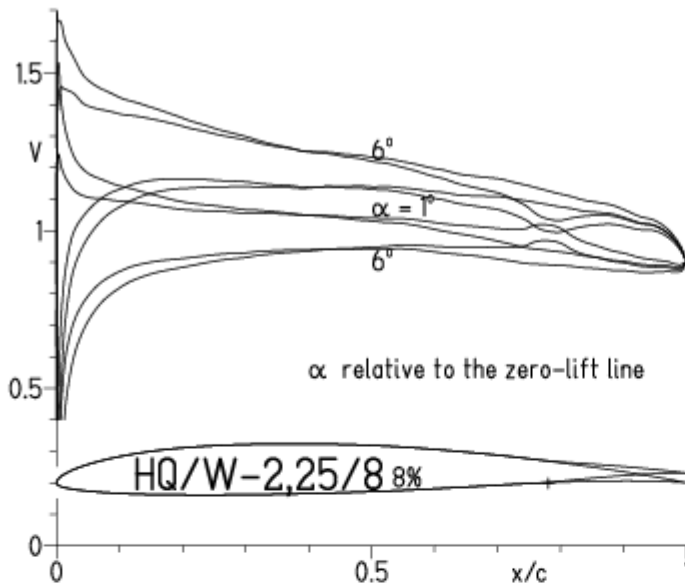
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

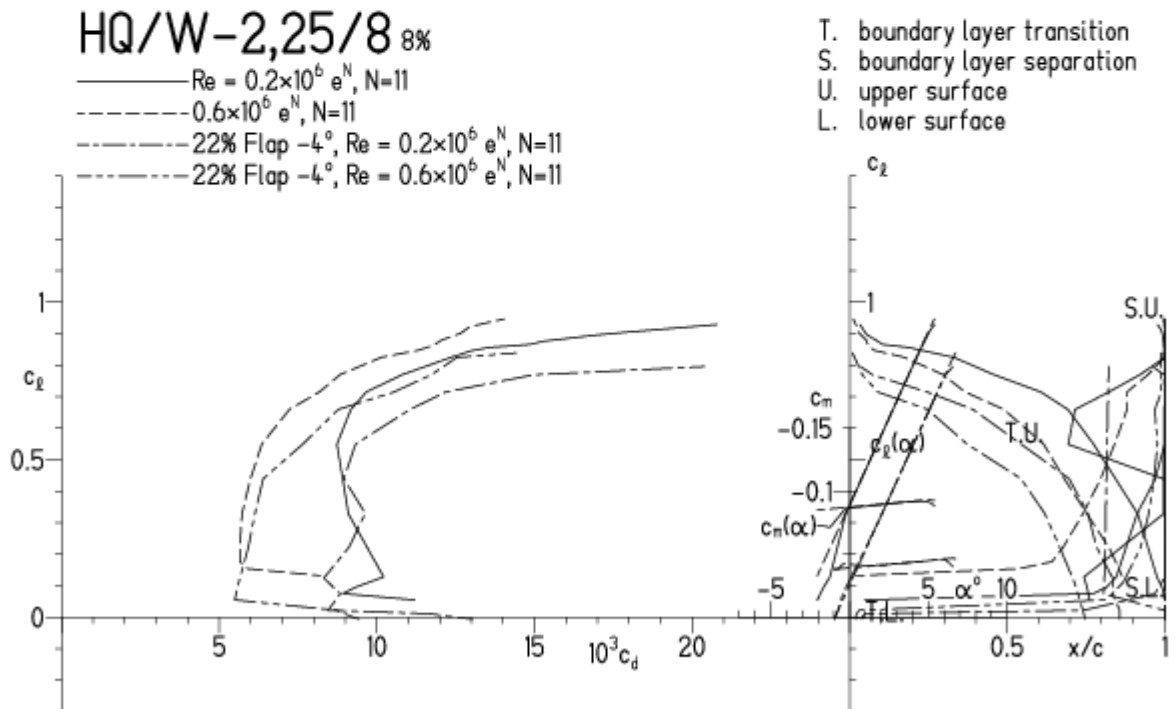


HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



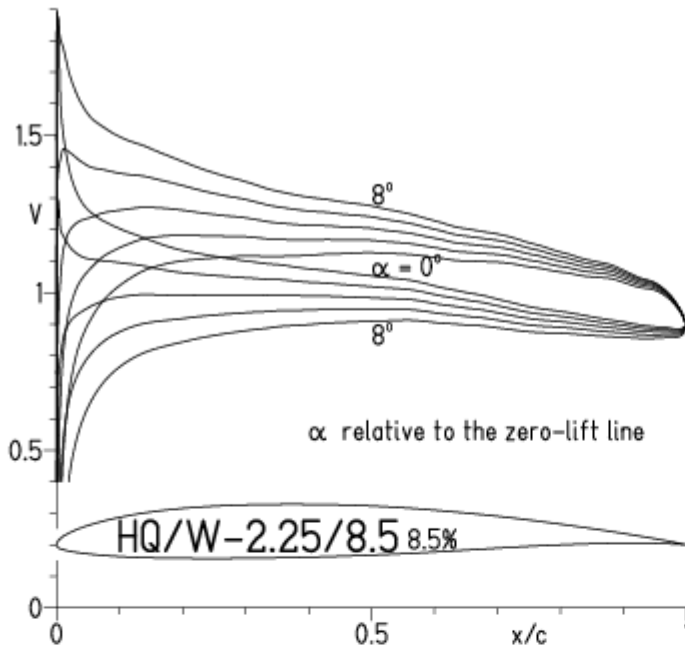
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

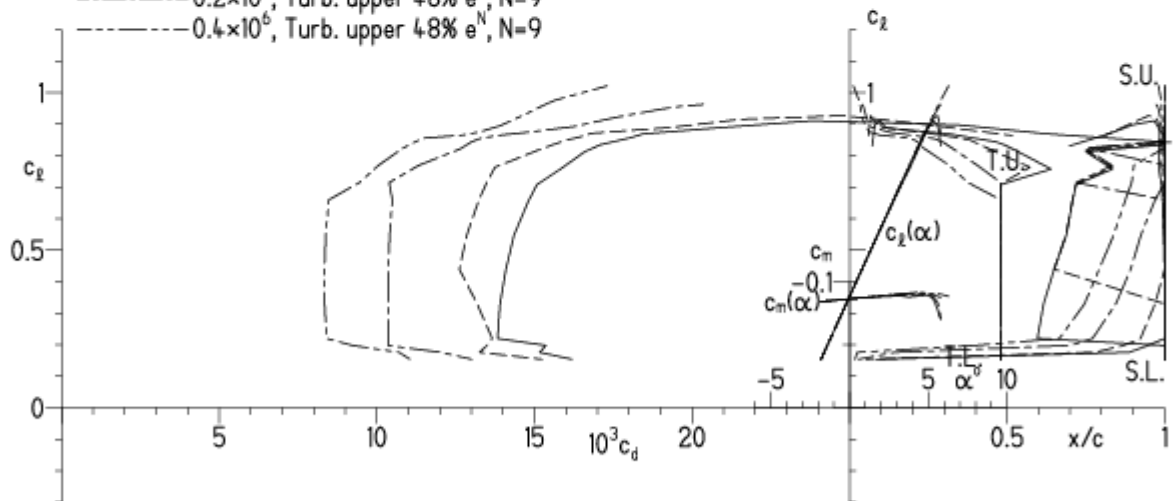
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

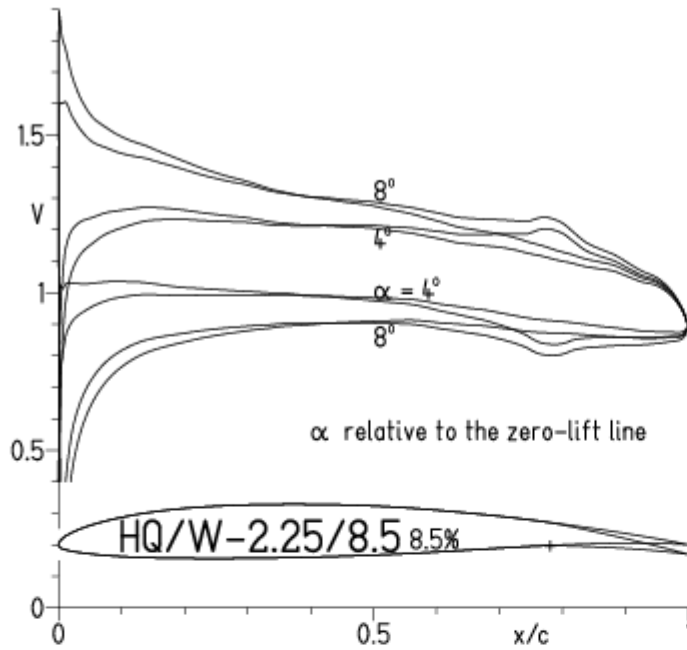
HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

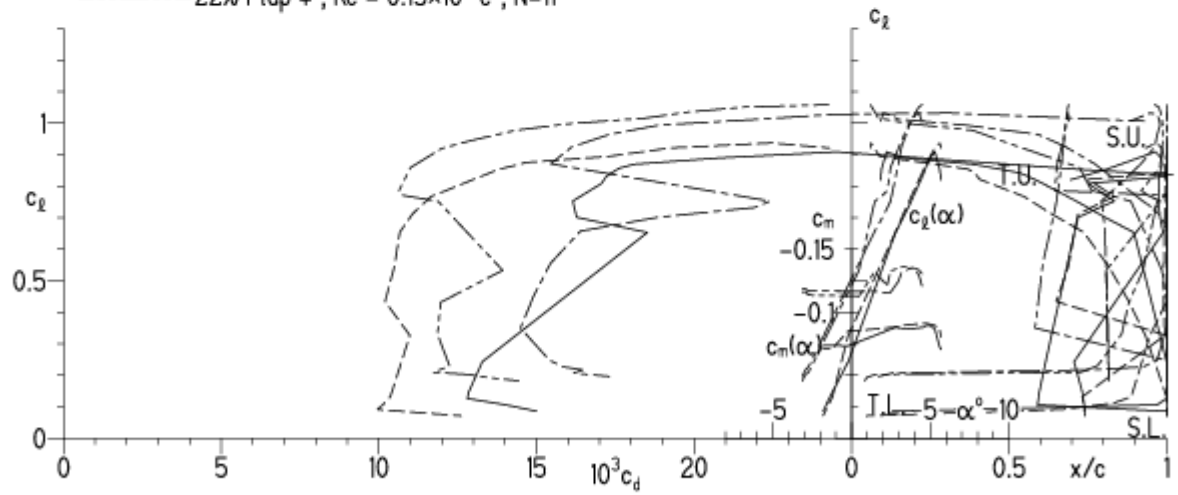


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

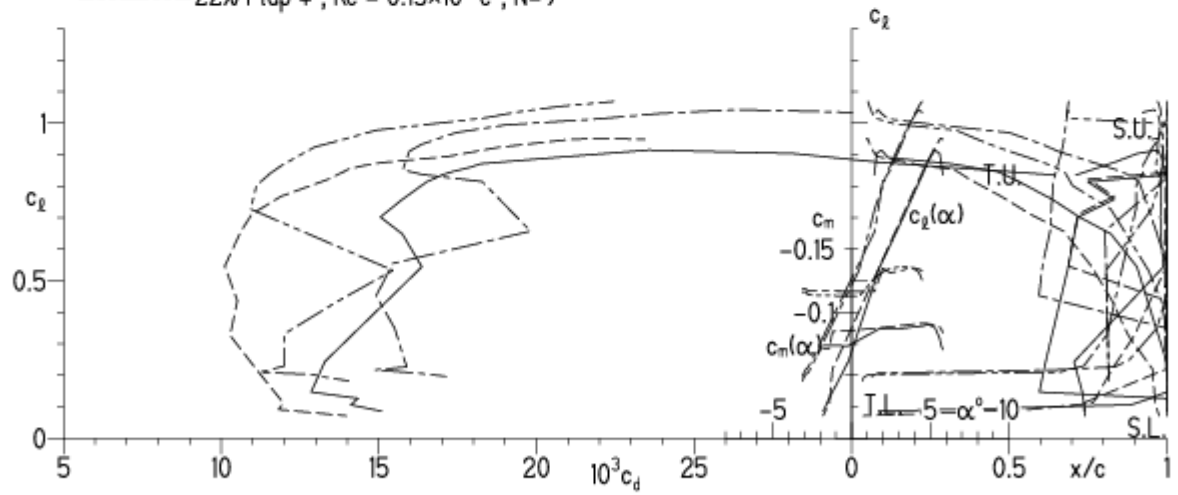


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

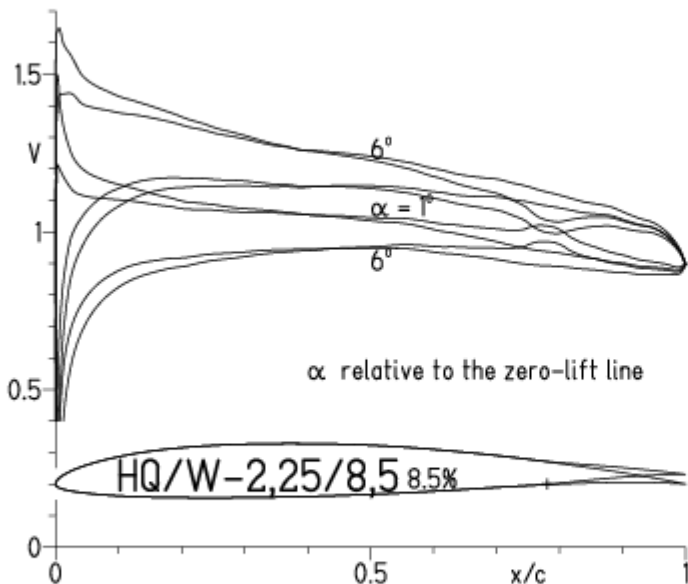
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

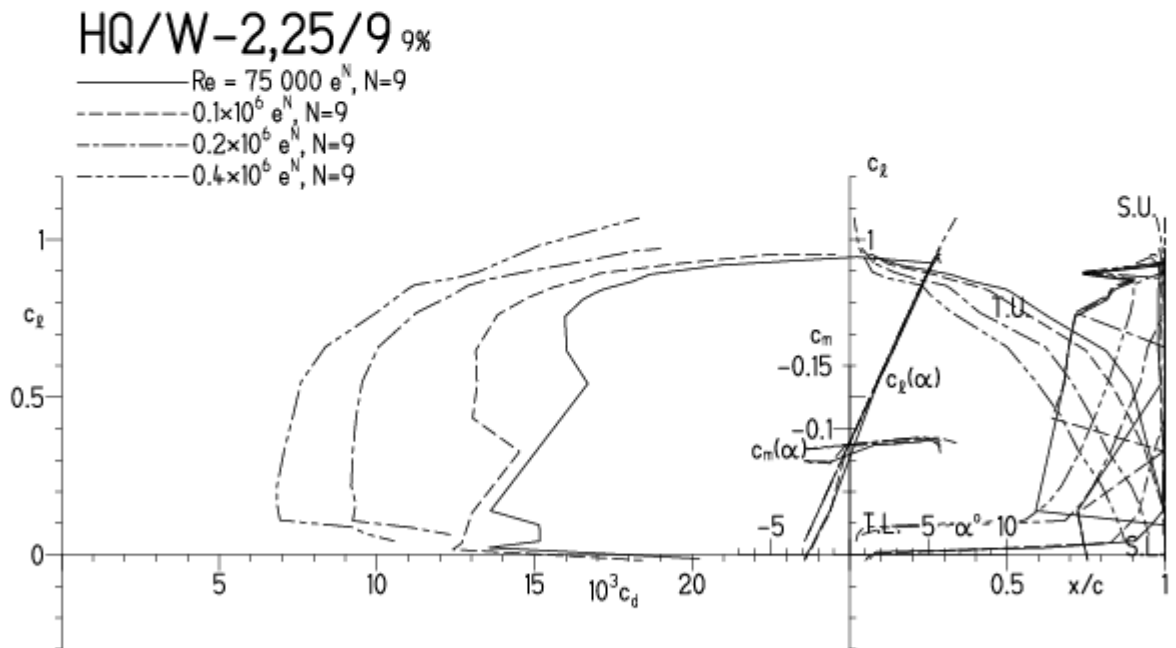


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

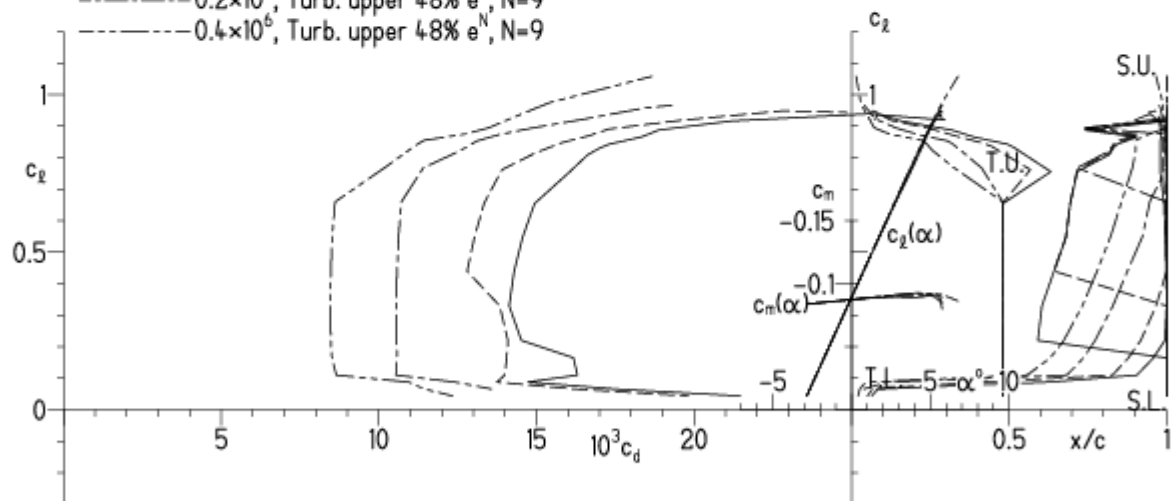
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

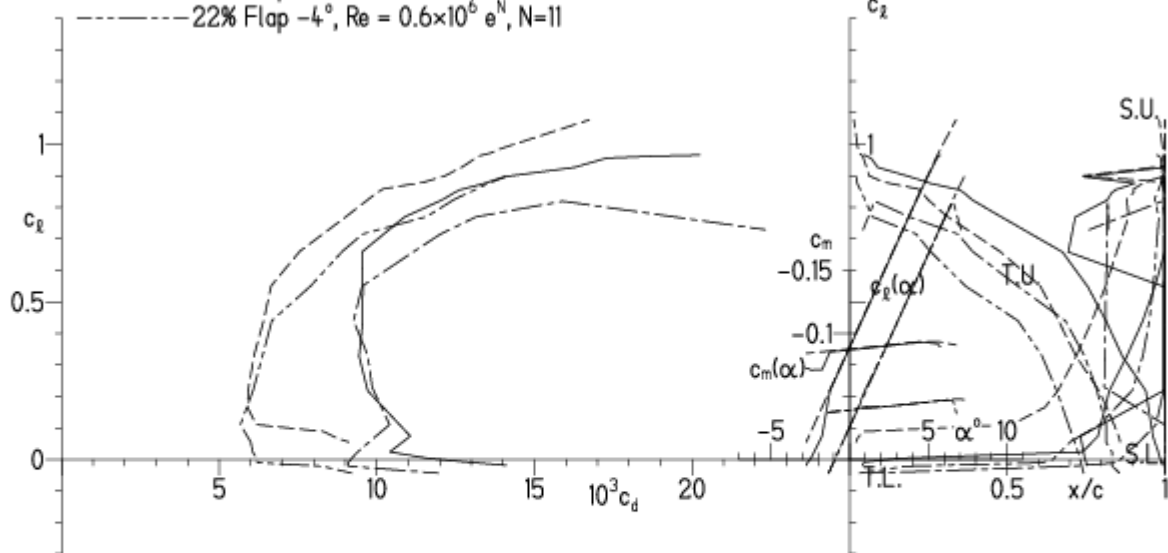
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

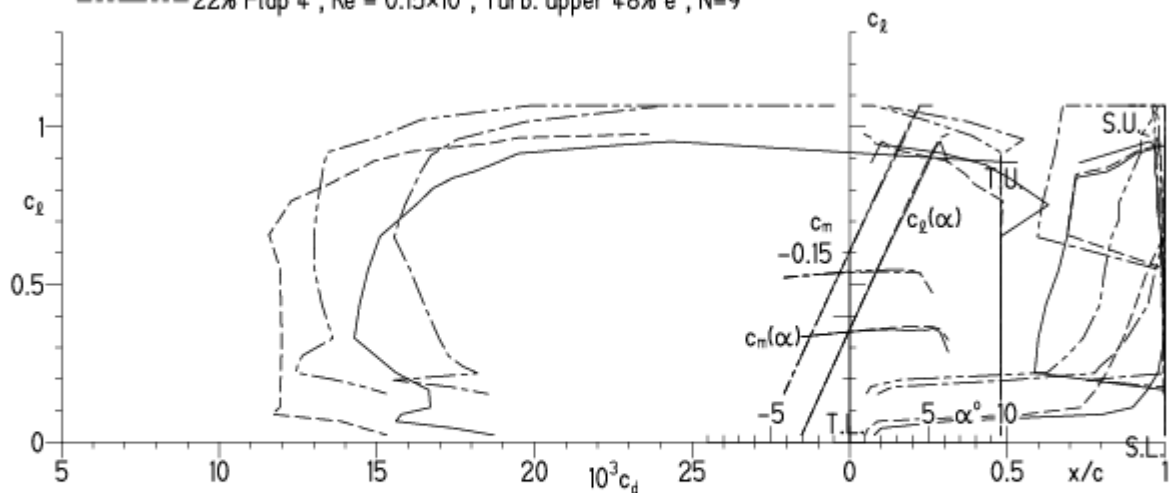


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



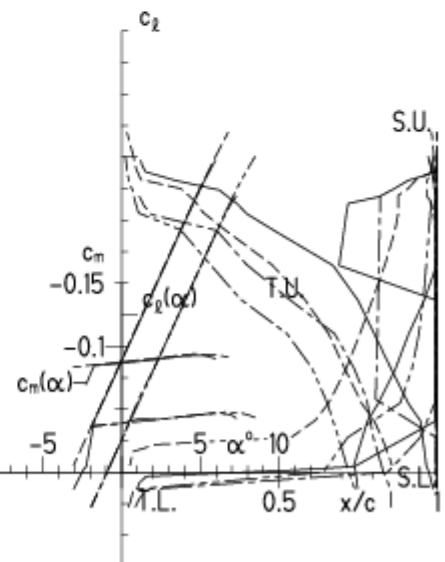
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

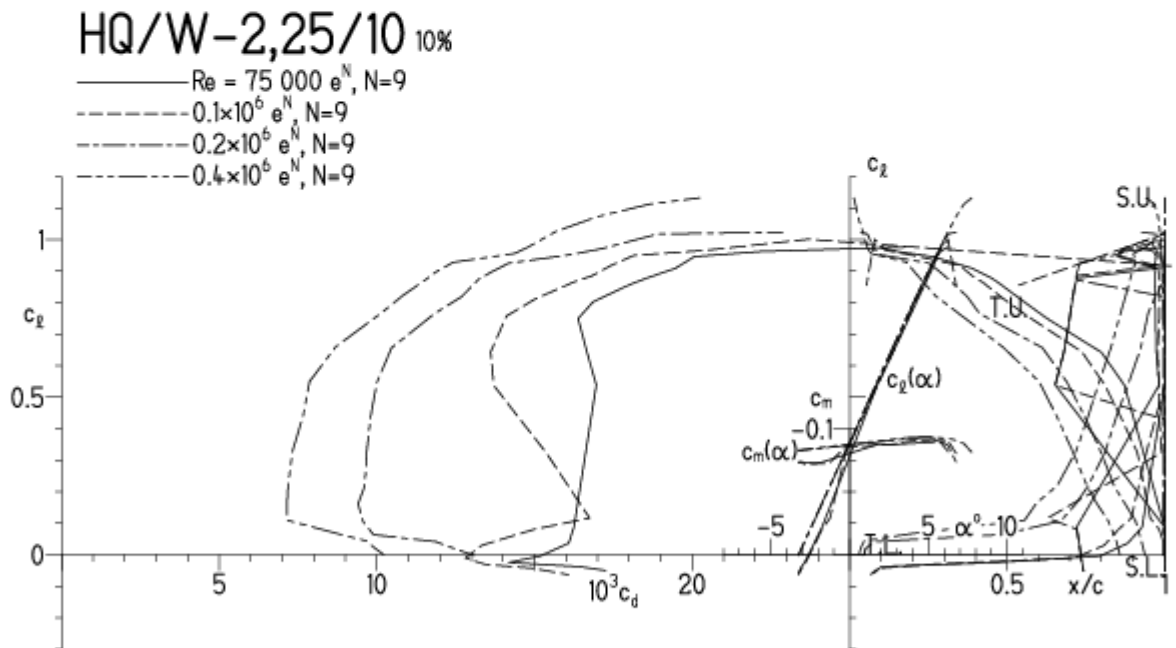


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

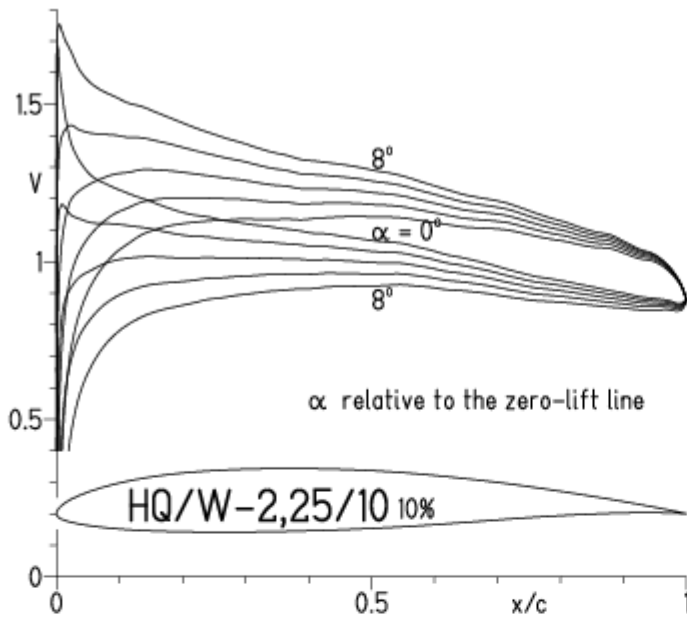


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

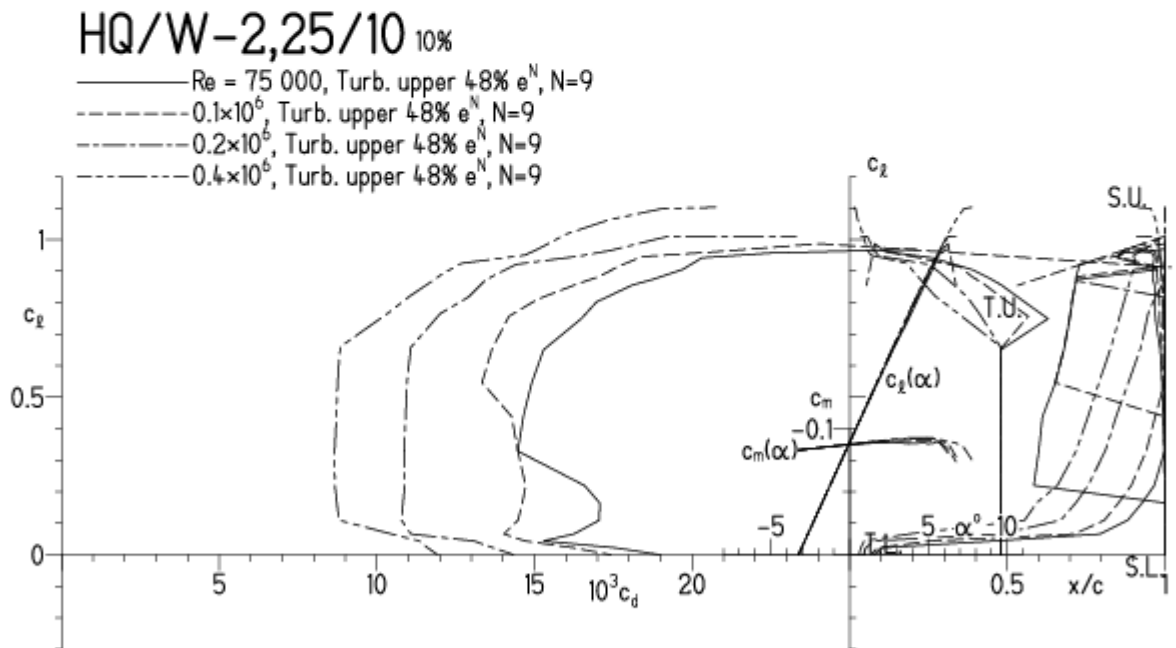


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

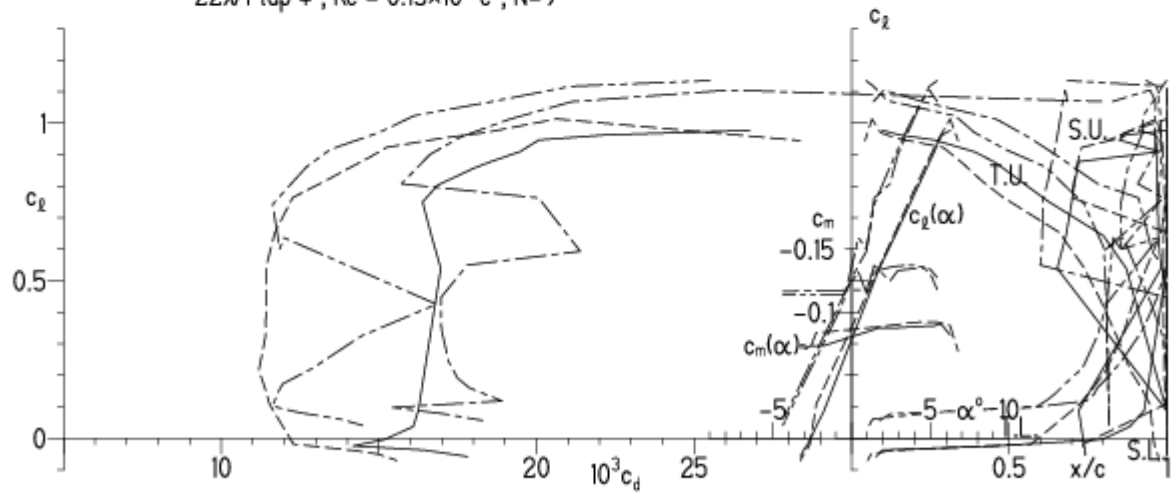


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

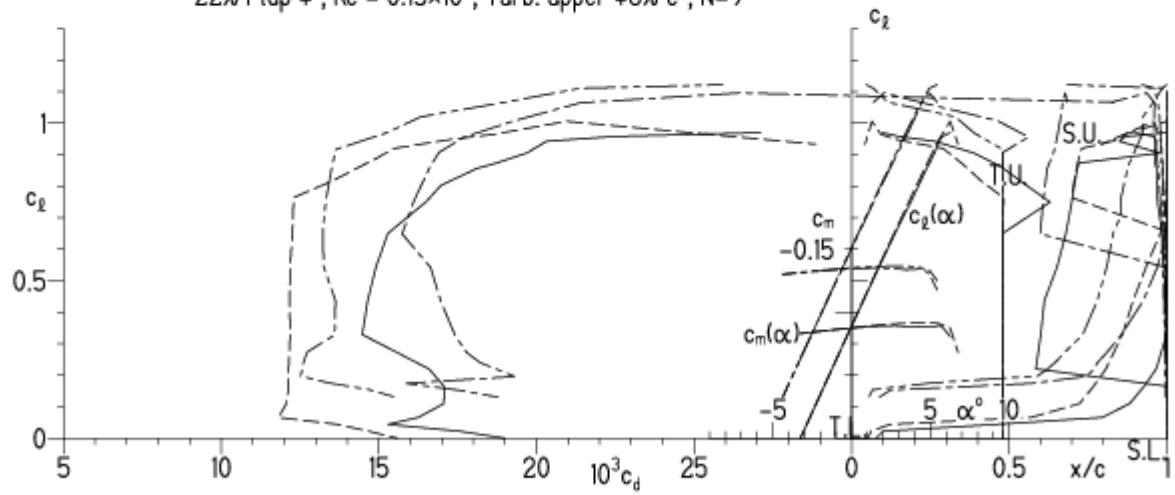


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

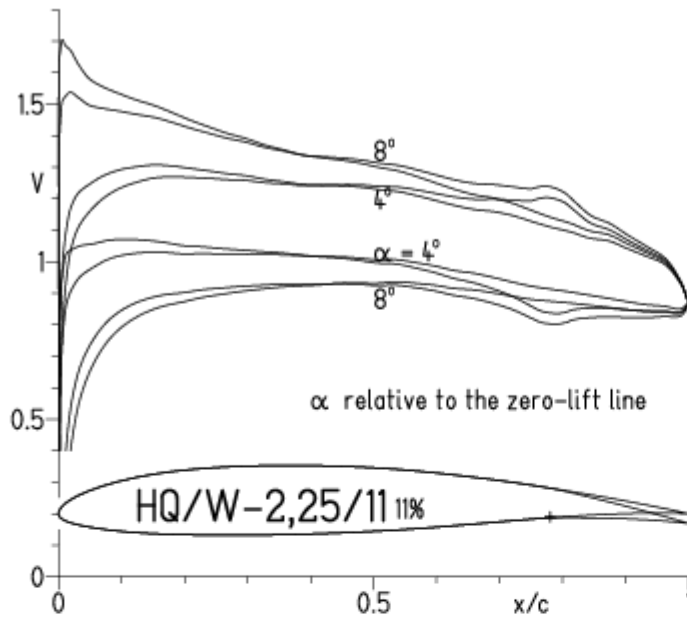
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

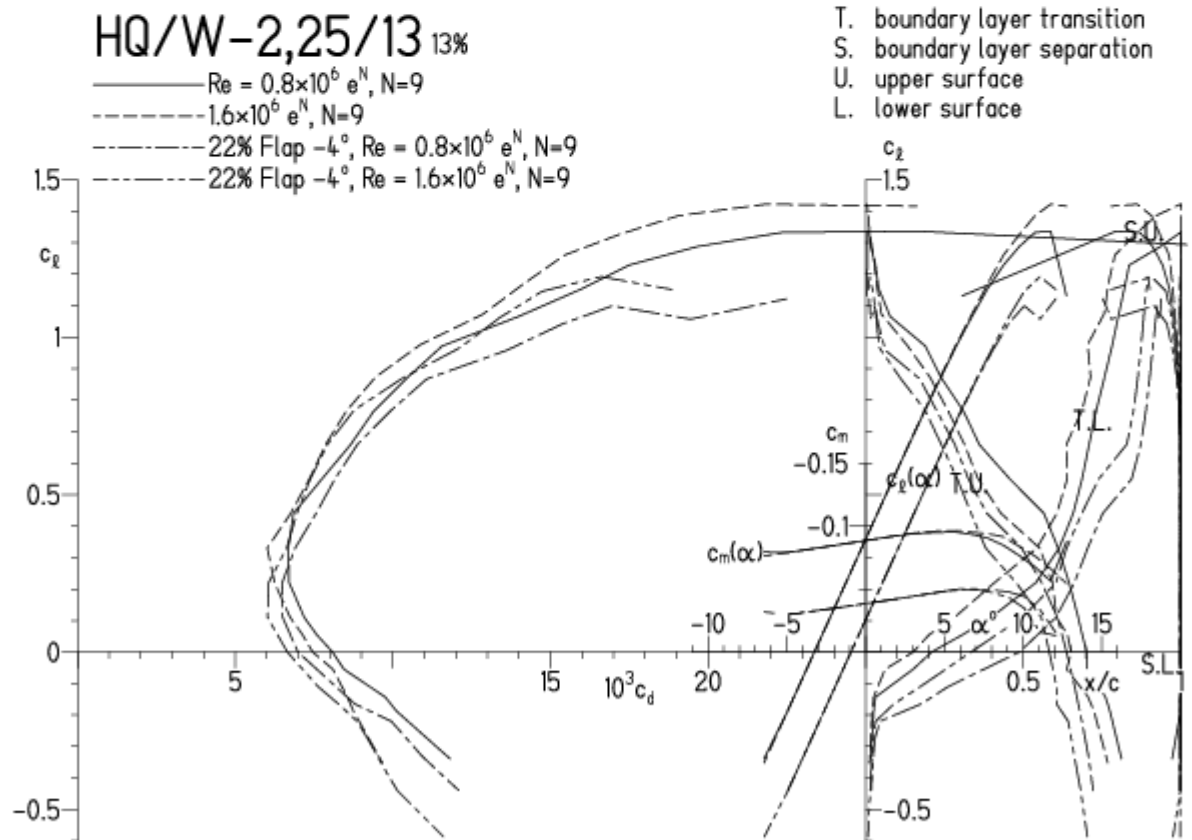


HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

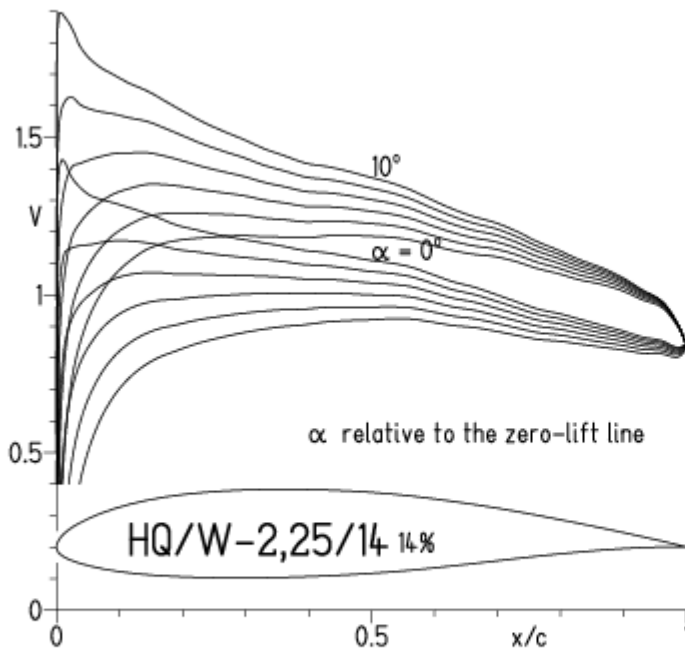


EPPLER 2005 V. 8.

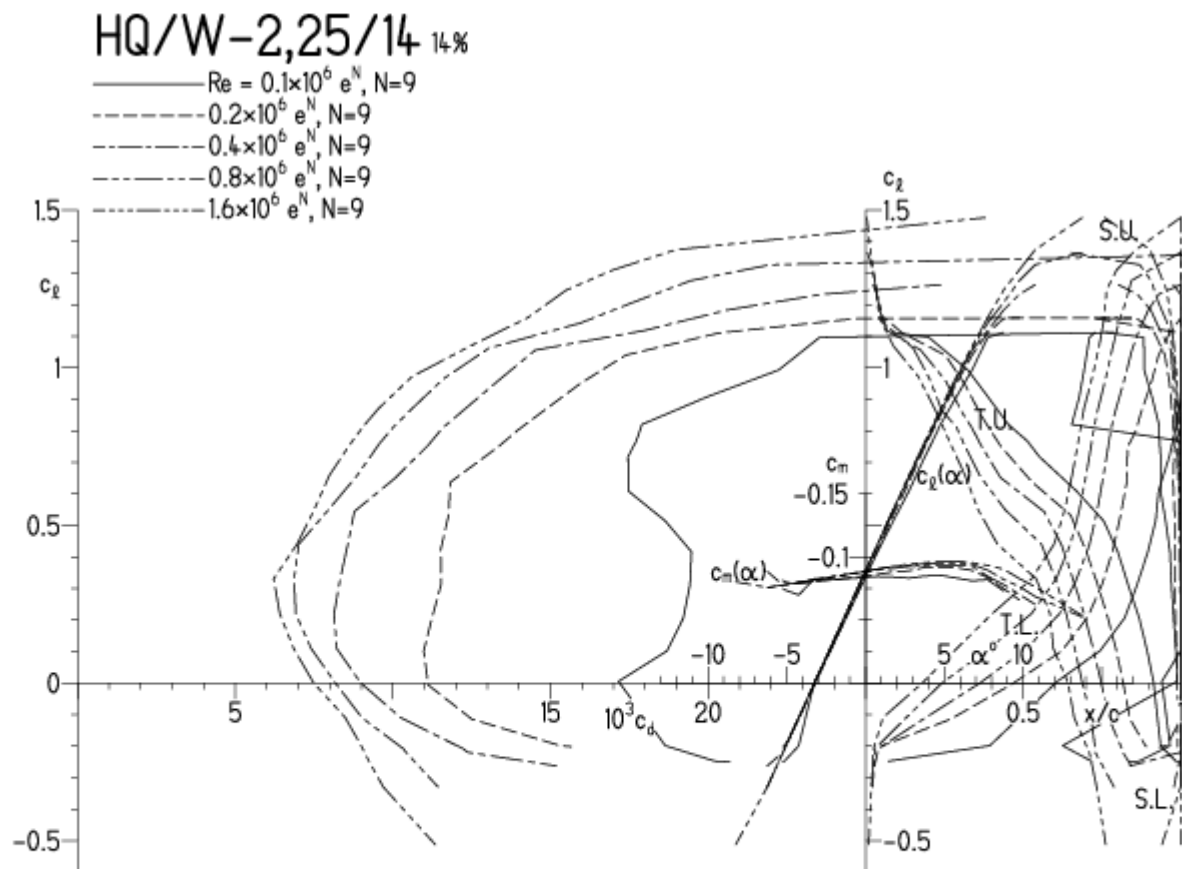


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

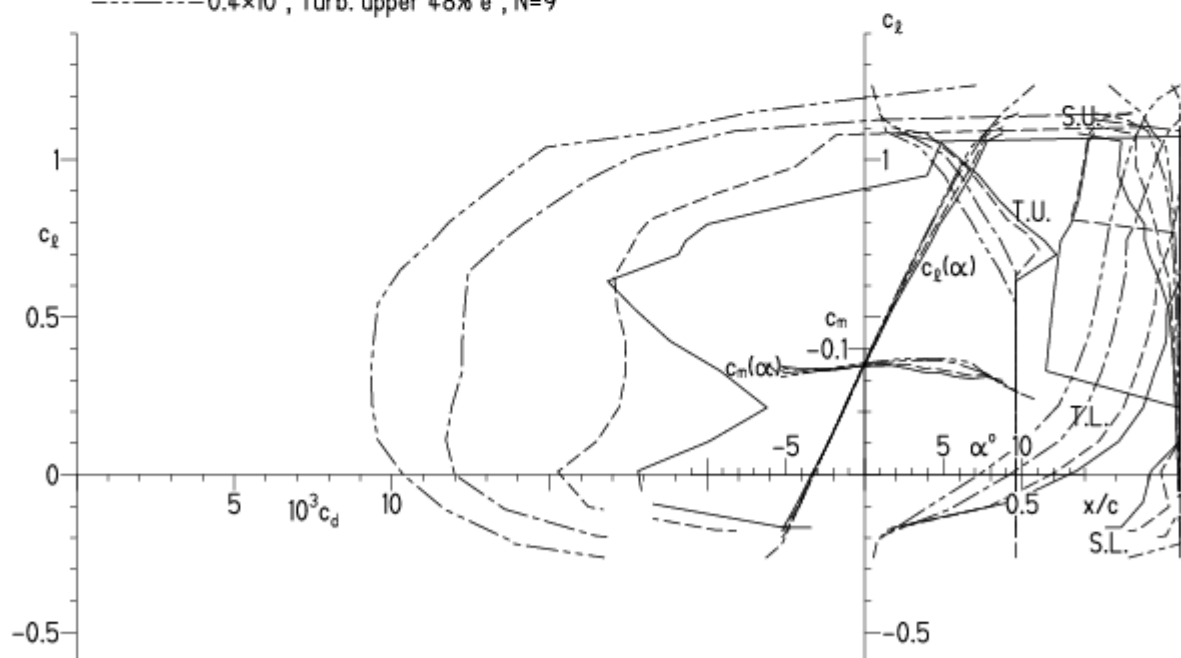
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

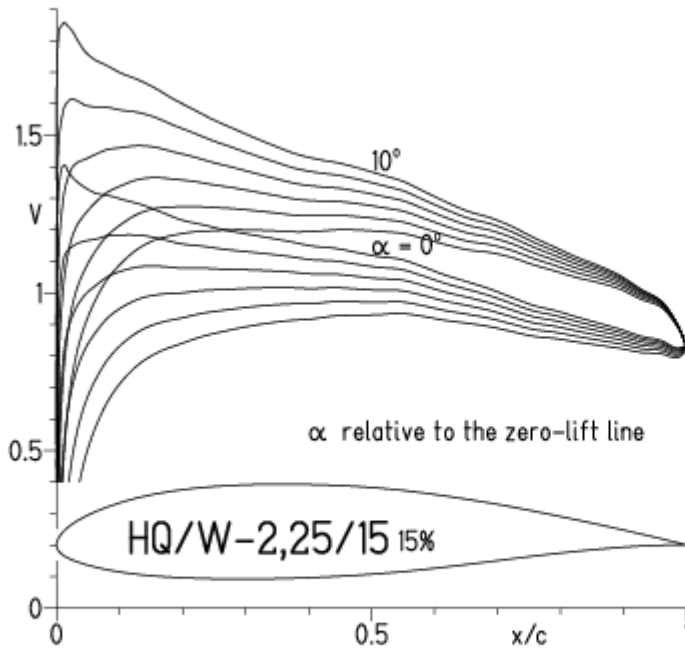


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

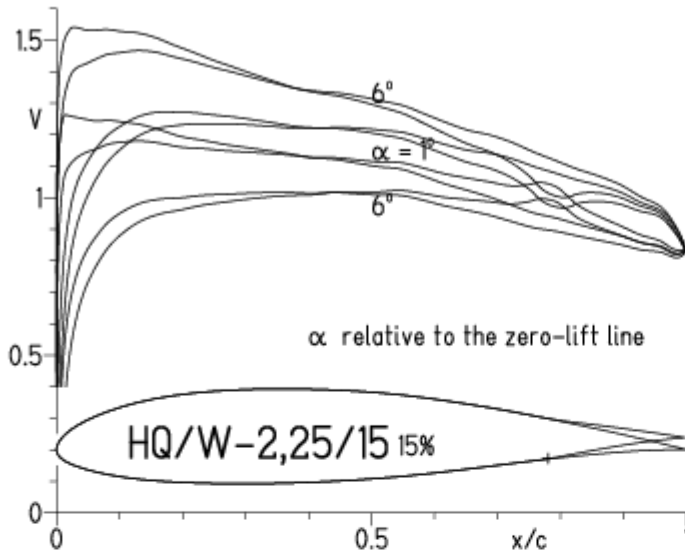


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

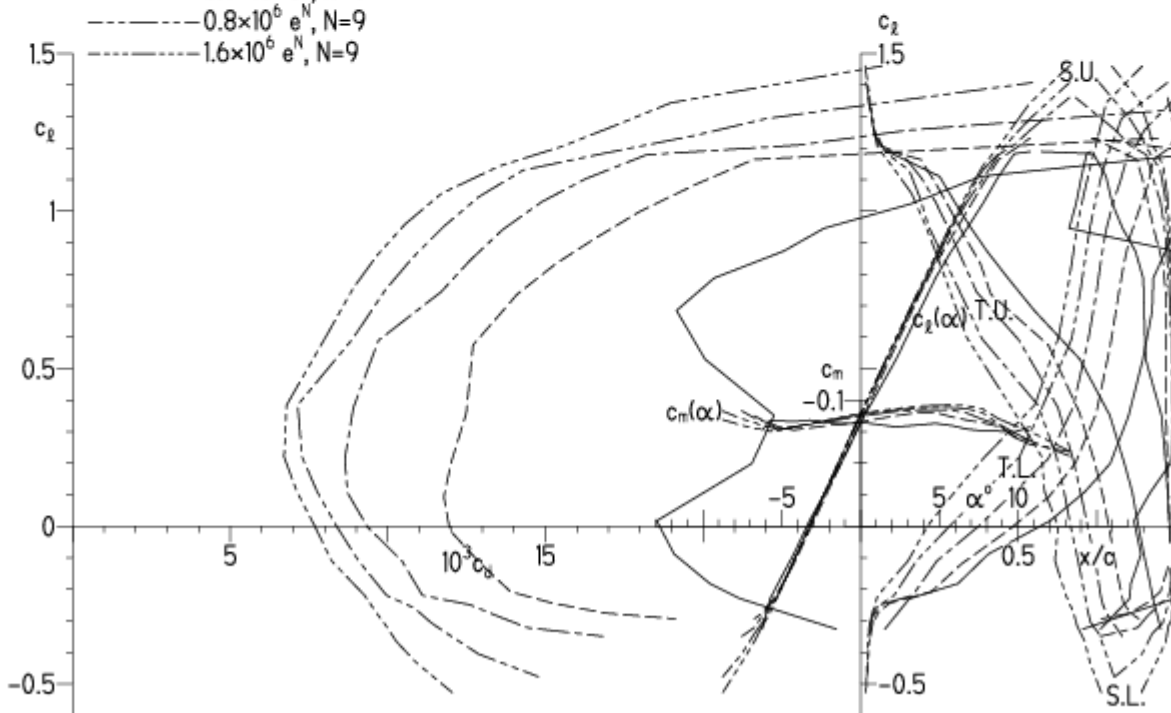
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

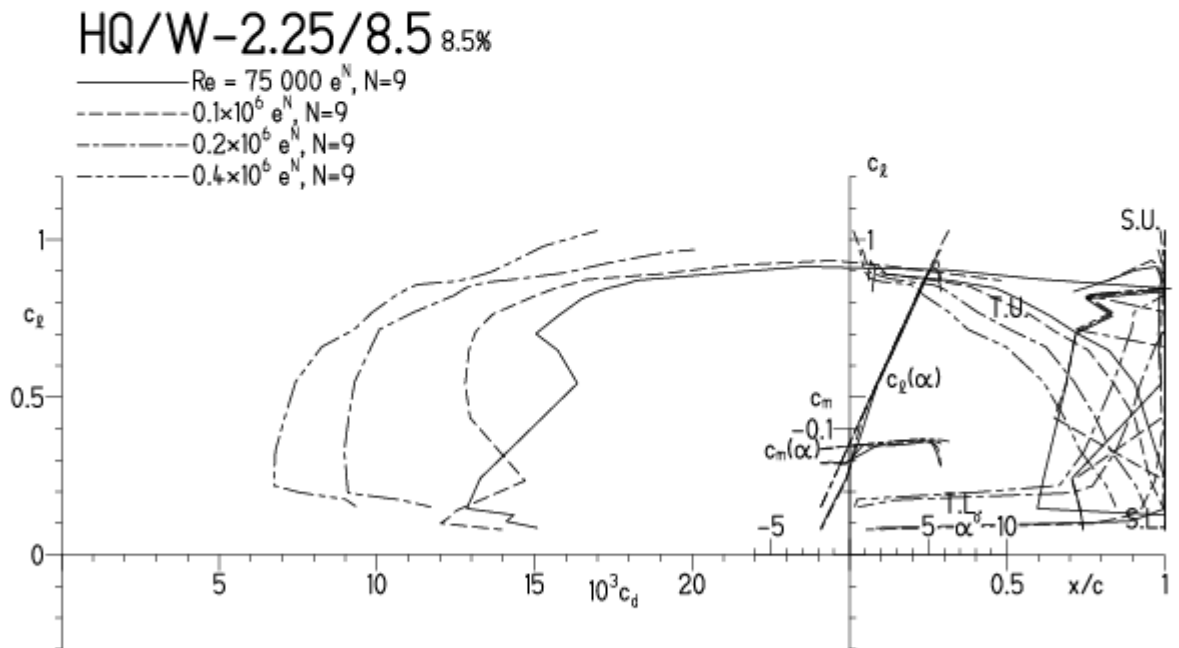


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

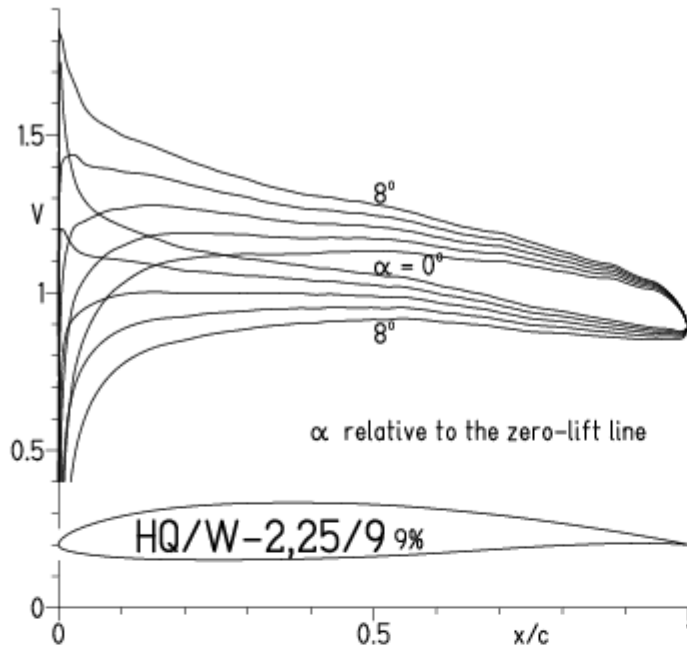


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

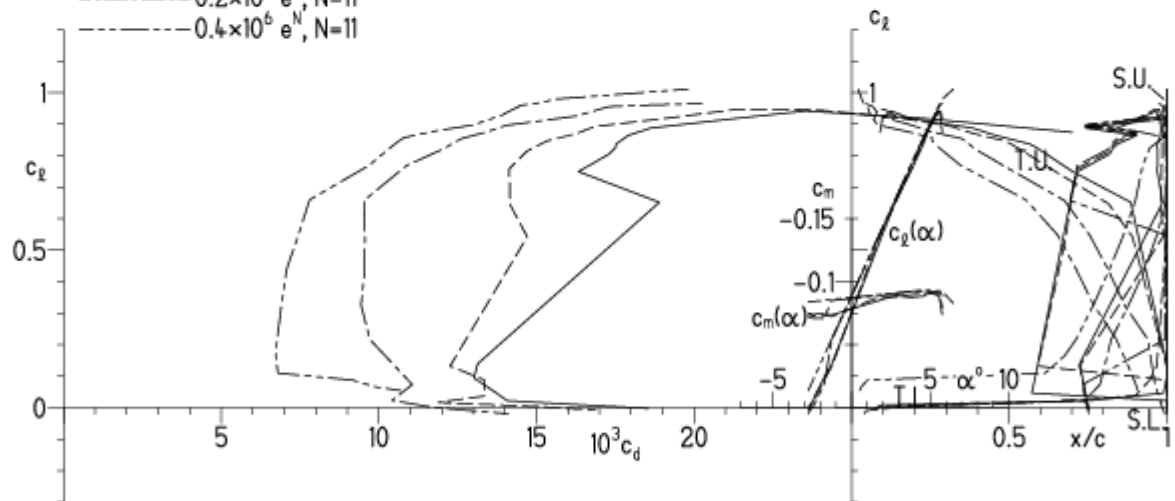
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$

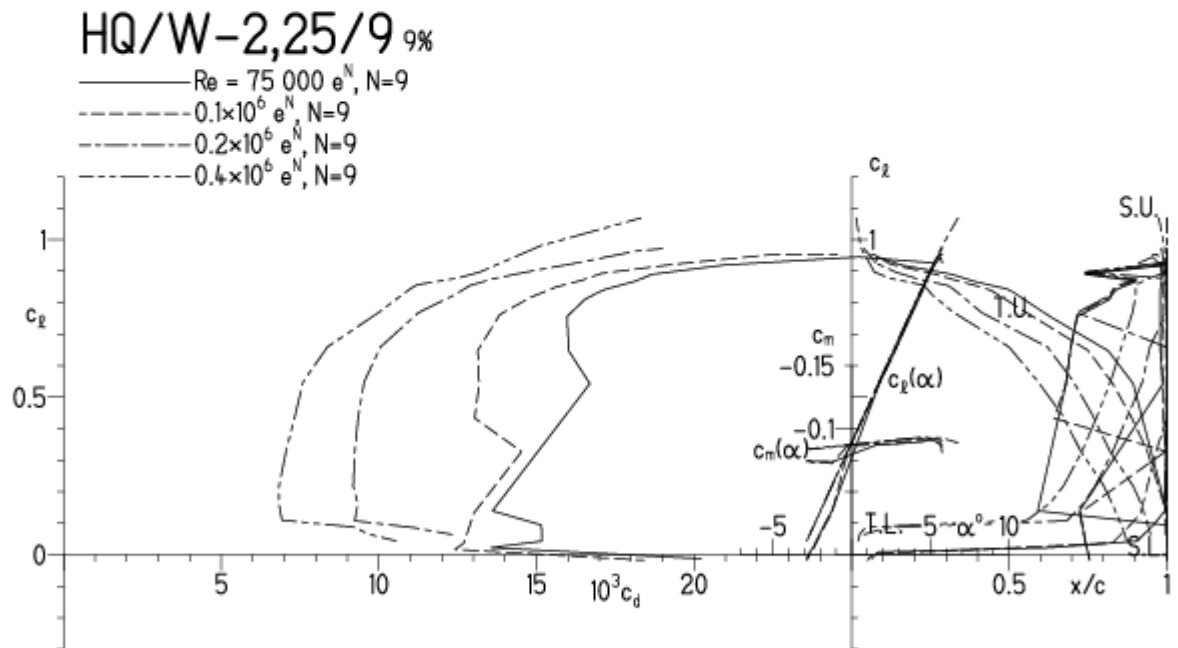


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08

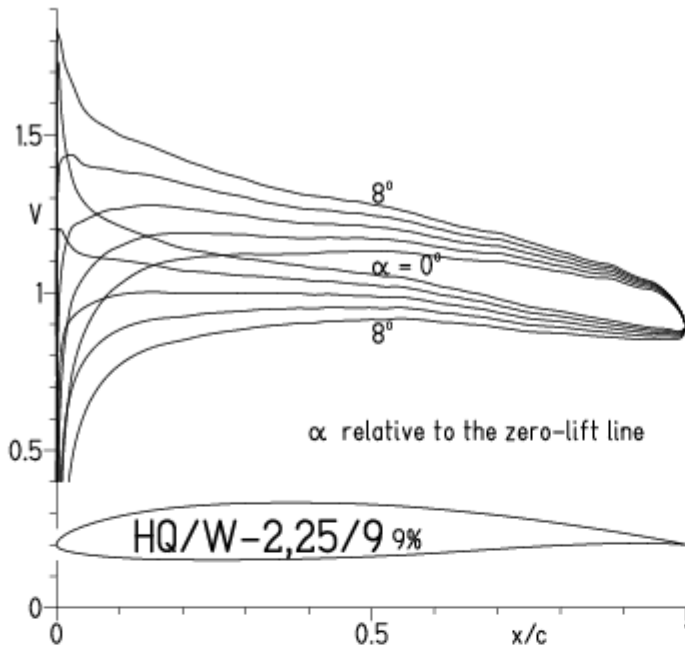


EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

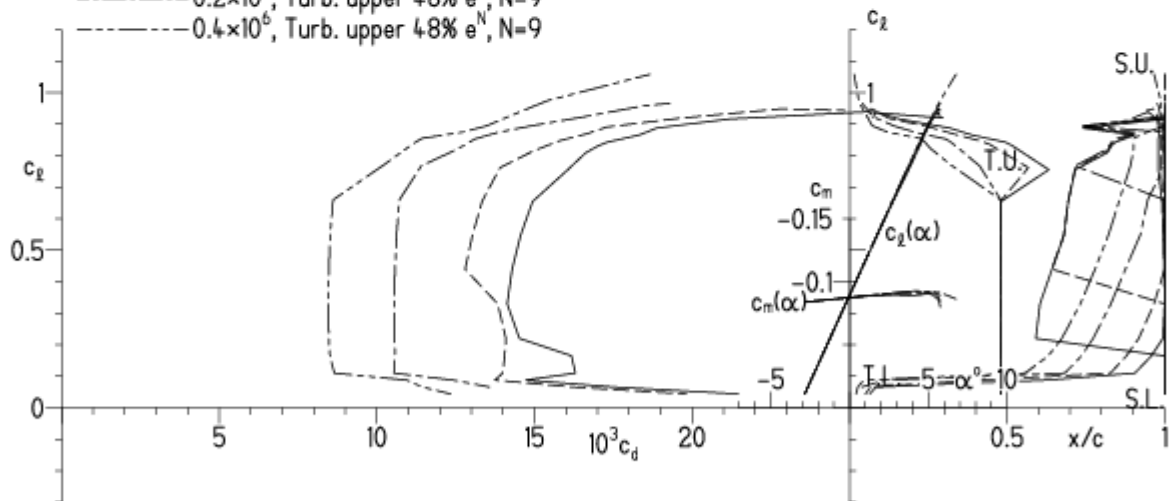
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

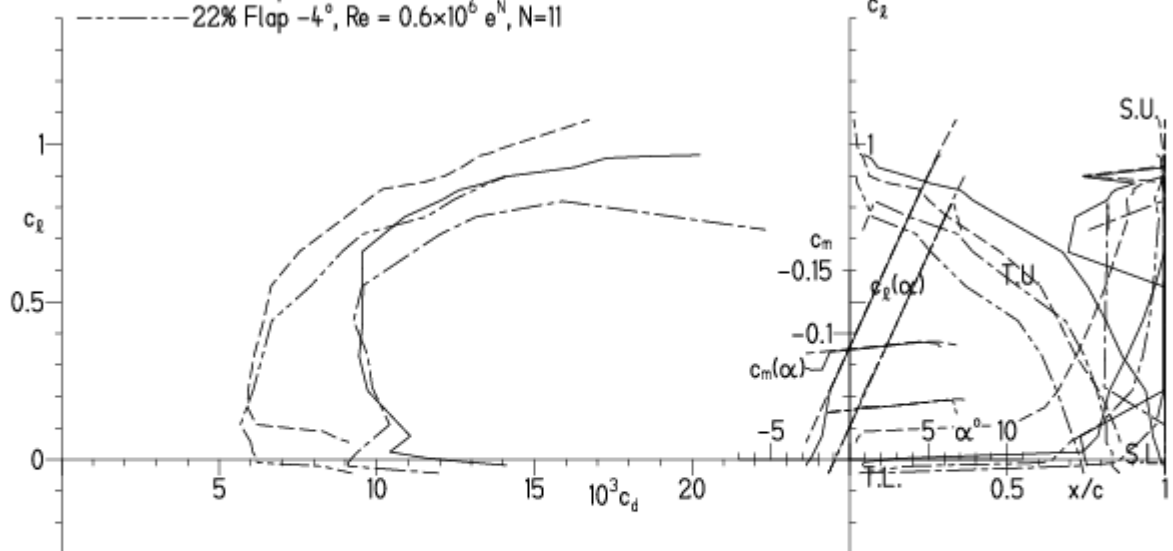
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

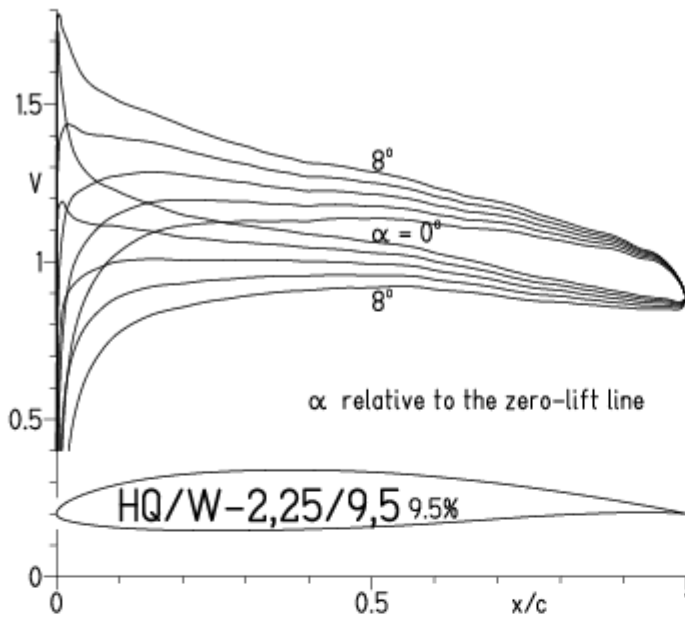
- Re = 0.2 × 10⁶ e^N, N=11
- - - 0.6 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.2 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.6 × 10⁶ e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



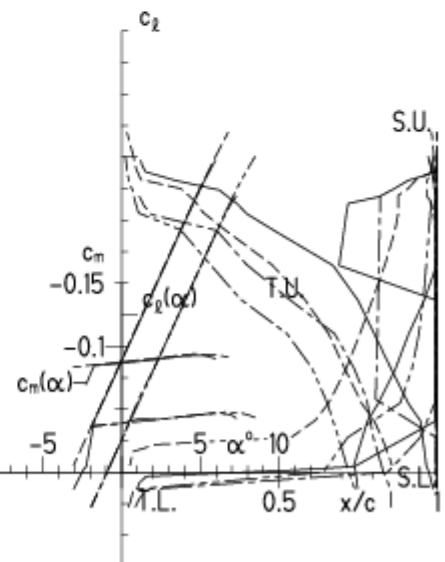
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

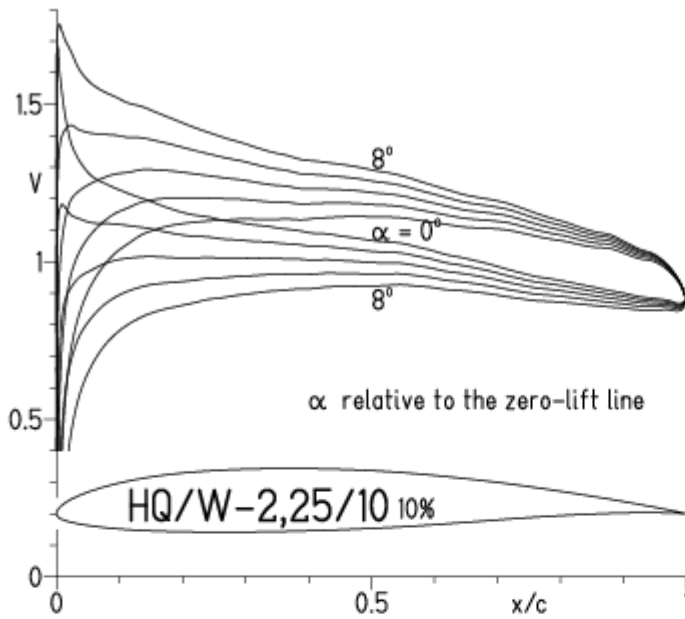


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

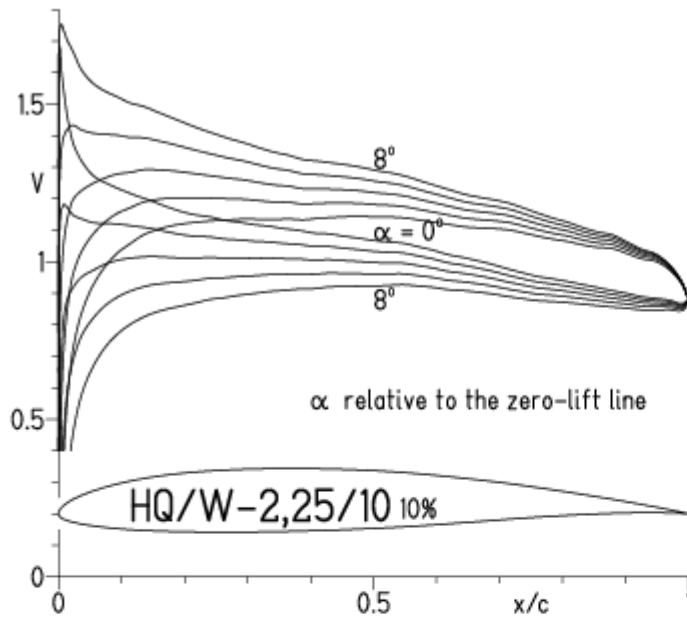


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

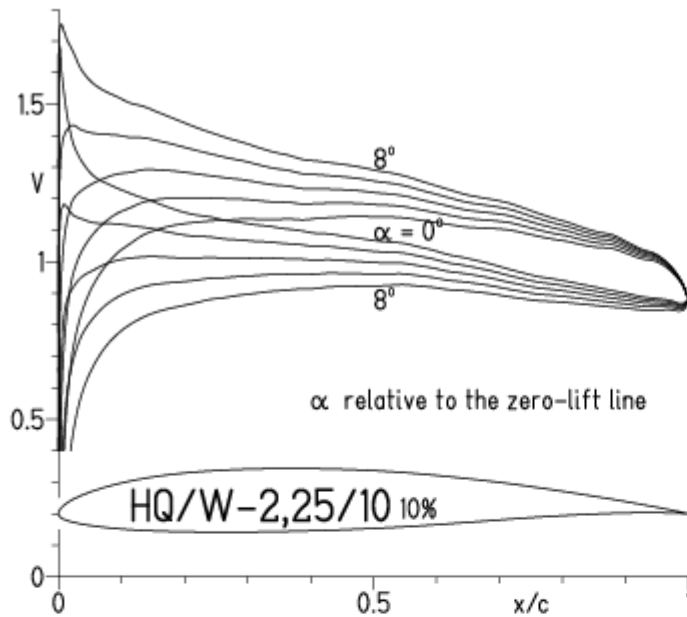


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

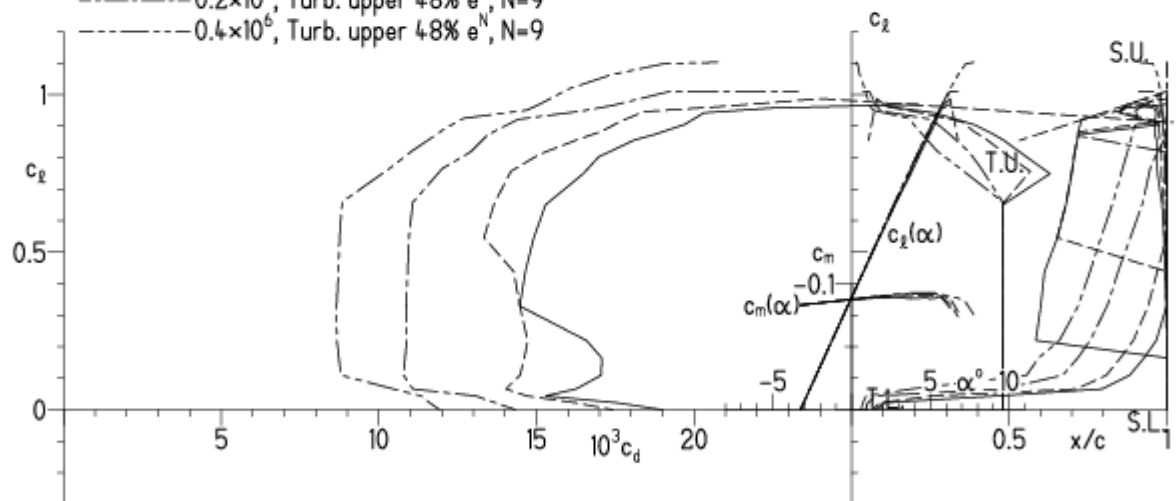
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

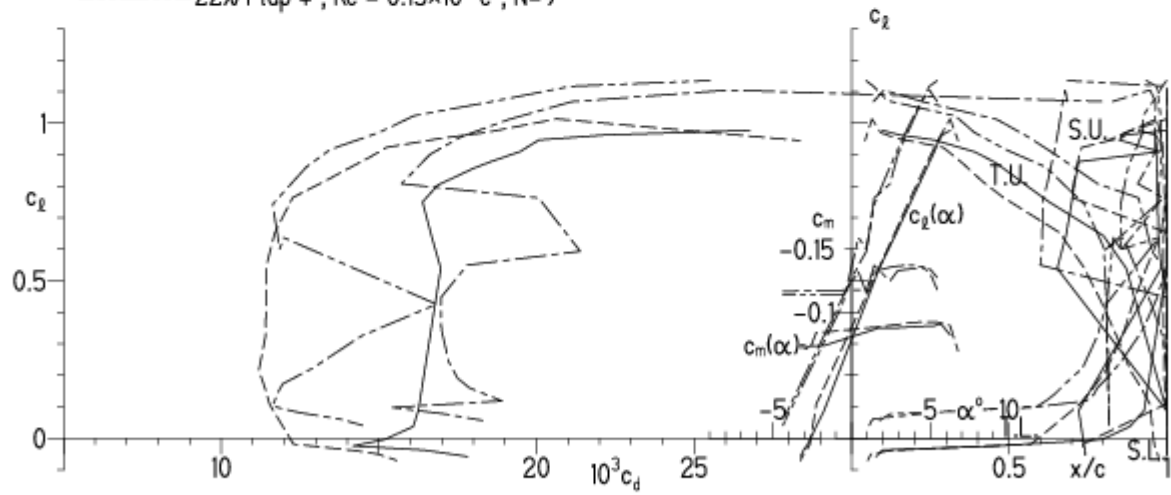


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

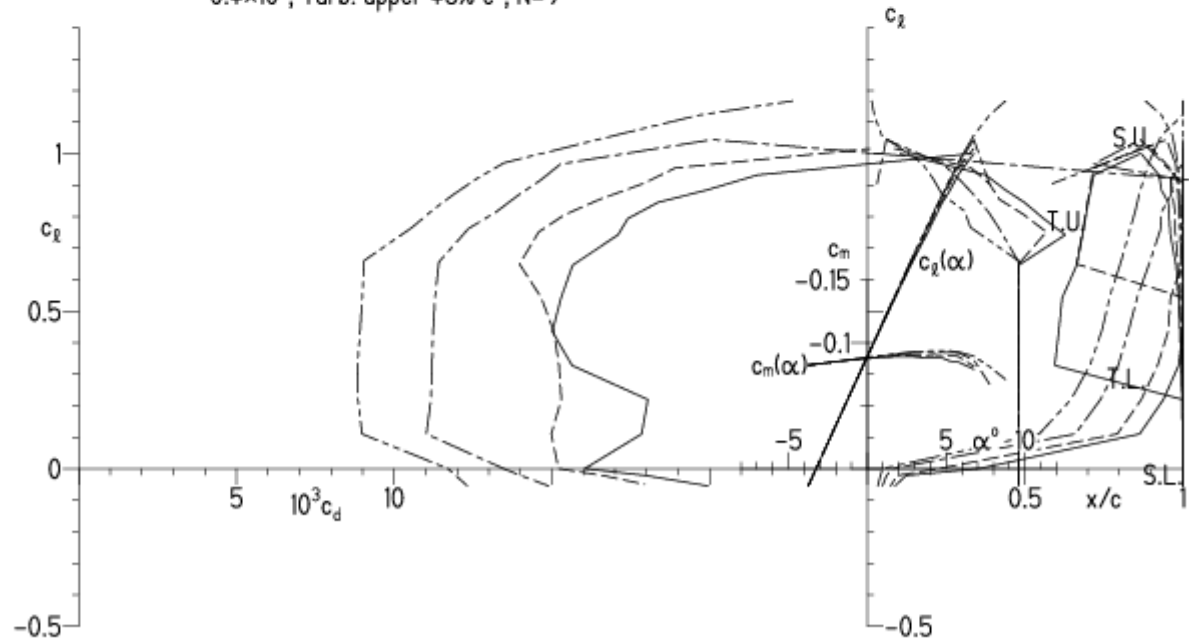
EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

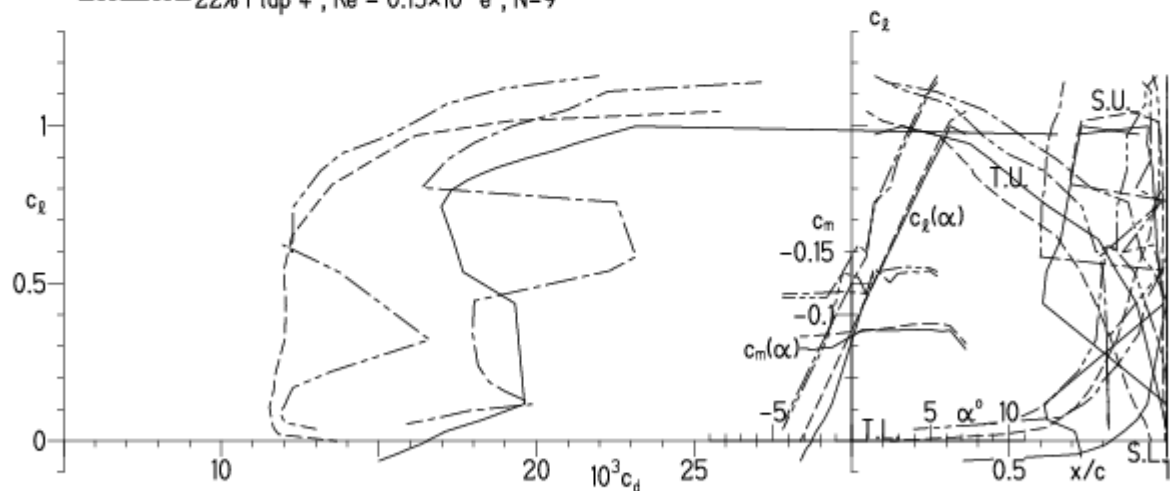


EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

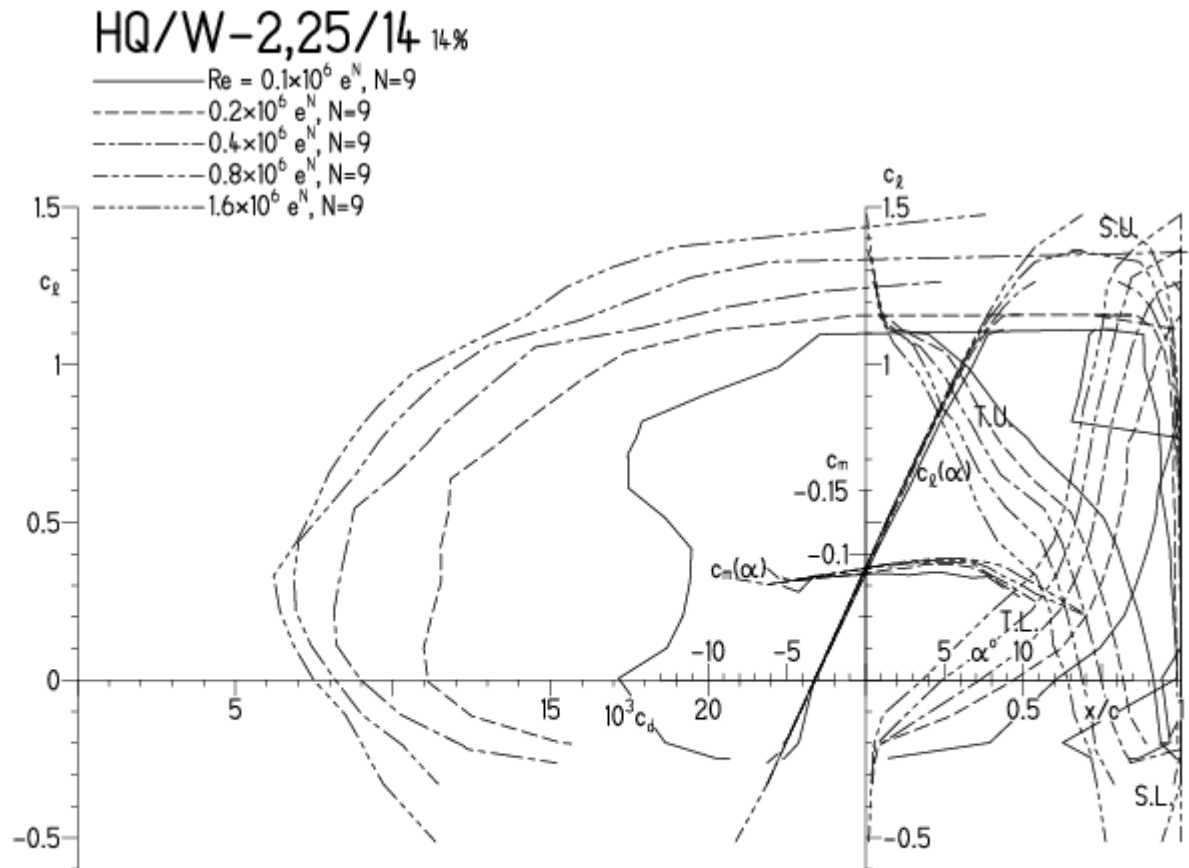


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

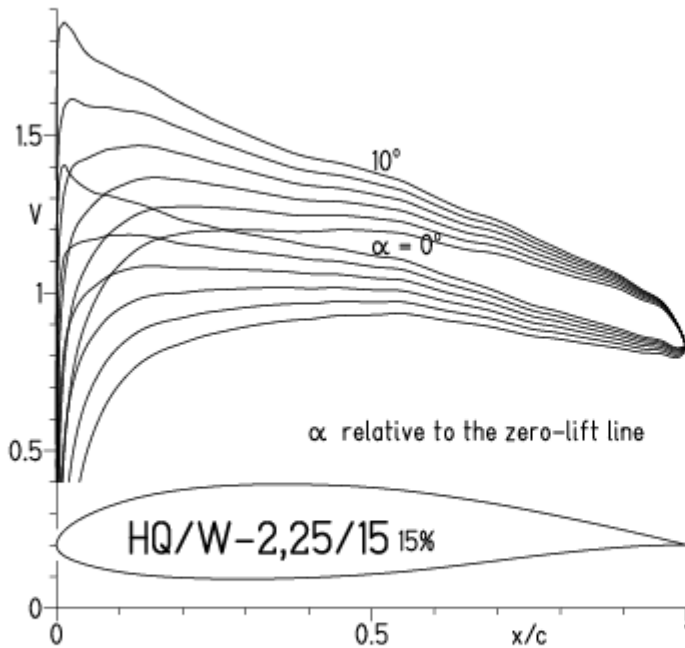


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

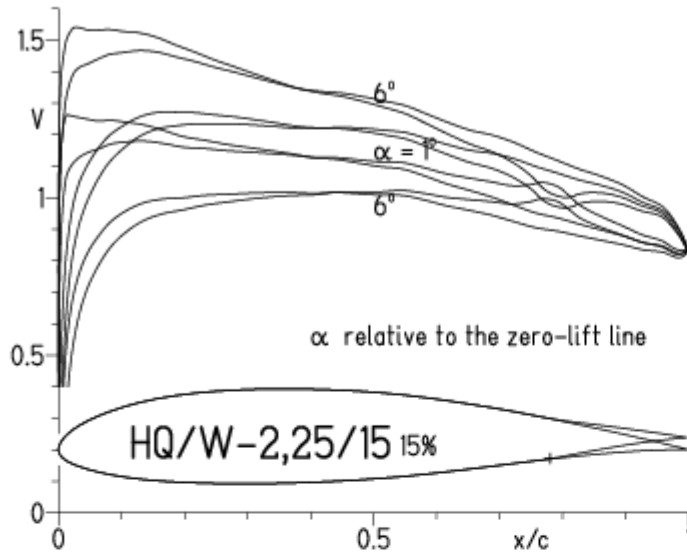


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



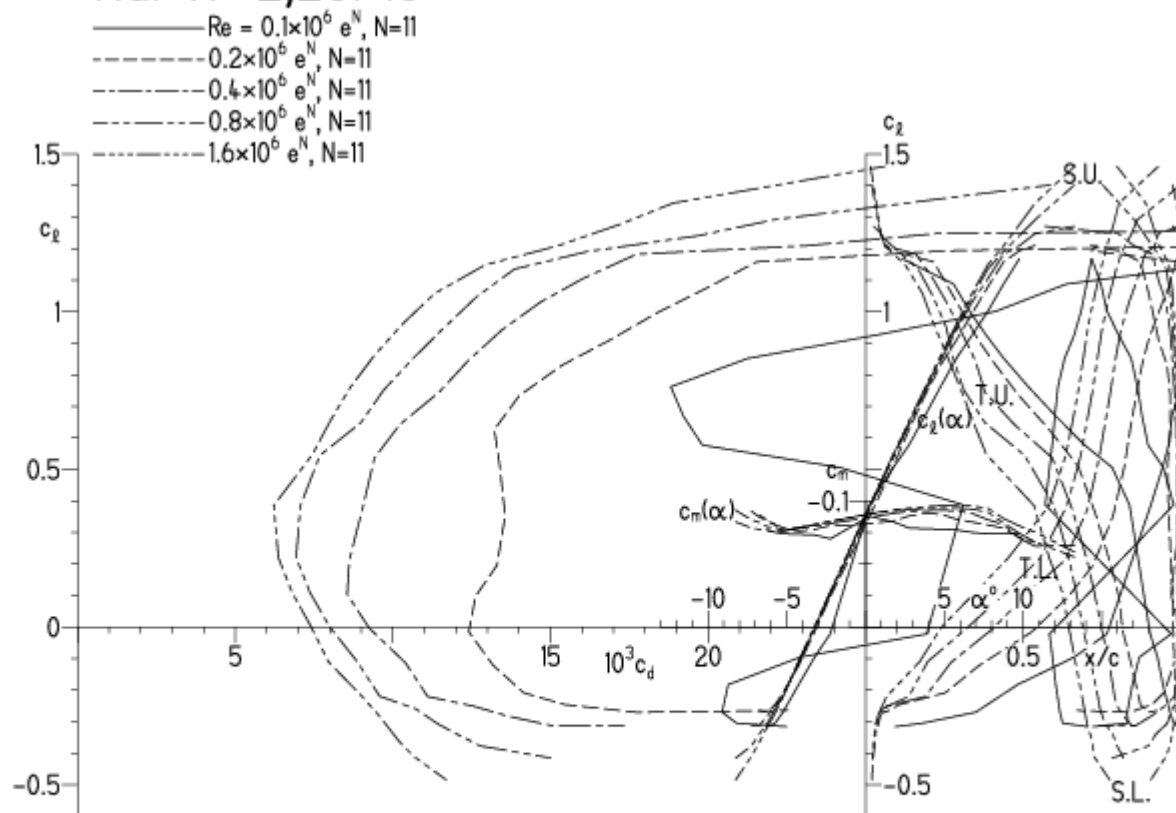
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

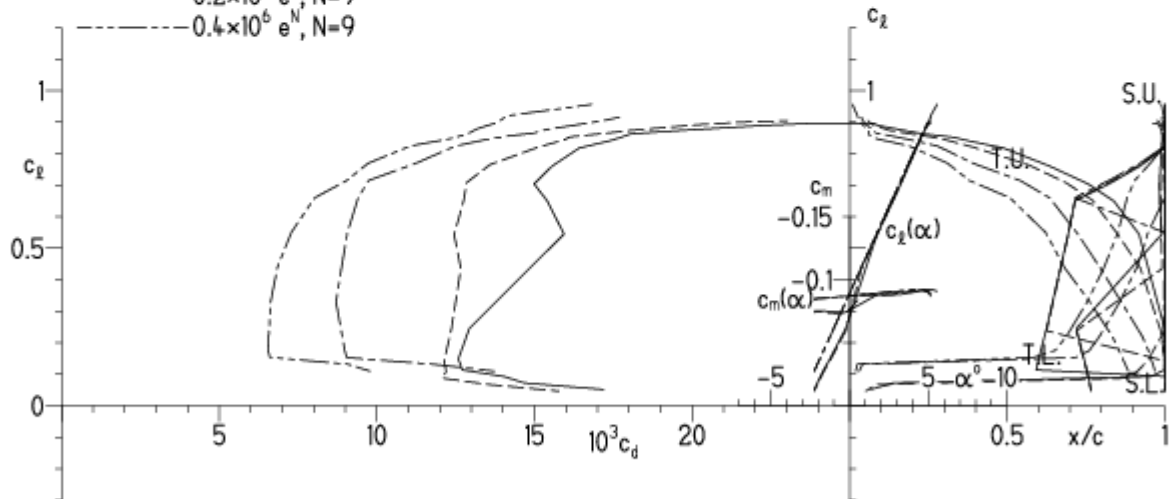
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23

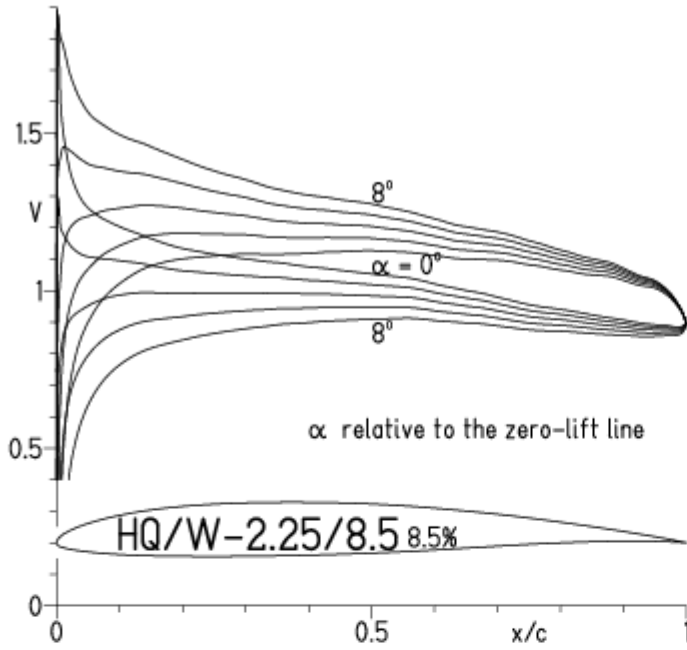


EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

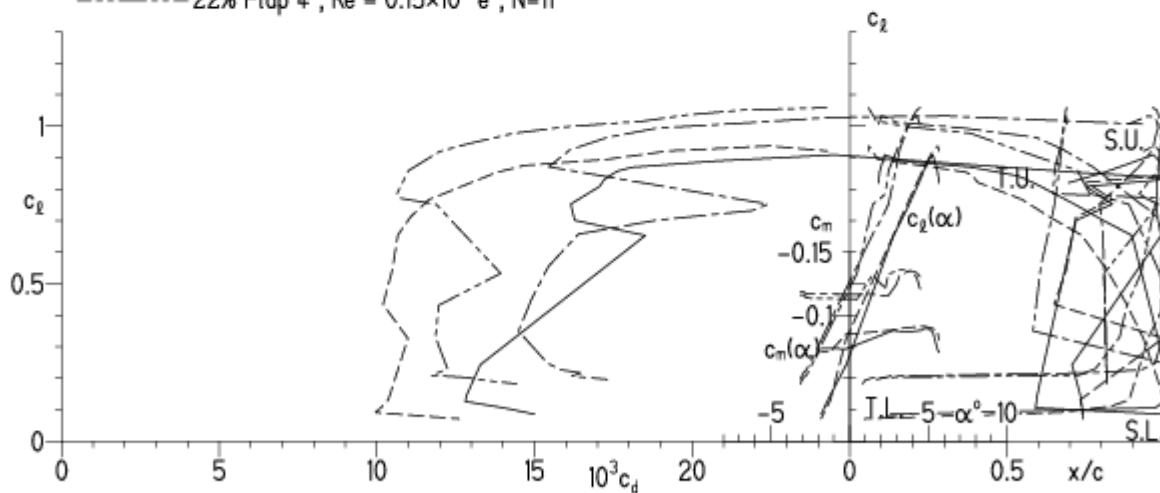


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

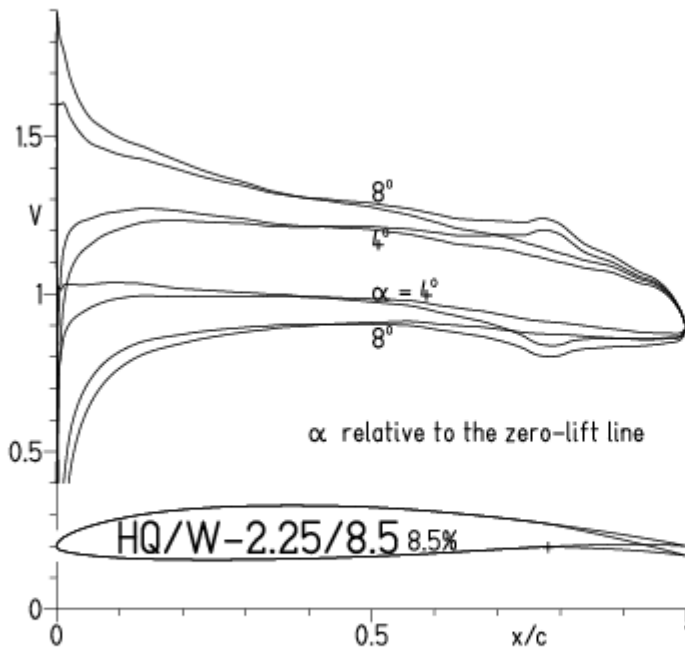
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

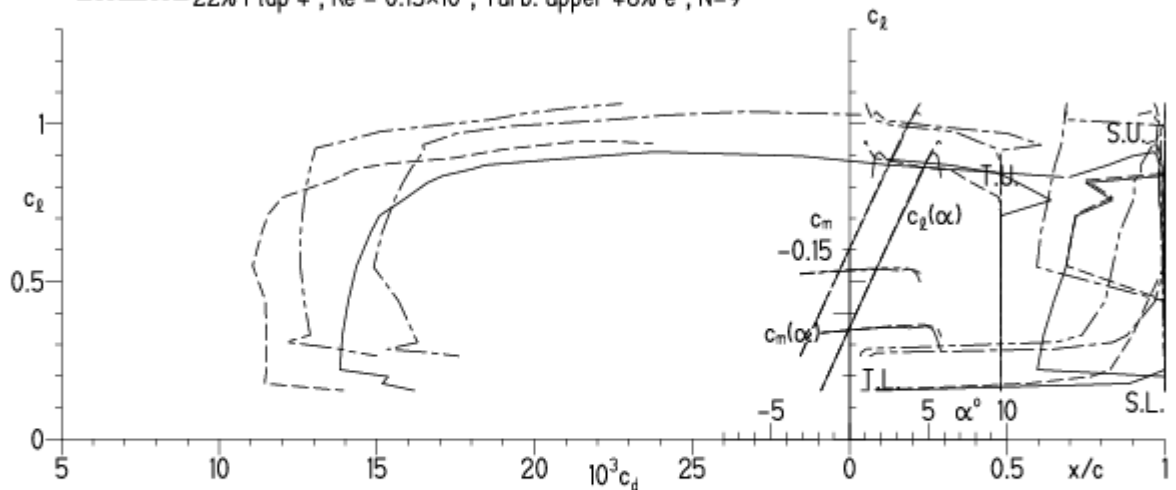


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15 × 10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

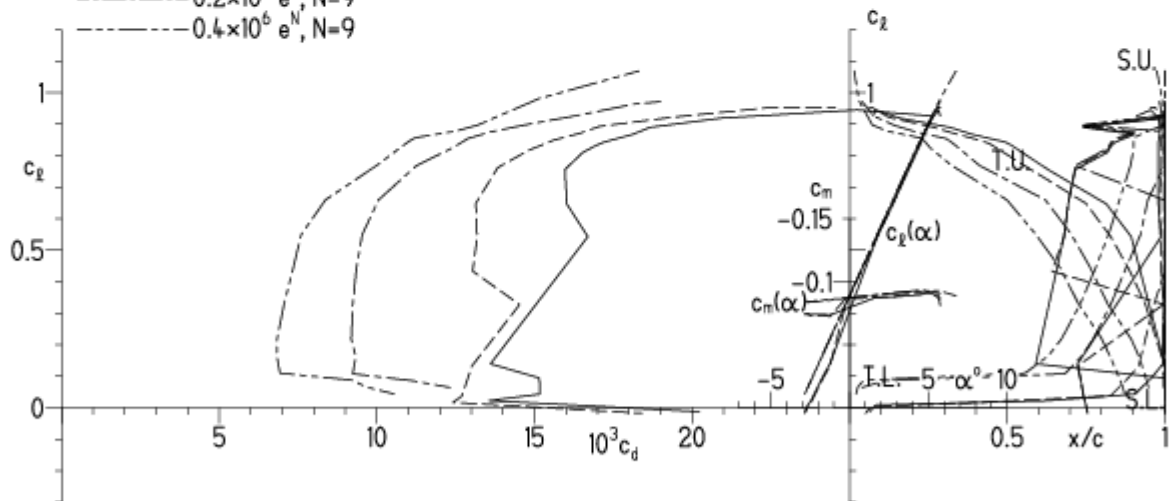
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

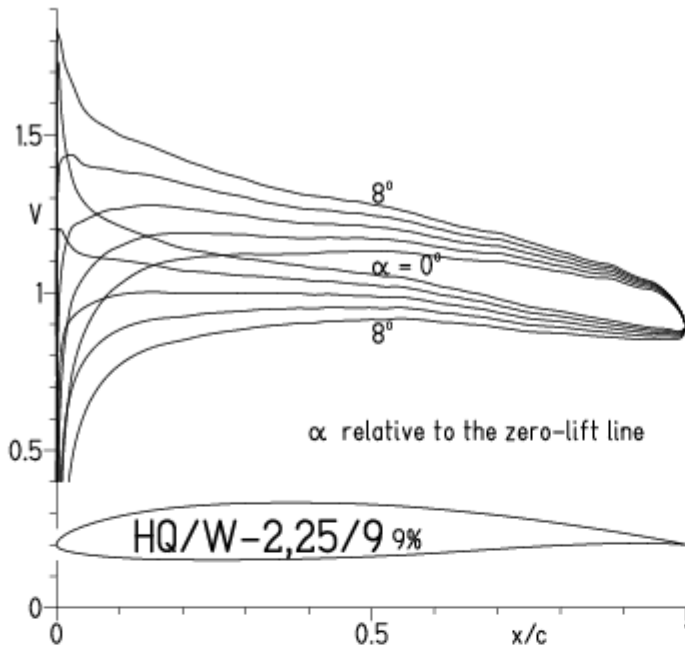
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

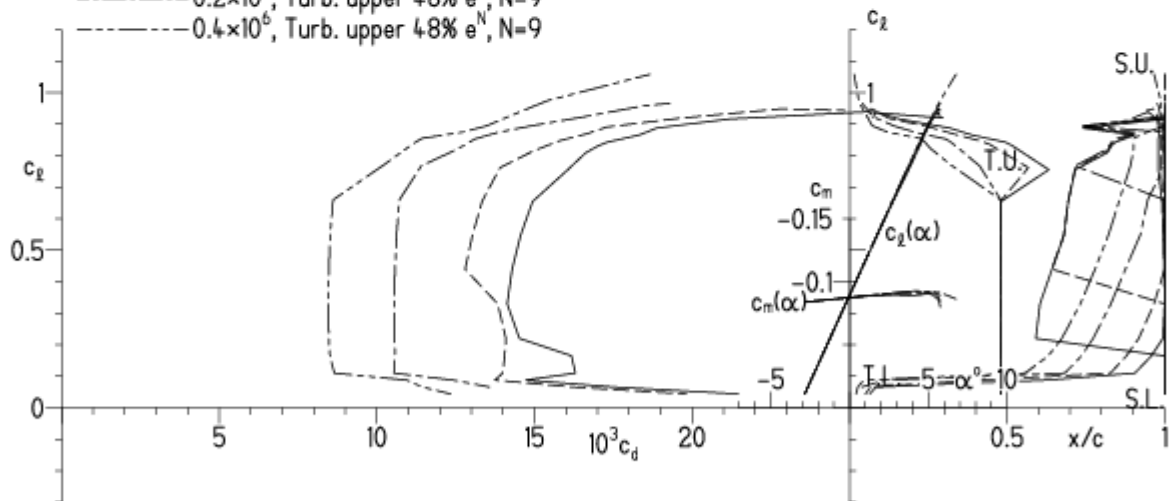
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

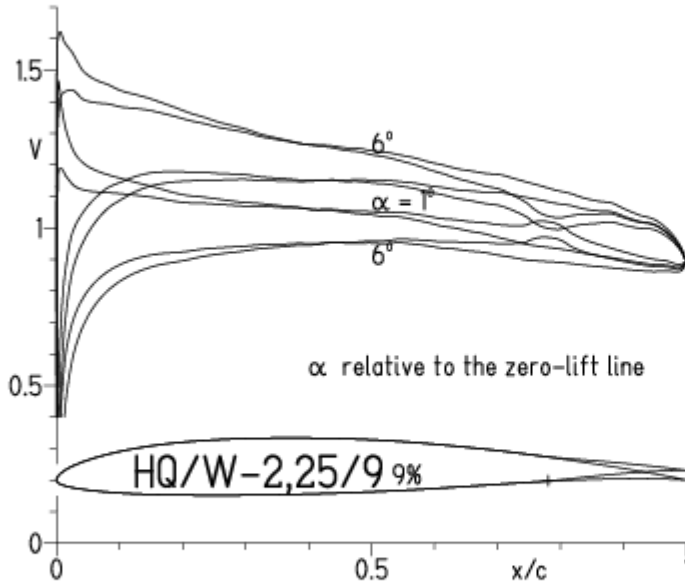
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

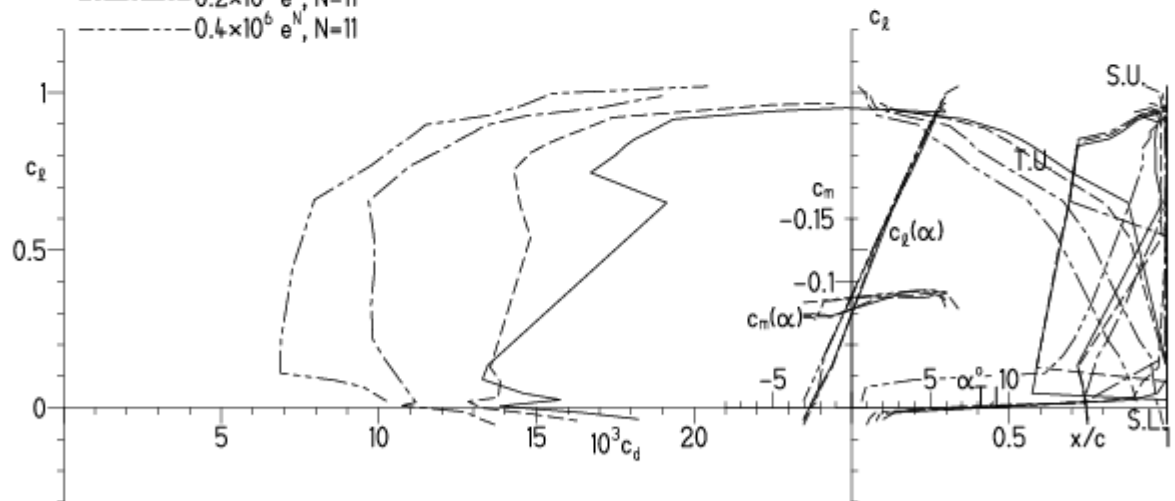
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
(Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

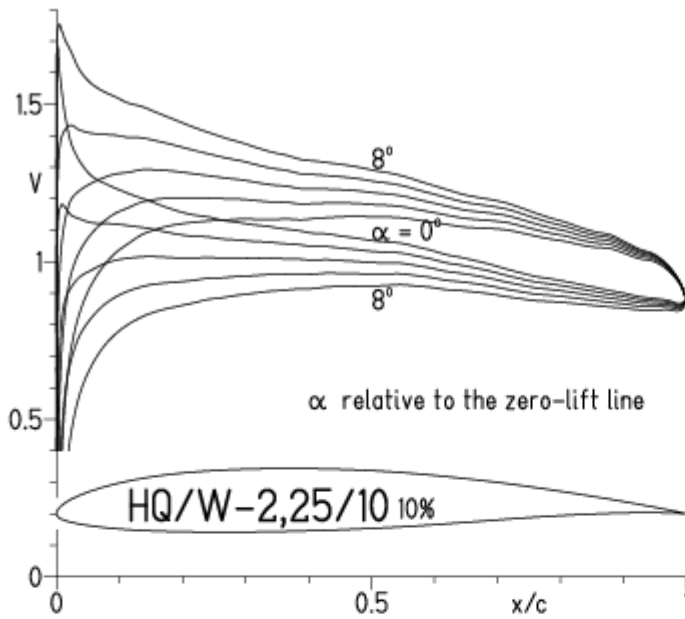


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

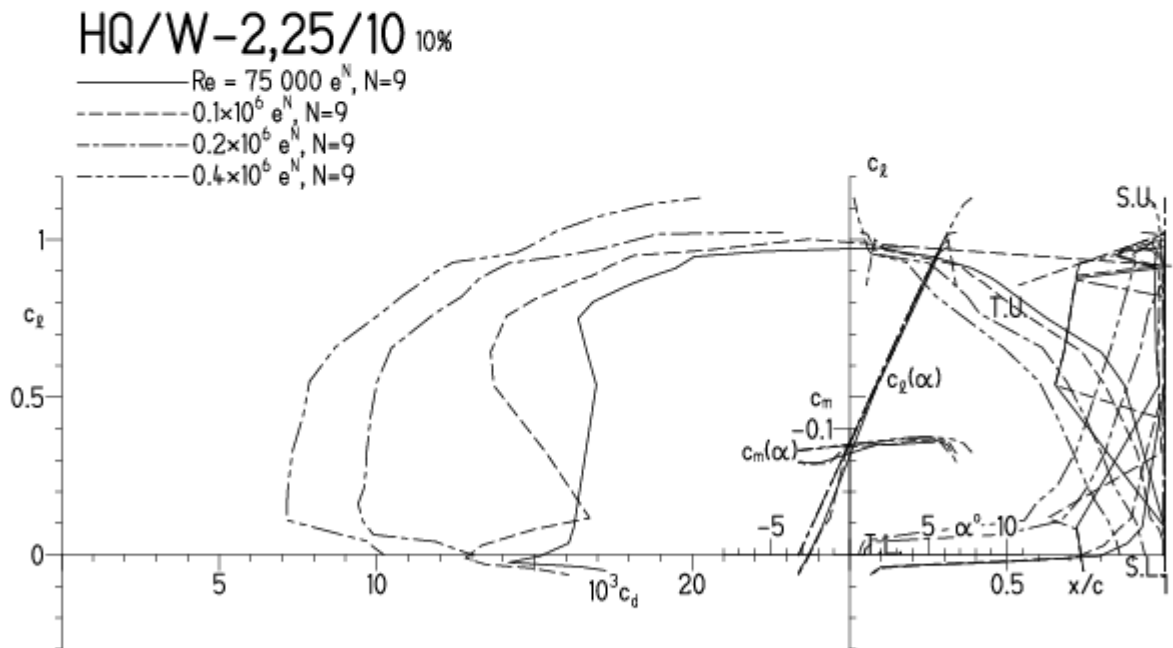


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

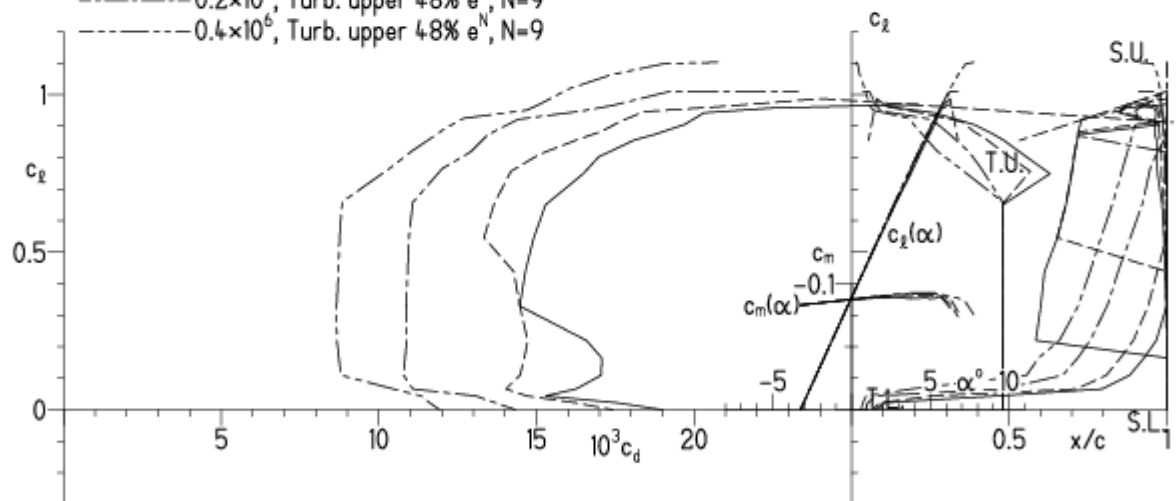
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

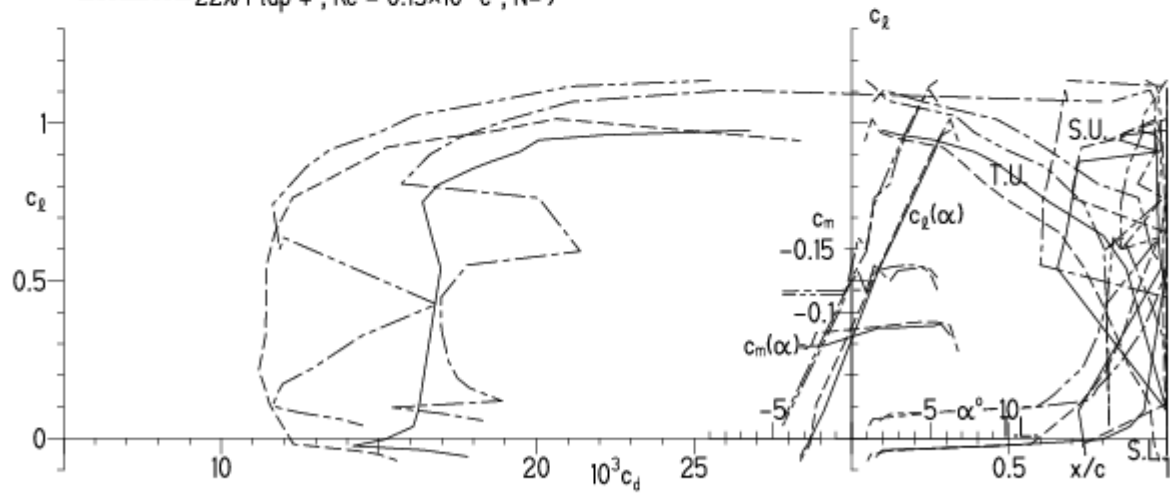


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

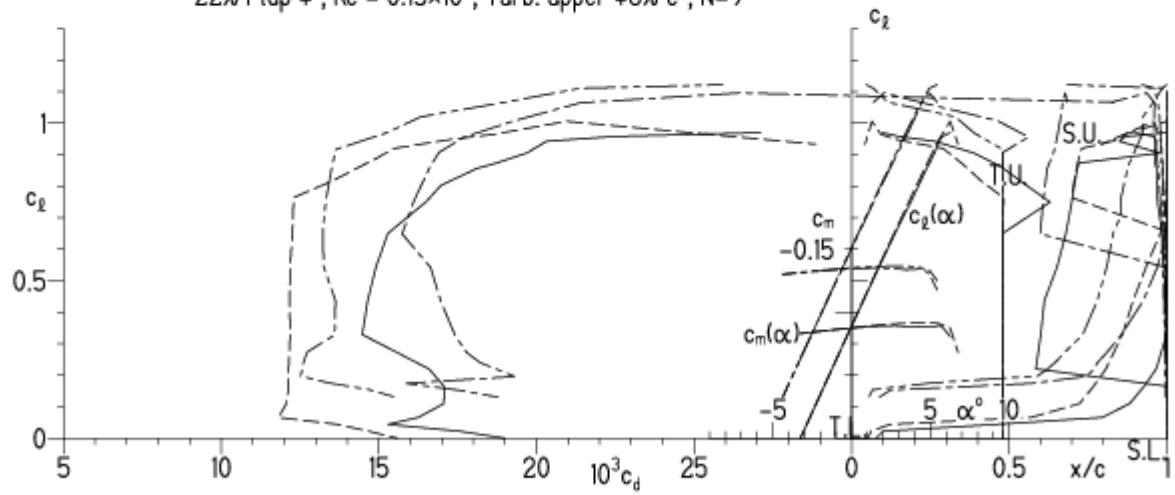


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

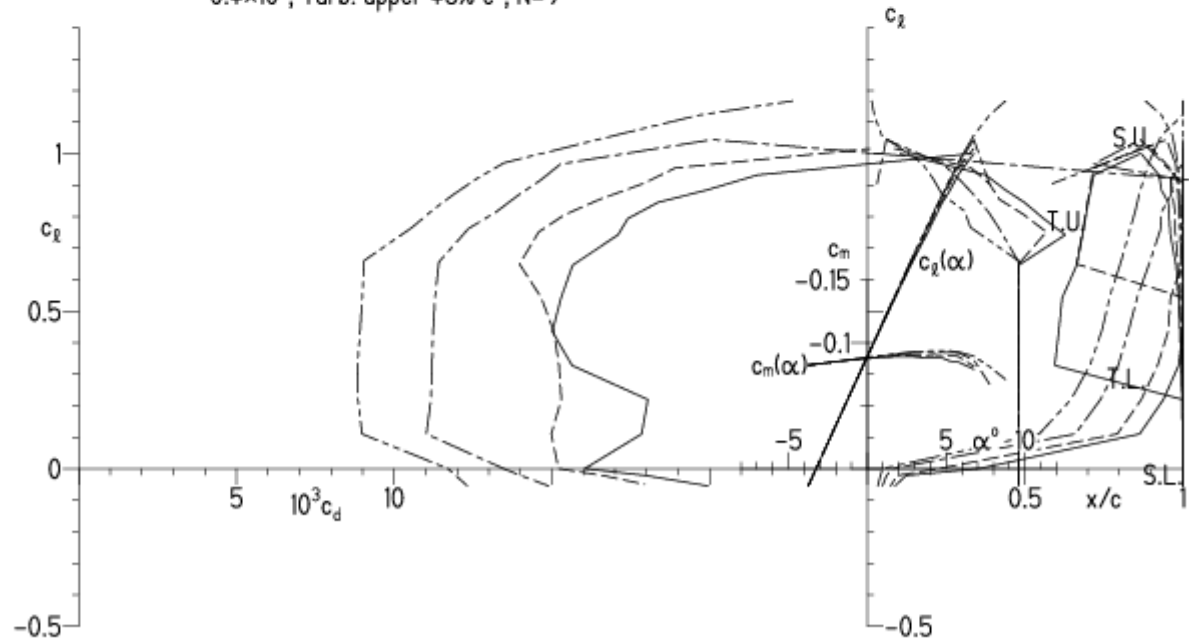
EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

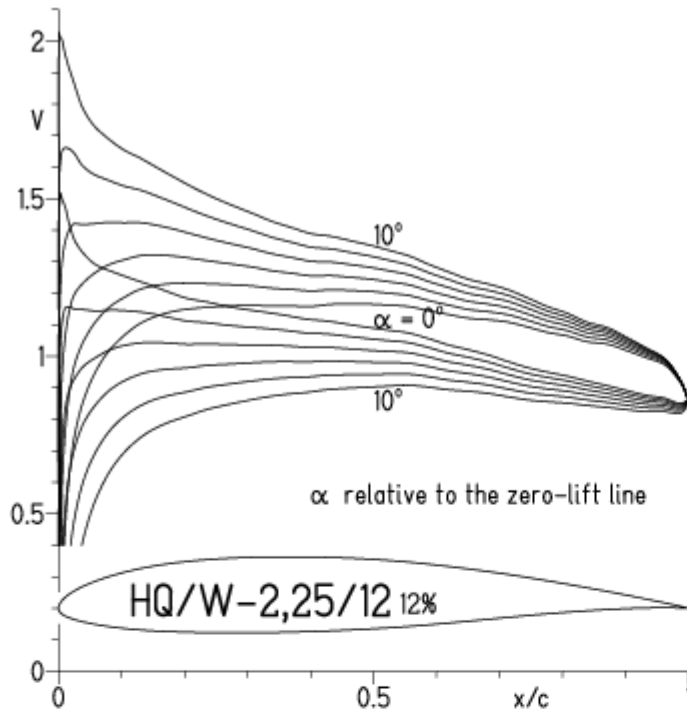
HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

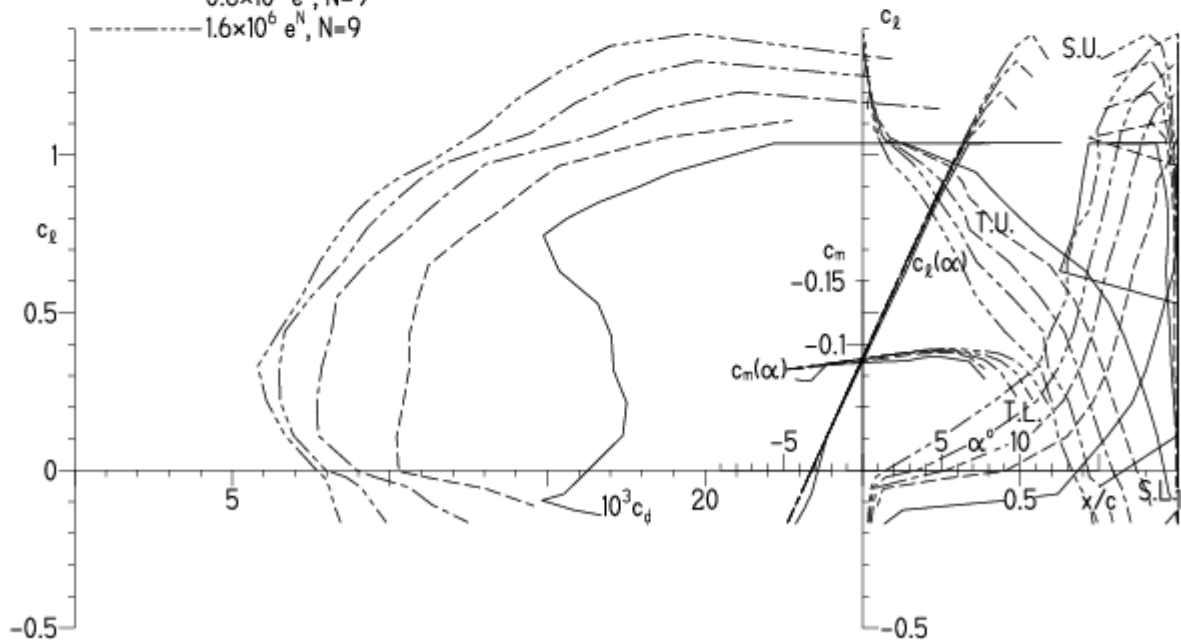
EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

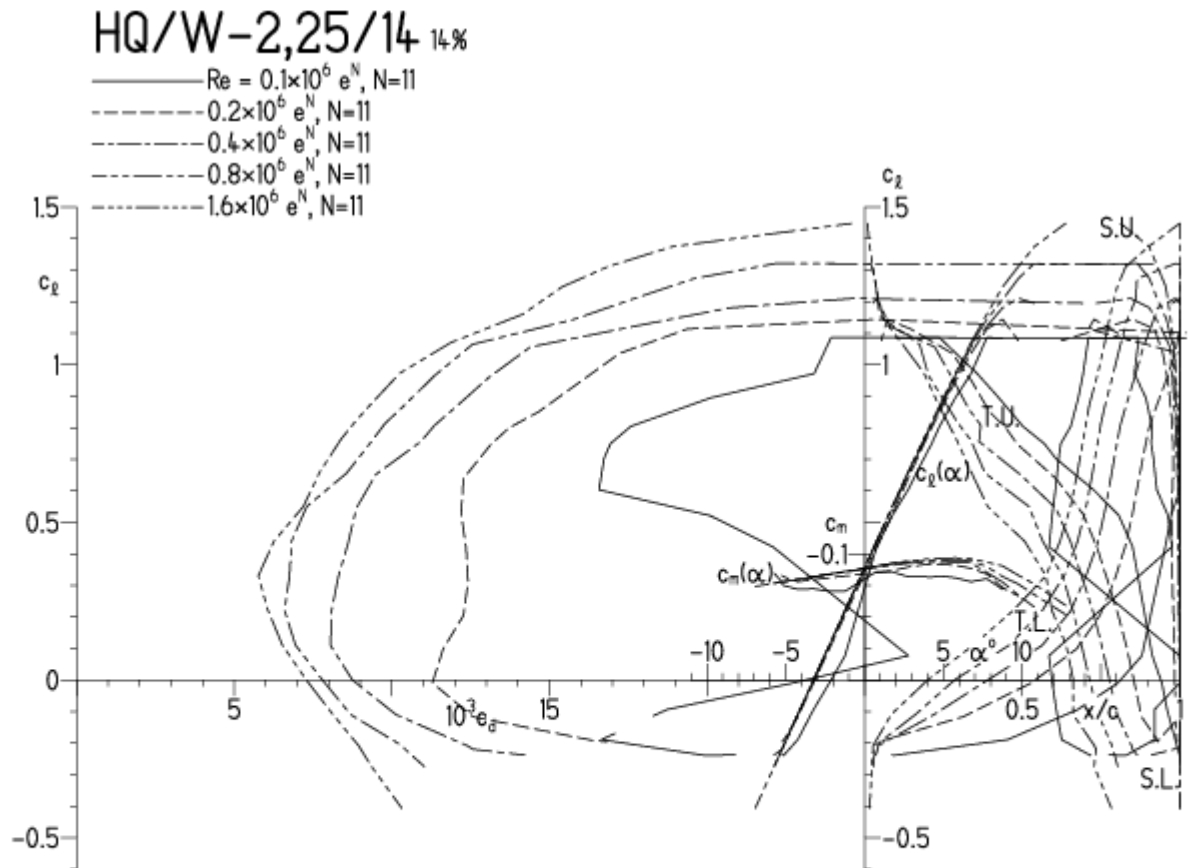


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

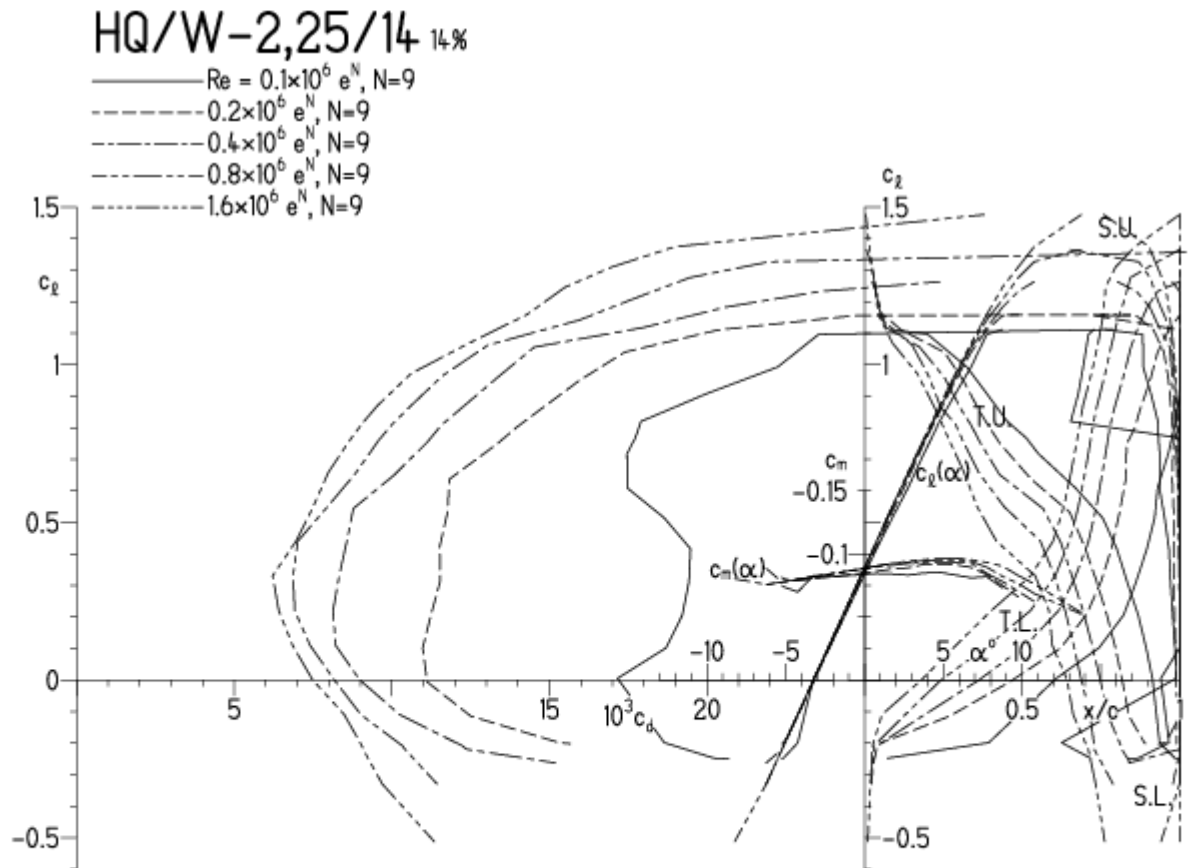


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

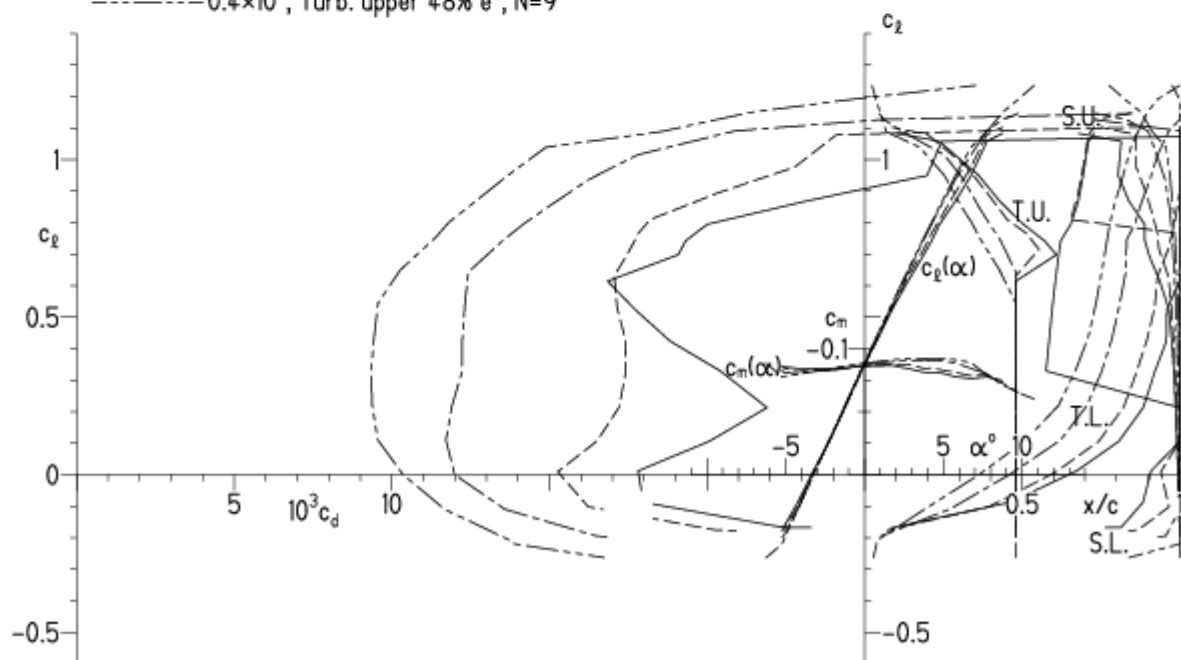
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

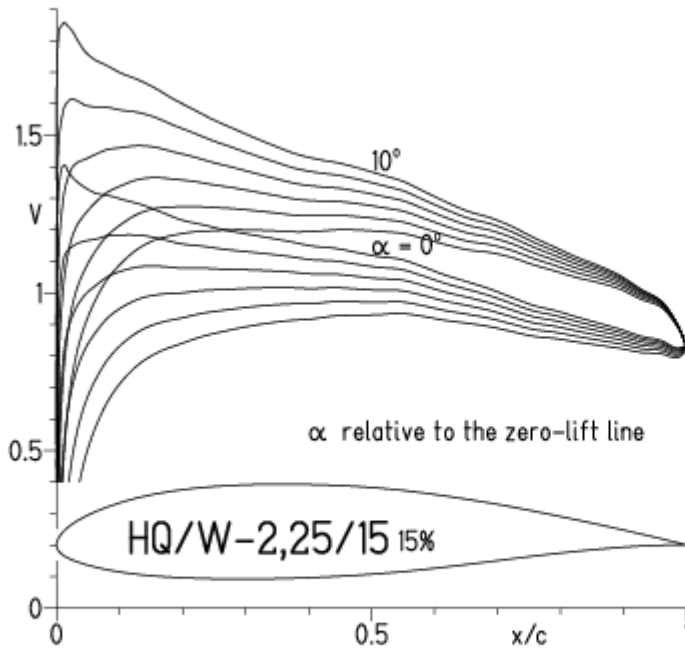


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

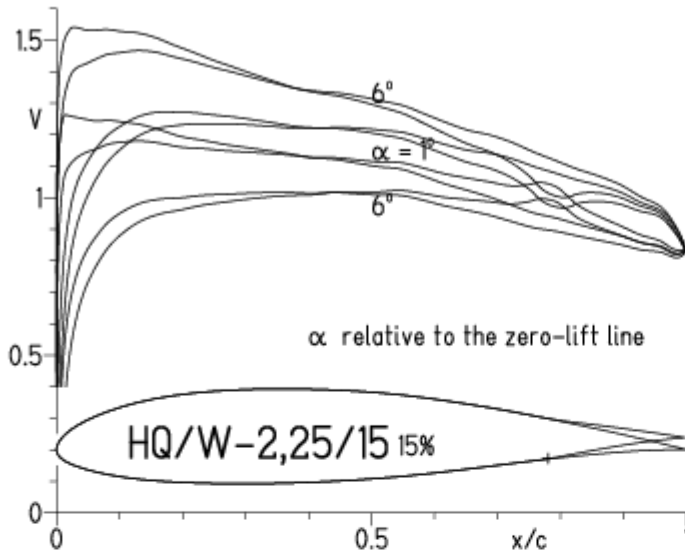


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



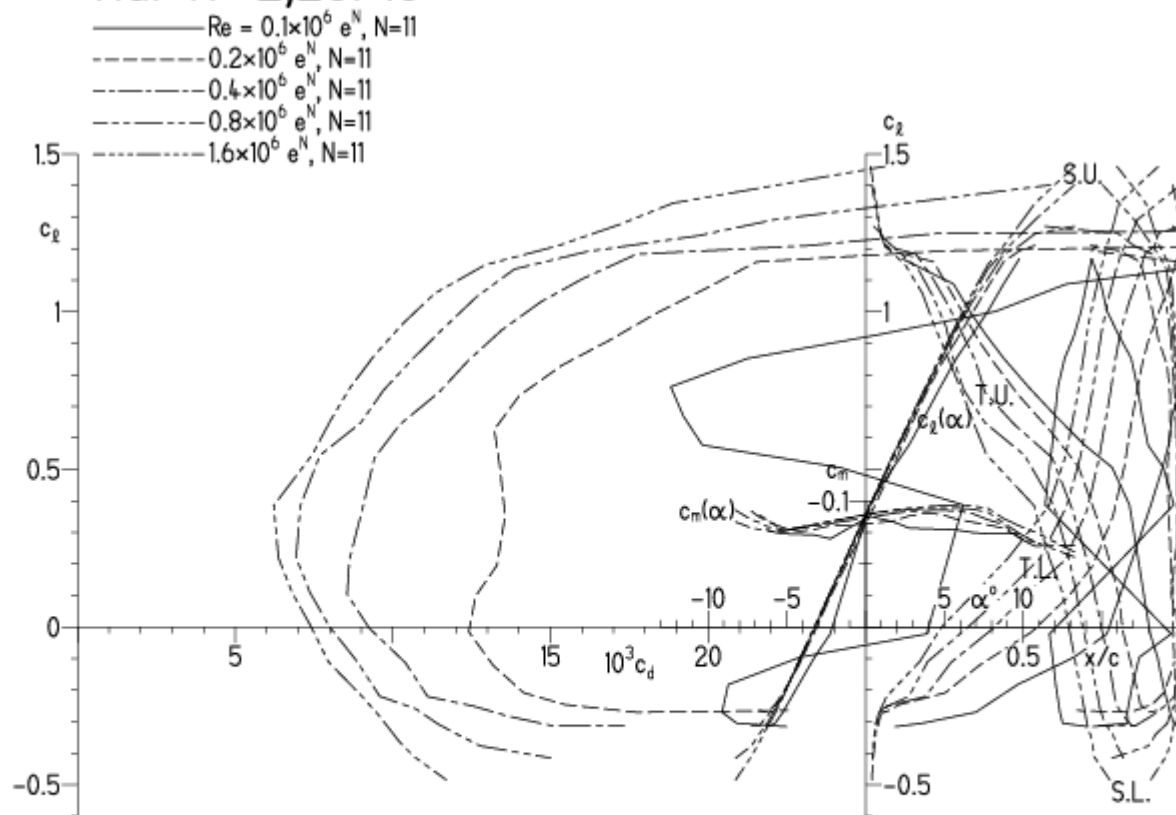
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41

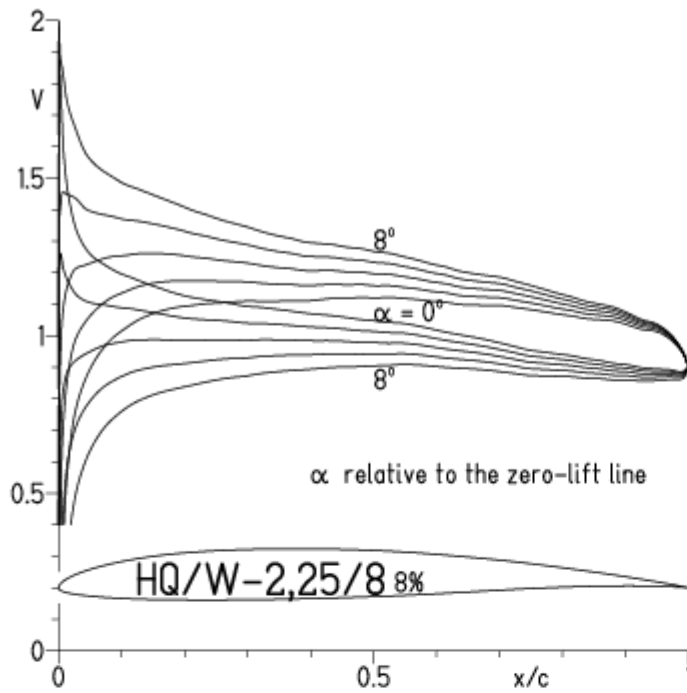


EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

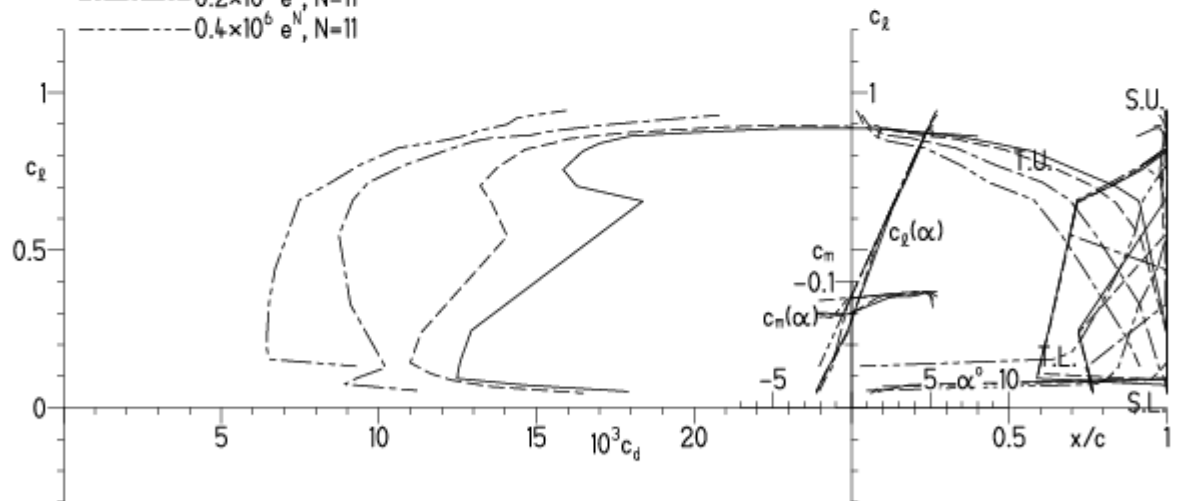
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

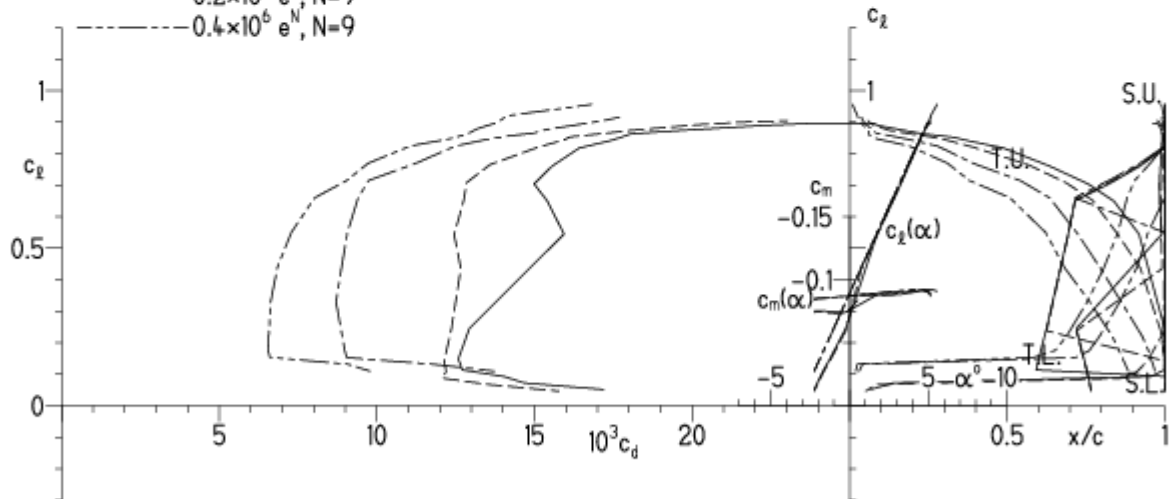
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

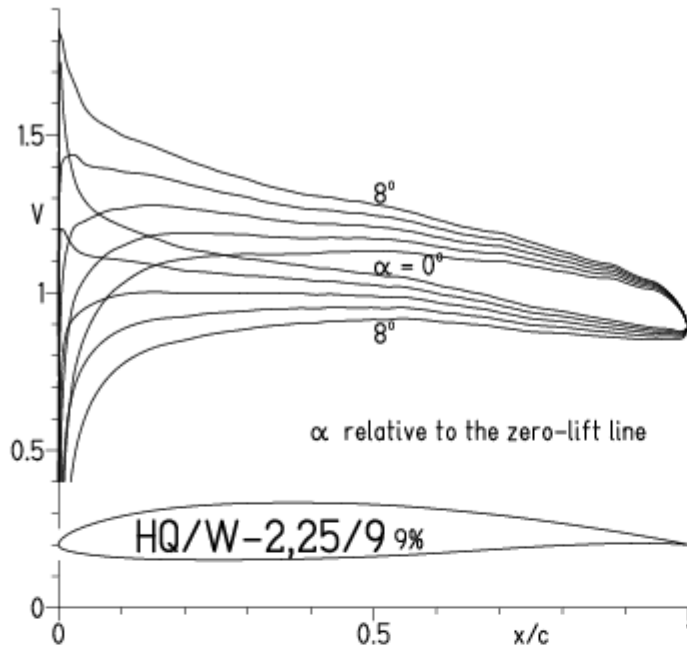


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

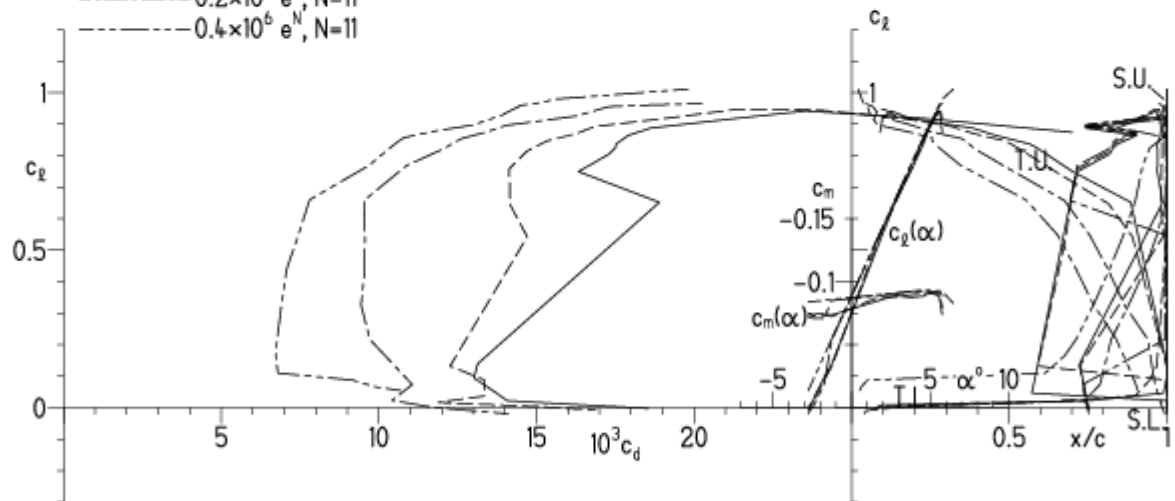
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

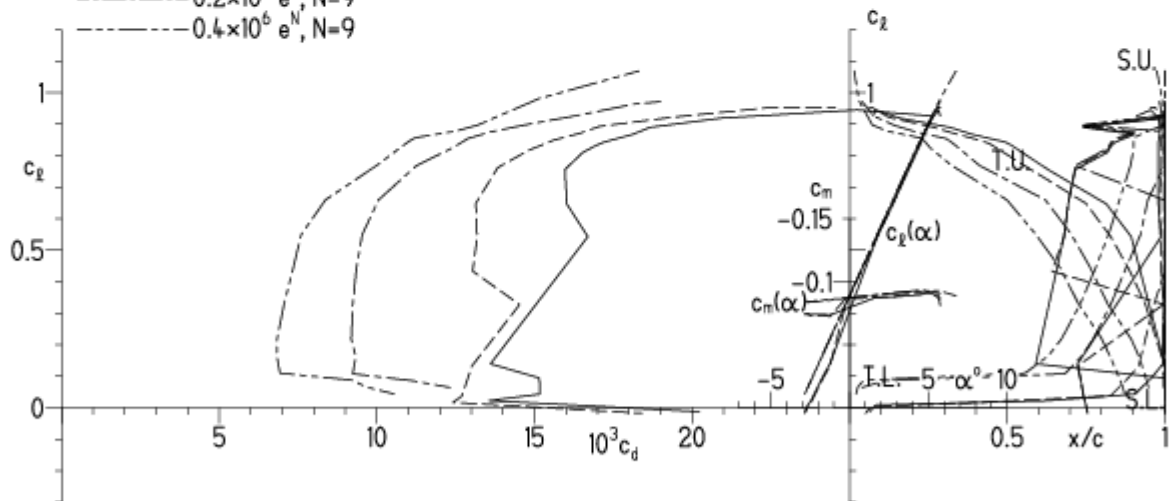
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

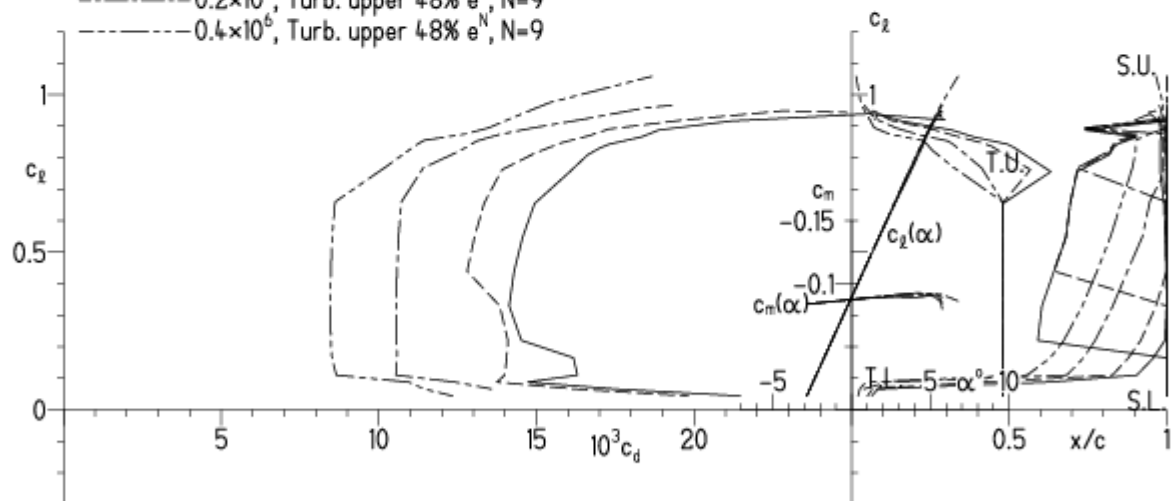
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

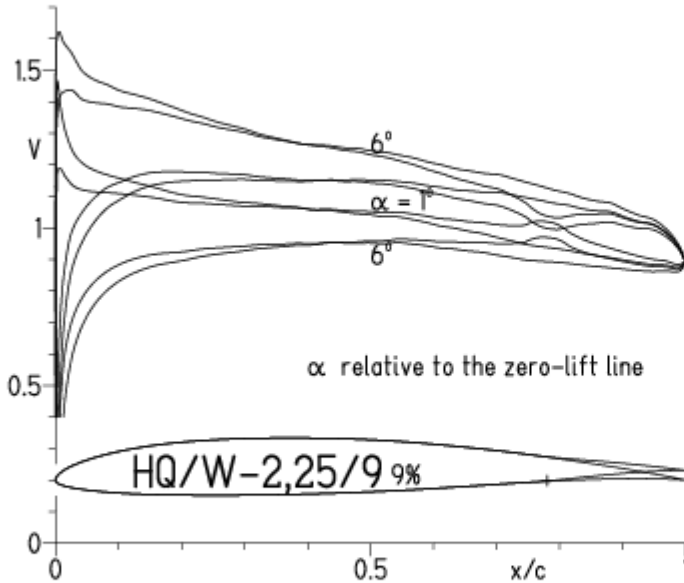
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

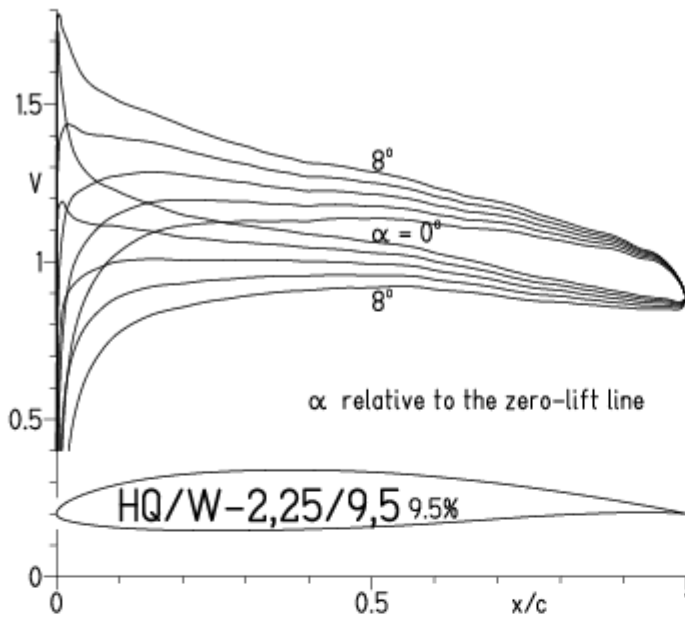
HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

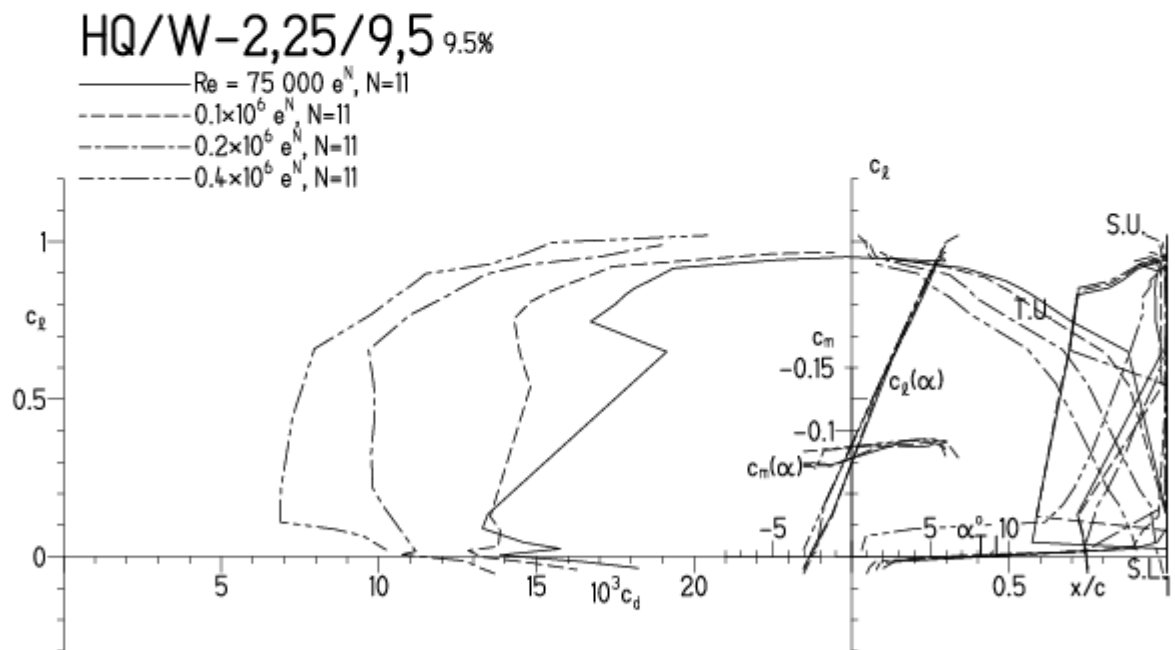


HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



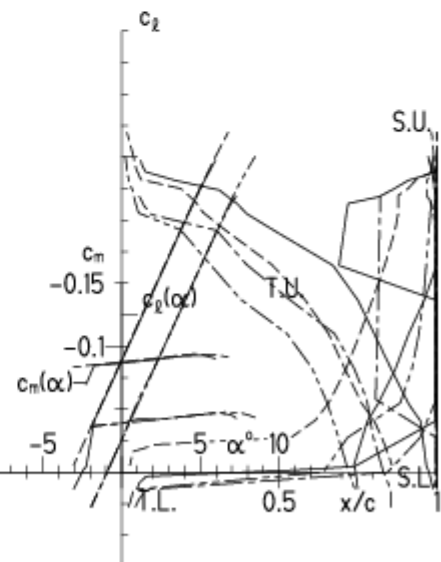
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

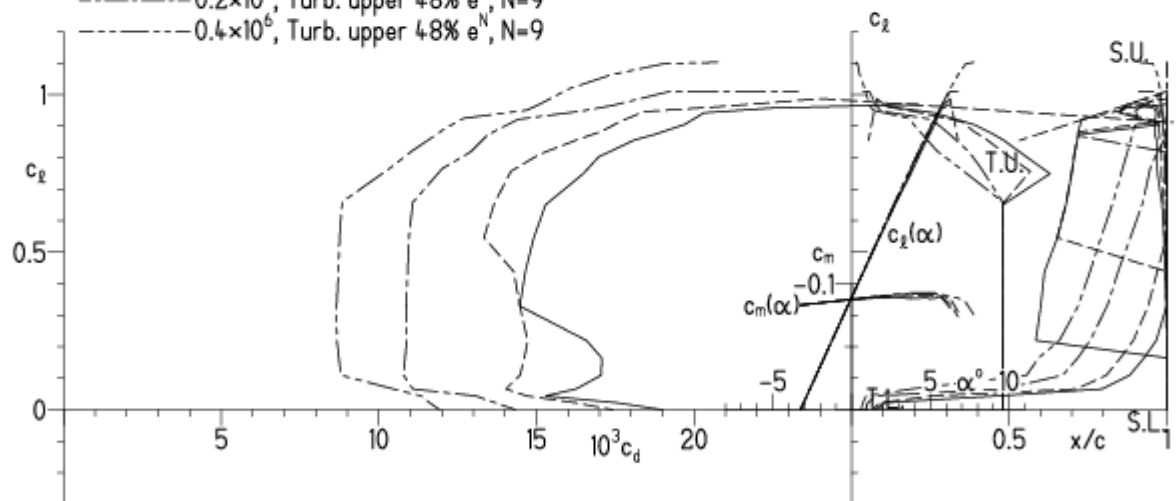
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

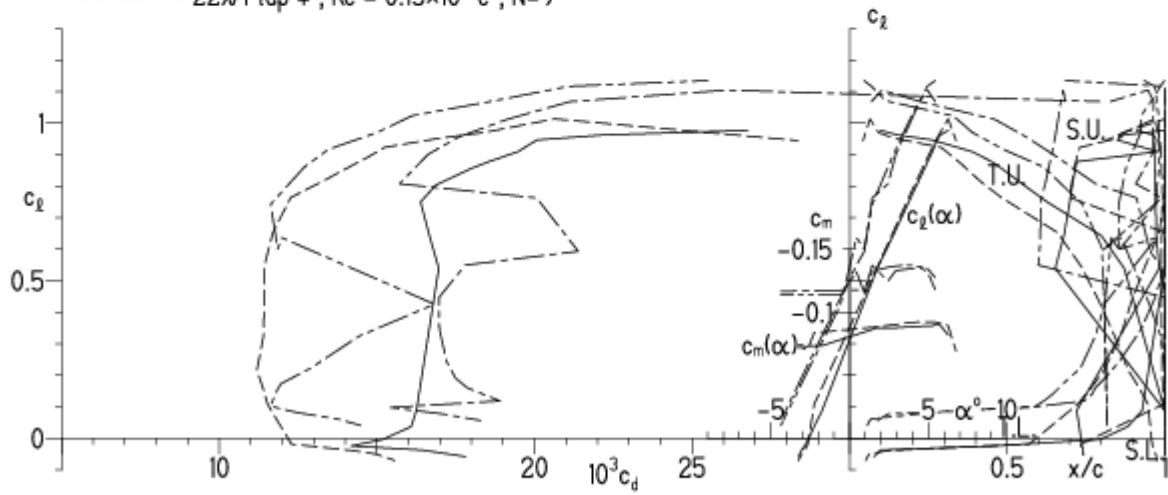


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

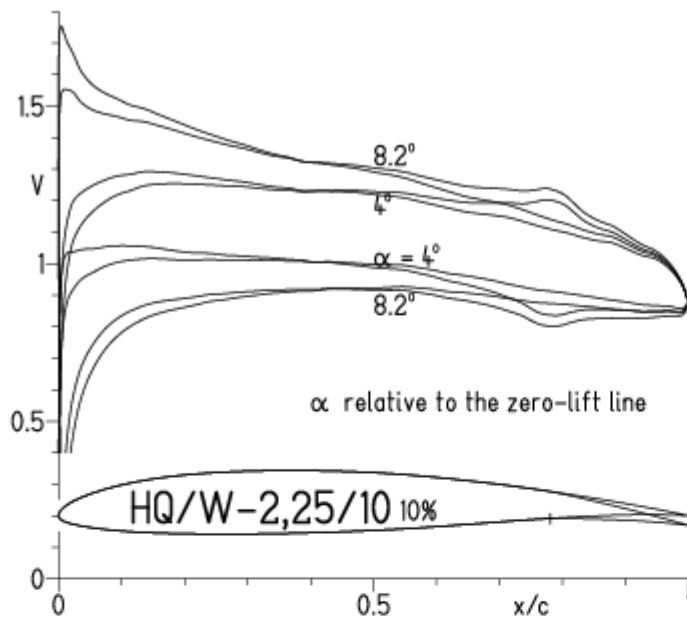
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

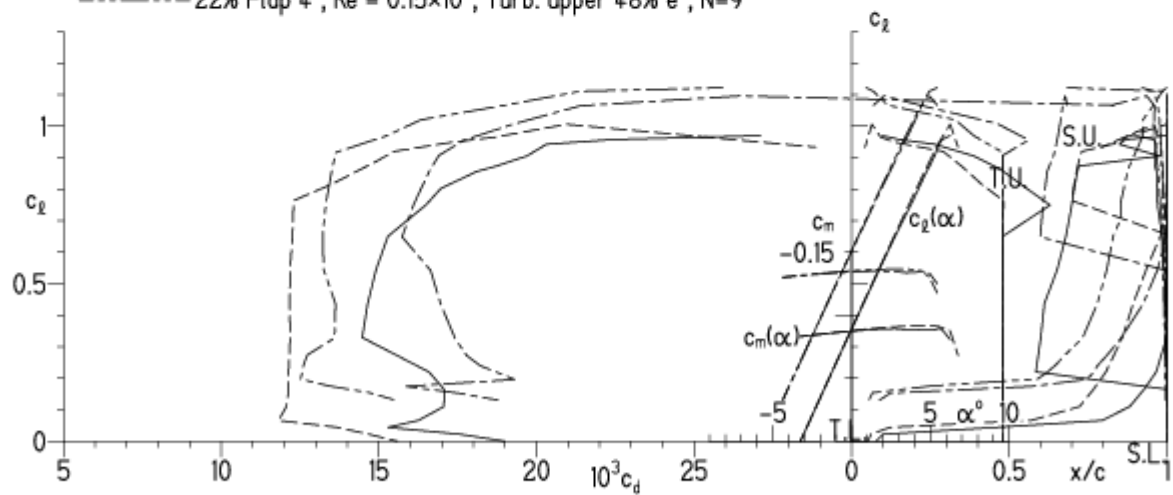


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

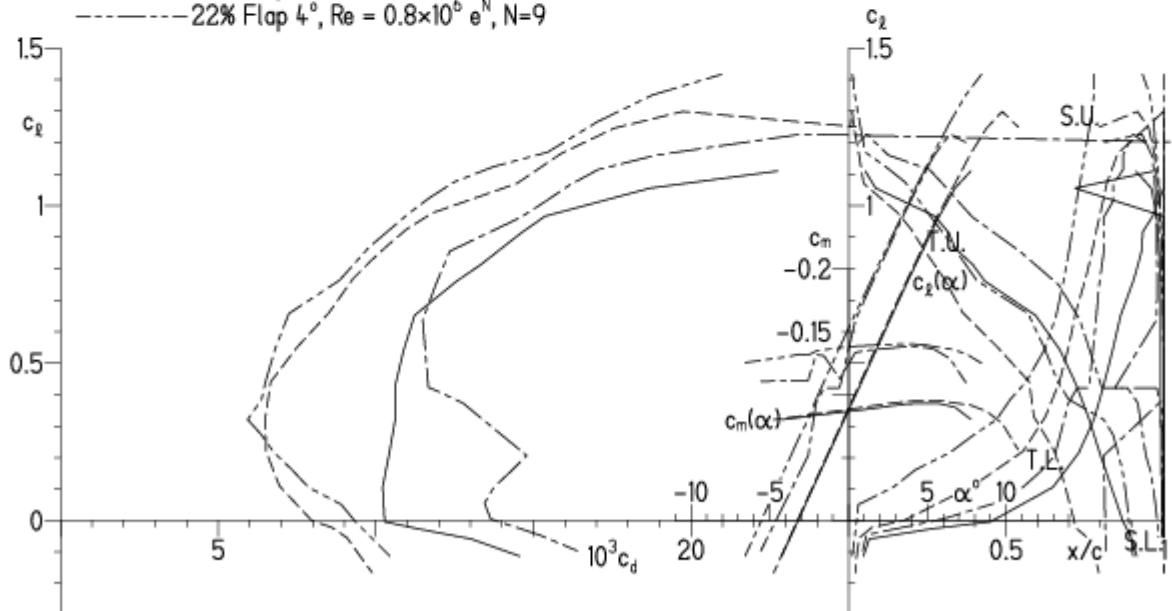


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:

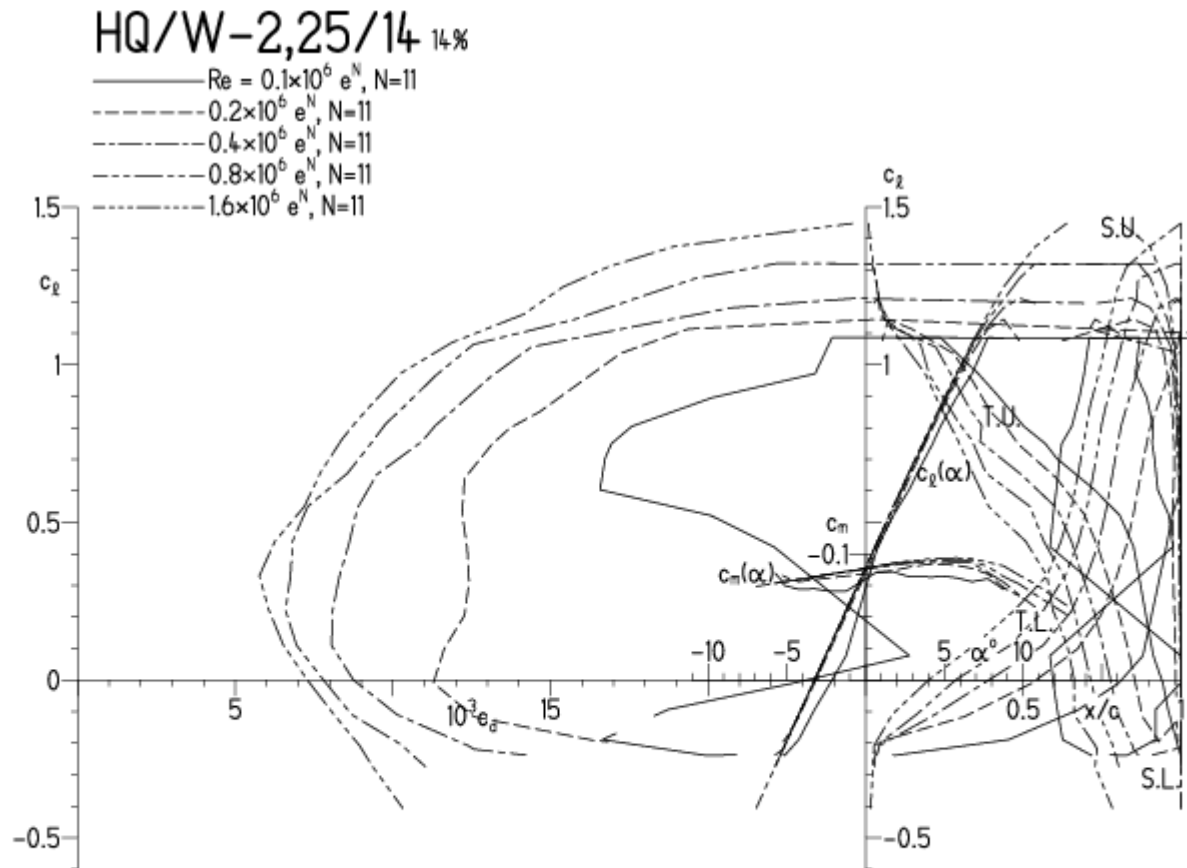


HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

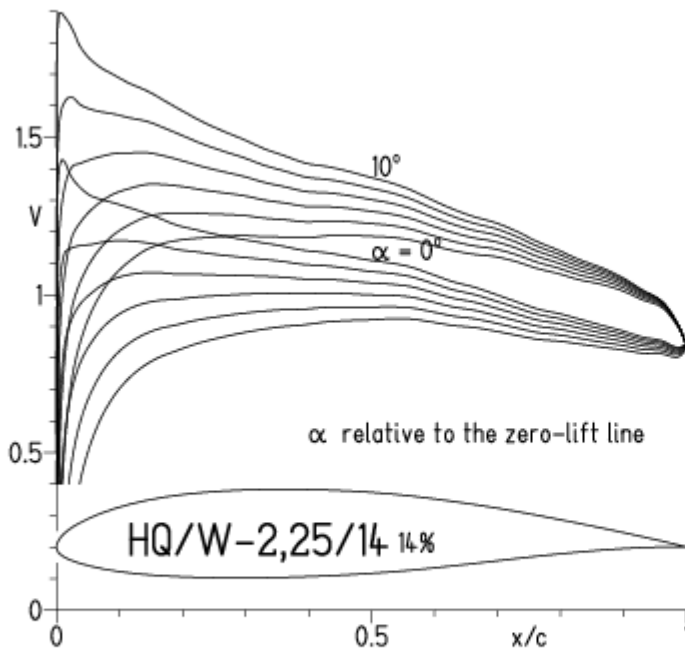


EPPLER 2005 V. 8.

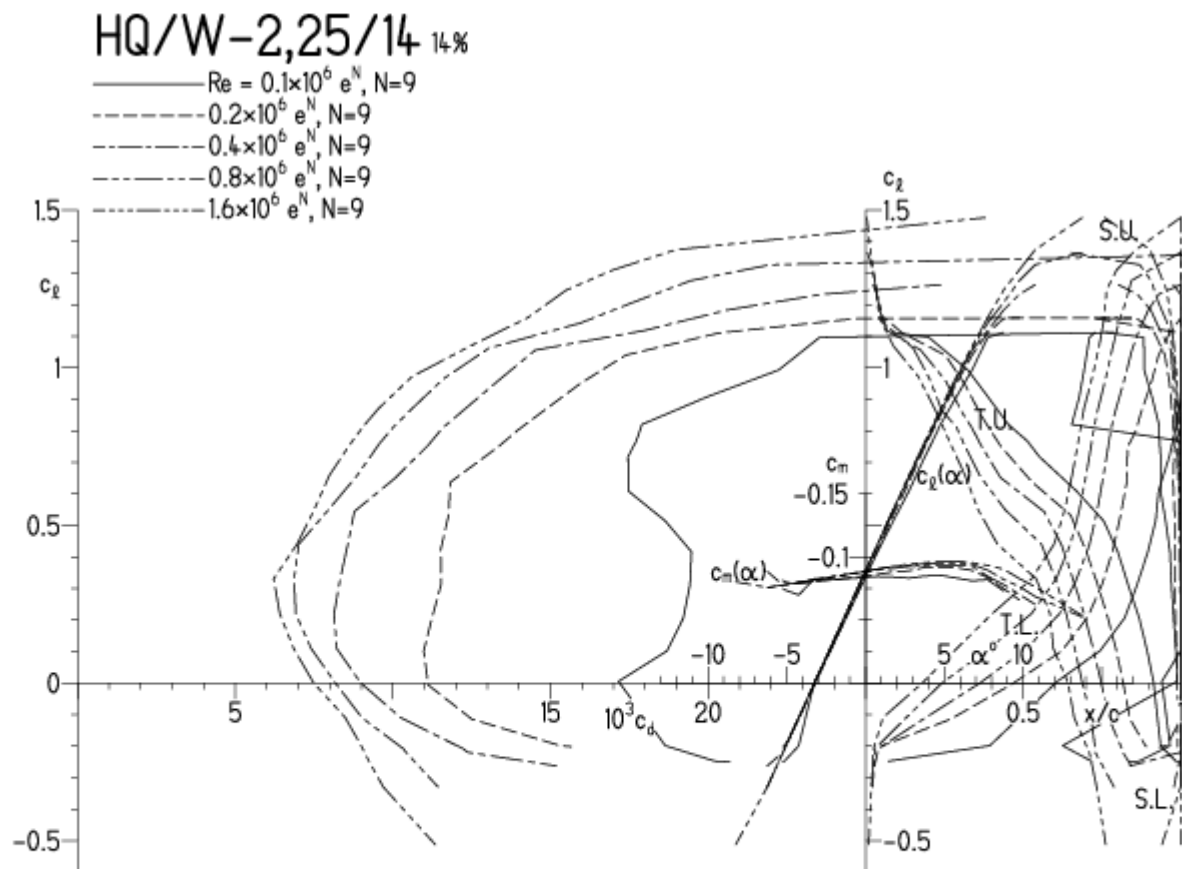


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

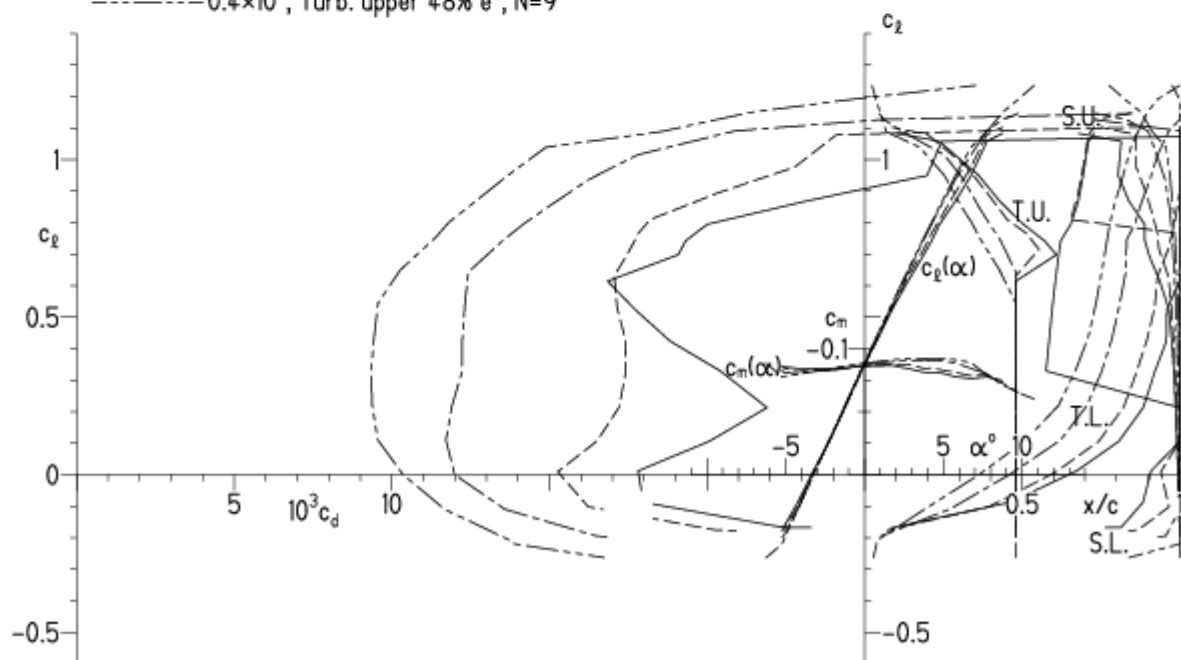
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

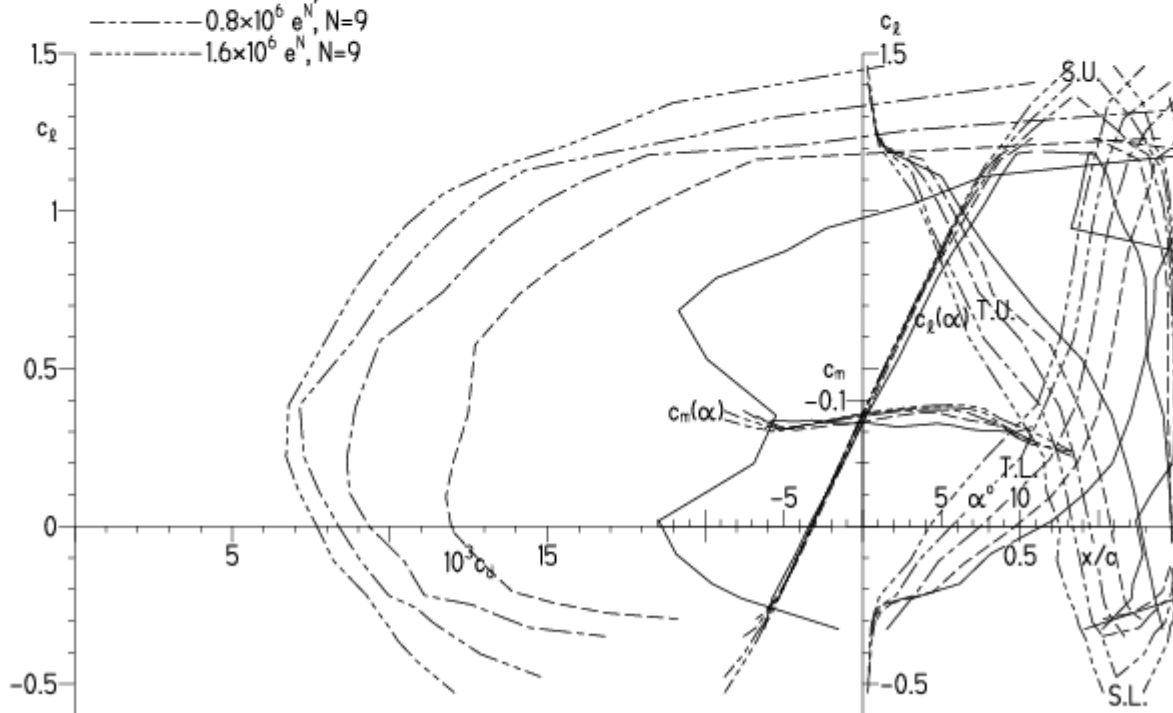
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

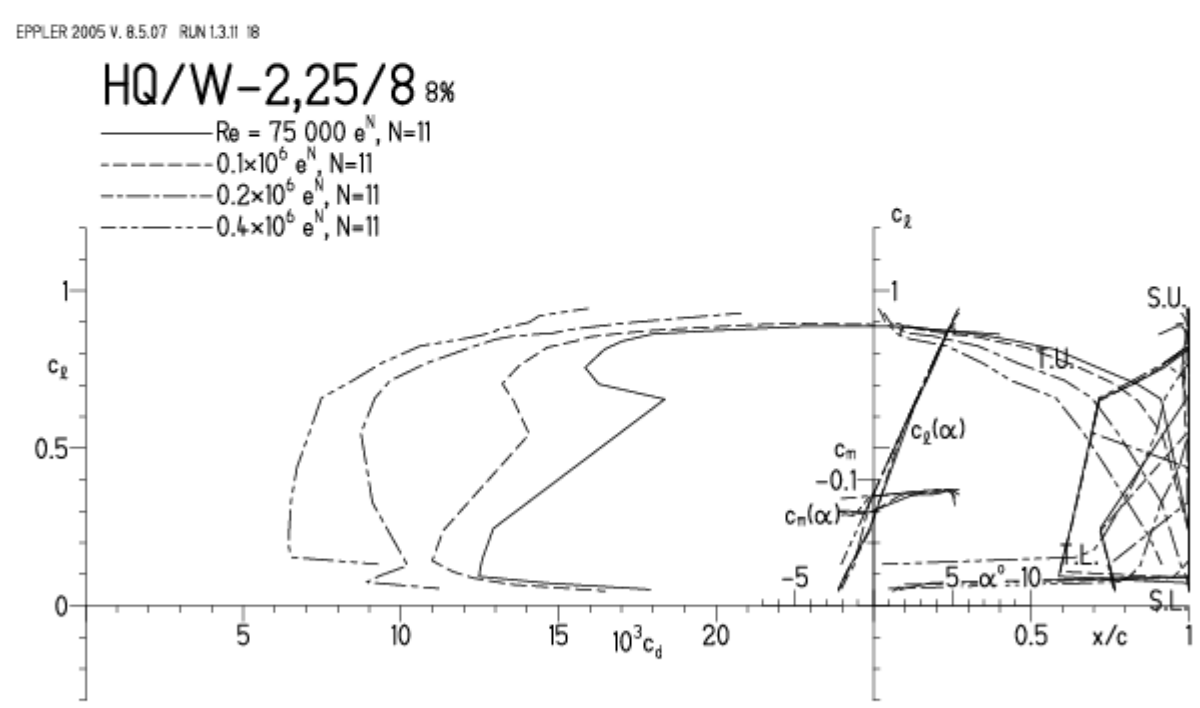
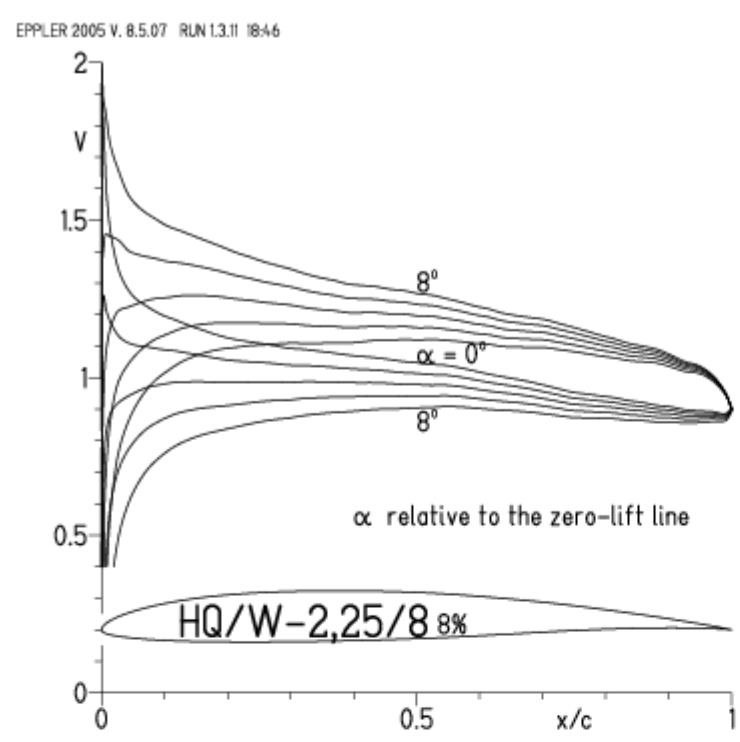
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11



HQ/W-2,25/8, N=9

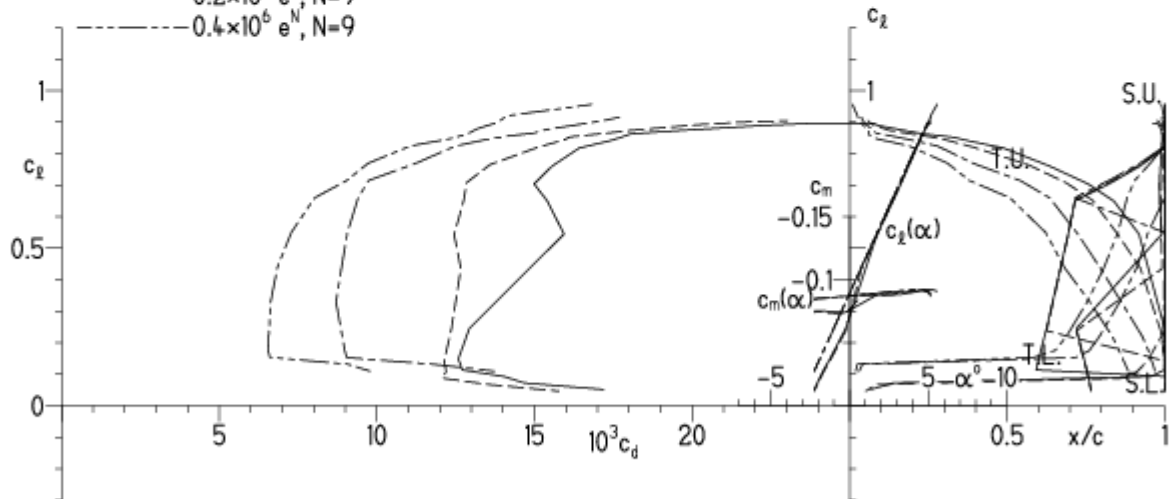
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

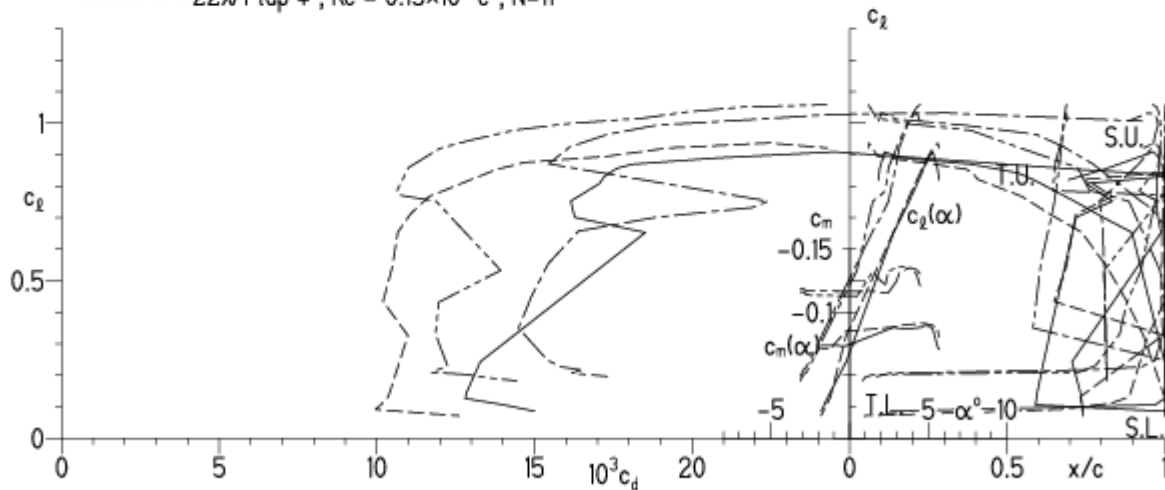


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

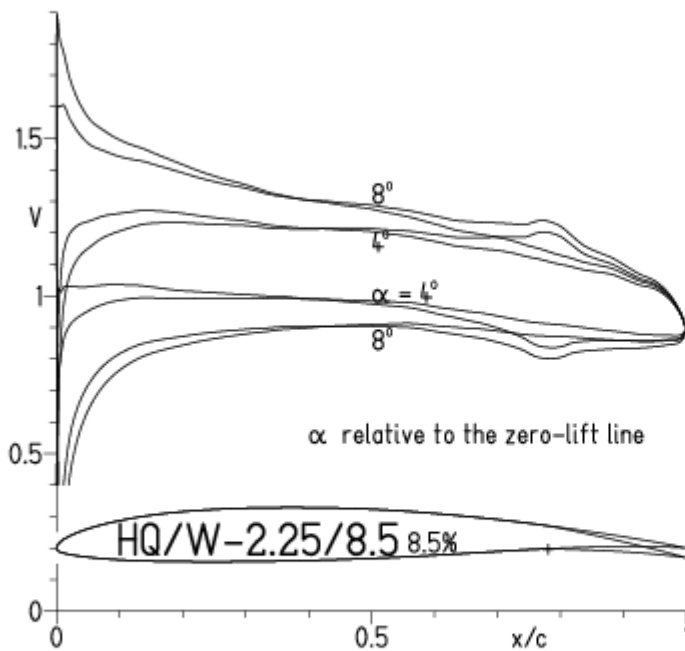
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

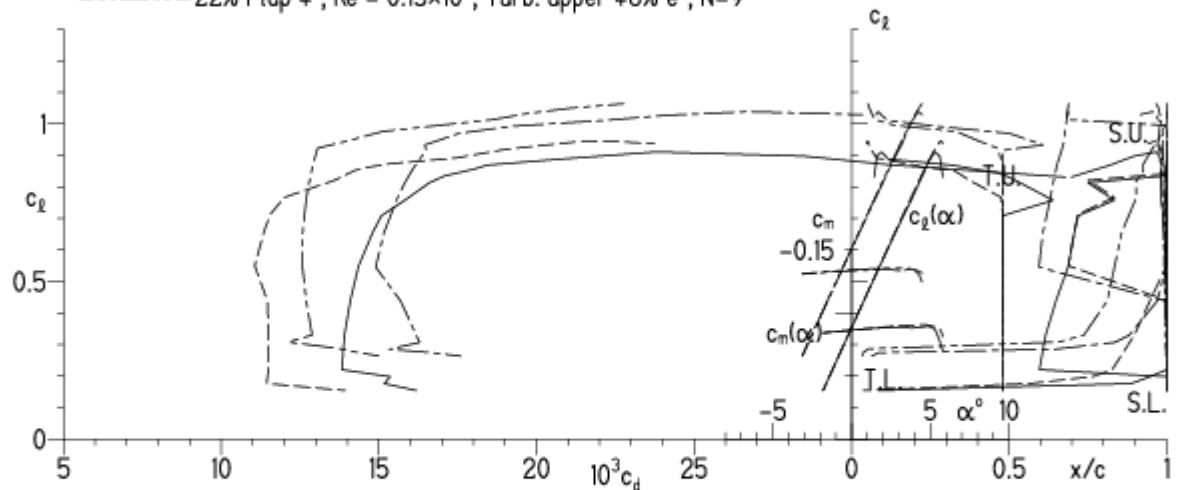


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

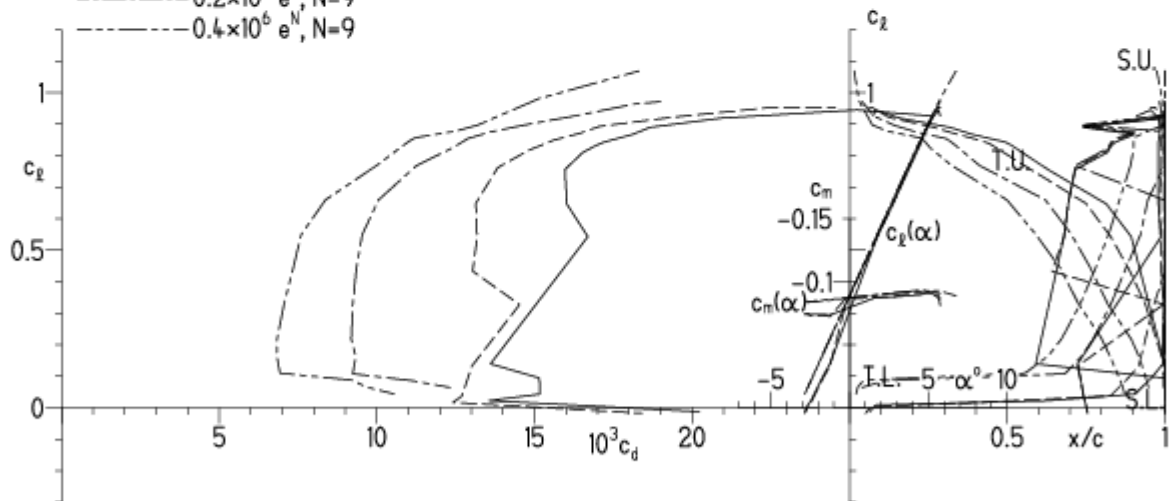
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

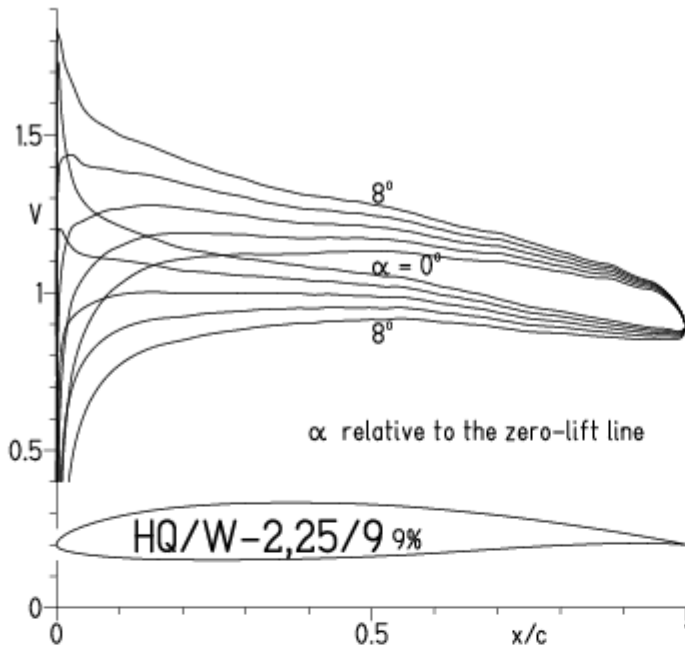
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

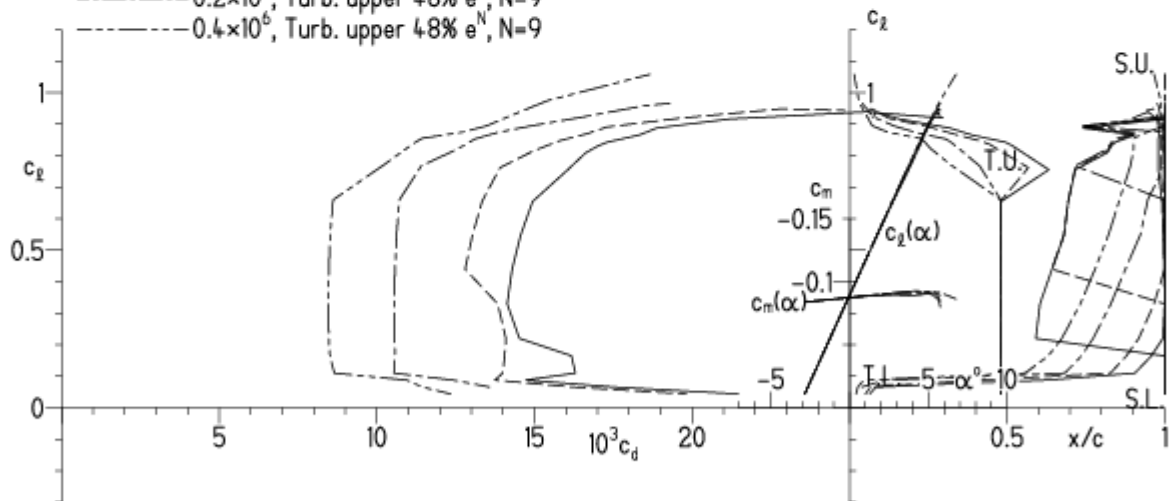
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17

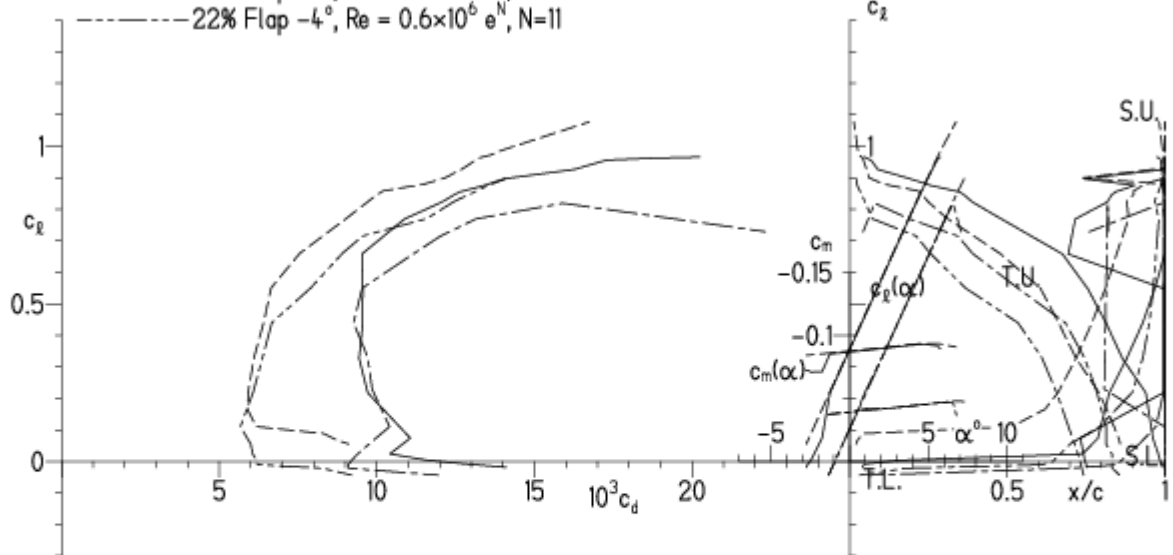


EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11

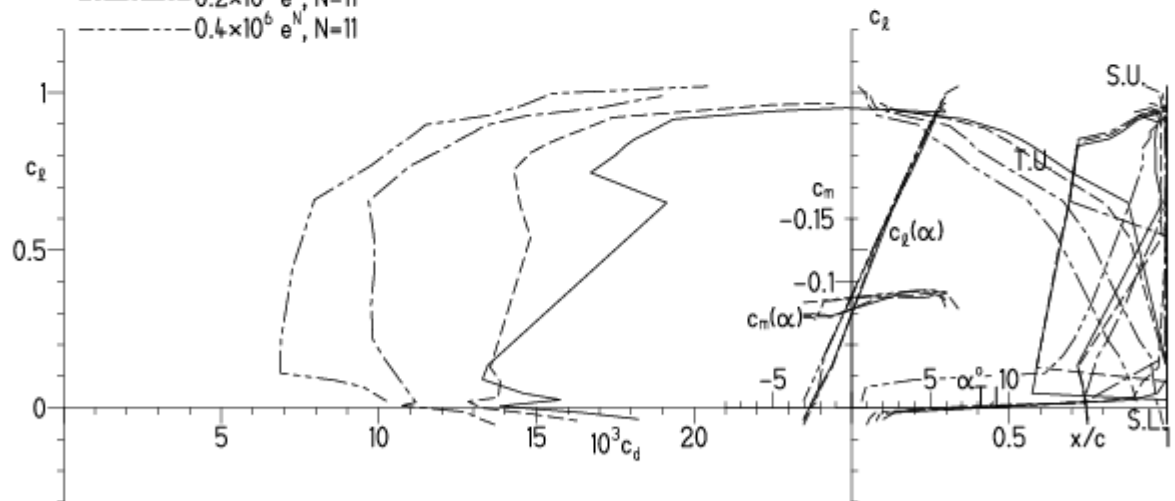
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

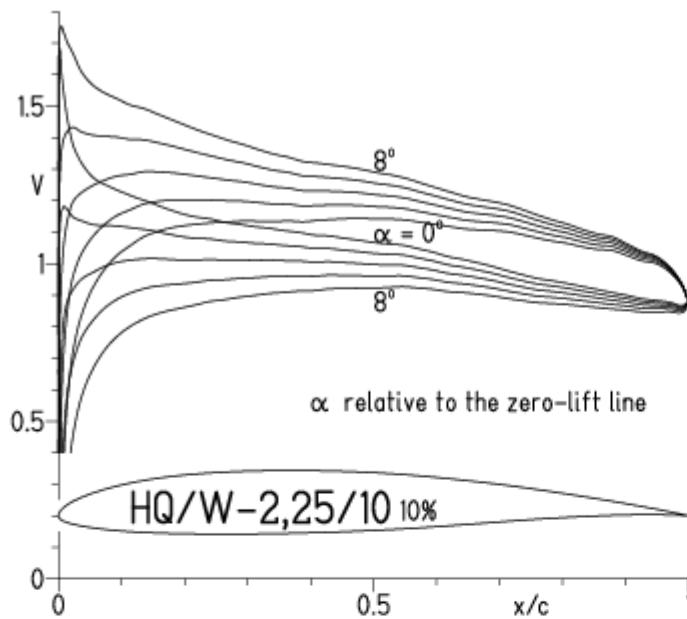


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

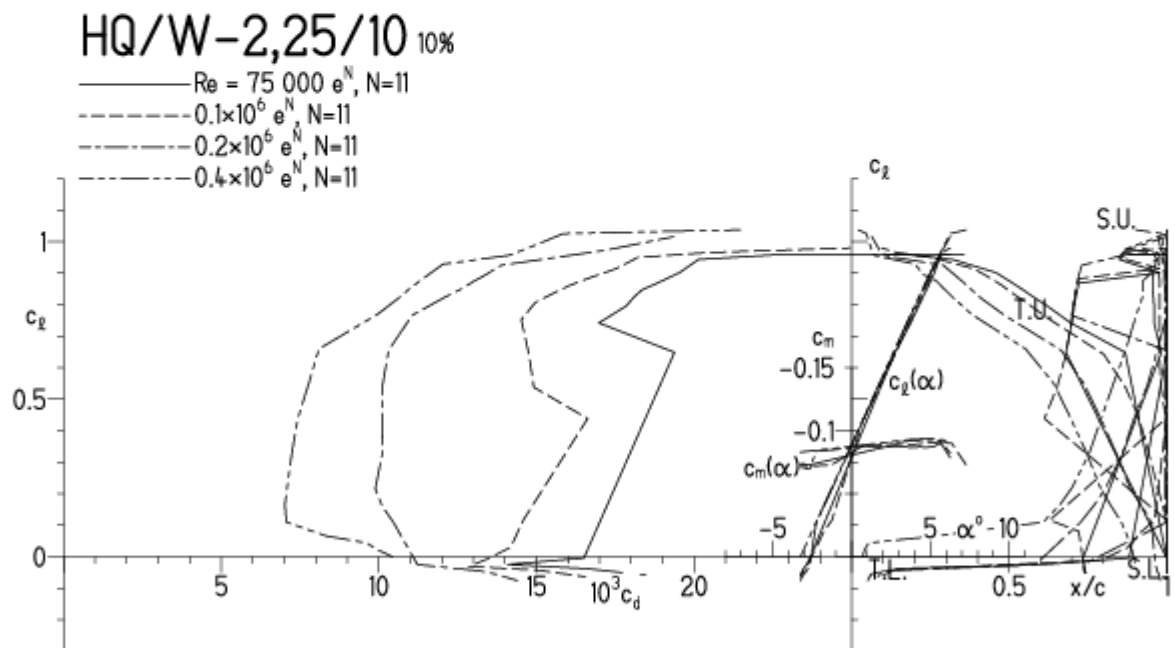


HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

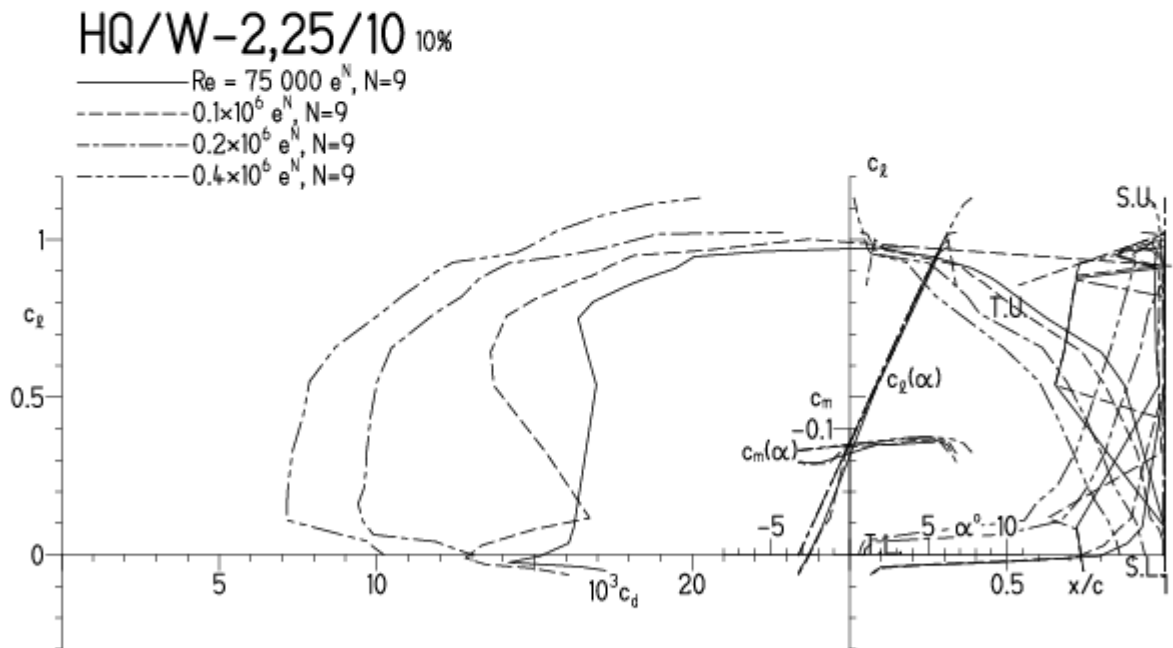


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

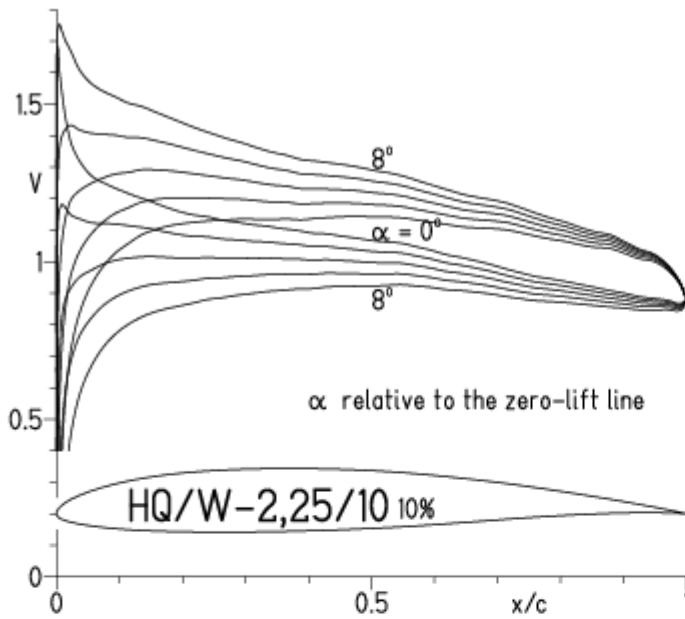


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

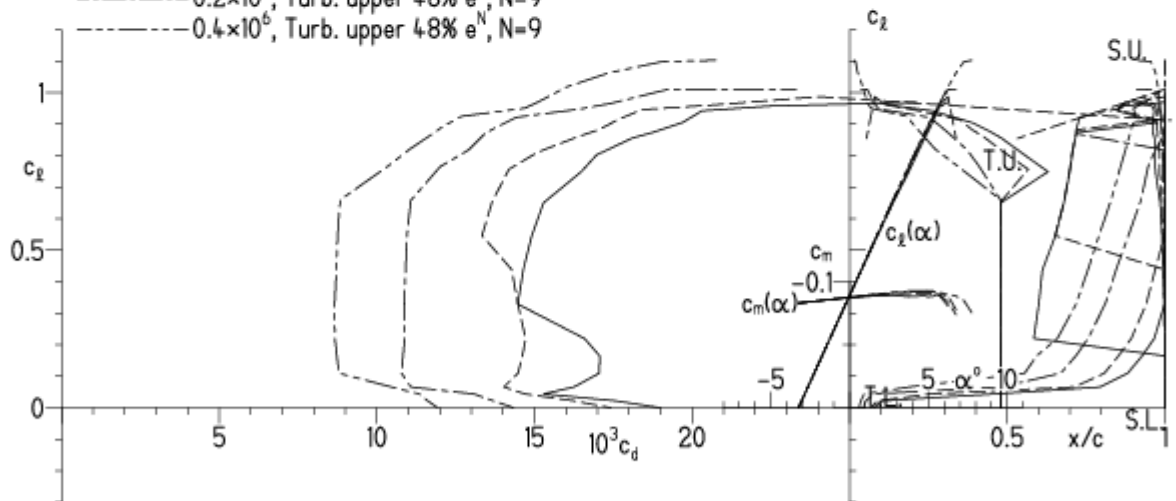
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

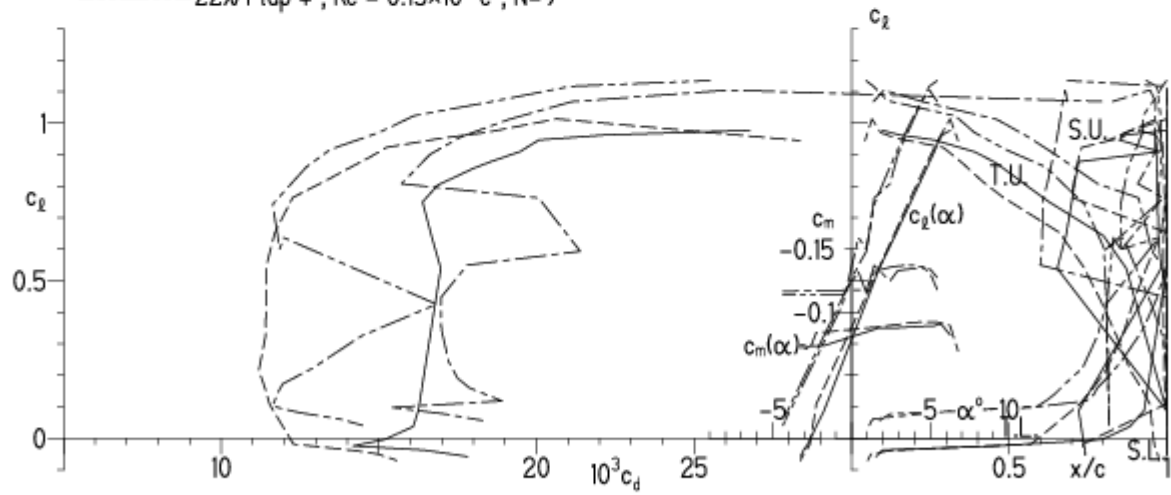


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

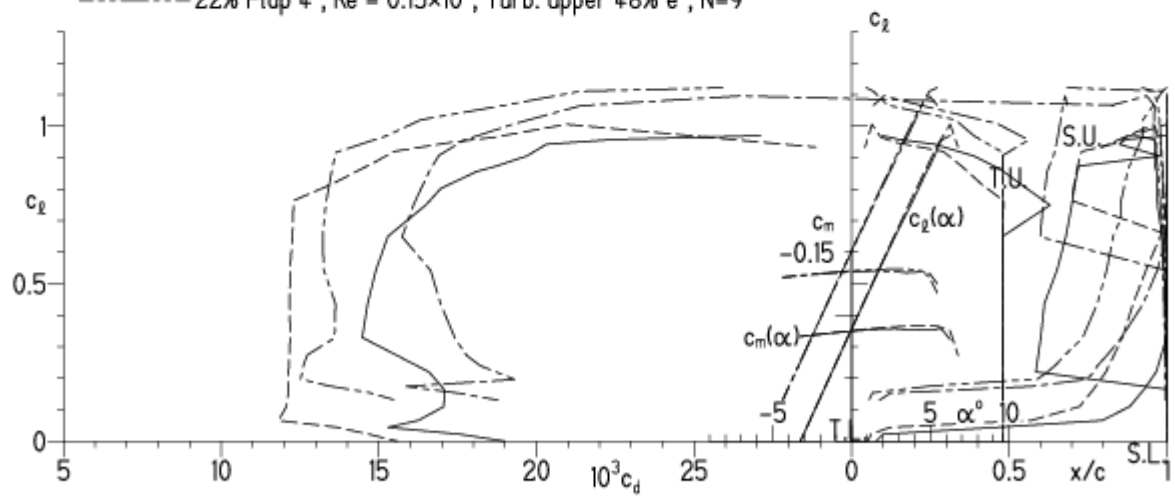


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

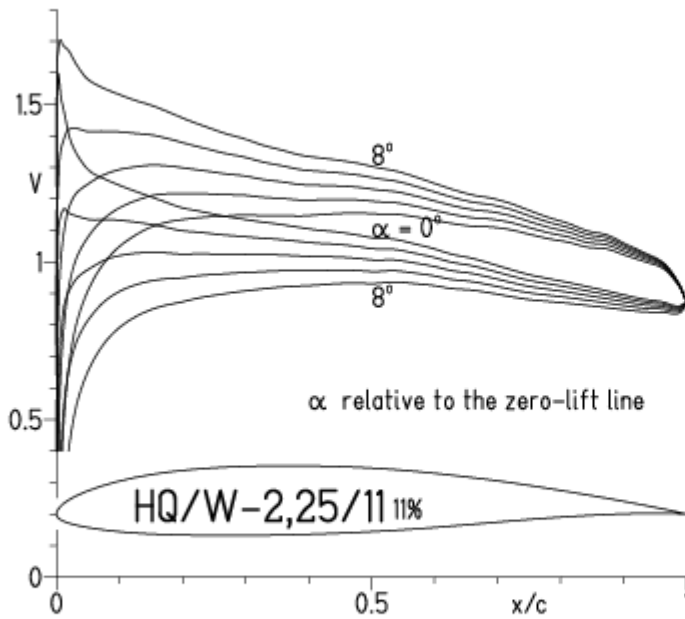


EPPLER 2005 V. 8.5.07 RUN

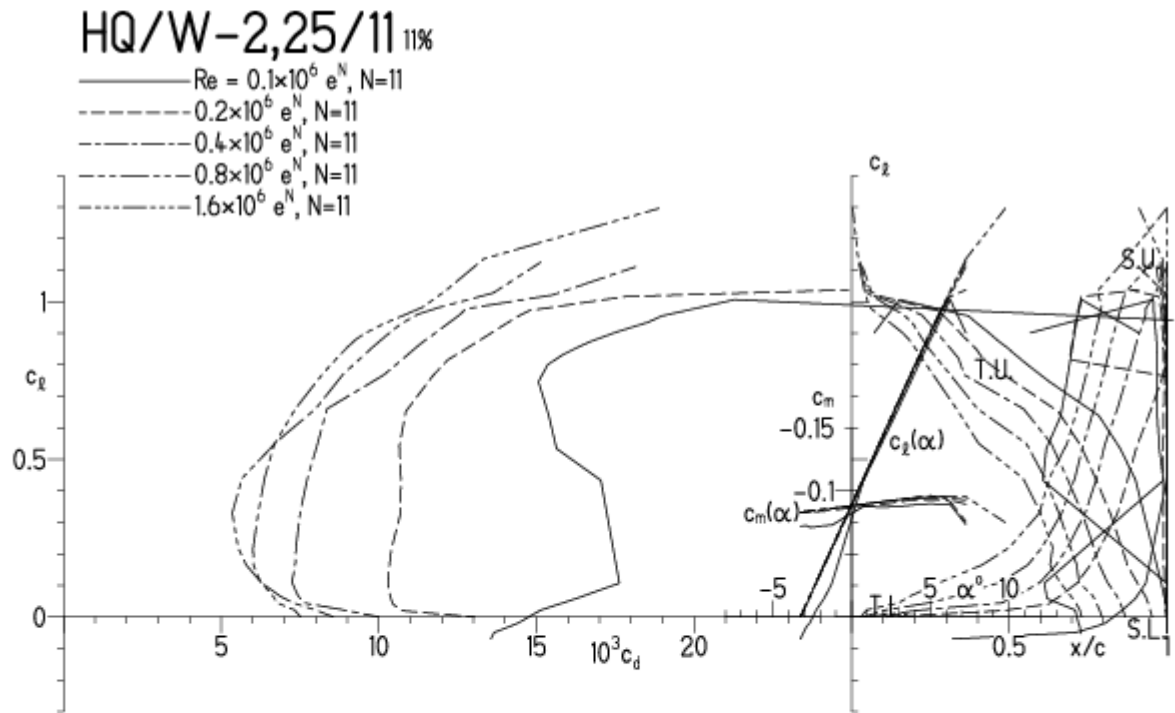


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

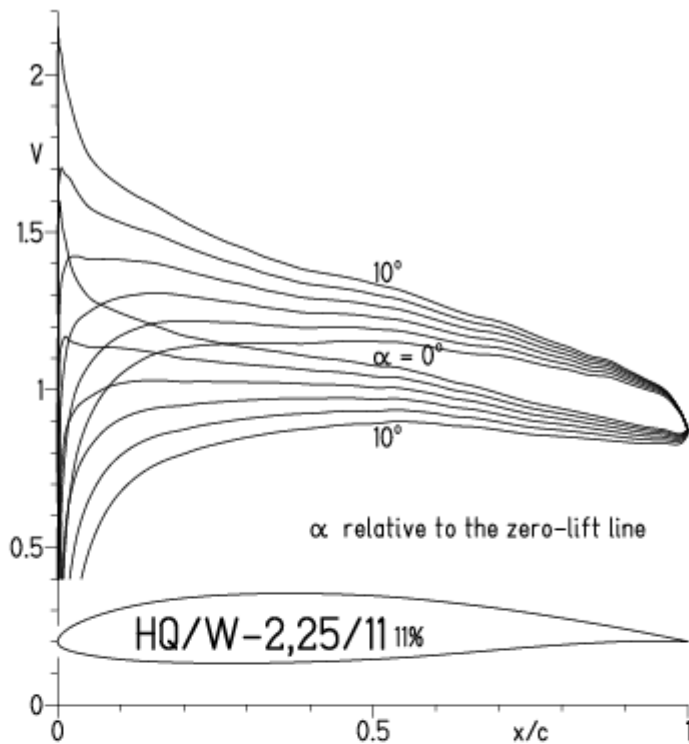


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- Re = 0.2×10^6 e^N, N=9
- - - Re = 0.8×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.2×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.8×10^6 e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

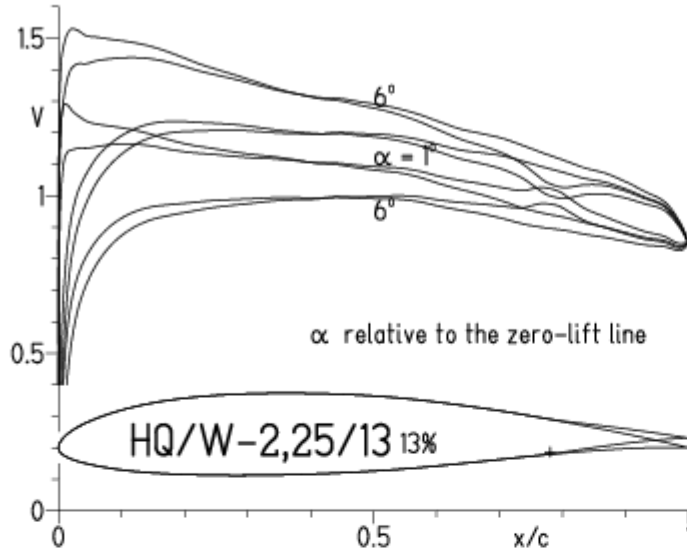
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

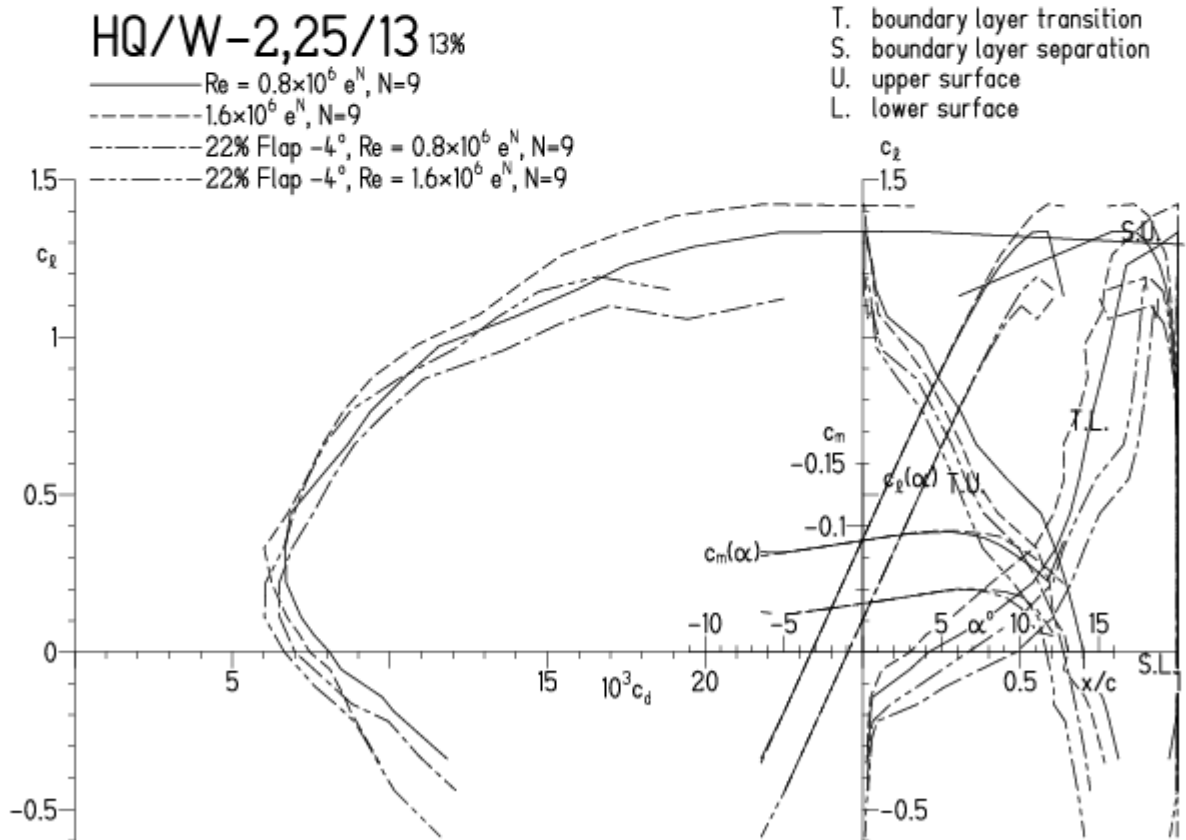


HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

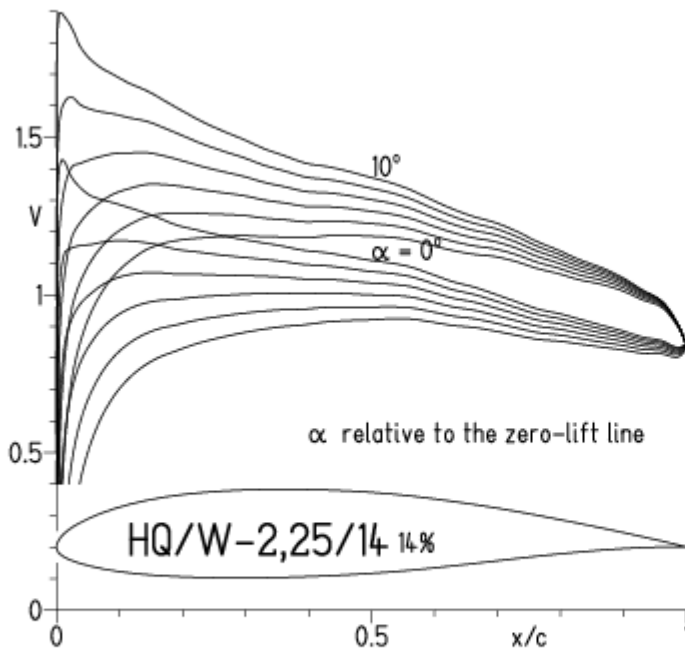


EPPLER 2005 V. 8.

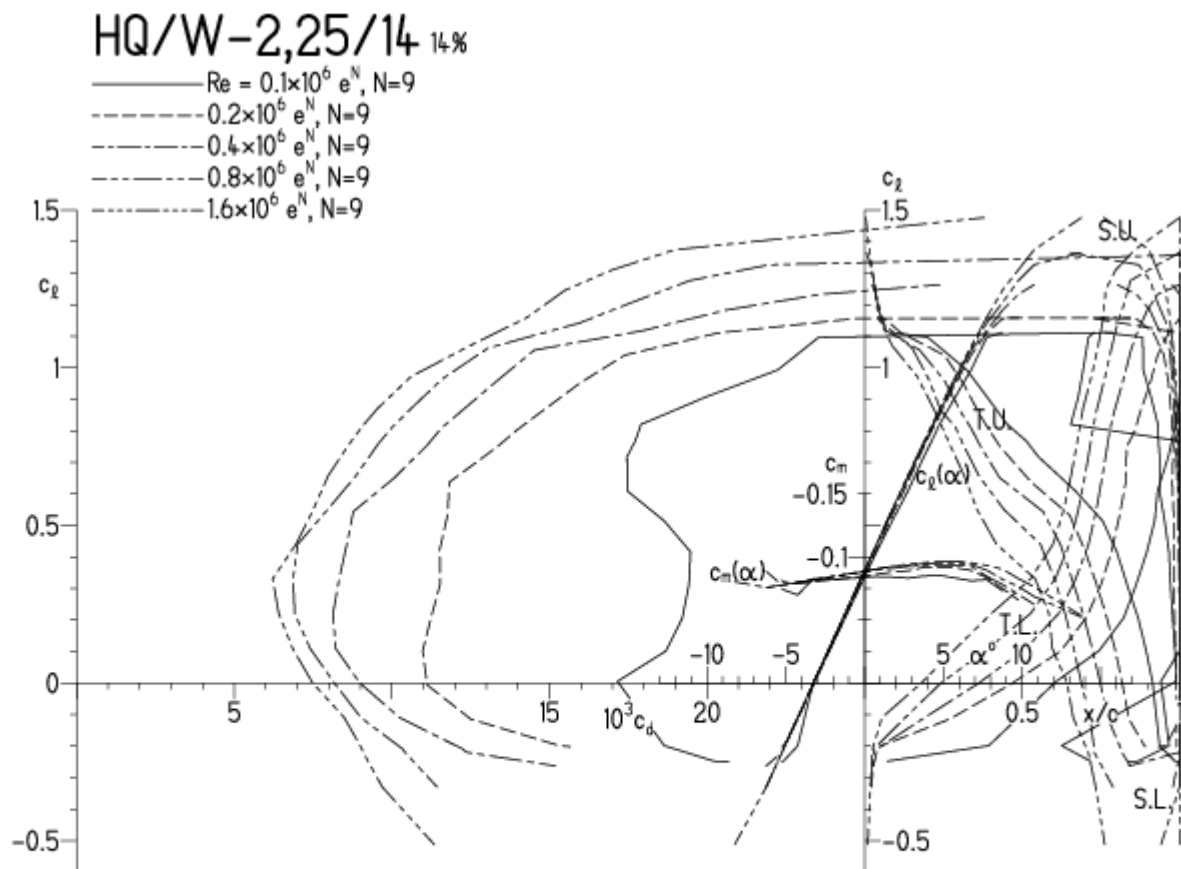


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

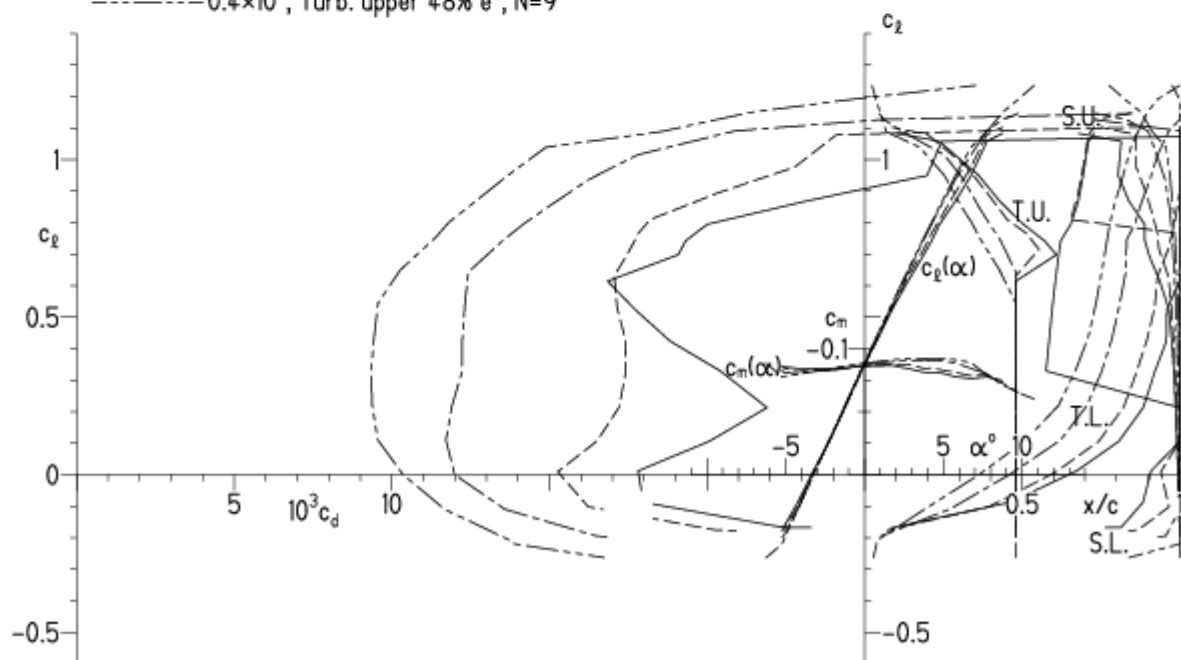
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

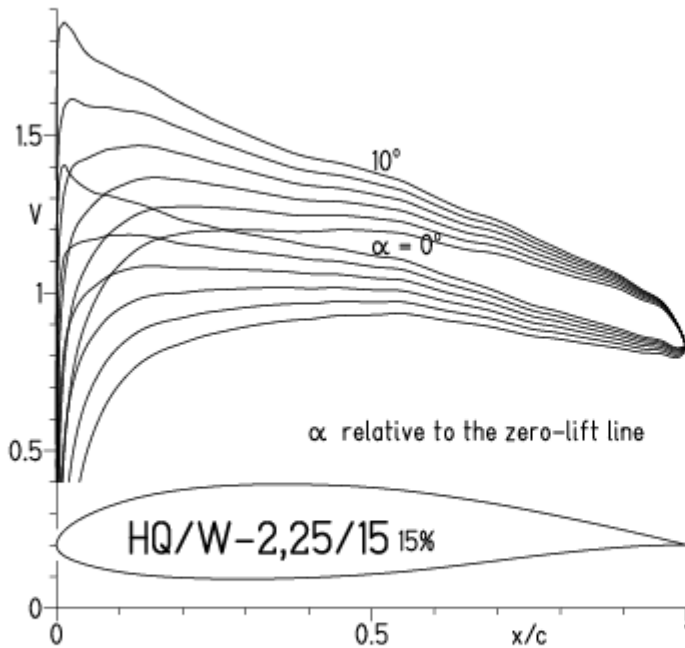


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31

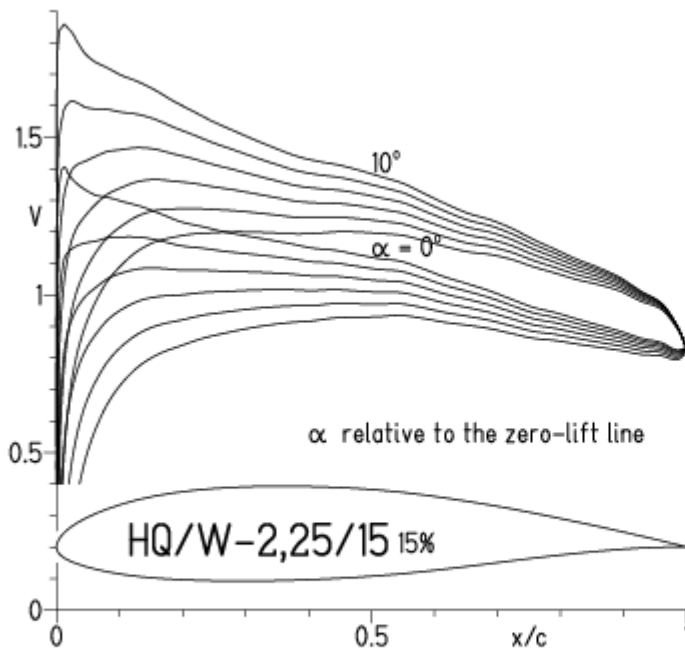


EPPLER 20

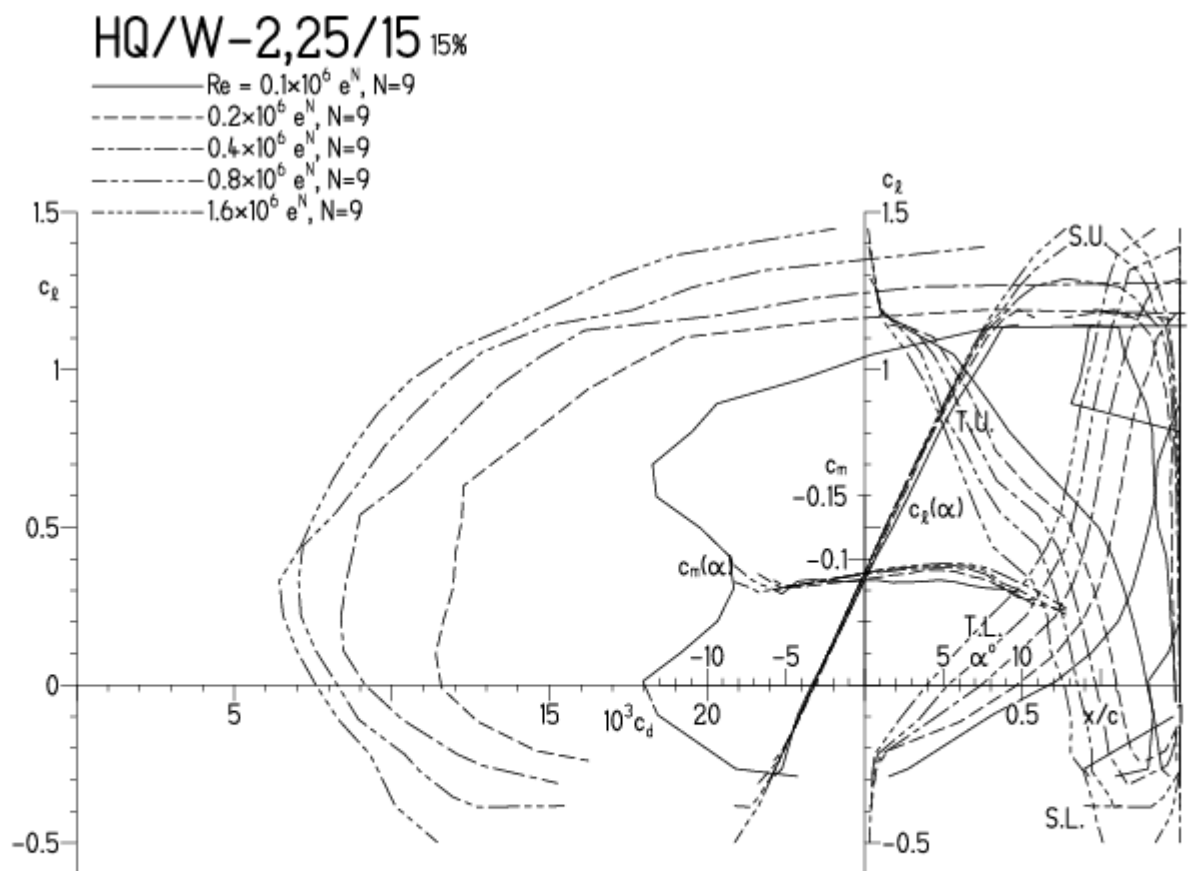


HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

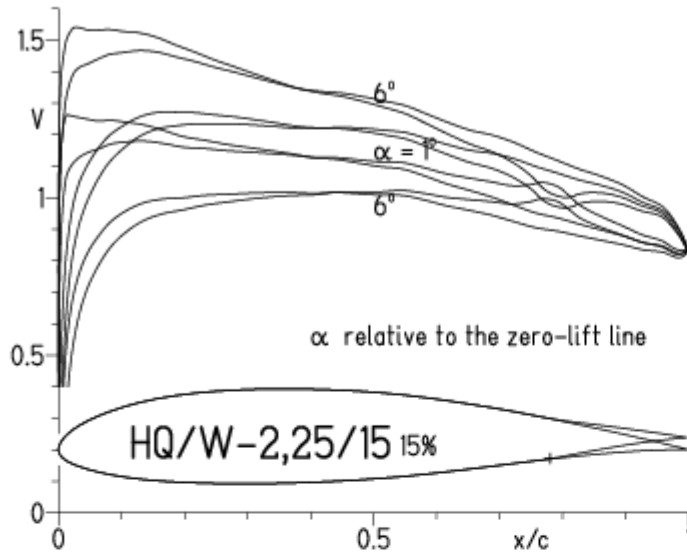


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

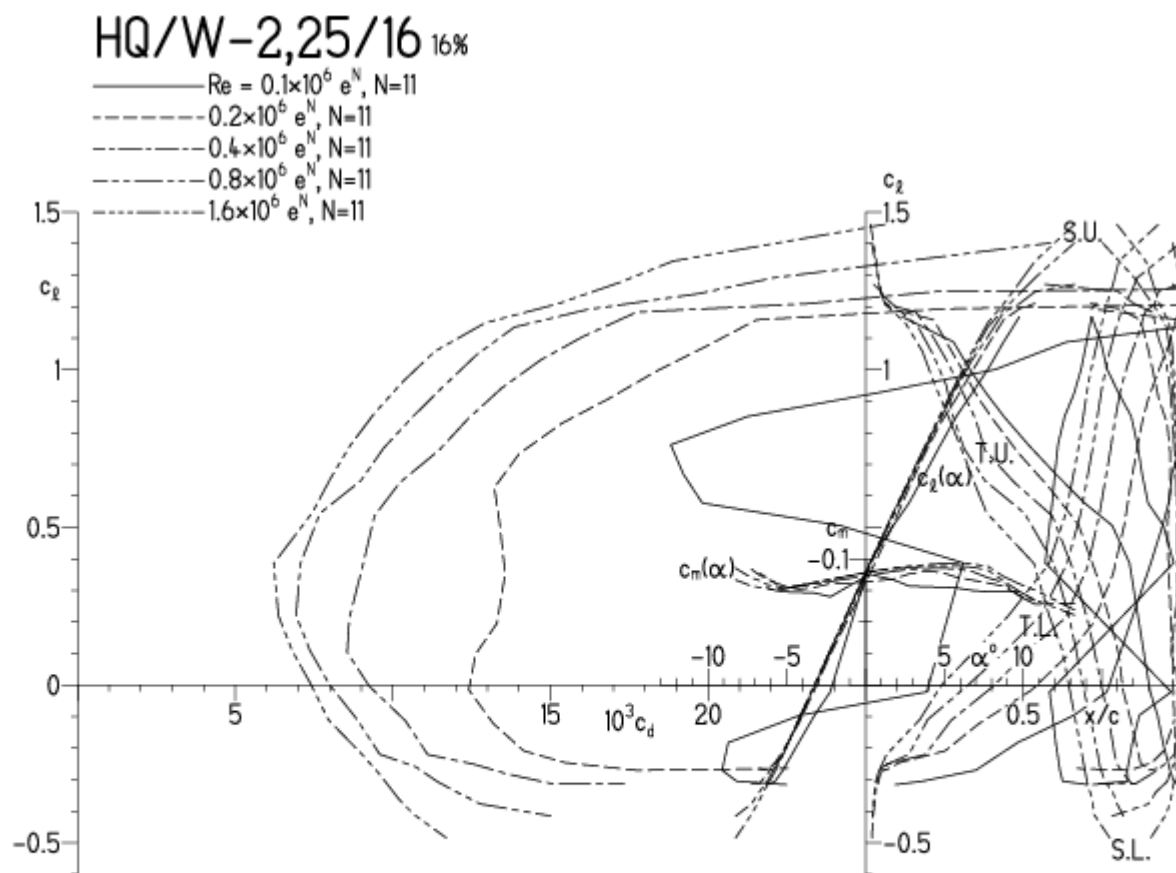


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

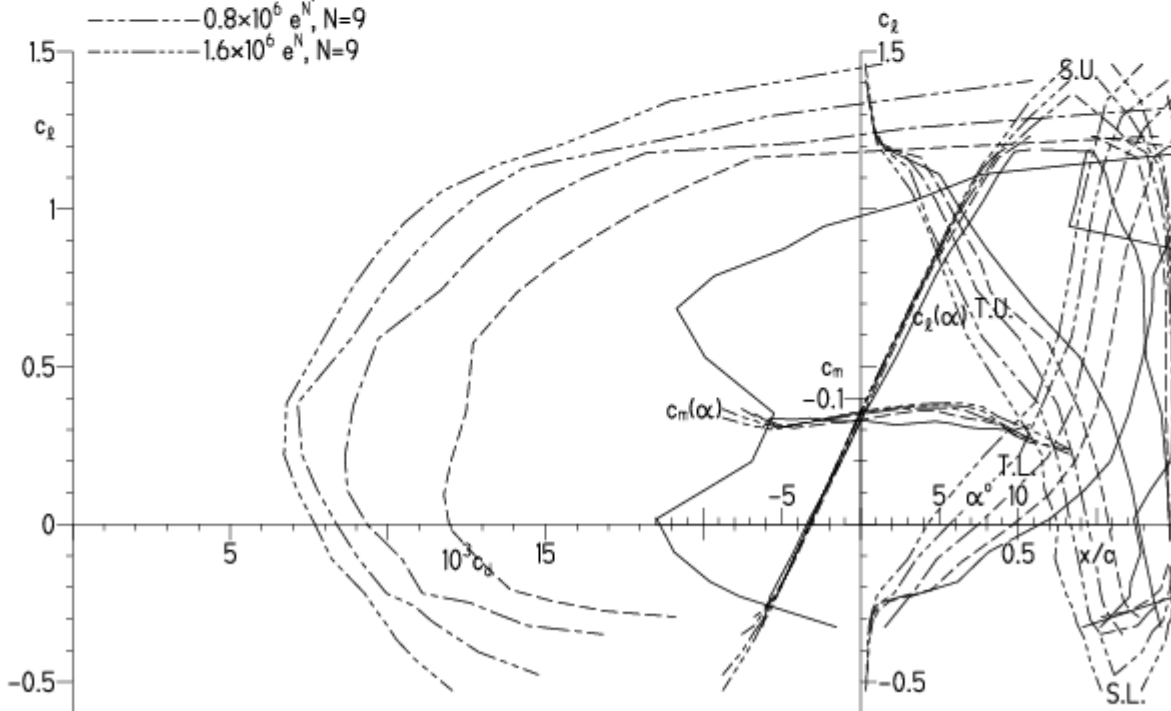
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

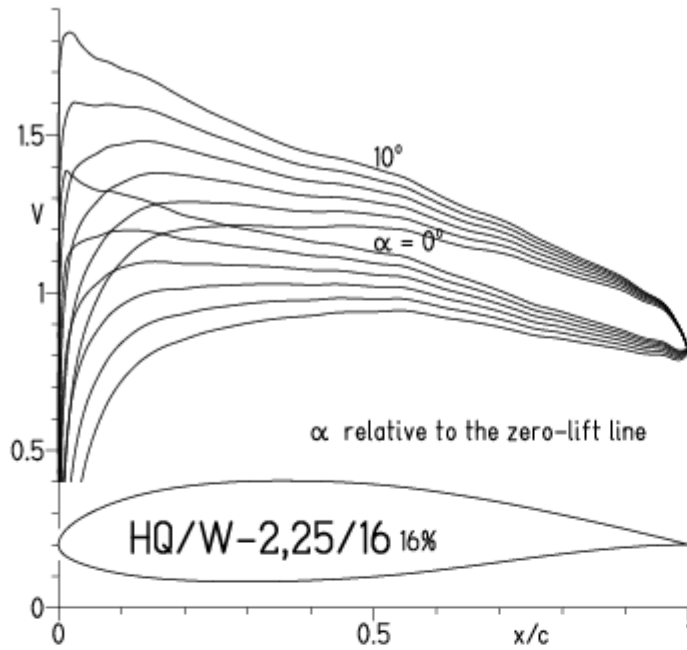
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1.

HQ/W-2,25/8 8%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. $30 - 35 \text{ m/s}$ Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



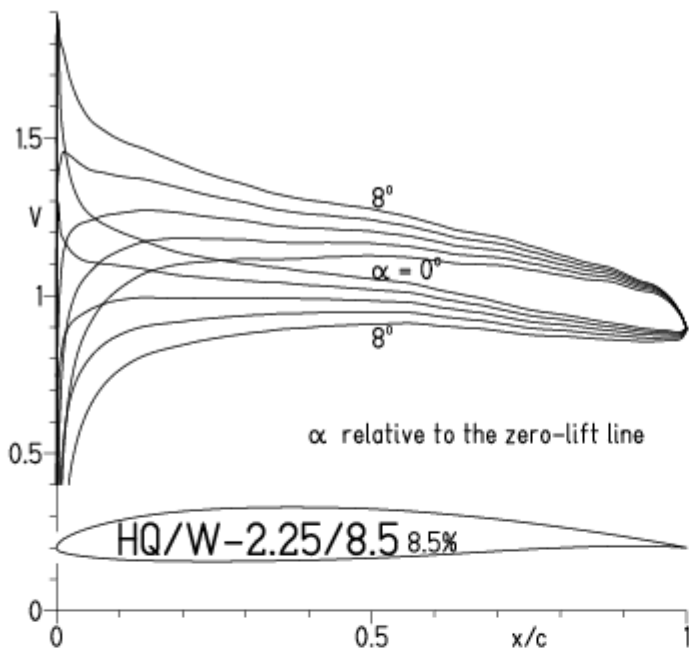
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

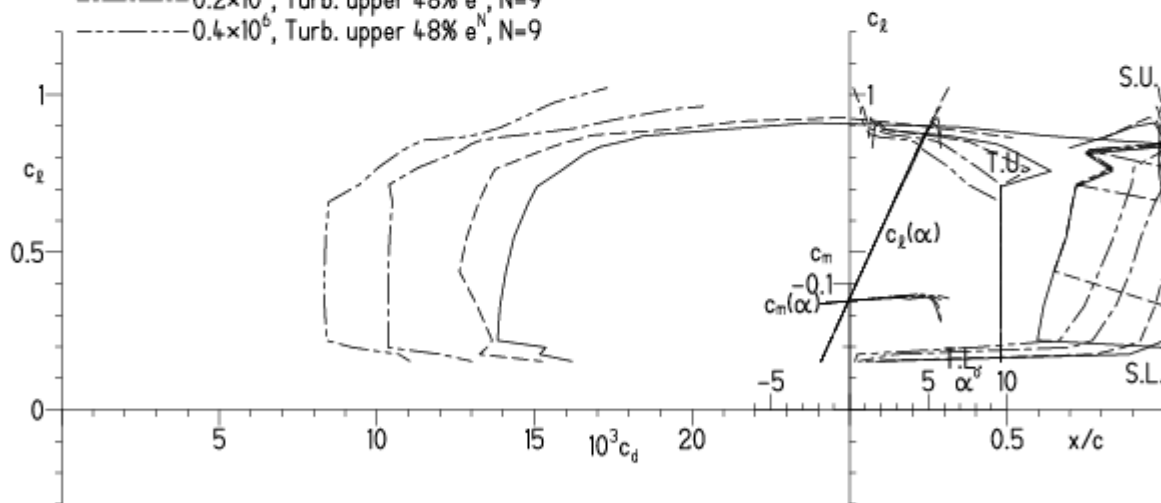
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

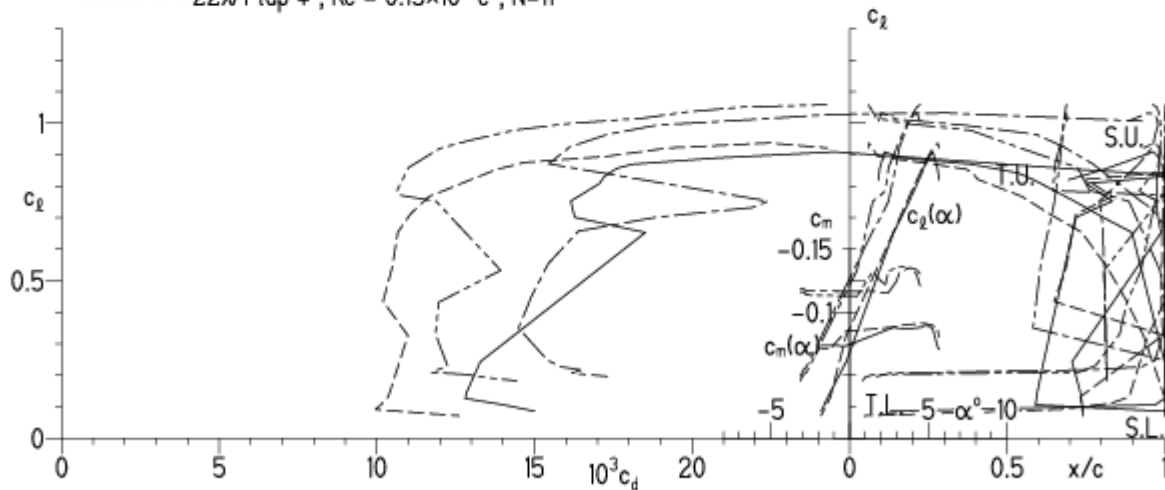


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

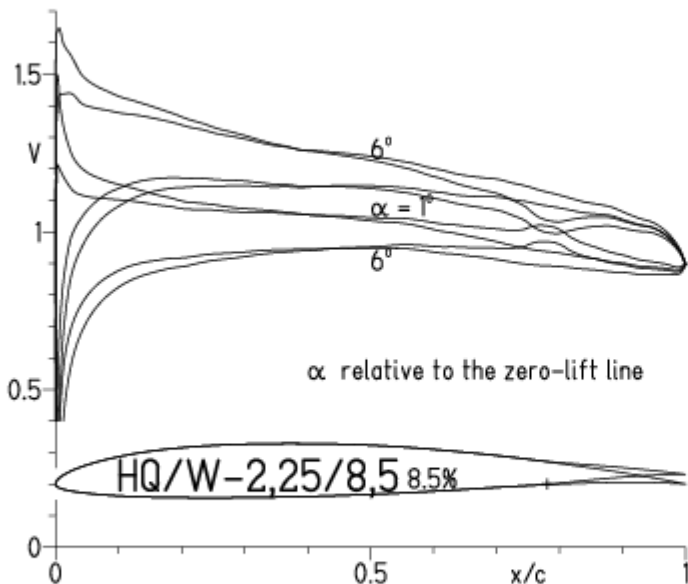
- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

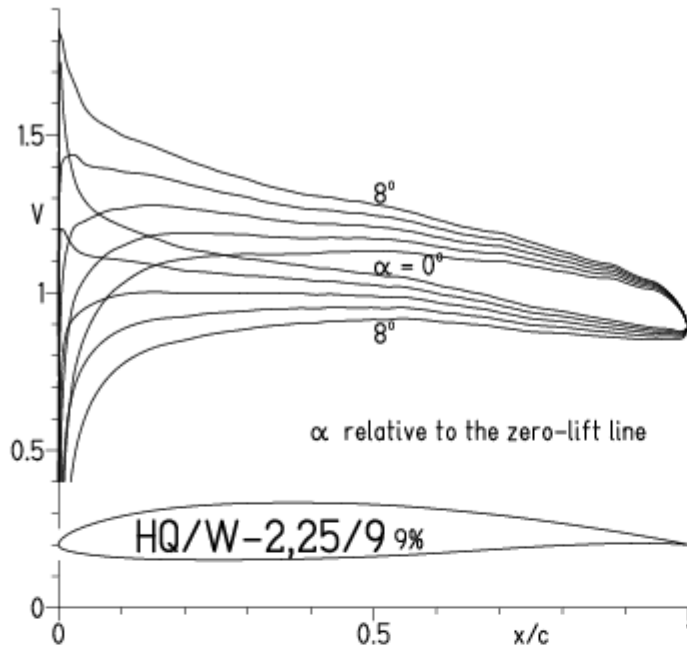


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

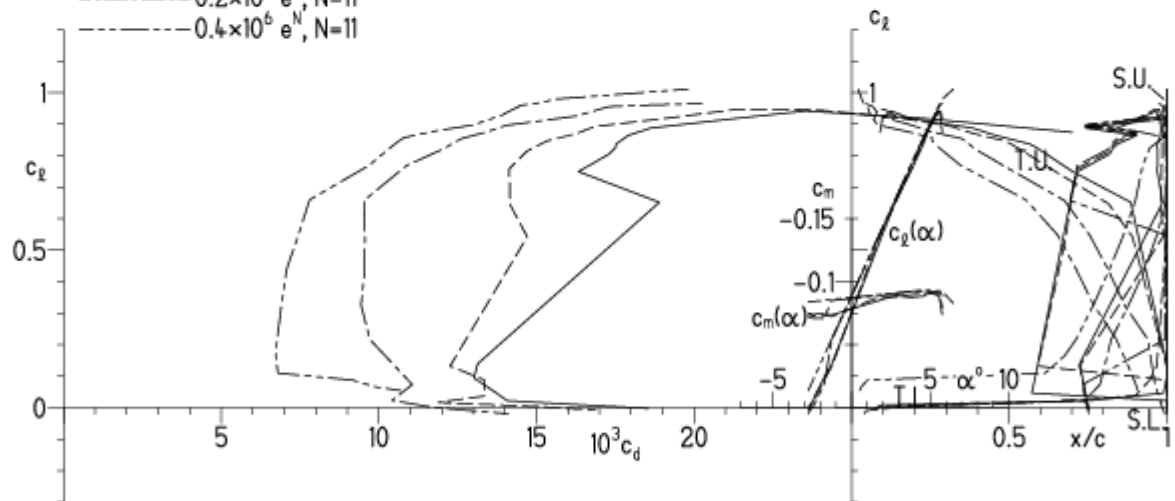
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$

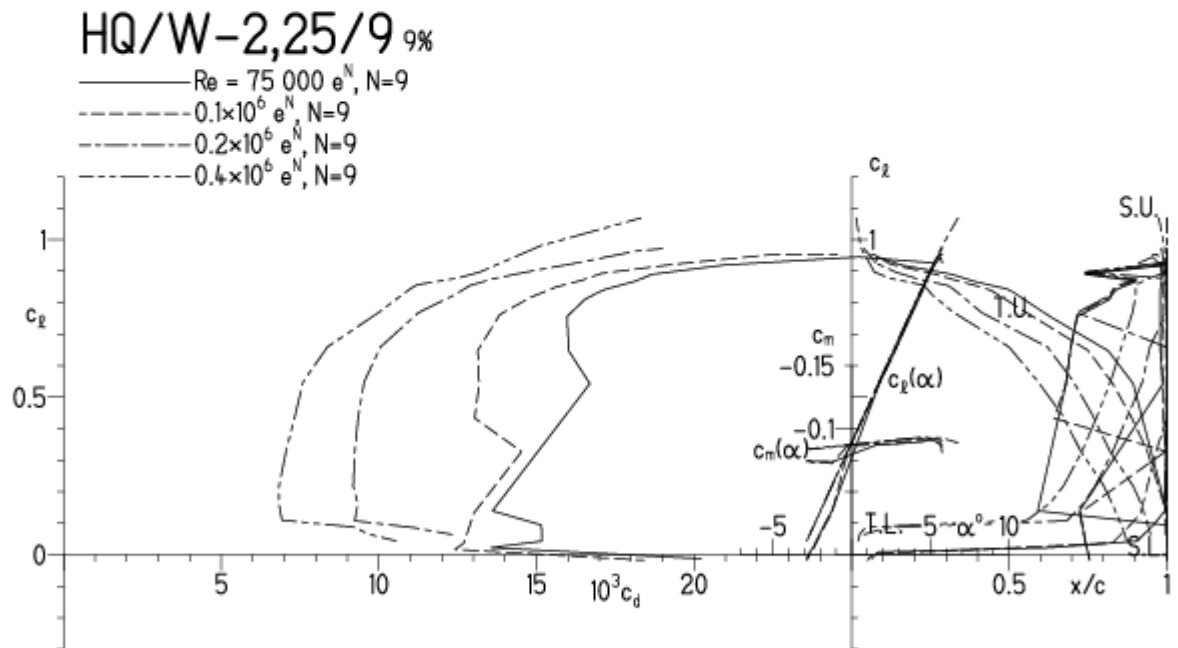


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

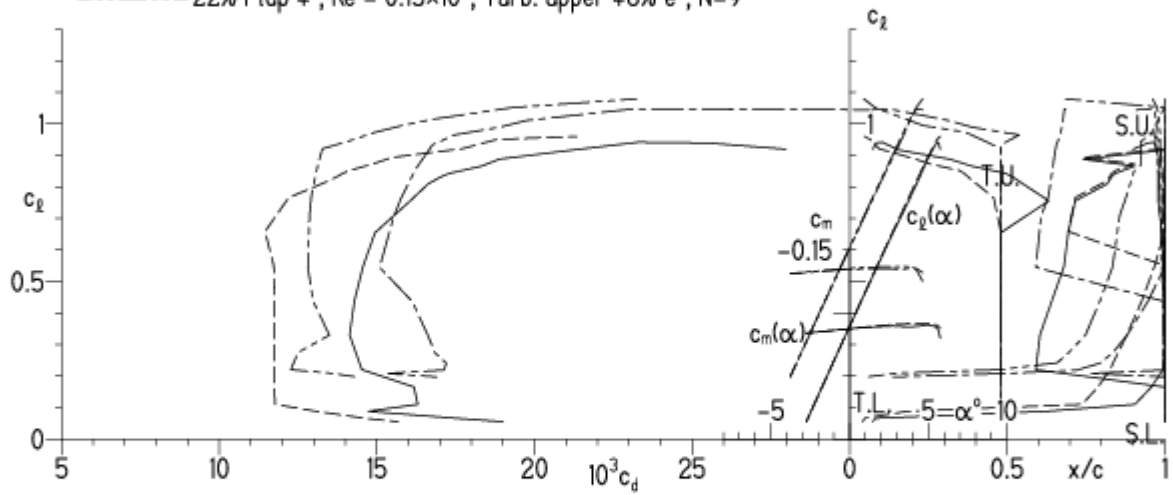


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

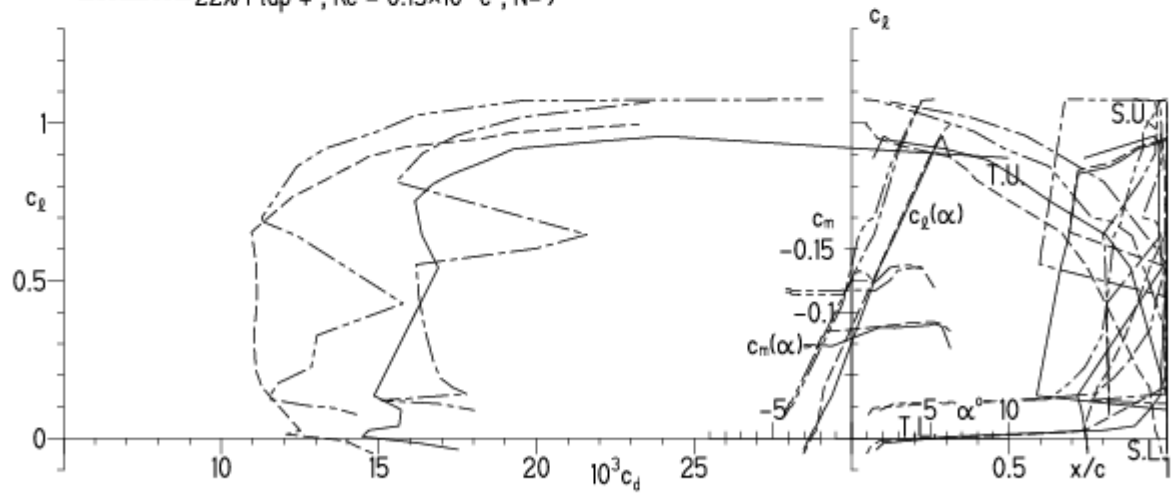


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

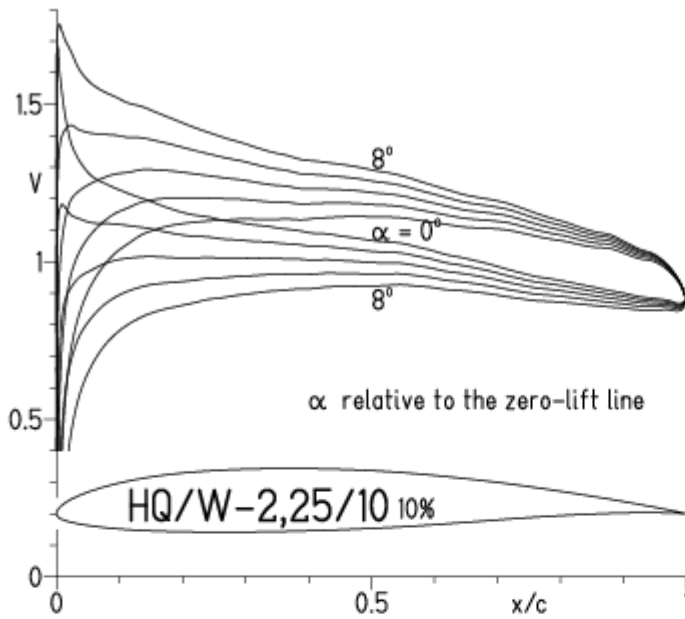


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

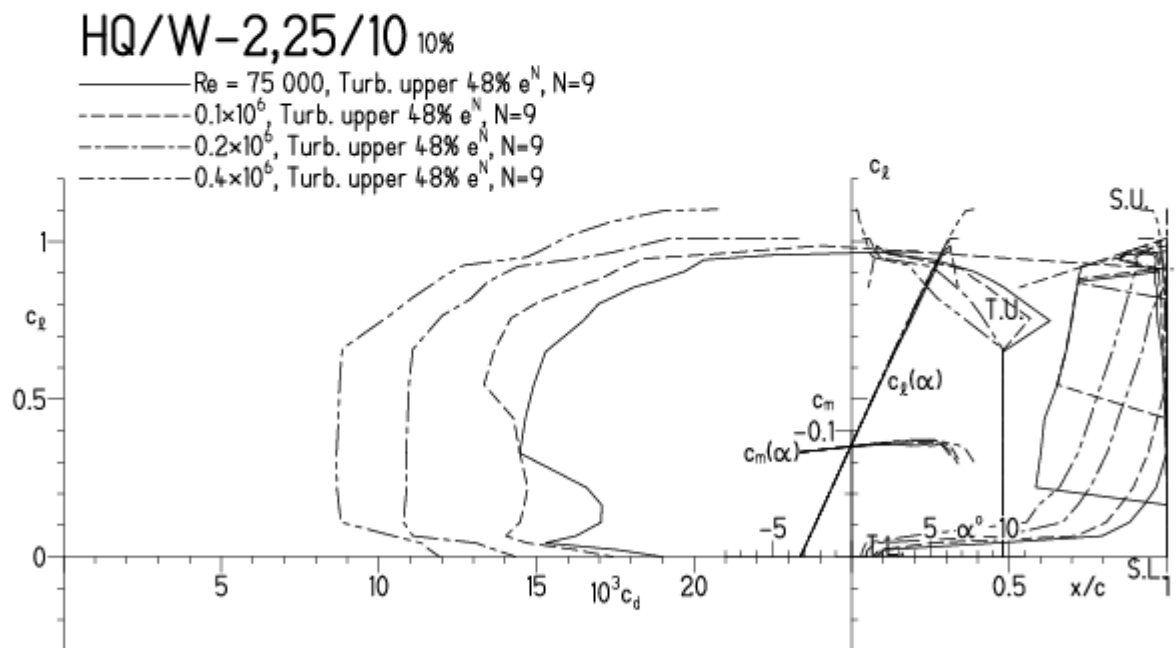


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

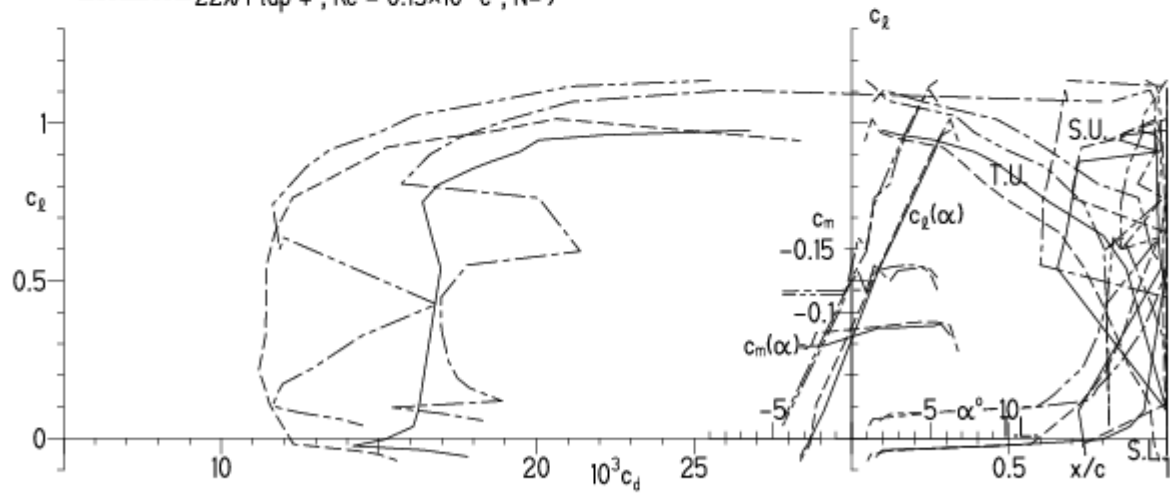


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- Re = 0.2×10^6 e^N, N=9
- - - Re = 0.8×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.2×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.8×10^6 e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12

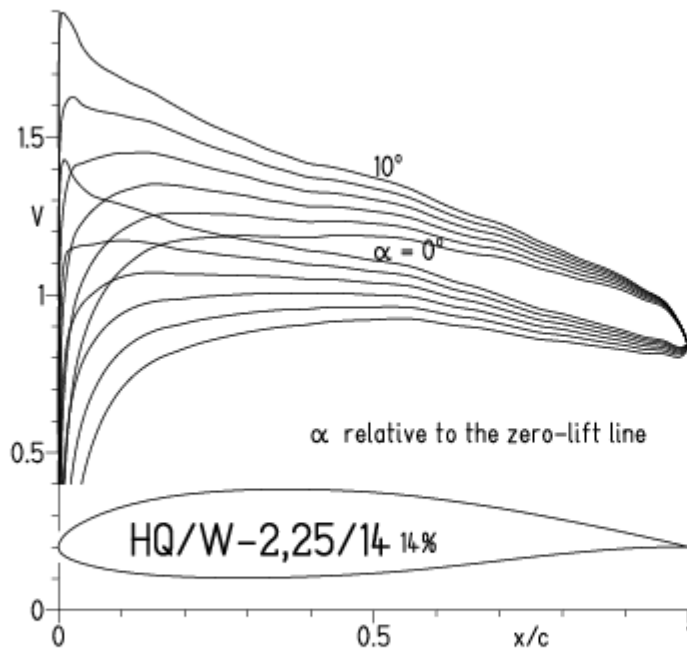


EPPLER 2005 V. 8.

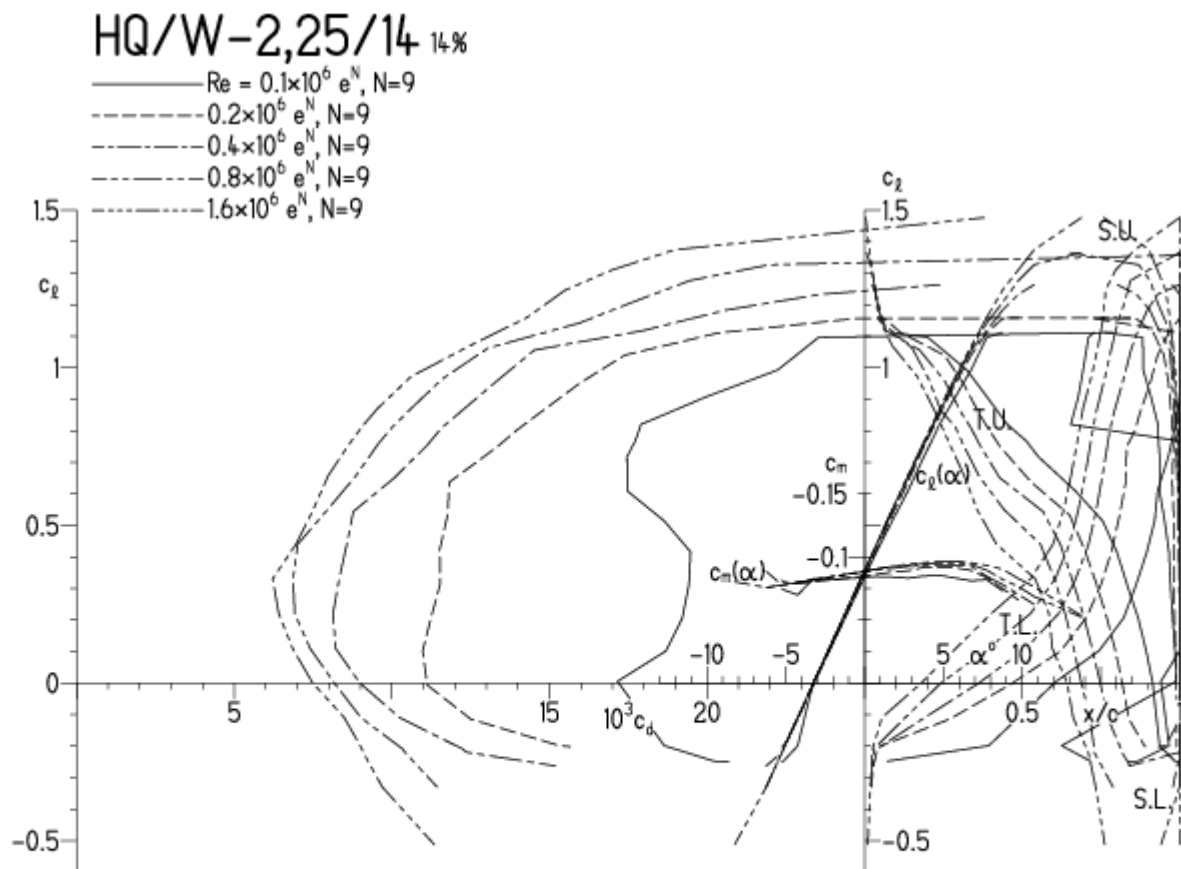


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

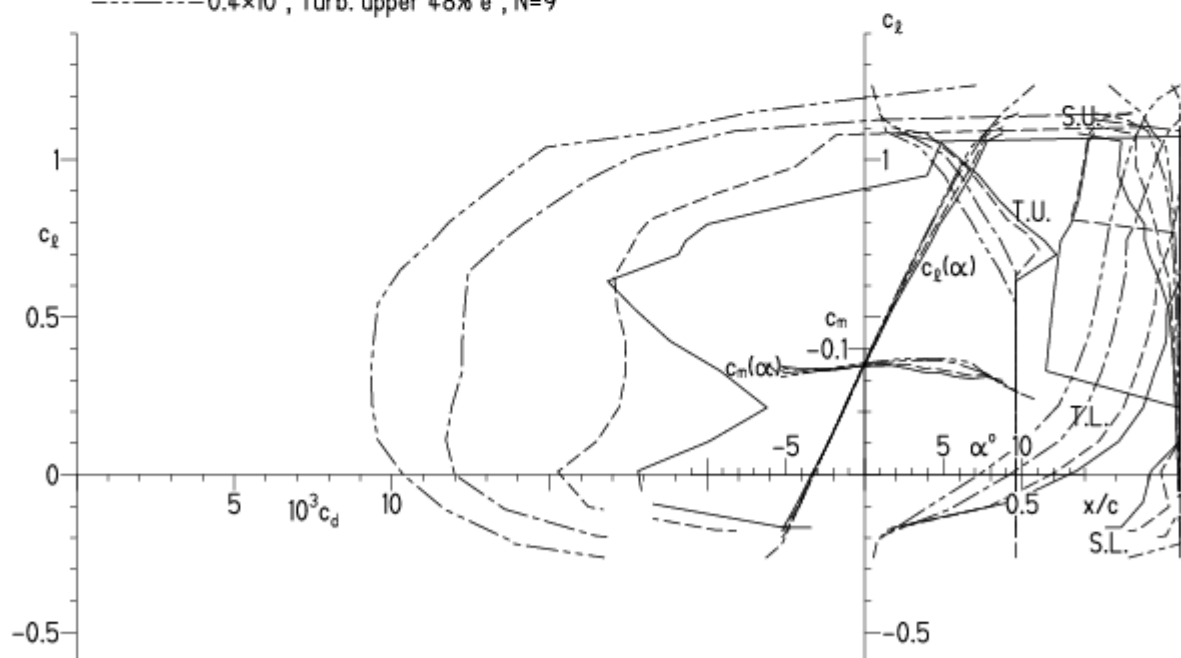
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

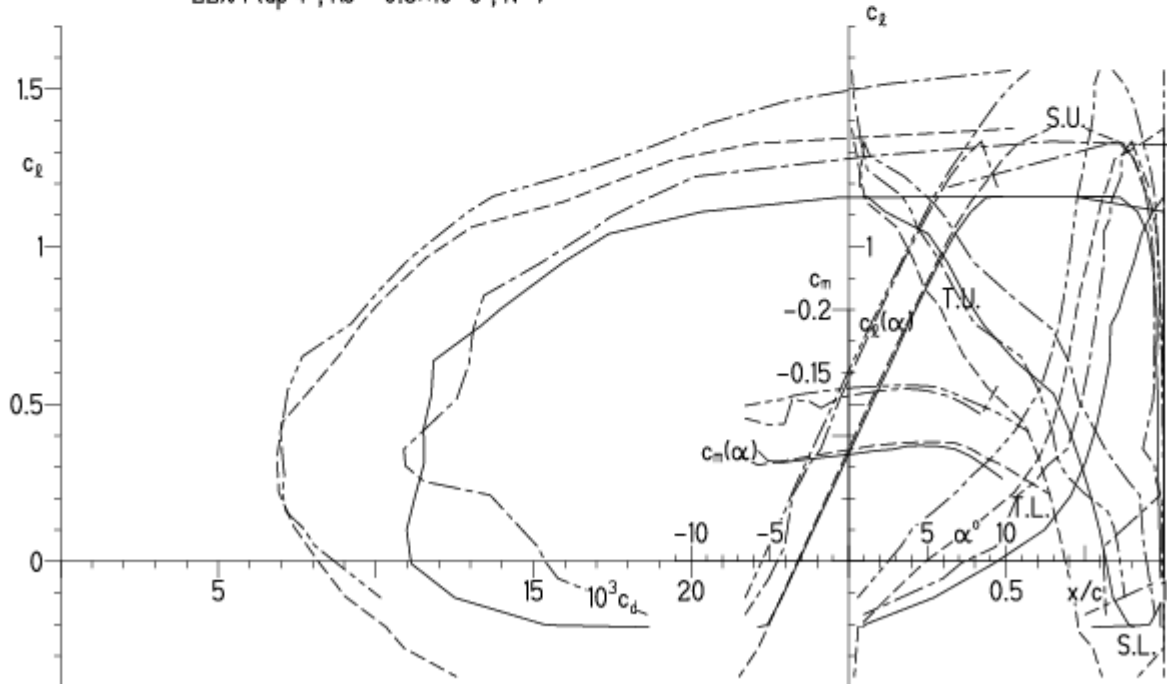


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

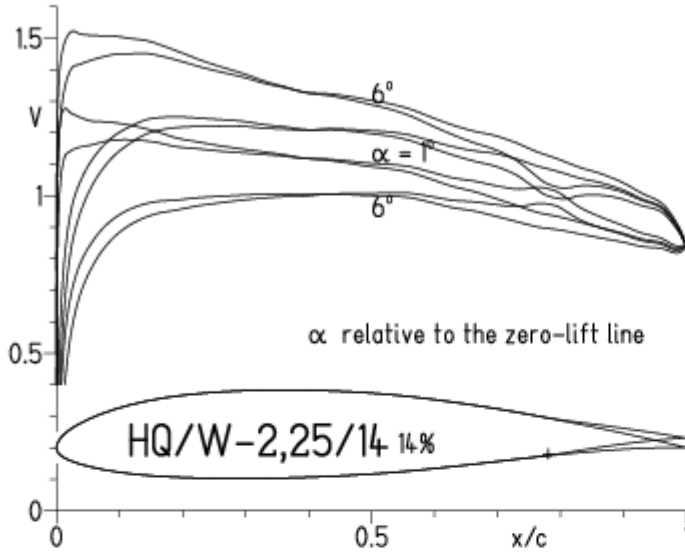
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

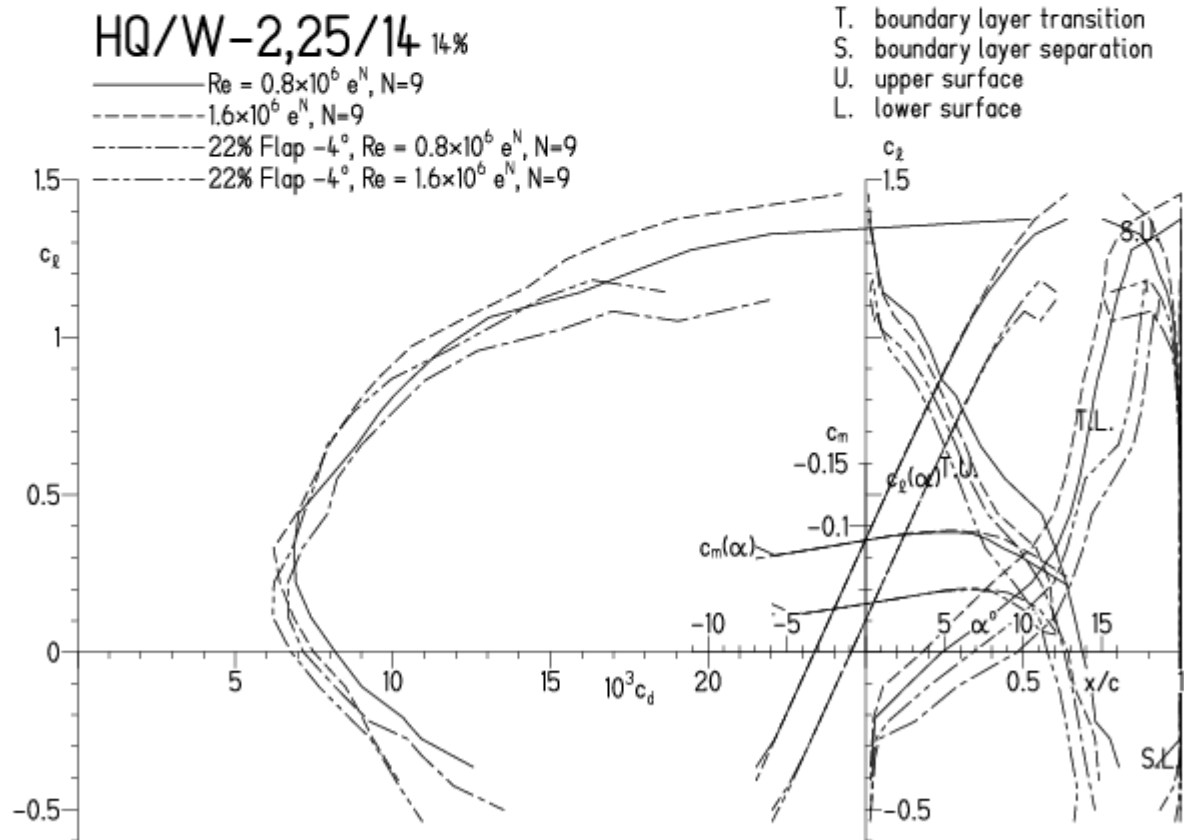


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

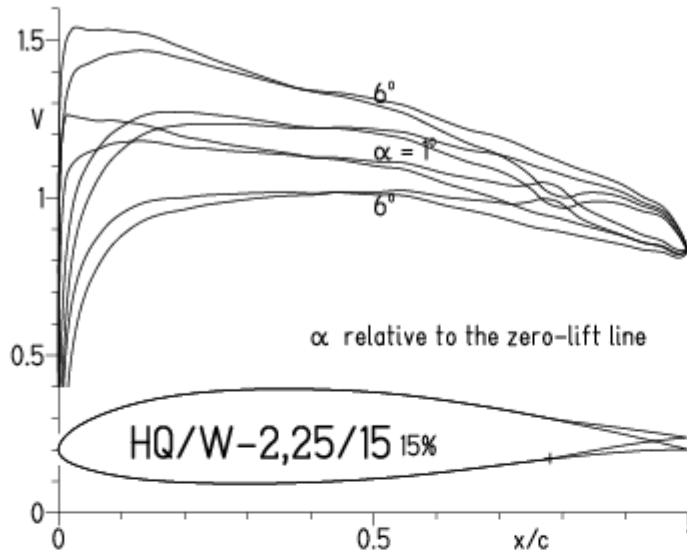


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- - - - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - · 22% Flap 4°, Re = 75 000 e^N, N=9
- · - · 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

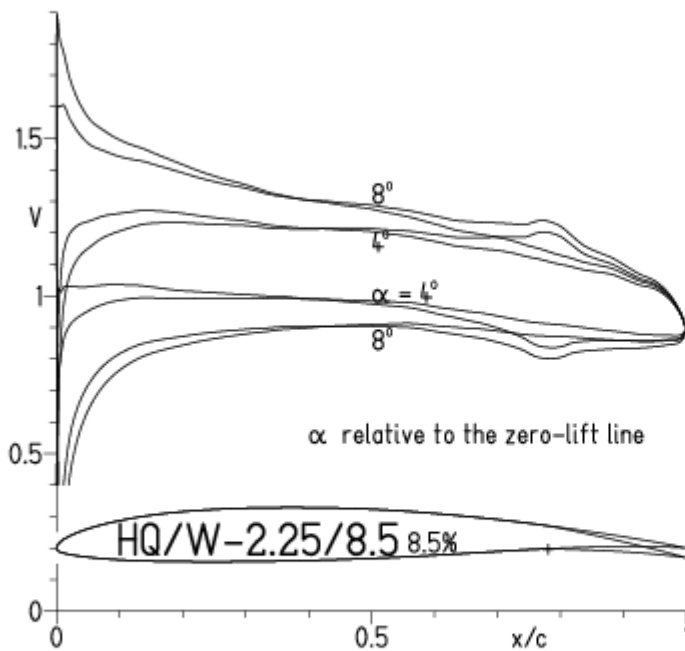
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

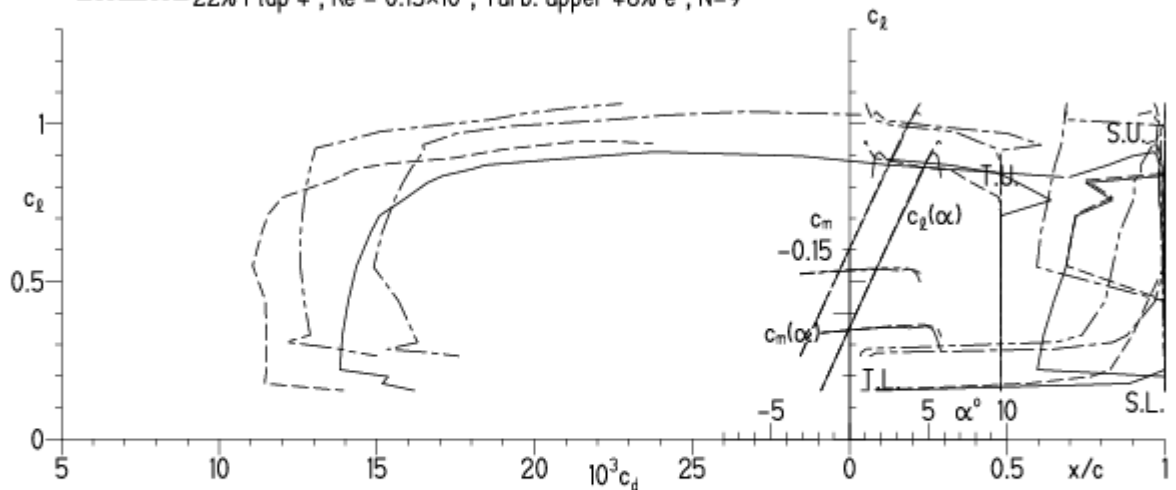


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · · - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

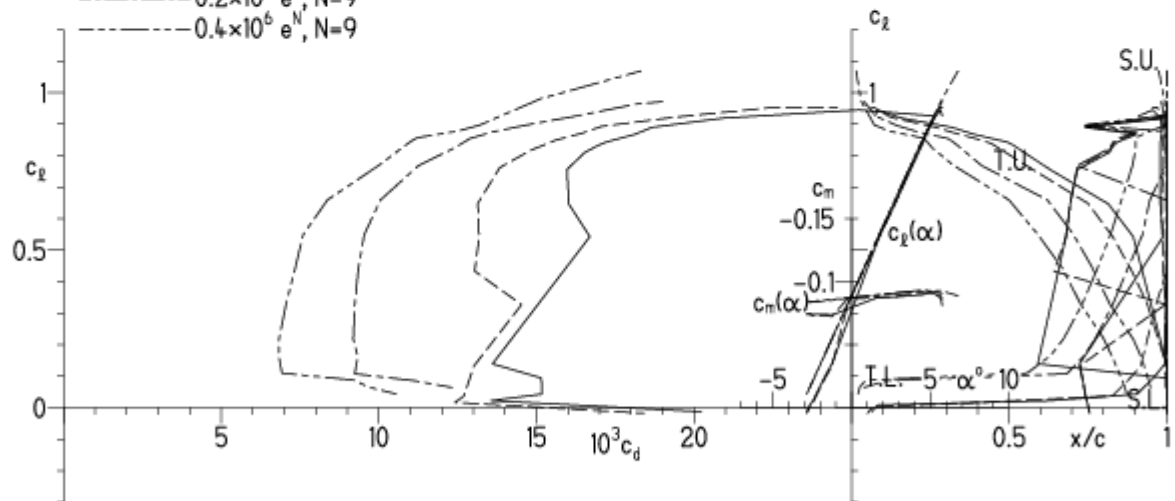
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

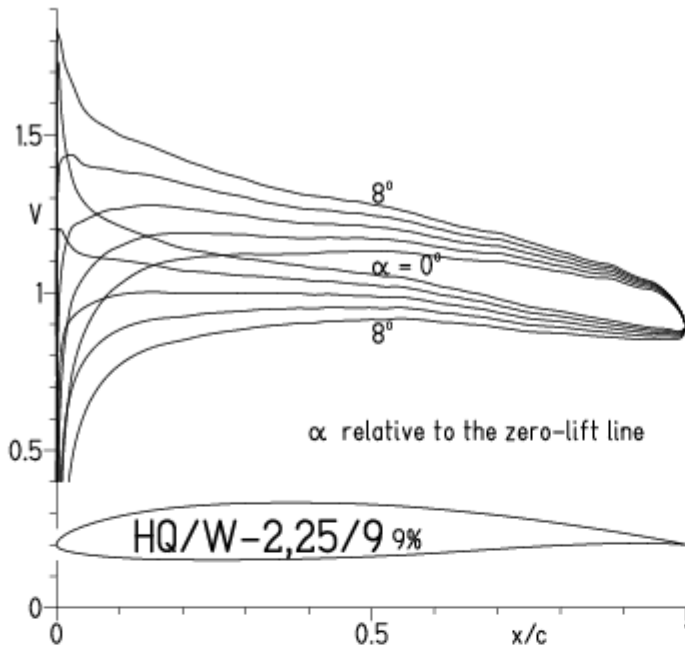
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

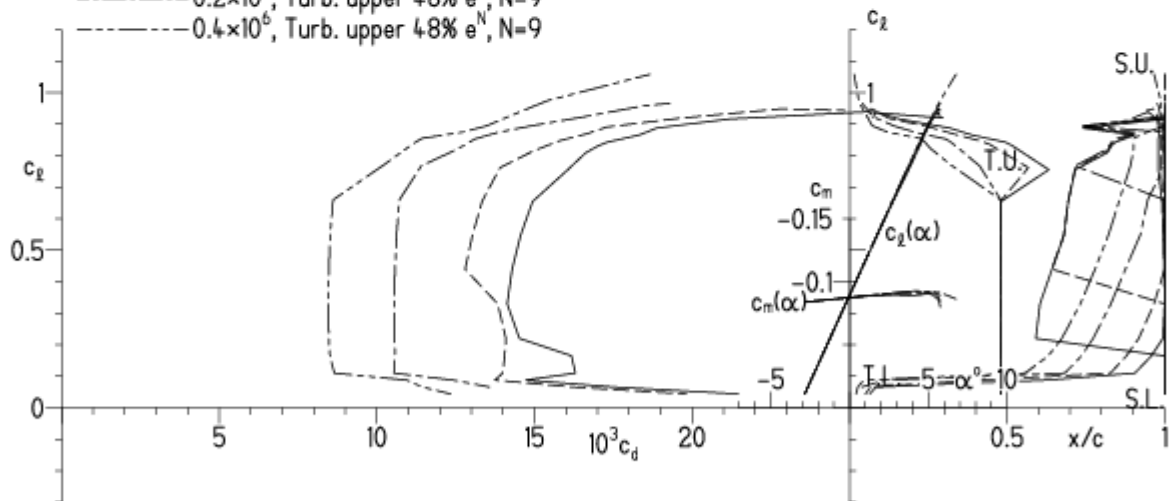
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48

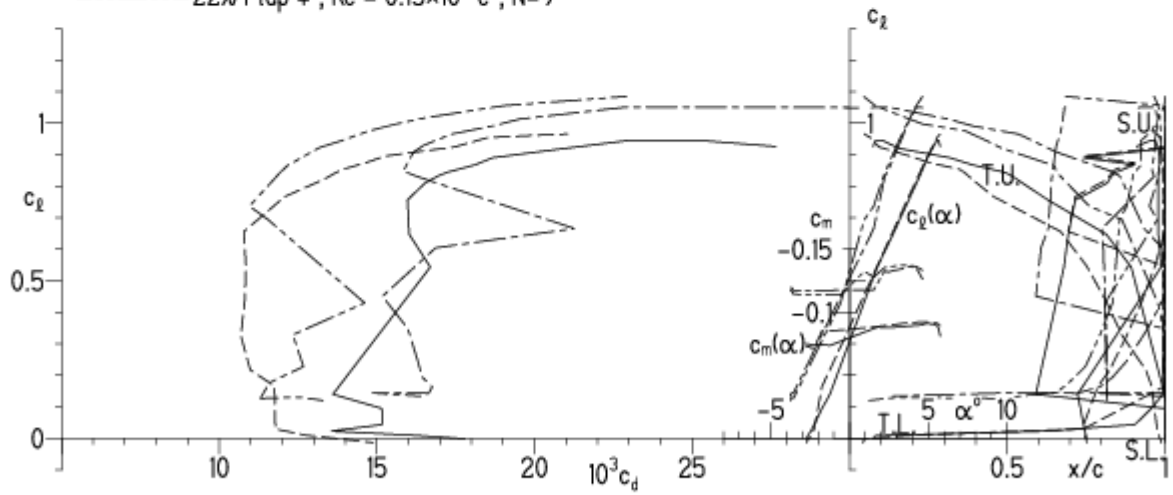


EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2 × 10⁶ e^N, N=11
- - - 0.6 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.2 × 10⁶ e^N, N=11
- · - · 22% Flap -4°, Re = 0.6 × 10⁶ e^N, N=11



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

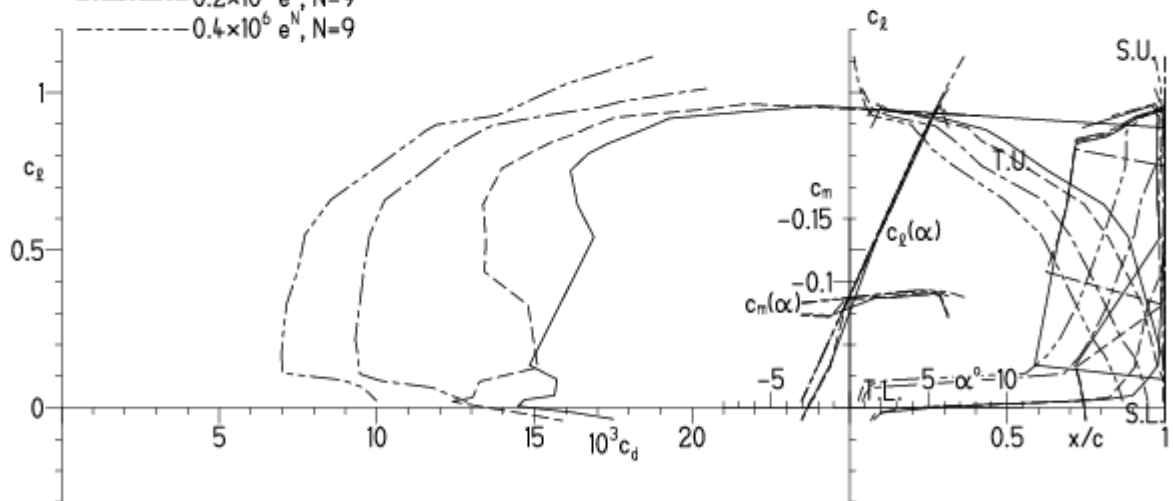
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

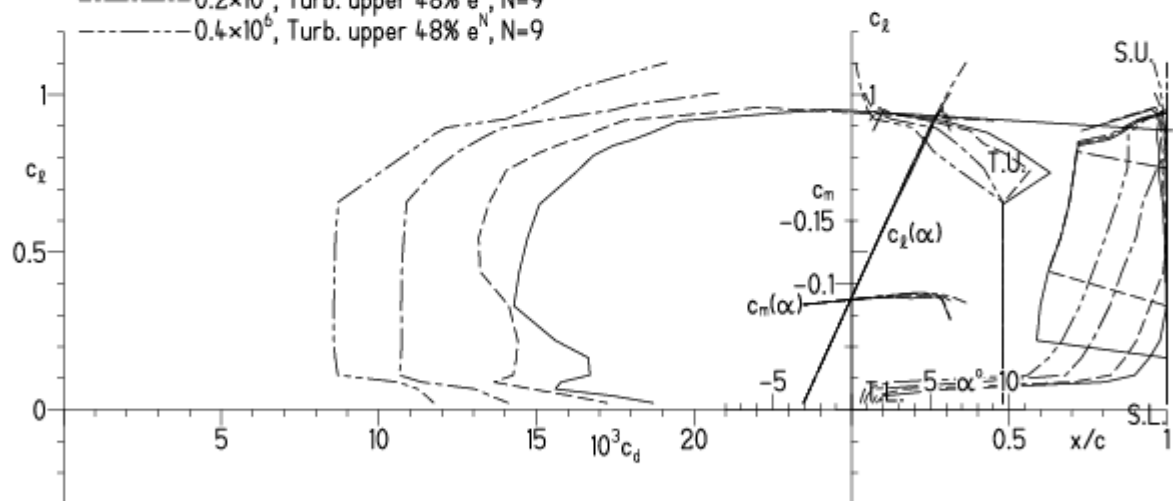
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

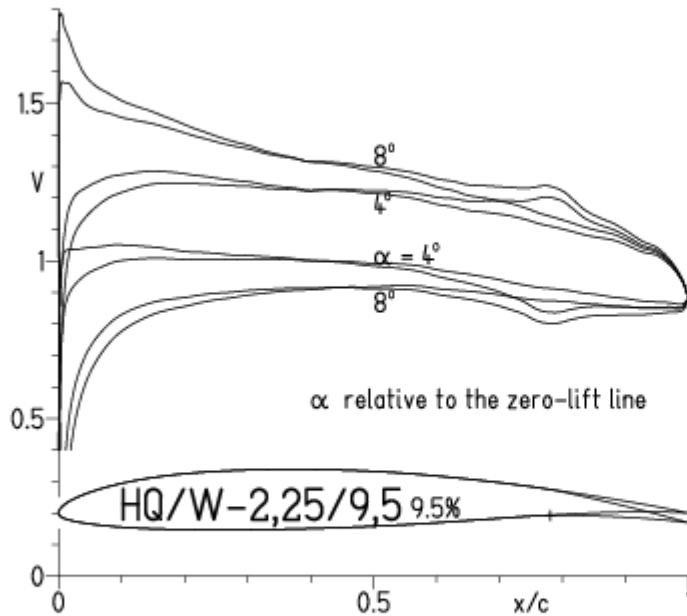
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

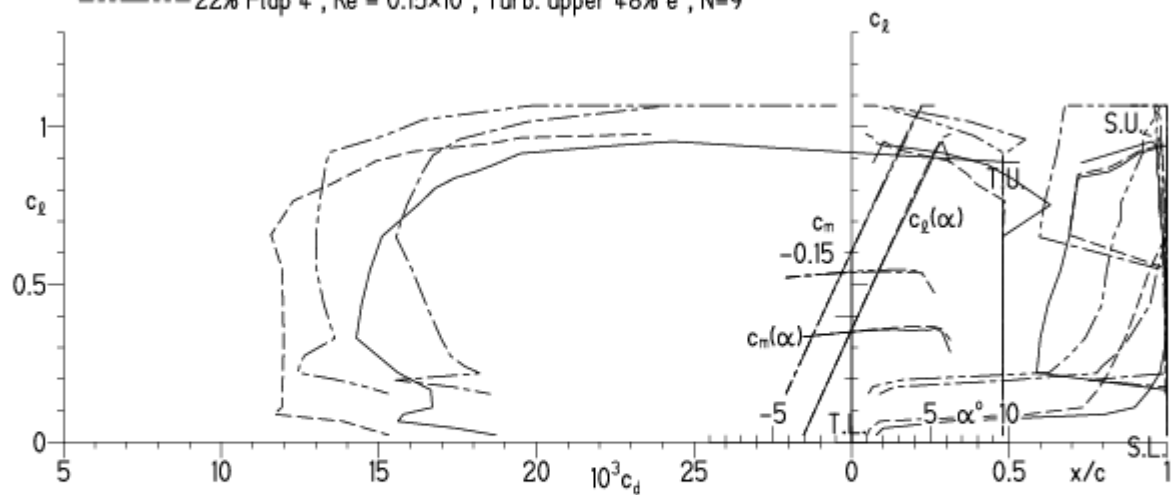


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

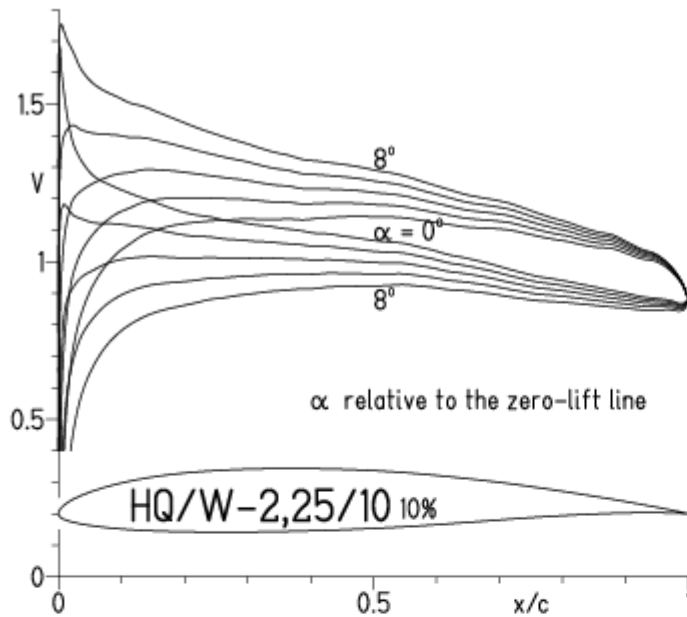


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

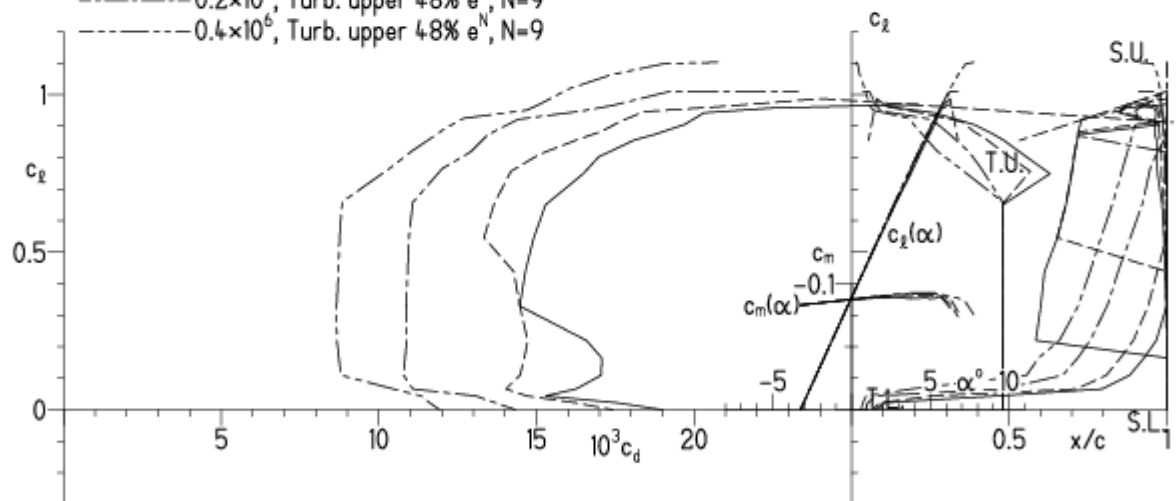
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

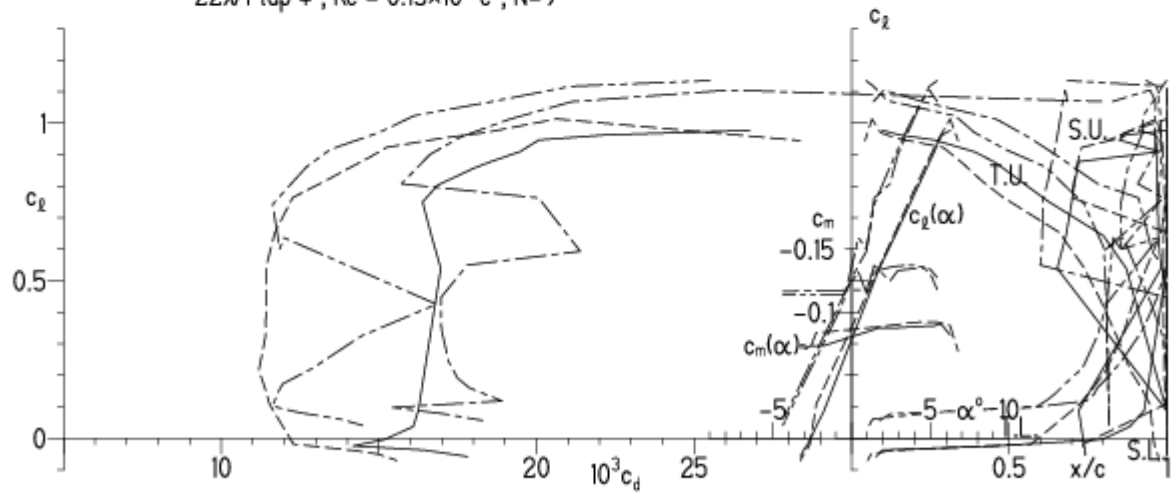


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

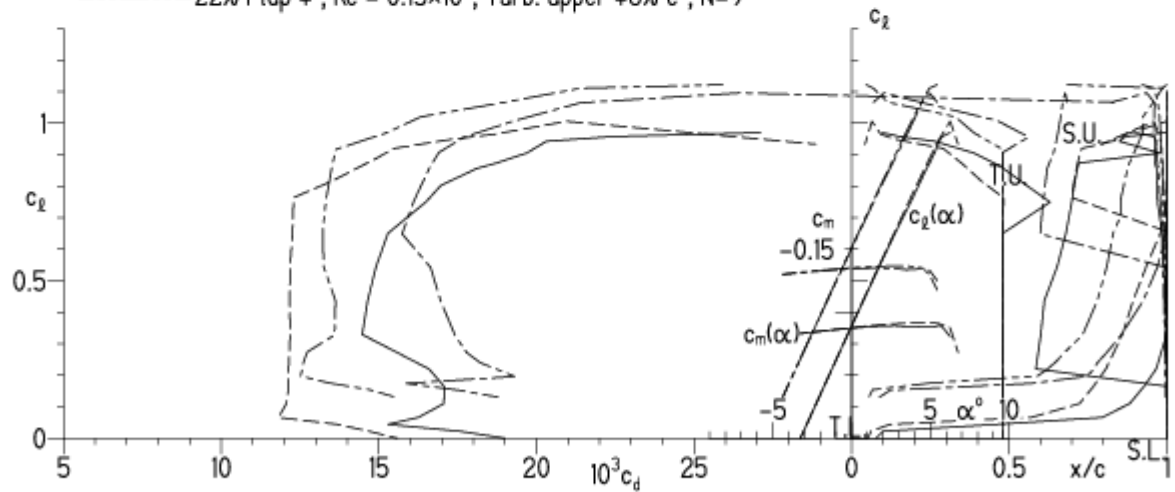


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

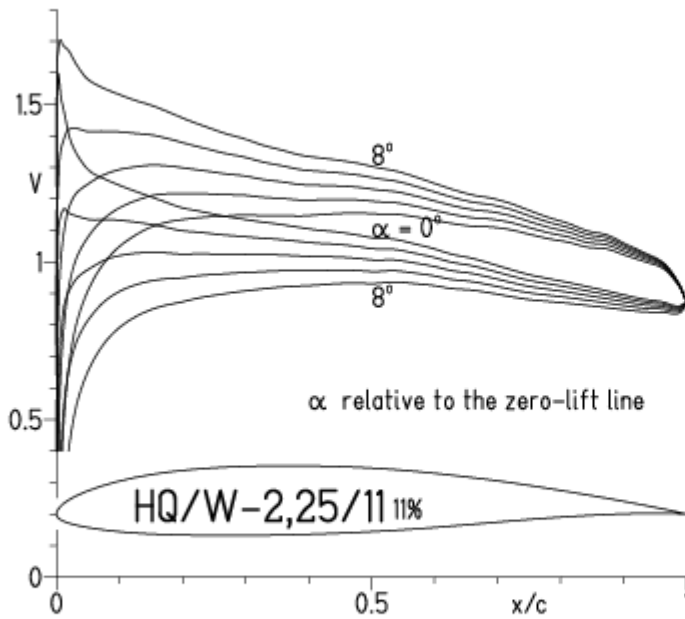


EPPLER 2005 V. 8.5.07 RUN

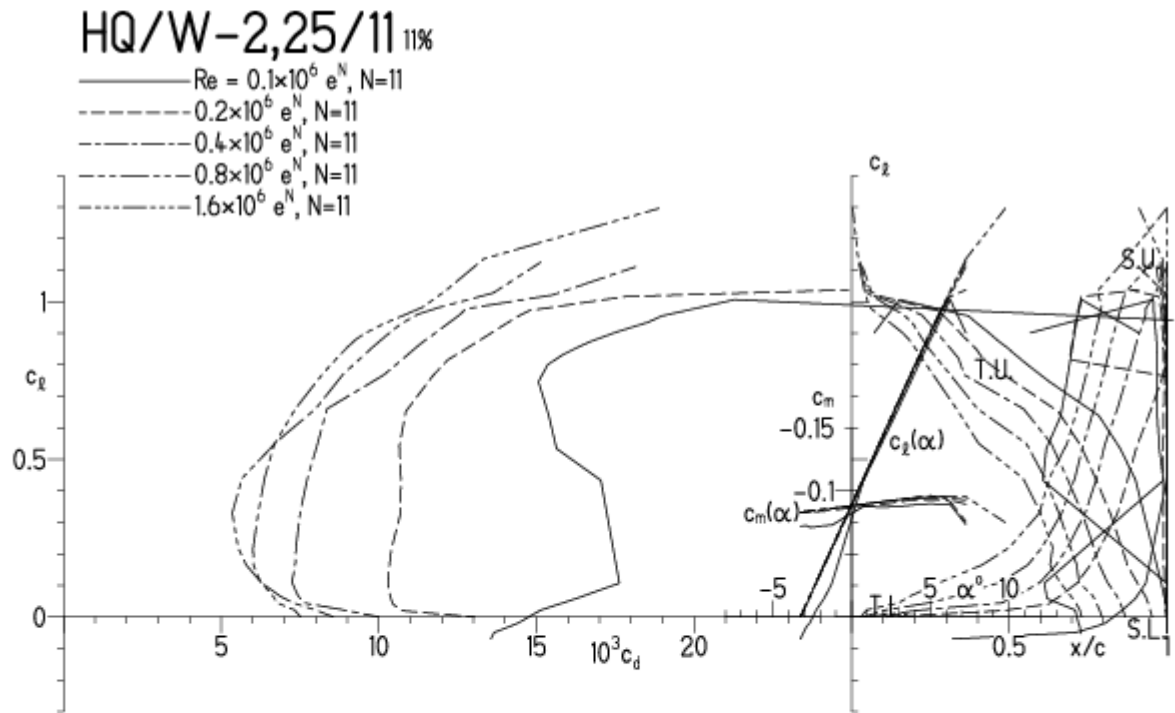


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

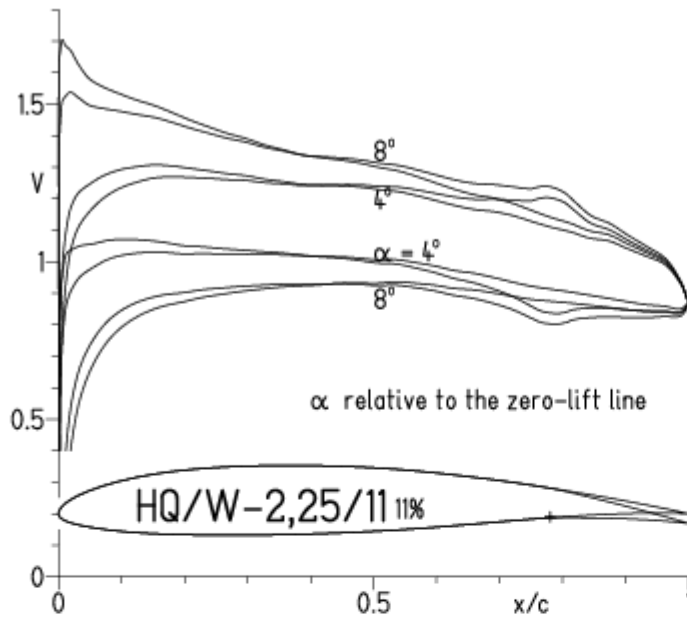
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

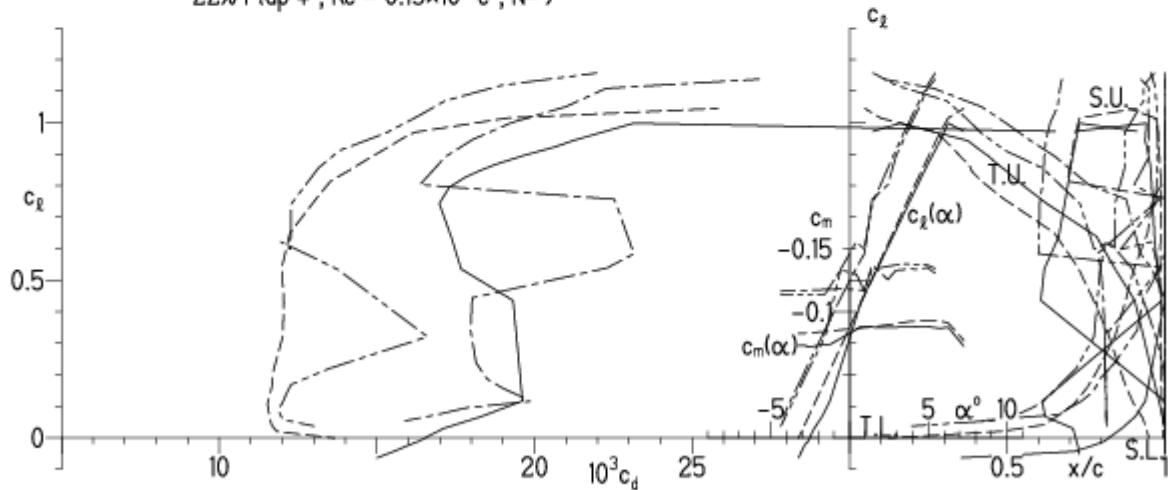


EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

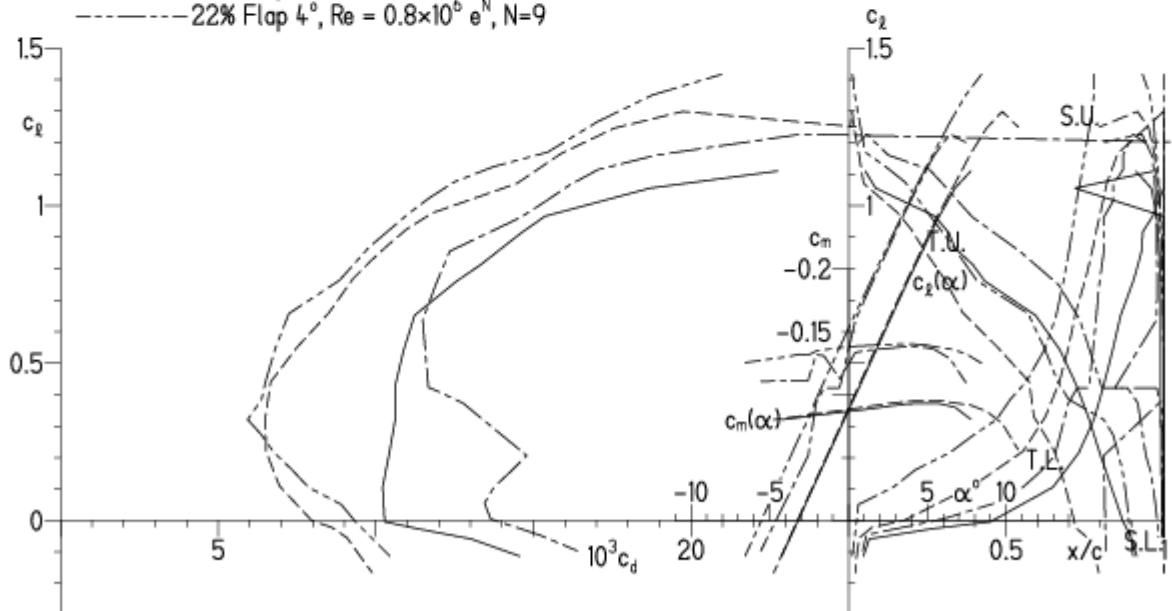


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

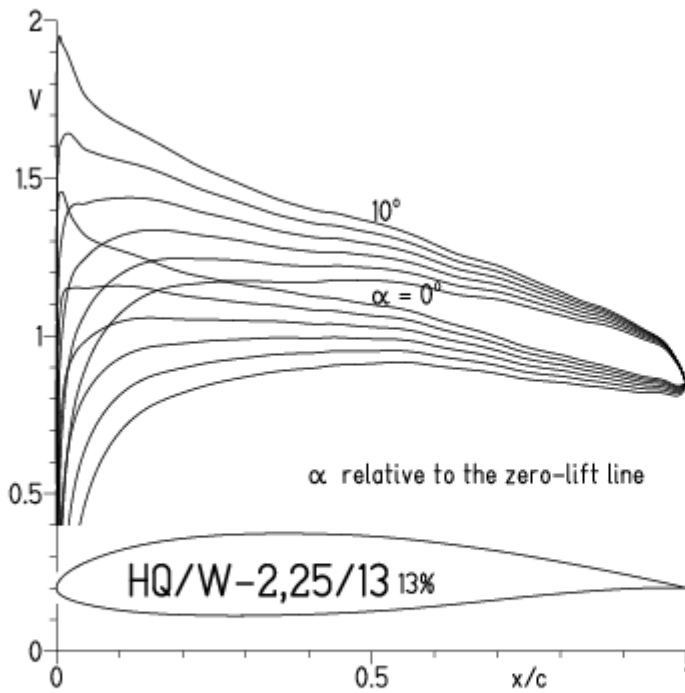


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

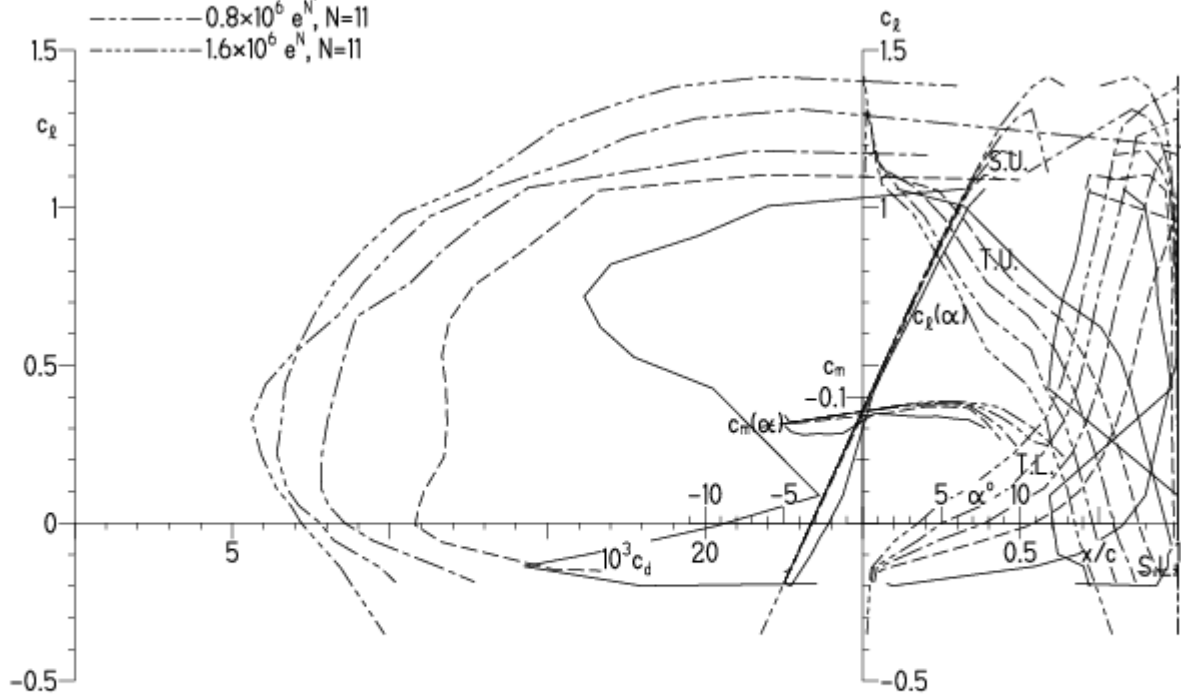
EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

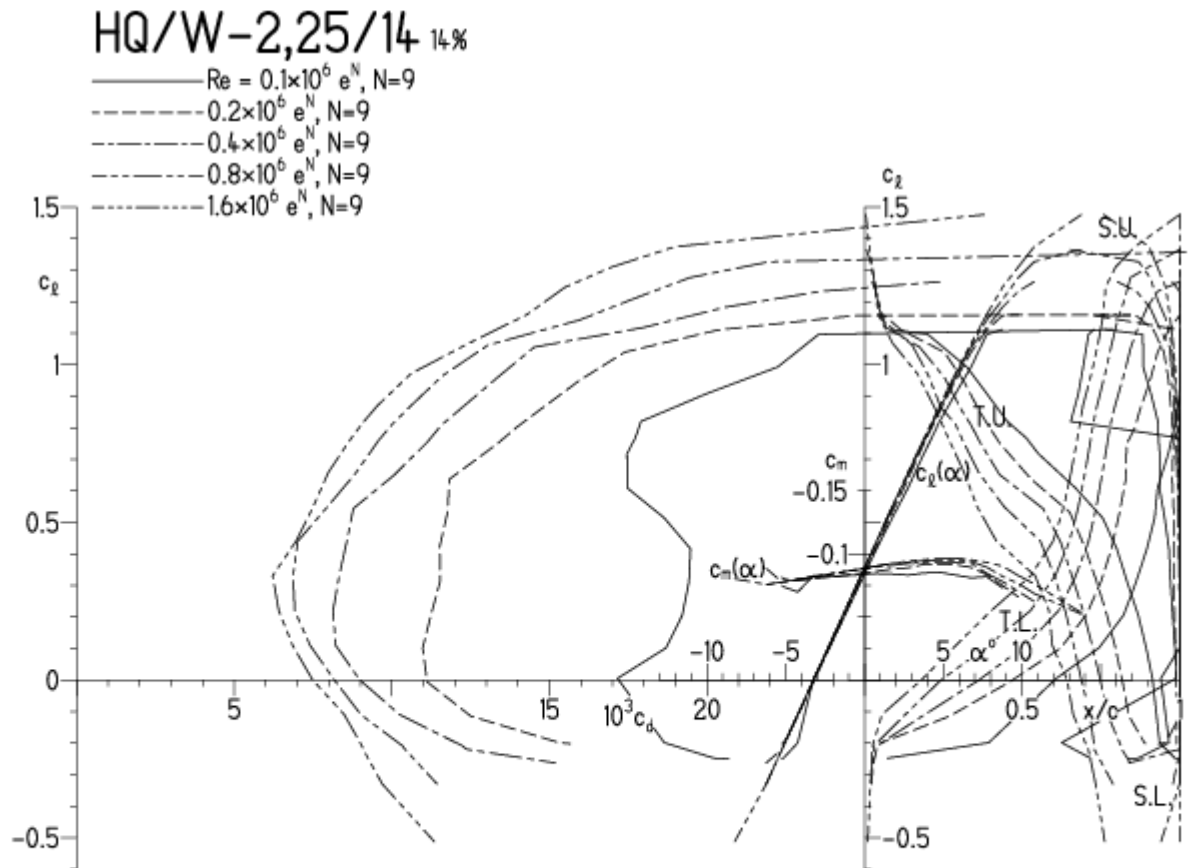


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

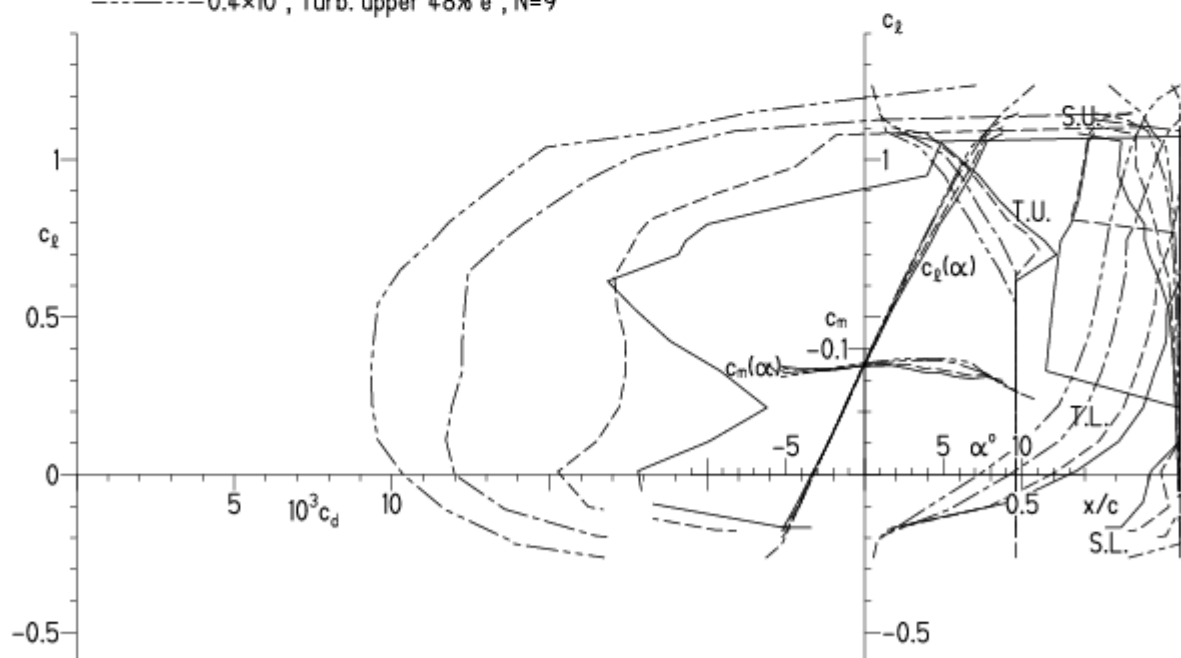
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

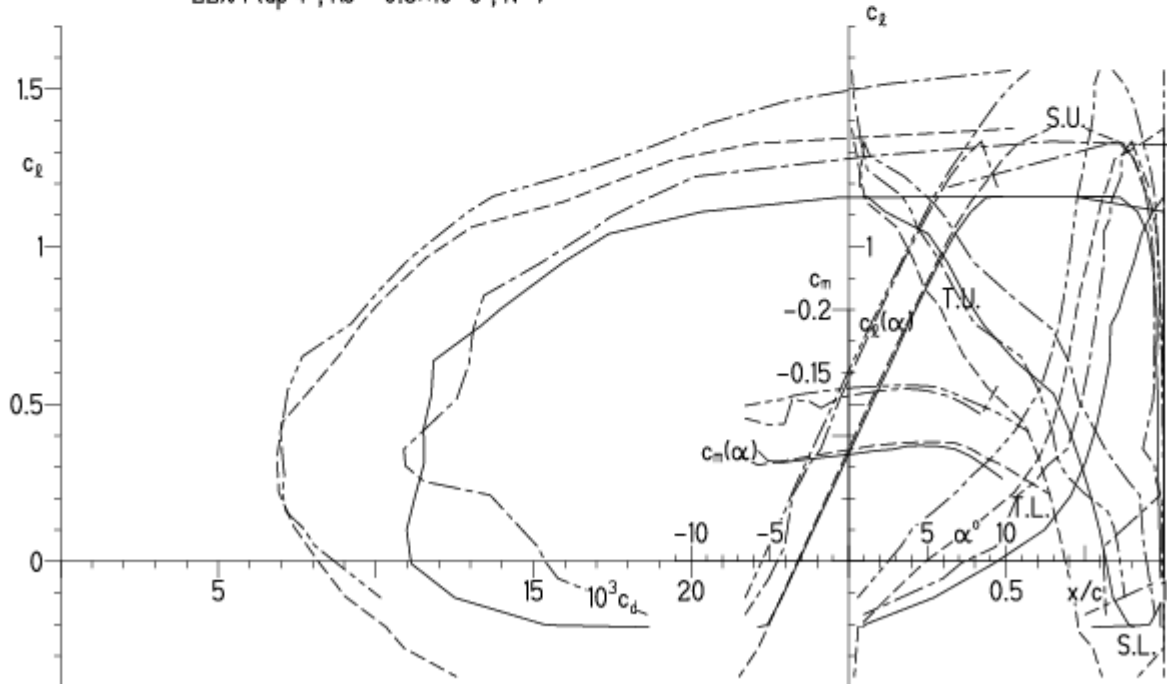


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

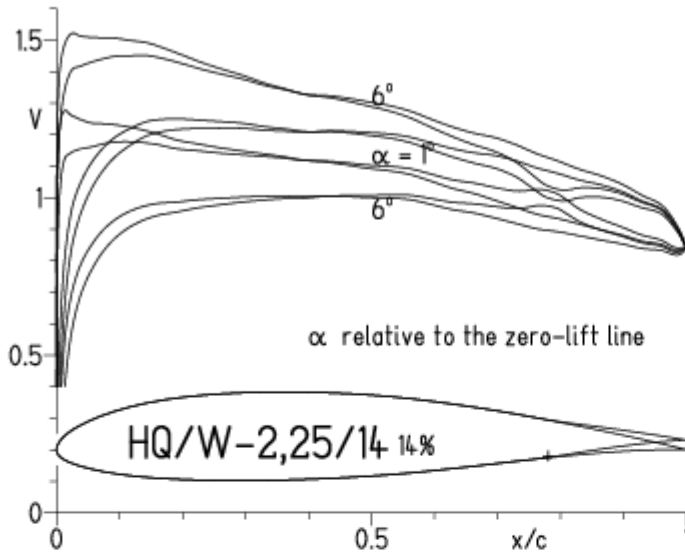
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

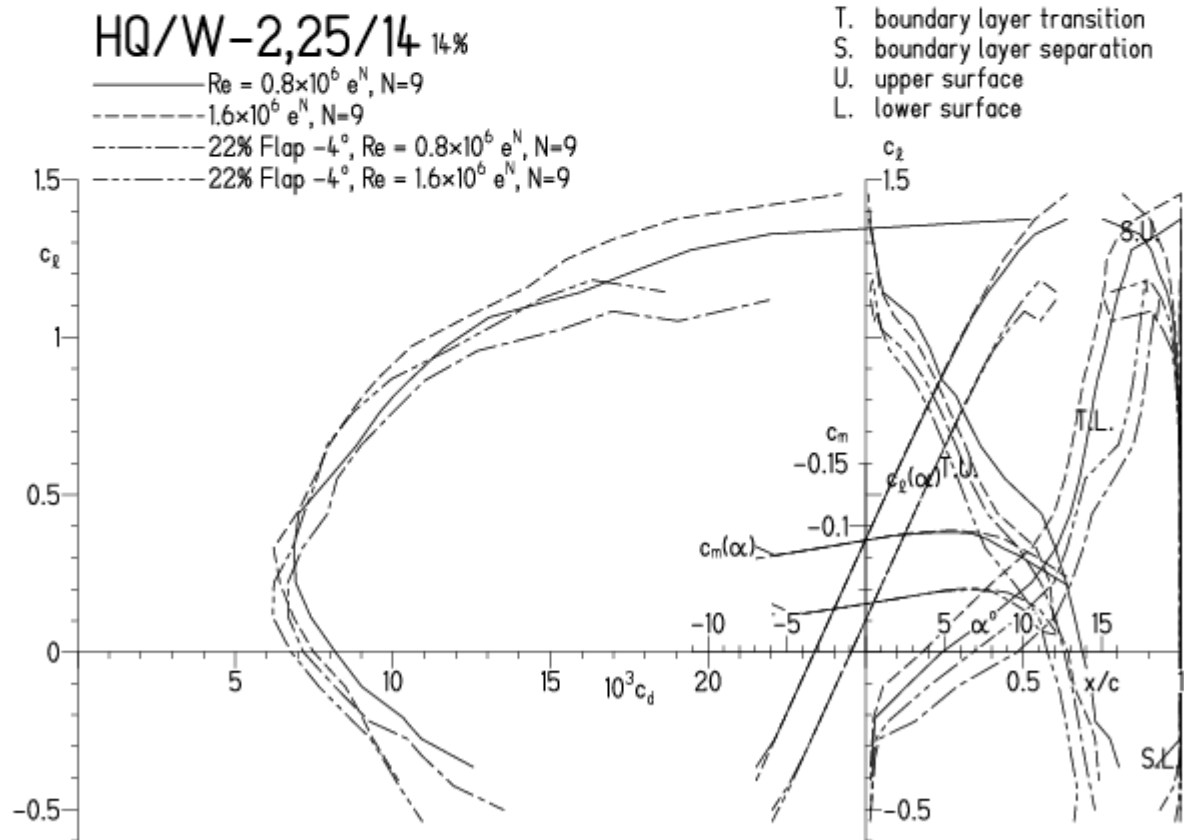


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

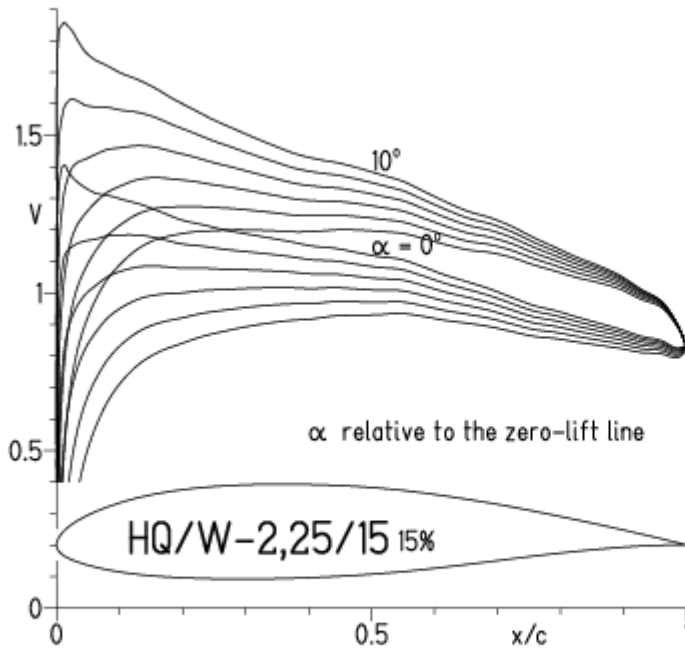


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31

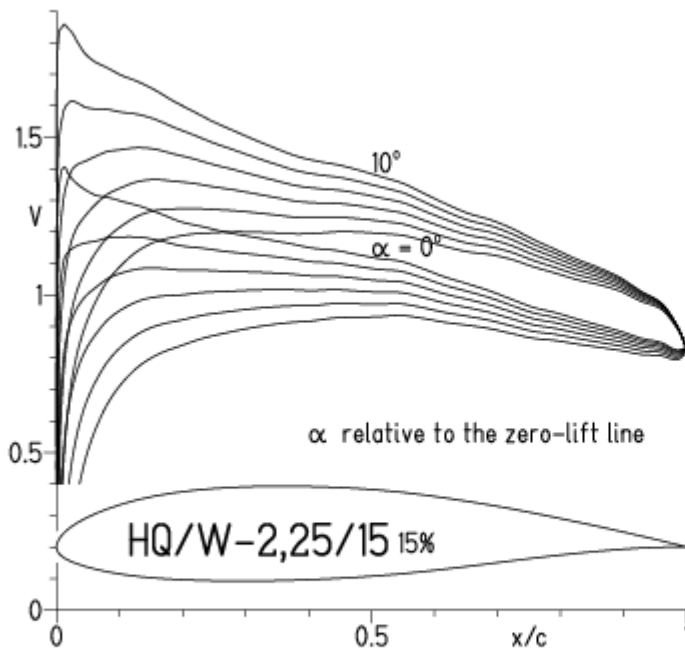


EPPLER 20

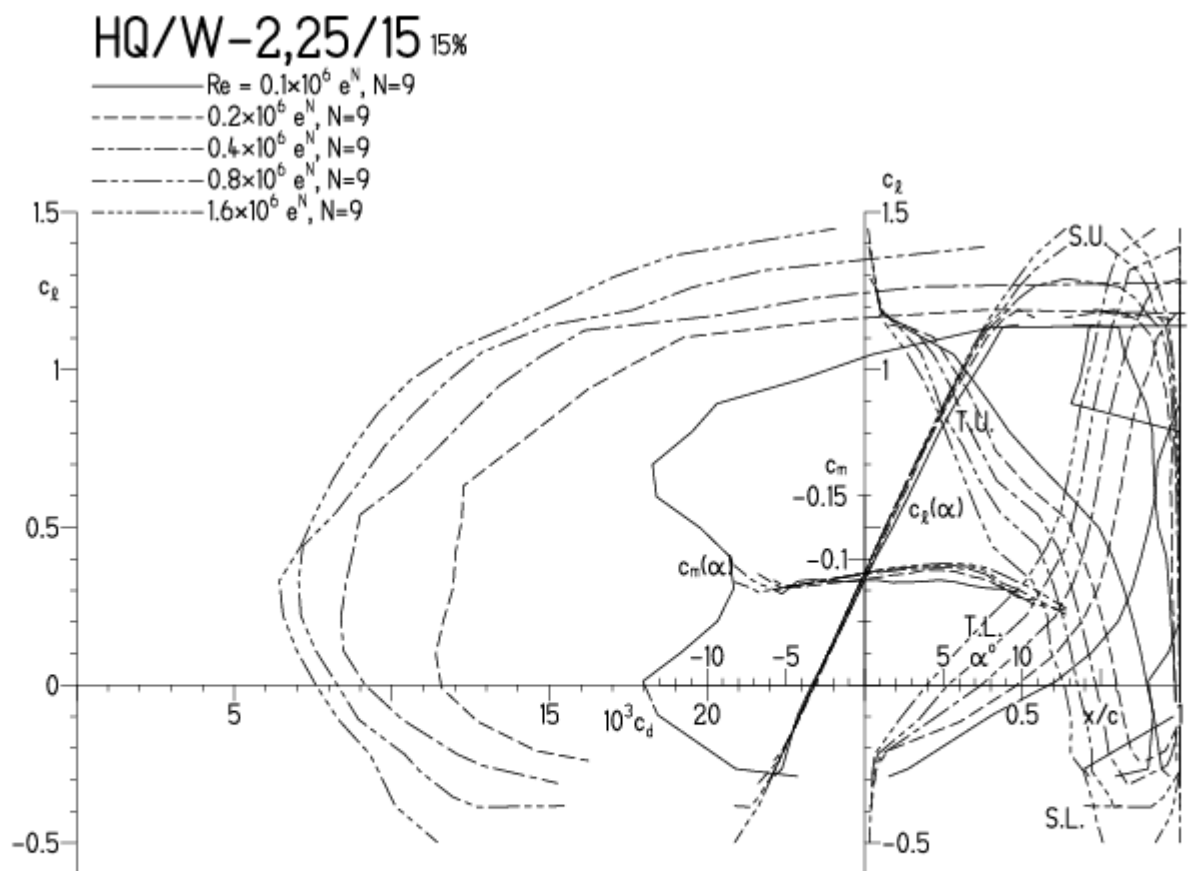


HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

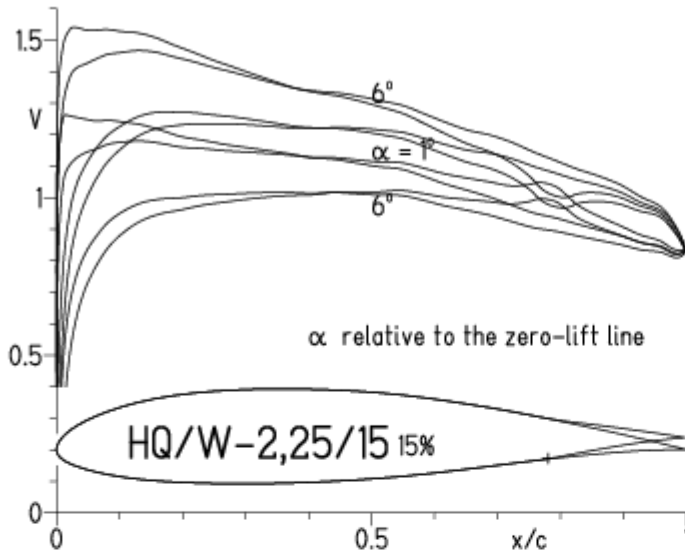


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:

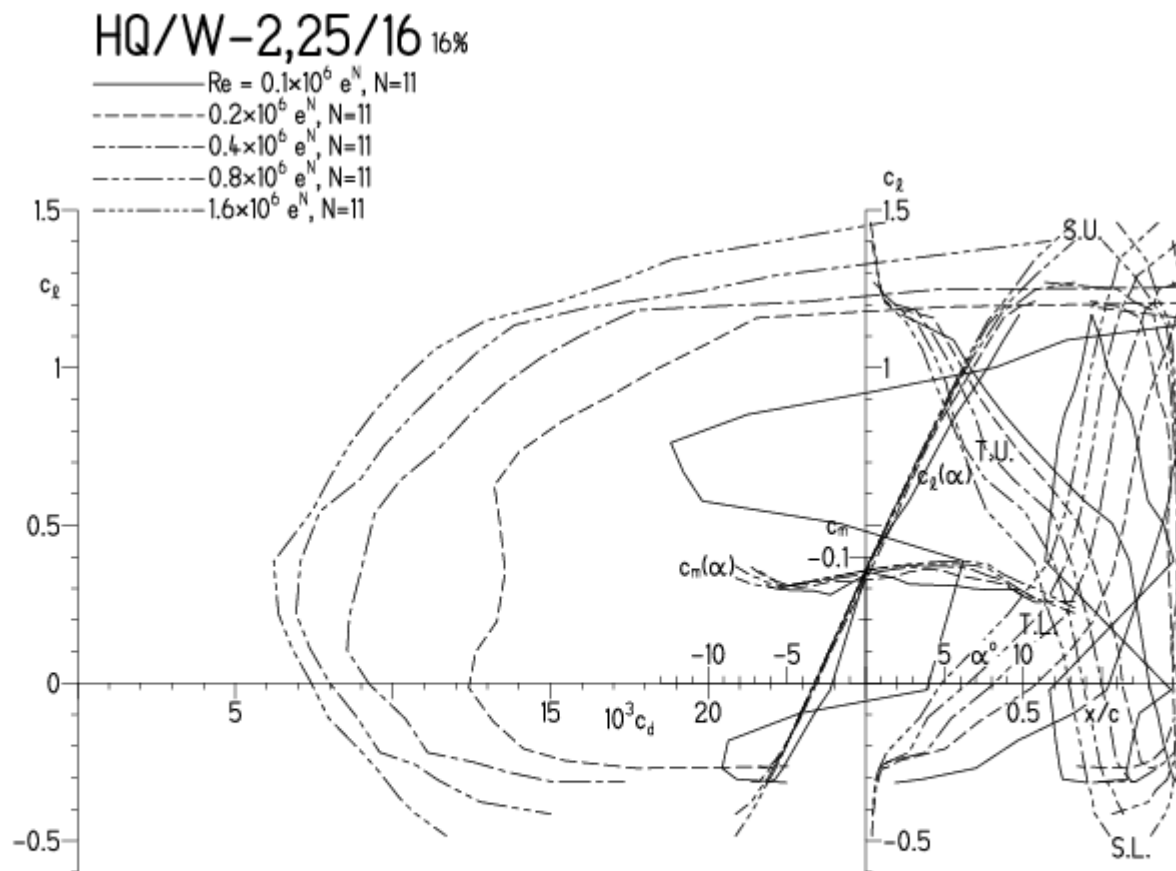


HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

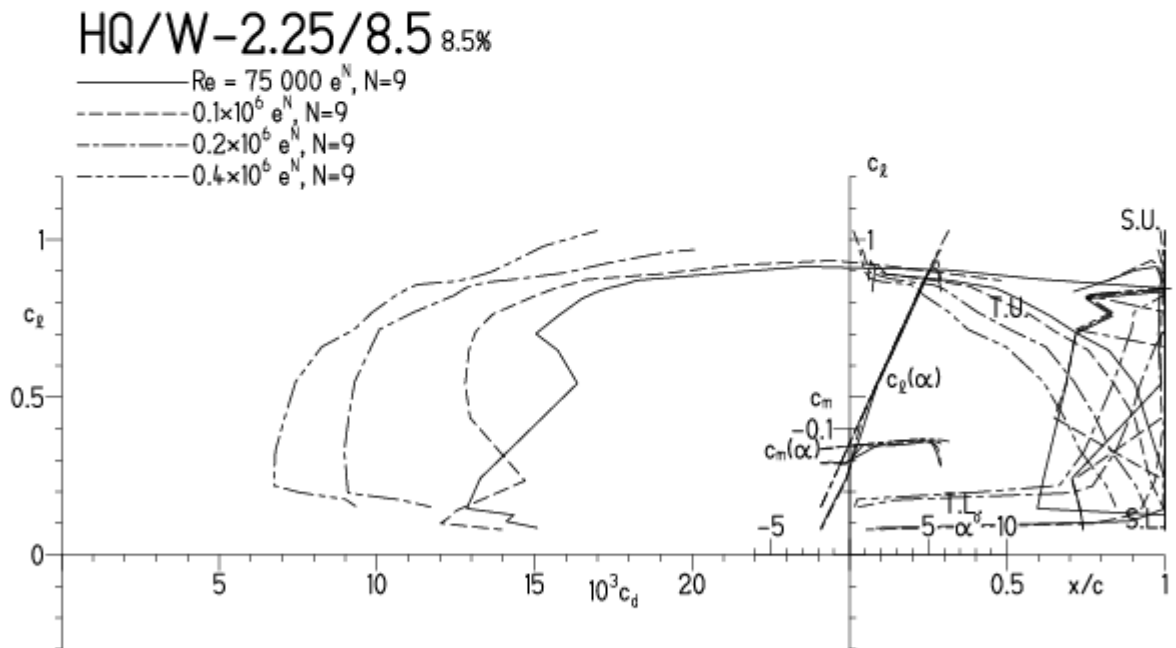


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

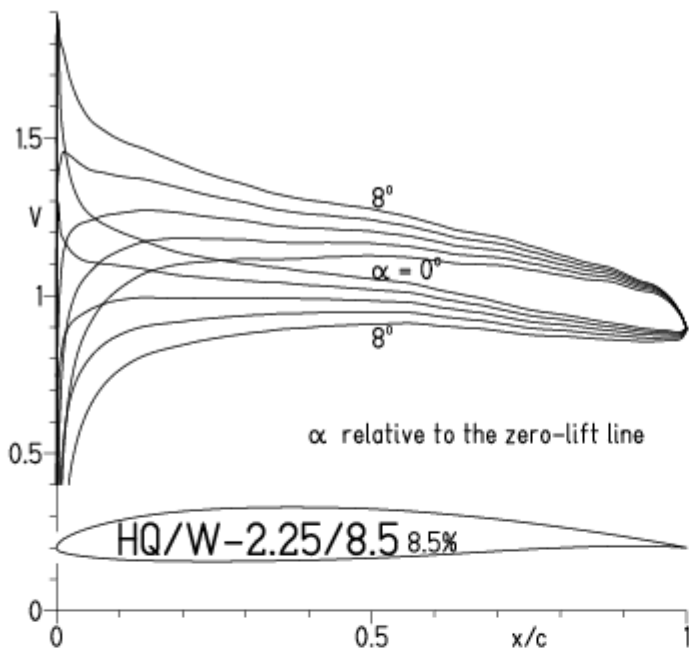


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

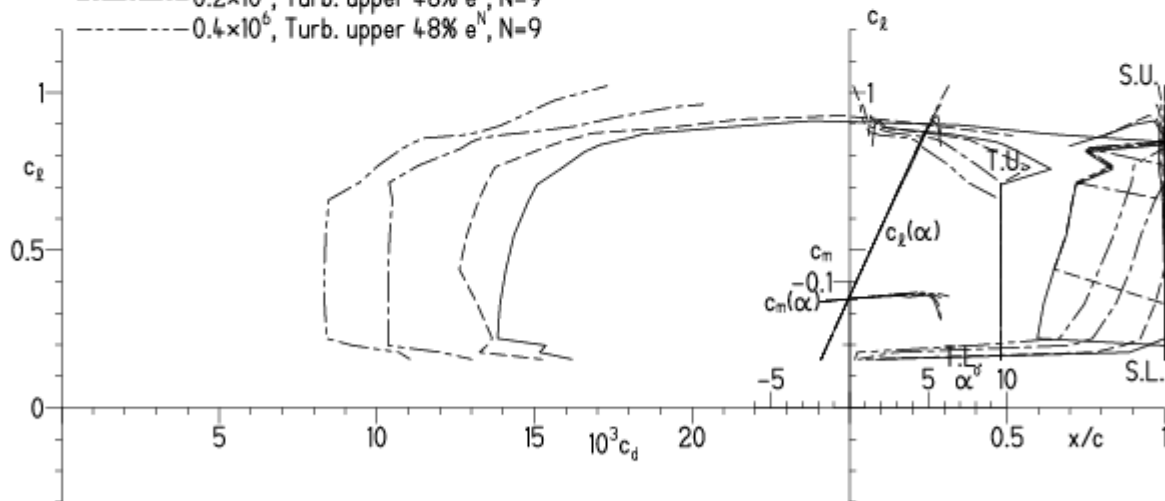
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

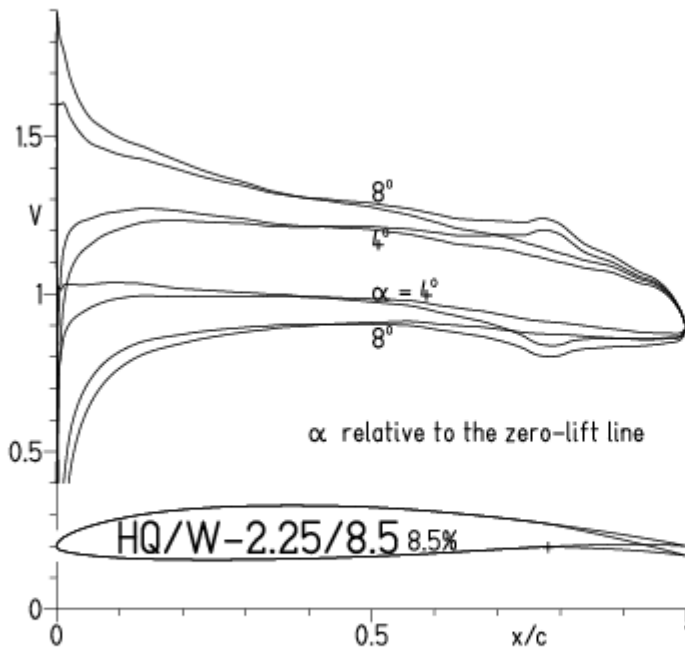
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

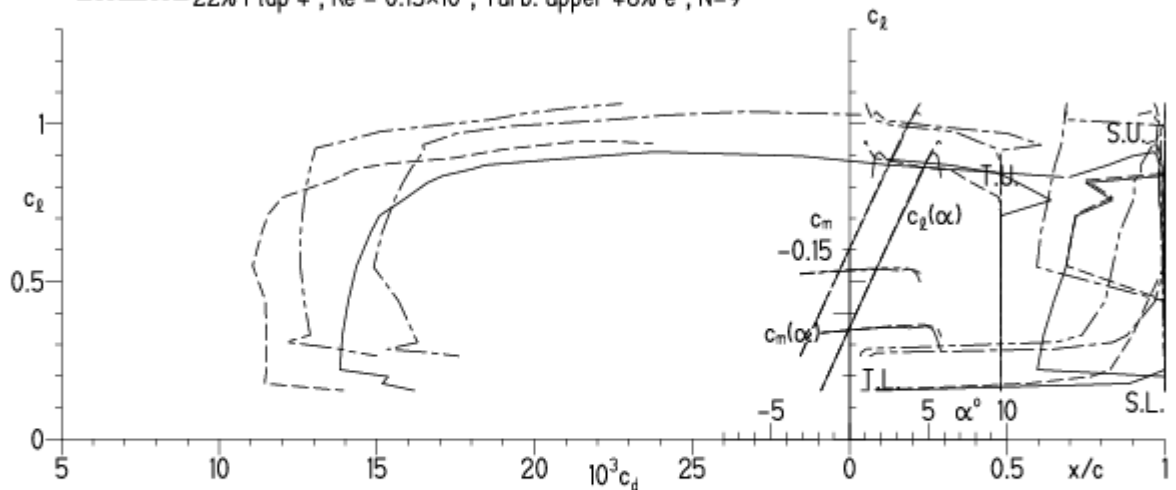


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

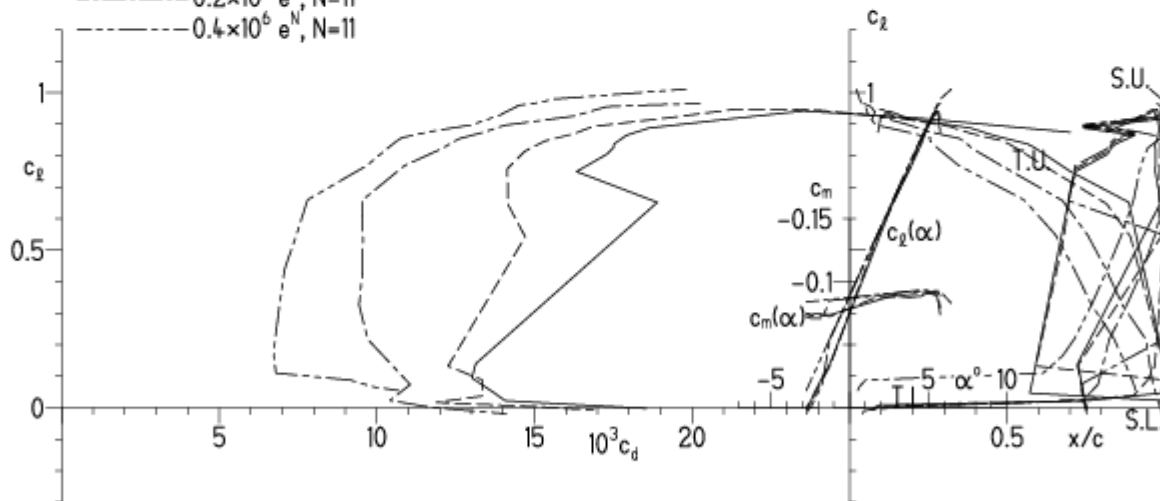
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



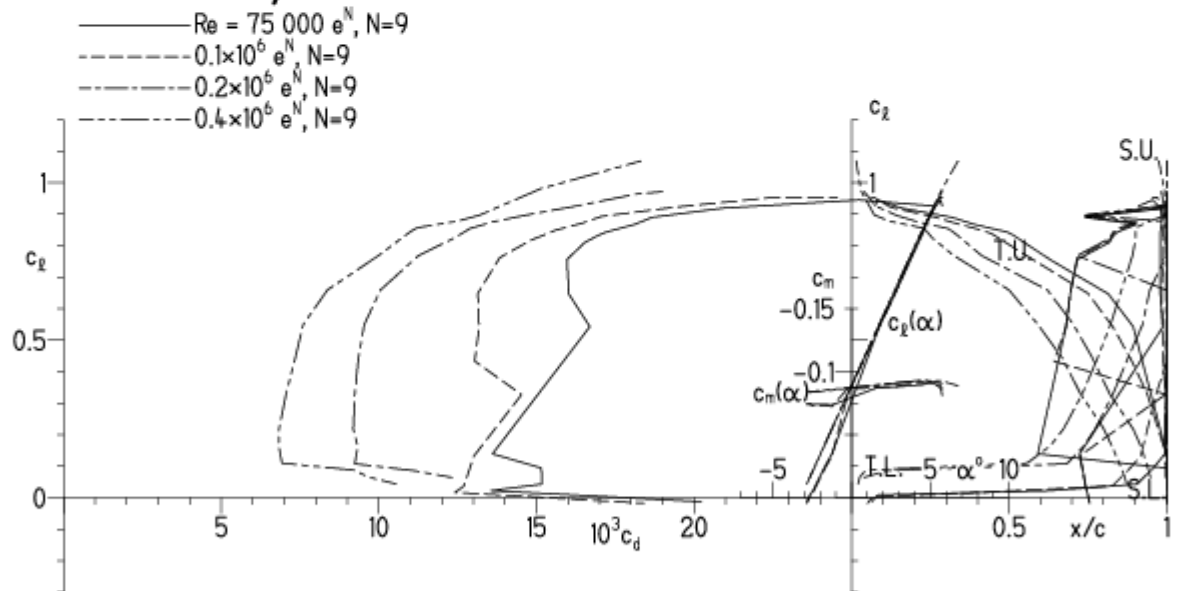
HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



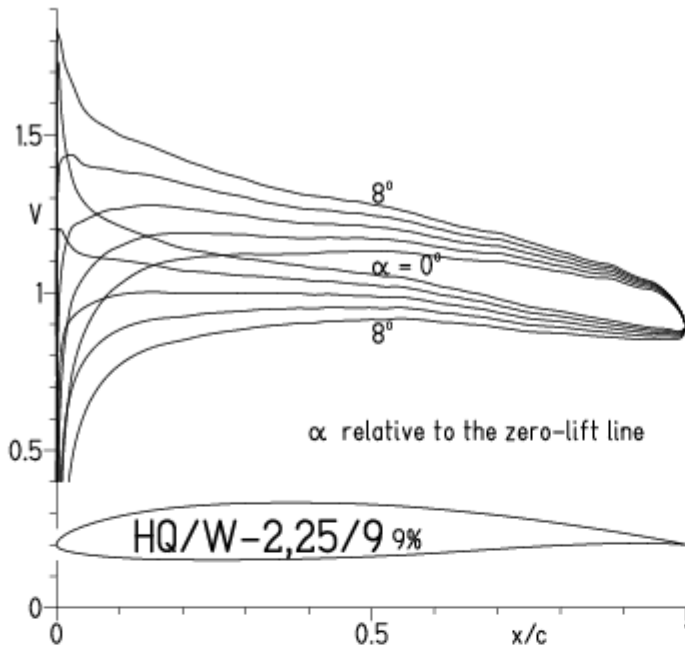
EPPLER 2005 V. 8.

HQ/W-2,25/9 9%



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

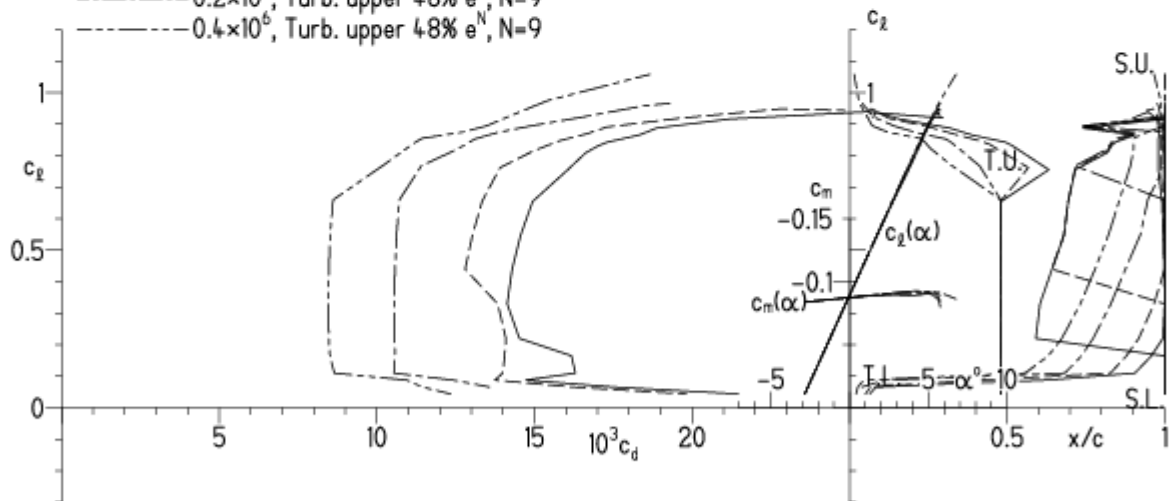
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

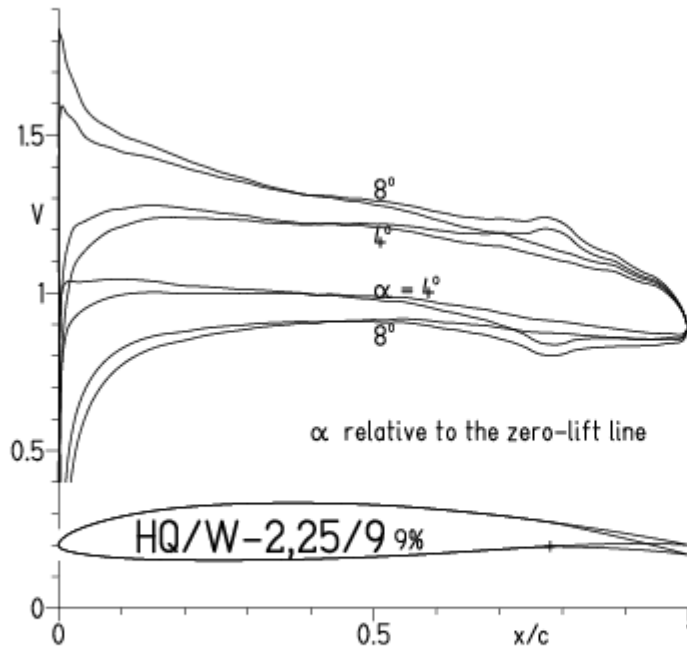
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - · 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=11

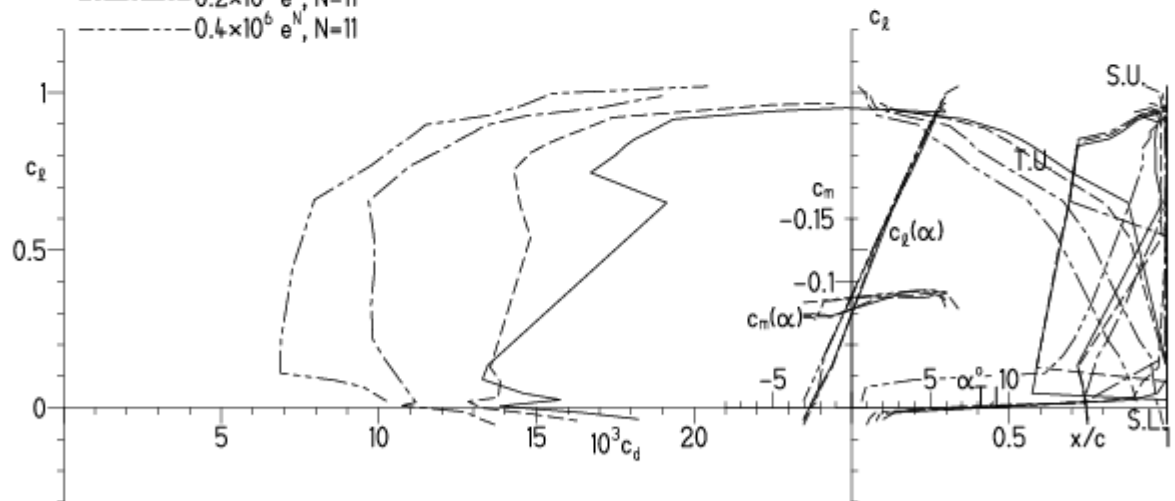
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

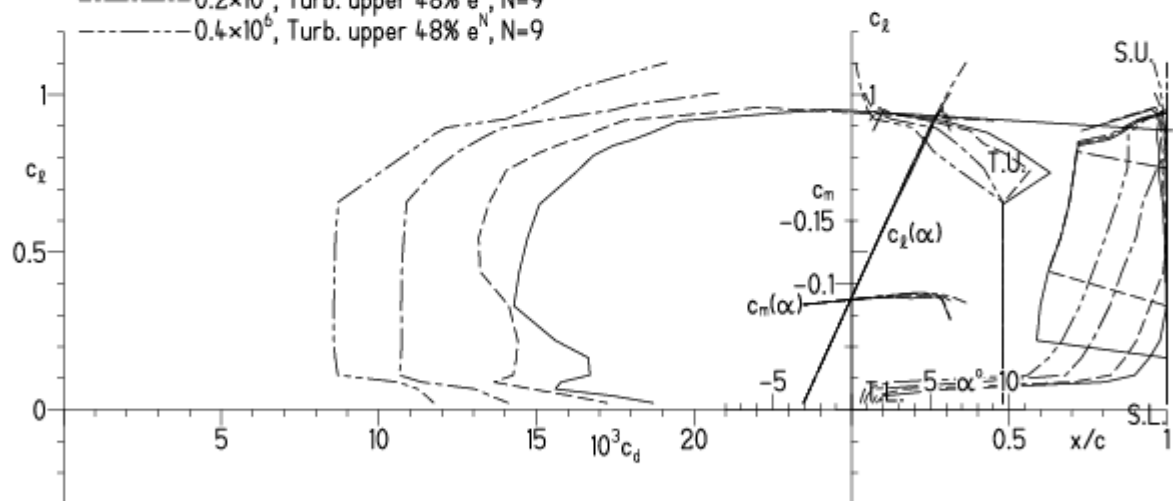
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12

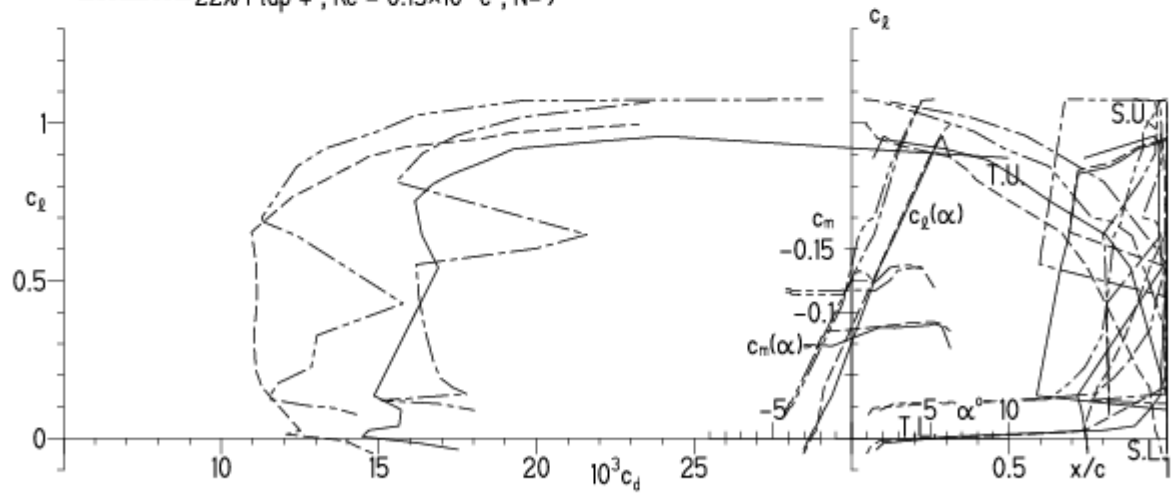


EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

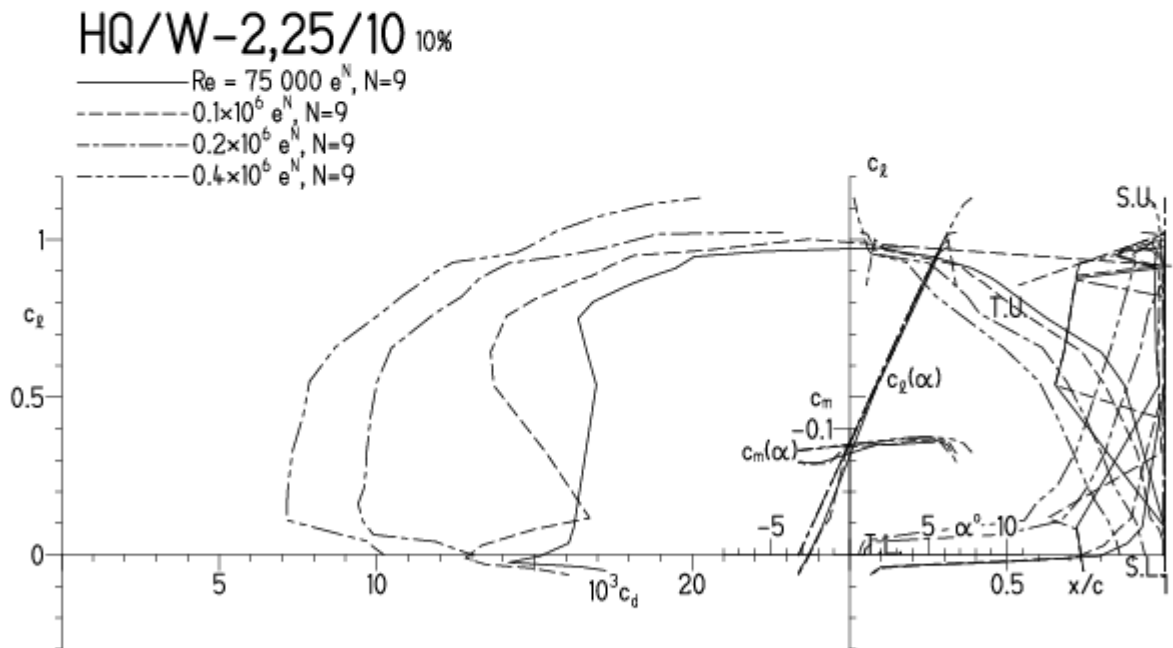


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

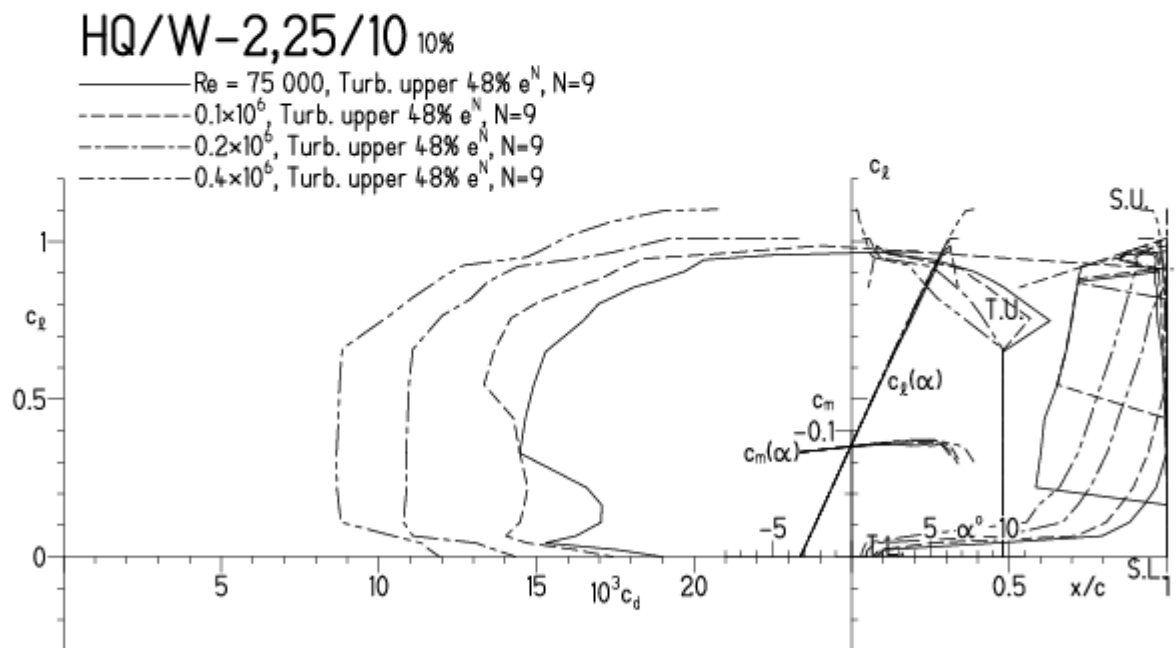


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

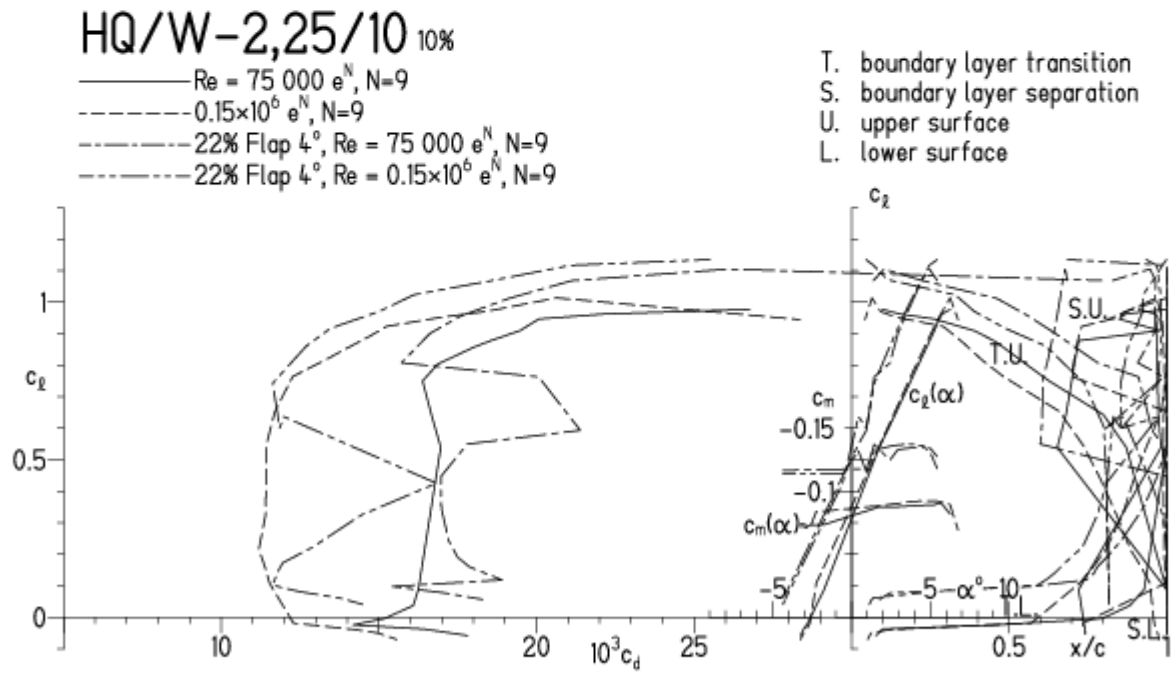


HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

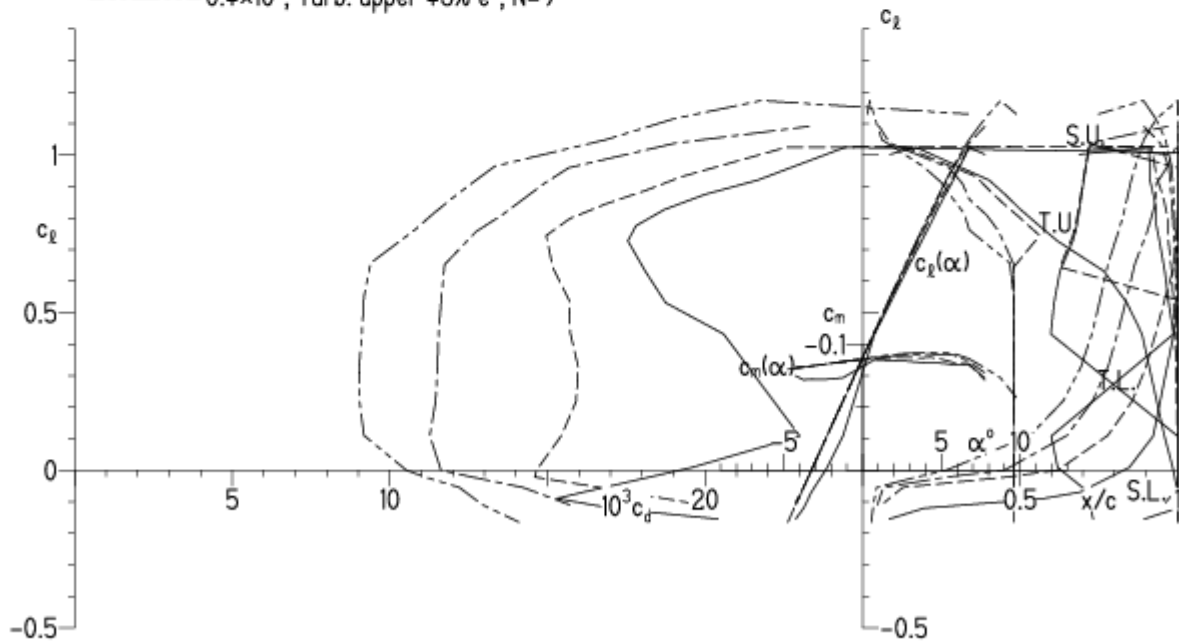
EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

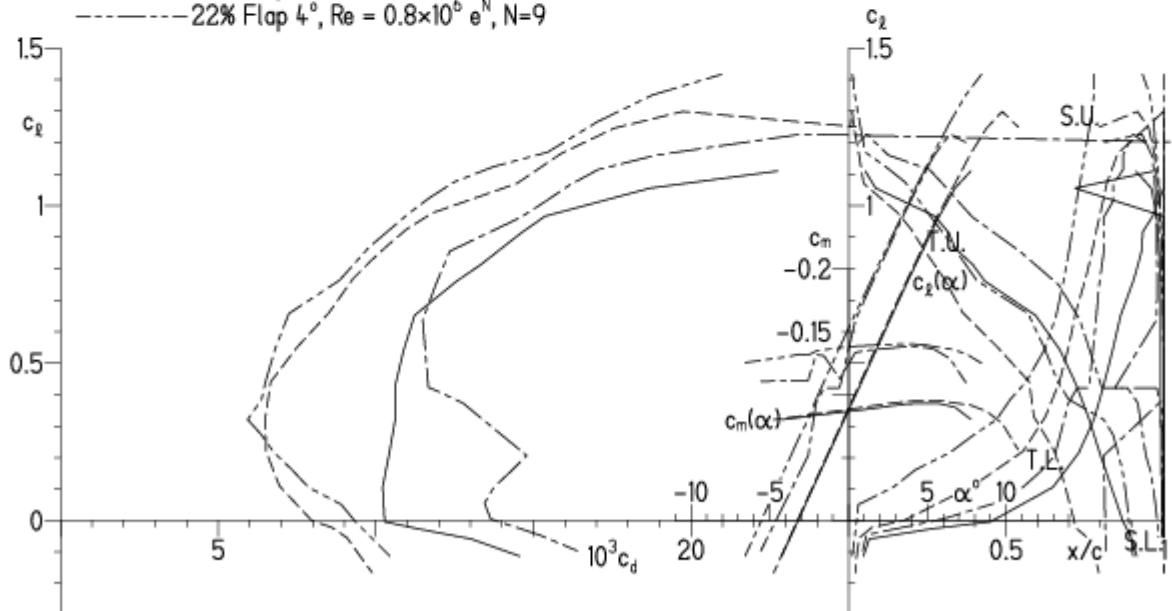


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- Re = 0.2×10^6 e^N, N=9
- - - Re = 0.8×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.2×10^6 e^N, N=9
- · - 22% Flap 4°, Re = 0.8×10^6 e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

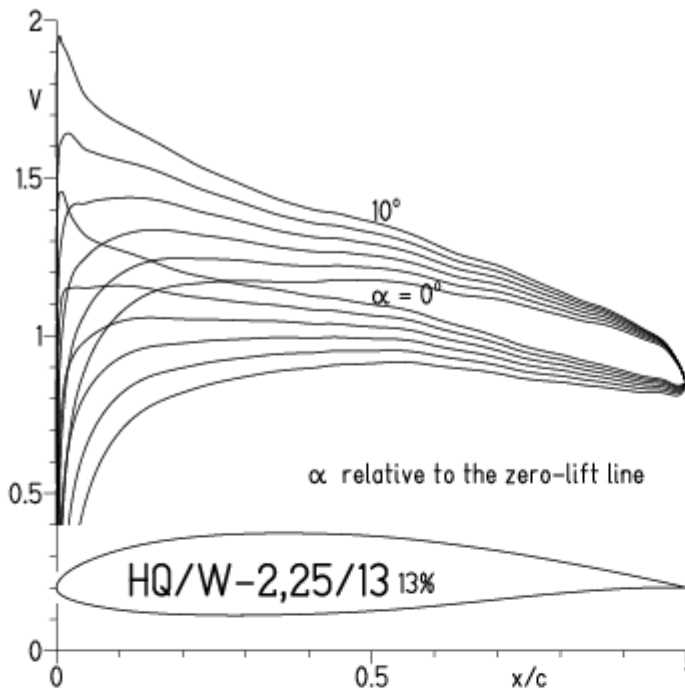
HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

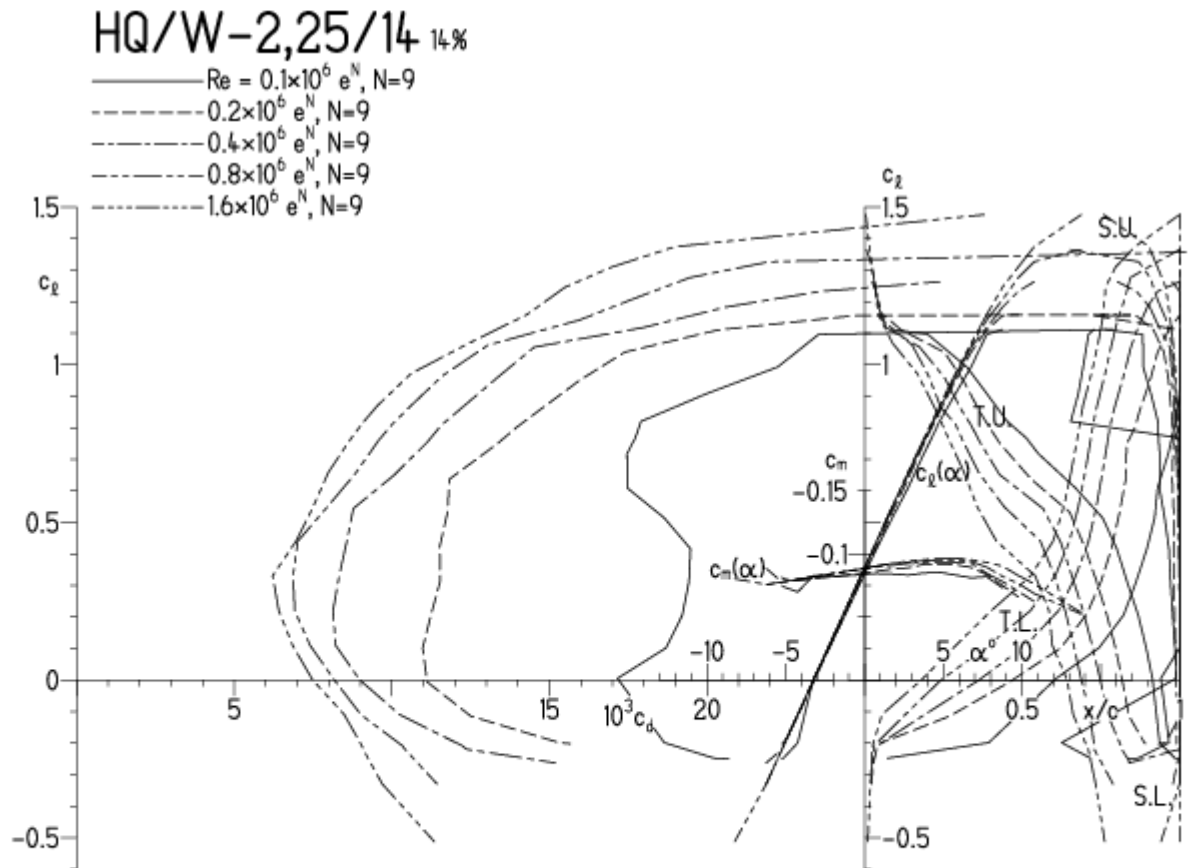


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

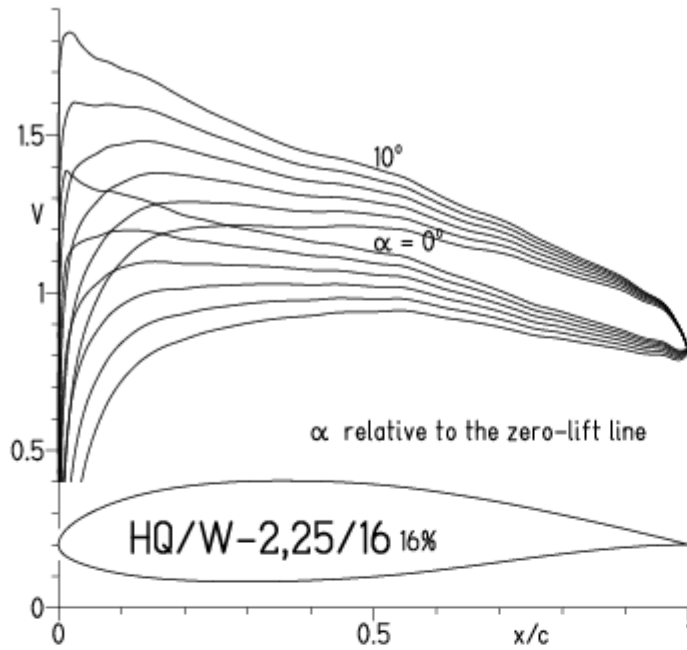
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

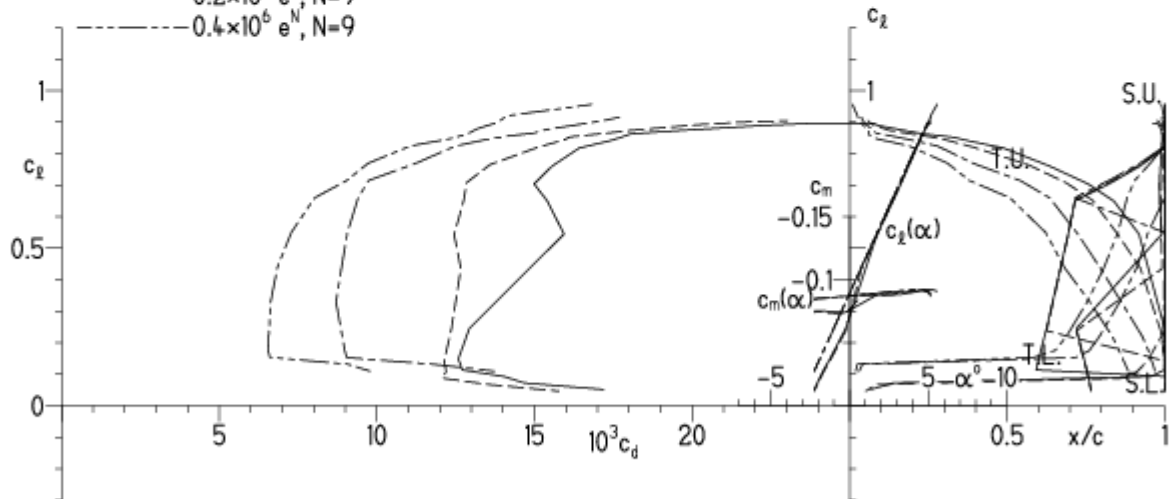
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

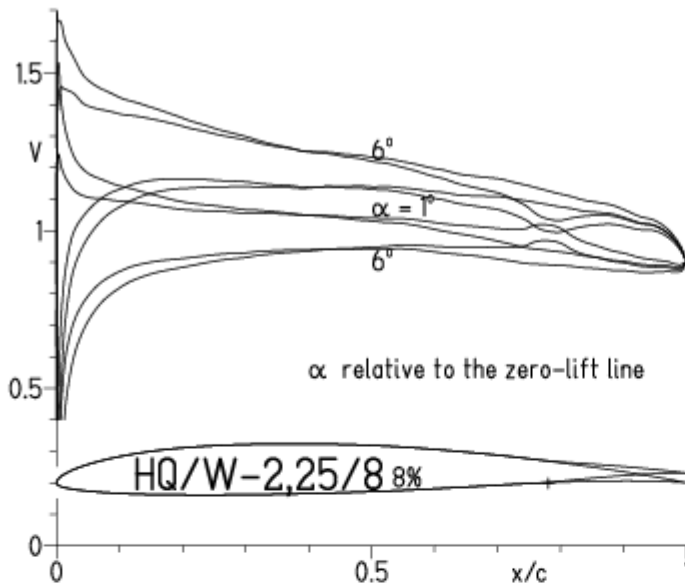
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

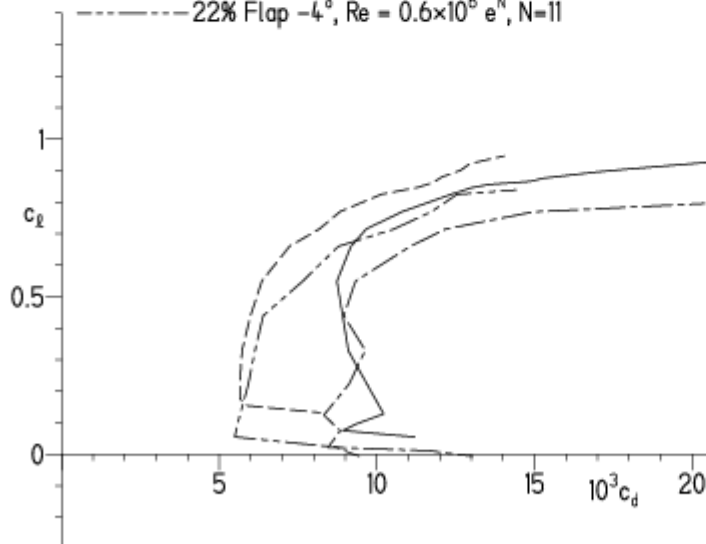
EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



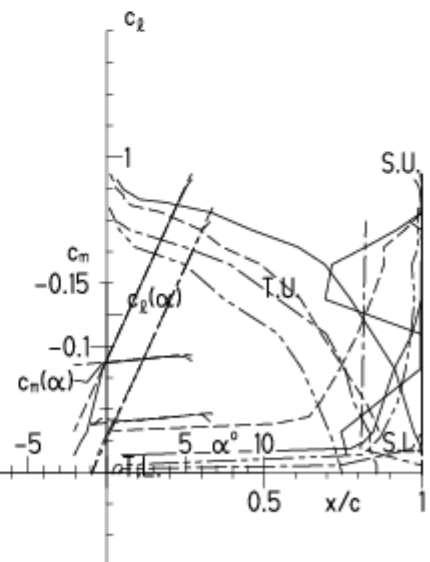
EPPLER 2005 V. 8.5.07 RUN 3.3.11 1

HQ/W-2,25/8 8%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



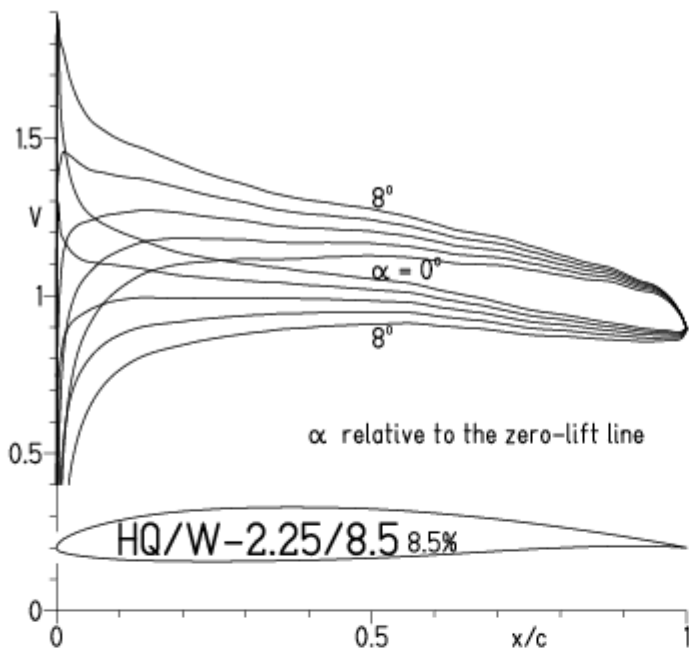
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

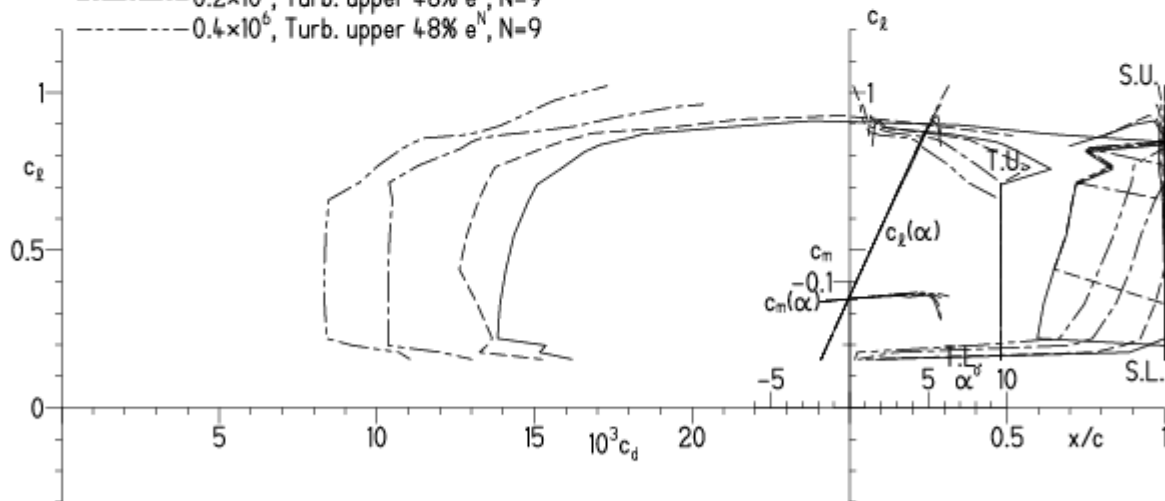
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$

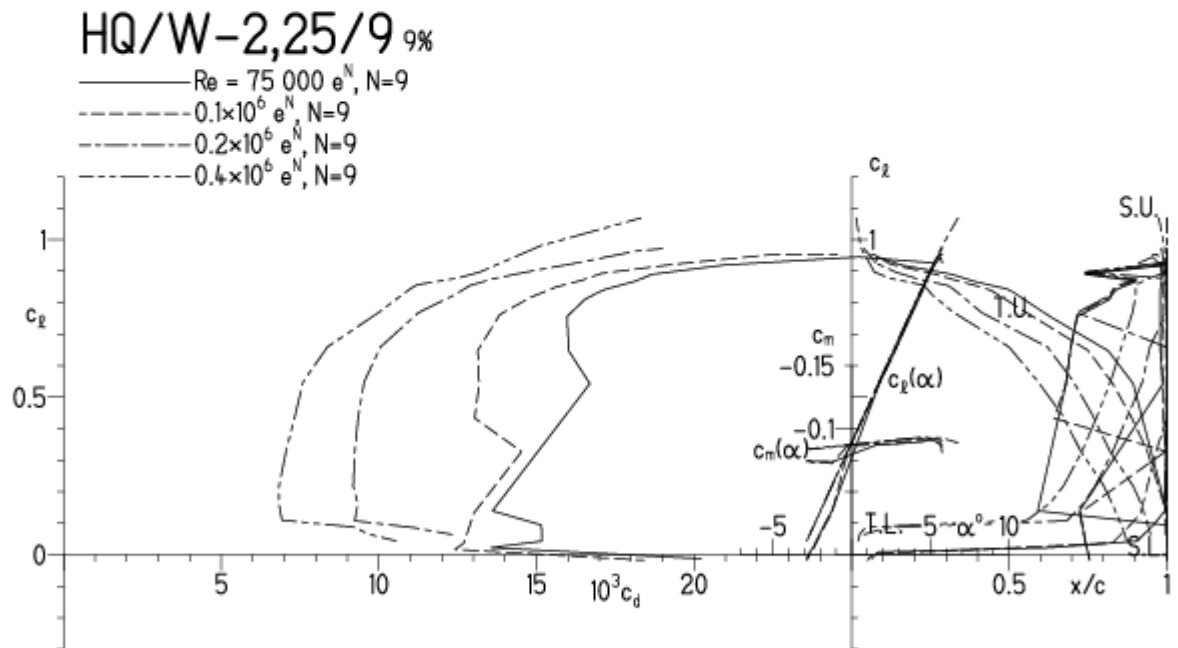


HQ/W-2,25/9, N=9

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08

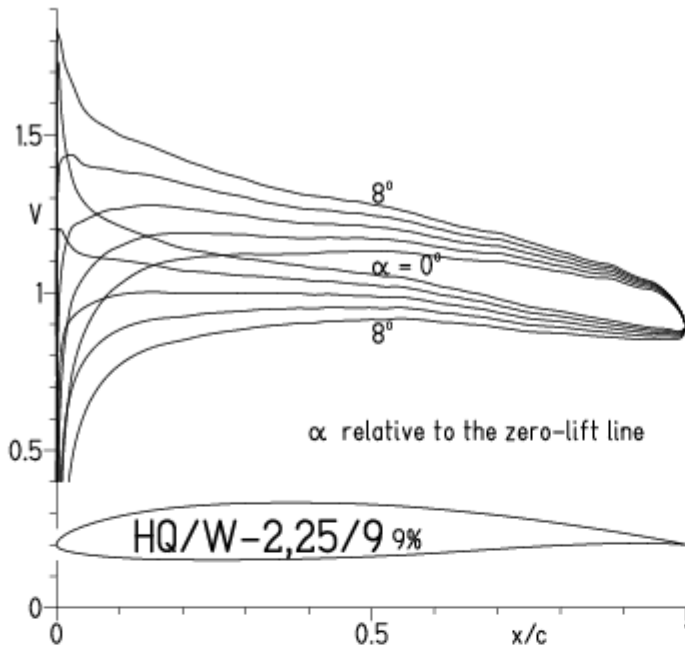


EPPLER 2005 V. 8.



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

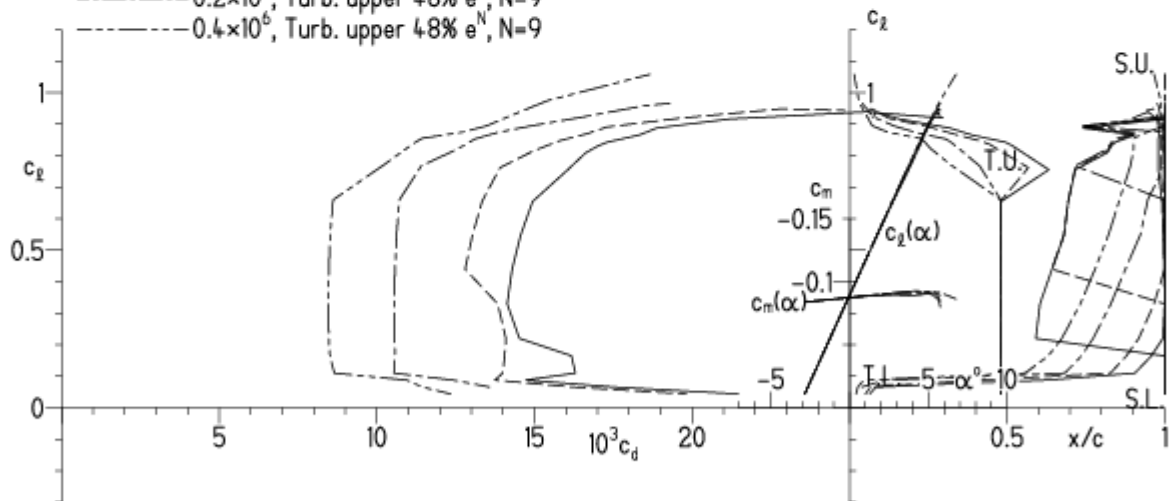
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$

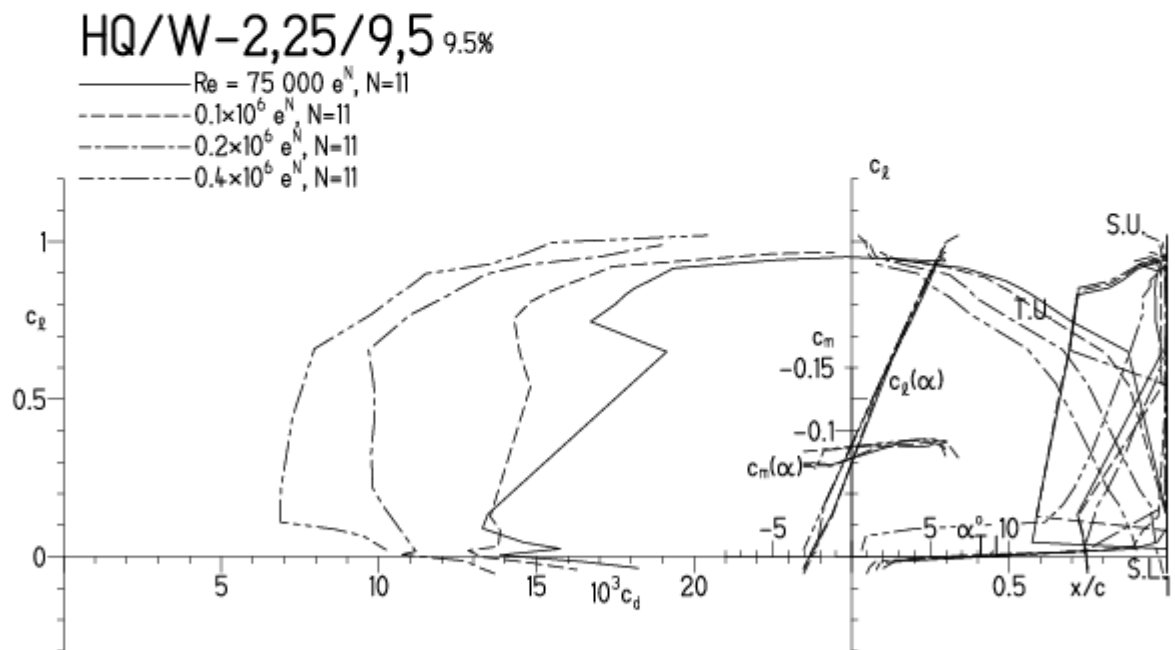


HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

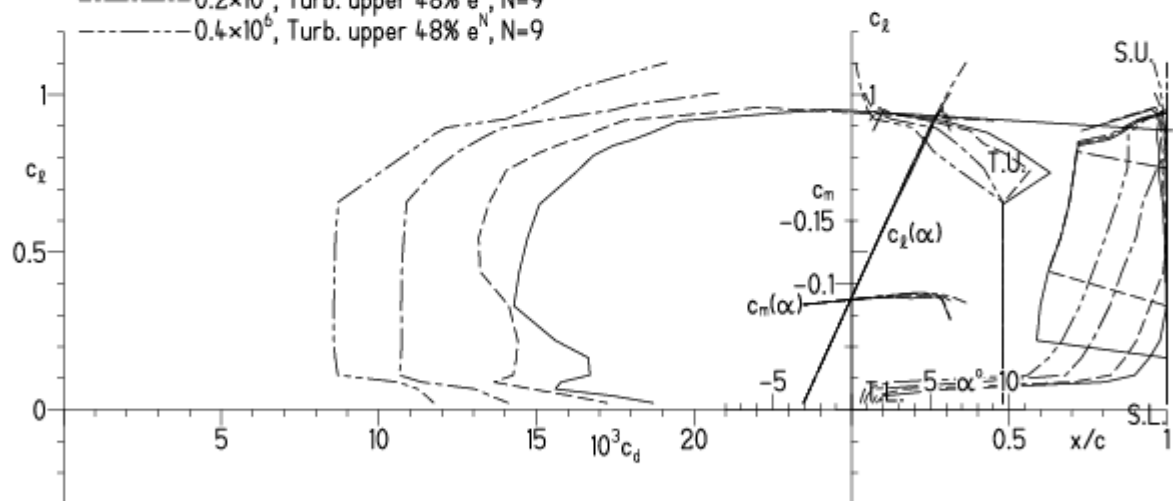
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

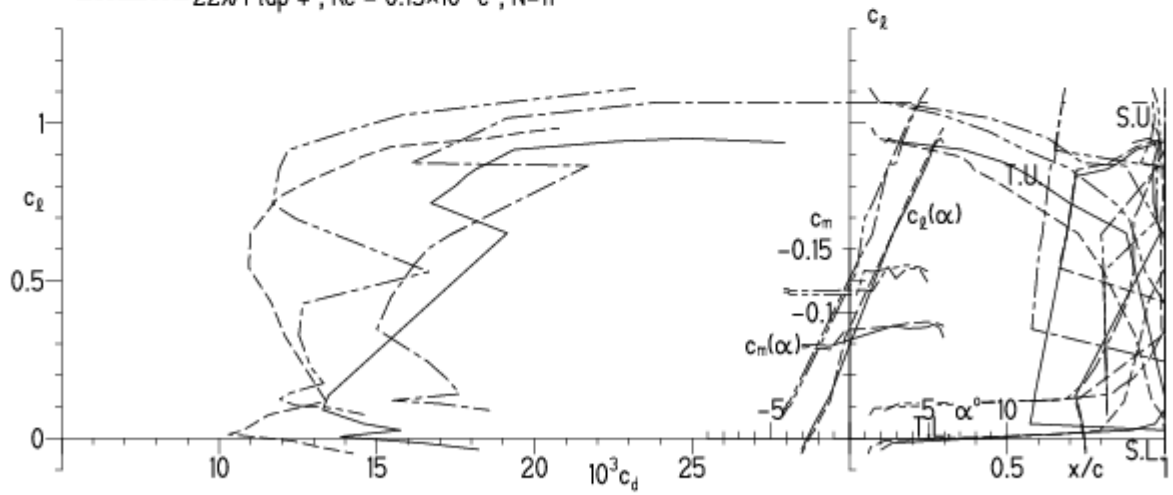


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

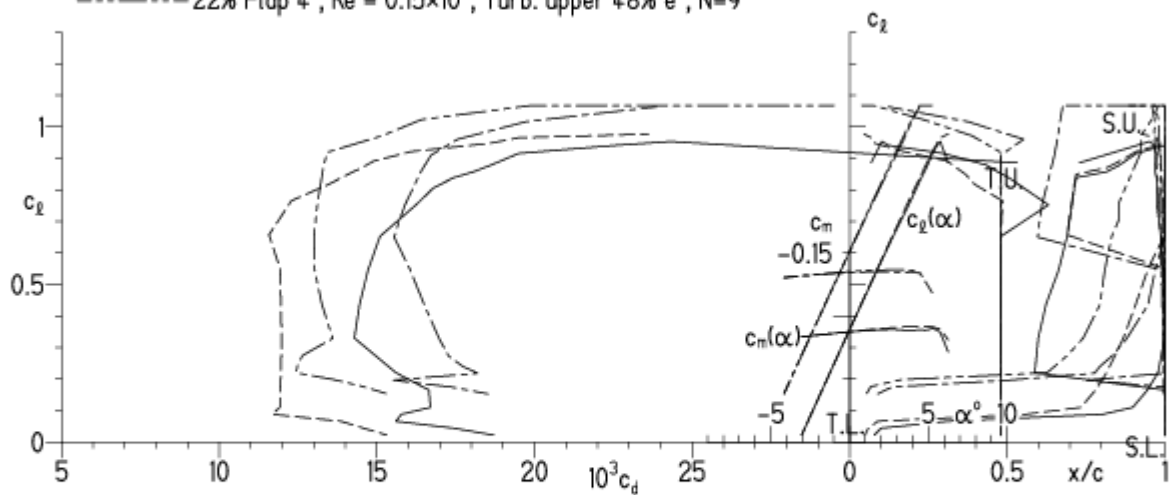


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



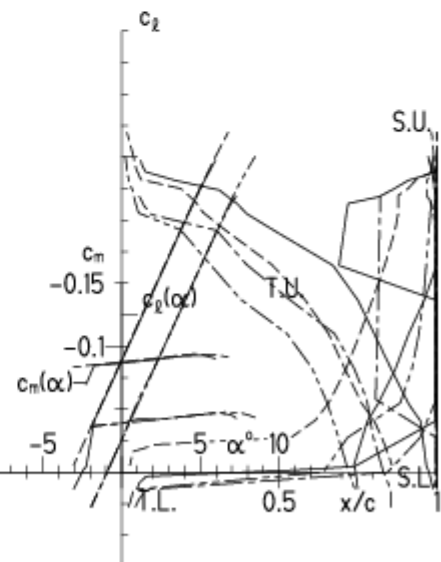
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

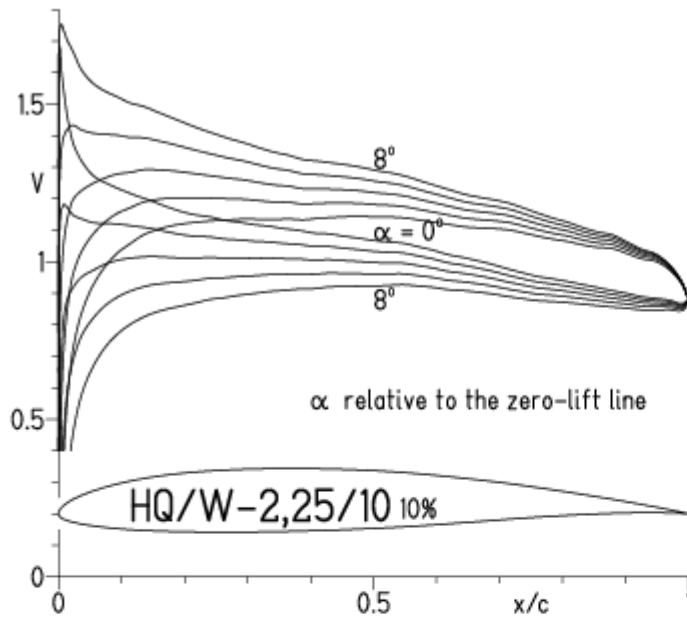


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

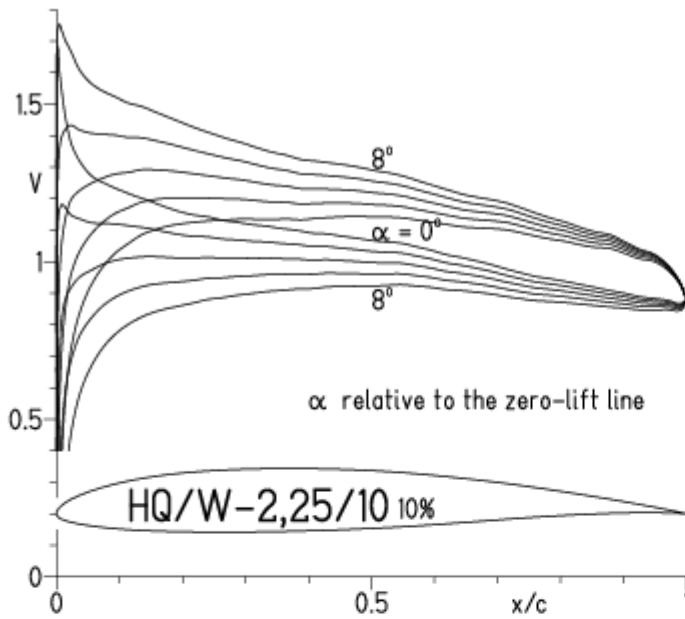


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

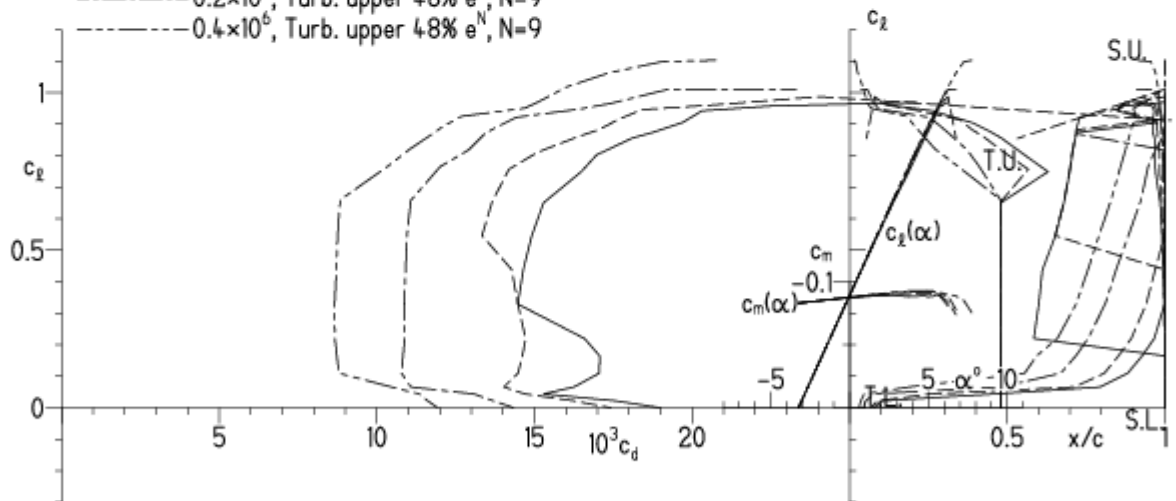
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

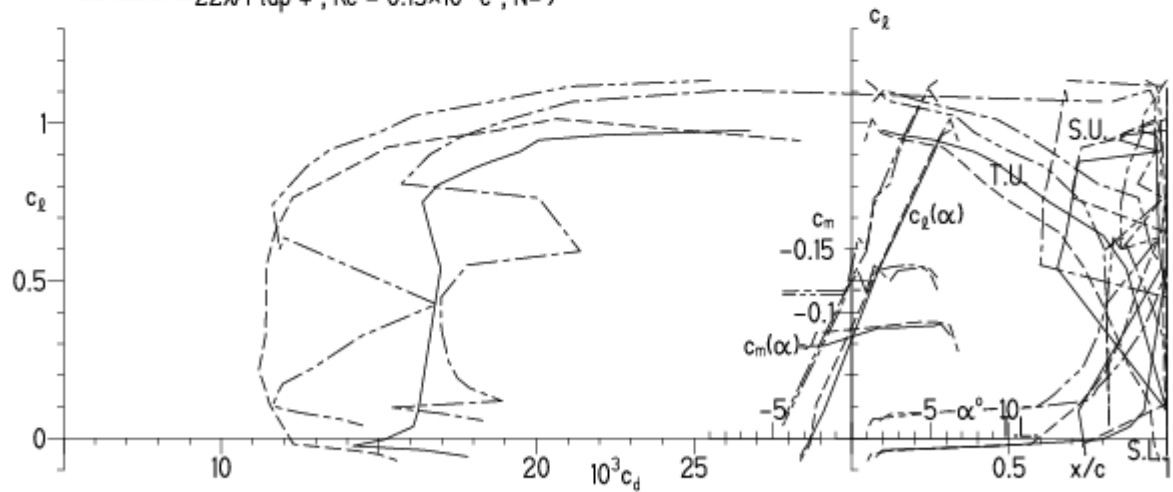


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

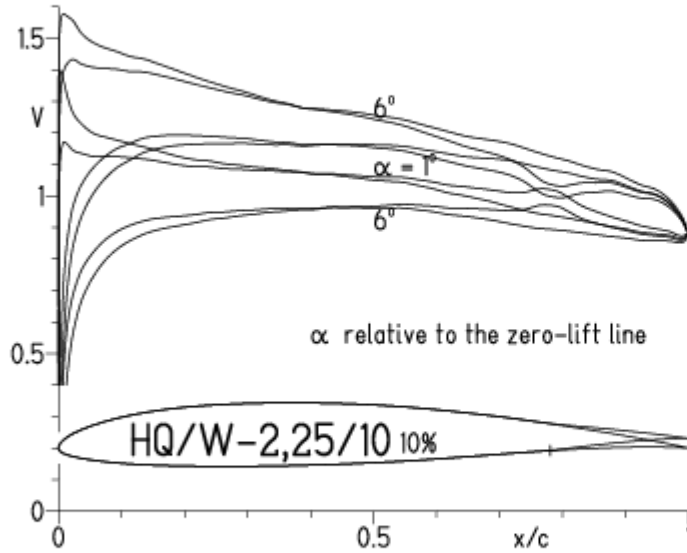
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

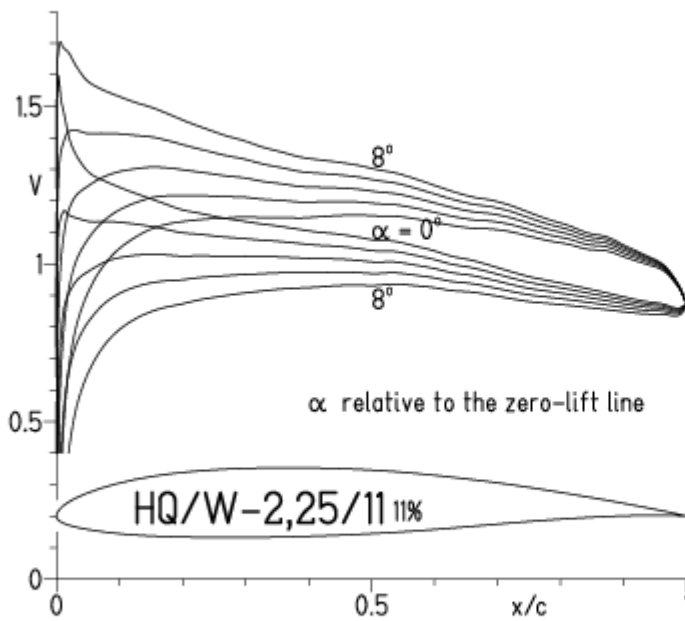


EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

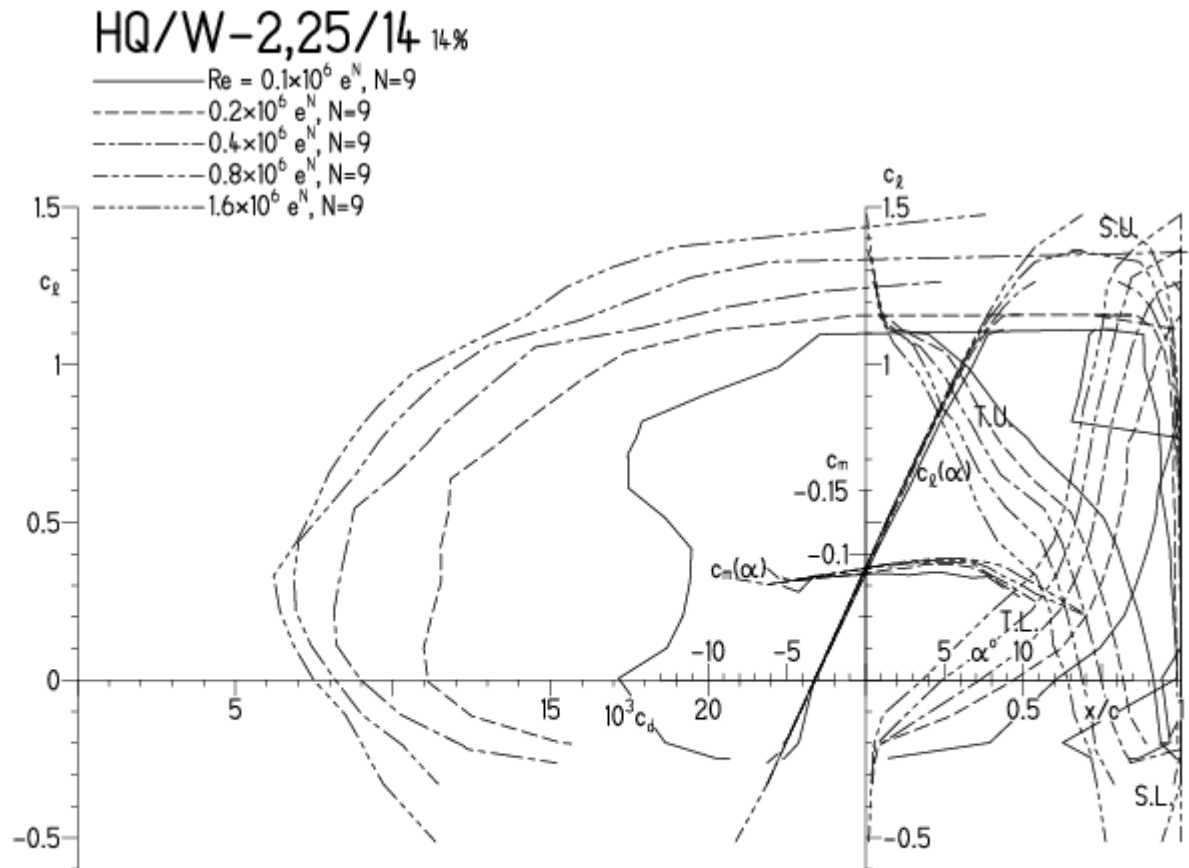


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

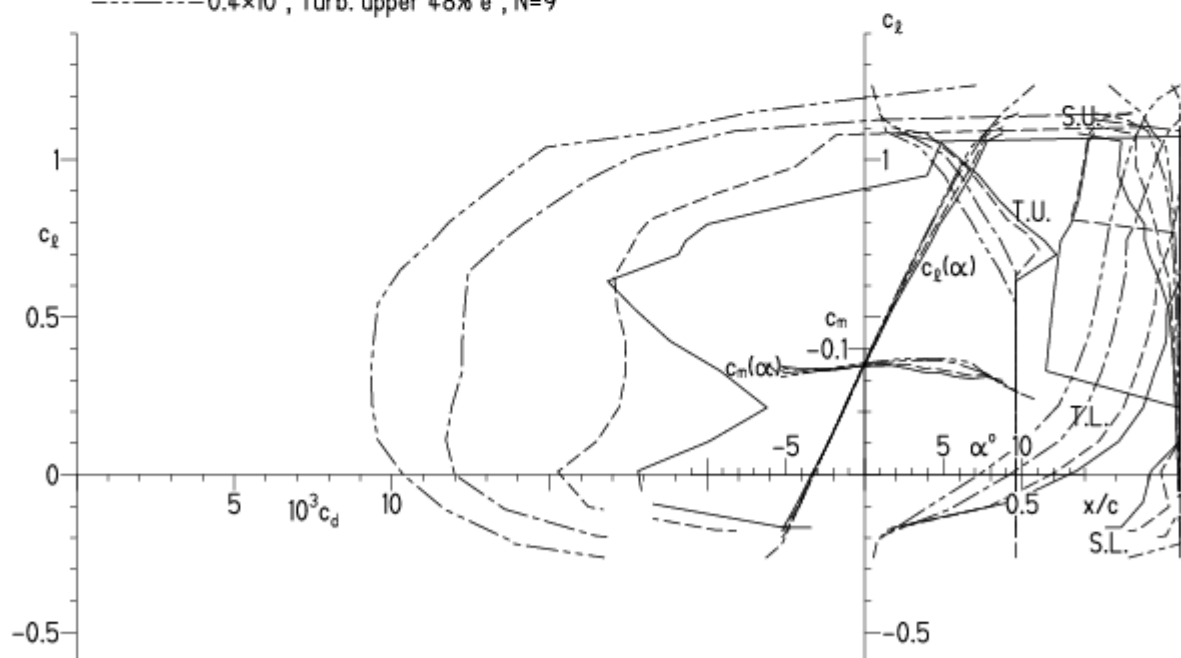
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

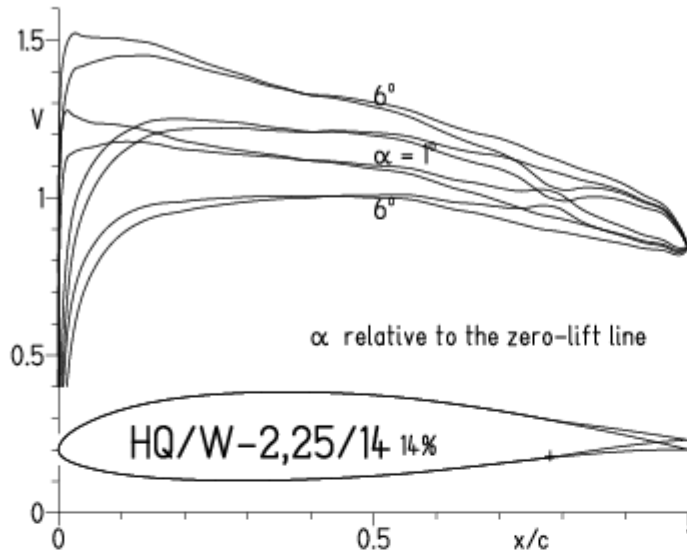
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

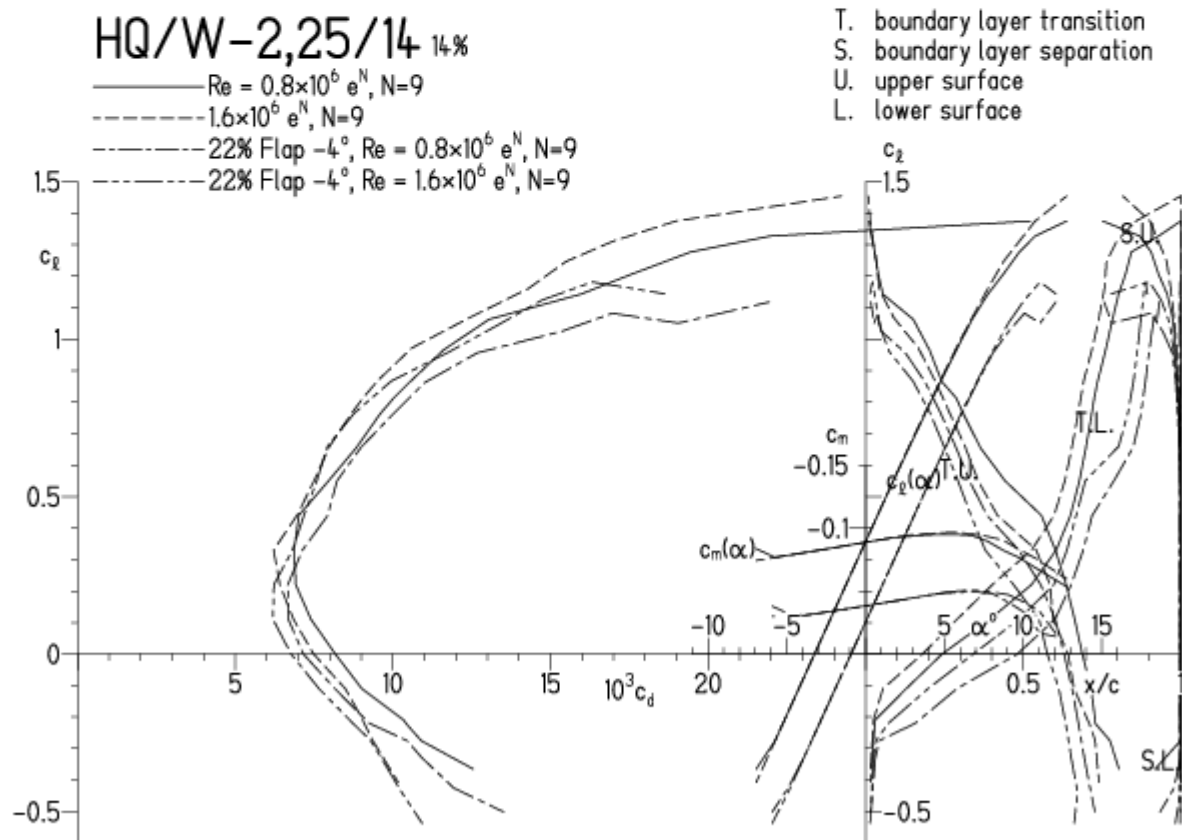


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

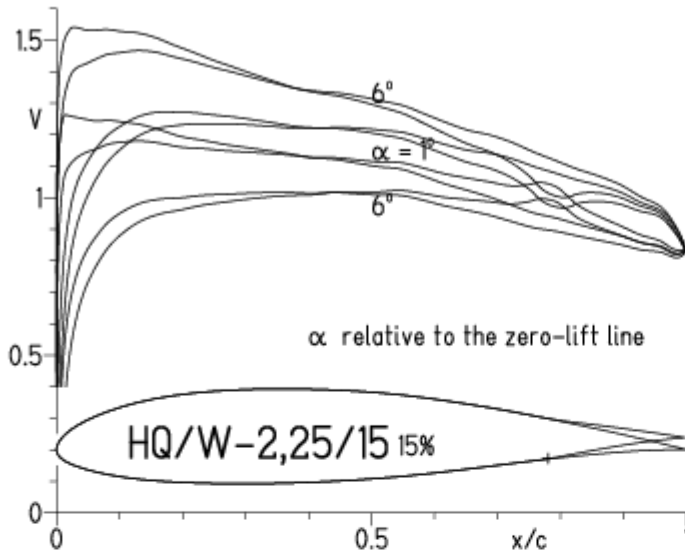


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

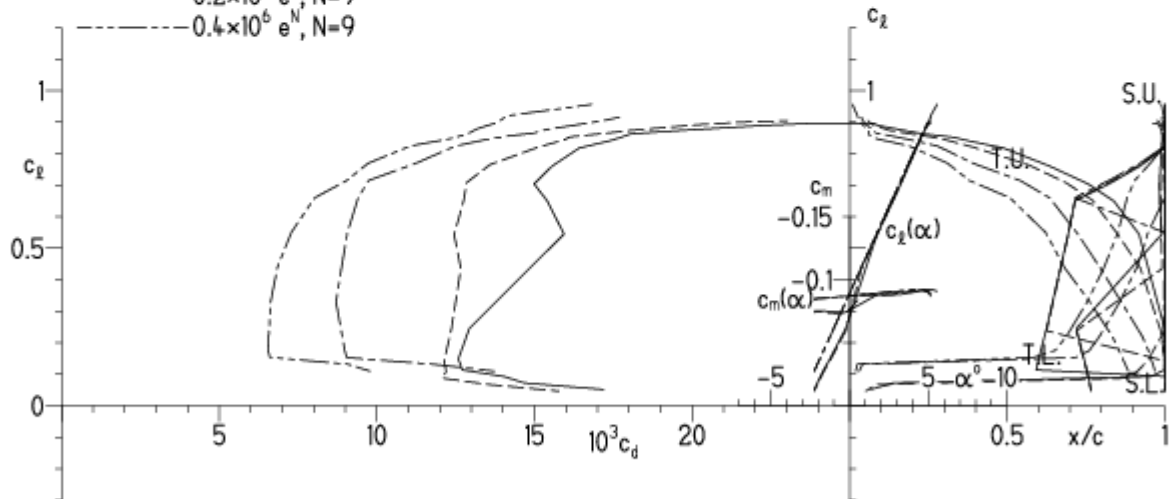
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

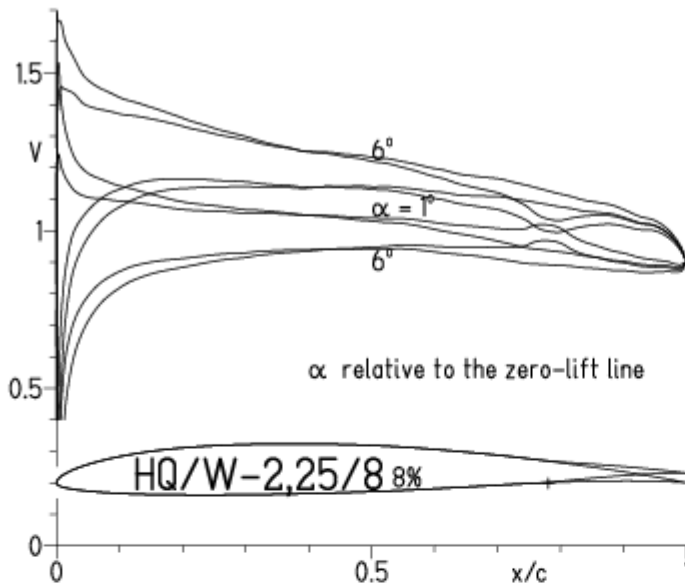
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

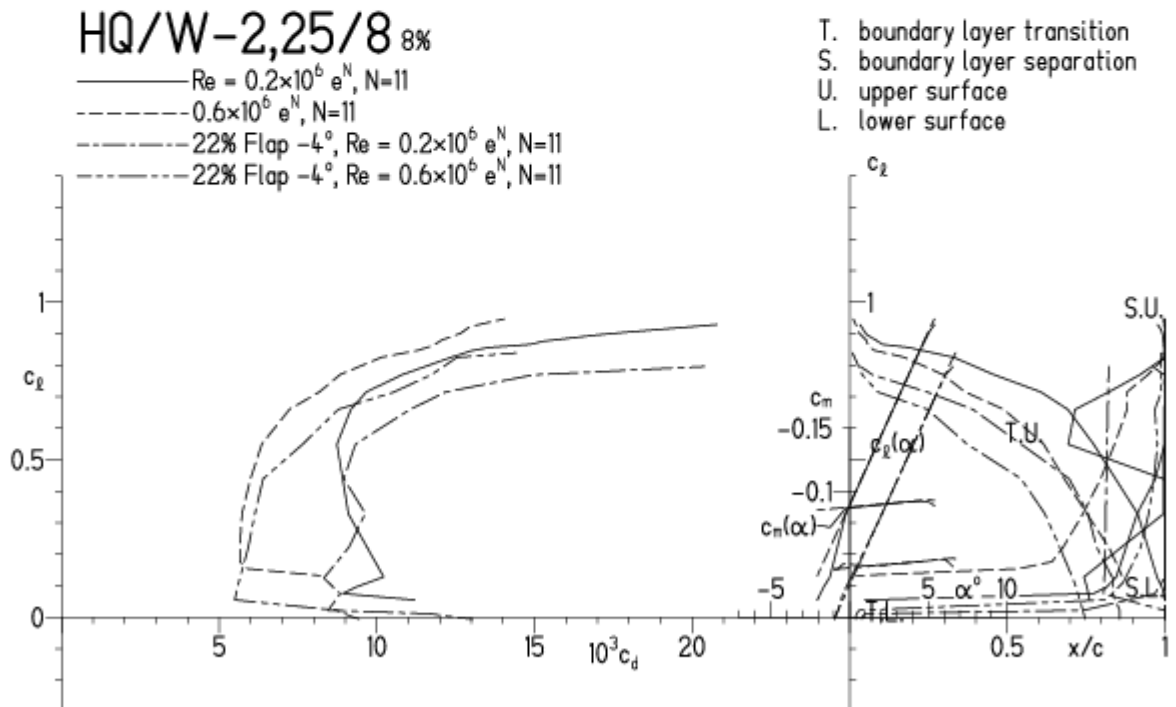


HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

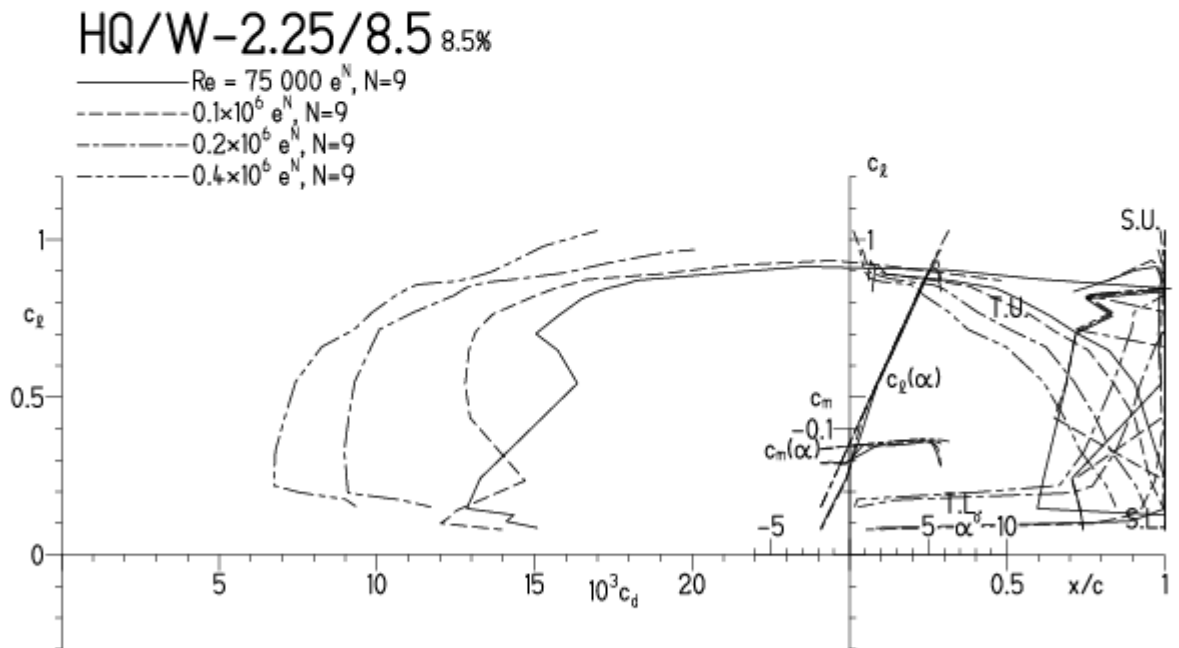


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

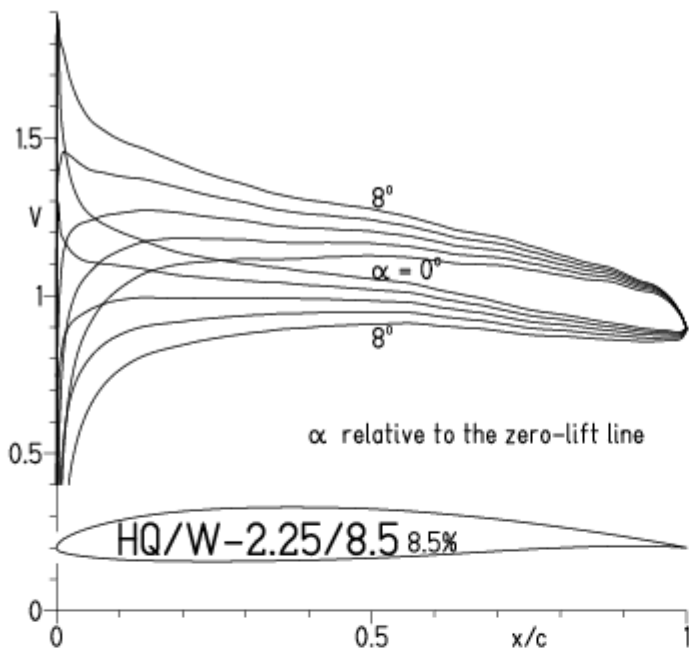


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

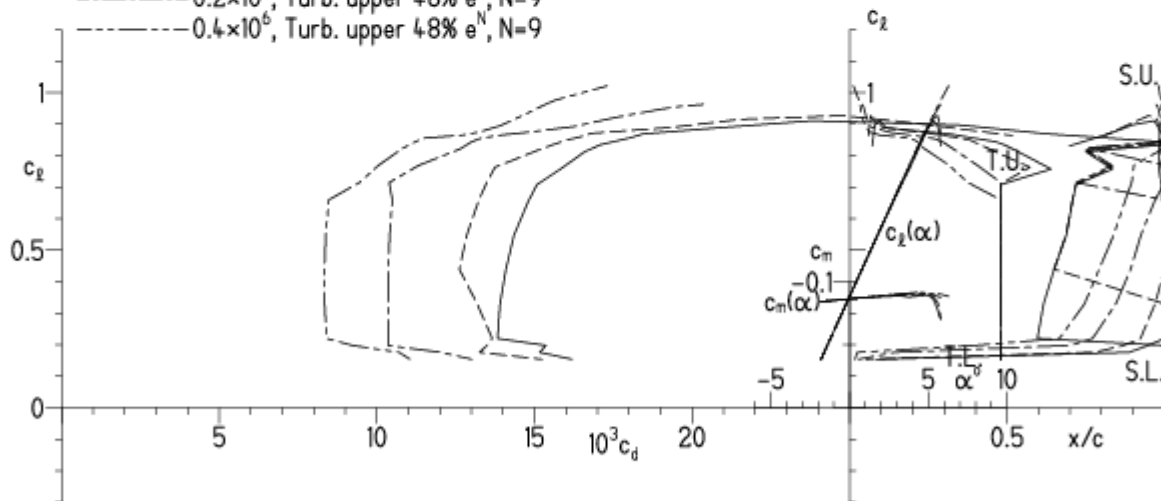
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

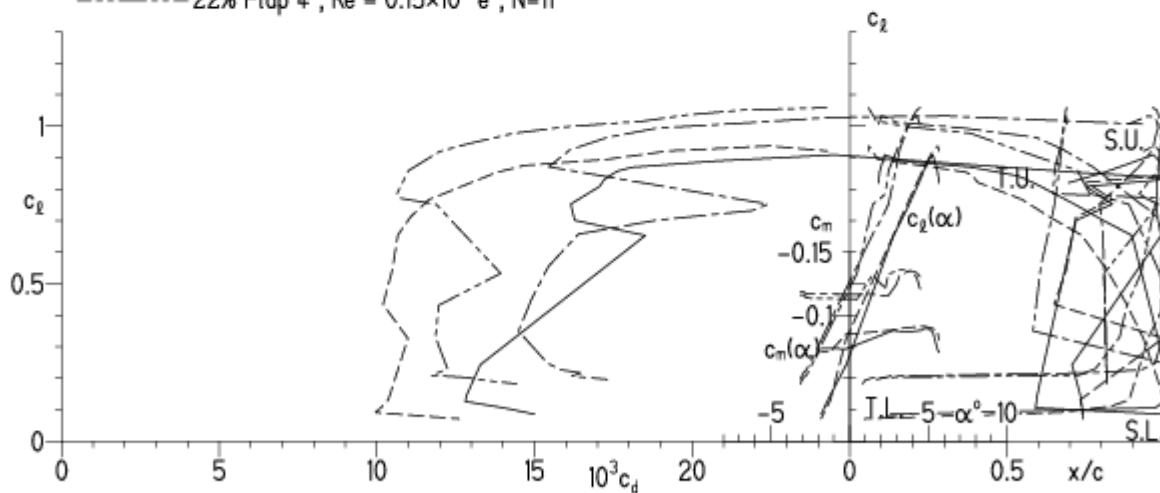


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.15×10^6 , Turb. upper 48% e^N , $N=9$
- · - 22% Flap 4° , $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- · - 22% Flap 4° , $Re = 0.15 \times 10^6$, Turb. upper 48% e^N , $N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

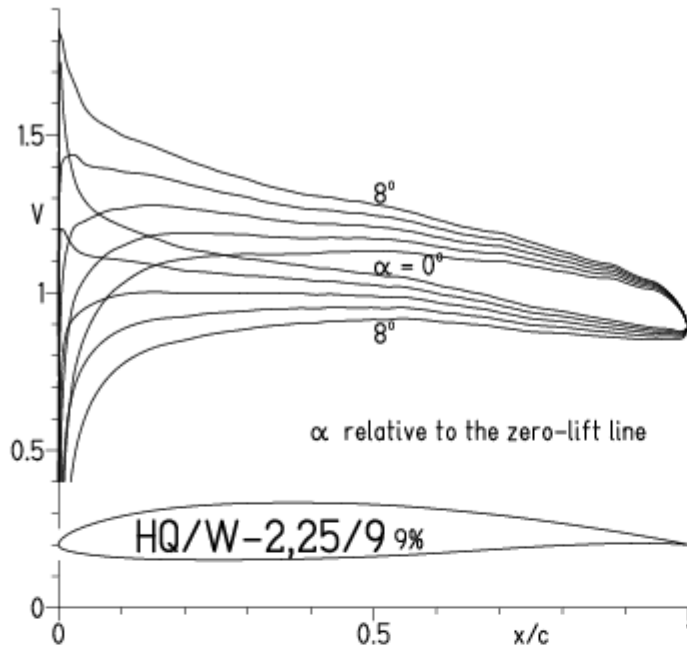


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

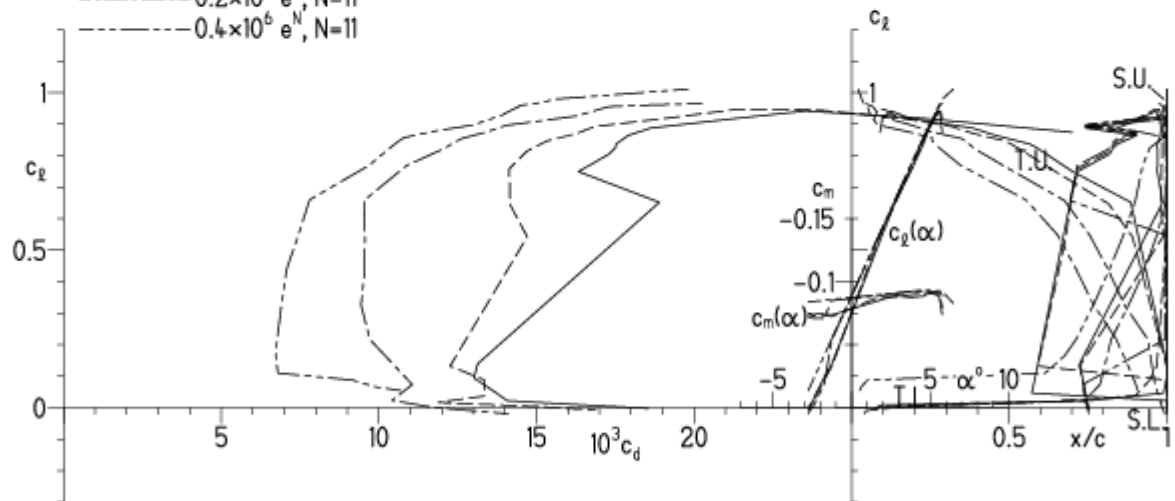
EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

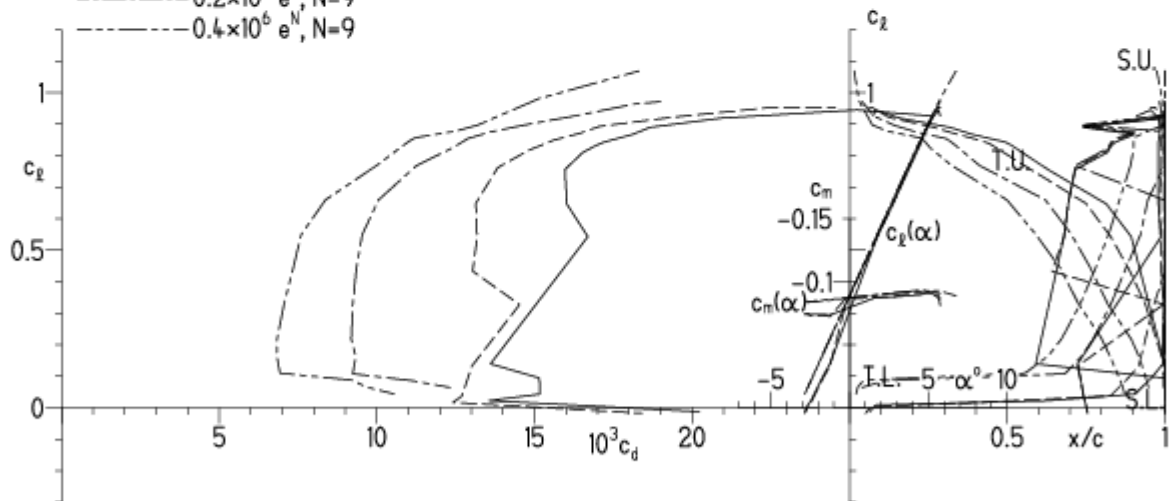
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

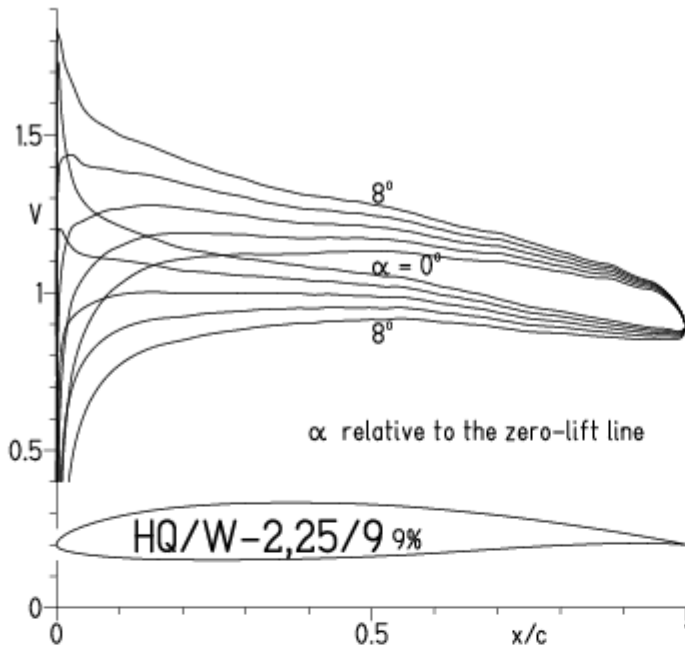
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

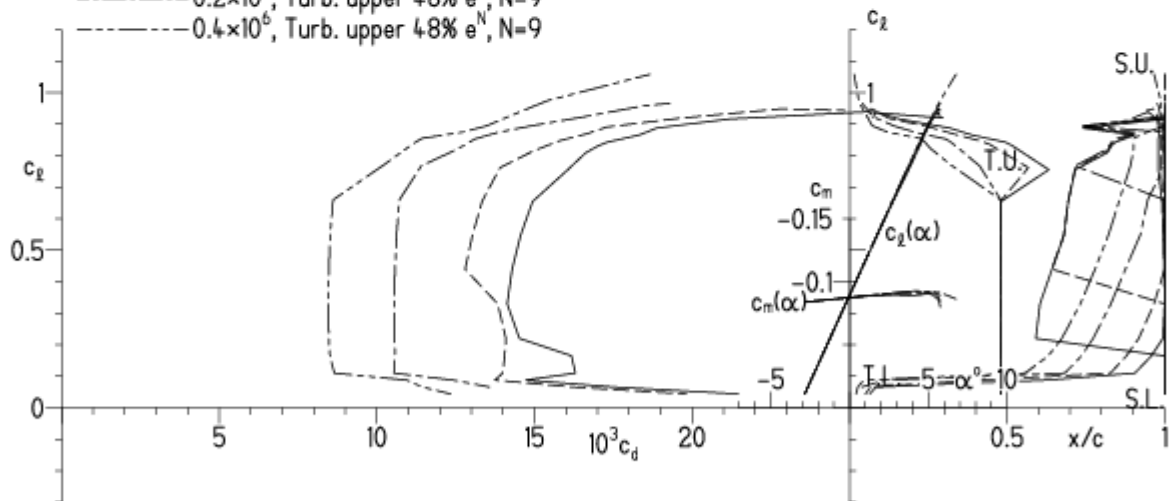
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

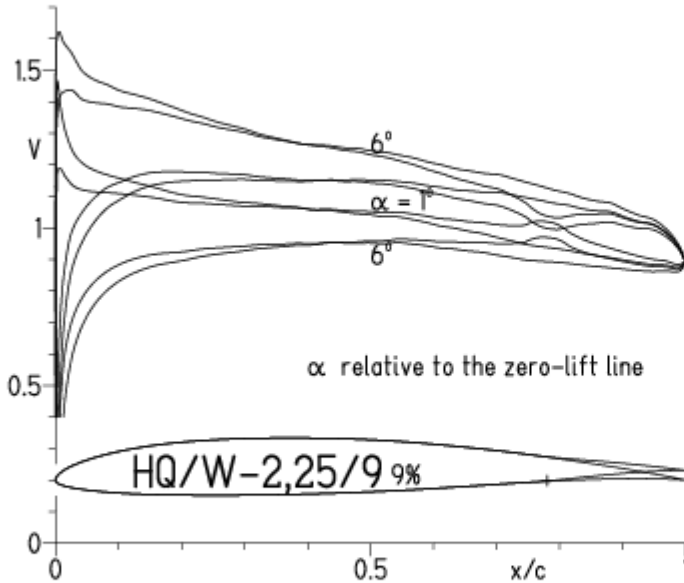
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



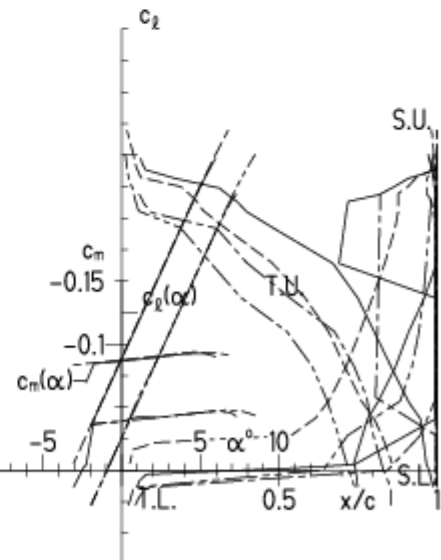
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N$, $N=11$
- - - $0.6 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 0.2 \times 10^6 e^N$, $N=11$
- · - · - 22% Flap -4°, $Re = 0.6 \times 10^6 e^N$, $N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

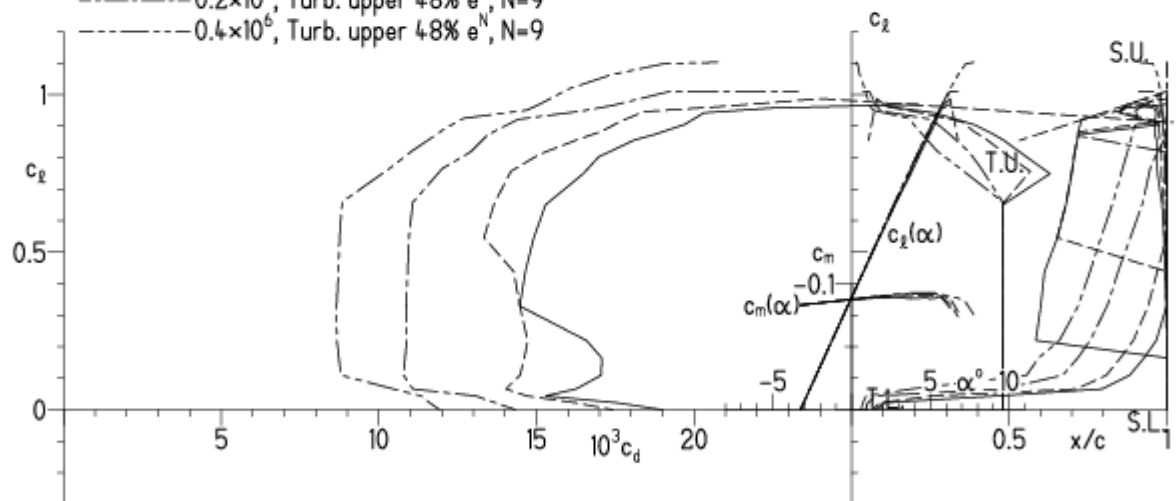
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

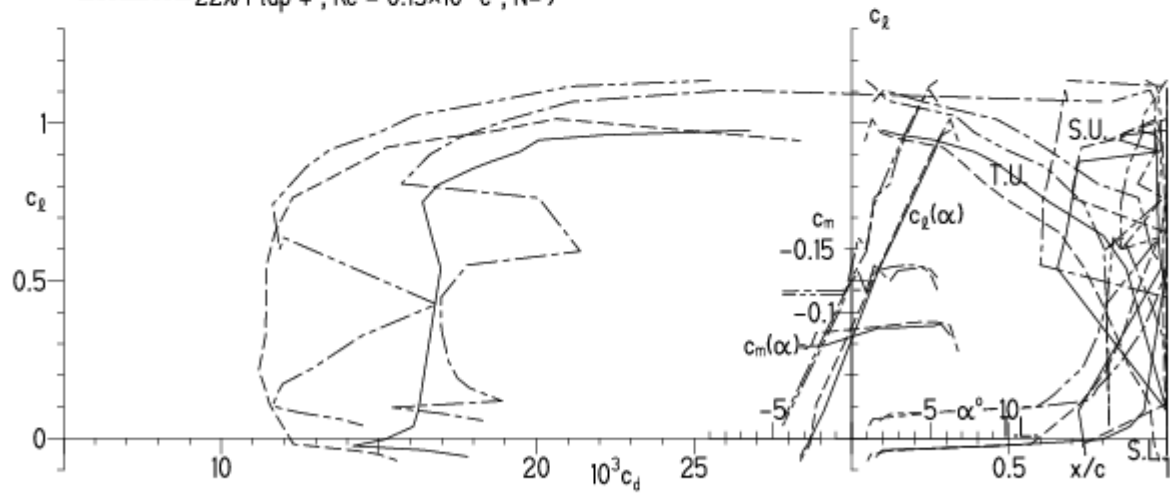


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

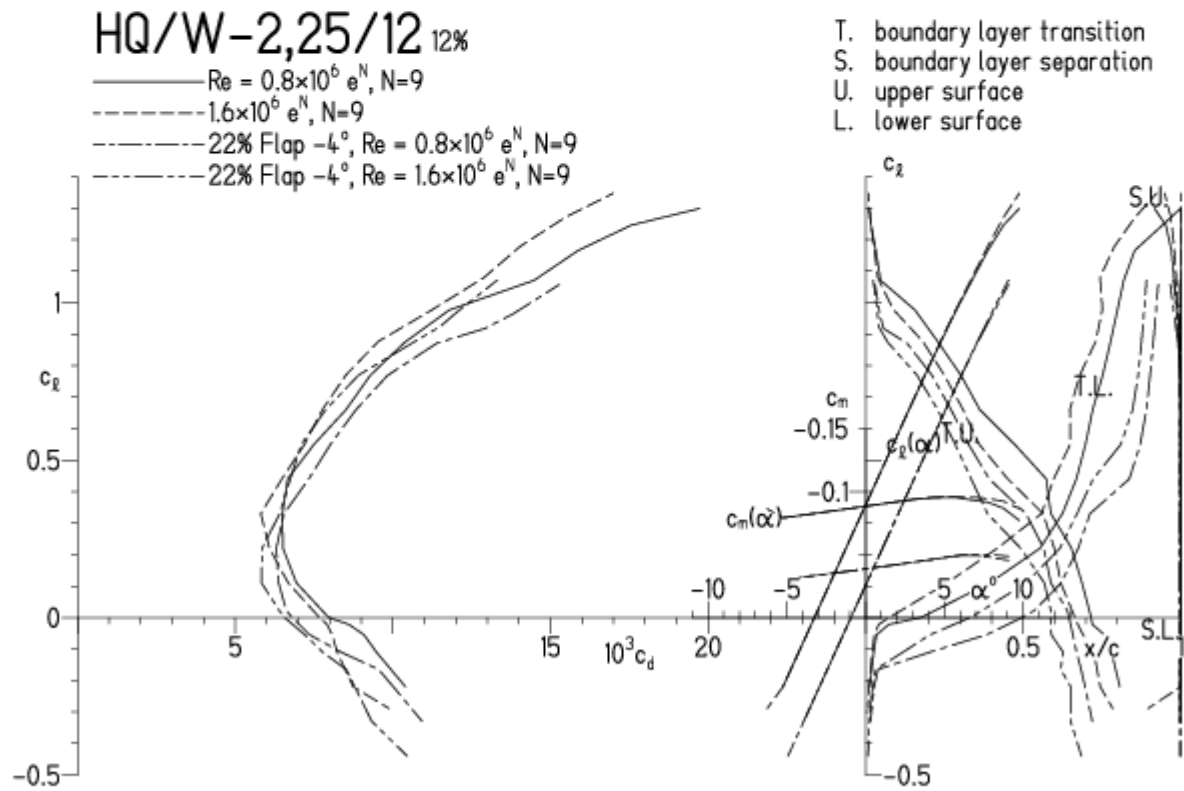


HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

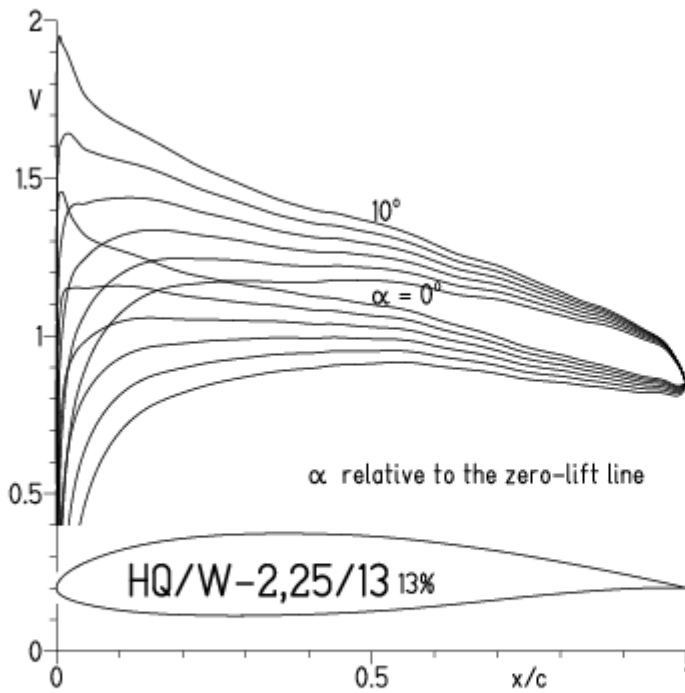


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

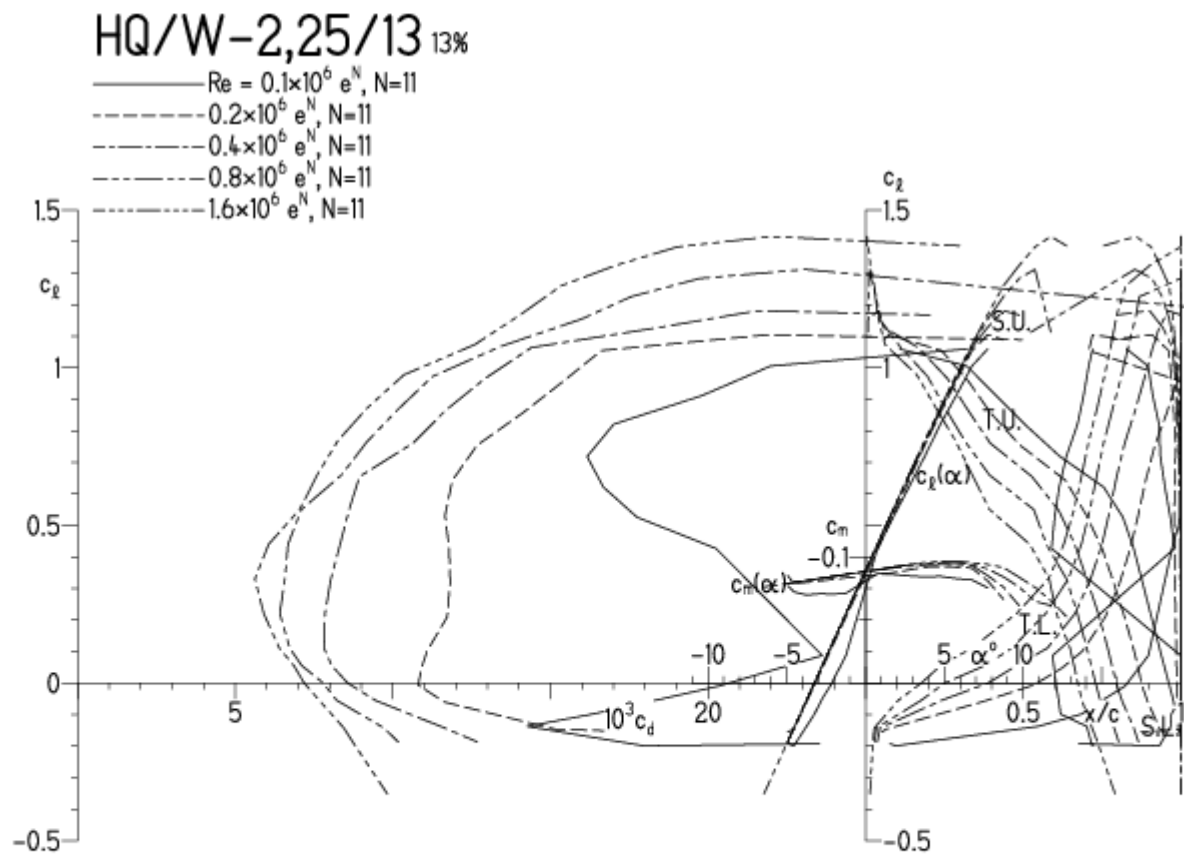


HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - · 0.4×10⁶, Turb. upper 48% e^N, N=9



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

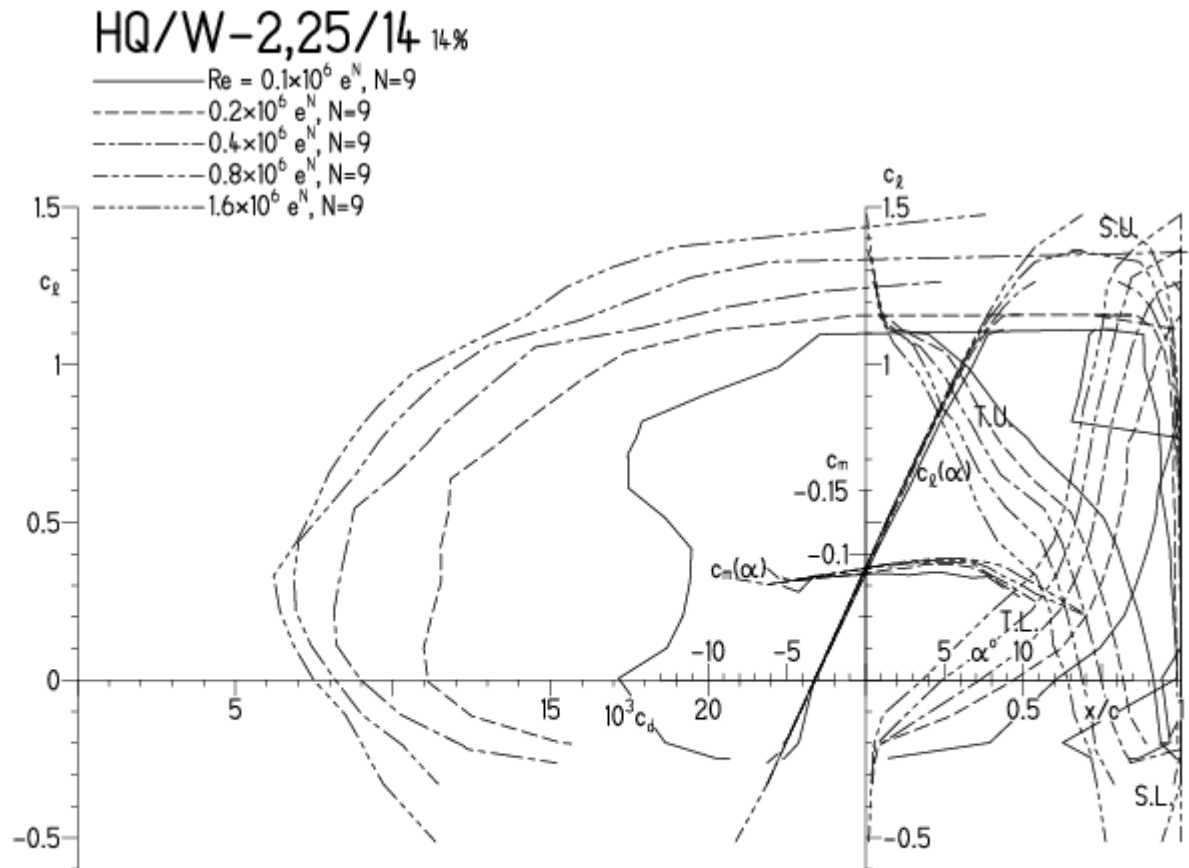


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

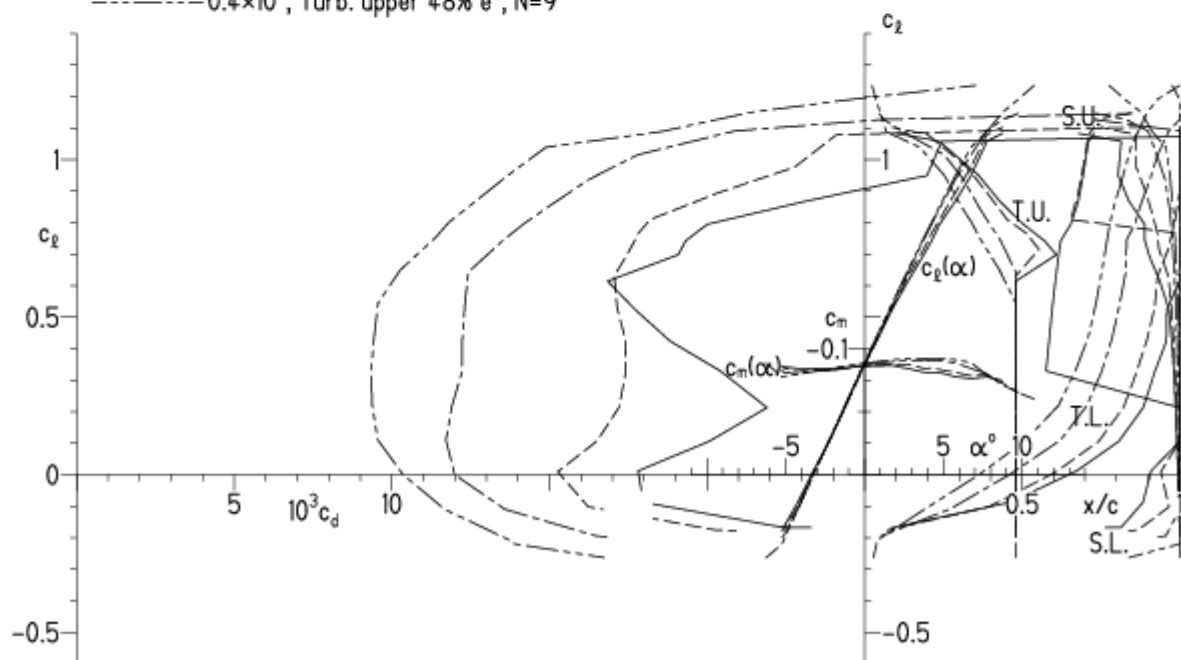
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

HQ/W-2,25/14 14%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56



EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

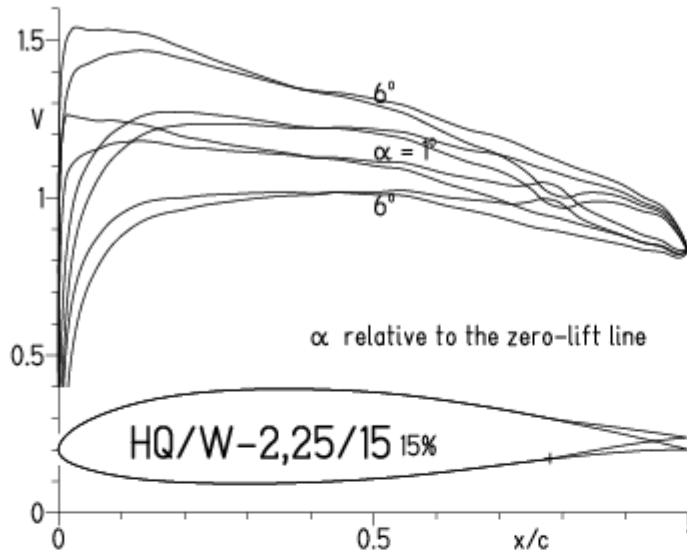


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



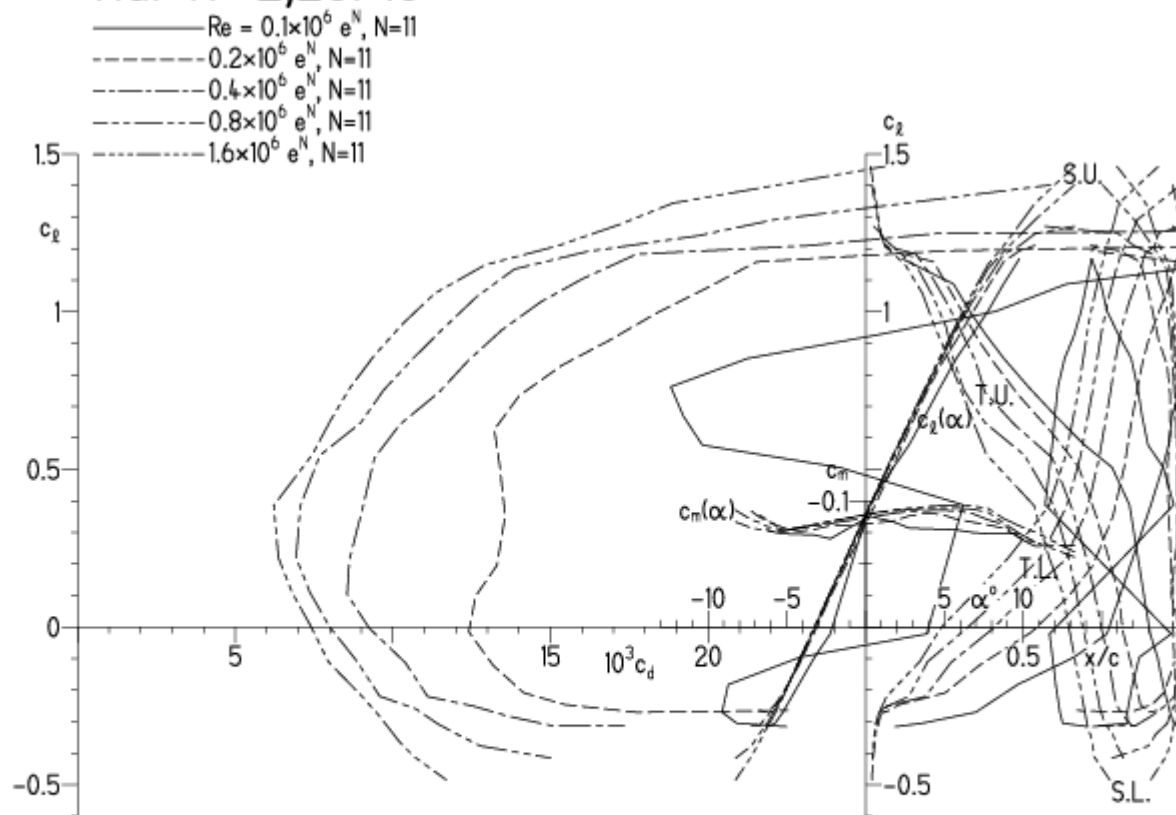
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

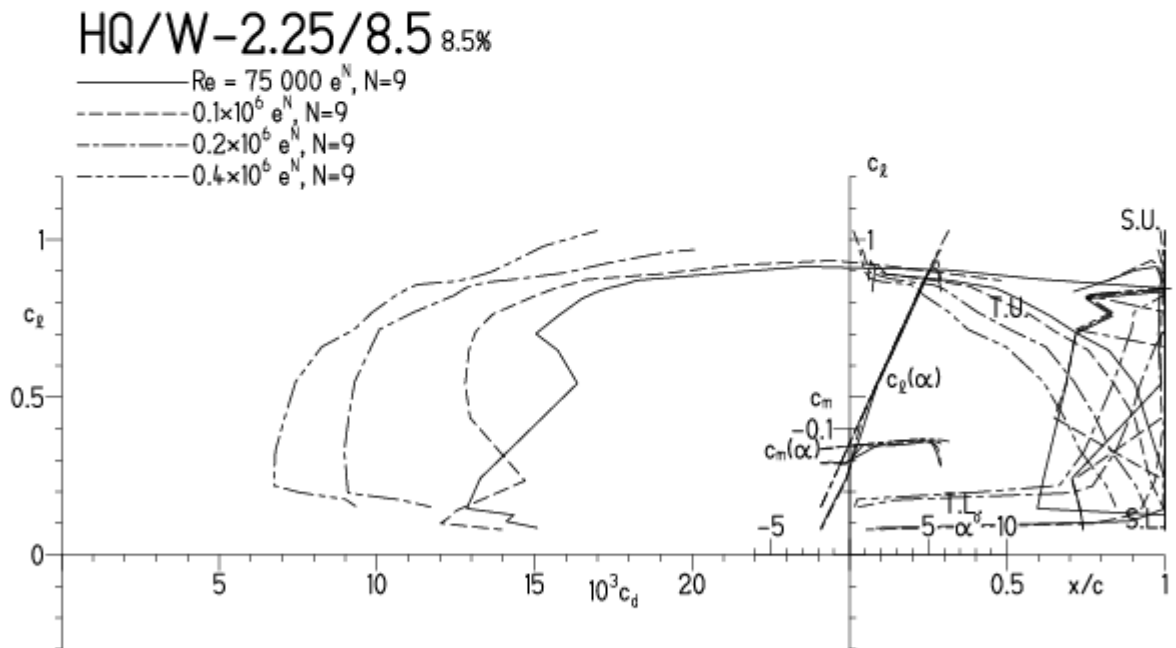


HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33

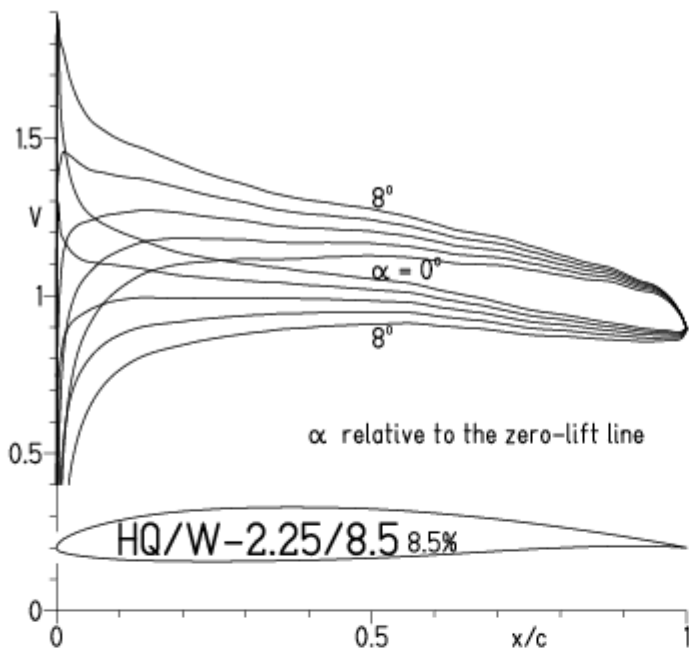


EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

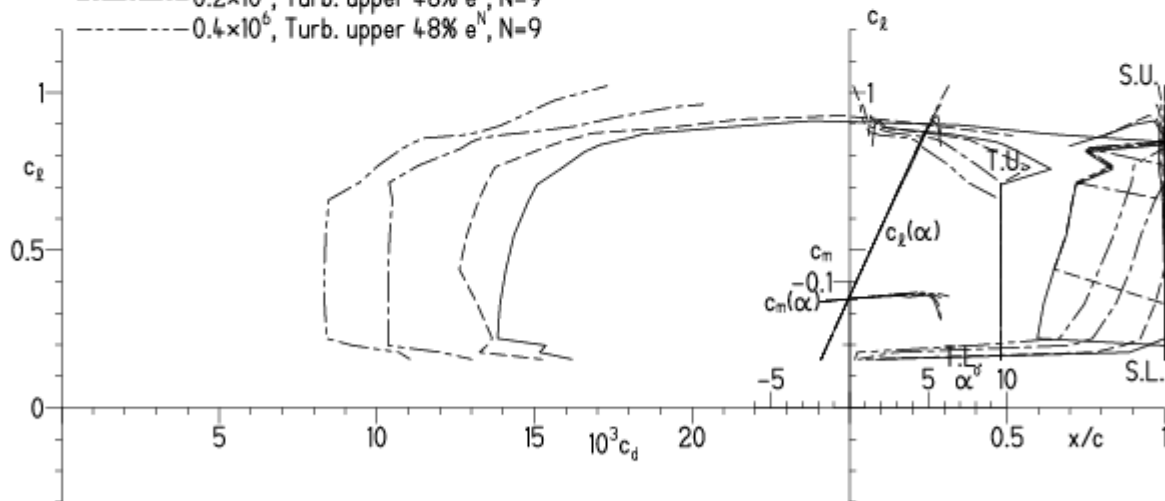
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12

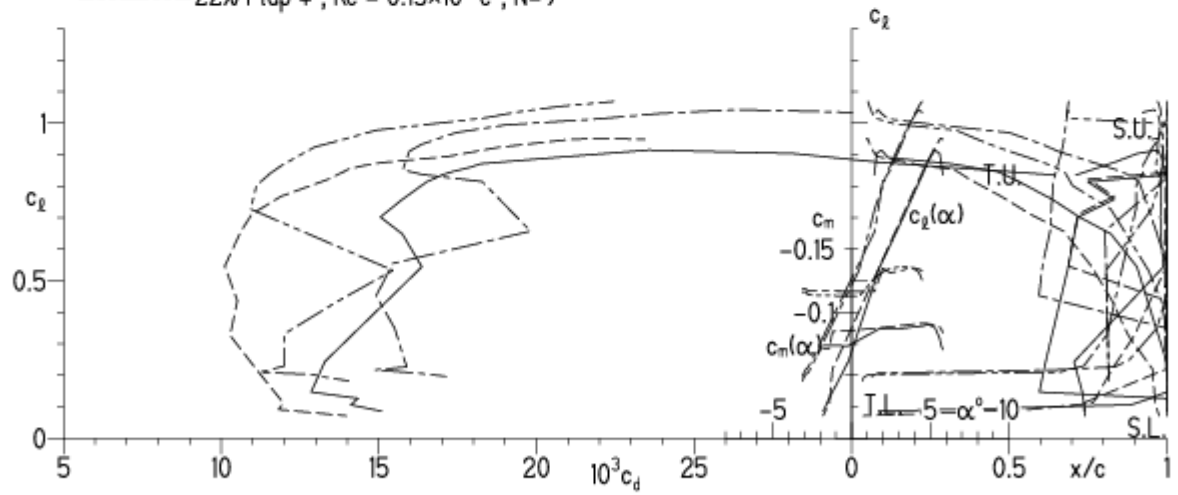


EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

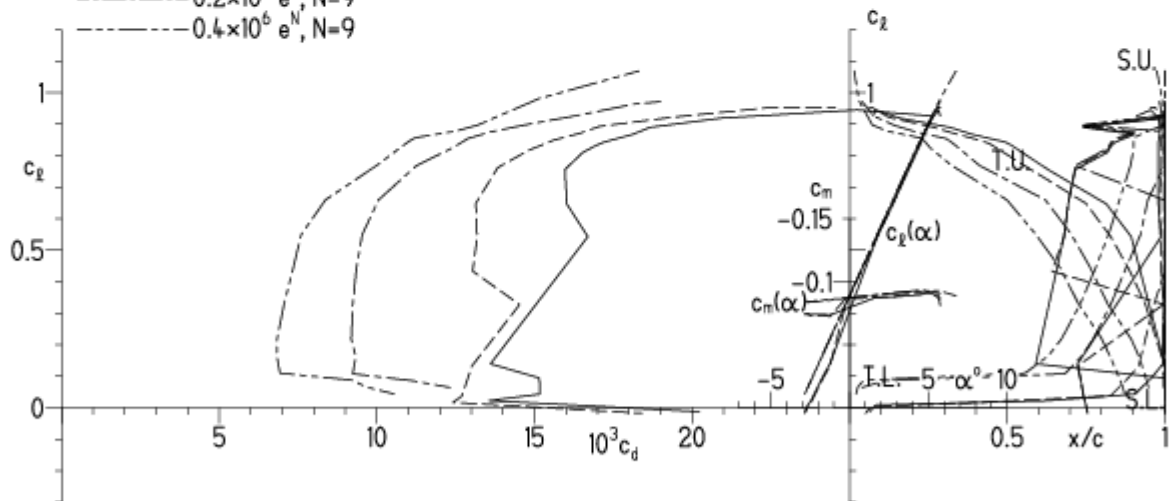
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

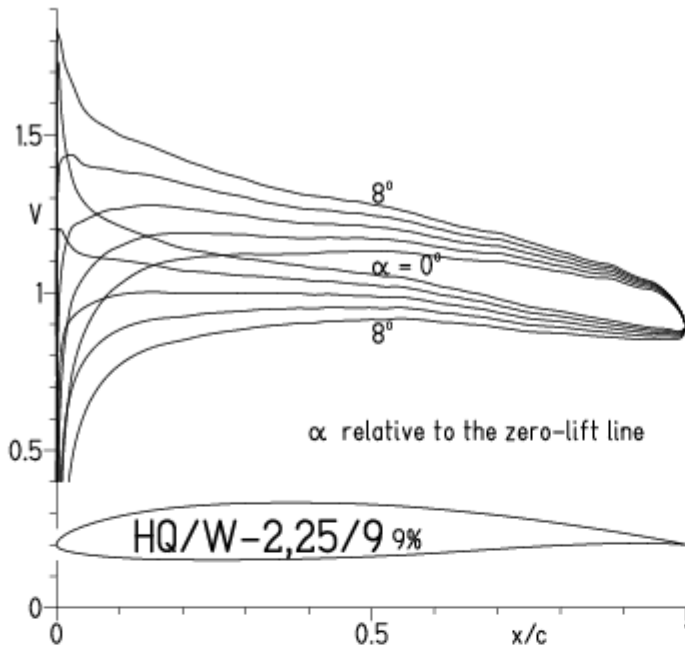
HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

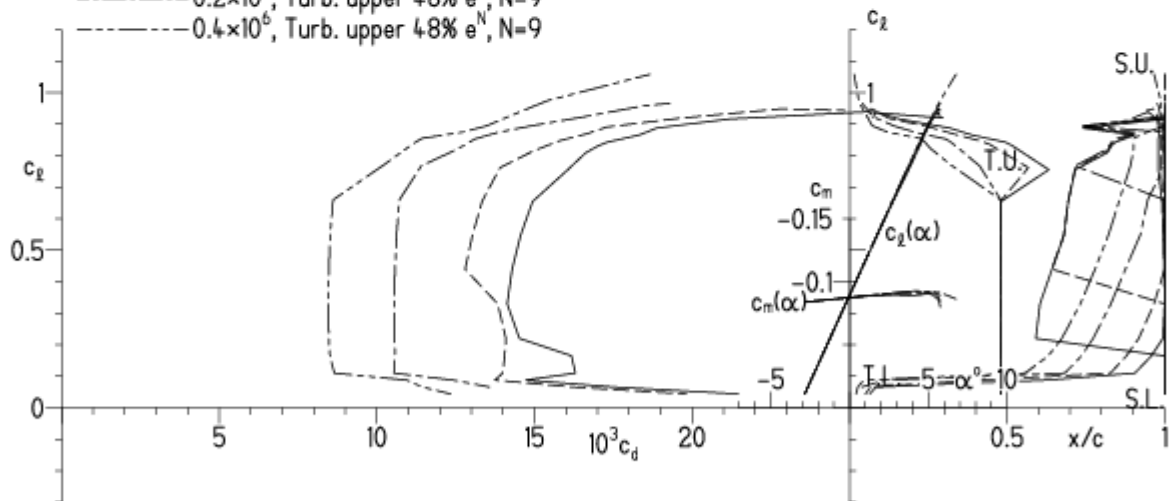
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- · - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11



HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

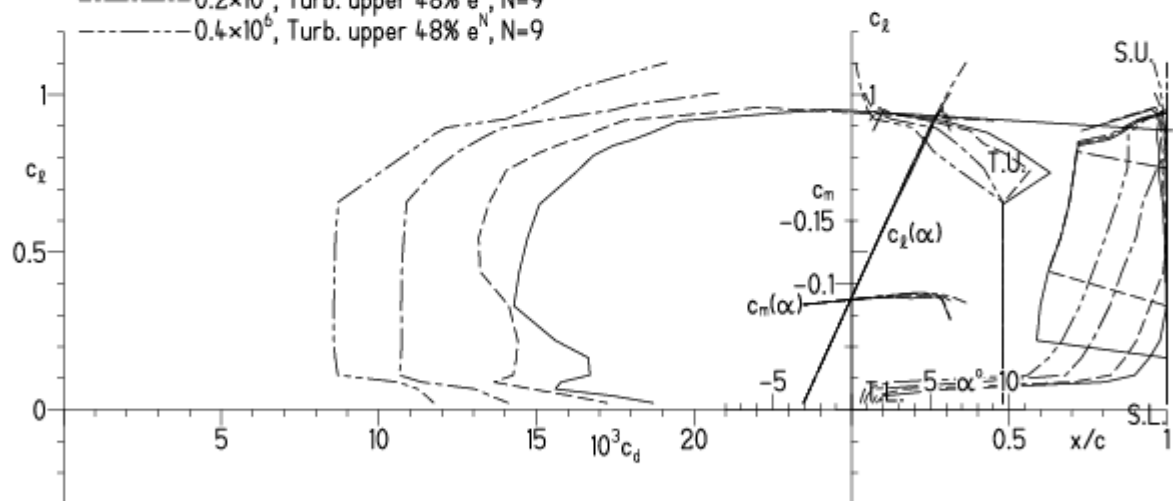
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

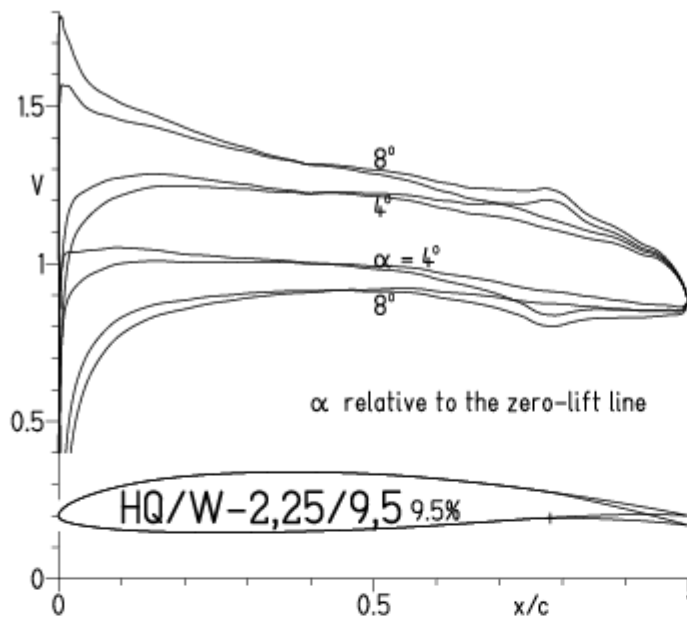
- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=11$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

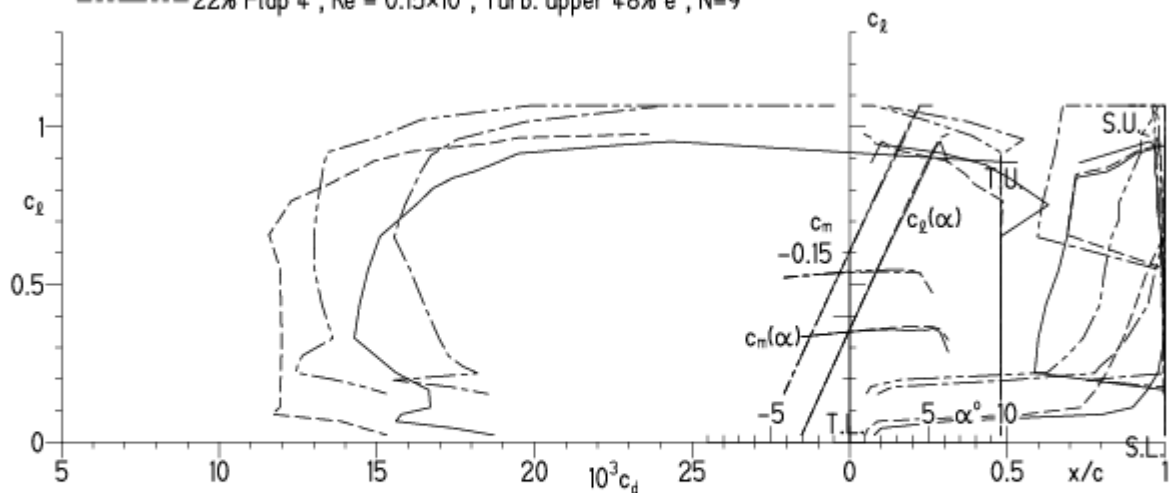


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.15×10^6 , Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N , N=9
- · - 22% Flap 4°, Re = 0.15×10^6 , Turb. upper 48% e^N , N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

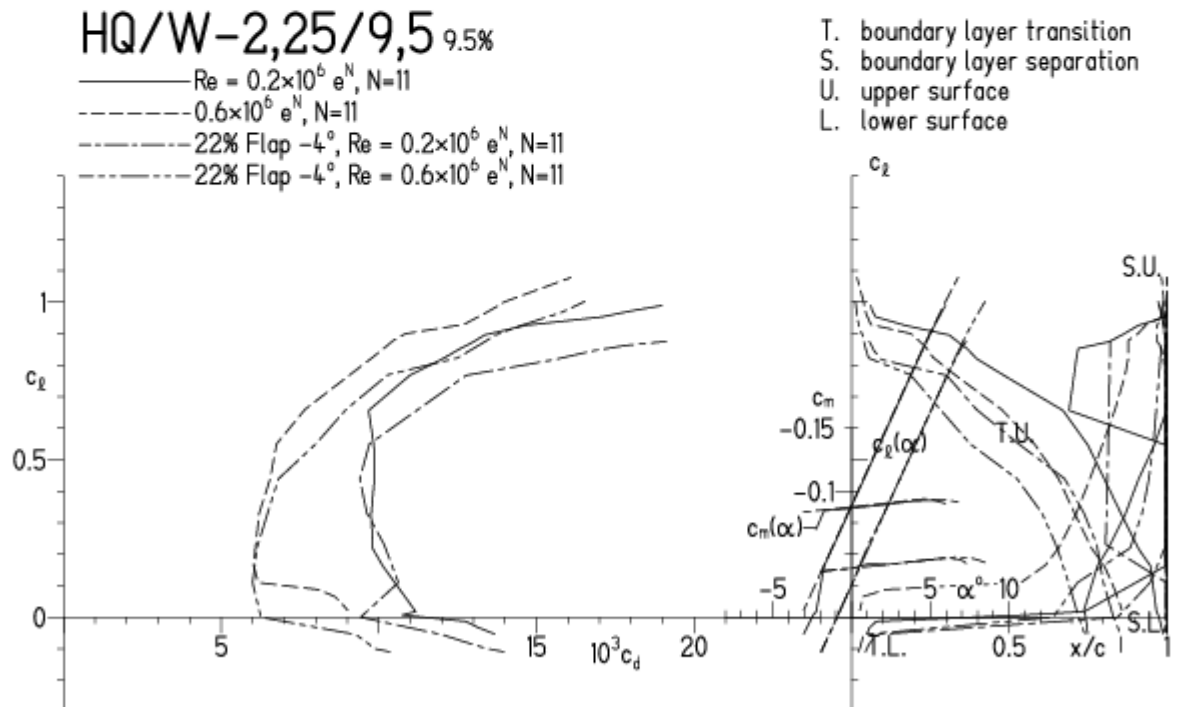


HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

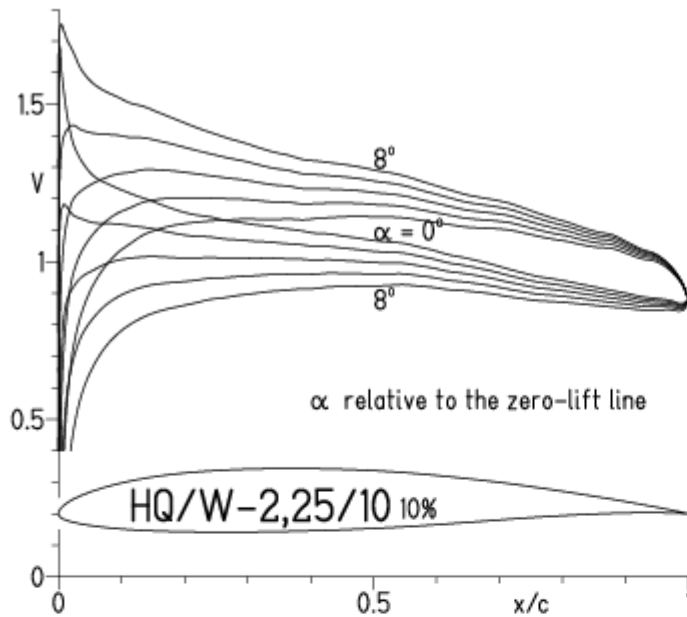


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

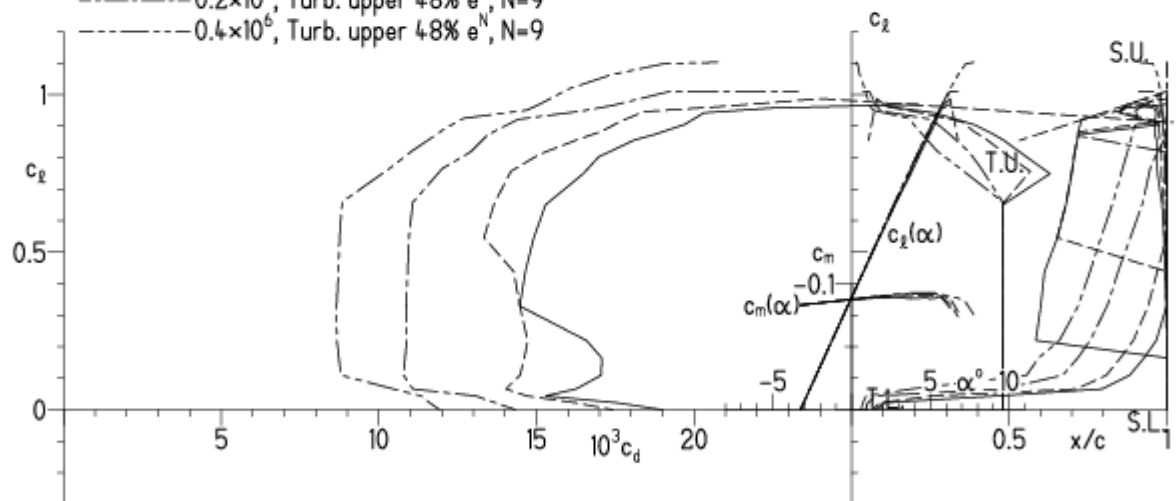
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

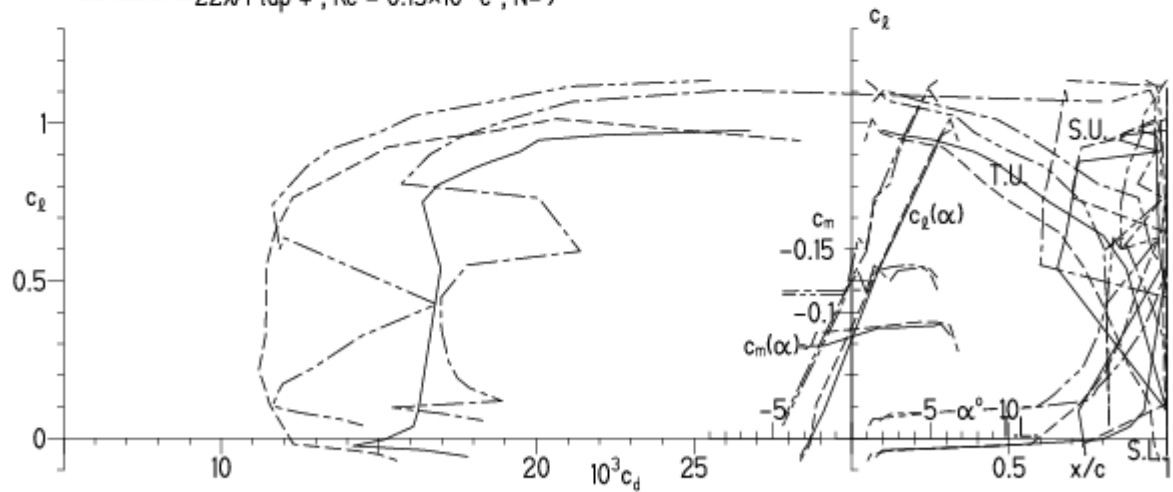


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32



EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

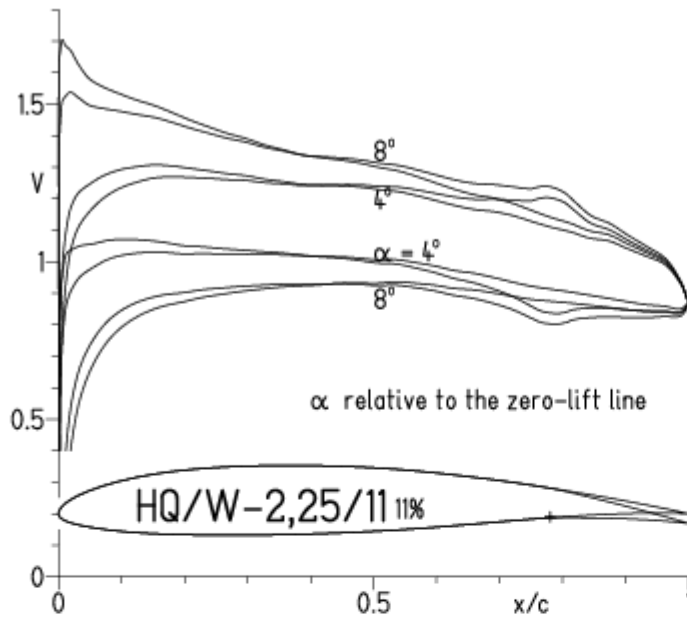
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24

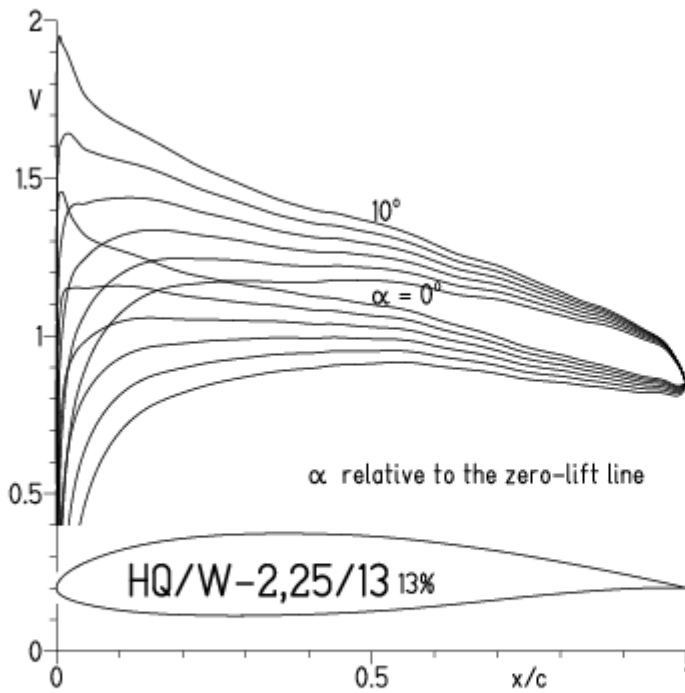


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

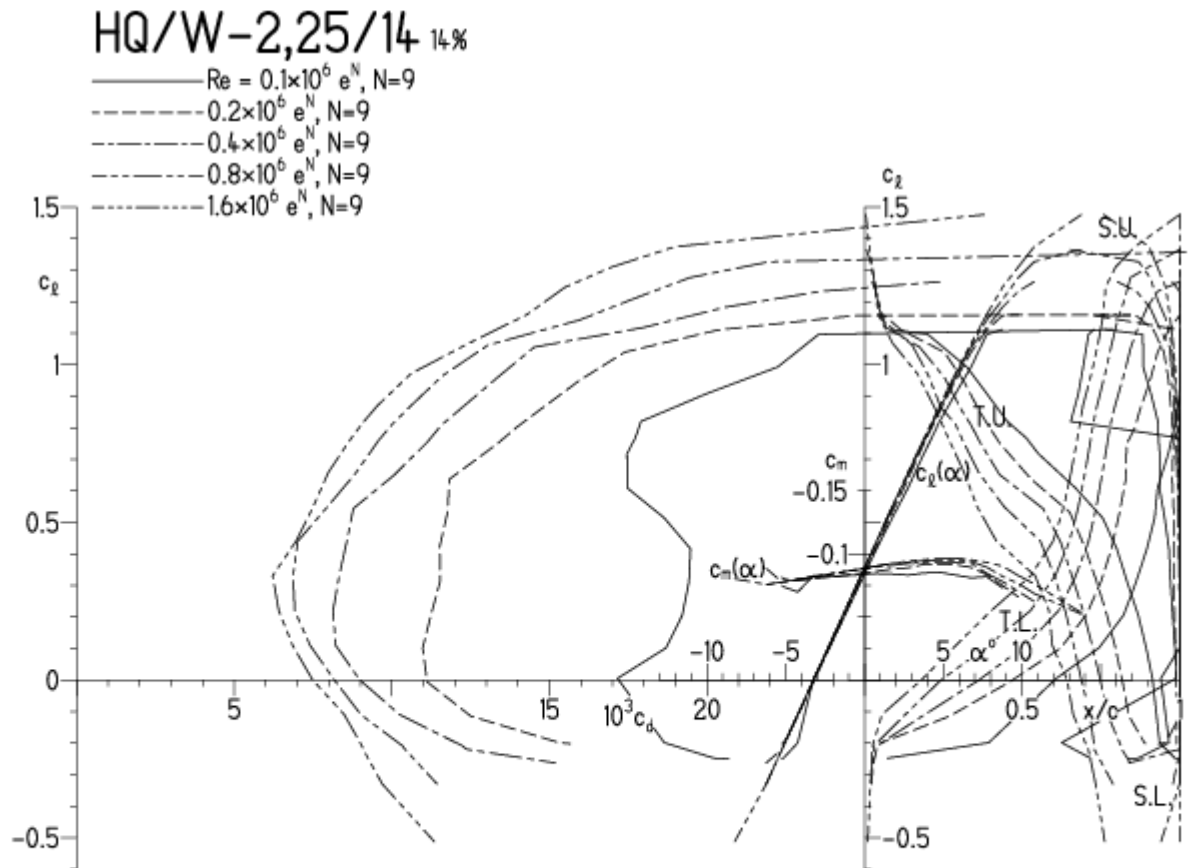


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

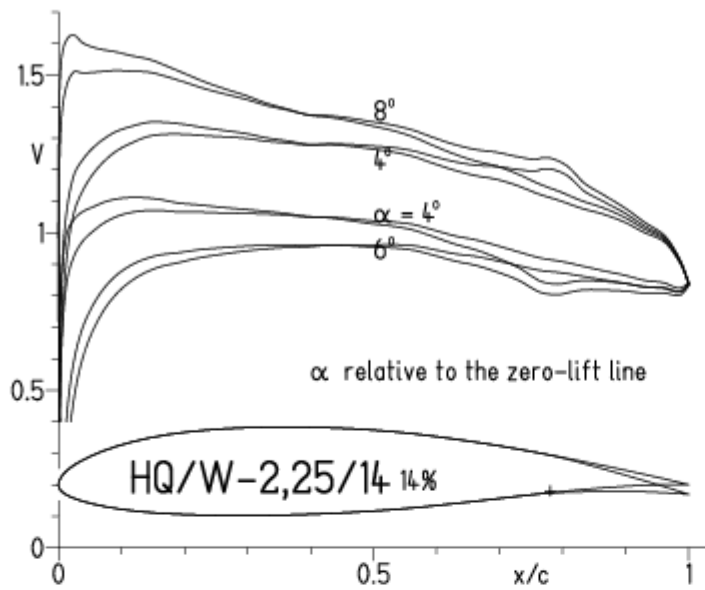
HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

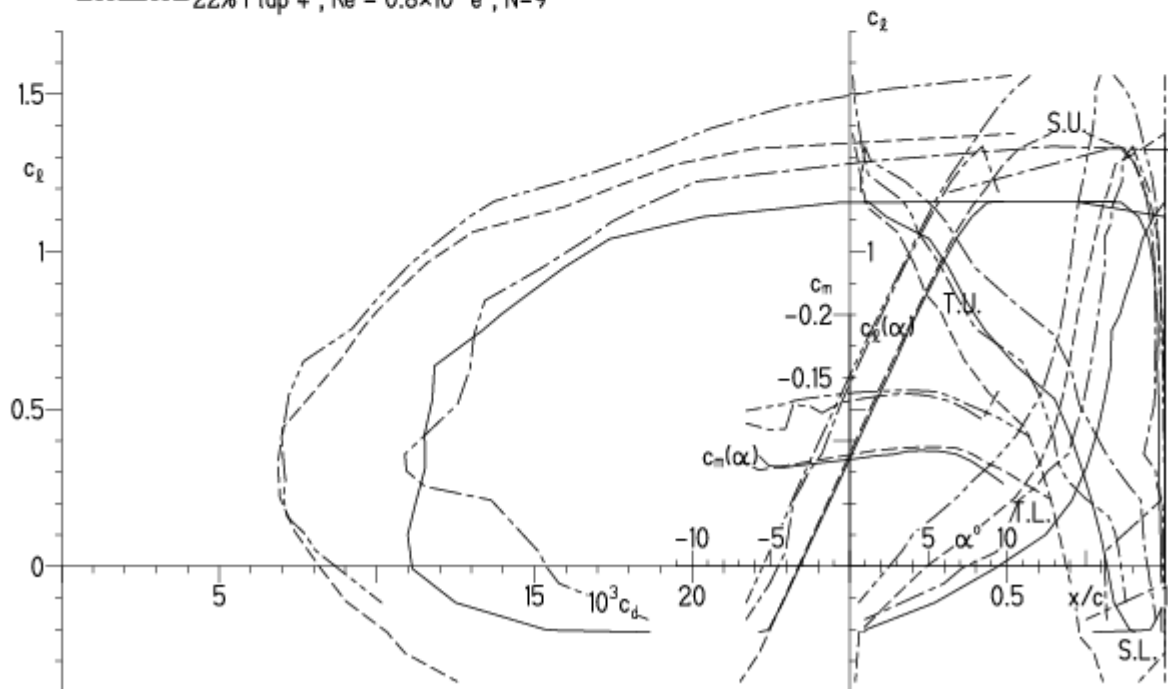


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

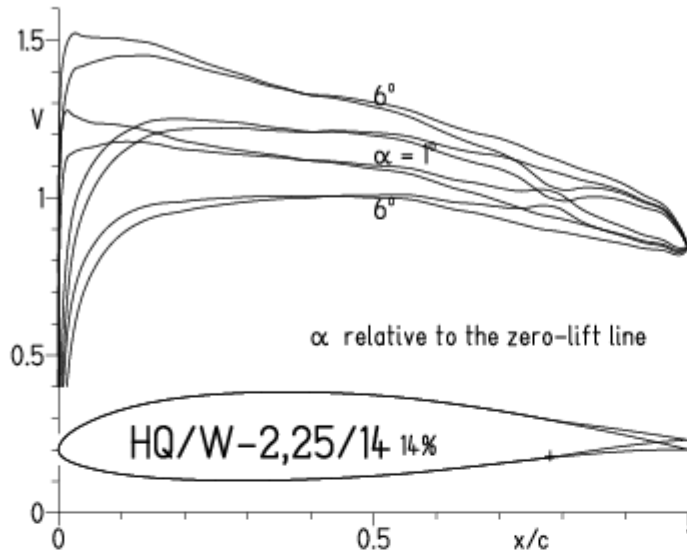
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

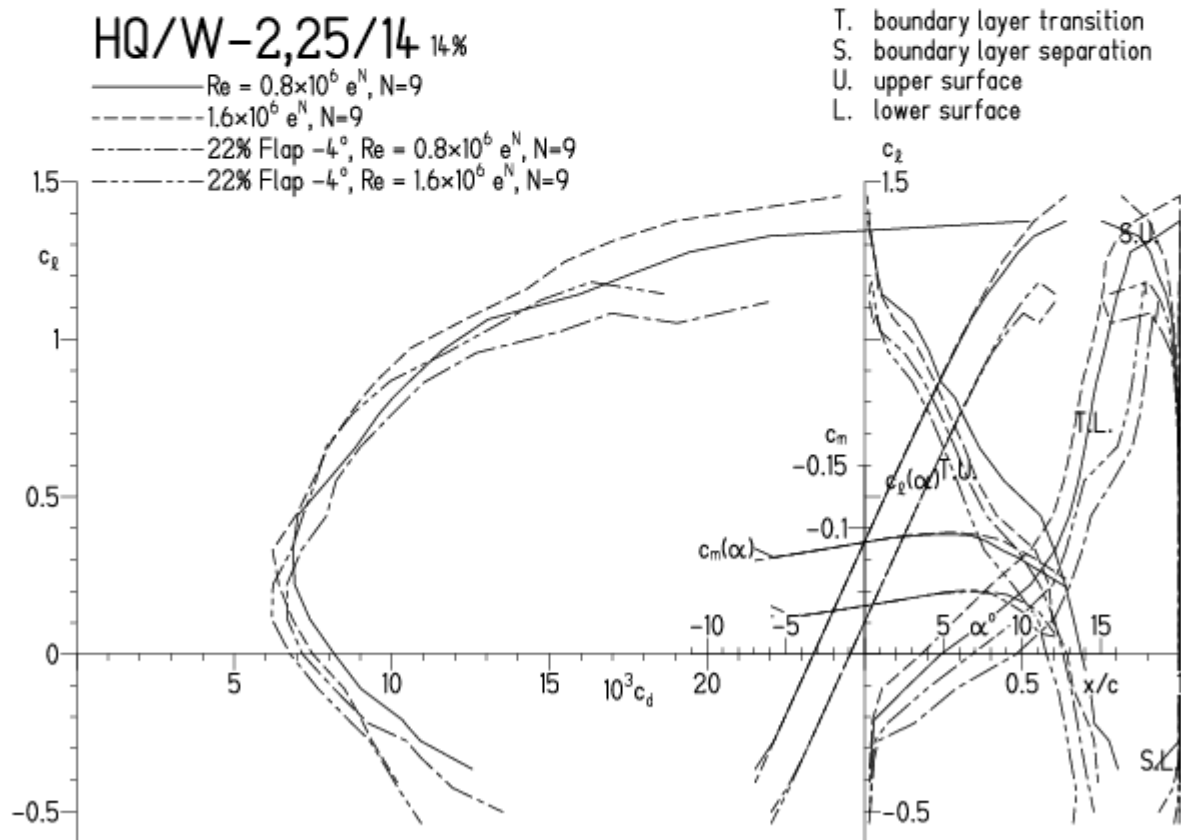


HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

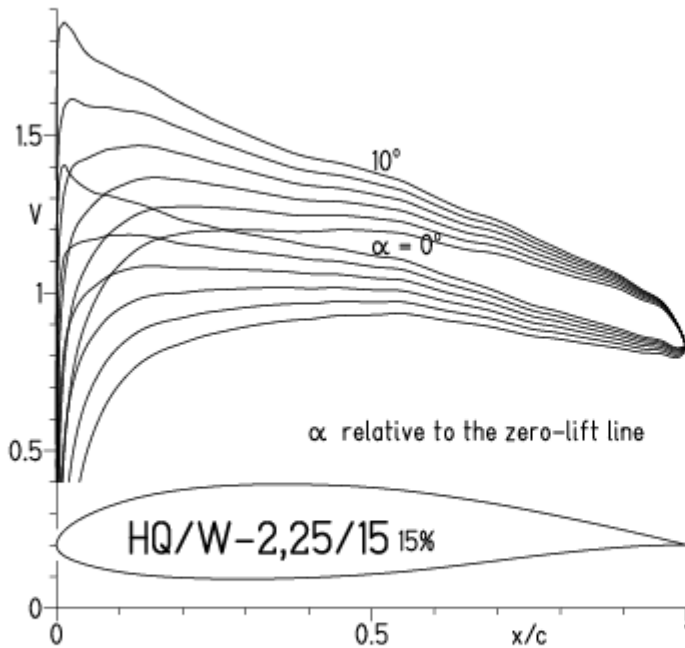


EPPLER 2005 V. 8.5.07

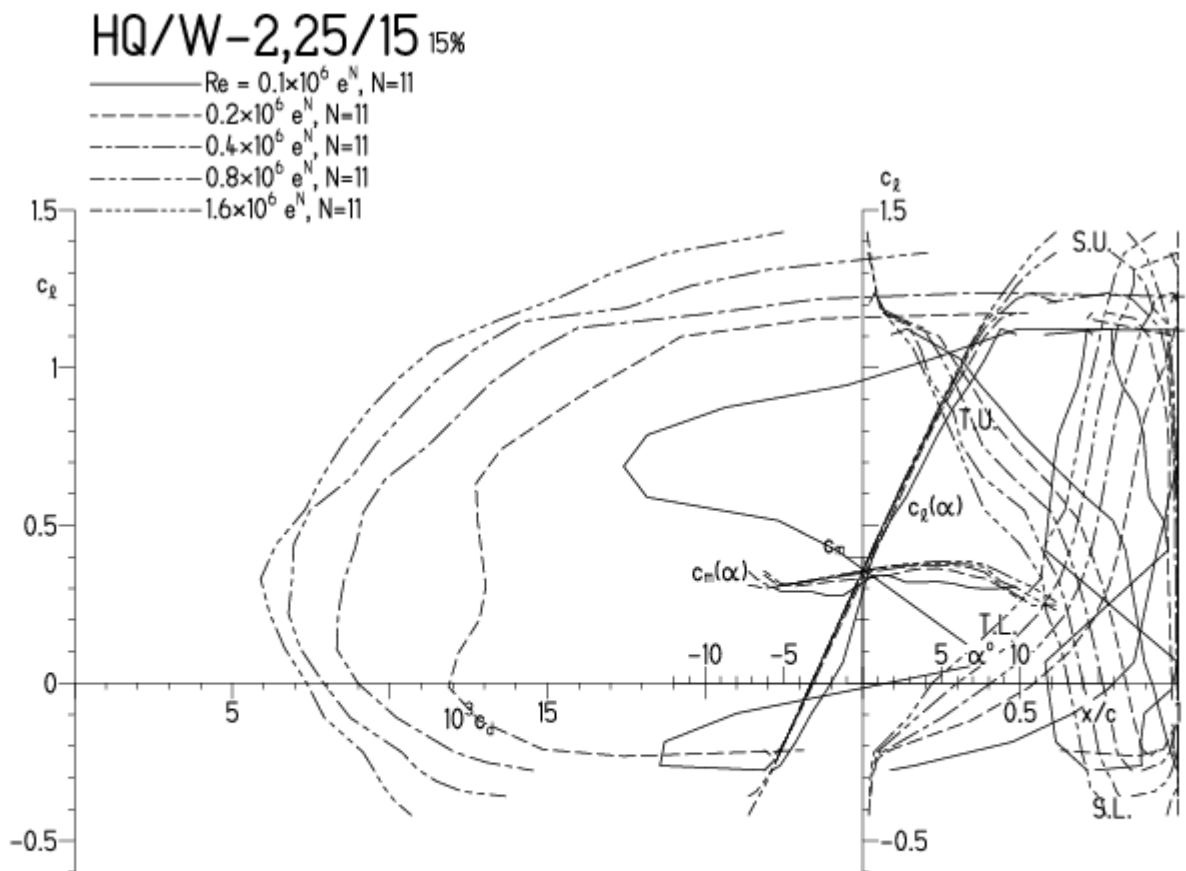


HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13

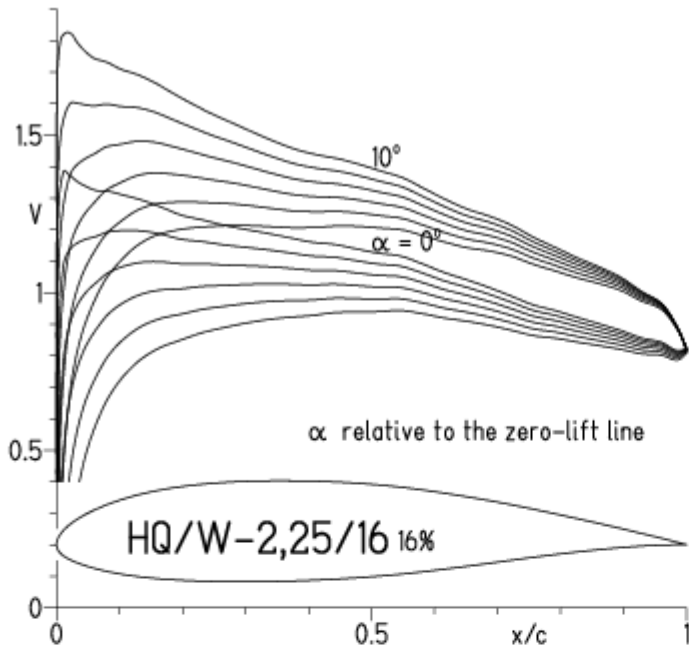


EPPLER 200



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41

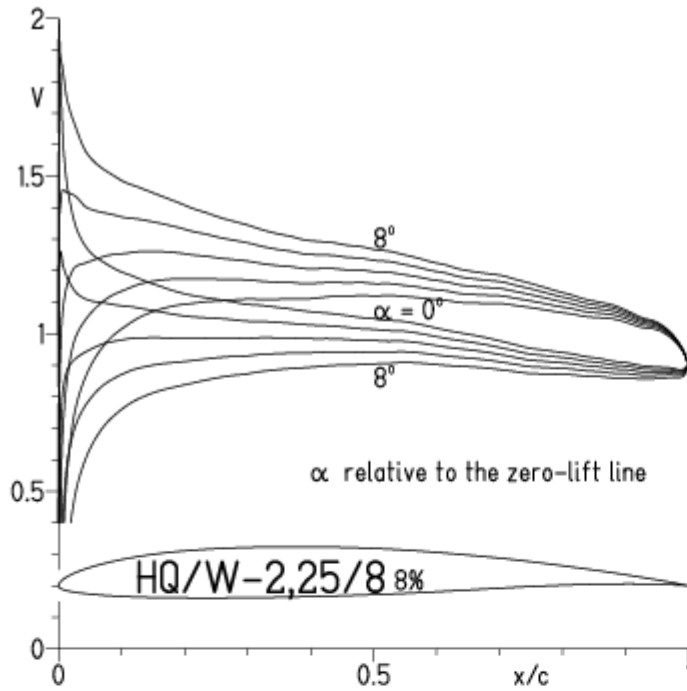


EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

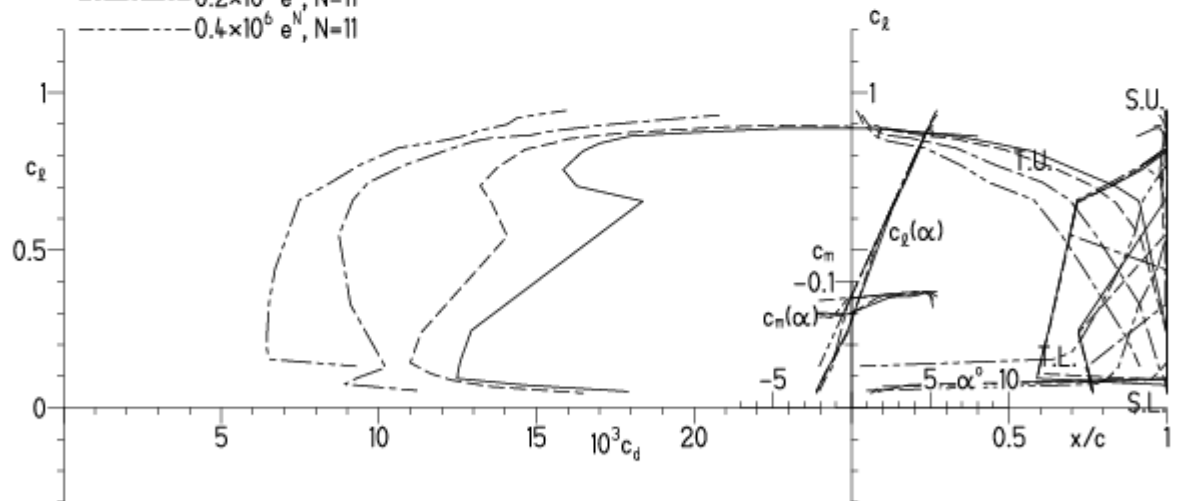
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



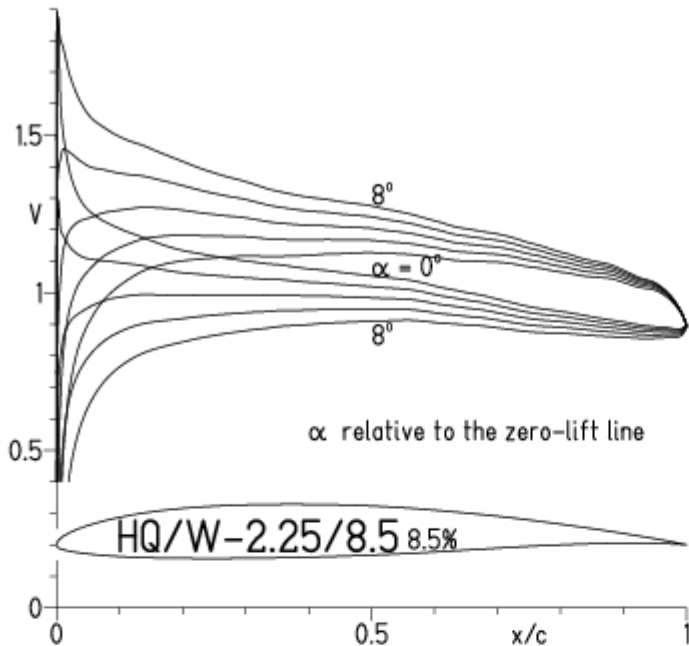
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

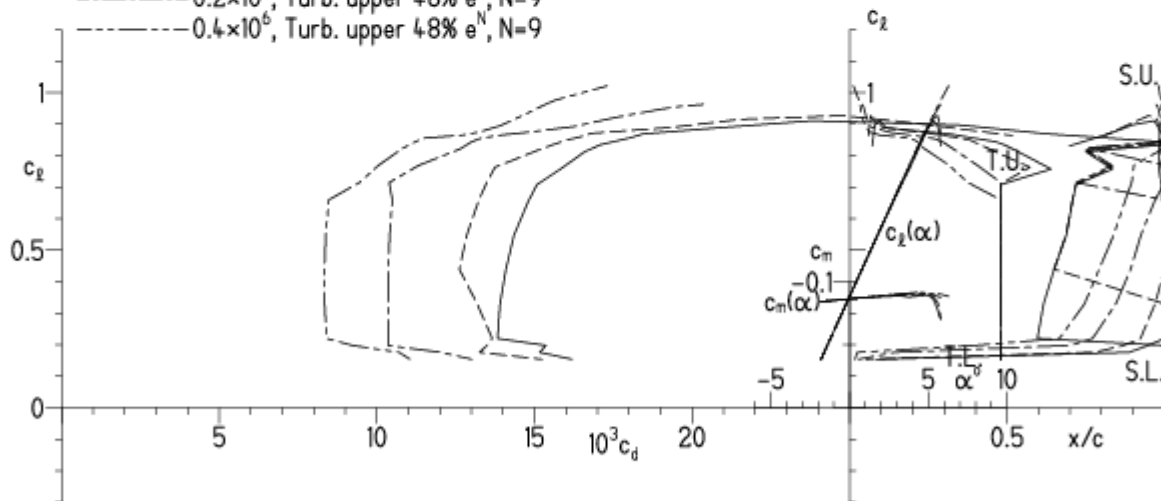
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000$, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08



EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

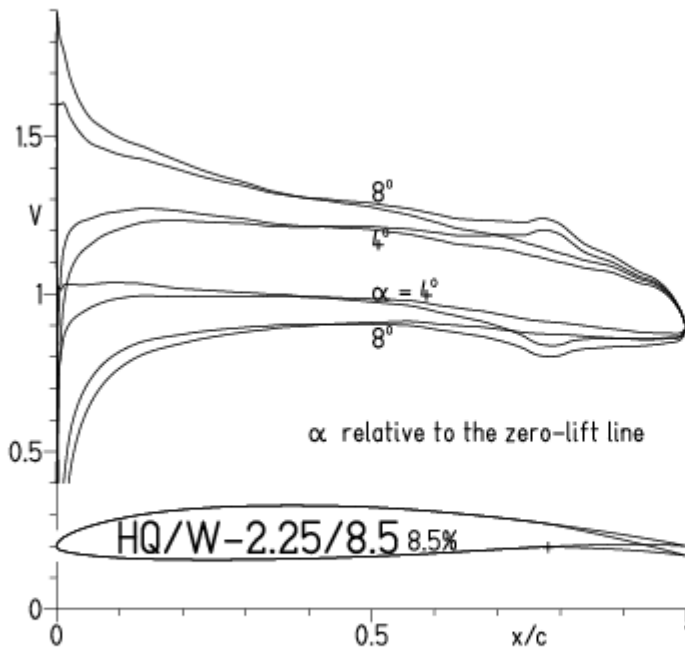
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

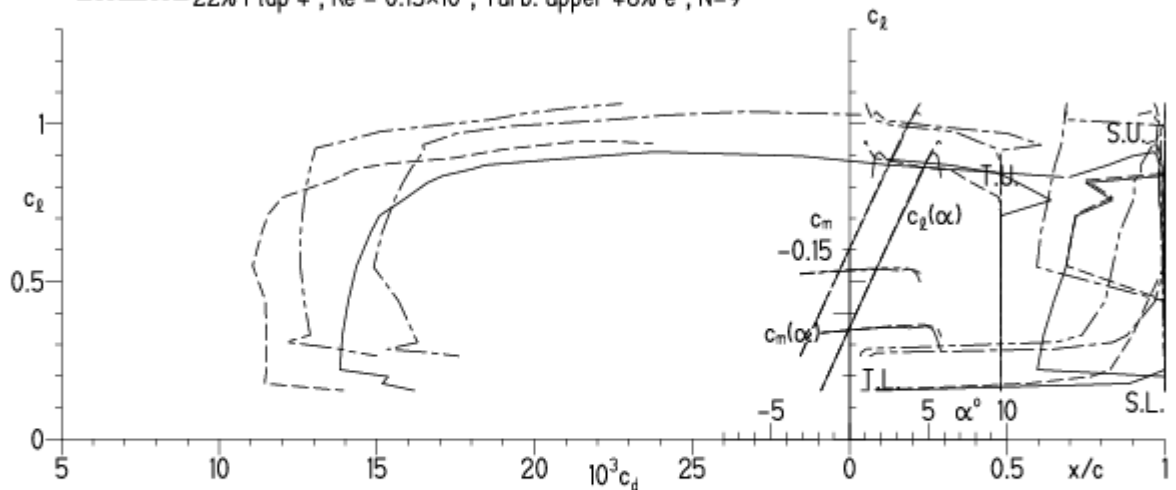


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

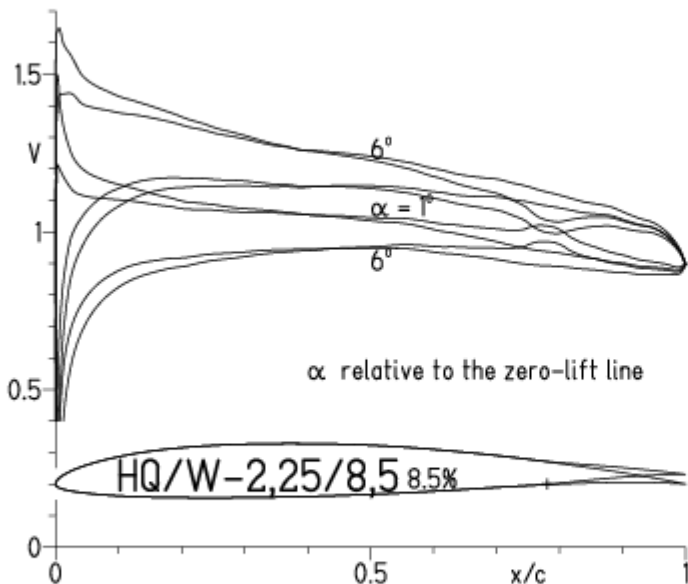
- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface

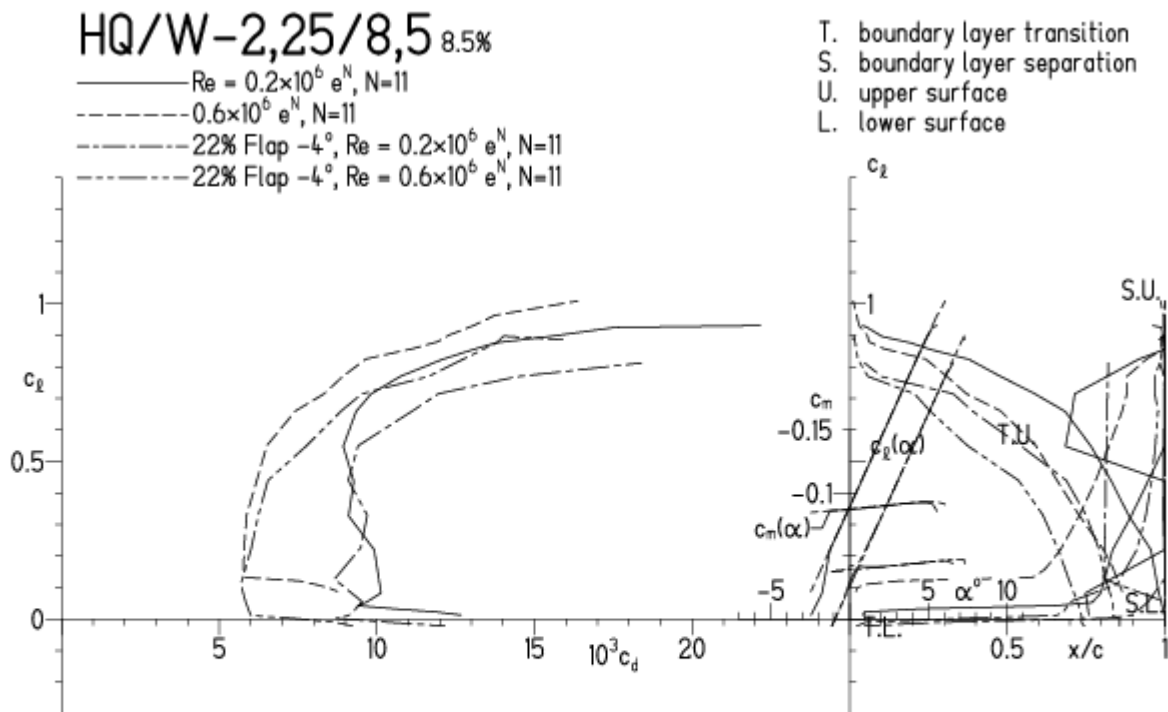


HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

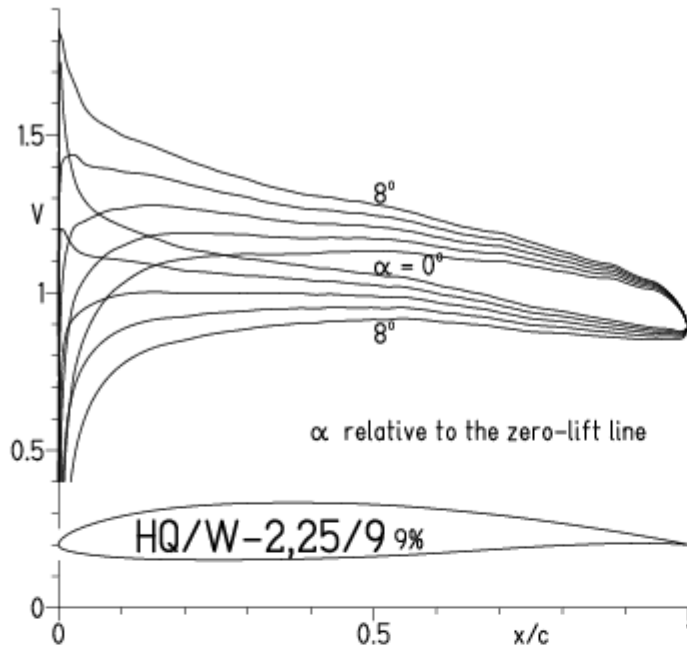


EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09

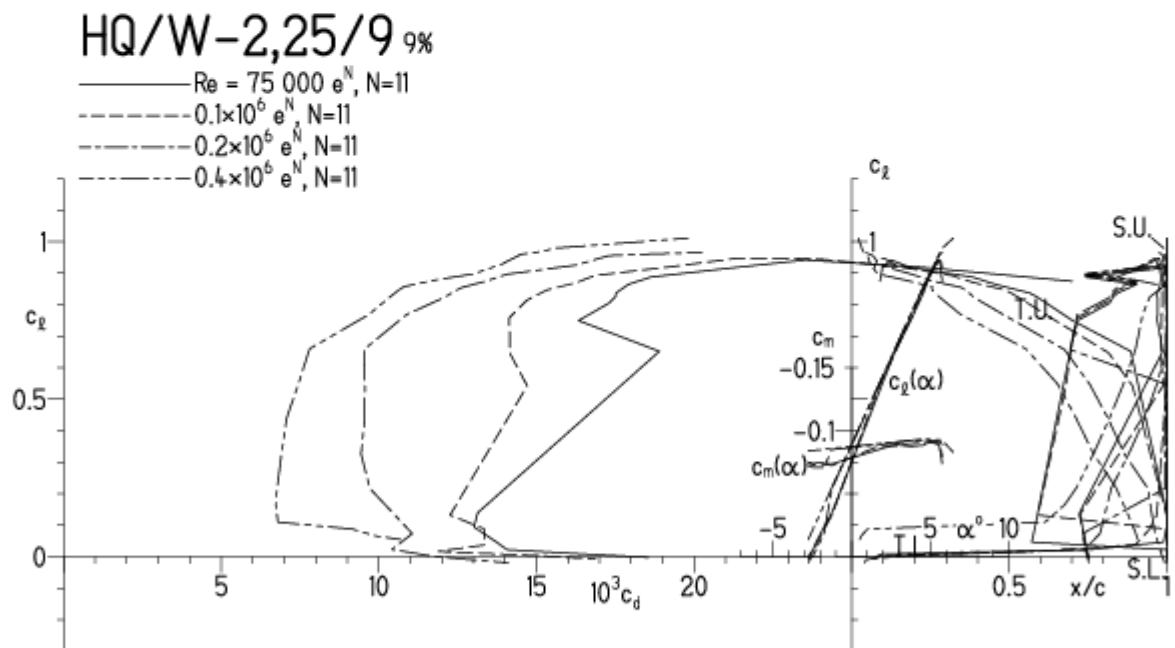


HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



HQ/W-2,25/9, N=9

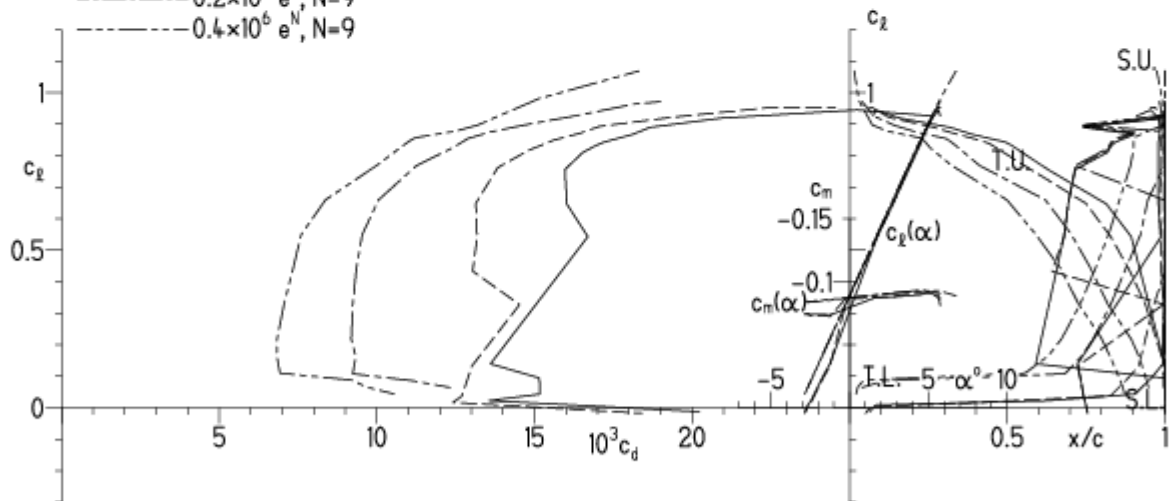
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

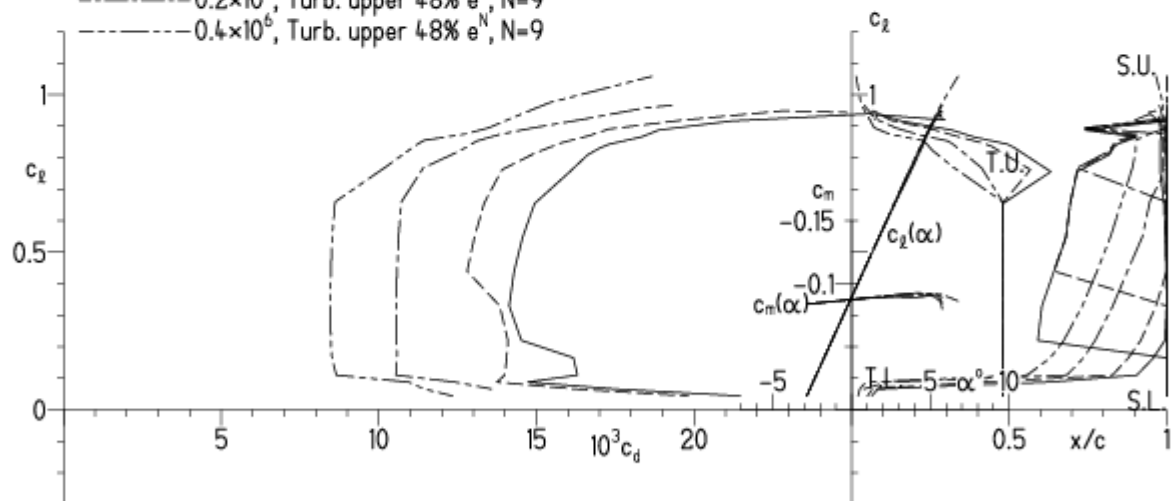
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38

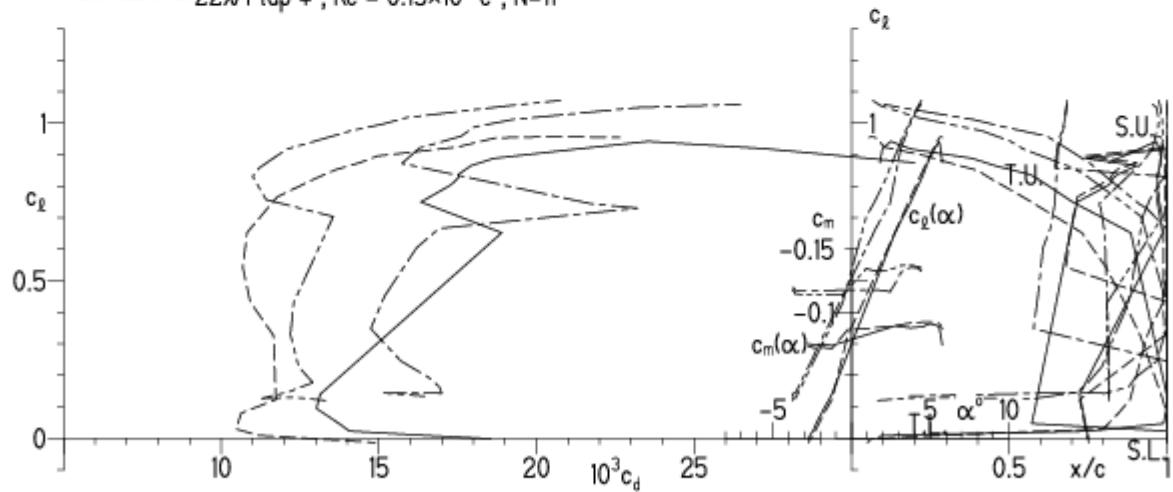


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- - - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17

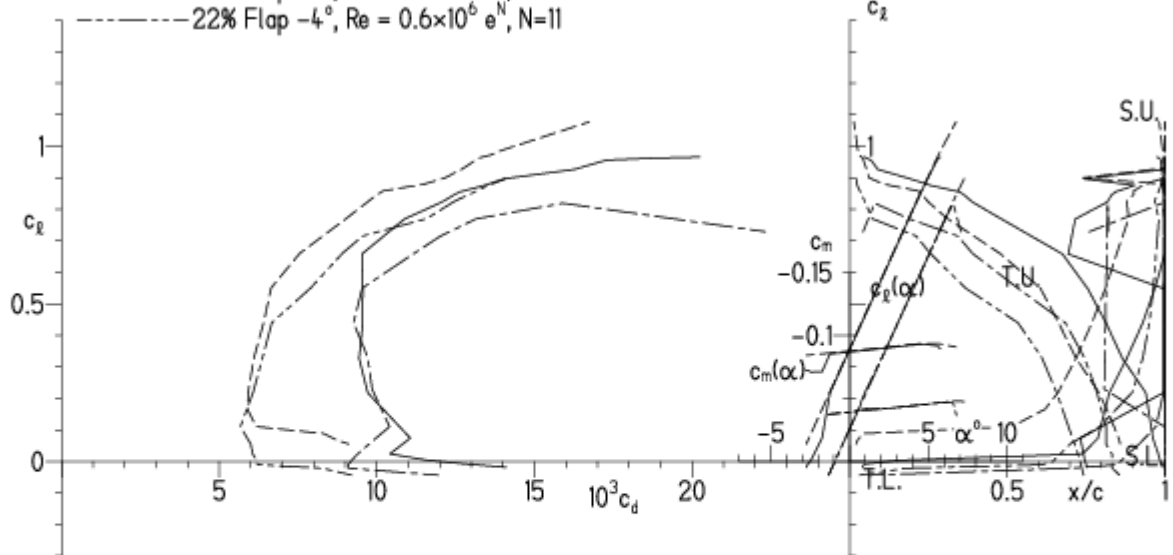


EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- Re = 0.2×10^6 e^N, N=11
- - - Re = 0.6×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.2×10^6 e^N, N=11
- · - · 22% Flap -4°, Re = 0.6×10^6 e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11

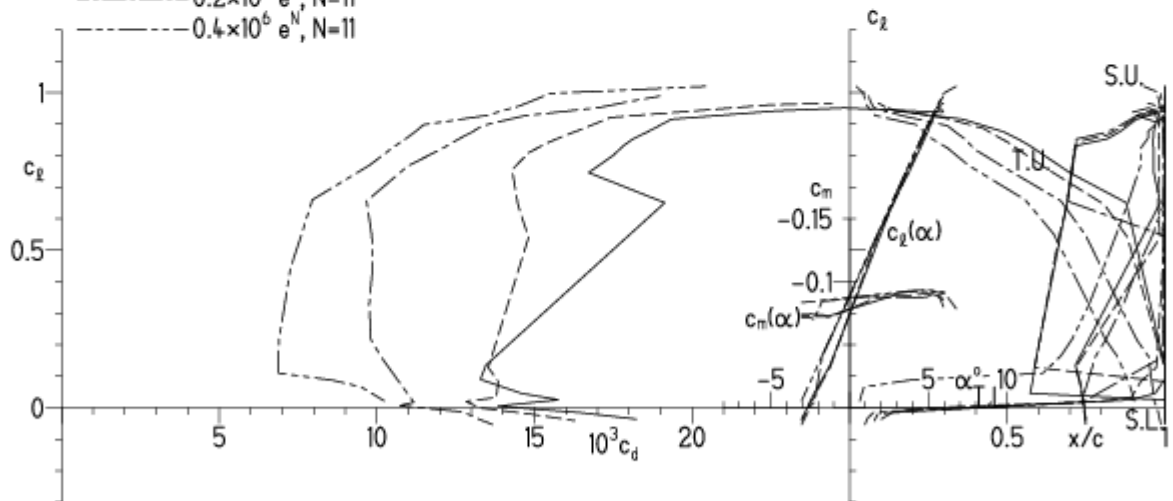
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

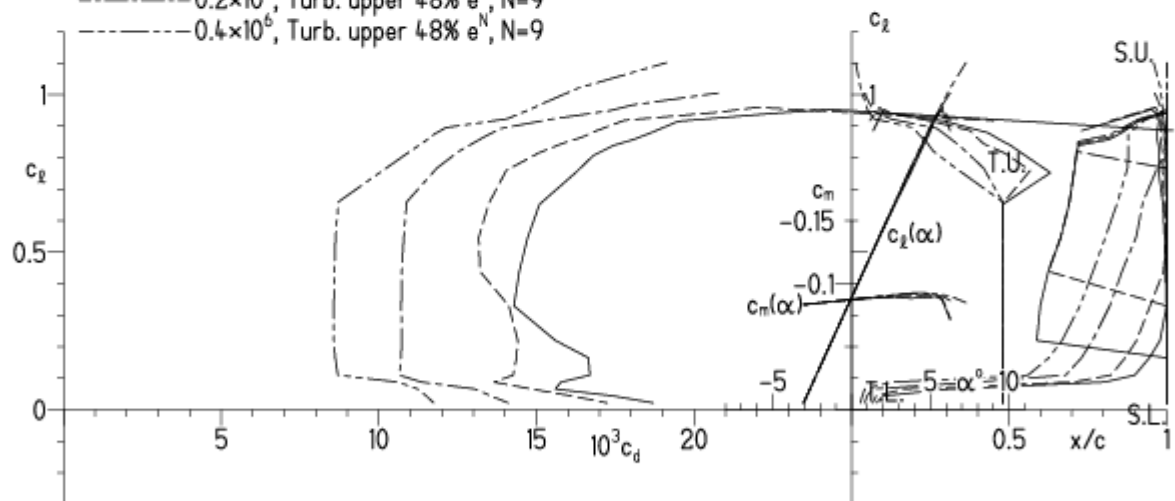
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

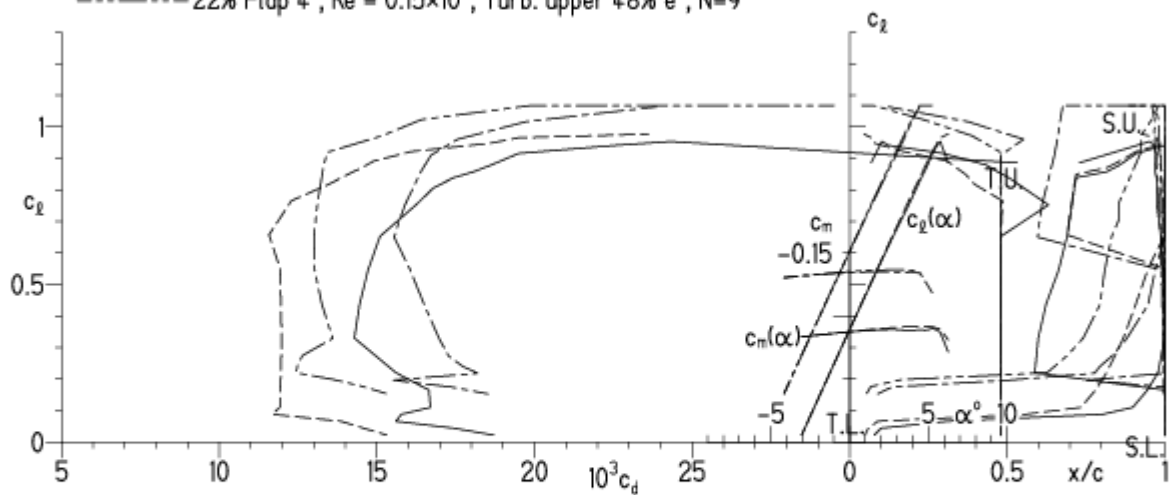


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$

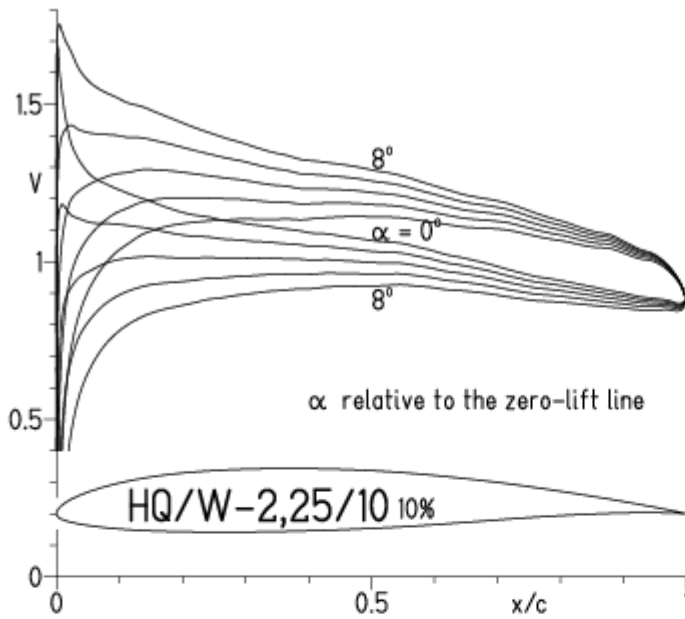


- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47

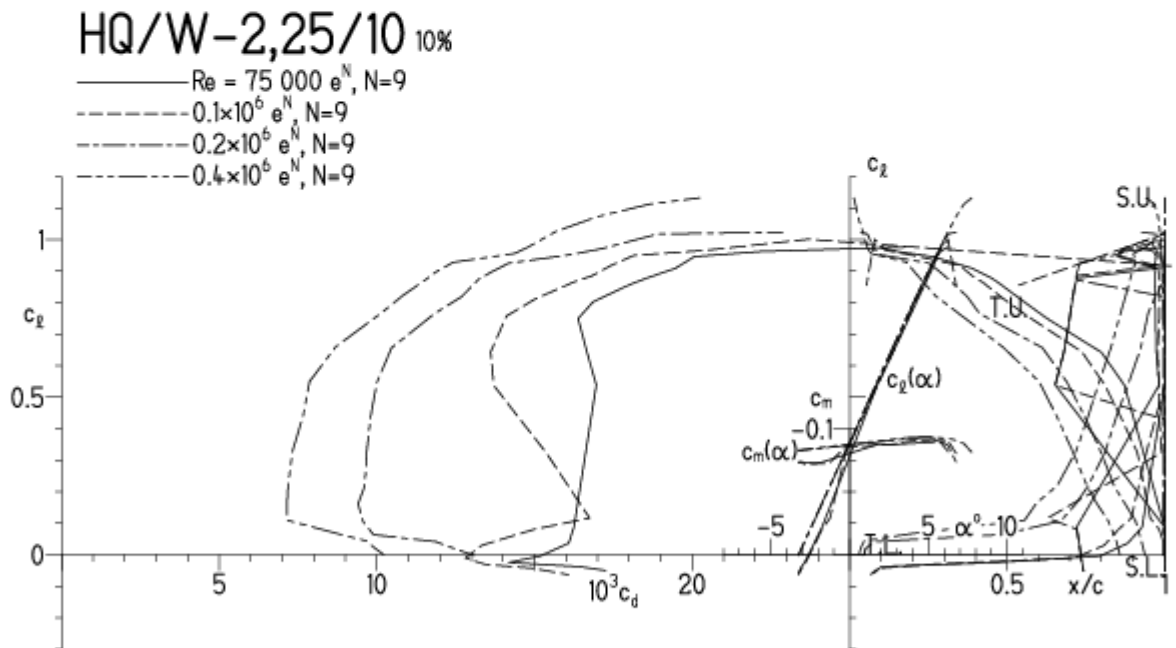


HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

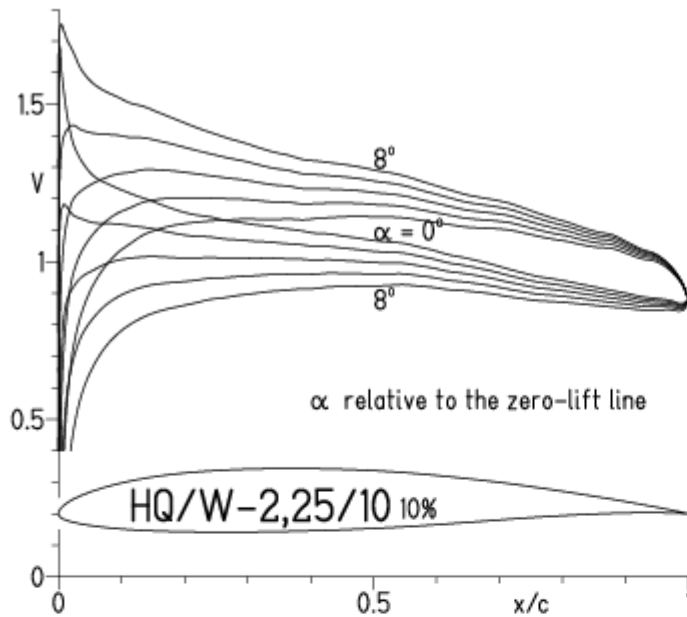


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53



HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

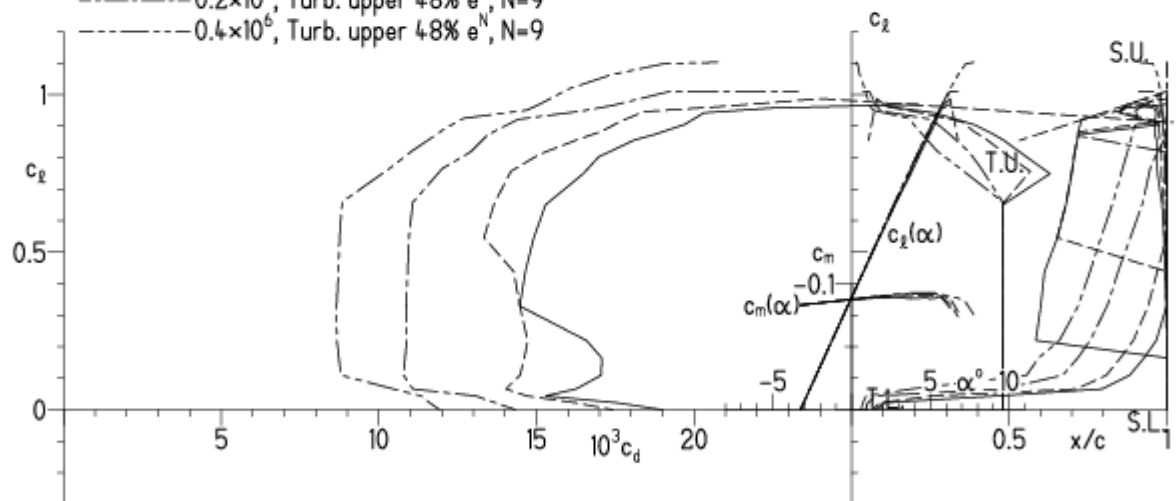
EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56

HQ/W-2,25/10 10%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

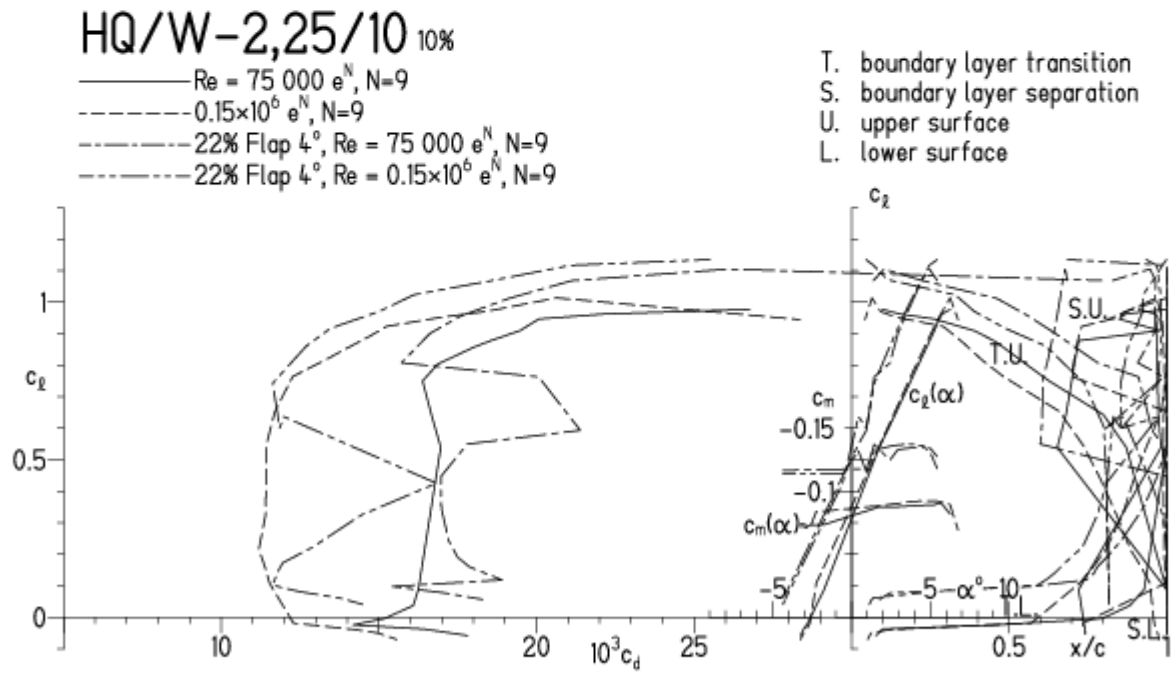


HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

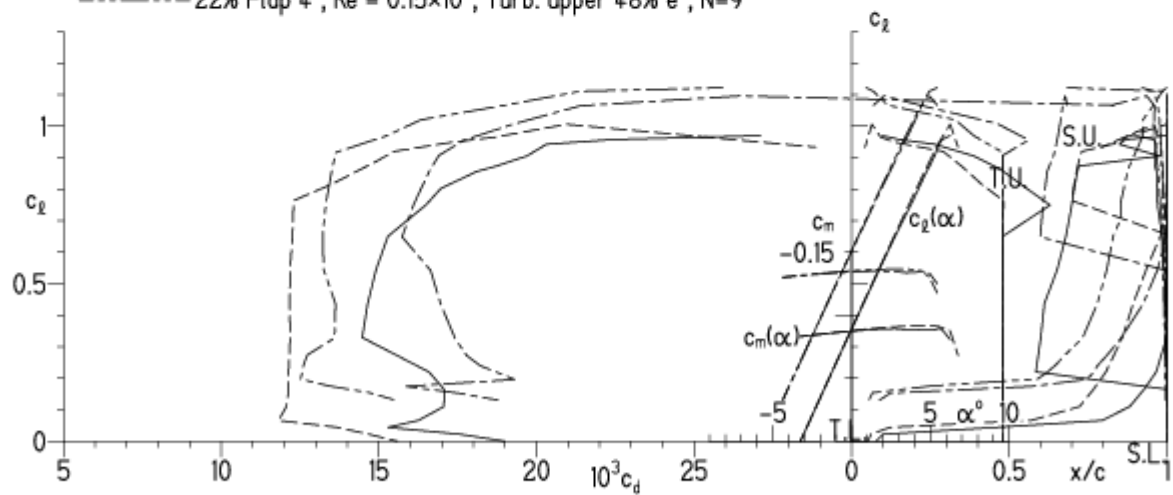


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23



EPPLER 2005 V. 8.5.07 RUN



HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

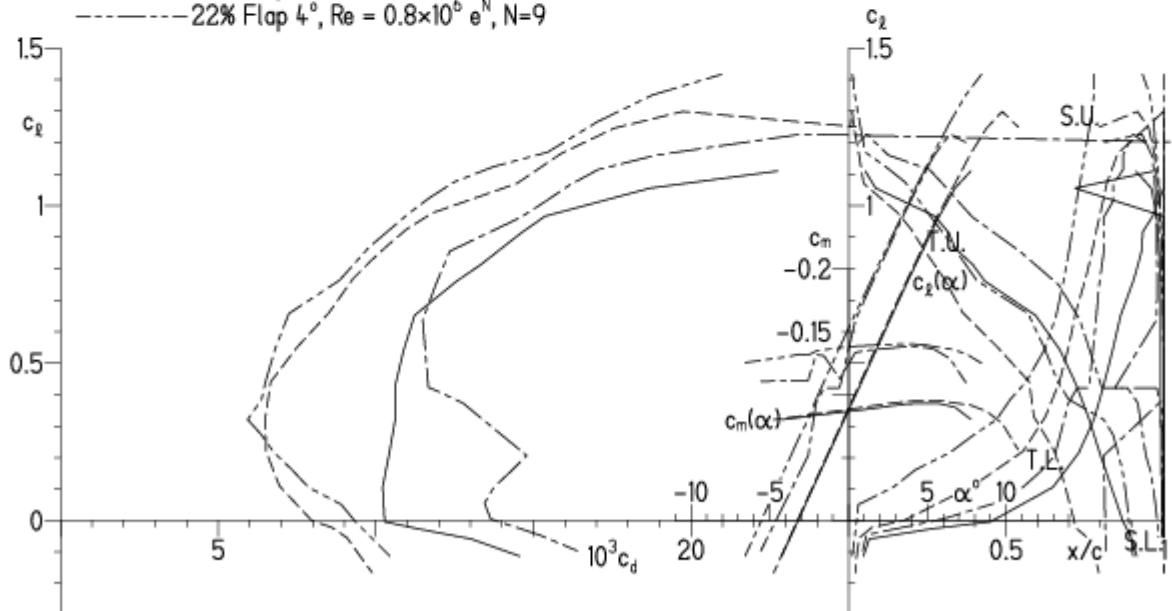


EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

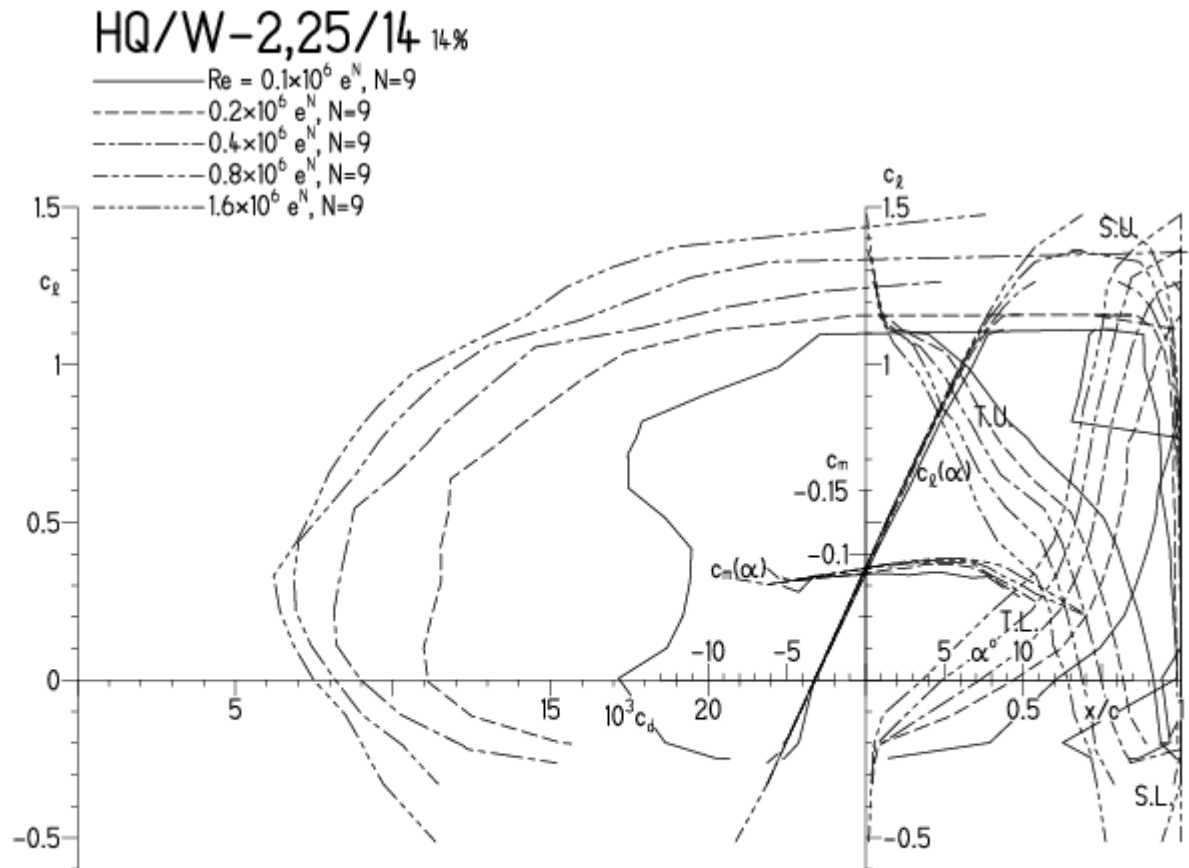


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

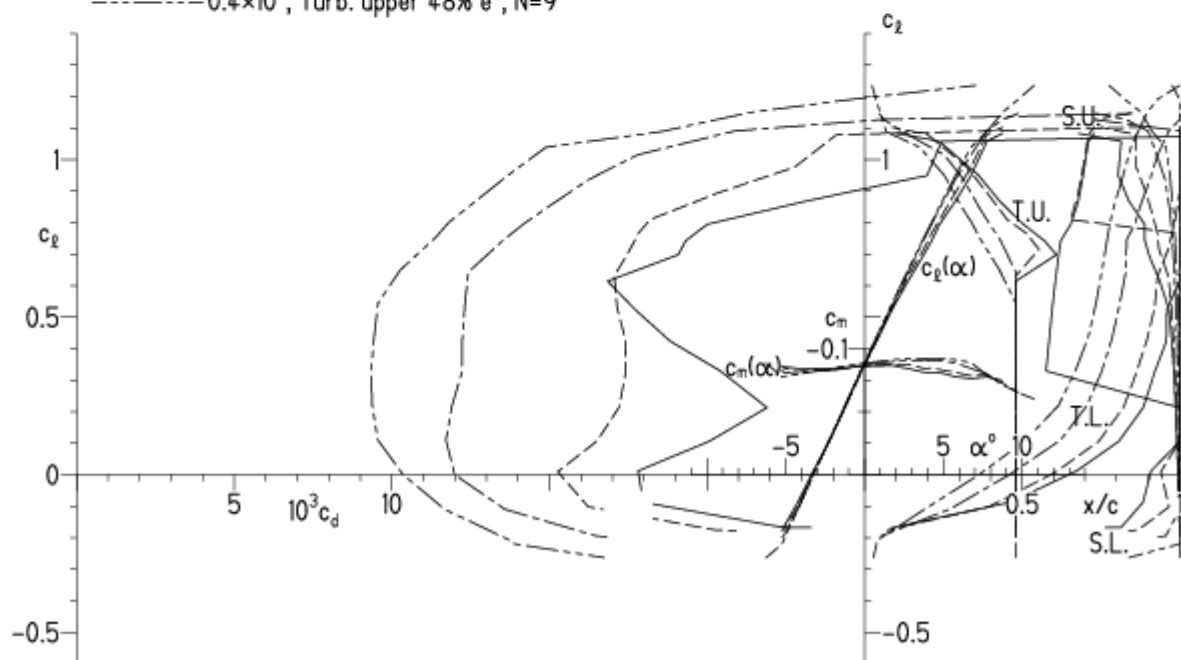
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

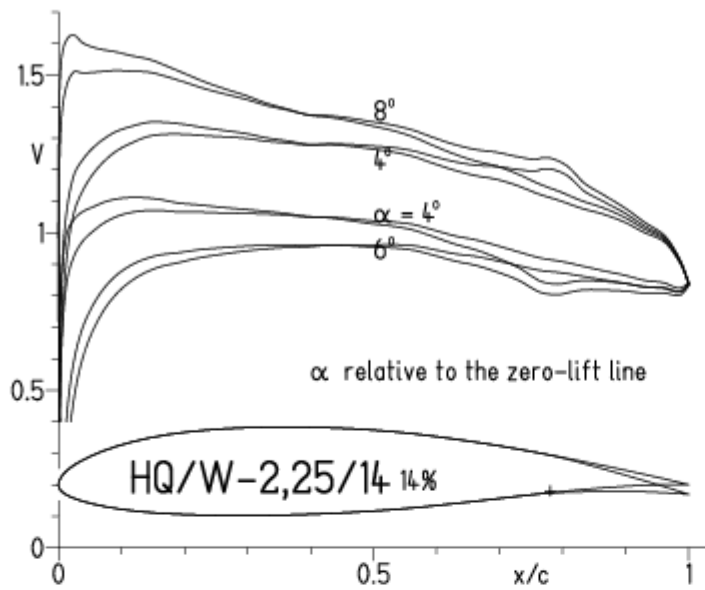
HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

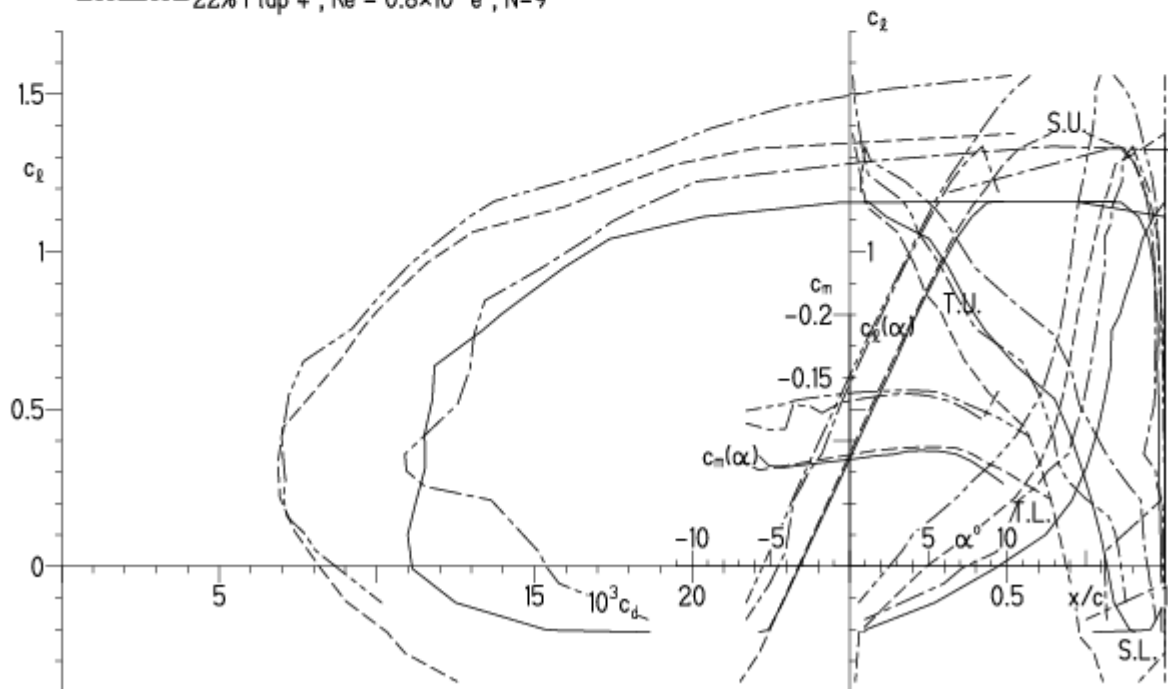


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51

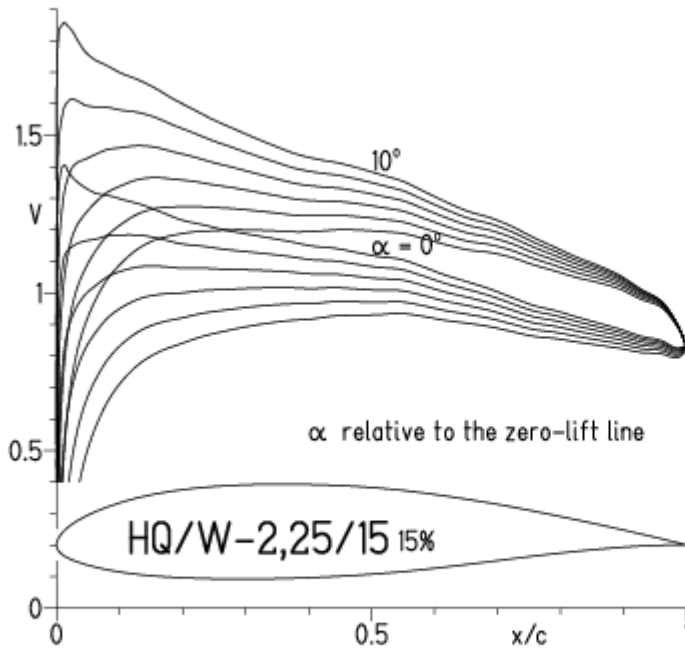


EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31

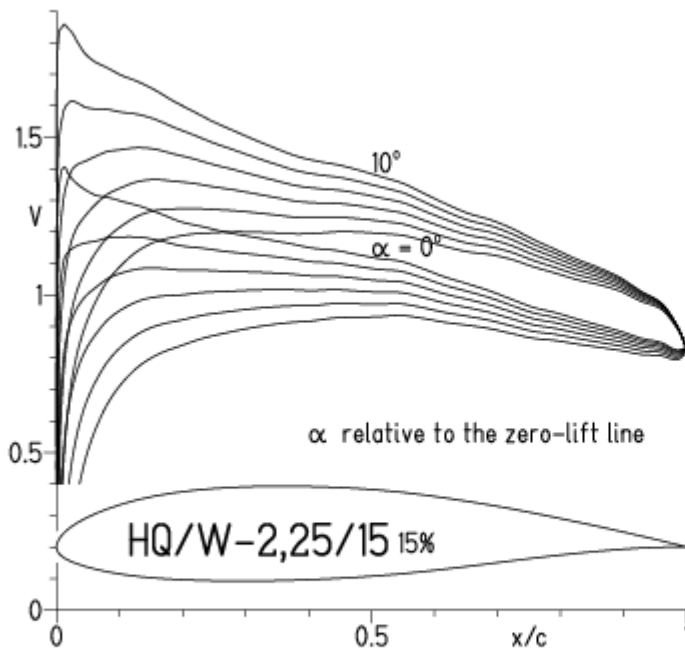


EPPLER 20

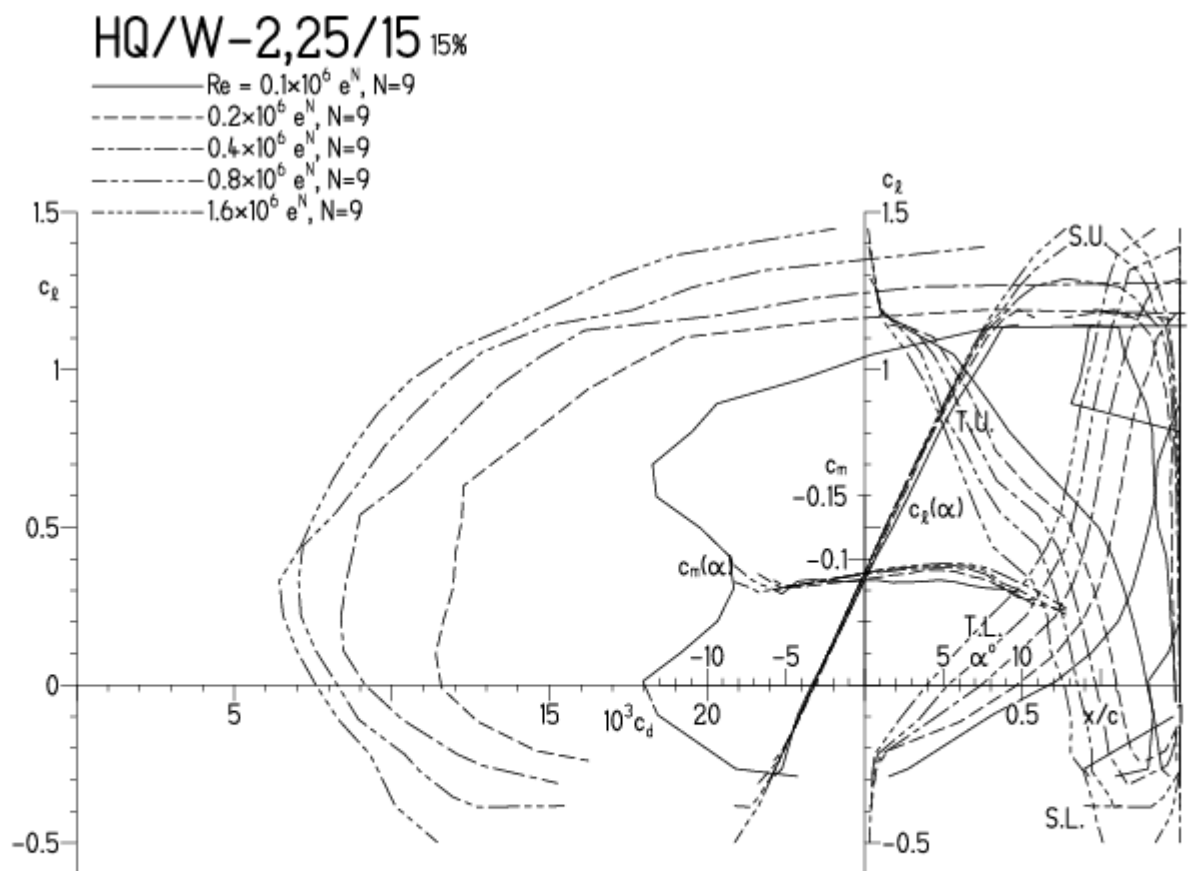


HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

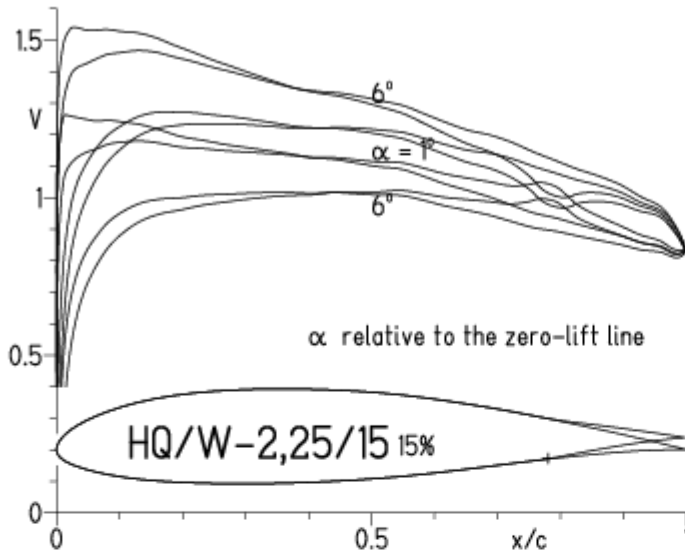


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04



EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200



HQ/W-2,25/16, N=9

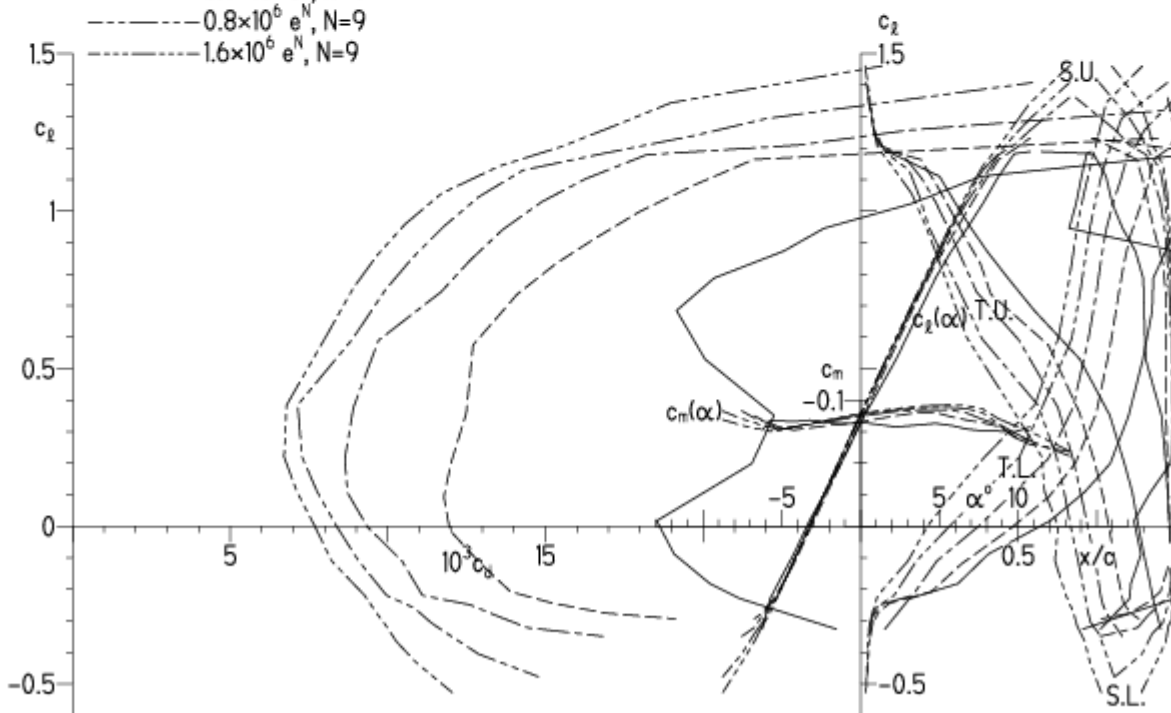
EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

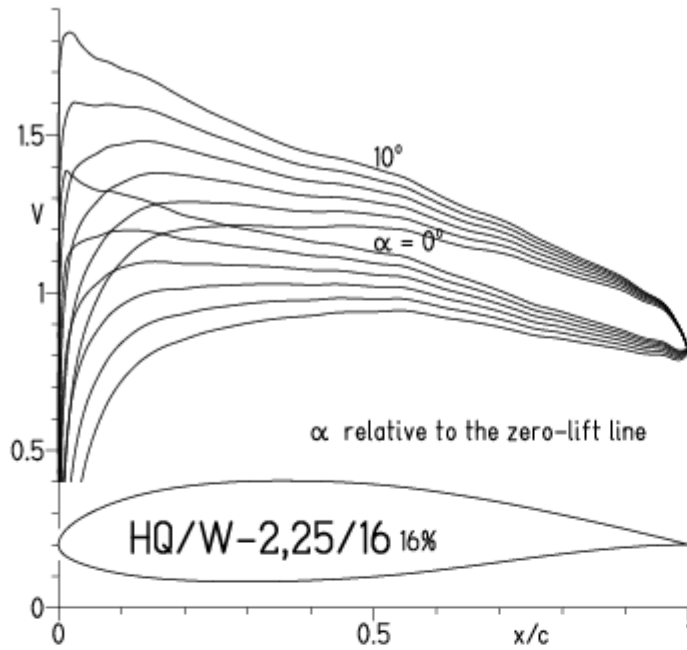
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



HQ/W-2,25/8, N=11

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:46



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- · - · $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8, N=9

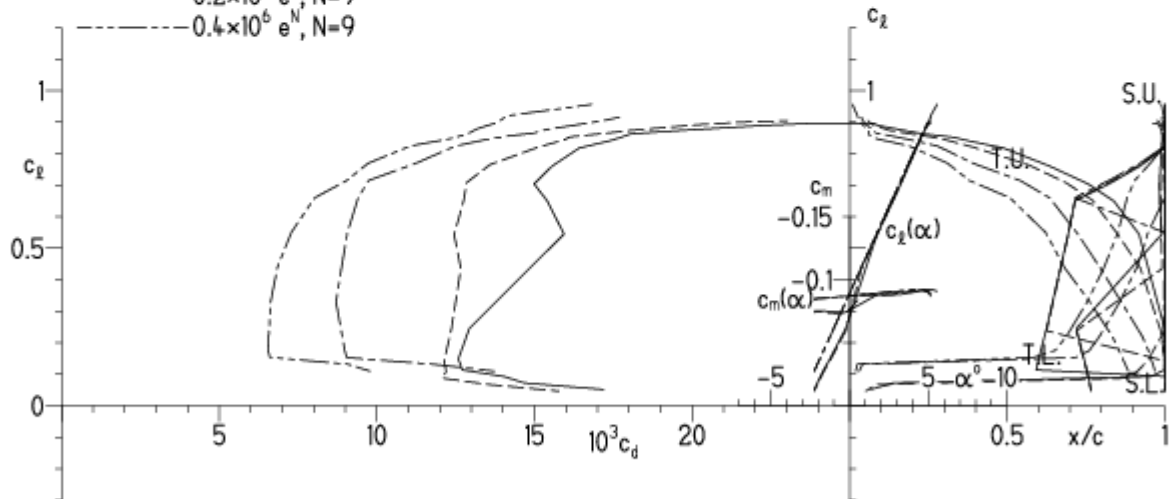
EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52



EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:52

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- · - · $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/8, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 1.3.11 18:57



EPPLER 2005 V. 8.5.07 RUN 1

HQ/W-2,25/8 8%

- $Re = 75\ 000$, Turb. upper 48% e^N , $N=9$
- 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/8, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:51

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:55



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11

HQ/W-2,25/8 8%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59



EPPLER 2005 V. 8.5.07 RUN 3.3.11 11:59

HQ/W-2,25/8 8%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15x10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15x10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm^2 erreichen damit nur ca. 30 – 35 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 3.3.11 12:23



EPPLER 2005 V. 8.5.07 RUN 3.3.11 1



HQ/W-2,25/8,5, N=11

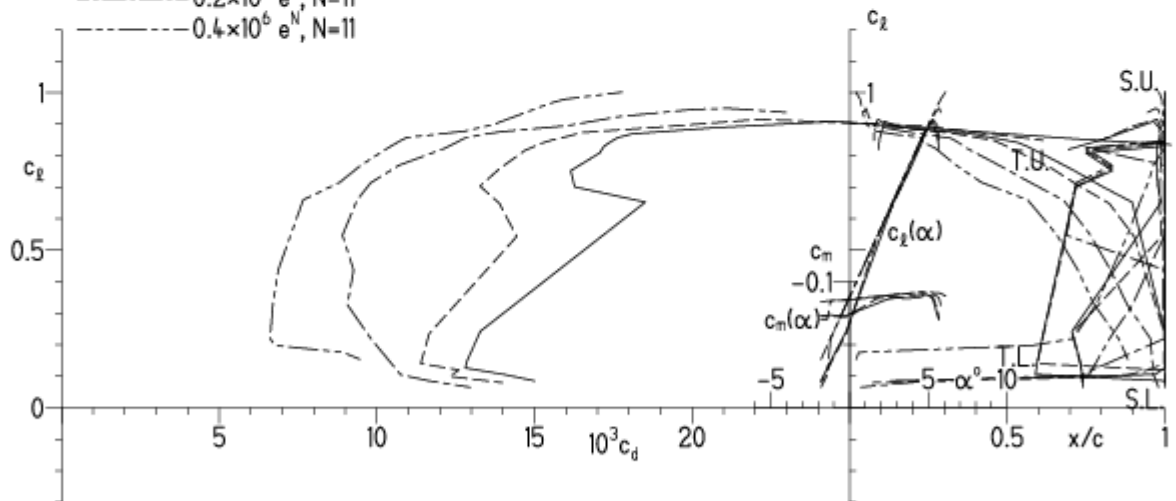
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:07



EPPLER 2005 V

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/8,5, N=9

EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:33



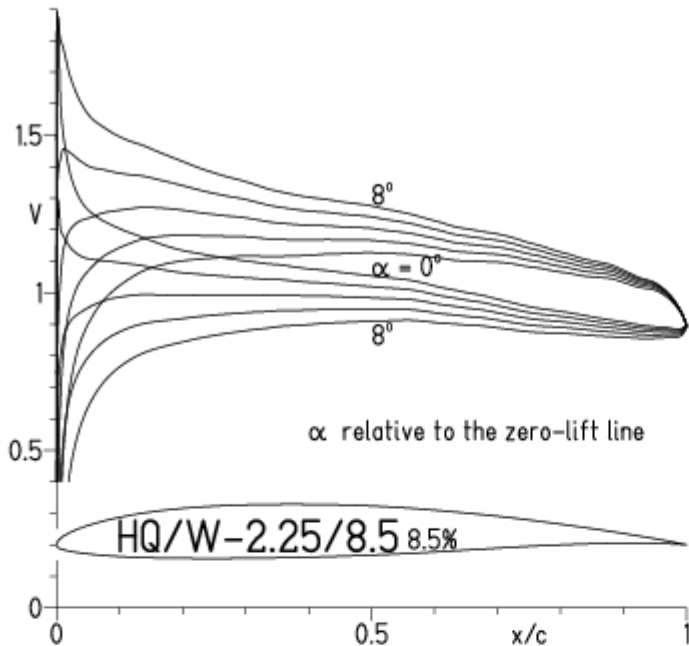
EPPLER 2005 V. 8.5.07 RUN 24.3.11 13:

HQ/W-2.25/8.5 8.5%



HQ/W-2,25/8,5, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

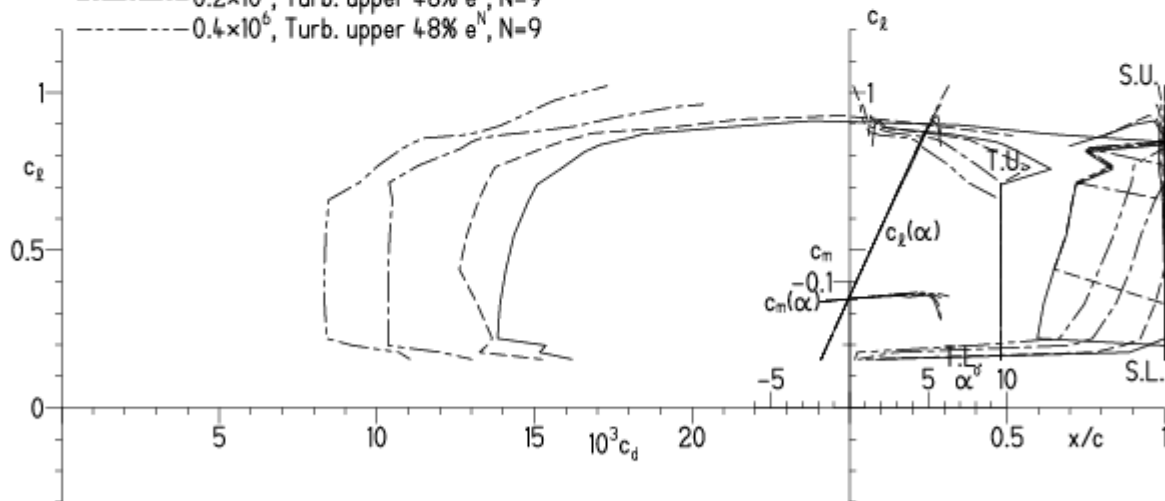
EPPLER 2005 V. 8.5.07 RUN 24.3.11 17:31



EPPLER 2005 V.

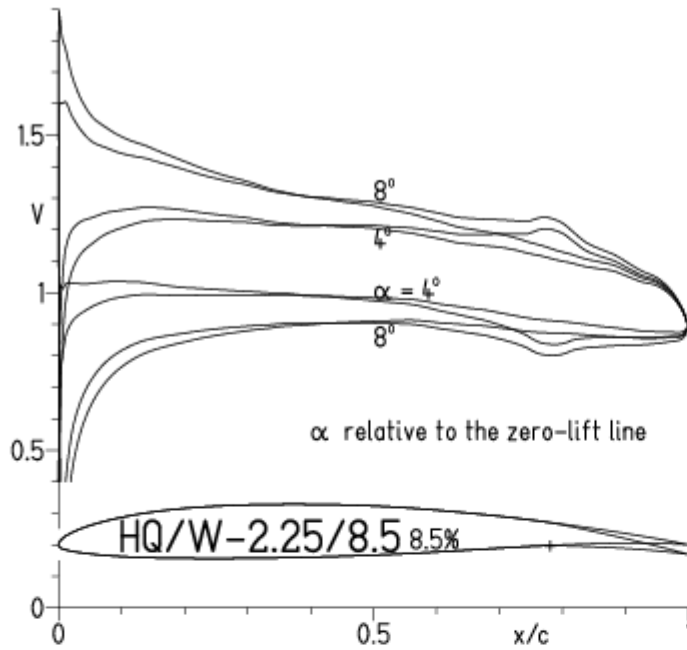
HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.1×10⁶, Turb. upper 48% e^N, N=9
- · - 0.2×10⁶, Turb. upper 48% e^N, N=9
- - - 0.4×10⁶, Turb. upper 48% e^N, N=9



HQ/W-2,25/8,5, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:08

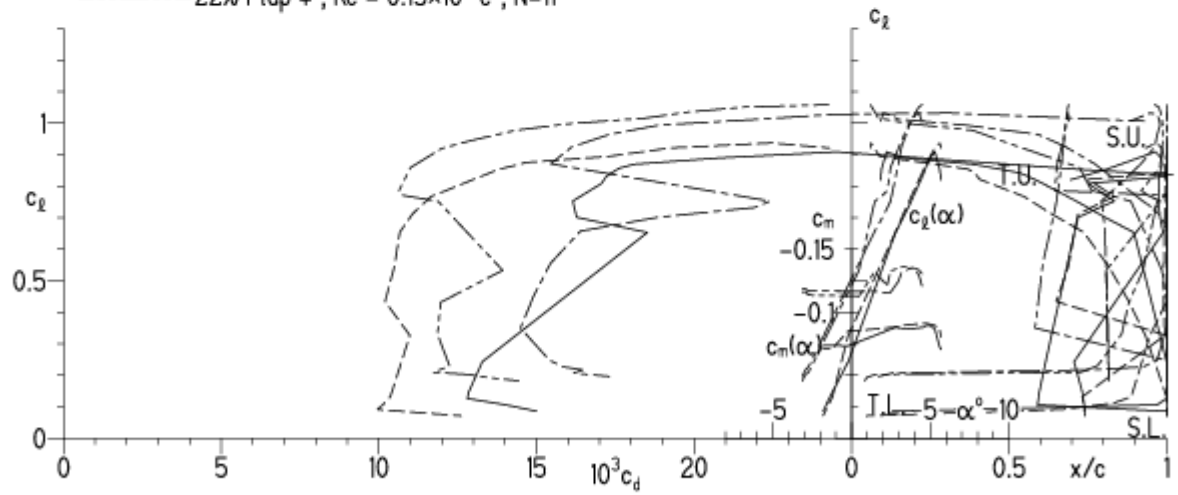


EPPLER 2005 V. 8.5.

HQ/W-2.25/8.5 8.5%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:12



EPPLER 2005 V.

HQ/W-2.25/8.5 8.5%

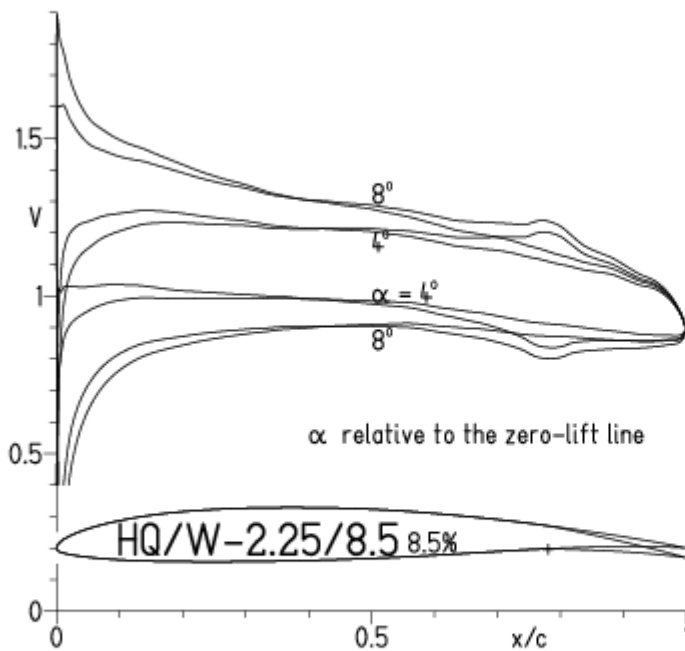
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · - 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 18:16

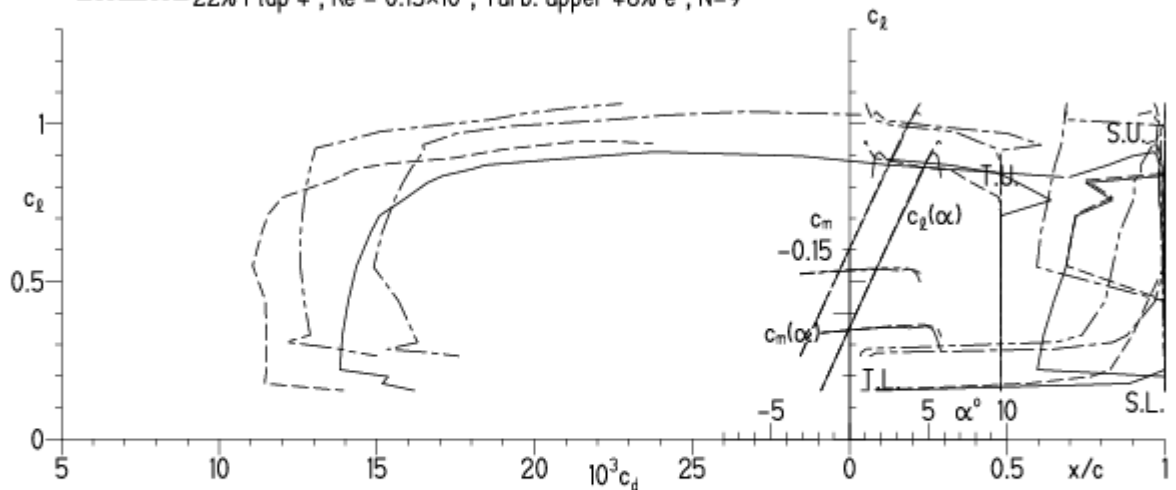


EPPLER 2005 V. 8.5.07 RUN 24.3.11 1

HQ/W-2.25/8.5 8.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/8,5, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



EPPLER 2005 V. 8.5.07 RUN 24.3.11 19:09



HQ/W-2,25/9, N=11

EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50



EPPLER 2005 V. 8.5.07 RUN 7.3.11 17:50

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.1 \times 10^6 e^N, N=11$
- · - $0.2 \times 10^6 e^N, N=11$
- - - $0.4 \times 10^6 e^N, N=11$



HQ/W-2,25/9, N=9

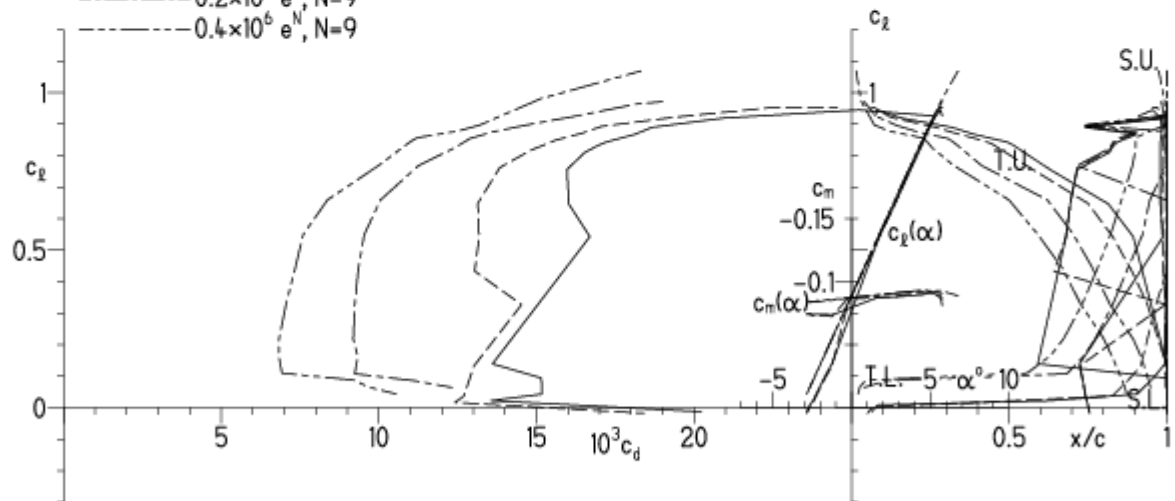
EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:08



EPPLER 2005 V. 8.

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.1 \times 10^6 e^N, N=9$
- · - $0.2 \times 10^6 e^N, N=9$
- - - $0.4 \times 10^6 e^N, N=9$



HQ/W-2,25/9, N=9, Turbulatoreffekt (optimal beim Maximum der Wölbung)

EPPLER 2005 V. 8.5.07 RUN 7.3.11 18:12



EPPLER 2005 V. 8.5.07 RUN 7

HQ/W-2,25/9 9%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9, N=11, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:38

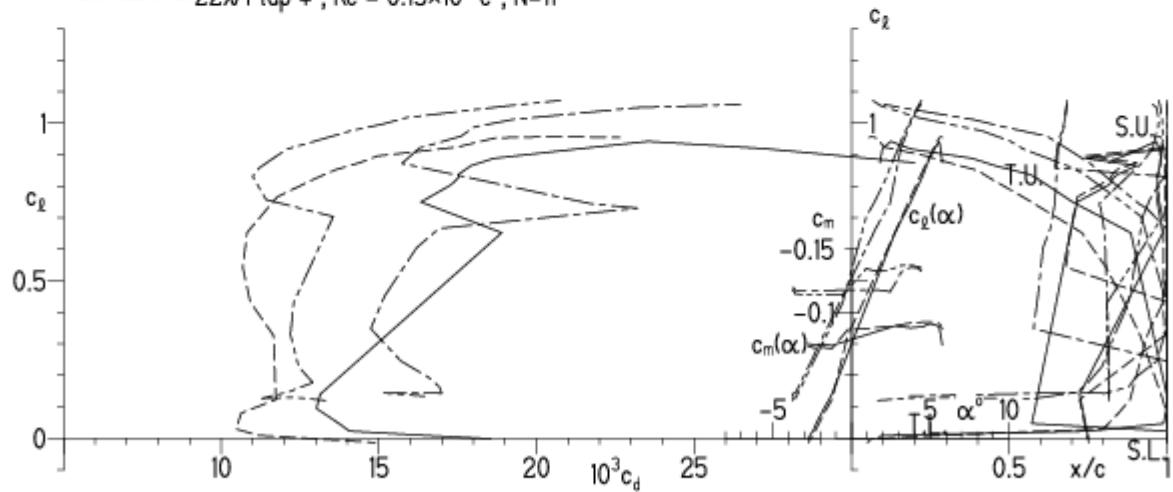


EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:3

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=11$
- - - $0.15 \times 10^6 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=11$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=11$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=9, mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:48



EPPLER 2005 V. 8.5.07 RUN 8.3.1

HQ/W-2,25/9 9%

- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · - 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54



EPPLER 2005 V. 8.5.07 RUN 8.3.11 15:54

HQ/W-2,25/9%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9, N=11 mit -4° Wölbklappenausschlag
 (F3J-Modelle mit 30 g/dm² erreichen damit ca. 50 m/s Höchstgeschwindigkeit)

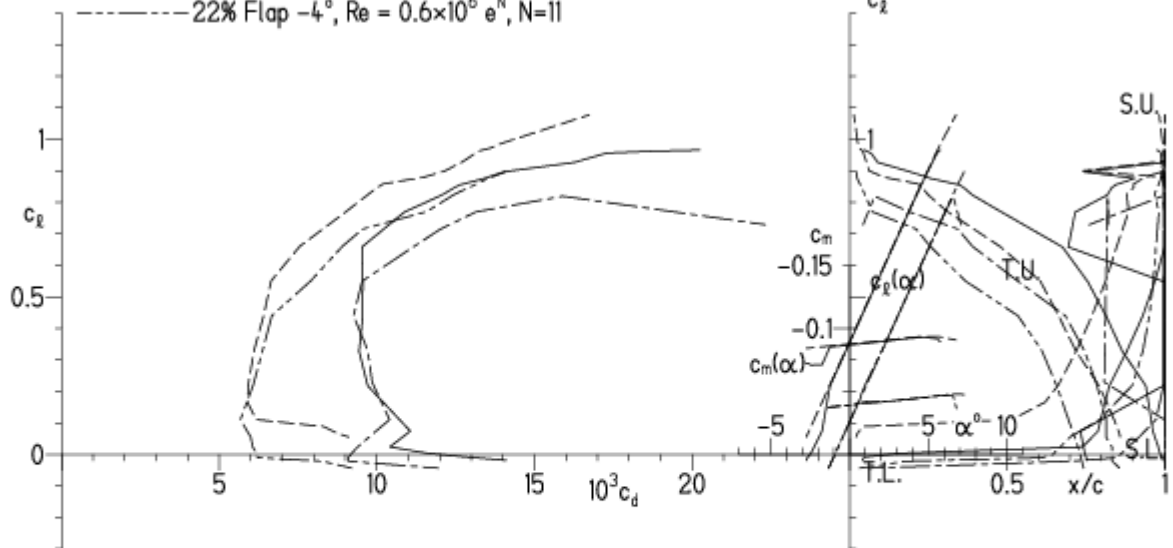
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:17



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:02

HQ/W-2,25/9 9%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.2 \times 10^6 e^N, N=11$
- · - · 22% Flap -4°, $Re = 0.6 \times 10^6 e^N, N=11$

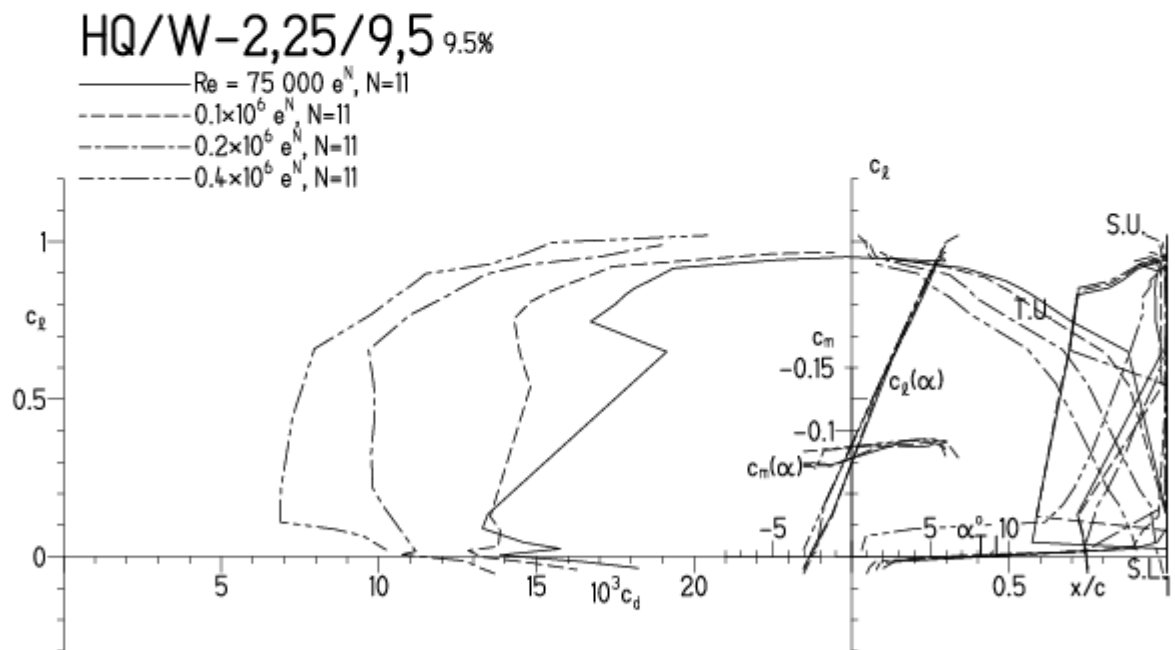


HQ/W-2,25/9,5, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:33



HQ/W-2,25/9,5, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:43



EPPLER 2005 V. 8.5.07 RUN 8.3.

HQ/W-2,25/9,5 9.5%



HQ/W-2,25/9,5, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

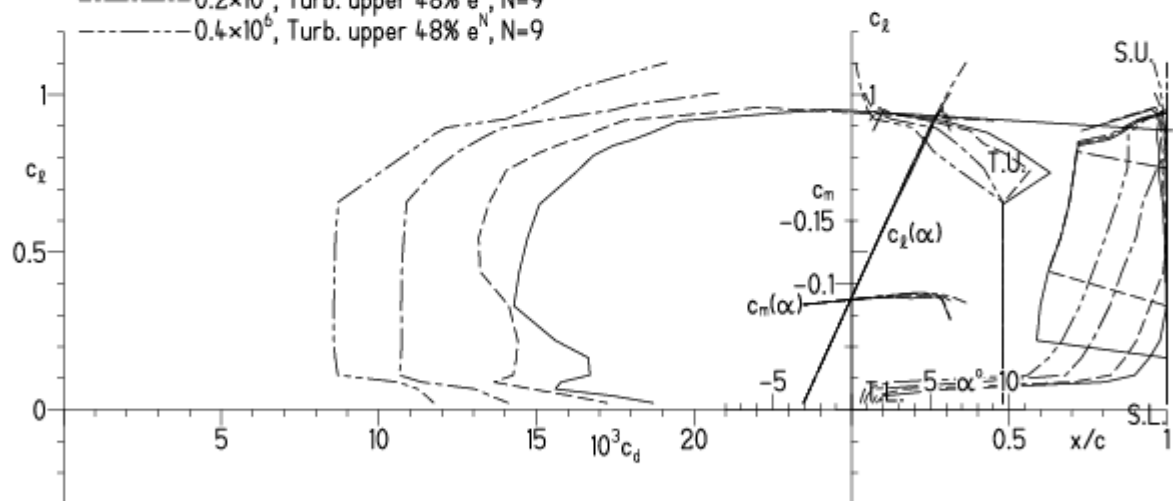
EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:46



EPPLER 2005 V. 8.5.07 RUN 8.3.11 16:

HQ/W-2,25/9,5 9.5%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQ/W-2,25/9,5, N=11 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

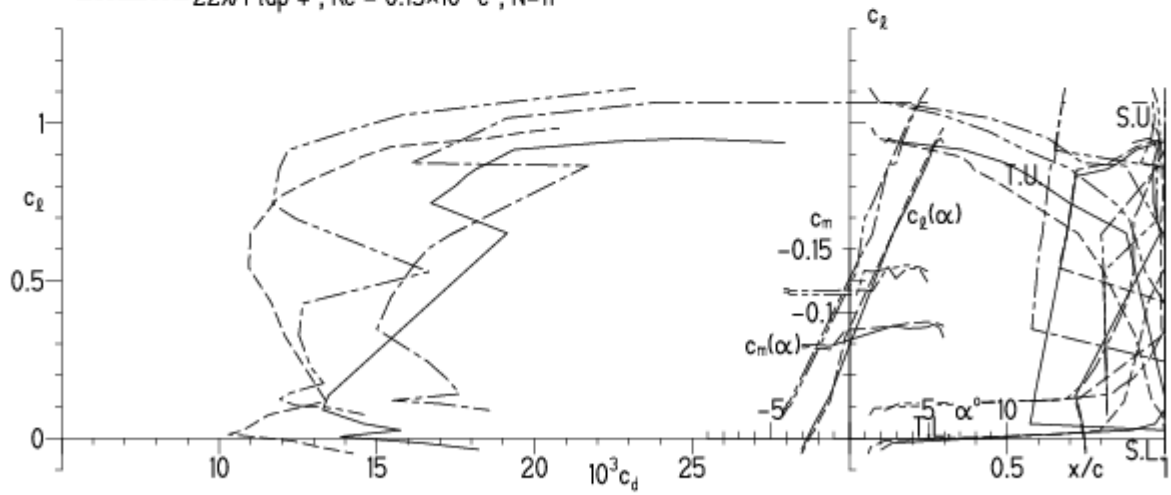


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:07

HQ/W-2,25/9,5 9.5%

- Re = 75 000 e^N, N=11
- - - 0.15 × 10⁶ e^N, N=11
- · - 22% Flap 4°, Re = 75 000 e^N, N=11
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=11

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:12



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/9,5 9.5%

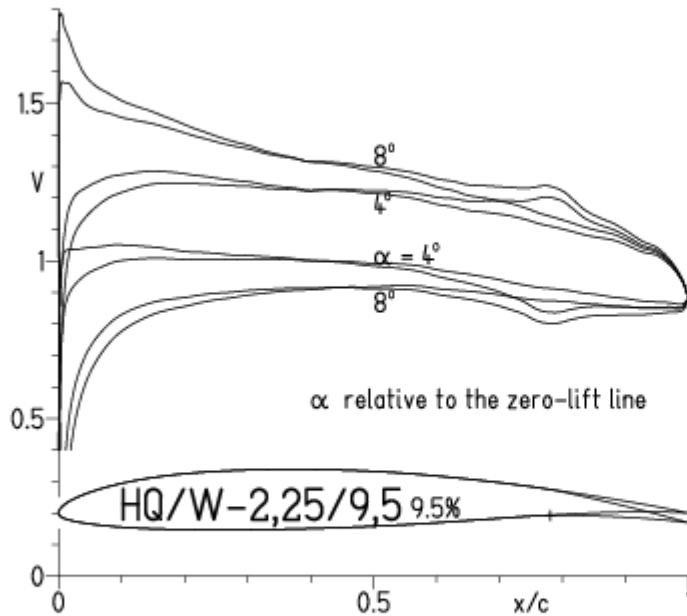
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 75\,000 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt
 (Verbesserungen für niedrige Geschwindigkeiten und Profiltiefen an Flügelenden)

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

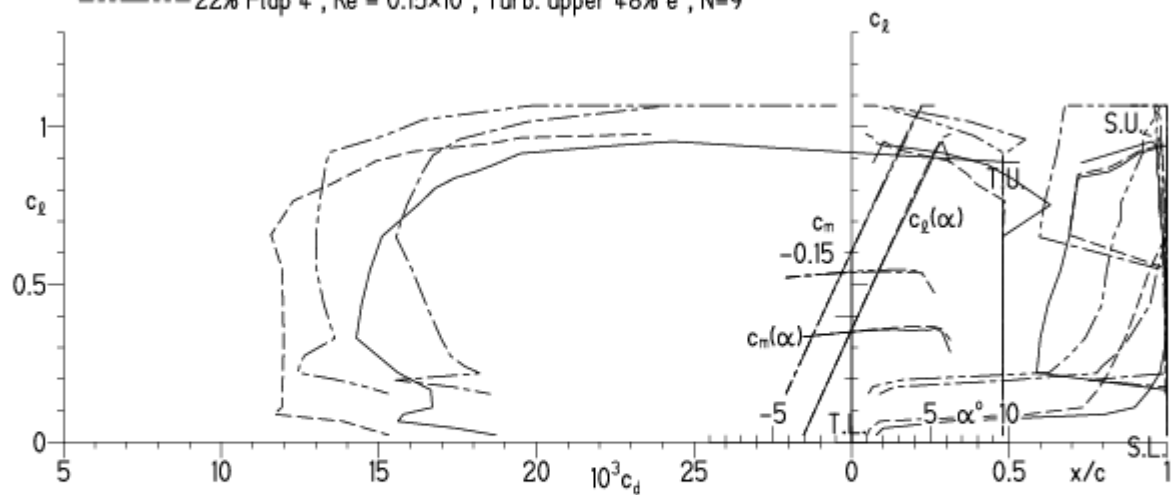


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:14

HQ/W-2,25/9,5 9.5%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/9,5, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:31



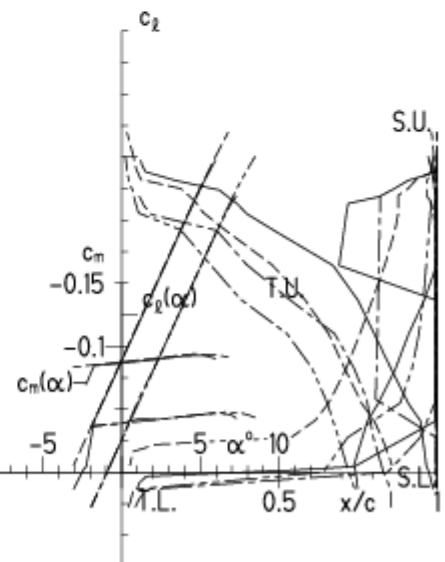
EPPLER 2005 V.

HQ/W-2,25/9,5 9.5%

- $Re = 0.2 \times 10^6 e^N, N=11$
- - - $0.6 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.2 \times 10^6 e^N, N=11$
- · - · - 22% Flap $-4^\circ, Re = 0.6 \times 10^6 e^N, N=11$



- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:47



HQ/W-2,25/10, N=9

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

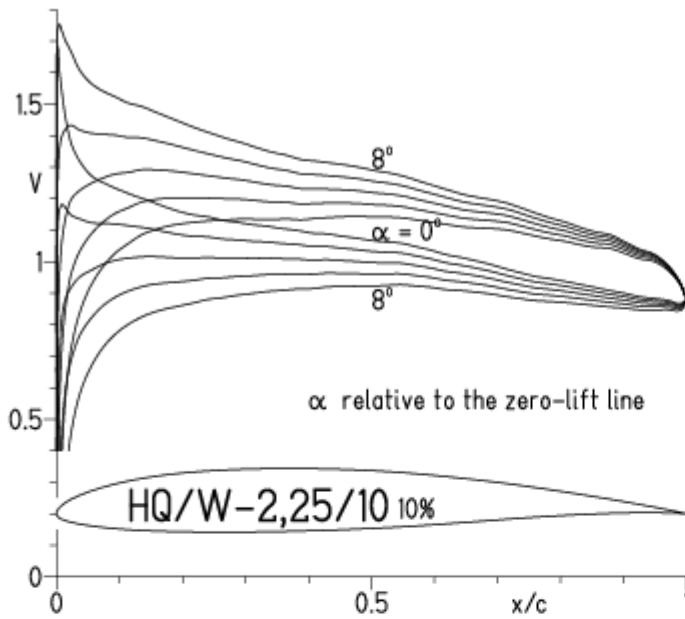


EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:53

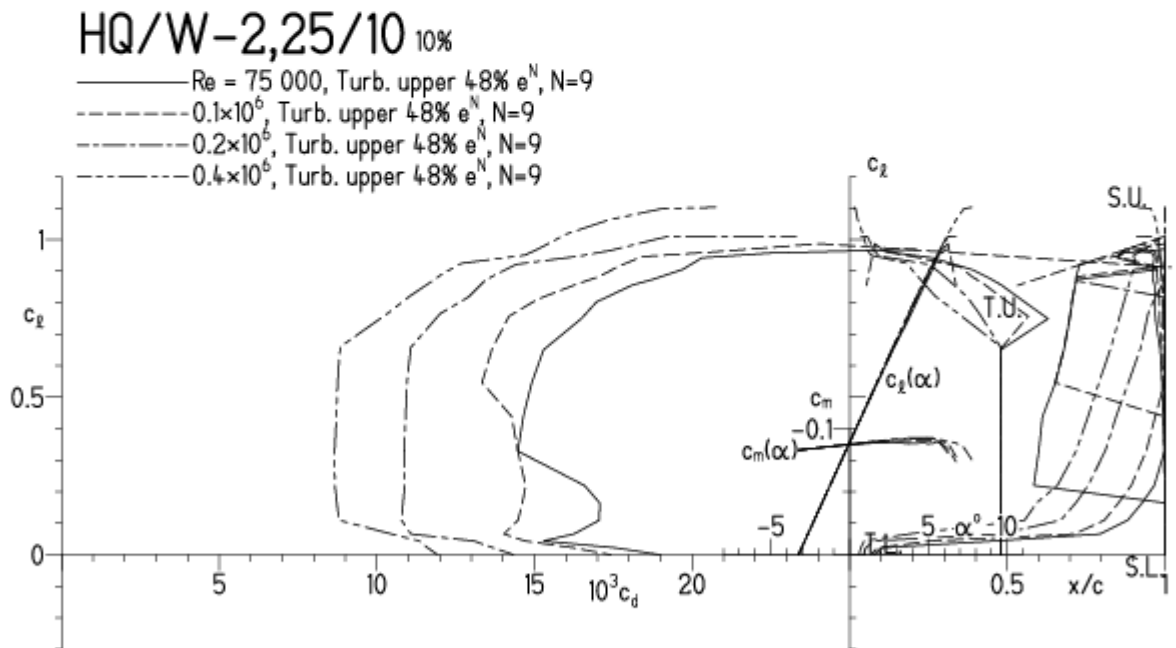


HQ/W-2,25/10, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



EPPLER 2005 V. 8.5.07 RUN 8.3.11 17:56



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

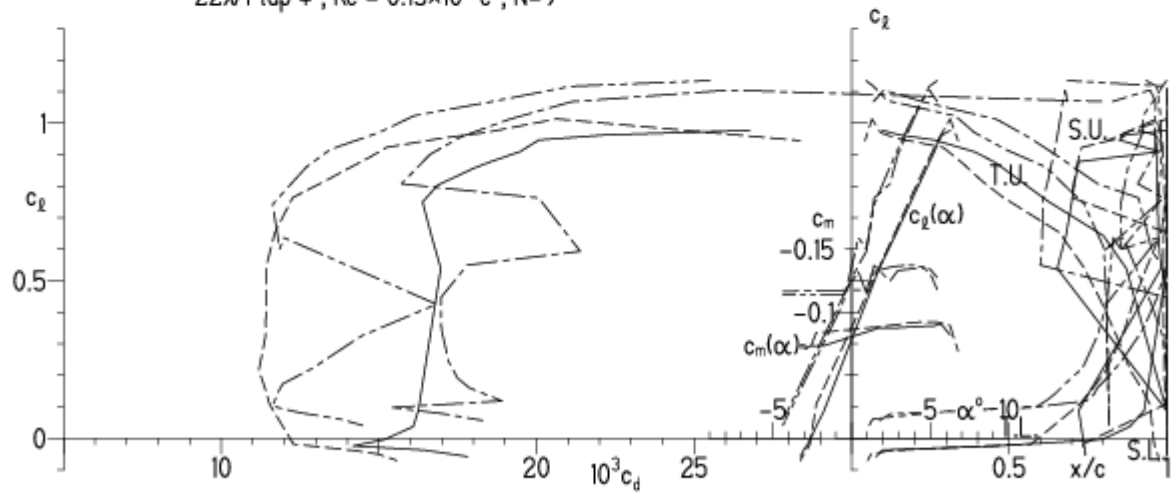


EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:16

HQ/W-2,25/10 10%

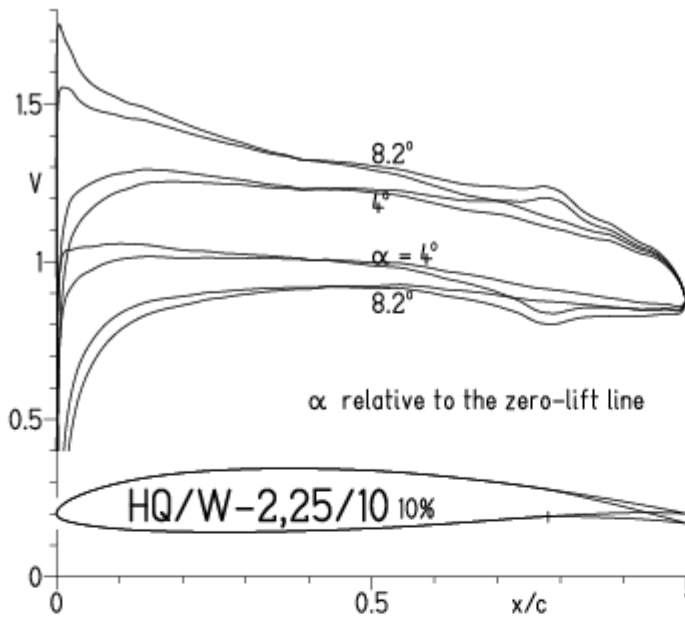
- $Re = 75\,000 e^N, N=9$
- - - $0.15 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 75\,000 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.15 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit +4° Wölbklappenausschlag, Turbulatoreffekt

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:32

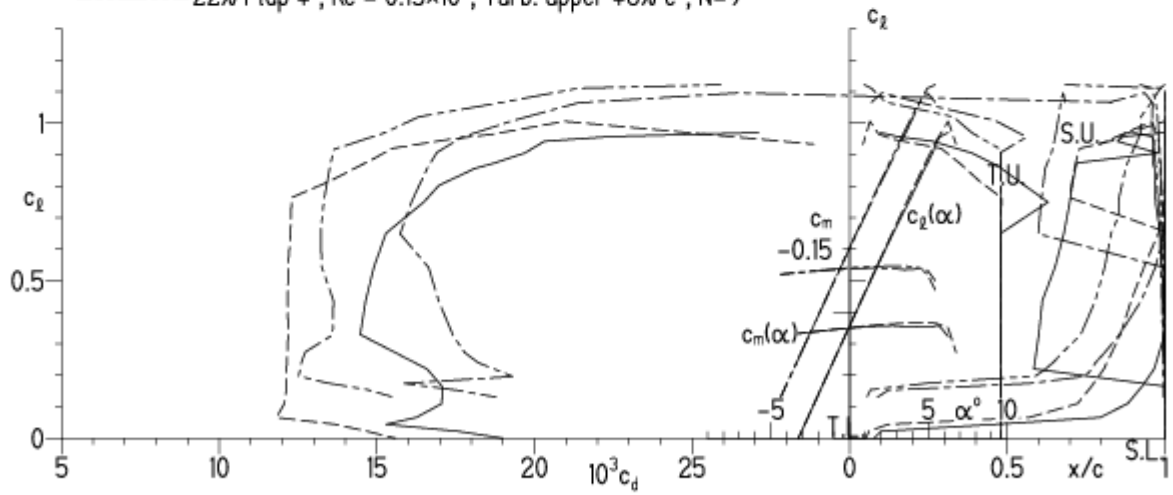


EPPLER 2005 V. 8.5.07 RUN 8.3

HQ/W-2,25/10 10%

- Re = 75 000, Turb. upper 48% e^N, N=9
- - - 0.15×10⁶, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 75 000, Turb. upper 48% e^N, N=9
- · - 22% Flap 4°, Re = 0.15×10⁶, Turb. upper 48% e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 8.3.11 18:23

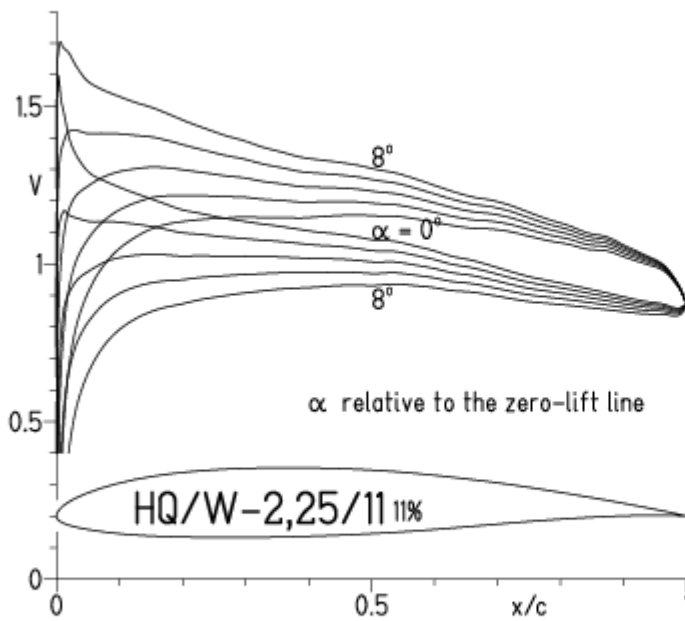


EPPLER 2005 V. 8.5.07 RUN

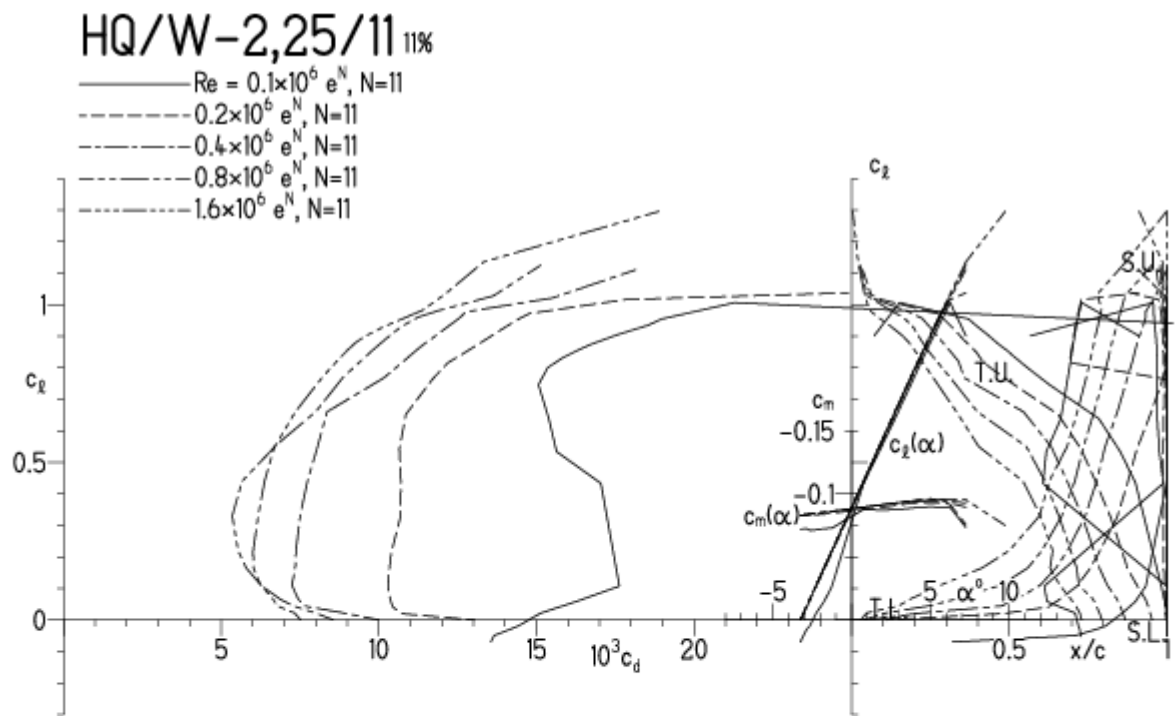


HQ/W-2,25/11, N=11

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:



HQQ/W-2,25/11, N=9

EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42

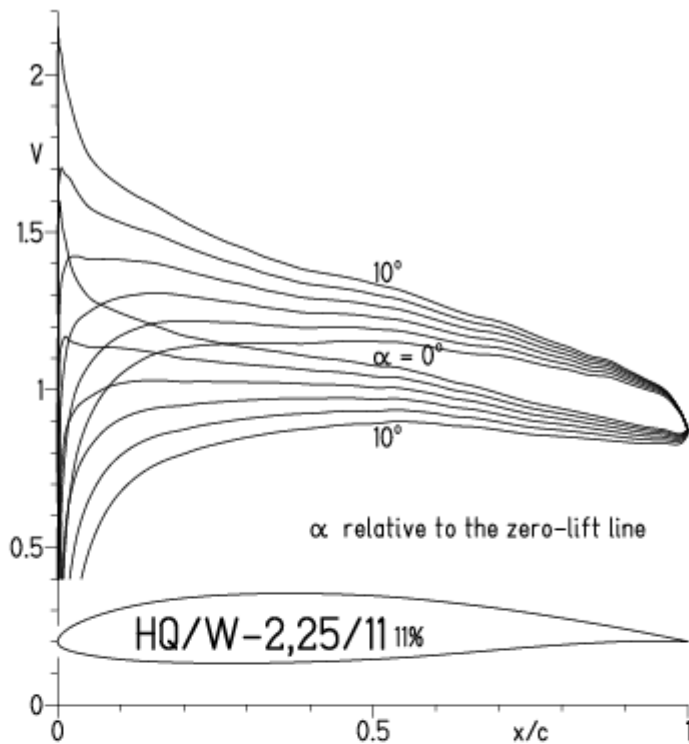


EPPLER 2005 V. 8.5.07 RUN 15.12.23 12:42



HQ/W-2,25/11, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16



EPPLER 2005 V. 8.5.07 RUN 15.12.23 13:16

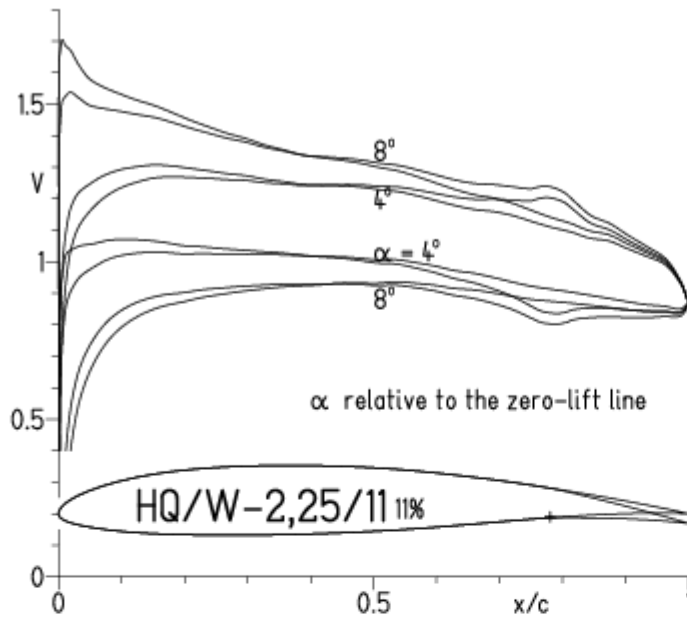
HQ/W-2,25/11 11%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/11, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17



EPPLER 2005 V. 8.5.07 RUN 14.12.23 17:17

HQ/W-2,25/11 11%

- Re = 75 000 e^N, N=9
- - - 0.15 × 10⁶ e^N, N=9
- · - 22% Flap 4°, Re = 75 000 e^N, N=9
- · - 22% Flap 4°, Re = 0.15 × 10⁶ e^N, N=9

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQ/W-2,25/10, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



EPPLER 2005 V. 8.5.07 RUN 14.12.23 16:52



HQ/W-2,25/12, N=11

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:32



EPPLER 2005 V. 8.5.07 RUN 18.12.23 1

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=11$
- - - $0.2 \times 10^6 e^N, N=11$
- · - $0.4 \times 10^6 e^N, N=11$
- · - · $0.8 \times 10^6 e^N, N=11$
- · - · - $1.6 \times 10^6 e^N, N=11$



HQ/W-2,25/12, N=9

EPPLER 2005 V. 8.5.07 RUN 18.12.23 12:44



EPPLER 2005 V. 8.5

HQ/W-2,25/12 12%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/12, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02



EPPLER 2005 V. 8.5.07 RUN 18.12.23 13:02

HQ/W-2,25/12 12%

- $Re = 75\,000 e^N, N=9$
- - - 0.1×10^6 , Turb. upper 48% $e^N, N=9$
- · - 0.2×10^6 , Turb. upper 48% $e^N, N=9$
- - - 0.4×10^6 , Turb. upper 48% $e^N, N=9$



HQW-2,25/12, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:47

HQ/W-2,25/12 12%

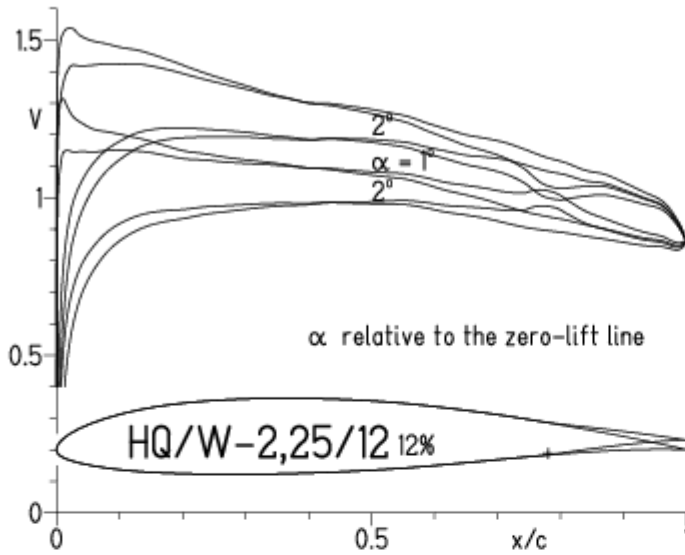
- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/12, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



EPPLER 2005 V. 8.5.07 RUN 19.12.23 17:24



HQ/W-2,25/13, N=11

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:11



HQ/W-2,25/13, N=9

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:26

HQ/W-2,25/13 13%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/13, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35



EPPLER 2005 V. 8.5.07 RUN 20.12.23 17:35

HQ/W-2,25/13 13%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/13, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:11



EPPLER 2005 V.

HQ/W-2,25/13 13%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap 4°, $Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/13, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:00



EPPLER 2005 V. 8.5.07 RUN 20.12.23 18:



HQ/W-2,25/14, N=11

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:12



EPPLER 2005 V. 8.

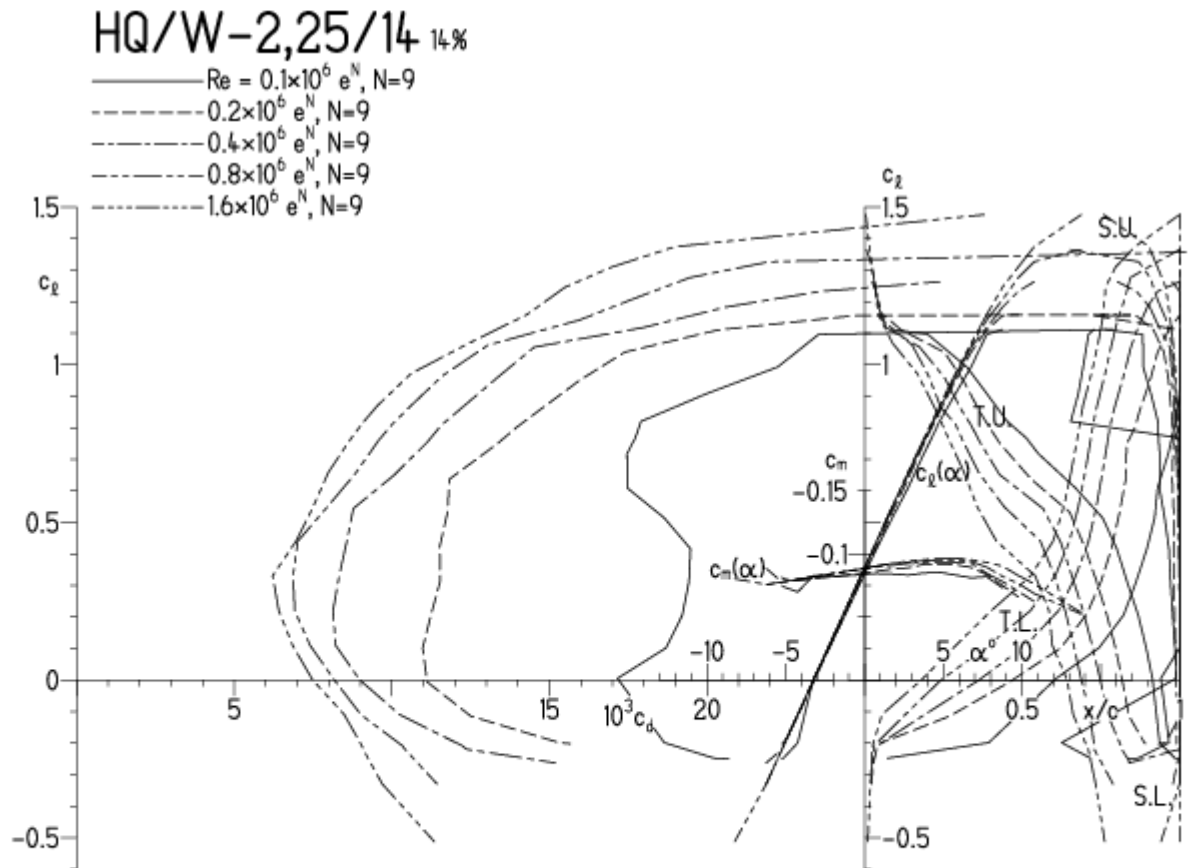


HQ/W-2,25/14, N=9

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:20



EPPLER 2005 V. 8.



HQ/W-2,25/14, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

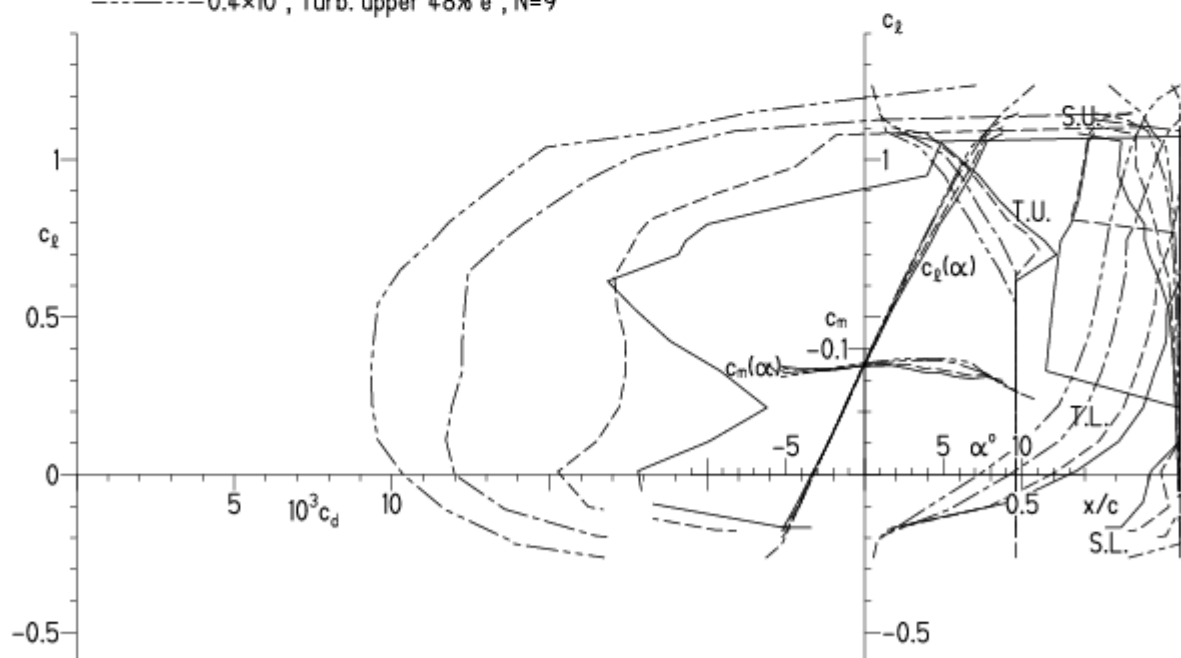
EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:29



EPPLER 2005 V. 8.5.07 RU

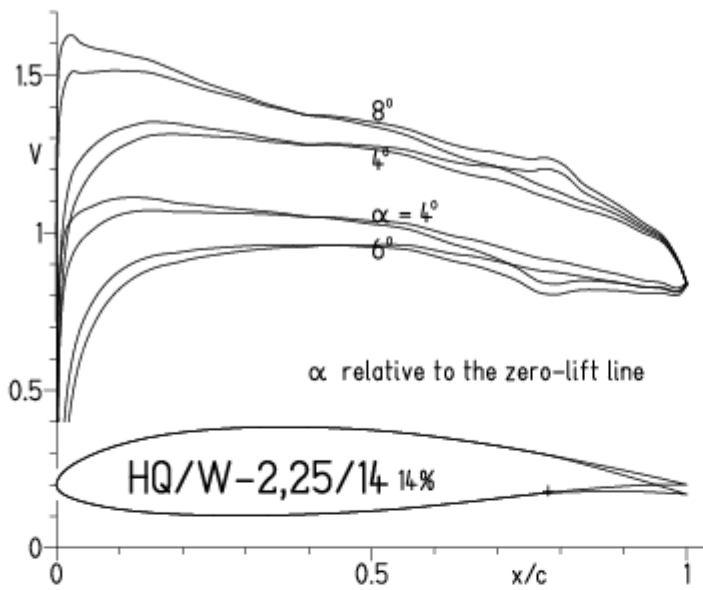
HQ/W-2,25/14 14%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$



HQW-2,25/14, N=9 mit +4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

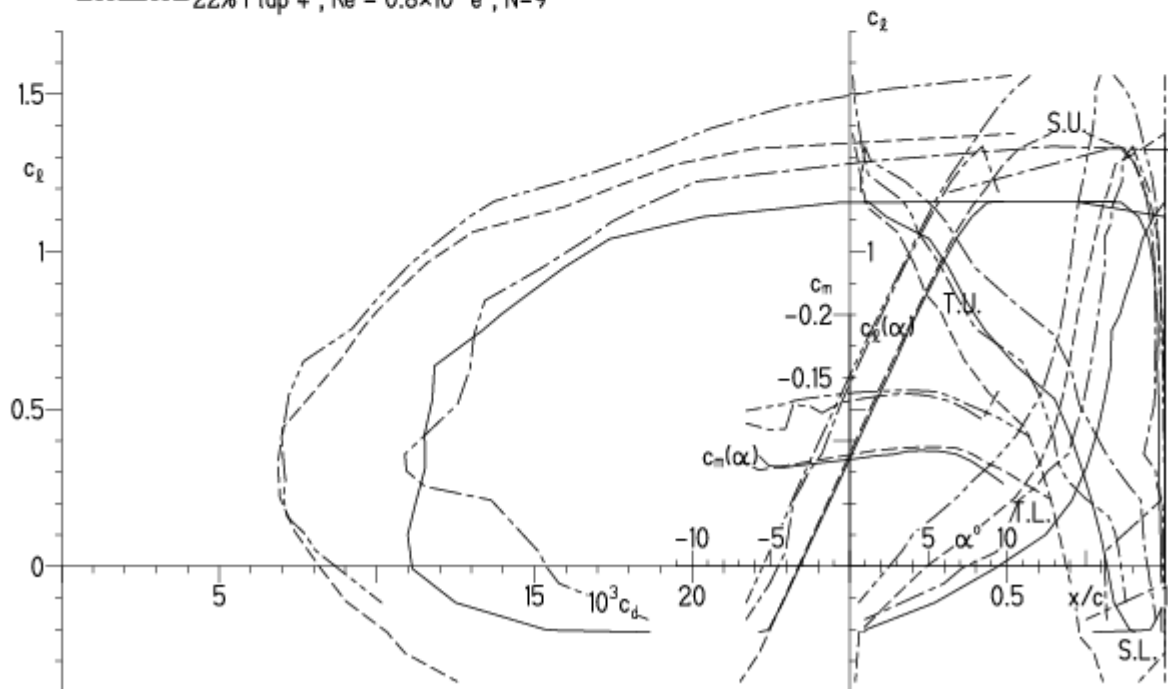


EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:56

HQ/W-2,25/14 14%

- $Re = 0.2 \times 10^6 e^N, N=9$
- - - $0.8 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.2 \times 10^6 e^N, N=9$
- · - · 22% Flap $4^\circ, Re = 0.8 \times 10^6 e^N, N=9$

- T. boundary layer transition
- S. boundary layer separation
- U. upper surface
- L. lower surface



HQW-2,25/14, N=9 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 21.12.23 17:51



EPPLER 2005 V. 8.5.07



HQ/W-2,25/15, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:31



EPPLER 20



HQ/W-2,25/15, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 11:25



EPPLER 2005 V. 8.5.07 RUN 22.12.23 11



HQ/W-2,25/15, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22:12:23 11:41



EPPLER 20

HQ/W-2,25/15 15%

- $Re = 75\,000$, Turb. upper 48% e^N , $N=9$
- - - 0.1×10^6 , Turb. upper 48% e^N , $N=9$
- · - 0.2×10^6 , Turb. upper 48% e^N , $N=9$
- - - 0.4×10^6 , Turb. upper 48% e^N , $N=9$

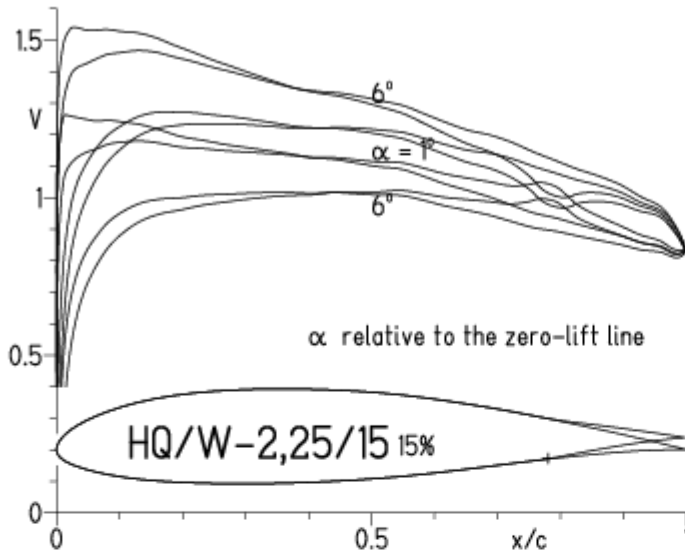


HQW-2,25/15, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/15, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:04

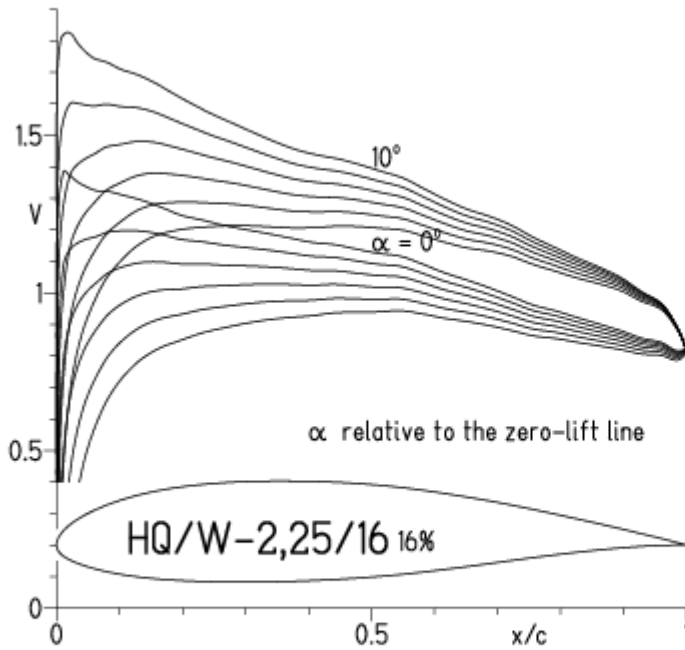


EPPLER 2005 V. 8.5.07 RUN 22:12:23 12:



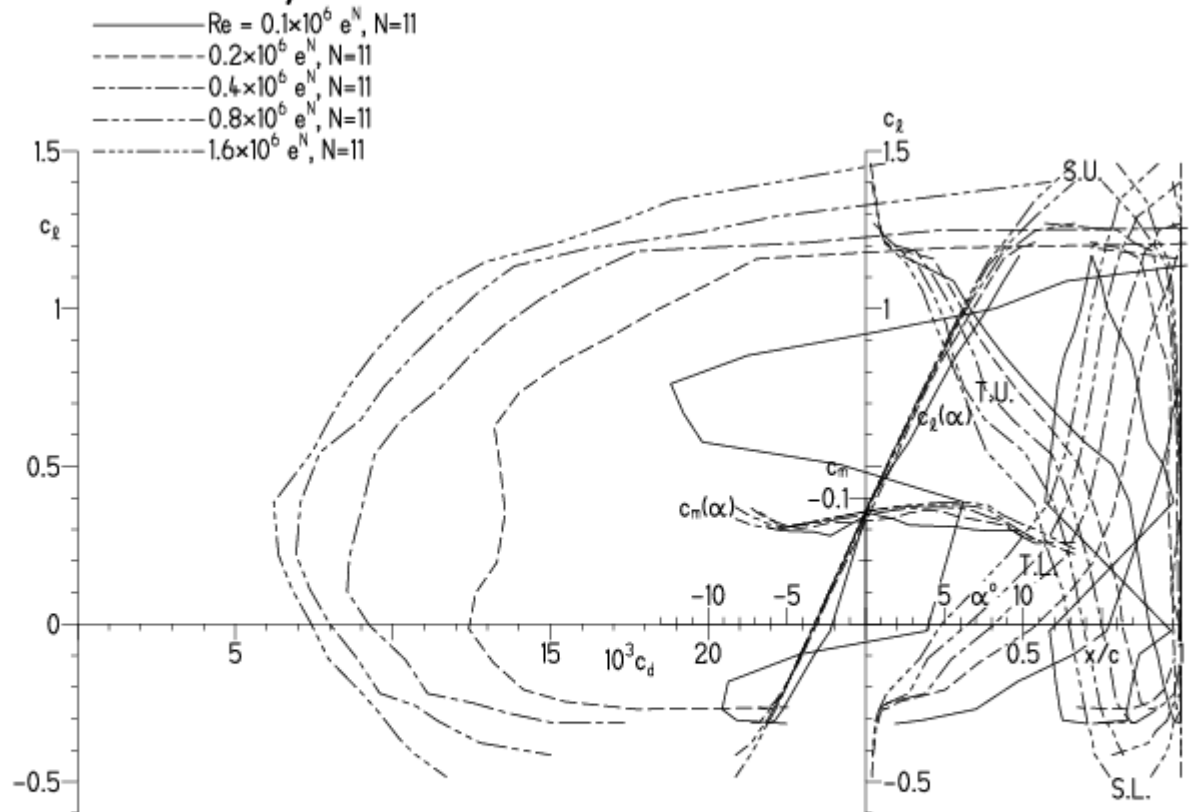
HQ/W-2,25/16, N=11

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:13



EPPLER 200

HQ/W-2,25/16 16%



HQ/W-2,25/16, N=9

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:21



EPPLER 200

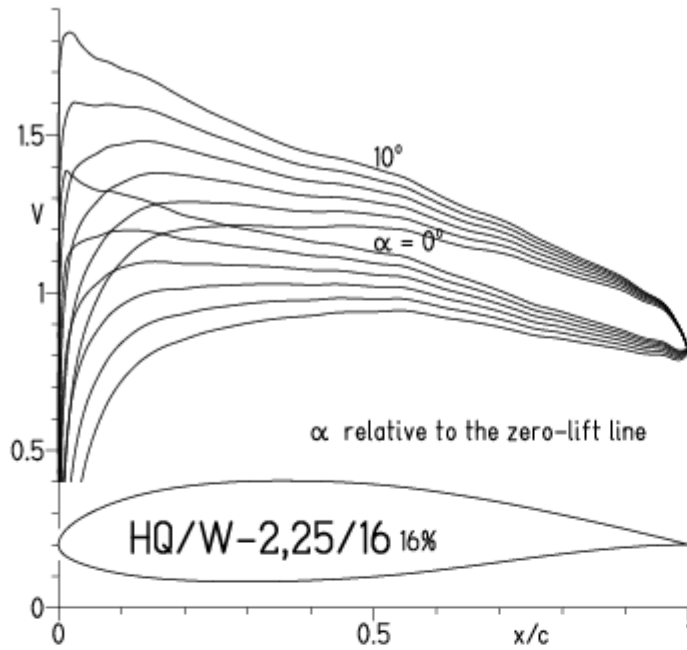
HQ/W-2,25/16 16%

- $Re = 0.1 \times 10^6 e^N, N=9$
- - - $0.2 \times 10^6 e^N, N=9$
- · - $0.4 \times 10^6 e^N, N=9$
- · - · $0.8 \times 10^6 e^N, N=9$
- · - · - $1.6 \times 10^6 e^N, N=9$



HQ/W-2,25/16, N=9, (Turbulatoreffekt (optimal beim Maximum der Wölbung))

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:30



EPPLER 2005 V. 8.5.07 R

HQ/W-2,25/16 16%

- Re = 75 000, Turb. upper 48% e^N , N=9
- - - 0.1×10^6 , Turb. upper 48% e^N , N=9
- · - 0.2×10^6 , Turb. upper 48% e^N , N=9
- - - 0.4×10^6 , Turb. upper 48% e^N , N=9



HQW-2,25/16, N=9 mit +4° Wölbklappenausschlag

Bringt keine merkliche Verbesserung im Langsamflug.

HQW-2,25/16, N=11 mit -4° Wölbklappenausschlag

EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41



EPPLER 2005 V. 8.5.07 RUN 22.12.23 12:41

